

Time for World Class Solutions

Advanced Thermoelectric Power System Investigations for
Light-Duty / Heavy-Duty Vehicle Applications
21st International Conference On Thermoelectrics
Long Beach, CA
28 August 2002



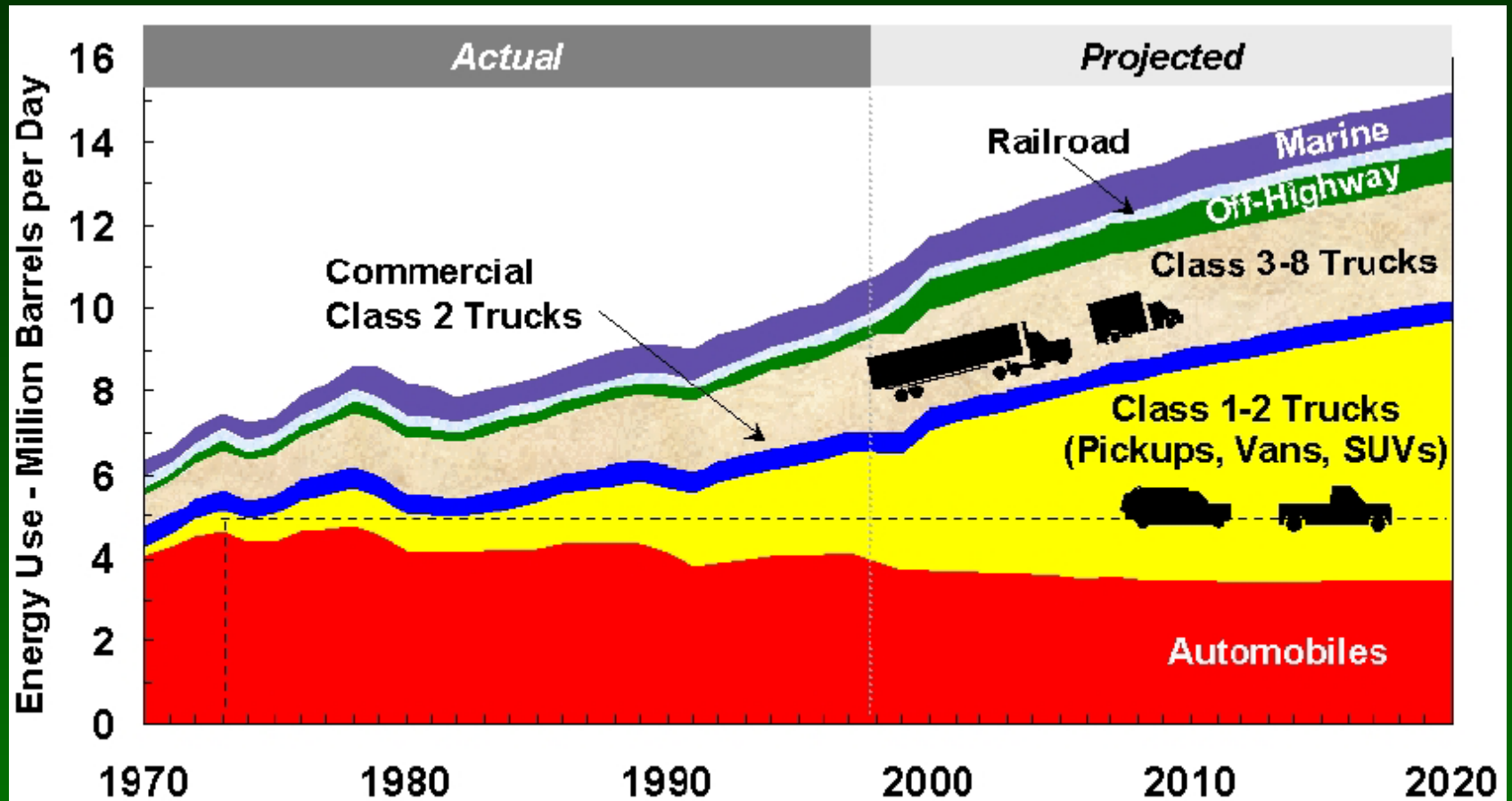
U.S. Department of Energy's National Renewable Energy Laboratory

Terry J. Hendricks, Ph.D., P.E., AHHPS Field Technology Manager

Jason Lustbader

CENTER FOR TRANSPORTATION TECHNOLOGIES AND SYSTEMS

Breakdown of US Historical and Projected Fuel Use by Platform



Sources: EIA Annual Energy Outlook 2000, DOE/EIA-0383(2000), December 1999
Transportation Energy Data Book: Edition 20, DOE/ORNL-6959, October 2000

National Impacts

- Creates Serious National Economic Issues
- Complicates Almost Every Political Issue & Landscape
- And

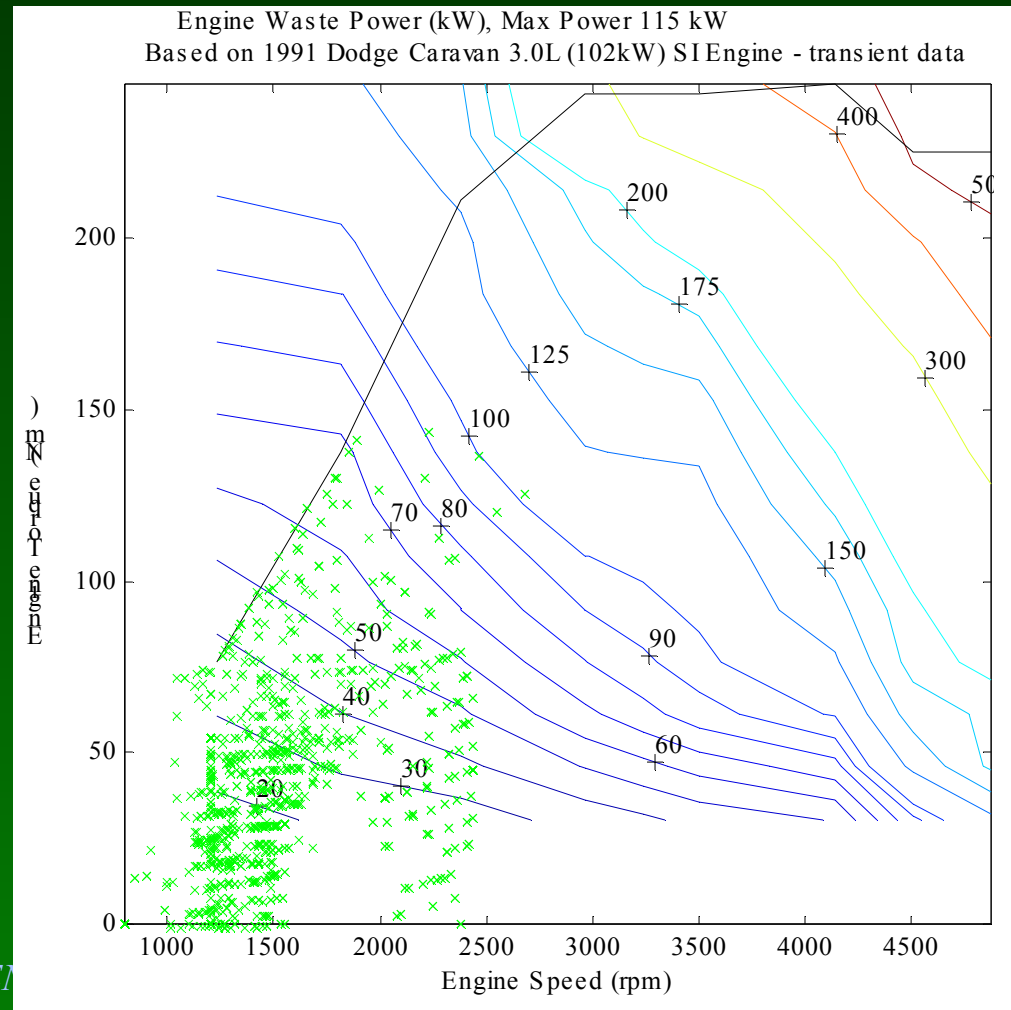
Continuing National Security Issue



- We Do This to Ourselves & There Is No Need To

Waste Power Available in Representative 115 kW Engine

- 20-400 kW Waste Power Available Across The Engine Map
- Average of 23 kW Over an FTP Drive Cycle



Objective

Low Grade Thermal
Energy From Various
Automotive Systems



High Grade Electrical
Energy To Operate
Various Automotive Systems

- Relatively Low Cost
- Passive System
 - No Noise
 - No Vibration
- High Reliability
- Ideally No Fluids

Advanced Thermoelectric Systems

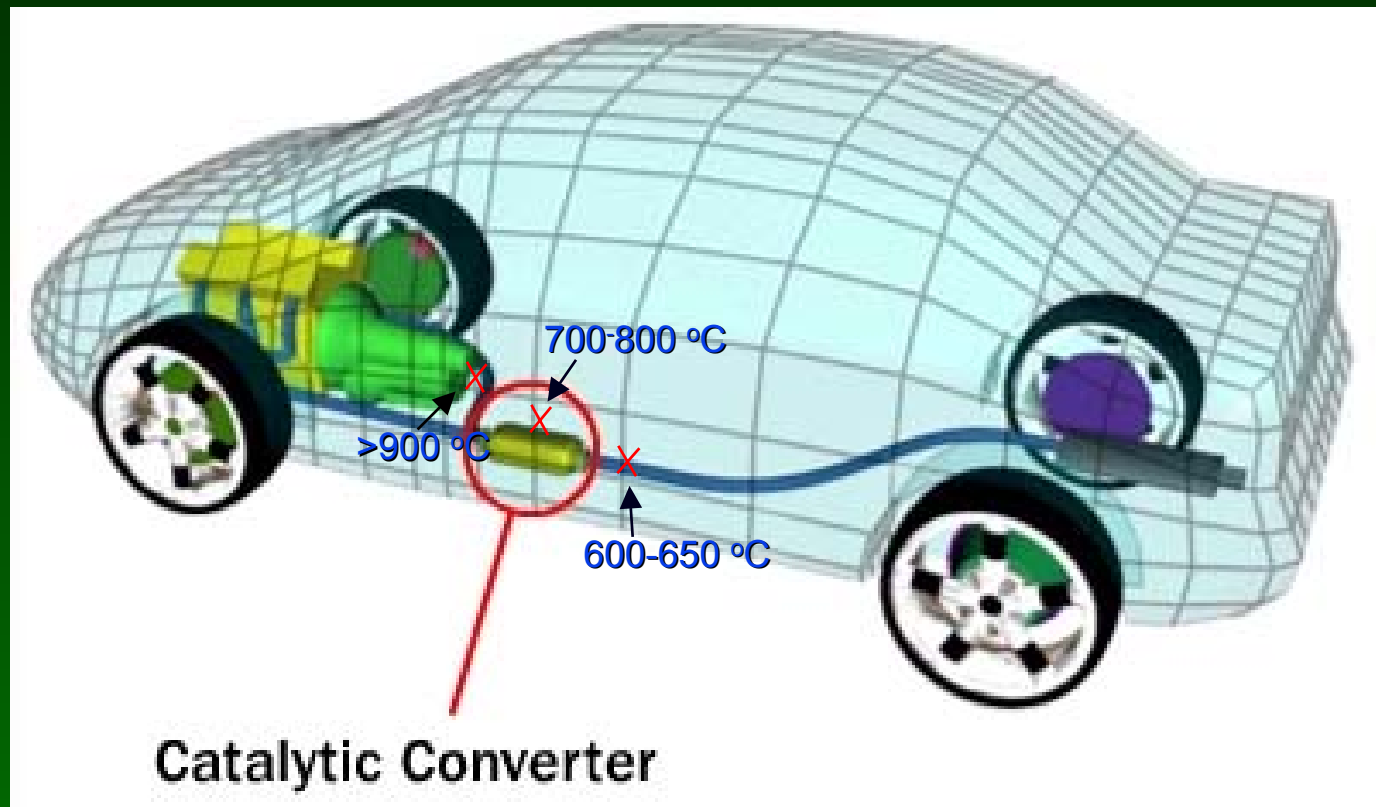
- **Convert Waste Thermal Energy Into High-Grade Electrical Energy**
 - Completely Solid State
 - No Moving Parts or Fluids
 - No Noise or Vibration
- **Latest Thermoelectric Materials Offer New Opportunity**
 - Skutterudites
 - Zn-Sb alloys
 - Quantum-Well Materials
- **Automotive Exhaust Heat Temperatures 600-700 °C**
 - Interested in ~1000 W System
- **Heavy Vehicle Exhaust Heat Temperatures 500-550 °C**
 - APUs
 - Truck Electrification

Light-Duty Vehicle Applications

Continuing National Security Issue



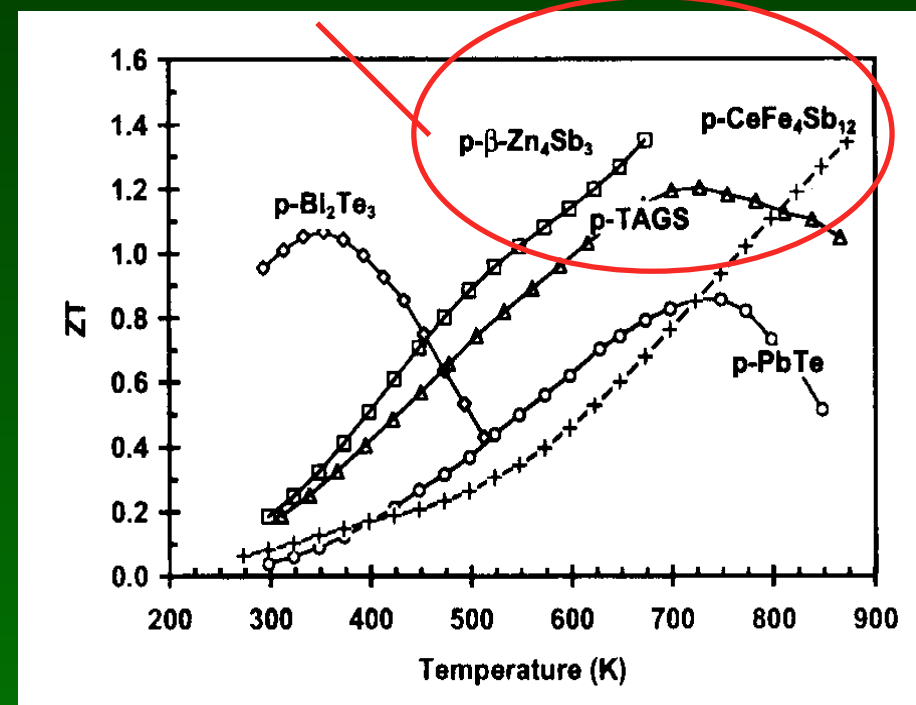
System Placement



New Thermoelectric Materials

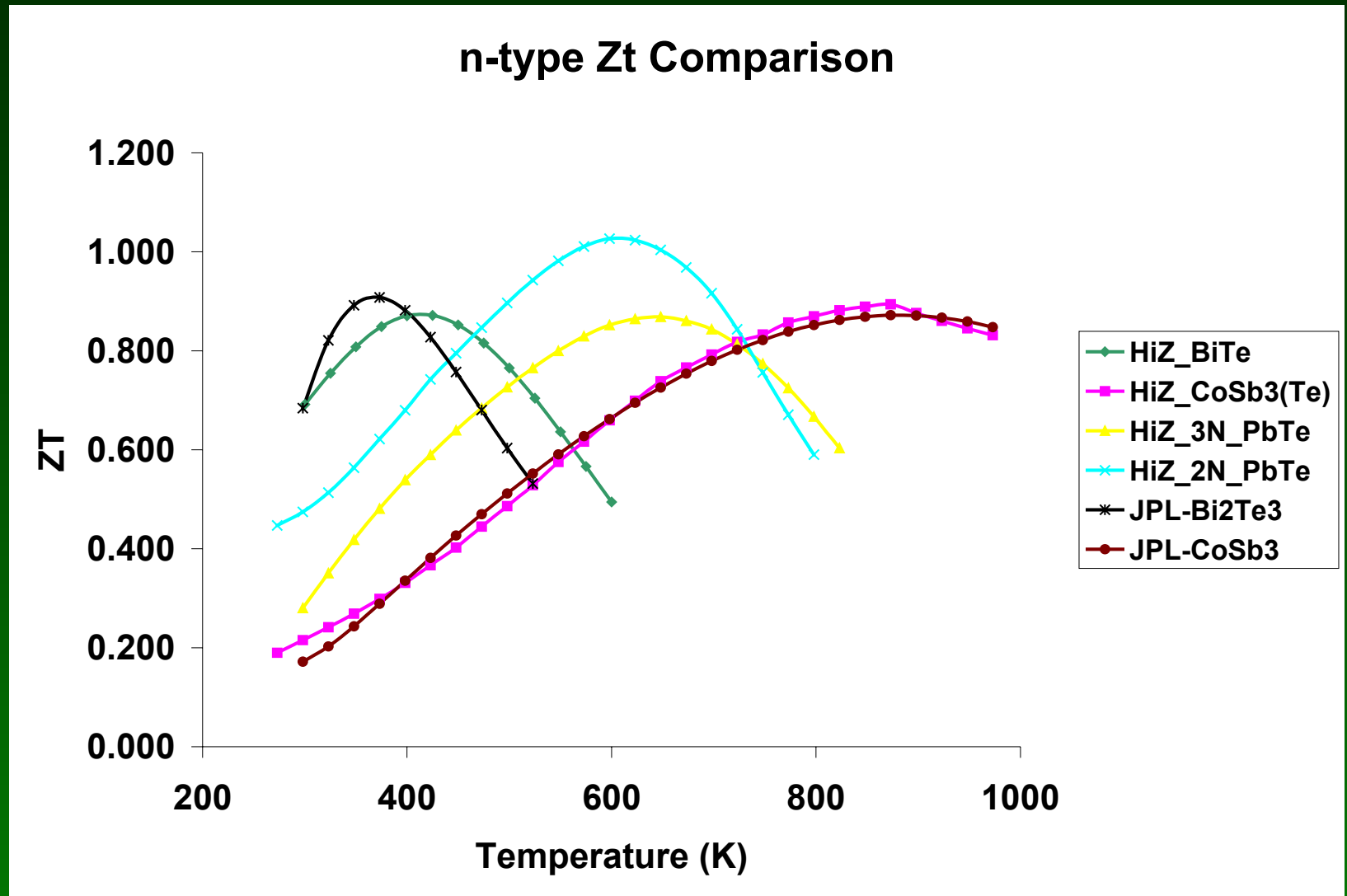
- New TE Materials Currently Being Studied
 - Skutterudites: $\text{CeFe}_4\text{Sb}_{12}$ & CoSb_3
 - Zn_4Sb_3 Alloys
 - Quantum Well Materials
 - Thin-Film Superlattice Materials
- TE Set #1: p-type $\text{CeFe}_4\text{Sb}_{12}$ – Bi_2Te_3 : n-type CoSb_3 - Bi_2Te_3
- TE Set #2: p-type TAGS - Bi_2Te_3 : n-type 2NPbTe - Bi_2Te_3
- TE Set #3: p-type $\text{CeFe}_4\text{Sb}_{12}$ – Zn_4Sb_3 - Bi_2Te_3 : n-type CoSb_3 - Bi_2Te_3

New TE Materials

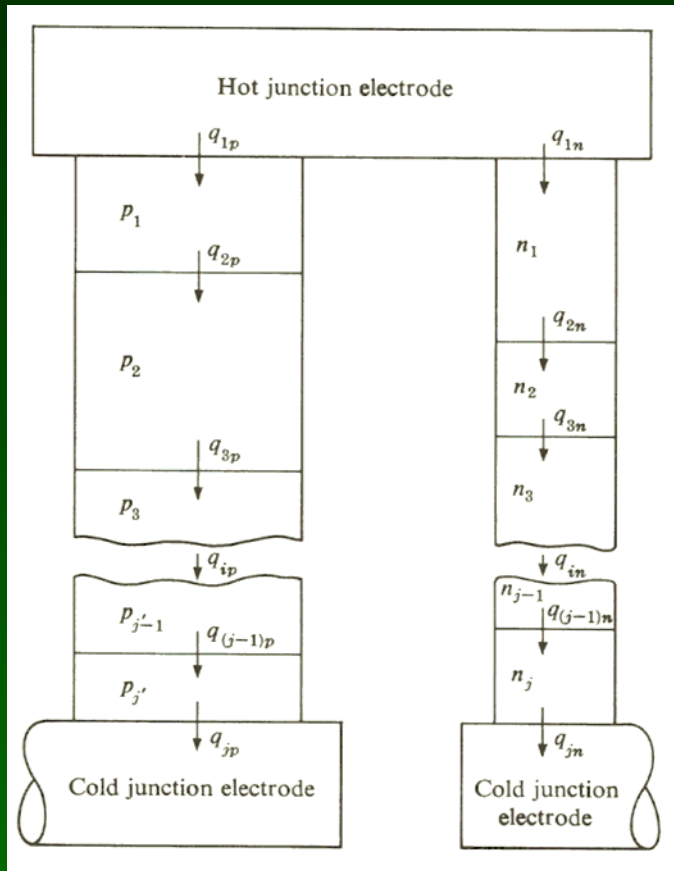


Caillat, T., Fleurial, J.-P., Snyder, G.J., Borshchevsky, A.
Journal of Phys. Chem. Solids, 1997

