# The RE-Cycle System for Hog Waste Management

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18 processed in this unit. Ash mineral content is dependent upon the composition of the gasifier feedstock, but is

19 generally high in P, K, and Ca. Ash minerals are bioavailable and can be used as a mineral supplement in

- 20 animal feeds. Feeding trials have demonstrated the bioavailability of its mineral constituents. Mass balance data
- 21 *indicate good nutrient accountability.*

*Keywords.* swine housing, animal manure, gasification, waste nutrients, waste management,
 sustainable agriculture.

# 24 **INTRODUCTION**

1

The United States currently imports over 60% of its petroleum supply (EIA, 2004). The push toward energy independence and environmental sustainability has focused attention on biomass since it is renewable, widely available, and, unlike fossil fuels, makes no net contribution to greenhouse gas emissions (Gielen et al, 1998). It has been estimated that biomass could supply 56% of US gasoline needs (Riley, 2001), essentially replacing the imported oil. Animal wastes are a valuable source of

bioenergy and offer advantages such as continuous availability without long-term storage, energy
content comparable to other traditional sources such as wood, and low intrinsic value due to present
disposal costs.

33 Swine waste solids are 1 to 10 % dry matter (DM) under present harvesting methods (Smith et 34 al., 2000). Attempts to reduce the moisture content have focused on post-collection technologies such 35 as centrifuges, settling basins, and screen separators that generally have low solids recovery, leave a 36 problematic residual aqueous stream, and do not address the barn emissions that are responsible for 37 over 50% of the NH<sub>2</sub> emitted from hog farms (Doorn et al., 2002). Moreover these technologies suffer 38 from high investment costs for equipment, maintenance, and skills on the farm level (Westerman and 39 Bicudo, 2000). In order to capture energy from the solids, they must be sufficiently dry (50 to 70%) 40 DM) to permit cost effective transport and processing.

41 One promising method of capturing the energy of biomass is through gasification. This 42 oxygen-deprived, thermal decomposition technology converts biomass to low molecular weight 43 combustible gases and retains mineral nutrients in a sterile ash byproduct rich in P and Ca. In the 44 reducing atmosphere of the gasifier, N is converted to NH<sub>3</sub> that can be easily scrubbed from the 45 product gas stream. Given the low sulfur content of biomass, SO<sub>x</sub> emissions are far less than in coal-46 fired processes (Graham et al., 1996). The resulting product gas can be combusted to sustain the 47 gasification process and waste heat can be captured to heat buildings, generate steam, or provide power 48 through a Sterling engine. The non-odorous ash by-product can be cost-effectively transported for use 49 as a mineral supplement in animal feeds, as a fertilizer ingredient, or as a building materials

50 component.

The objective of the research presented here was to demonstrate a management strategy that would avoid the negative environmental consequences of hog production while capturing the energy and nutrients of waste in value-added products. The belt-based housing system is designed for separate collection of urine and feces and for improving the air quality in and emissions from hog buildings. The harvested solids have been processed through gasification to dispose of the waste and

recover valuable nutrients. Ash digestibility has been evaluated in vitro and in vivo. This approach
also allows for energy capture in the form of heat and steam.

# 58 **EXPERIMENTAL PROCEDURES**

59 The belt-based housing was modeled after a conventional grow-finish facility at 75% of full scale 60 (Figure 1). Pens were two-thirds solid floor, one-third slatted floor (tri-bar, Nooyen, Mt. Sterling, 61 KY). A high-density polyethylene (1 mm thick) belt conveyor system (Big Dutchman, Vechta, 62 Germany) was installed beneath the tri-bar. There were 5 pens with 16 pigs per pen (25-55 kg) at a stocking density of 0.63 m<sup>2</sup> pig<sup>-1</sup>. This is similar to the commercial stocking density of 0.4 to 0.7 m<sup>2</sup> 63 pig<sup>-1</sup> for pigs of 18 to 72 kg body weight (Meyer et al., 1991). The solid flooring had an 8% slope 64 allowing liquids to run off into the belt gutter. The 1° lengthwise slope of the belt, designed to mimic 65 the slope of a commercial building, insured that urine flowed continuously into an enclosed liquid 66 67 collection vessel at the end of the belt. Two different gutter designs, the "duct" design and the 68 "trough" design, were evaluated for odor and emissions reduction and for ease of cleaning. Animals 69 were fed a standard commercial diet and monitored for weight gain, feed and water intake, and waste 70 production. Ammonia and  $CH_4$  concentrations in the exhaust air from the belt housing facility were 71 determined by Fourier Transform Infrared Spectroscopy (FTIR) as described in van Kempen (2001). 72 Emissions were calculated, after subtraction of background levels in the input air, as the detected 73 differential concentration times the ventilation rate at the time of analysis. The detected differential 74 concentration was multiplied by the ventilation rate at the time of analysis to determine emission levels 75 over time. Materials harvested from the belt were characterized by proximate and ultimate analysis 76 (Hazen Research Laboratories), and mineral composition was determined in house by inductively 77 coupled plasma spectroscopy (ICP). Energy content was established by bomb calorimetry and dry matter determinations were calculated from weights before and after drying samples in a 60 °C oven 78 79 till weight change was less than 1% in a 24 h period.



