

Time for World Class Solutions

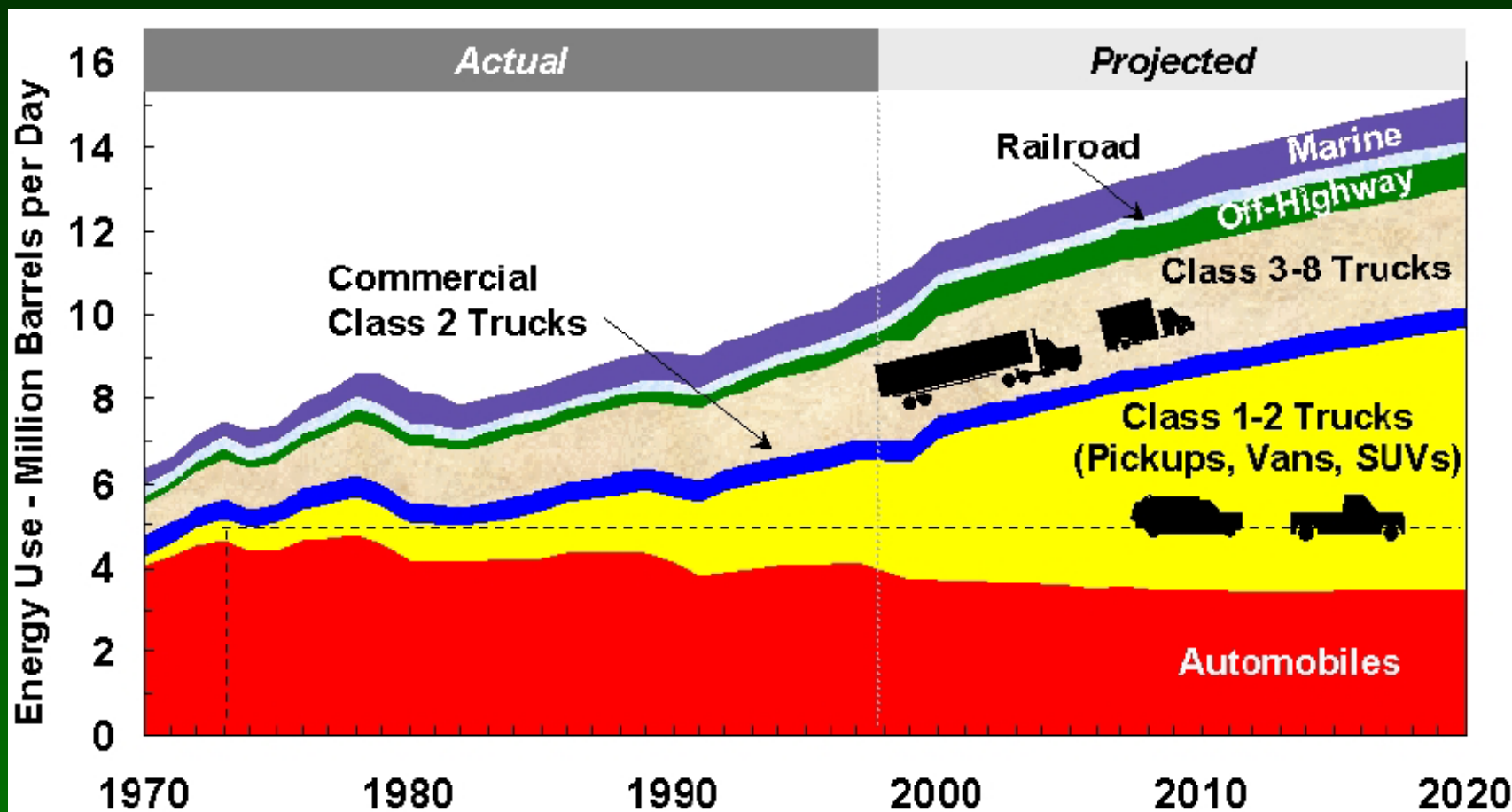
Advanced Thermoelectric Energy Recovery Systems in Future Vehicle Systems