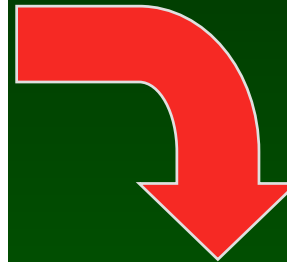
New Thermoelectric Materials



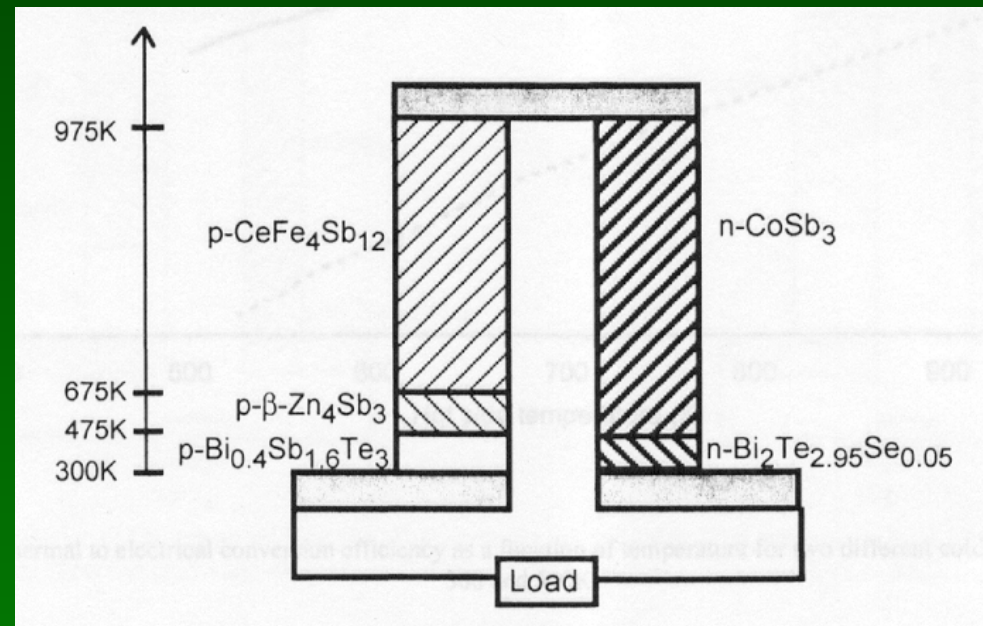
Segmented Unicouple Design Approach



Basic Segmented Leg Concept



Current Embodiment/Materials





Modeling Goals

- System Approach
 - Simultaneous Modeling of Heat Exchangers and Thermoelectric Device
- Single Material Legs
- Multi-Material Legs
- Effects of System Placement
- Heat Exchanger Performance (UA) Effects
- System Thermal Resistance Effects
- Thermal Loss Effects

System Solution Method

(Single & Multiple Material Legs)

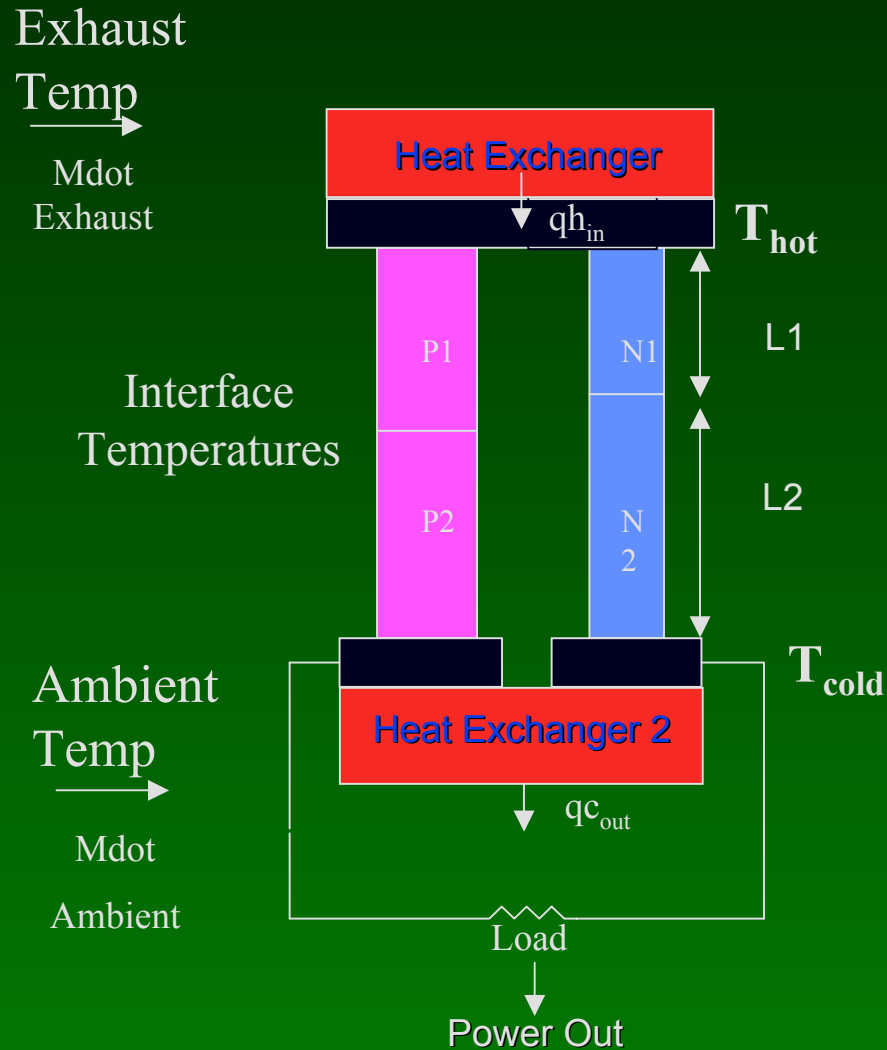
- Maximum Device Efficiency Analysis (This Paper)
- Maximum Device Power Density Analysis (Future Work)
- Challenges
 - Highly Non-linear equations (with respect to temp)
 - Temperature Dependent TE Properties
 - Mathematics Discussed in Paper
 - Needed:
 - 1 Thermoelectric Parameter
 - 1 Heat Exchanger Parameter
 - Thermoelectric Hot and Cold Sides (T_h & T_c)
- Solution
 - Iterative Solutions For Range of Thermoelectric Hot & Cold Side
 - Cases Done: $n_c, V : n_c, \gamma_n : n_h, \gamma_n : n_h, V : N, \gamma_n : q_h, \gamma_n : n_h, I : n_c, I$



Advanced Thermoelectric System Design

2-p/2-n Segmented-Leg TE Design Analysis

Advanced Thermoelectric System Design



P1=CeFeSb

P2=BiTe

N1=CoSb

N2=BiTe

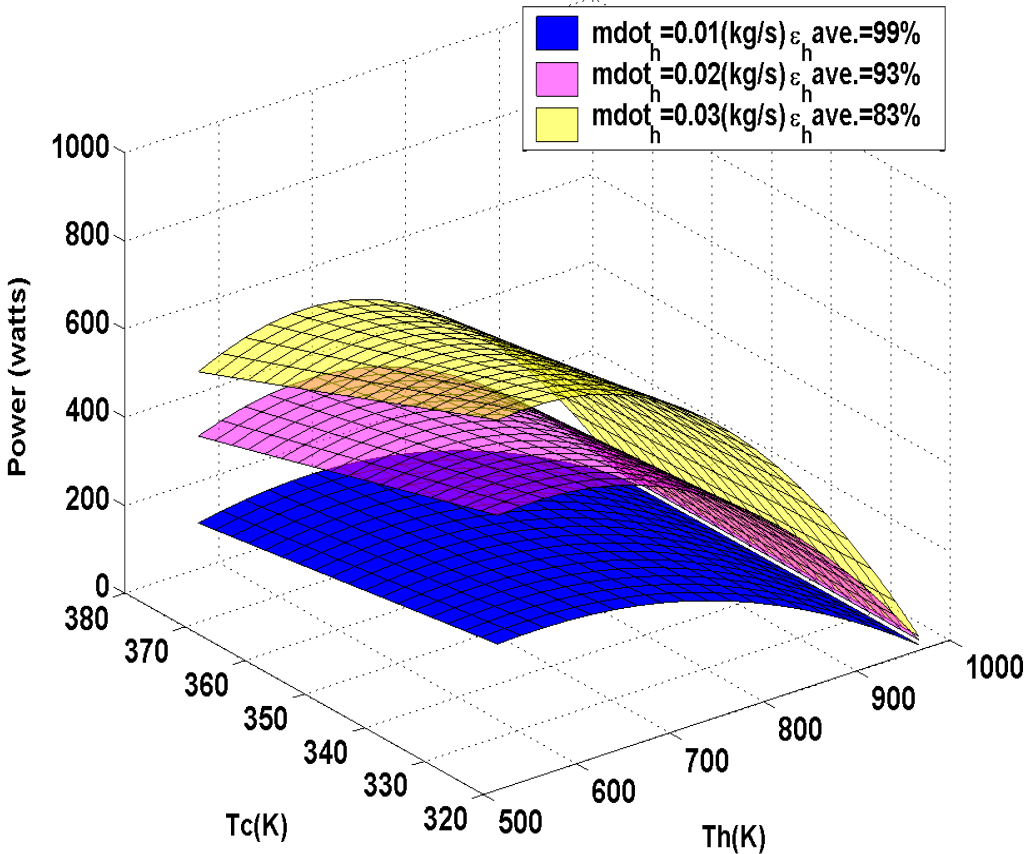
Results: Maximums Found

Peak Power: 333, 626, 843 (W)

At Peak P: 0.21, 0.41, 0.71 (kg/s)

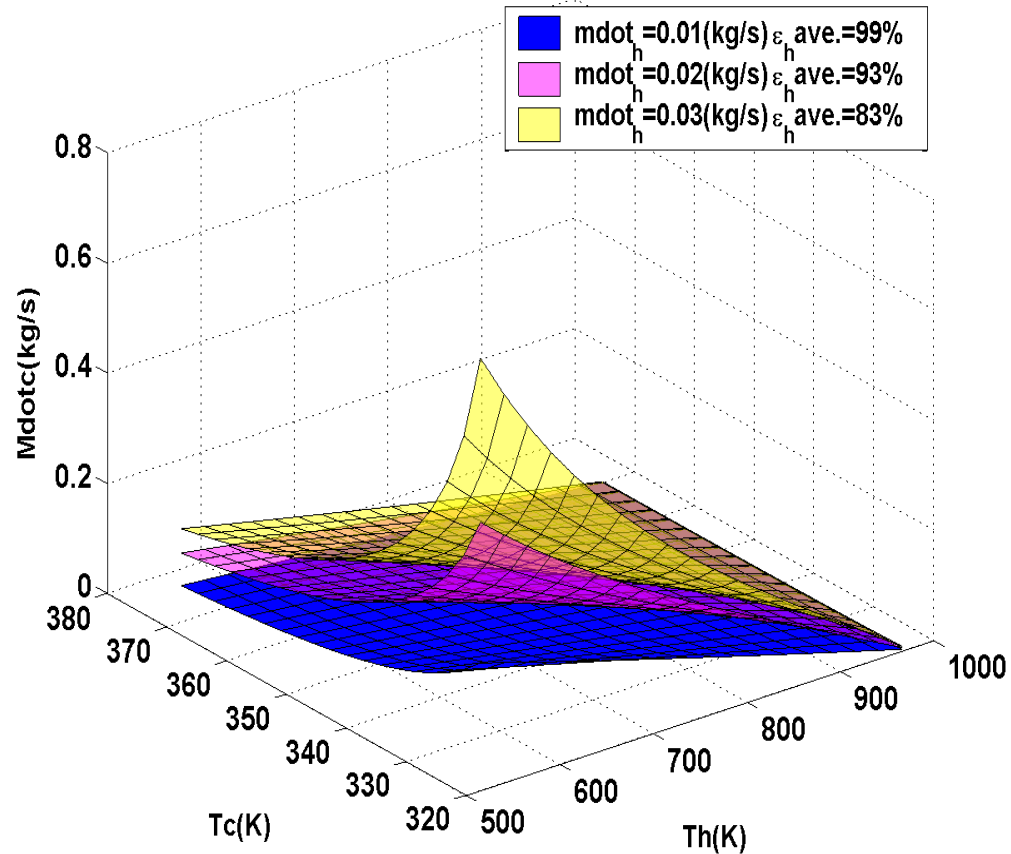
Power (2p-2n): Ce-BiTe&CoSb-BiTe
 $UA_h = 60(W/K)$, $UA_c = 1070(W/K)$, $T_{ex} = 973(K)$, $T_{amb} = 300(K)$

- $\dot{m}_h = 0.01(kg/s)$ ϵ_h ave.=99%
- $\dot{m}_h = 0.02(kg/s)$ ϵ_h ave.=93%
- $\dot{m}_h = 0.03(kg/s)$ ϵ_h ave.=83%



Required Ambient \dot{m}_{dot} (2p-2n): Ce-BiTe&CoSb-BiTe
 $UA_h = 60(W/K)$, $UA_c = 1070(W/K)$, $T_{ex} = 973(K)$, $T_{amb} = 300(K)$

- $\dot{m}_h = 0.01(kg/s)$ ϵ_h ave.=99%
- $\dot{m}_h = 0.02(kg/s)$ ϵ_h ave.=93%
- $\dot{m}_h = 0.03(kg/s)$ ϵ_h ave.=83%



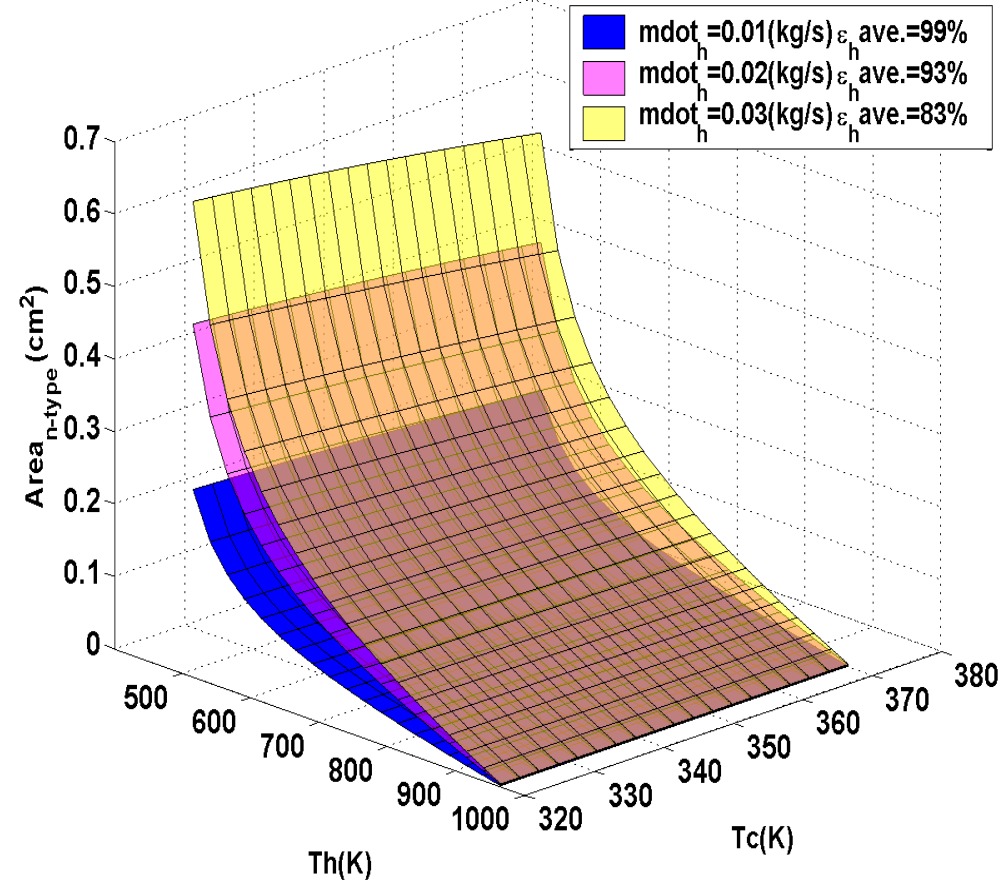
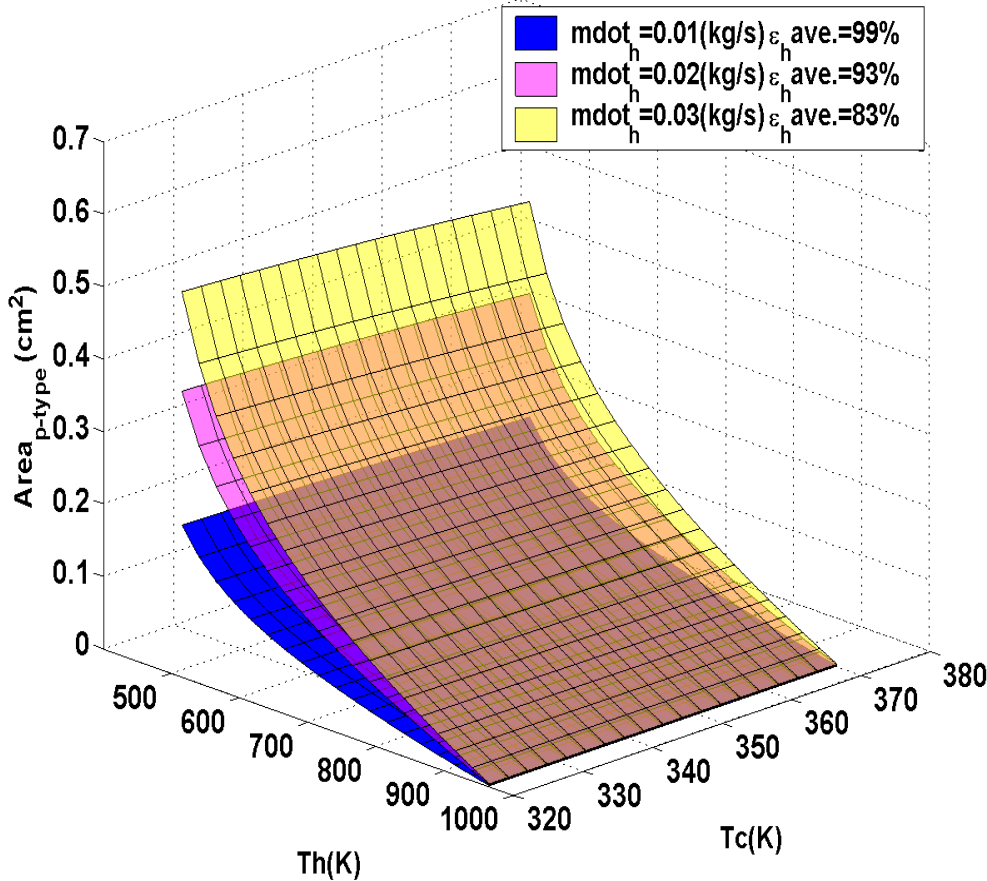
Results: TE Cross-Sectional Area Comparison

At Peak P: 0.15, 0.28, 0.44 (cm²)
Decrease from 12V ~ 71%

At Peak P: 0.16, 0.29, 0.49 (cm²)
Decrease from 12 V ~ 71%

Required p-type Cross-Sectional Area (2p-2n): Ce-BiTe&CoSb-BiTe
V=42(volts), UA_h=60(W/K), UA_c=1070(W/K), T_{ex}=973(K), T_{amb}=300(K)

Required n-type Cross-Sectional Area (2p-2n): Ce-BiTe&CoSb-BiTe
V=42(volts), UA_h=60(W/K), UA_c=1070(W/K), T_{ex}=973(K), T_{amb}=300(K)