Figure 1. Schematic diagram of the pen and belt layout as tested. The belt is positioned beneath the slats so that animals defecate most on the highest portion of the belt. Urine is allowed to run off into a gutter that continuously carries it out of the room, by gravity flow, into a closed container. The "duct" and "trough" gutter designs are shown in the expanded views of the boxed pen area.

64 Gasification employs heat and sub-stoichiometric amounts of oxygen to break down, or crack, the 65 feedstock into carbon monoxide and hydrogen gases, as well as other low molecular weight gases. The 76 idealized, general equation (Reed and Gaur, 1999) is:

87

88 (1) 
$$CH_{14}O_{0.6} + 0.35 O_2 \rightarrow 0.4 CO + 0.6 H_2 + 0.4 CO_2 + 0.1 H_2O + 0.2 C$$

89

90 For biomass, temperatures are generally held below 1000 °C to avoid agglomeration within the ash 91 bed. Gasification studies were conducted in a Brookes Gasification Process (BGP) gasifier. This is a 92 batch-fed, indirectly heated, staged-combustion gasifier selected for its simplicity and ease of operation 93 (Figure 2). At start-up, the burner in the secondary chamber combusts propane to heat the firebrick 94 and, indirectly, the primary chamber containing the feedstock. At temperatures of 600 to 900 °C, 95 biomass feedstock is cracked into low molecular weight gases that are then drawn into the secondary 96 chamber where they are combusted to sustain the process. Ash is removed after completion of the feedstock processing. Combustion gases exit the flue along with waste heat. Gases in the two 97

98 chambers and the flue are monitored at 15 minute intervals to evaluate temperature,  $NO_x$ ,  $SO_2$ , CO,

99 CO<sub>2</sub>, and O<sub>2</sub> levels using a combustion meter (Kane May Instruments). Temperature and oxygen

100 availability can be controlled during the reaction. This control and the static nature of the system result

- 101 in a clean process that meets both European and Californian emission standards without requiring gas
- 102 cleanup.



103Figure 2. Schematic of the Brookes Gasification Process gasifier. Heat from the burner in the secondary104chamber heats the primary chamber containing the feedstock. Gases from the feedstock are drawn into the105combustion chamber to sustain the reaction.

106 **RESULTS AND DISCUSSION** 

# 107 BELT OPERATION, PIG PERFORMANCE, AND EXCRETA PROPERTIES

- 108 Belt operating variables were evaluated in the first two experiments in order to optimize
- 109 performance. Prior to data collection, it was hypothesized that the DM content would increase
- 110 with belt residence time; this was evaluated in Exp. 1. DM content of the recovered solids
- 111 was found to decrease after 30 h of belt residence time (data not shown). Apparently, when

112 solids remained on the belt for greater than 30 h, the increased fecal load trapped more of the 113 urine thereby reducing the DM content. Collection time-of-day was examined in Exp. 2 by harvesting 114 waste solids at a 27-hour interval with 3 replicates of each time-of-day. A sigmoidal DM pattern was observed (Figure 3). Collections at 06:00 resulted in a  $9.8 \pm 5.0\%$  DM increase over collections at 115 116 15:00. The diurnal activity pattern of the pigs probably produced this result since animals eliminate 117 less at night when they are resting and more when they first eat and become active in the morning. In 118 all subsequent experiments, the belt contents were harvested every 24 hours at 06:00 resulting in an 119 average DM content of  $49 \pm 4\%$  (TABLE 1). At this DM content, swine feces typically have a brittle, 120 dry appearance externally with a moist core present in larger pieces. It does not clump or pack during 121 handling and it has minimal odor.



