

Progress toward Developing a Durable High-Temperature Solar Selective Coating



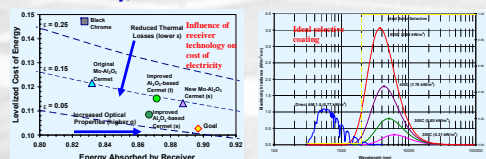
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1. Abstract

Increasing the operating temperature of parabolic trough solar fields from 400°C to >450°C will increase their efficiency and reduce the cost of electricity. Current coatings do not have the stability and performance necessary to move to higher operating temperatures. The objective is to develop new, more-efficient selective coatings with both high solar absorptance ($\alpha > 0.96$) and low thermal emittance ($\epsilon < 0.07$) that are thermally stable above 450°C, ideally in air, with improved durability and manufacturability, and reduced cost.



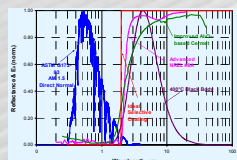
5. Optical Modeling

Modeled solar-selective coatings with $\alpha=0.959$ and $\epsilon=0.061$ that meet CSP goals

Emittance excellent & absorptance of modeled coatings is very good but further improvements are expected.

- Plan to model:
 - Error analysis
 - Measured properties
 - Cermet
 - Material selection properties (Ashby type diagrams)

	Original Mo-Al ₂ O ₃ Cermet	Improved Al ₂ O ₃ based Cermet	NREL #6A
Solar α	0.938	0.954	0.959
Thermal ϵ @			
25°C	0.061	0.052	0.027
100°C	0.077	0.067	0.033
200°C	0.095	0.085	0.040
300°C	0.118	0.107	0.048
400°C	0.146	0.134	0.061
450°C	0.162	0.149	0.070
500°C	0.179	0.165	0.082



Ideal, commercial, and modeled selective coating

8. Selective Coating Performance

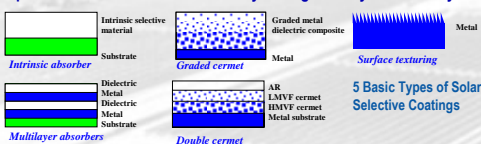
Actual performance of the absorber at high temperatures commonly does not correspond to the calculated ϵ

- Small errors in p lead to large errors in ϵ
- ϵ is a surface property & depends on surface condition of material & substrate
 - Surface roughness
 - Surface film
 - Oxide layers
- Selective coatings can degrade at high T due to
 - Thermal load (oxidation)
 - High humidity or water condensation on the absorber surface (hydration & hydrolysis)
 - Atmospheric corrosion (pollution)
- Diffusion processes (inter-layer substitution)
 - Chemical reactions
 - Poor interlayer adhesion

Therefore it is important that p is measured accurately & to measure ϵ of the selective coating at operating temperatures & conditions before using calculated ϵ ⇒ Round robin test

2. Technical Approach

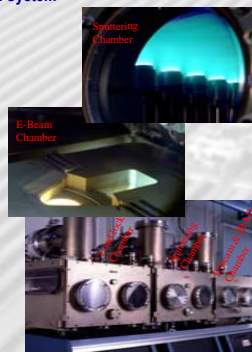
- Review literature to determine potential high-temperature oxidation-resistant solar selective coatings
- Use modeling software to optically model solar-selective designs or refine existing ones and extract optical constants used in the design.
- Develop modeled high-temperature solar-selective coatings using physical vapor deposition (PVD).
- Characterize material and optical properties, perform high-temperature optical characterization and durability testing to verify functionality.



6. Deposition Capabilities

Pernicka Three-Chamber Deposition System

- Load-Lock Chamber
- Pulsed DC Sputtering Chamber
 - 2- 3"x12" Linear Magneton Cathode (or)
 - 3- Linear arrays of 5-1.5" Mini-Mak Guns
 - Pulsed DC Power Supply
- Electron-Beam Chamber
 - Multi-Pocket (6) E-Beam Source (or)
 - Co-deposition plate w/ 2 single e-beam sources
- IBAD w/ 12" Linear Ion Gun
- System
 - Turbo molecular drag pumps
 - 2x10⁻⁶ torr
 - 12" x 12" ambient or heated substrate
- Co-deposition
- Monitoring
 - Residual gas analysis (RGA)
 - Quartz Crystal Monitor
 - Pressure/Gas
 - 4 Reactive Gases
 - Computer