Results: Required TE Couples Comparison

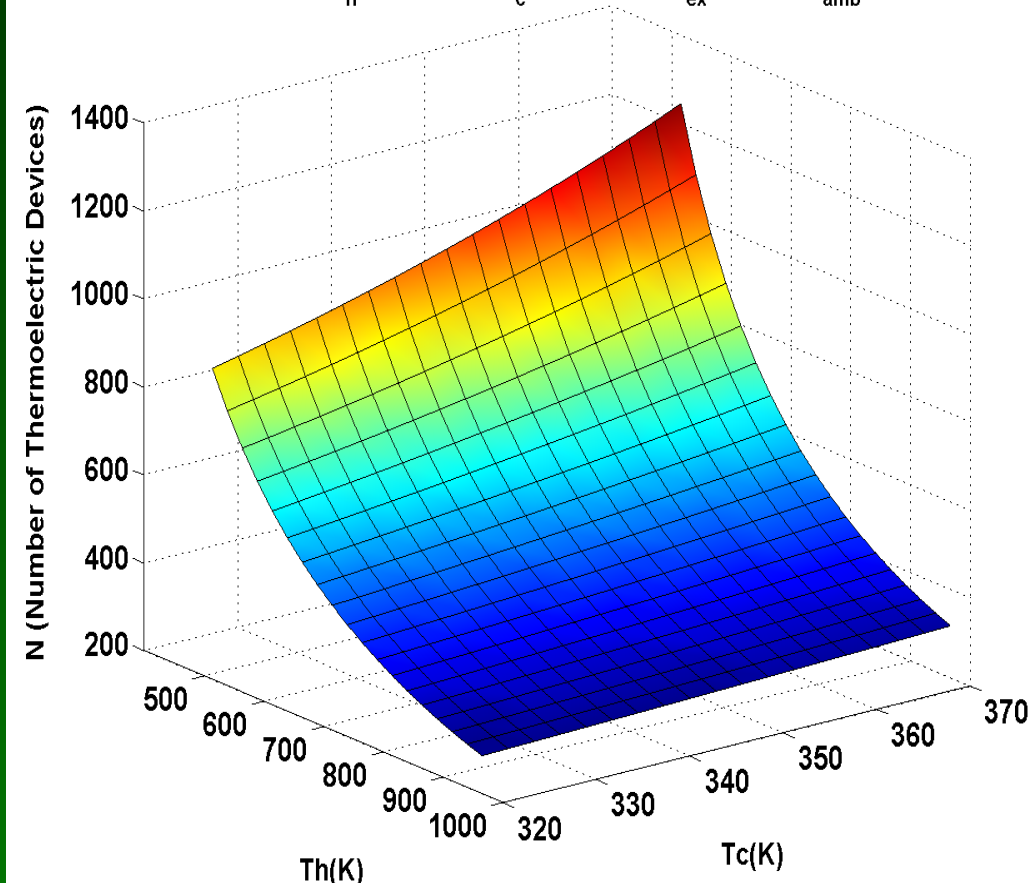
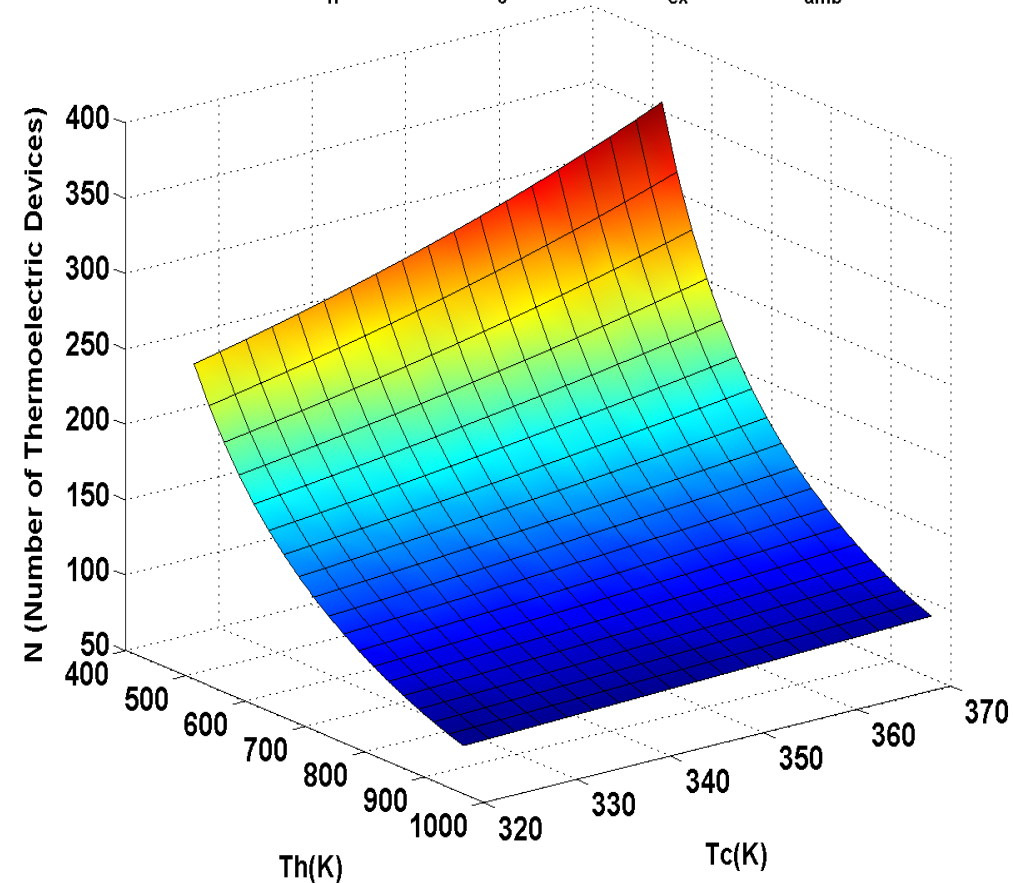
42 V Larger by ~ 235%

At Peak P: 225 (devices)

At Peak P: 754 (devices)

Required Thermoelectric Devices (2p-2n): Ce-BiTe&CoSb-BiTe
 $V=12(\text{volts})$, $UA_h=60(\text{W/K})$, $UA_c=1070(\text{W/K})$, $T_{ex}=973(\text{K})$, $T_{amb}=300(\text{K})$

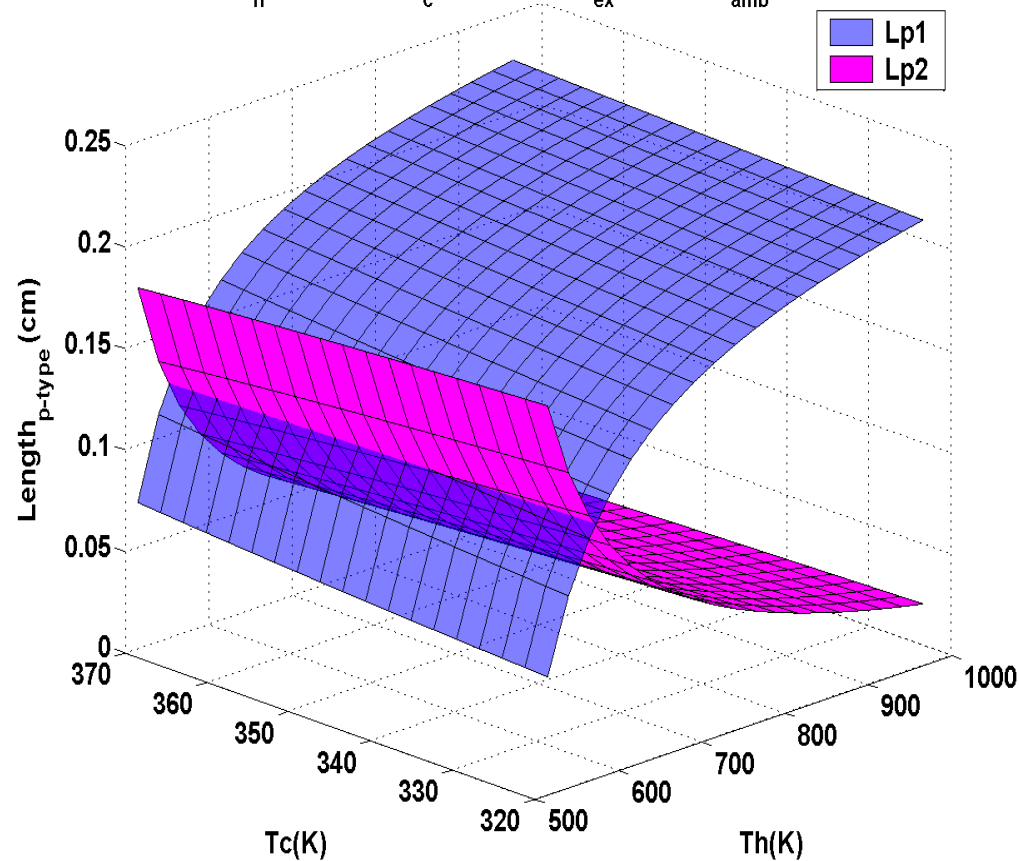
Required Thermoelectric Devices (2p-2n): Ce-BiTe&CoSb-BiTe
 $V=42(\text{volts})$, $UA_h=60(\text{W/K})$, $UA_c=1070(\text{W/K})$, $T_{ex}=973(\text{K})$, $T_{amb}=300(\text{K})$



Results: TE Element Length Trends

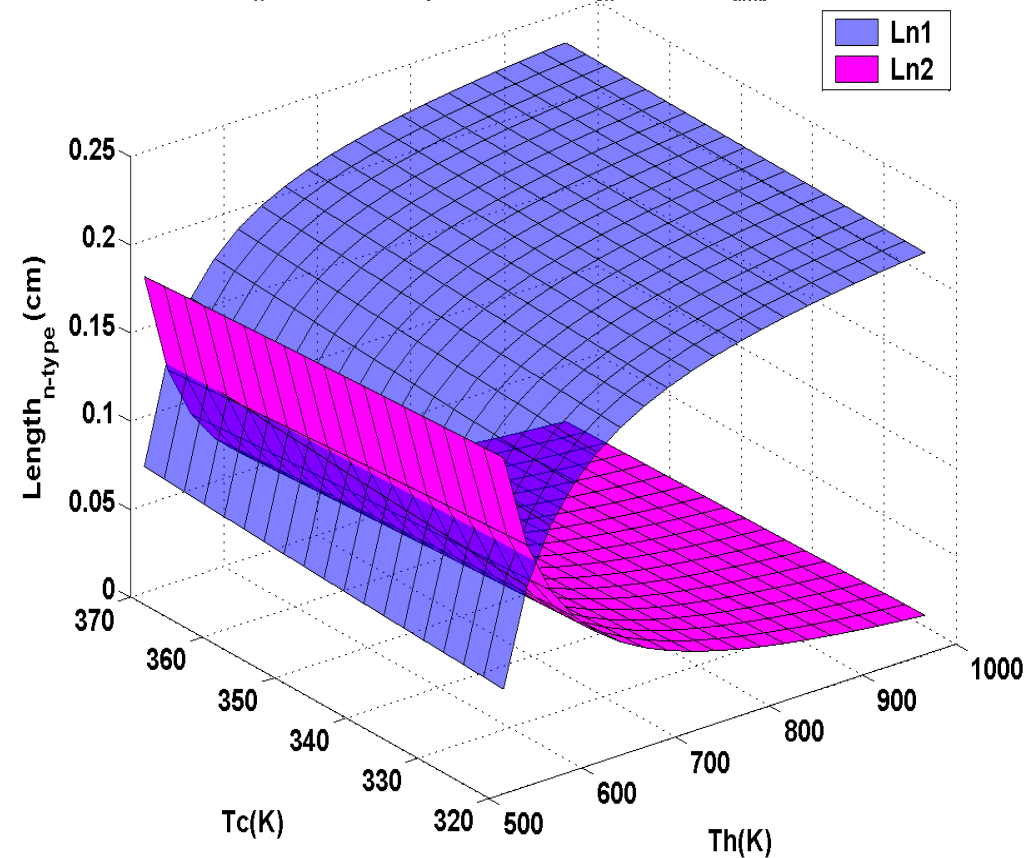
p-Type

Optimized Lengths of p-type Segment (2p-2n): Ce-BiTe&CoSb-BiTe
 $UA_h = 60(W/K)$, $UA_c = 1070(W/K)$, $T_{ex} = 973(K)$, $T_{amb} = 300(K)$



n-Type

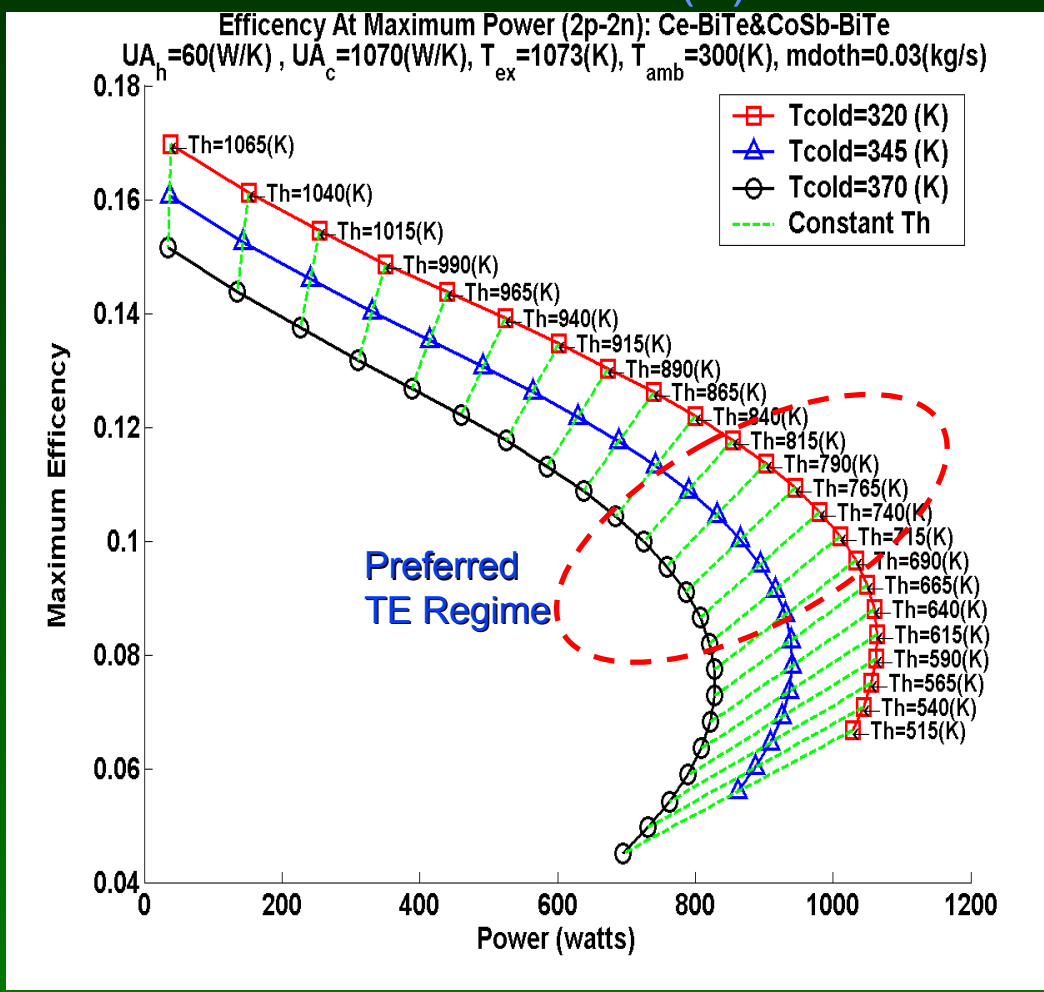
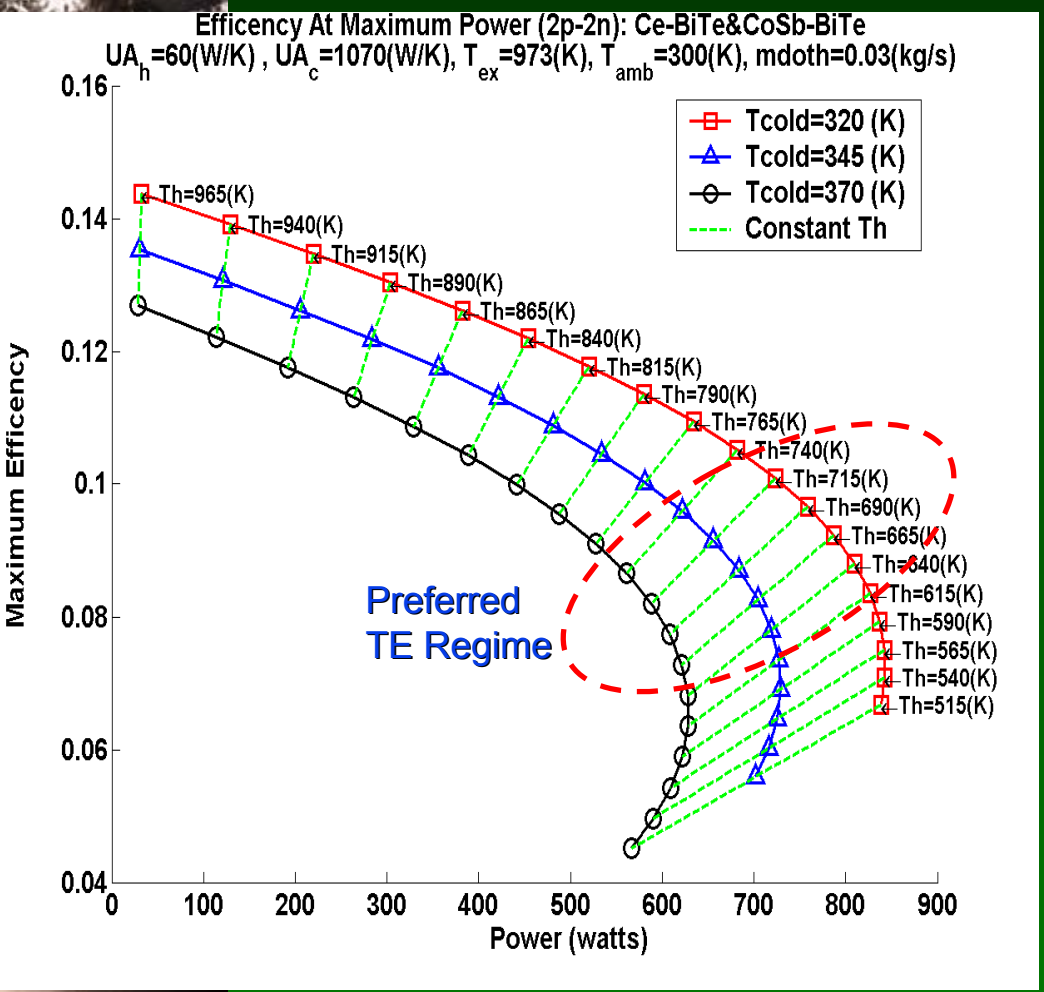
Optimized Lengths of n-type Segment (2p-2n): Ce-BiTe&CoSb-BiTe
 $UA_h = 60(W/K)$, $UA_c = 1070(W/K)$, $T_{ex} = 973(K)$, $T_{amb} = 300(K)$



Results: Peak Power Not At Peak Eff.