Figure 3. Effect of collection time-of-day on feces DM content. Belt residence time was constant at 27
 h and each time-of-day was evaluated in triplicate.

- 124 TABLE 1. Experimental parameters and animal performance for five trials designed to evaluate a housing system
- 125 employing a belt for harvesting urine and feces separately. Data are expressed on a per animal basis, except as
- 126 indicated.

Trial date and Number	Aug 01	Jan 02	Mar 02	Oct 02	Apr 03	Mar 02	Mean $\pm$ SE
	1	2	3	4	5	3	
						Ref.	
N, number of animals	100	80	80	80	80	80	
Avg. T, °C	28	30	26	22	25		$26 \pm 3$
Avg. humidity, %	66	54	52	64	64		$60 \pm 5$
Gutter design	duct	duct	duct	trough	trough	none	
Ave. Wts, in - out, kg	23-57	27-55	23-51	30-57	32-56	24-53	
ADG, kg·d-1	0.79	0.76	0.82	0.97	0.83	0.83	$0.83\pm0.07$
ADFI, kg·d-1	1.54	1.52	1.72	1.96	1.73	1.84	$1.69\pm0.16$
Gain/Feed	0.51	0.50	0.48a	0.48	0.51	0.45b	$0.50\pm0.02$
Fecal output, kg DM·d-1	0.23	0.26	0.22	0.34	0.26	ND	$0.26\pm0.04$
Fecal DM as coll'd, %	§	52	54	43	46	ND	$49 \pm 4$
Urine output, L·d-1	ND	1.05	1.54	1.27	1.42	ND	$1.32\pm0.19$
NH3 emission, kg·y-1,c	1.08	0.80	0.84	1.20	1.24	ND	$1.03\pm0.18$
CH4 emission, kg·y-1	1.27	1.06	0.75	1.39	0.76	ND	$1.05\pm0.26$

Collected feces indicate a fecal DM production of  $0.26 \pm 0.05 \text{ kg} \cdot \text{pig}^{-1} \cdot \text{day}^{-1}$  (TABLE 1), similar 127 to the 0.27 kg reported by Smith et al. (2000) for the grower pig. Absolute levels of NH<sub>3</sub> emissions 128 averaged  $1.0 \pm 0.2$  kg NH<sub>3</sub>·pig<sup>-1</sup>·y<sup>-1</sup> over the five experiments (TABLE 1). This suggests a 73% 129 reduction from the literature value of 3.7 kg  $NH_3$   $\cdot pig^{-1}$  y<sup>-1</sup> for conventional barns (Doorn et al., 2002). 130 131 The low levels of NH, are attributed to the minimal contact time between urea and the fecal microbes 132 that metabolize it to NH<sub>3</sub> and CO<sub>2</sub> (Rom, 1995) and to the rapid sequestering of the urine in closed containers. Emissions of CH<sub>4</sub>, a potent greenhouse gas, were only  $1.05 \pm 0.26$  kg CH<sub>4</sub>  $\cdot$  pig<sup>-1</sup>  $\cdot$  y<sup>-1</sup>. 133 134 The gutter design was altered between Exp. 3 and 4 and this may have impacted NH<sub>3</sub> emissions and solids DM. NH, emissions and DM content were 1.22 kg NH, pig<sup>-1</sup>y<sup>-1</sup> and 45% DM 135 with the trough design, but 0.91 kg NH<sub>2</sub>·pig<sup>-1</sup>·y<sup>-1</sup> and 53% DM with the duct design. This could be 136 137 attributable to the gutter design or to the higher average temperatures and lower average humidity in 138 Exp. 2 and 3 (duct gutter) relative to Exp. 4 and 5 (trough gutter). The trough design does offer some 139 unique advantages, namely: it occupies less space and so facilitates retrofits, and it is cleaned each time 140 the belt is operated. Addition of a cover to the trough design could limit airflow across the urine and 141 might help to further reduce NH, emissions from the trough gutter, if indeed the gutter is responsible 142 for the changes noted.