3. Literature Review

Candidate High-temperature >400°C Solar Selective Coatings

- Graded Mo,W, ZrB, Pt- Al₂O₃ cermets
- Si tandem absorber
- Black Co, Mo,W
- Double cermets- SS-AlN, AlN/Mo, or AlN/W
- 4-layer V-Al₂O₃, W-Al₂O₃, Cr-Al₂O₃, Co-SiO₂, Cr-SiO₂, Ni-SiO₂
- Double AR
- Multilayers; Al-AlN_x-AlN
- Au/TiO₂ cermet
- ZrC_xN_y/Ag
- Ti_{1-x}Al_xN
- Quasicrystals multilayers & cermets
- Surface Texturing

7. Prototype Development

Key issue then becomes trying to make the coating — prototype development underway

- Initial prototype by compound evaporation
 - Individual layers and characterization completed
 - Preliminary runs of compound multi-layer deposited & optical properties characterized
 - XPS showed compound evaporation produced layered stoichiometry
- Despite depositing layers with over- and under-thickness and compound layered structure, the optical performance of the prototype NREL#6A was quite encouraging.
- Need to codeposit materials
- Required significant upgrade to equipment
 - Installed codeposition guns & sweeps
 - Pneumatic shutters
 - Second quartz crystal sensor
 - Upgrade computer & RGA software
 - Upgrade Gas control system
 - Plus upgrade of associated air, water, electrical, & control systems
 - Installed e-beam base plate lift (safety concerns)

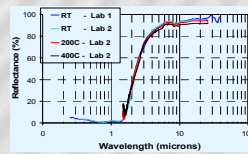
4. Oxidation Resistant Properties

Desirable Properties for stable coating in air > 400°C

- High thermal & structural stabilities for combined & individual layers
 - Elevated melting points
 - Large negative free energies of formation
 - Materials that form a multicomponent oxide scale
 - Single-compound formation
 - Lack of phase transformations at elevated temperature
- Suitable texture to drive nucleation, subsequent growth of layers with suitable morphology
 - Stable nanocrystalline or amorphous materials
- Excellent adhesion between the substrate and the adjacent layers
- Enhanced resistance to thermal and mechanical stresses
 - Acceptable thermal and electrical conductivities
 - Higher-conductivity materials have improved thermal shock resistance
 - Some ductility at room temperature reduces thermal-stress failures
- Good continuity and conformability over the tube
- Compatibility with fabrication techniques

9. Round Robin Testing

- 4 Commercial Coatings
 - Black Ni, Mo-cermet, UVAC A & B
- 3 Laboratories
 - 2 commercial
 - NREL
- Preliminary Results
 - Room Temperature (RT) measurements within error of 400°C measurements
 - 2 Commercial laboratories give comparable RT results
 - NREL near-IR more noisy



Comparison of UVAC reflectance measurements made at two laboratories and at low- and high-temperature.

⇒ Purchased IR spectrophotometer & NIST traceable standards

10. Thermal Stability

- Thermal stability is sometimes given based on the thermal properties of the individual materials or the processing temperature parameters
- Actual durability data is uncommon for high temperature absorber coatings
- Durability or thermal stability is typically tested by heating the selective coating, typically in a vacuum oven but sometimes in air, for a relatively short duration (100's of hours) compared with the desired lifetime (5-30 years)
 - IEA Task X performance criterion (PC) developed for flat plate collector absorber testing (i.e., non-concentrating, 1-2X sunlight intensity)
 - No analogous criterion known for testing high-temperature selective coatings for CSP applications
- Building capability for long term testing of thermal stability
 - Purchased & installed high-temperature (600°C) Inert Gas Oven

11. Accomplishments

- Using computer-aided optical design software, a solar selective coating exceeding the goals has been modeled. A solar selective coating with $\alpha = 0.959$ and $\epsilon = 0.061$ at 400°C composed of materials with high-temperature stability has been modeled. This exceeds the goal specification by about 1% overall, because 1% in emittance equates to about 1.2% in absorptance.
- Initial prototype deposited by compound e-beam evaporation & characterized showed need to codeposit modeled structure.
- System upgraded significantly to perform codeposition.
- Codeposition of prototype showed stoichiometry of reflective layer important. Working to determine correct stoichiometry of reflective layer and to deposit coating without thickness errors.
- Round robin test performed, preliminary data analysis completed. Data analysis and report needs to be completed
- Upgraded testing and durability capabilities with purchase of IR spectrophotometer & standards, and high-temperature inert gas oven.
- Patent being pursued.