$T_{ex}=973(K)$ P_{pk} : 333, 626, 843 (W)

$T_{ex}=1073(K)$ P_{pk} : 423, 793, 1064 (W)
Increased from 973(K) ~ 26%

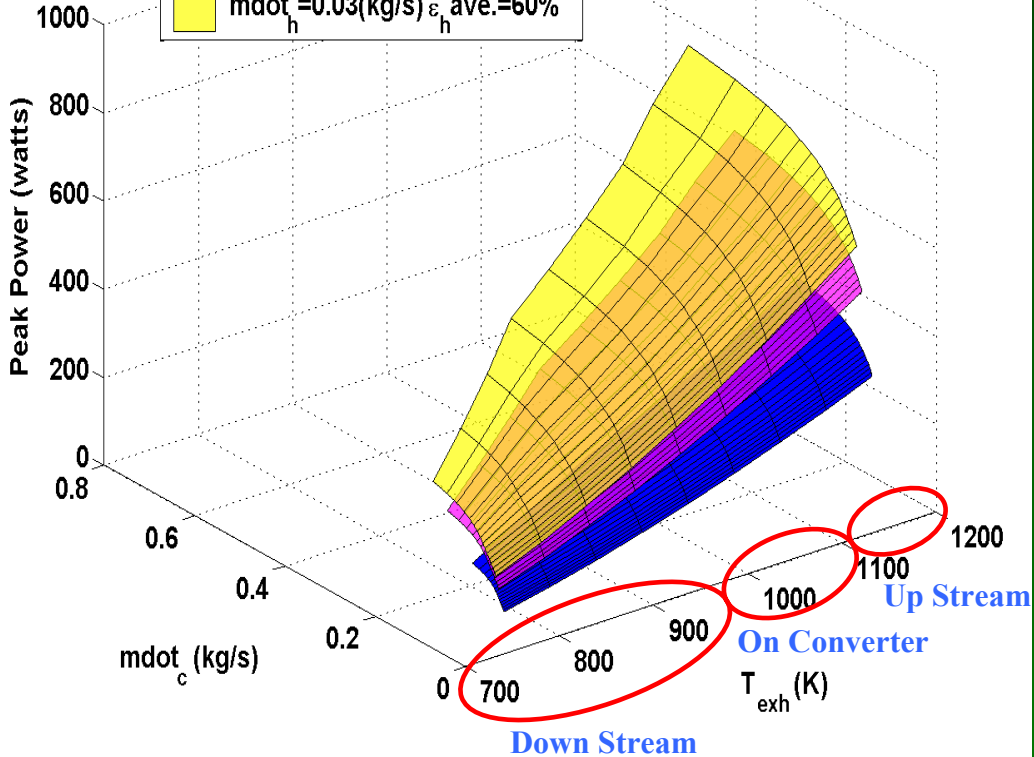


Results: Effects of Placement and UA_h

UA_h=30 (W/K)

Effects of Placement (Exhaust Temperature): (2p-2n) Ce-BiTe&CoSb-BiTe
 UA_h=30(W/K), UA_c=1000(W/K), R_{th,h}=0.002(W/K), R_{th,c}=0.0004(W/K)

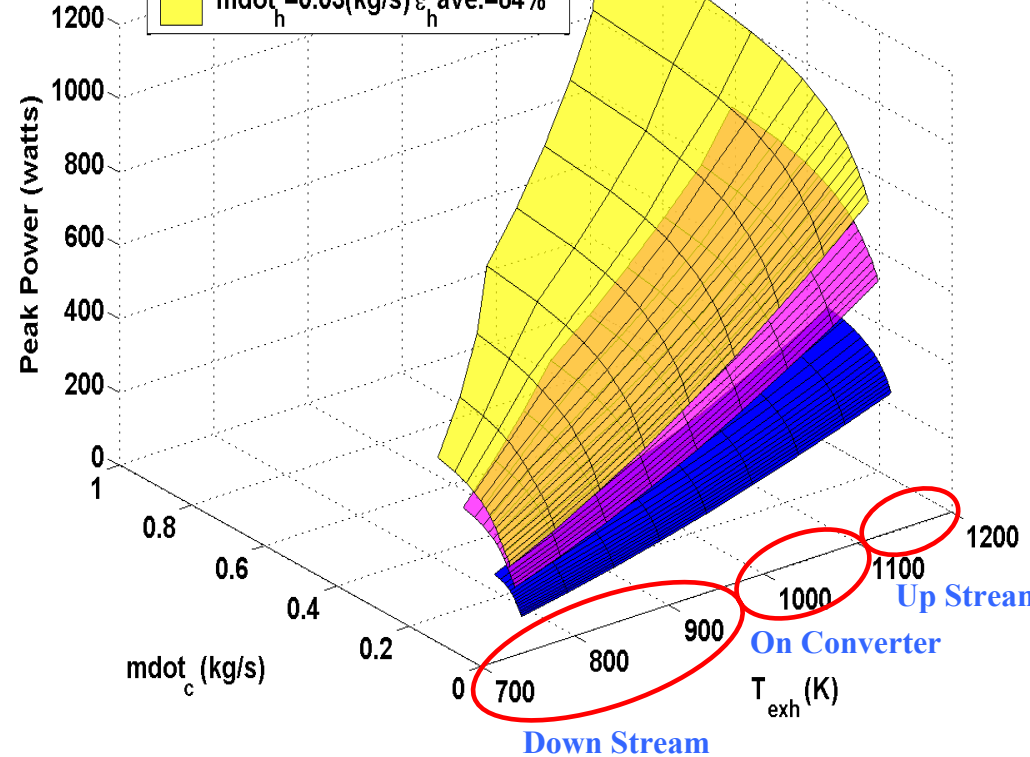
- $\dot{m}_h = 0.01(\text{kg/s})$ $\epsilon_h \text{ ave.} = 93\%$
- $\dot{m}_h = 0.02(\text{kg/s})$ $\epsilon_h \text{ ave.} = 75\%$
- $\dot{m}_h = 0.03(\text{kg/s})$ $\epsilon_h \text{ ave.} = 60\%$



UA_h=60 (W/K)

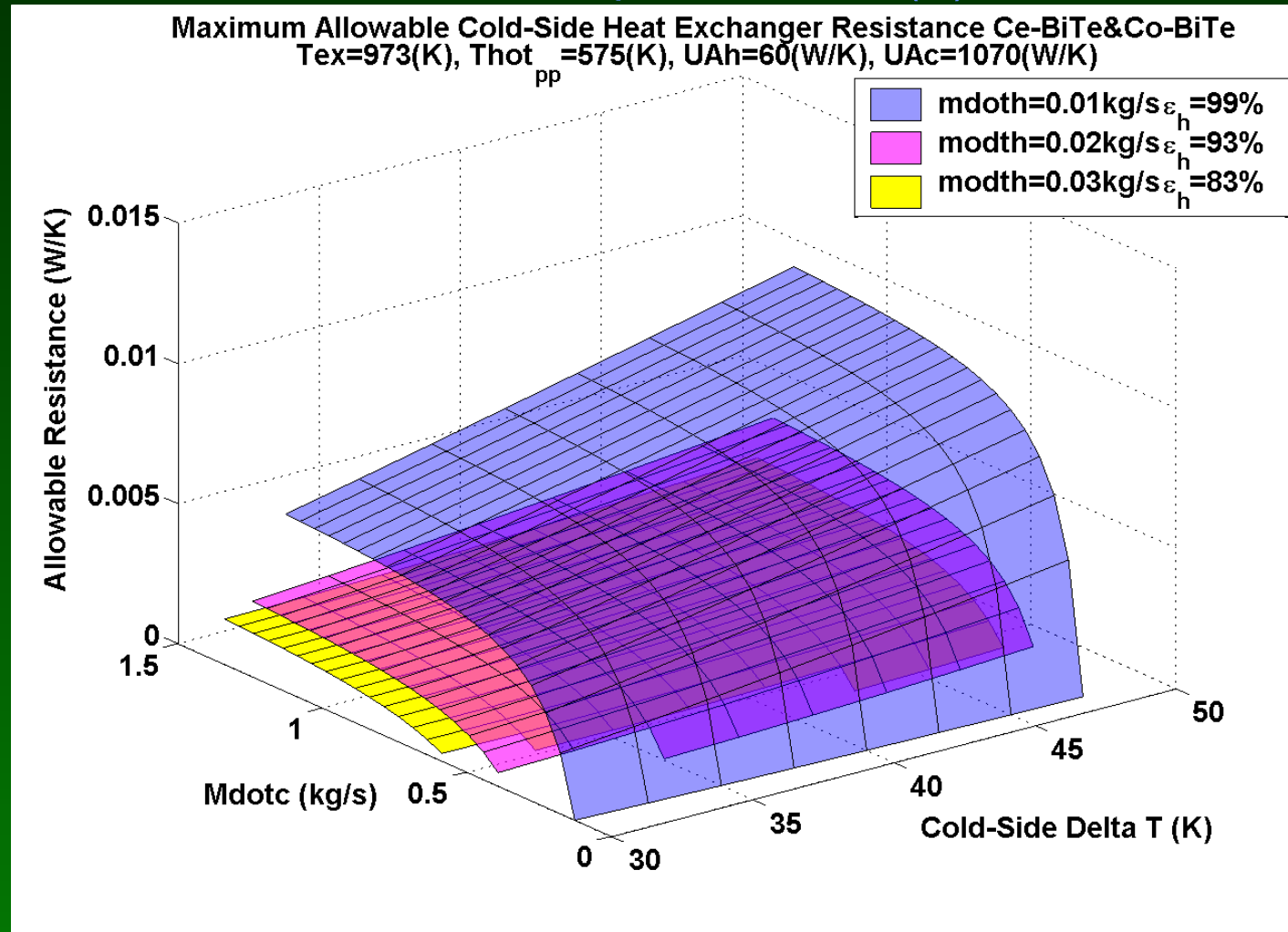
Effects of Placement (Exhaust Temperature): (2p-2n) Ce-BiTe&CoSb-BiTe
 UA_h=60(W/K), UA_c=1000(W/K), R_{th,h}=0.002(W/K), R_{th,c}=0.0004(W/K)

- $\dot{m}_h = 0.01(\text{kg/s})$ $\epsilon_h \text{ ave.} = 99\%$
- $\dot{m}_h = 0.02(\text{kg/s})$ $\epsilon_h \text{ ave.} = 94\%$
- $\dot{m}_h = 0.03(\text{kg/s})$ $\epsilon_h \text{ ave.} = 84\%$



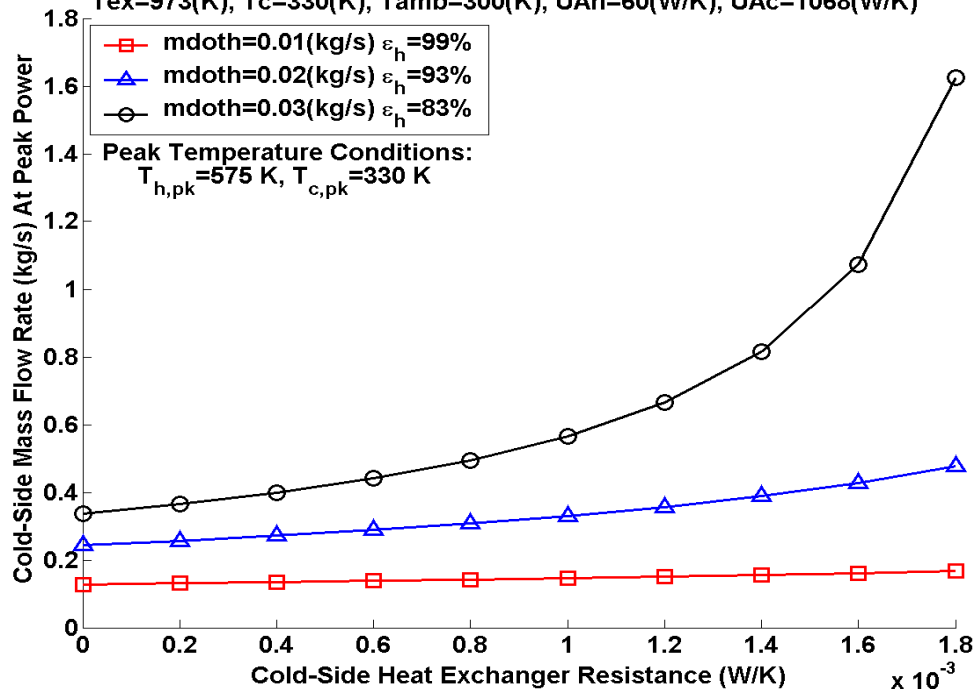
Results: Cold Side Thermal Resistance Study

Exhaust Temperature=973(K)

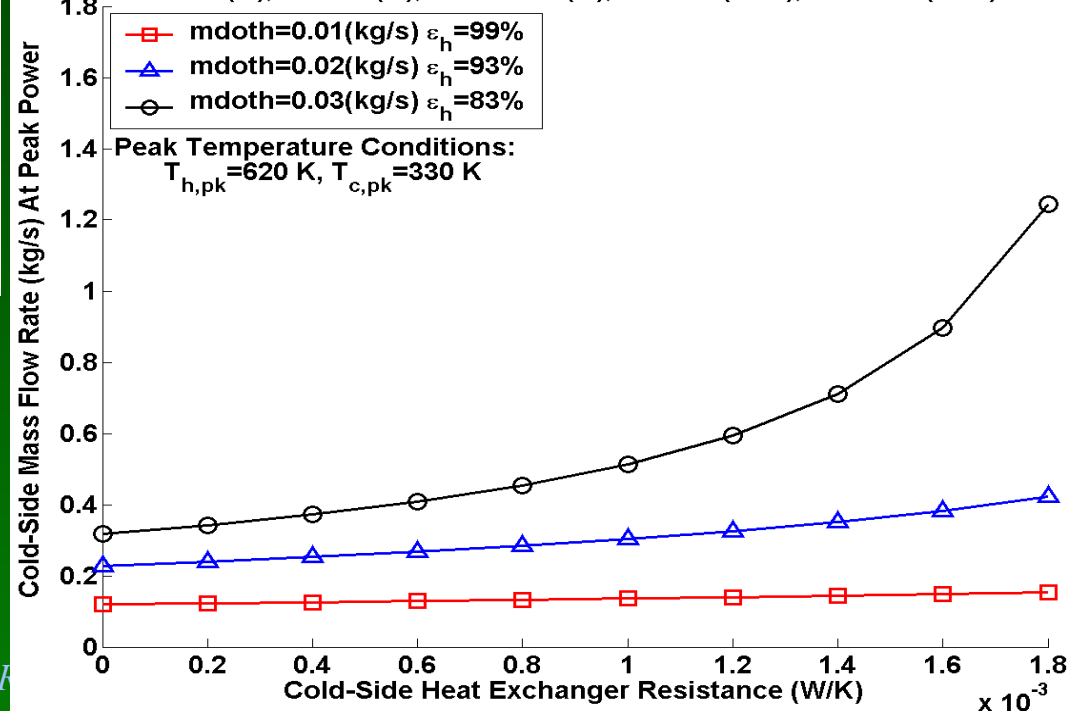


Results: Cold Side Thermal Resistance Study

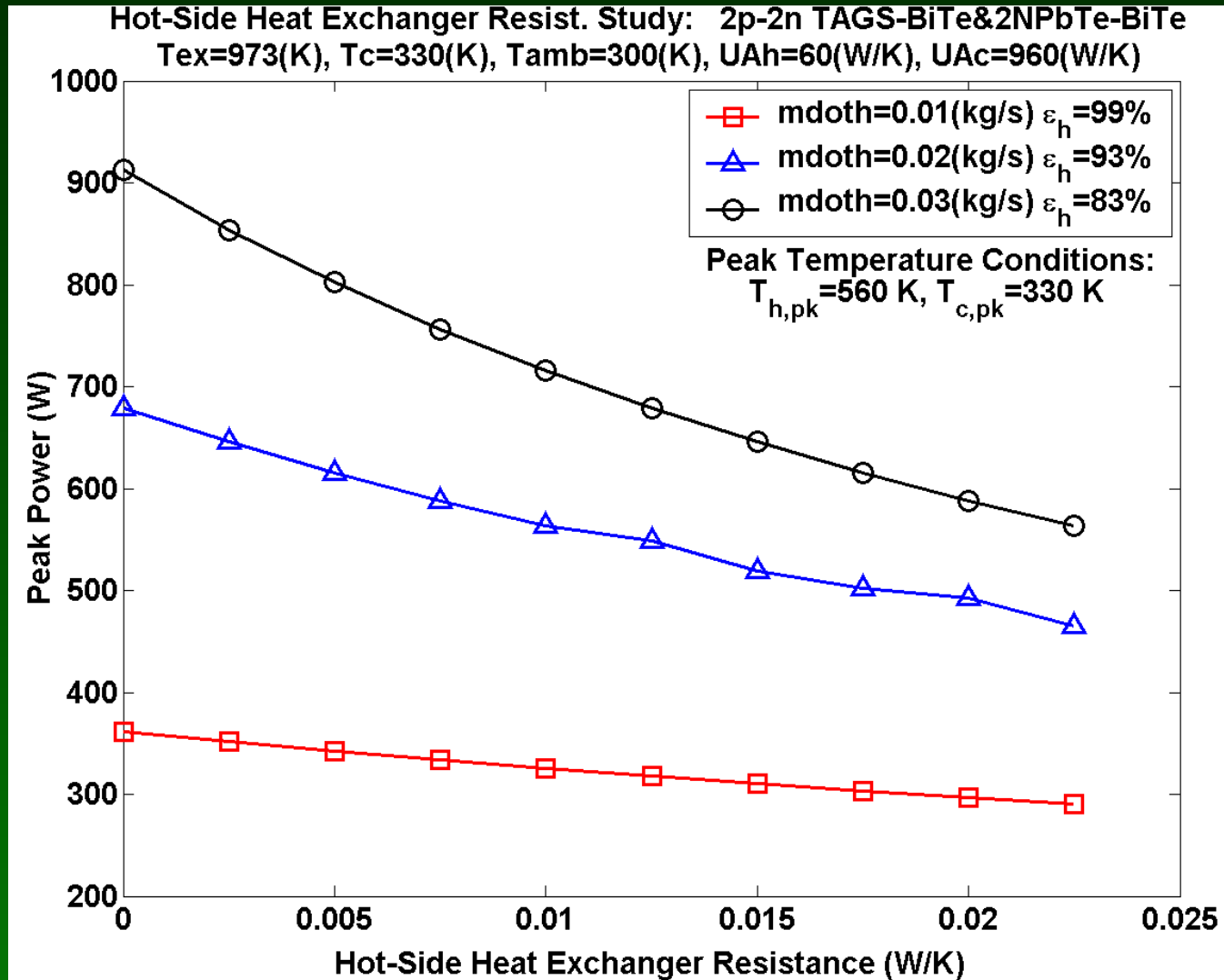
Cold-Side Heat Exchanger Resist. Study: 2p-2n Ce-BiTe&Co-BiTe
 $T_{ex}=973(K)$, $T_c=330(K)$, $T_{amb}=300(K)$, $UA_h=60(W/K)$, $UA_c=1068(W/K)$



Cold-Side Heat Exchanger Resist. Study: 2p-2n TAGS-BiTe&2NPbTe-BiTe
 $T_{ex}=973(K)$, $T_c=330(K)$, $T_{amb}=300(K)$, $UA_h=60(W/K)$, $UA_c=960(W/K)$



Results: Hot Side Thermal Resistance Study





Advanced Thermoelectric System Design

3-p/2-n Segmented-Leg TE Design Analysis

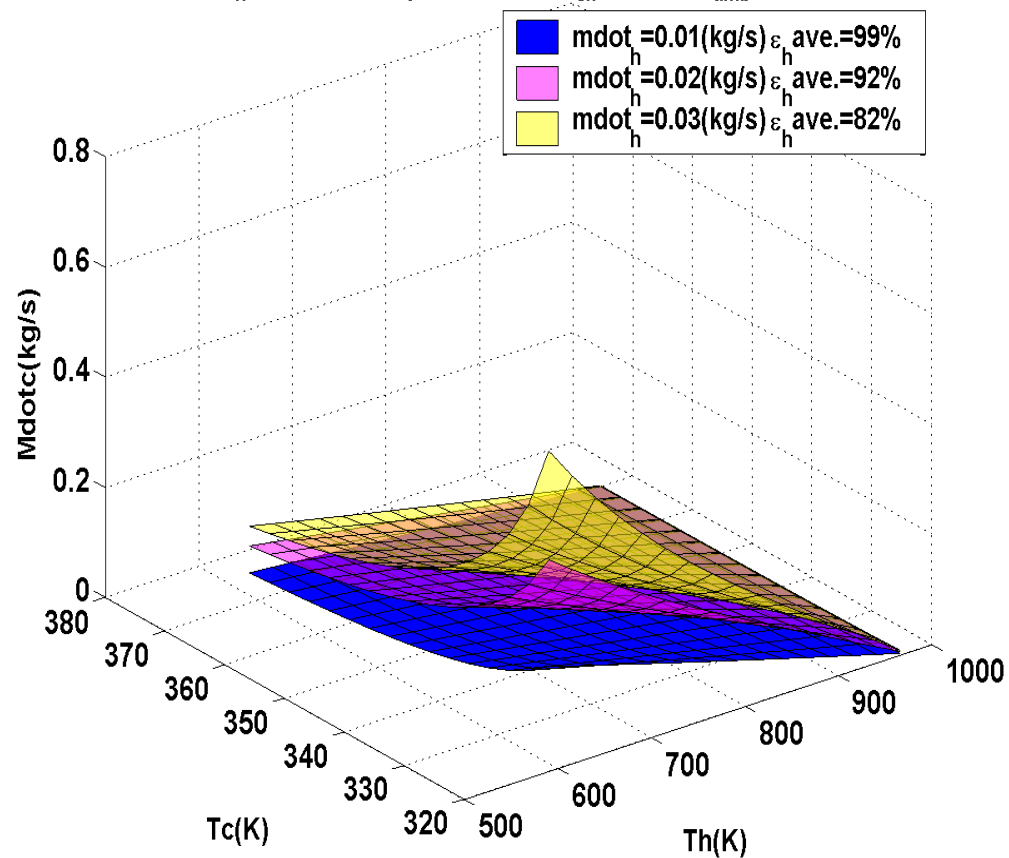
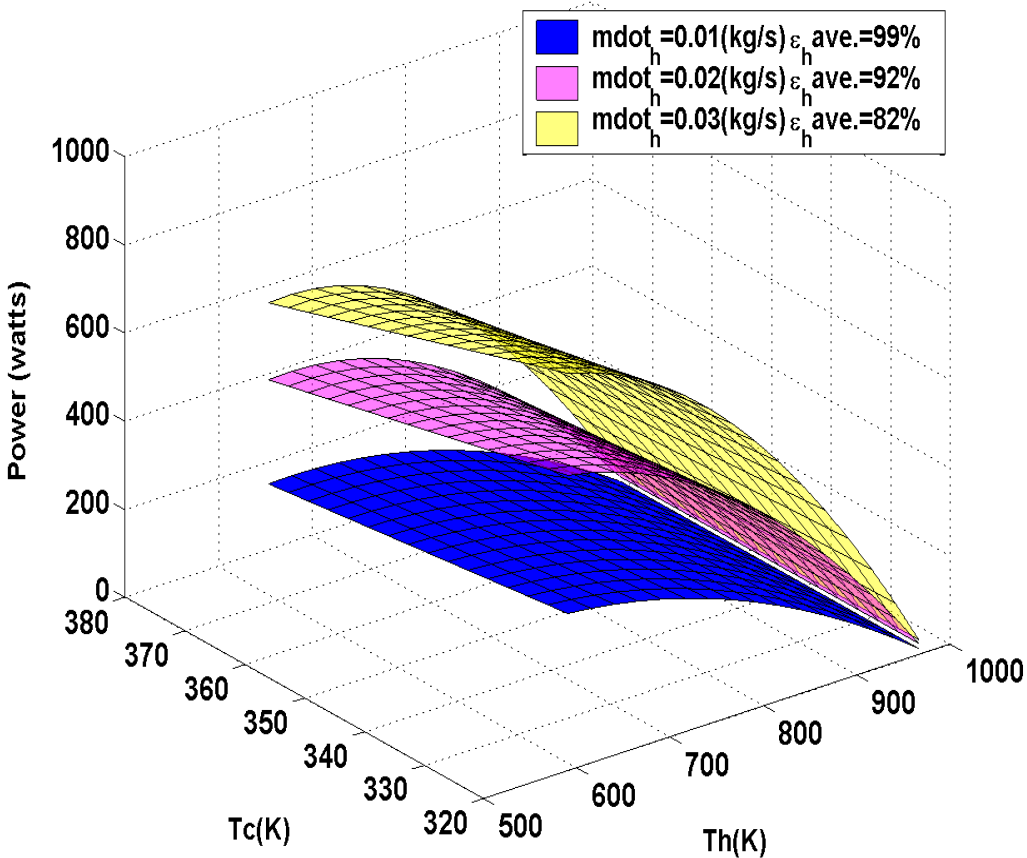
Results: Maximums Found