143 Animal performance was evaluated in each of the trials (TABLE 1). The average daily feed 144 intake (ADFI) was  $1.69 \pm 0.18 \text{ kg} \cdot \text{pig}^{-1} \cdot \text{d}^{-1}$  and average daily gain (ADG) was  $0.83 \pm 0.08 \text{ kg} \cdot \text{pig}^{-1} \cdot \text{d}^{-1}$ . 145 The gain to feed ratios (G/F) averaged  $0.50 \pm 0.02$  across the five belt-based housing trials. In Exp. 3, 146 where performance in the belt-based housing was compared to that in conventional flush system barns, 147 there was a significant improvement in the G/F ratio of 5.5% (P = 0.01) for the belt-based animals 148 despite the fact that housing density, diet, and animals were matched. Experiments 1, 2, 4 and 5 149 combined yielded an 11% improvement in feed efficiency when compared to the Exp. 3-Reference or 150 to other trials carried out in the conventional housing system. The reference farm had a lower group size (7 animals pen<sup>-1</sup> compared to 16 animals pen<sup>-1</sup> in the belt-based facility) necessitated by the desire 151 152 to match housing density despite different pen sizes. Group size has been shown not to impact the G/F 153 ratio, although larger groups may reduce both FI and growth rate (Hyun and Ellis, 2001; Wolter et al., 154 2001). Housing environment, however, has been shown to impact pig health and productivity 155 (Donham, 1991). The source of the G/F improvement requires further investigation, but may be due to 156 improvements in air quality resulting from the separate collection of urine and feces. If these 157 improvements are indeed attributable to the housing design, then the belt-based system could result in 158 substantial feed cost savings to producers.

159 The nutrient loads for various inputs and outputs of the RE-Cycle system were calculated based 160 on consumption and production data for feed and wastes as well as nutrient concentration data for all 161 streams under investigation (TABLE 2). Data for accretion calculations were from Mahan and Shields 162 (1998) for the weight pigs used in our studies. The feed nutrients recovered in the various waste 163 streams plus those calculated as accreted by the animal, show good closure with the nutrients present in 164 the feed consumed. For N, P, K, and Ca, the percent closure is close to or exceeds 90%. For Mg, the 165 lack of accretion data limits conclusions, but the fact that there is 75% accountability in the absence of 166 accretion data is very promising. For Cu and Zn, however, the situation is just the reverse; it seems 167 that more of these nutrients have been recovered than were provided to the animals. Perhaps some 168 copper could have been added through contact of the drinking water with copper pipes. Both of these 169 elements, though, are in very low abundance making it more difficult to segregate the mineral 170 analytical response from the background noise. It is thought that the results shown for Cu and Zn in 171 feces are an overestimation of the amount present and this is probably due to analytical error.

172 TABLE 2. Nutrient closure from the belt-based housing system.

Component	Intake/Output	Energy	Mineral			Nu	trients per	pig per d	ay		
	g DM/pig/d	kJ/pig/d	%	units	Ν	Р	К	Ca	Mg	Cu	Zn
IN Feed	1690	29925		g/pig/d	49.1	10.8	13.4	12	2.7	0.038	0.259
OUT Feces Urine NH <sub>3</sub> Emissions Accretion	260 1320	5319	12 - 15	g/pig/d g/pig/d g/pig/d g/pig/d	10.5 9.2 2.4 21.04	5.1 0.2 3.99	5.1 6.1 0.632	4.9 0.1 6.79	2 0.0 UNK	0.037 0.01 0.001	0.540 0.02 0.01
OUT / IN				%	87.9	86.0	88.3	98.3	74.7	126.4	220.3

173

#### **GASIFICATION OF SWINE MANURE SOLIDS**

174 Prior to gasification, swine waste solids were analyzed for DM, energy, mineral content, and ash 175 fusion temperature in an effort to understand the probable operating conditions required by this 176 feedstock. At 19.7 MJ/kg DM, swine waste compares favorably with wood (20.2 MJ/kg DM) from an 177 energy standpoint. Waste solids were 45% C, 0.4 % S, and 0.3% C<sup>1</sup>. Fixed C was 13%; volatile 178 matter, 75%; and ash, 12.2%. The lowest temperature for ash fluidization, seen under oxidizing 179 conditions, was 1218 °C so processing temperatures less than 1000 °C were not expected to cause ash 180 agglomeration problems.