Peak Power: 360, 670, 900 (W)
Increase from 2p-2n ~7%

At Peak P: 0.19, 0.38, 0.58 (kg/s)
Decrease from 2p-2n ~7%

Power (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
 $UA_h = 60(W/K)$, $UA_c = 1020(W/K)$, $T_{ex} = 973(K)$, $T_{amb} = 300(K)$

Required Ambient Mdot (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
 $UA_h = 60(W/K)$, $UA_c = 1020(W/K)$, $T_{ex} = 973(K)$, $T_{amb} = 300(K)$



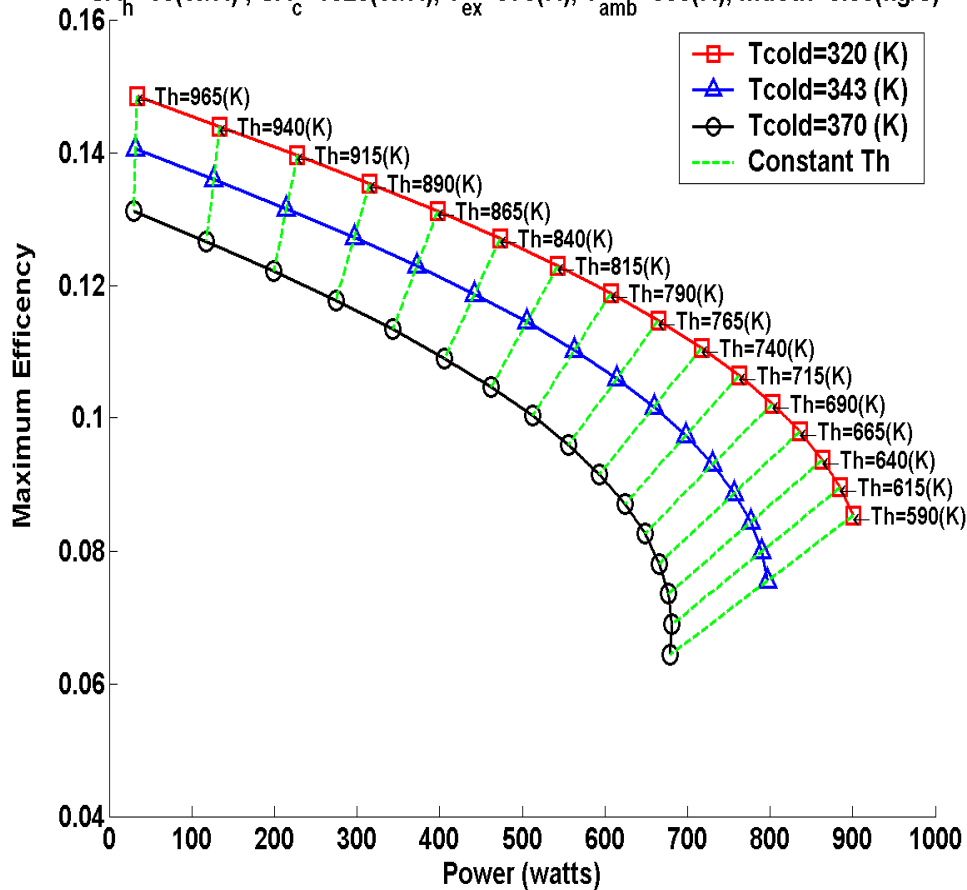
Results: Comparison To 2p-2n Segments

Peak Power: 356, 670, 901 (W)
Increase from 2p-2n ~ 7%

Peak Power: 454, 852, 1144 (W)
Increase from 973(K) ~ 27%

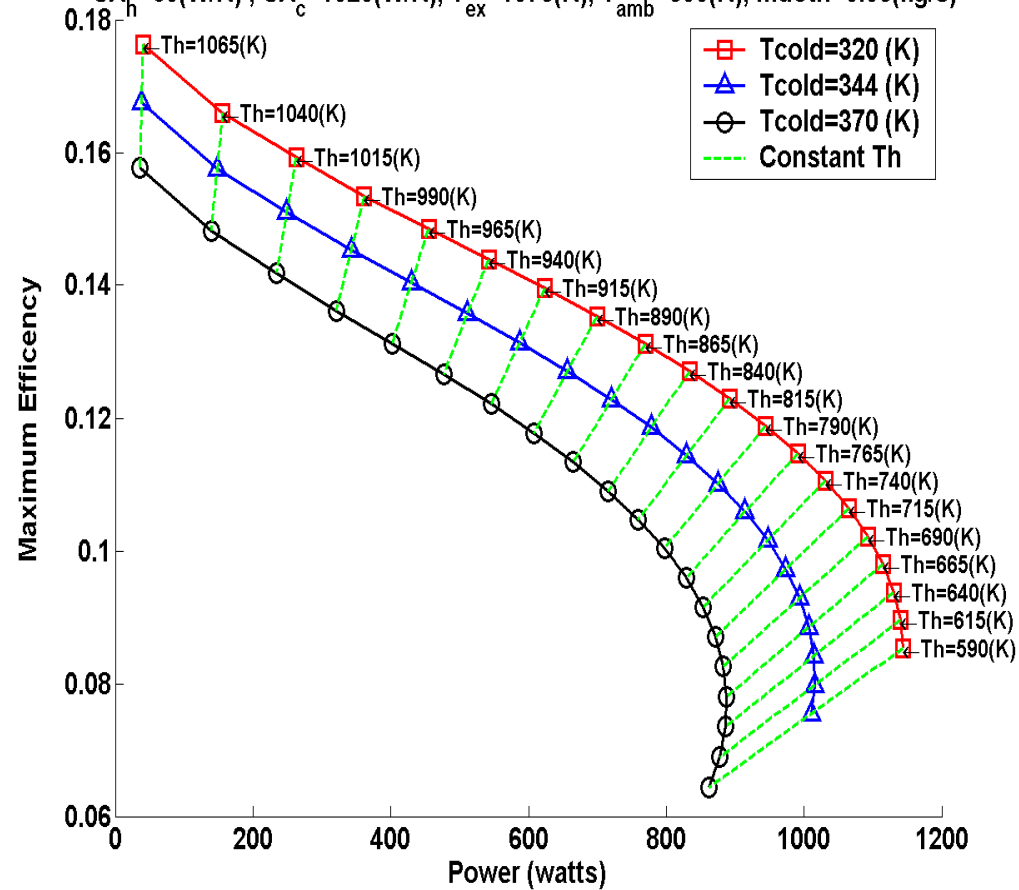
Efficiency At Maximum Power (3p-2n): Ce-Zn-BiTe&CoSb-BiTe

$UA_h = 60(W/K)$, $UA_c = 1020(W/K)$, $T_{ex} = 973(K)$, $T_{amb} = 300(K)$, $\dot{m} = 0.03(kg/s)$



Efficiency At Maximum Power (3p-2n): Ce-ZnSb-BiTe&CoSb-BiTe

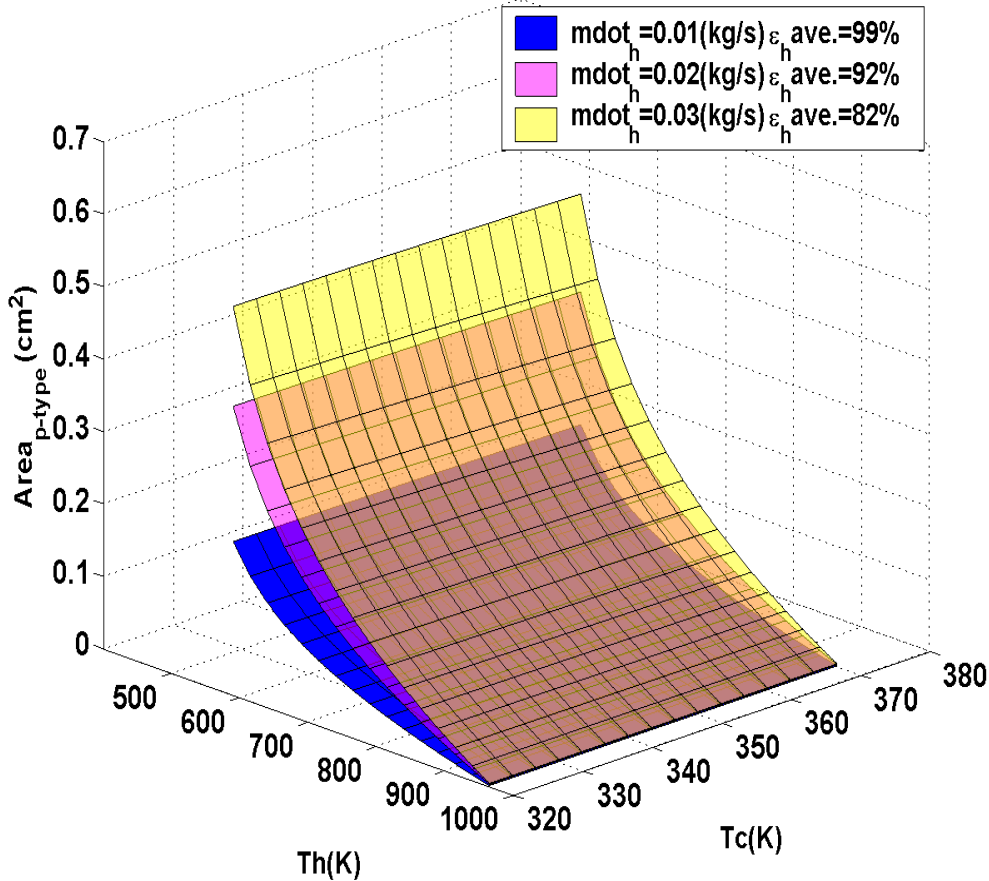
$UA_h = 60(W/K)$, $UA_c = 1020(W/K)$, $T_{ex} = 1073(K)$, $T_{amb} = 300(K)$, $\dot{m} = 0.03(kg/s)$



Results: TE Cross-Sectional Area Comparison

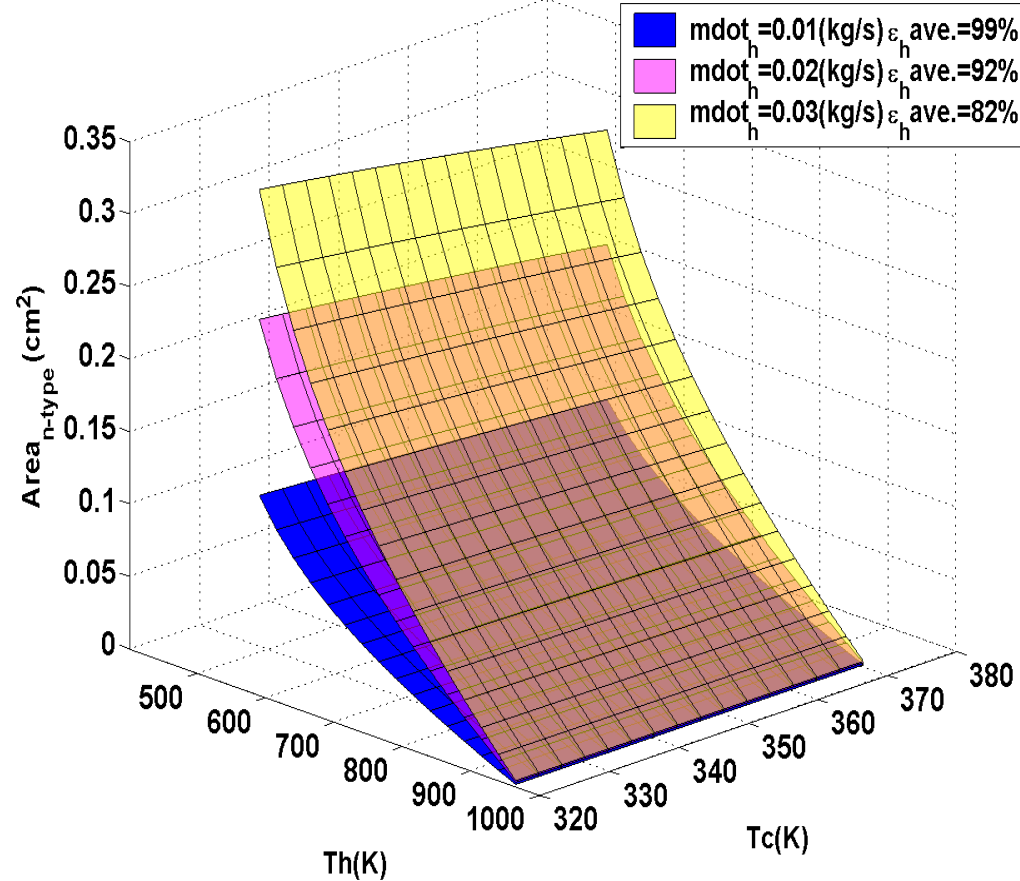
At Peak P: 0.21, 0.40, 0.54 (cm²)
Increased from 2p-2n

Required p-type Cross-Sectional Area (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
V=42(volts), UA_h=60(W/K), UA_c=1020(W/K), T_{ex}=973(K), T_{amb}=300(K)



At Peak P: 0.14, 0.26, 0.35 (cm²)
Increased from 2p-2n

Required n-type Cross-Sectional Area (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
V=42(volts), UA_h=60(W/K), UA_c=1020(W/K), T_{ex}=973(K), T_{amb}=300(K)



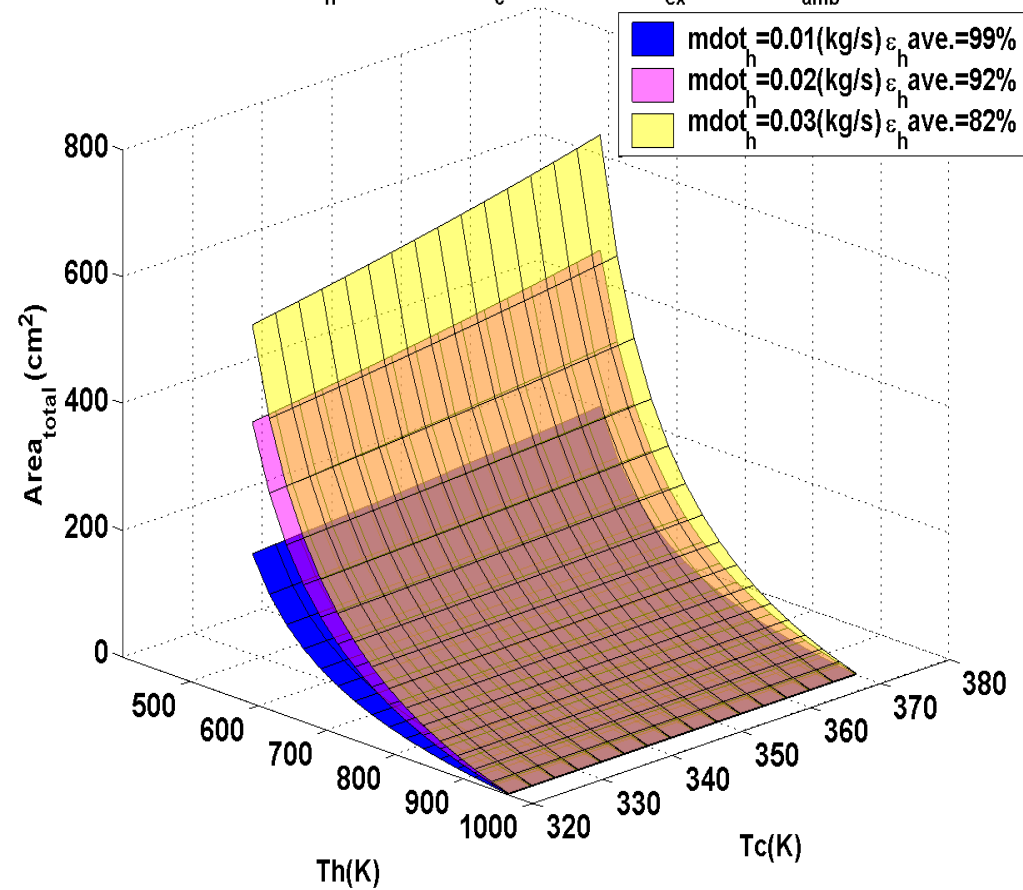
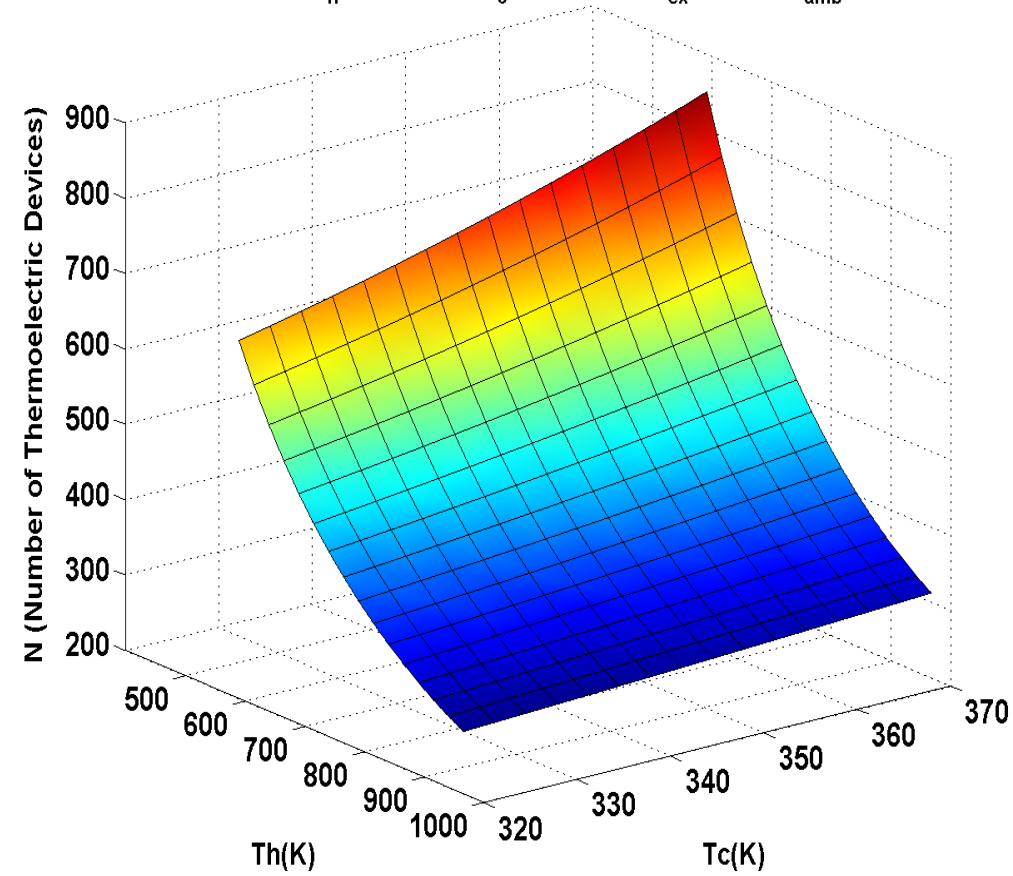
Results: Required TE Couples & Total Area

At Peak P: 674 (devices)
Decrease from 2p-2n

At Peak P: 236, 444, 597 (cm²)
Approximately Equal to 2_2

Required Thermoelectric Devices (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
V=42(volts), UA_h=60(W/K), UA_c=1020(W/K), T_{ex}=973(K), T_{amb}=300(K)