181 The static system of the BGP gasifier makes it ideal for a wide variety of feedstocks since 182 virtually anything can be loaded into an open cavity for a batch feed reaction. In addition to the swine 183 waste feedstock, the gasifier has thus far processed nursery pig mortalities, poultry litter, chicken and 184 turkey mortalities. Ashes from swine waste solids and poultry litter were compared to the ashes 185 obtained by incinerating pig mortalities (Prestage Farms, grower/finisher, G/F) and by gasifying turkey 186 litter (Energy Products of Idaho), TABLE 3. The data were corrected to an ash only basis for purposes 187 of comparison. High levels of Ca are found in mortality ash in keeping with the bone content of this 188 feedstock. The elevated Cu levels in turkey litter ash may result from dietary levels of this mineral. In 189 short, differences in the ash mineral compositions appear to result from differences in the feedstock 190 rather than from differences in the processing technologies.

Alterna	tive Feedstocks	Corrected to 100% ash-expressed on "ash only" basis								
			C	%		pp	ppm			
Туре	Source	Р	K	Ca	Mg	Zn	Cu			
Hog waste	Ash, gasifier NCSU-BGP	14.34	11.34	16.05	4.97	9044.5	619.4			
Chicken litter	Ash, gasifier NCSU-BGP	4.7	4.0	23.3	1.1	0.1	0.02			
swine mortalities	Ash, incinerator Prestage G/F	17.45	5.49	27.40	1.22	945.2	480.1			
Turkey litter	Ash, gasifier EPI	6.15	3.38	9.76	1.98	586.5	1443.1			

192 TABLE 3. Comparison of ashes from different feedstocks and from various thermochemical processing technologies.

193

194	Experiments with a pilot-scale gasifier (~70 kg per batch), on loan from BGP, have confirmed its
195	ease of operation. One load can be processed in 3 to 4 h providing a 20 kg/h through-put with this
196	demonstration unit. In order to determine the optimal operating temperature, two trials were performed
197	each day at each temperature ranging from 700°C to 900°C (Table 4). The second trial of each day is
198	reported here in order to compare "steady-state" conditions. From these trials, 800°C was selected as
199	the standard operating temperature since it balanced residence time with propane usage and provided
200	sufficient temperature to guarantee sterile ash and minimal dioxin formation. Since the BGP gasifier is
201	designed to consume its product gases, the only available energy output is heat from the flue stack. We
202	do not currently have the ability to use this energy, but this heat could be used for steam generation,
203	hot water, heating animal barns, or any other process that needs a high heat source.

204

TABLE 4	Effect of operating	o temnerature on	feedstock nr	ocessing time	and nronane use
I ADLL T.	Effect of operating	g temperature on	iccustock pro	occosing time	and propane use.

Set Temperature	700	750	800	850	900
Feedstock: expired pelleted	70 kg at 73% DM				
Teed	2.5	2.05	2.05	2.05	2.75
Total time, h	3.5	3.25	3.25	3.25	3.75
Total Propane used, cf	85.5	81.9	87.6	96.6	118.3
PC, max, °C	1003	1033	1035	1047	1028

205

There are several factors that influence the efficiency of the BGP unit. The feedstock type, DM, feedstock load, and whether the unit was in steady state operation. Data from processing pig mortalities indicate that propane use in a cold start experiment is 3 times that when the unit has been preheated (28.4 cf propane /kg 100% DM feedstock when cold and 9.5 cf propane when preheated). 210 Recovery of fecal nutrients in BGP gasifier ash has also been evaluated with good results. Gasifying concentrates these nutrients into a mass that is only 17% of the initial feedstock mass (from 211 260 g manure solids to 44 g pig<sup>-1</sup>  $\cdot$  d<sup>-1</sup>. The reduced mass has obvious advantages for transport of these 212 213 nutrients to areas deficient in them. With the exception of Cu and Zn, mineral recoveries were generally in the 80 to 110% range. The Cu and Zn results again suggest that the fecal values obtained 214 for these minerals are spurious. Artificially high fecal values would result in greater than 100% 215 216 recovery when feces are compared to feed, and substantially lower than expected recovery when ash is 217 compared to feces.