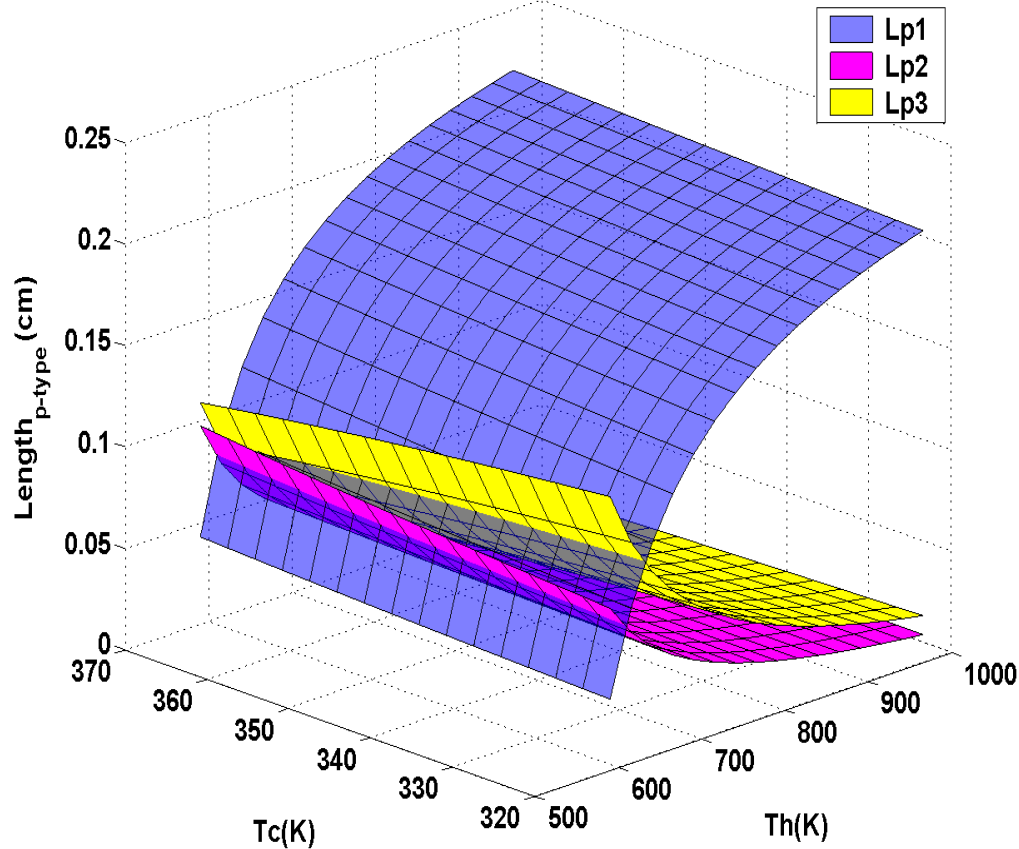
Required Total Cross-Sectional Area (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
V=42(volts), UA_h=60(W/K), UA_c=1020(W/K), T_{ex}=973(K), T_{amb}=300(K)



Results: TE Element Length Trends

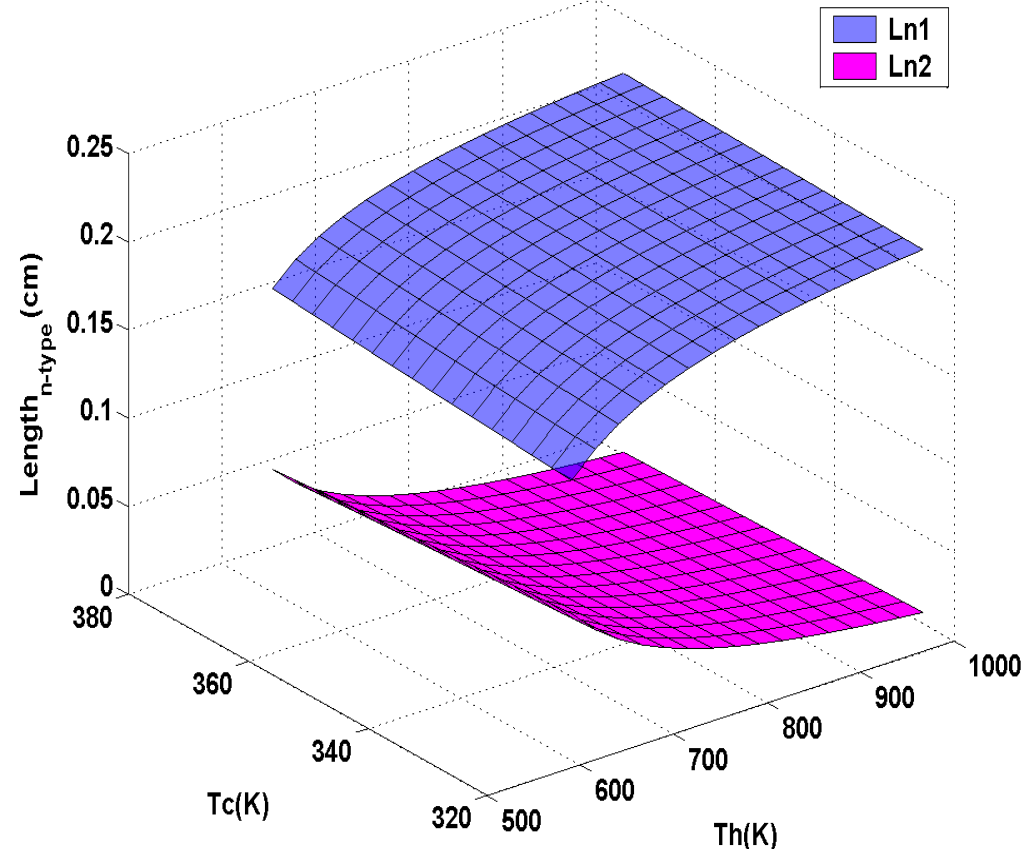
p-Type

Optimized Lengths of p-type Segment (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
 $V=42(\text{volts})$, $UA_h=60(\text{W/K})$, $UA_c=1020(\text{W/K})$, $T_{ex}=973(\text{K})$, $T_{amb}=300(\text{K})$



n-Type

Optimized Lengths of n-type Segment (3p-2n): Ce-Zn-BiTe&CoSb-BiTe
 $V=42(\text{volts})$, $UA_h=60(\text{W/K})$, $UA_c=1020(\text{W/K})$, $T_{ex}=973(\text{K})$, $T_{amb}=300(\text{K})$



Automotive Vehicle Definitions



Dodge Neon
Ford Focus
Honda Civic
Saturn S-Series SL

Ave Power = 120 (hp)
Ave Weight = 2500 (lbs)



Buick LeSabre
Cadillac DeVille
Ford Crown Victoria
Lincoln Continental

Ave Power = 250 (hp)
Ave Weight = 3900 (lbs)



Ford Explorer
Toyota 4 Runner
GMC Envoy
Land Rover Discovery

Ave Power = 211 (hp)
Ave Weight = 4300 (lbs)

Advisor Interface



Vehicle Def.
& Cycle

Avg.
Exhaust
Temp &
Mdoth

Material Props,
Heat Exchanger,
Other Temps,
Voltage,
Resistances

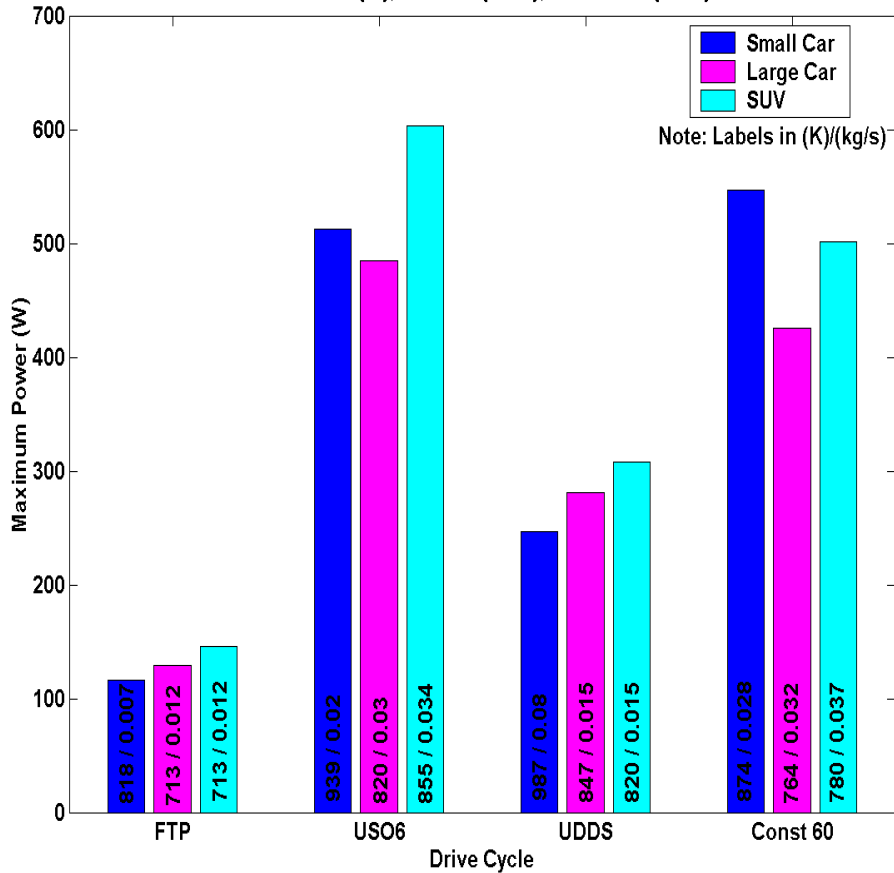
TE Model

Results
Numerical
and
Graphical

Drive Cycle Summary

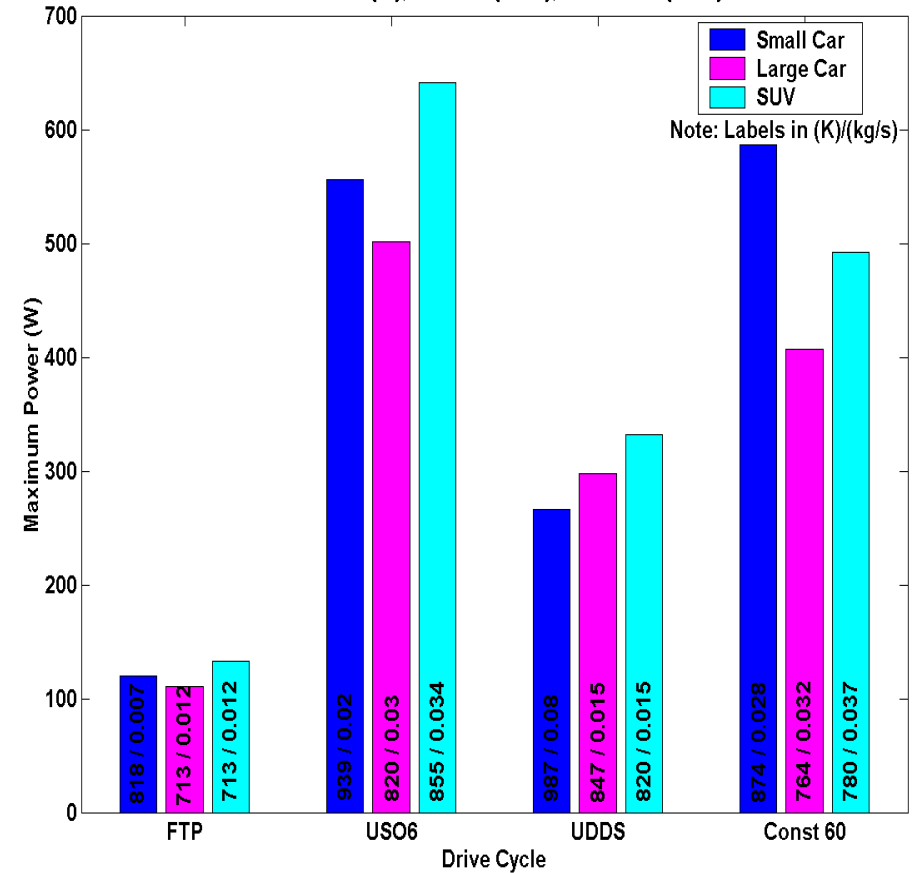
2-2 Drive Cycle Summary

2-2 Maximum Power by Vehical and Drive Cycle
 $T_{amb}=300(K)$, $UA_h=90(W/K)$, $UA_c=8000(W/K)$



3-2 Drive Cycle Summary

3-2 Maximum Power by Vehical and Drive Cycle
 $T_{amb}=300(K)$, $UA_h=90(W/K)$, $UA_c=8000(W/K)$



Heavy-Duty Vehicle Applications

Continuing National Security Issue



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Heavy Duty Diesel Characterization



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2p-2n Diesel (WAVE): Maximums Found

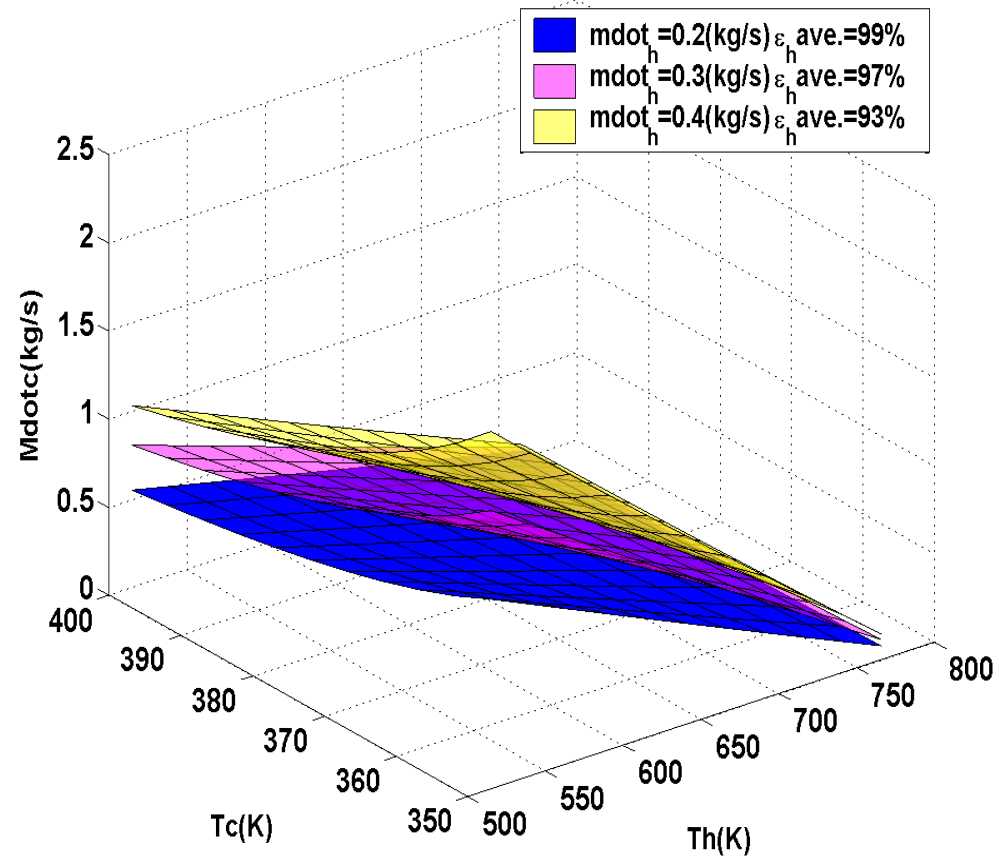
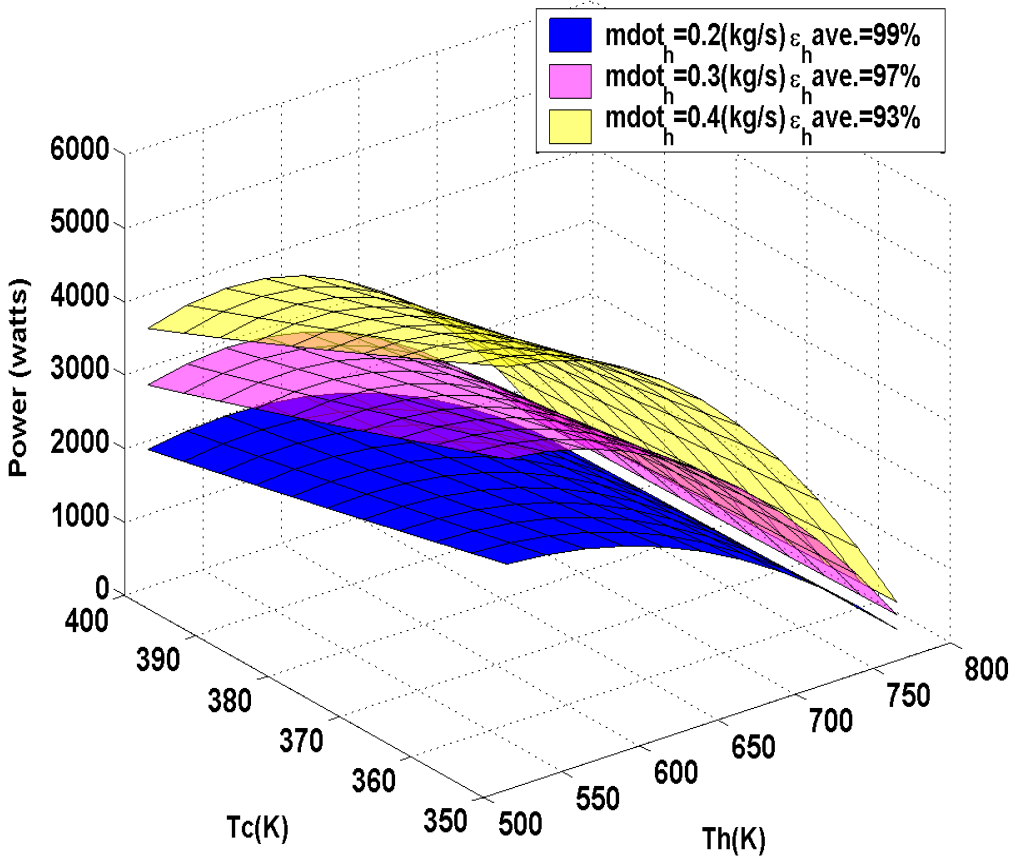
Skutterudite- Bi_2Te_3 & CoSb_3 - Bi_2Te_3

Peak At: 3.1, 4.5, 5.8 (kW)

At Peak P: 1.1, 1.6, 2.0 (kg/s)

Power (2p-2n): Ce-BiTe&CoSb-BiTe Post-Turbo Diesel
 $UA_h = 1150(\text{W/K})$, $UA_c = 10560(\text{W/K})$, $T_{ex} = 785(\text{K})$, $T_{amb} = 300(\text{K})$

Required Ambient Mdot (2p-2n): Ce-BiTe&CoSb-BiTe Post-Turbo Diesel
 $UA_h = 1150(\text{W/K})$, $UA_c = 10560(\text{W/K})$, $T_{ex} = 785(\text{K})$, $T_{amb} = 300(\text{K})$



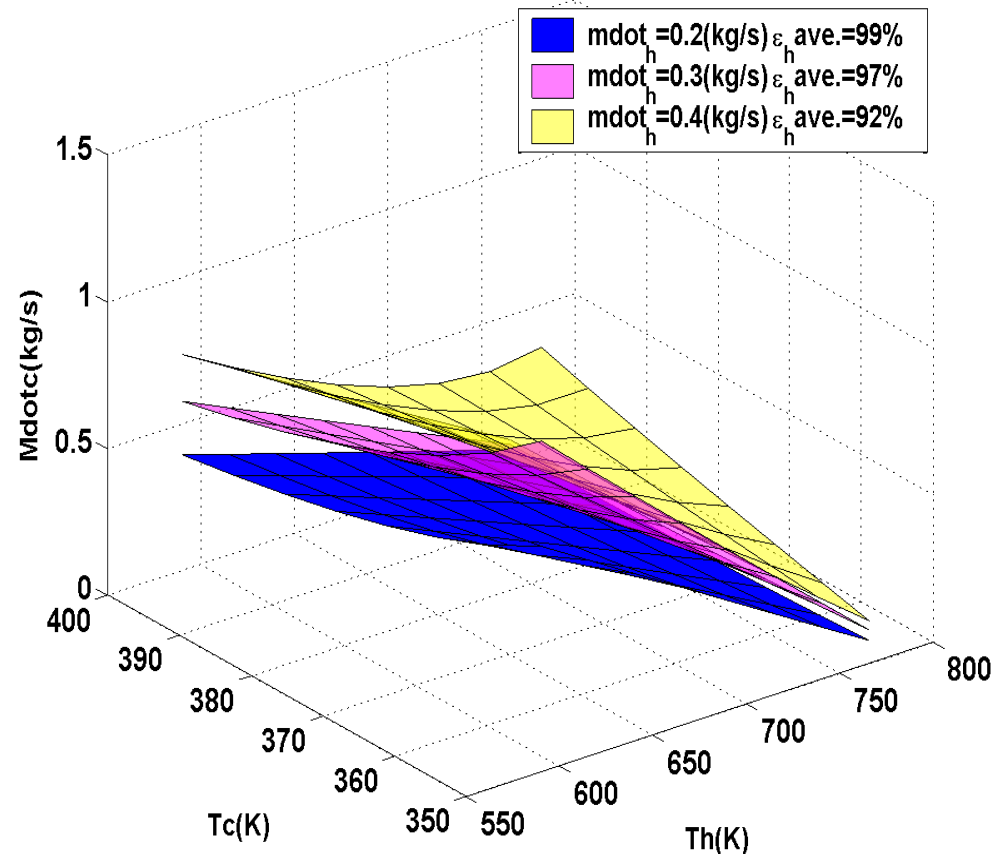
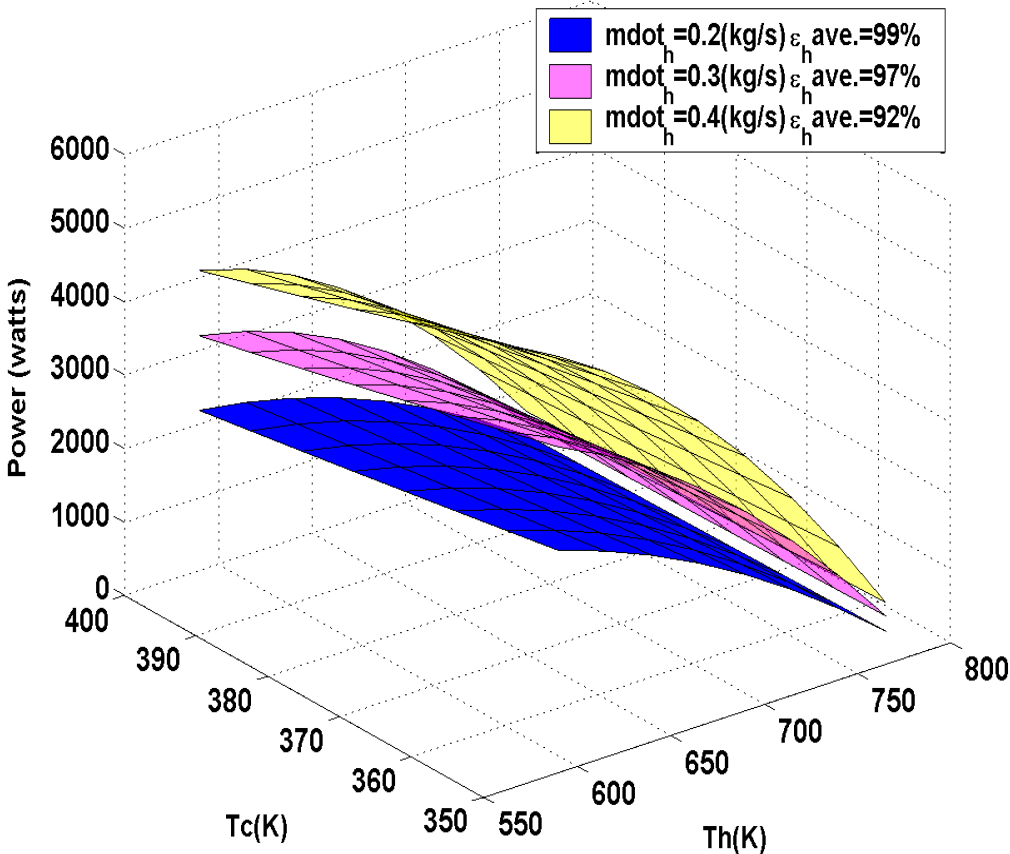
3p-2n Diesel (WAVE): Maximums Found Skutterudite- Zn_4Sb_3 - Bi_2Te_3 & $CoSb_3$ - Bi_2Te_3

Peak Power: 3.0, 4.4, 5.7 (kW)
Decrease from 2p-2n ~ 2-3%

At Peak P: 0.77, 1.1, 1.4 (kg/s)
Decrease from 2p-2n ~ 30%

Power (3p-2n): Ce-ZnSb-BiTe&CoSb-BiTe Post-Turbo Diesel
 $UA_h = 1150(W/K)$, $UA_c = 7520(W/K)$, $T_{ex} = 785(K)$, $T_{amb} = 300(K)$

Required Ambient Mdot (3p-2n): Ce-ZnSb-BiTe&CoSb-BiTe Post-Turbo Diesel
 $UA_h = 1150(W/K)$, $UA_c = 7520(W/K)$, $T_{ex} = 785(K)$, $T_{amb} = 300(K)$



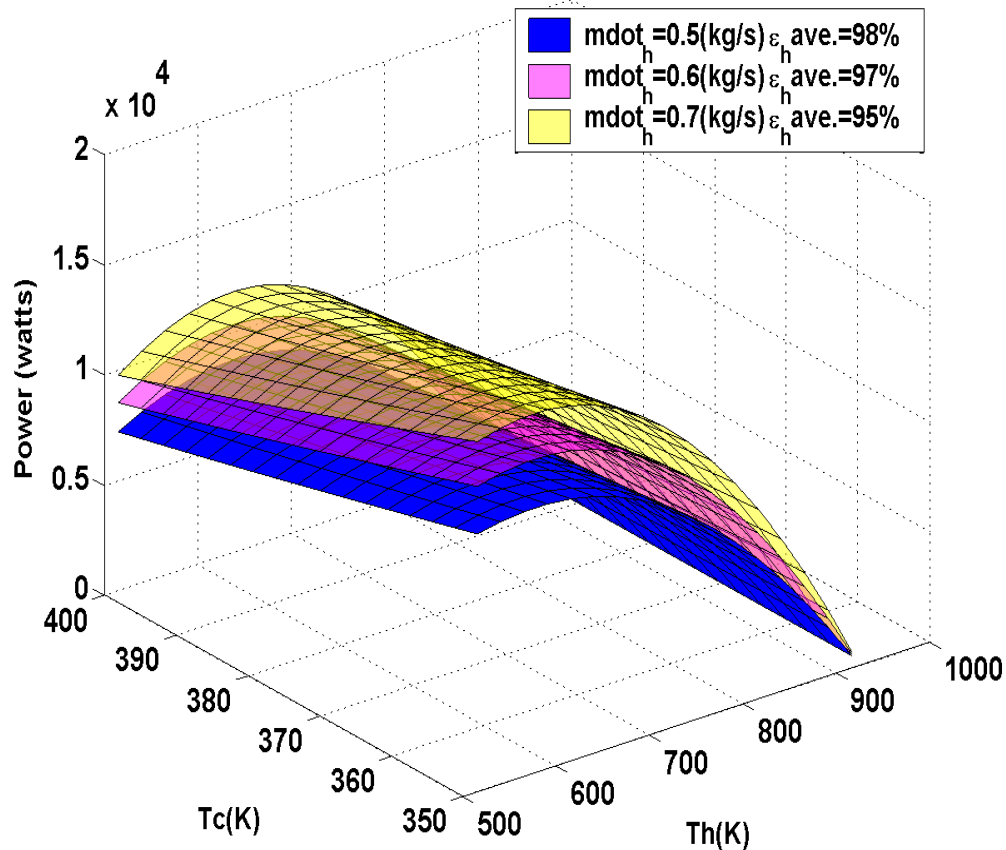
2p-2n Diesel (Cat): Maximums Found

Skutterudite- Bi_2Te_3 & CoSb_3 - Bi_2Te_3

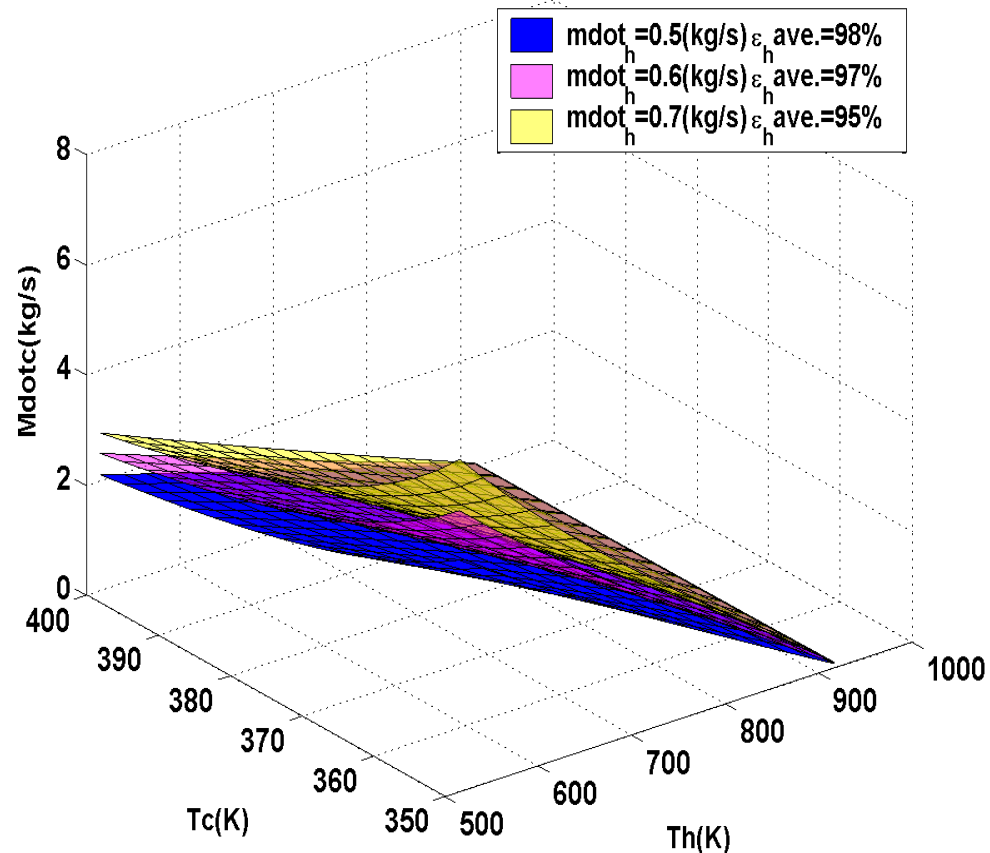
Peak At: 12.0, 14.2, 16.3 (kW)

At Peak P: 3.6, 4.2, 4.8 (kg/s)

Power (2p-2n): Ce-BiTe&CoSb-BiTe Caterpillar
 $UA_h = 2400(\text{W/K})$, $UA_c = 15400(\text{W/K})$, $T_{ex} = 923(\text{K})$, $T_{amb} = 300(\text{K})$



Required Ambient \dot{m}_{dot} (2p-2n): Ce-BiTe&CoSb-BiTe Caterpillar
 $UA_h = 2400(\text{W/K})$, $UA_c = 15400(\text{W/K})$, $T_{ex} = 923(\text{K})$, $T_{amb} = 300(\text{K})$



3p-2n Diesel (Cat): Maximums Found

Skutterudite- Zn_4Sb_3 - Bi_2Te_3 & $CoSb_3$ - Bi_2Te_3

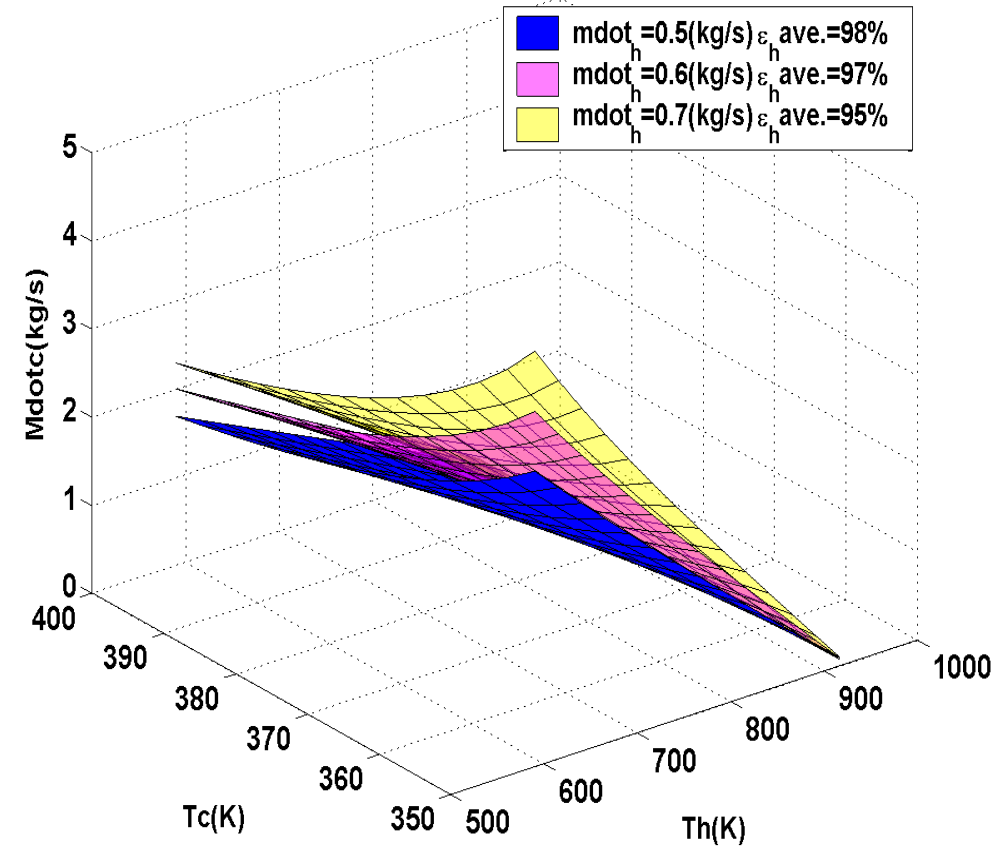
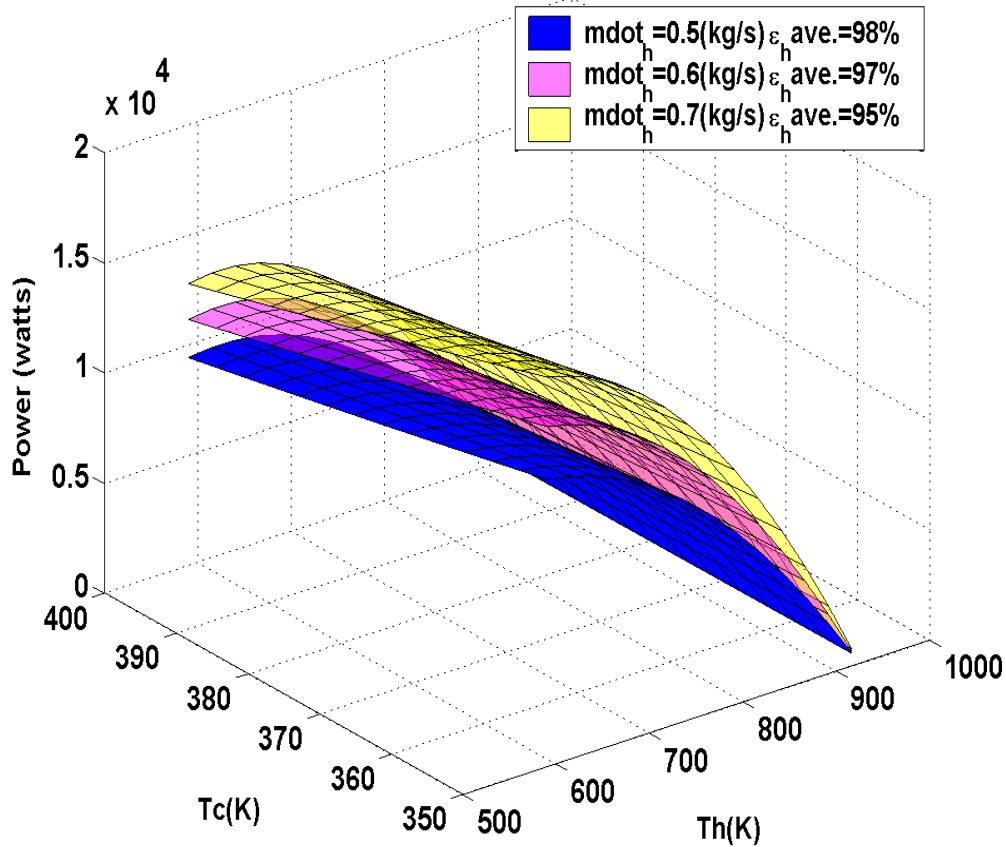


Peak At: 13.0, 15.4, 17.6 (kW)
Increase from 2p-2n ~ 8%

At Peak P: 3.3, 3.9, 4.5 (kg/s)
Decrease from 2p-2n ~ 6-8%

Power (3p-2n): Ce-ZnSb-BiTe&CoSb-BiTe Caterpillar
 $UA_h = 2400(W/K)$, $UA_c = 14200(W/K)$, $T_{ex} = 923(K)$, $T_{amb} = 300(K)$

Required Ambient Mdot (3p-2n): Ce-ZnSb-BiTe&CoSb-BiTe Caterpillar
 $UA_h = 2400(W/K)$, $UA_c = 14200(W/K)$, $T_{ex} = 923(K)$, $T_{amb} = 300(K)$



Diesel (Cat): Peak Power Not At Peak Eff.

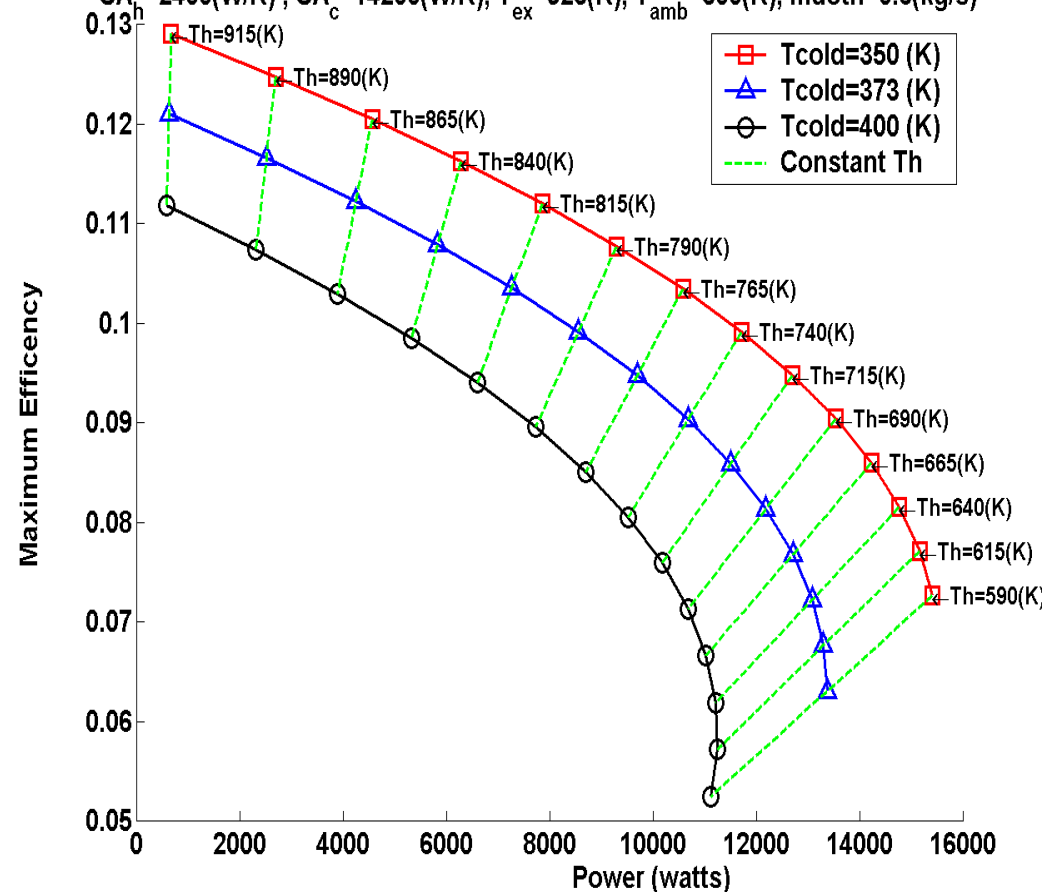
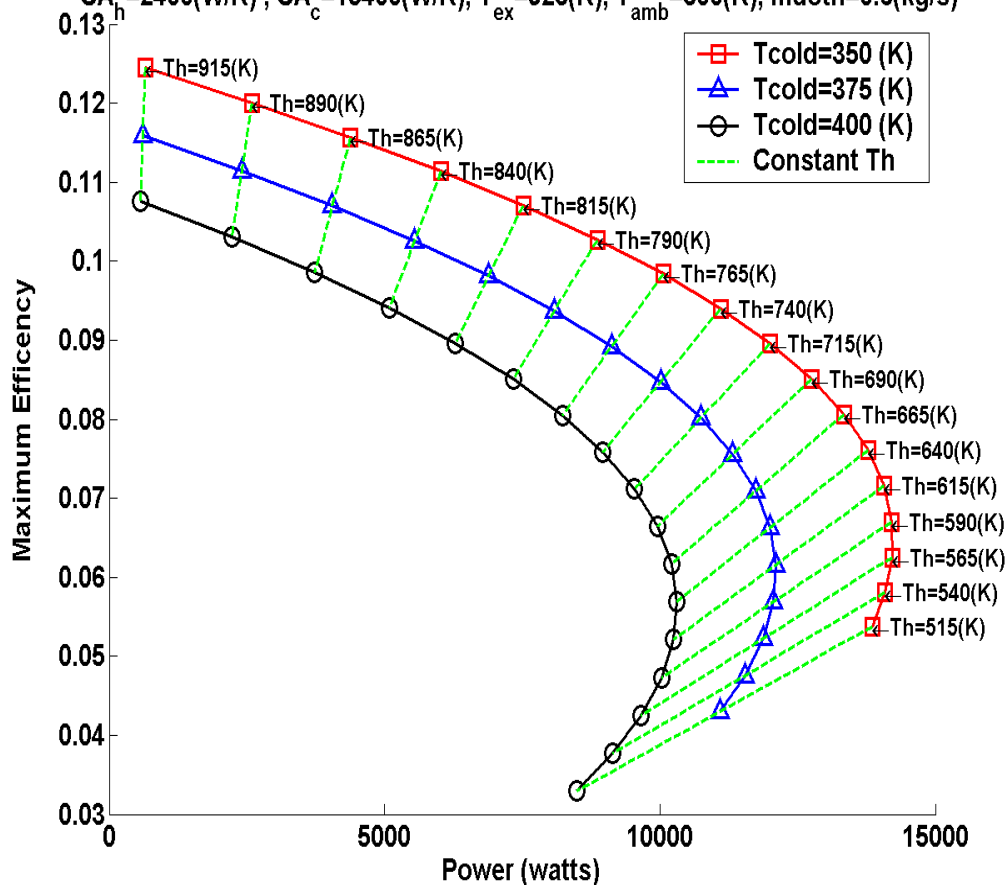
Skutterudite-(Zn_4Sb_3)- Bi_2Te_3 & $CoSb_3$ - Bi_2Te_3