218

	219	TABLE 3.	Nutrient	balance fro	om gasification	of swine	waste solids
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Component	Intake/Output	Energy	Mineral Ash	Nutrients per pig per dav							
	g DM/pig/d	kJ/pig/d	%	units	Ν	Р	Κ	Ca	Mg	Cu	Zn
Feedstock IN Feces	260	5319	12 – 15	g/pig/d	10.5	5 1	5 1	4.0	2	0.03	0.54
PDOCESSED					10.5	5.1	5.1	4.9	2	/	0
Ash <sup>α</sup>	44	612	85	g/pig/d	ND	4.8	4.0	5.3	1.7	0.02	0.29
ASH / FEEDSTOCK				% Closure		94.5	78.3	108.1	84.2	65.6	54.3

<sup>220</sup> 

Prior to generating sufficient gasifier ash in house, preliminary digestibility trials were conducted 221 222 with gasified swine waste solids from the EPI process. In vitro solubilities serve to predict 223 bioavailability and are determined by the extent to which ash minerals are soluble in an aqueous 224 solution of HCl at pH 2 (Figure 5). P, K, Ca, and Mg were monitored and all these minerals were very 225 soluble under the conditions described. In vivo, digestibility was determined with 7 pigs in a crossover design. Animals were fed 80g/kg<sup>0.75</sup> per day of a highly purified (low mineral) cornstarch-casein diet 226 227 supplemented with either ash or a mineral mix based on monocalcium phosphate, limestone, KOH, 228 magnesium acetate, HCl, and salt. After 5 days of adaptation, feces were collected quantitatively for 3 229 days before the crossover and repeat. Digestibility was determined as the difference between total 230 intake and total fecal excretion for each nutrient studied. While palatability was a problem, the 231 absorption data indicate that ash minerals are bioavailable and digestibility (Figure 5). Two problems occurred in this preliminary trial: phosphorus was inadvertently over-formulated in the test diet (due to 232

- 233 inaccurate analytical results) and an inappropriate, non-digestible source (MgSO<sub>4</sub>) was used in
- thecontrol diet. A full scale trial is planned to better confirm digestibility data, pig performance, and
- pig health when fed ash as a mineral supplement throughout the grow/finish period.



236 237

238 NO, levels were monitored in the secondary chamber and the flue stack to determine the extent of 239 these emissions to the environment. Flue stack gases are most relevant to environmental impact, but 240 vary with damper opening so that measurements from the secondary chamber were used to follow 241 reaction progress. NO, levels in the flue ranged from 2 to 20 ppm. NO, is elevated initially, but decreases after 3 hours of processing as feedstock is reduced to carbon char and mineral ash. 242 243 Preliminary tests have been conducted to determine the effect of injecting liquid waste into the BGP 244 gasifier secondary chamber to reduce NO<sub>2</sub> levels in flue gas as predicted by Pulkrabek (1997). Data 245 obtained were very encouraging since NO<sub>x</sub> levels were reduced from over 340 ppm to less than 80 246 ppm. However, no measure of flue ammonia levels was available during this process, and further 247 testing is required before the exact impact of the procedure can be described. For this reason, the fate 248 of nitrogen has not yet been well characterized throughout the system.

249 **C** 

# **CONCLUSION AND FUTURE DIRECTIONS**

Belt-based housing holds promise for reducing emissions from hog buildings, improving pig
performance, and facilitating waste nutrient transport to areas of need. Improved feed efficiency may
help to improve producers' profitability. The solid material recovered from the belt is ~50% DM and

253 suitable for gasification. A commercial-scale belt installation is a vital component for verifying the 254 benefits observed with the demonstration unit and for supplying sufficient waste to operate the gasifier 255 over extended periods. The BGP gasifier is easy to operate, completely disposes of bioactive 256 molecules and pathogens, and offers the potential of recovering energy from waste heat. The residual ash retains valuable nutrients, such as P, K, and Mg, that can replace mined mineral supplements in 257 258 feed or be part of a fertilizer blend. More work must be done to optimize the gasification process and 259 reduce secondary fuel use. A continuous feed gasifier is currently under development; it will be 260 operated under steady state conditions which is expected to dramatically enhance efficiency. Addition 261 of steam reforming and product gas capture to the new design will make it possible to modify the 262 product gas composition and recover it for synthesis of biofuels.

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