Middle Mdoth (0.3 kg/s)

Higher Efficiency & Higher Power

Efficiency At Maximum Power (2p-2n): Ce-BiTe&CoSb-BiTe Caterpillar
 $UA_h = 2400(W/K)$, $UA_c = 15400(W/K)$, $T_{ex} = 923(K)$, $T_{amb} = 300(K)$, $m_{doth} = 0.6(kg/s)$

Efficiency At Maximum Power (3p-2n): Ce-ZnSb-BiTe&CoSb-BiTe Caterpillar
 $UA_h = 2400(W/K)$, $UA_c = 14200(W/K)$, $T_{ex} = 923(K)$, $T_{amb} = 300(K)$, $m_{doth} = 0.6(kg/s)$



2p-2n Diesel (Cat): Maximums Found

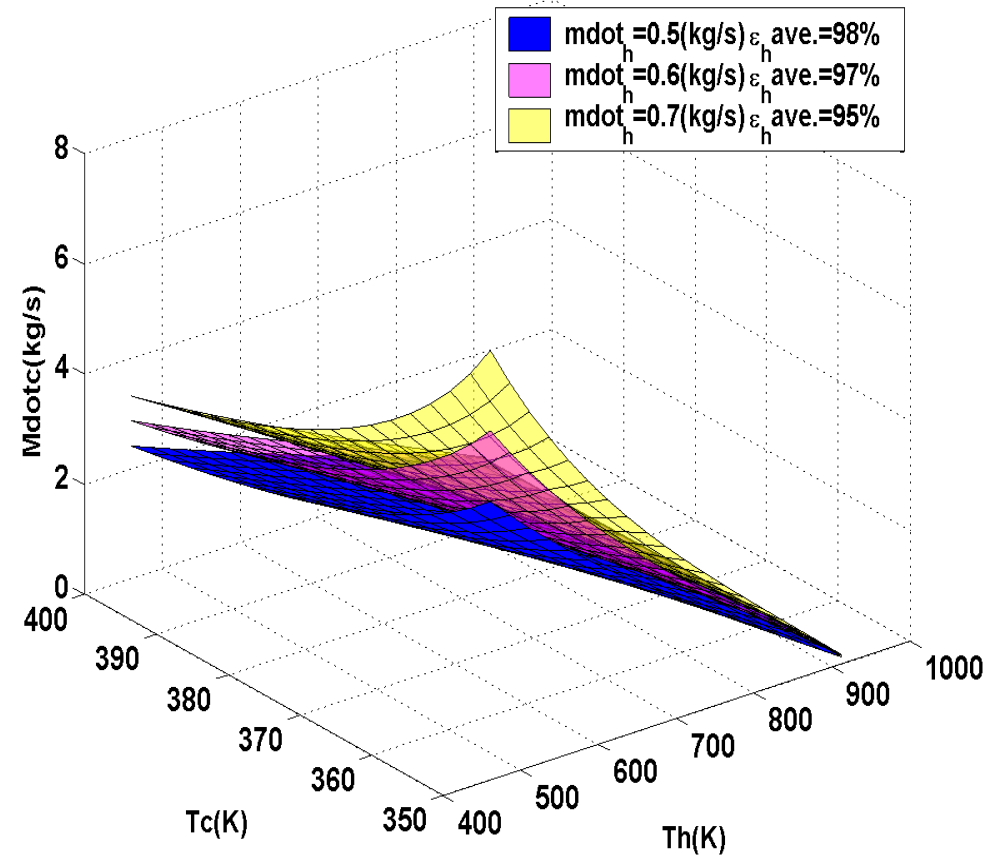
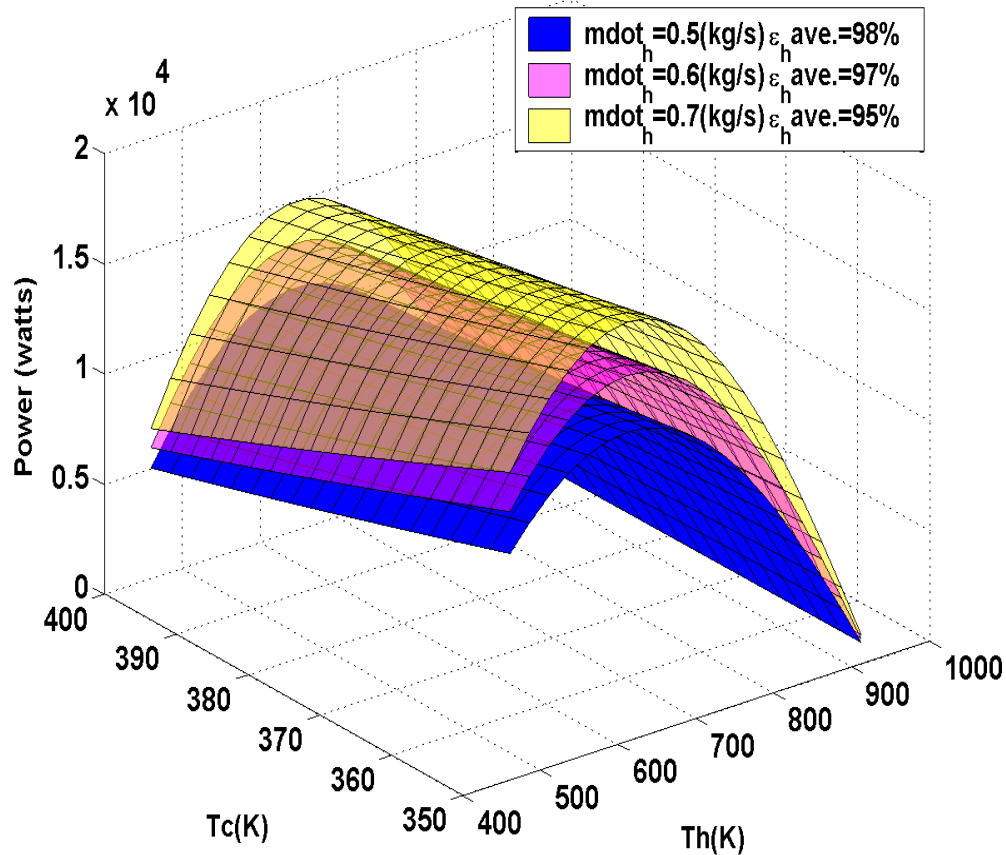
TAGS-Bi₂Te₃ & 2NPbTe-Bi₂Te₃

Peak At: 14.0, 16.6, 19.0 (kW)
 Increase from 1st Material Set ~ 17%

At Peak P: 3.1, 3.6, 4.2 (kg/s)
 Decrease from 1st Material Set ~13-14%

Power (2p-2n): TAGS-BiTe&2NPbTe-BiTe Caterpillar
 UA_h =2400(W/K), UA_c =13230(W/K), T_{ex} =923(K), T_{amb} =300(K)

Required Ambient Mdot (2p-2n): TAGS-BiTe&2NPbTe-BiTe Caterpillar
 UA_h =2400(W/K), UA_c =13226(W/K), T_{ex} =923(K), T_{amb} =300(K)



2p-2n (Diesel WAVE): Maximums Found

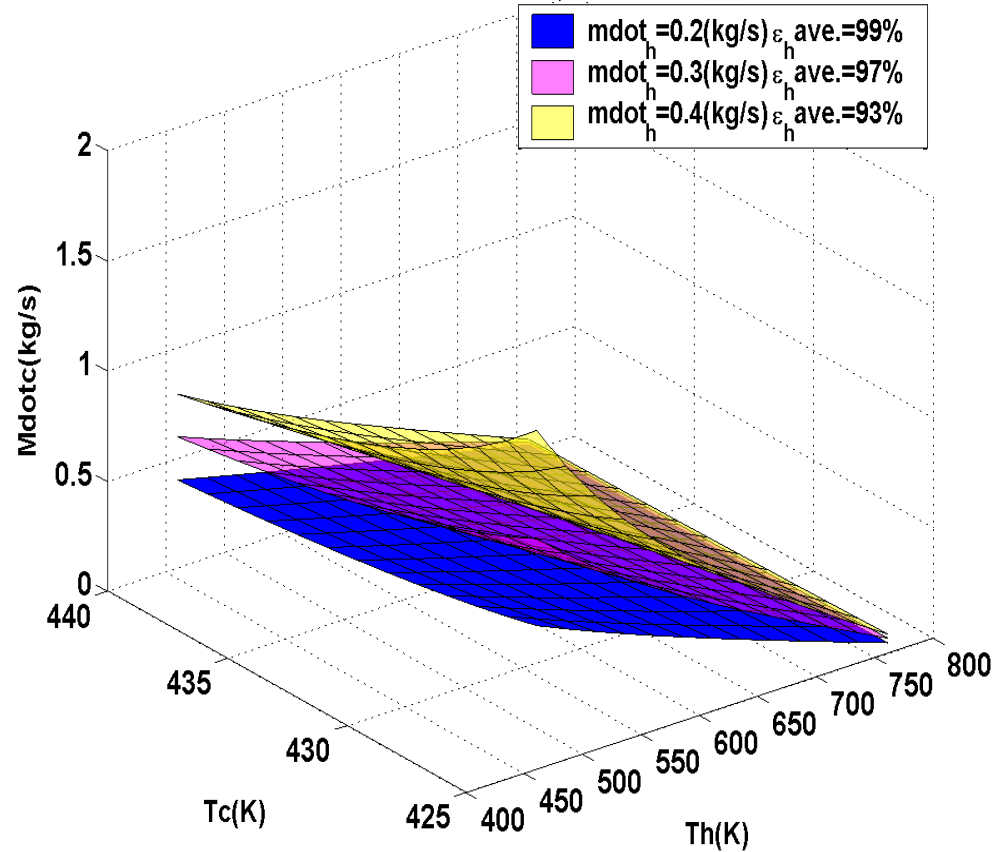
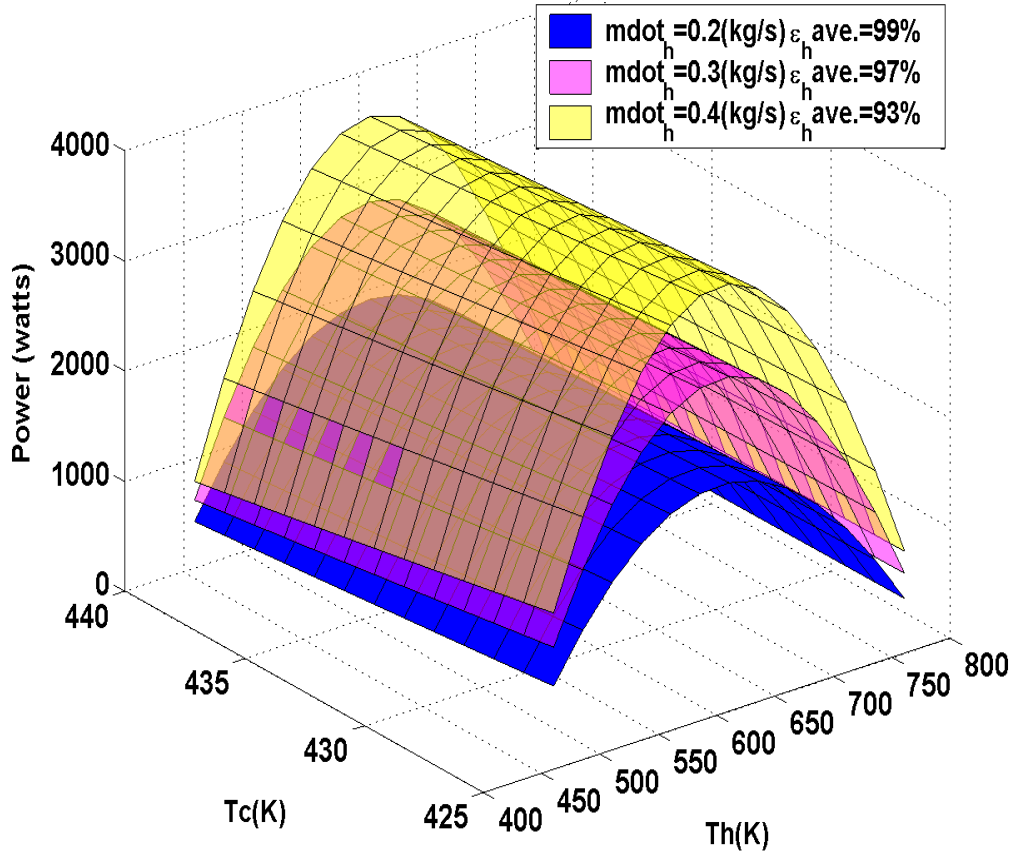
TAGS-Bi₂Te₃ & 2NPbTe-Bi₂Te₃ Water Cooled

Peak At: 2.1, 3.0, 3.9 (kW)
 Decrease from Air Cooled ~ 37 %

At Peak P: 0.33, 0.49, 0.64 (kg/s)

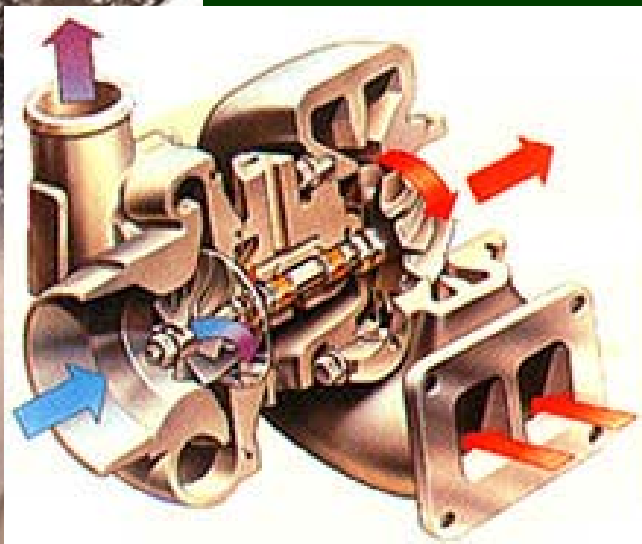
Power (2p-2n): TAGS-BiTe&2NPbTe-BiTe Post-Turbo Diesel Water Cooled
 UA_h =1150(W/K), UA_c =9700(W/K), T_{ex} =785(K), T_{amb} =400(K)

Required Ambient Mdot (2p-2n): TAGS-BiTe&2NPbTe-BiTe Post-Turbo Diesel Water Cooled
 UA_h =1150(W/K), UA_c =9700(W/K), T_{ex} =785(K), T_{amb} =400(K)



Turbocharger Configuration

High Pressure Loop Exhaust Gas Recirculation



Power Available
~ 500-600 Watts

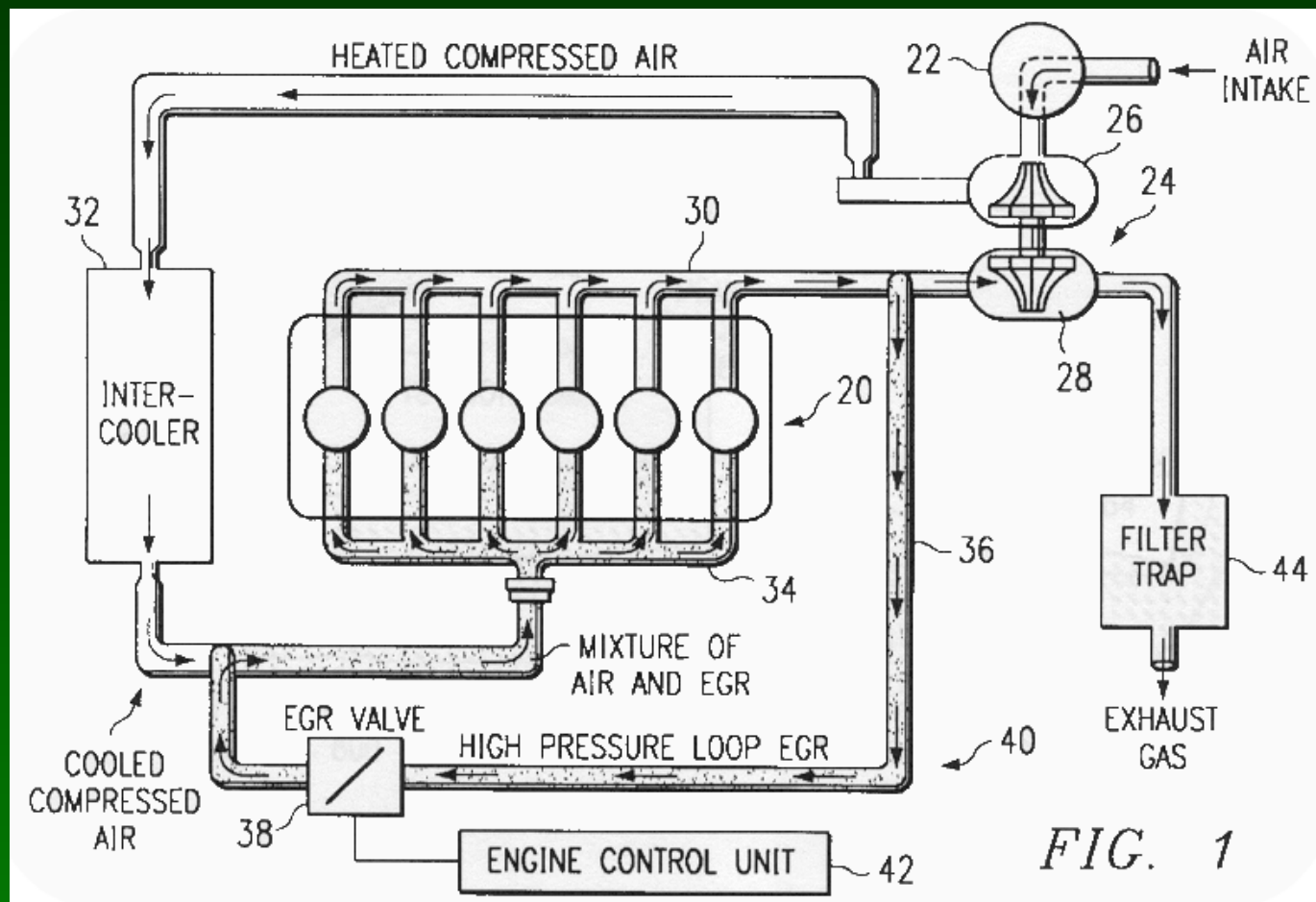


FIG. 1

How Much Fuel Can Be Saved?

- Potential to Recover 8-10%
 - Light Duty
 - 45 Billion Gallons Out the Exhaust
 - Save **30 Billion** Gallons/Year
 - Heavy Duty
 - Save **1.3 Billion** Gallons/Year
 - 5 kW TE System



Technical Challenges in Automotive Applications

- Cost
- Material Interface Contacts
 - Electrical Resistance
 - Structural Ruggedness - Shock & Vibration
 - Thermal Expansion
 - Thermal Diffusion
- Tailor TEG Systems to Vehicle Systems & Requirements
 - Design/Fabricate For New TE Materials
 - Establish TE System Cost Basis
- Location for Optimal Heat Recovery
- Maintaining Relatively Constant Cold Side Temperatures
- Maximum Power Output is at Maximum Engine Output
 - Not Necessarily Synchronized With Times of Maximum Power Requirement
 - Requires Energy Storage (e.g., batteries)
- Establish Supplier Infrastructure
 - TE Materials, System Fabrication, System Testing

Conclusions

- WHR Applications Currently In Light-Duty & Heavy-Duty Vehicles
 - Automotive Exhaust Waste Heat Recovery
 - Heavy-Duty Vehicle APUs, Truck Electrification, & Anti-Idling
- Heat Exchanger / Thermoelectric Device Design Analyzed & Optimized Simultaneously Within ADVISOR for Vehicle-Level Studies
 - Design Issues Identified Simultaneously
 - Design Requirements Identified Simultaneously
- Heat Exchanger / TE Device Tradeoffs
 - Maximum Power Near $T_h = 625$ K
 - Cold Side Mass Flow Rates Could Be Challenging
 - Optimum Design Regimes Exist (TE Performance & Cold Mass Flow Reasons)
 - TE Materials Strongly Impact Thermal System Design
 - Heavy Duty Power Potential Higher Than Light Duty Vehicle Power
 - Exhaust Temperature Constraints May Limit Need for 3p-2n Elements
 - Thermal Interfaces & Thermal Losses Could Limit Power Potential (Be Smart!)

Acknowledgments

- Sincerest Thanks to:
 - Dr. Thierry Caillat, NASA-JPL
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- Test:

Continuing National Security Issue



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