DOE/EPRI High-Efficiency Thermoelectrics Workshop
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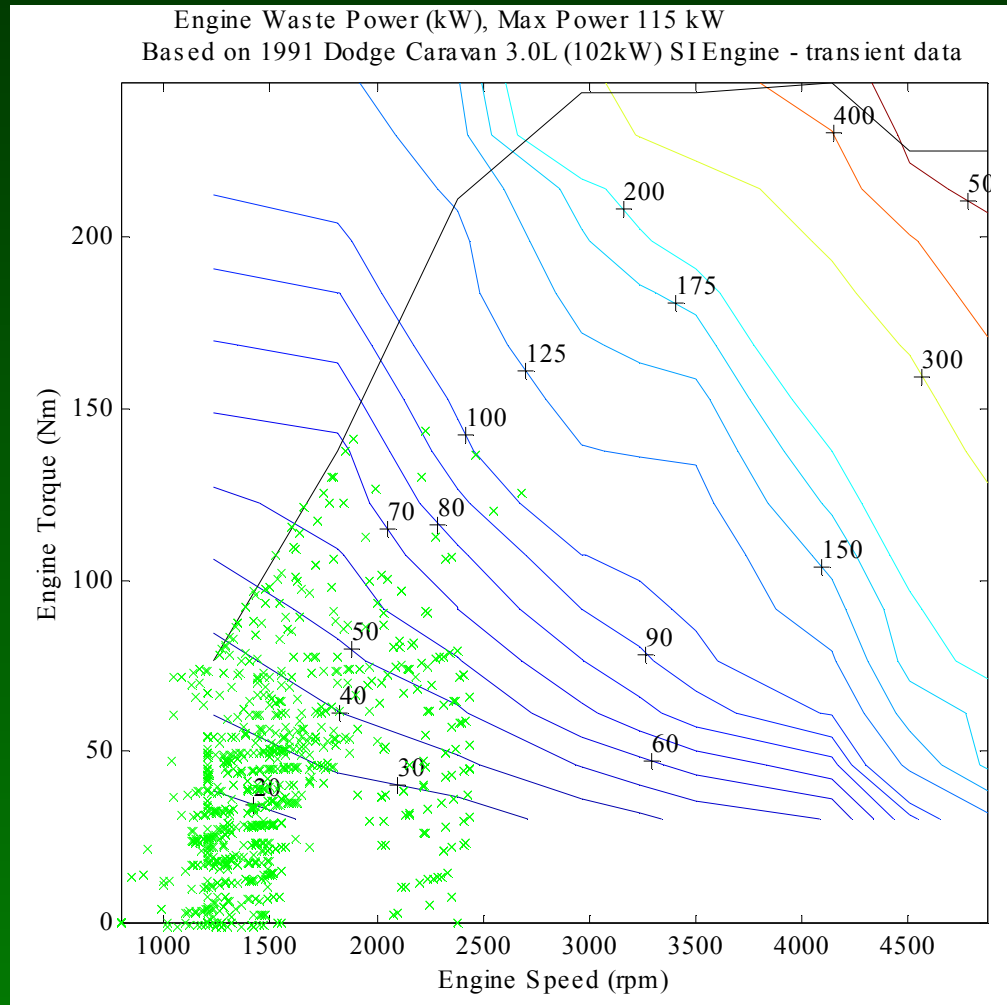
Breakdown of US Historical and Projected Fuel Use by Platform



Sources: *EIA Annual Energy Outlook 2000*, DOE/EIA-0383(2000), December 1999
Transportation Energy Data Book: Edition 20, DOE/ORNL-6959, October 2000

Waste Power Available in Representative 115 kW Engine

- 20-400 kW Waste Power Available Across The Engine Map
- Average of 23 kW Over an FTP Drive Cycle



Objective

Low Grade Thermal
Energy From Various
Automotive Systems



High Grade Electrical
Energy To Operate
Various Automotive Systems

- Relatively Low Cost
- Passive System
 - No Noise
 - No Vibration
- High Reliability
- Ideally No Fluids

Advanced Thermoelectric Systems

- **Convert Waste Thermal Energy Into High-Grade Electrical Energy**
 - Completely Solid State
 - No Moving Parts or Fluids
 - No Noise or Vibration
- **Latest Thermoelectric Materials Offer New Opportunity**
 - Skutterudites
 - Zn-Sb alloys
 - Quantum-Well Materials
 - Quantum Dots, 1-D Quantum Wires, 2-D Thin Film Superlattices
- **Automotive Exhaust Heat Temperatures 600-650 °C**
 - Interested in ~1000 W System
- **Heavy Vehicle Exhaust Heat Temperatures 500-550 °C**
 - APUs
 - Truck Electrification

Advisor Interface



Light-Duty Vehicle Applications

Continuing National Security Issue

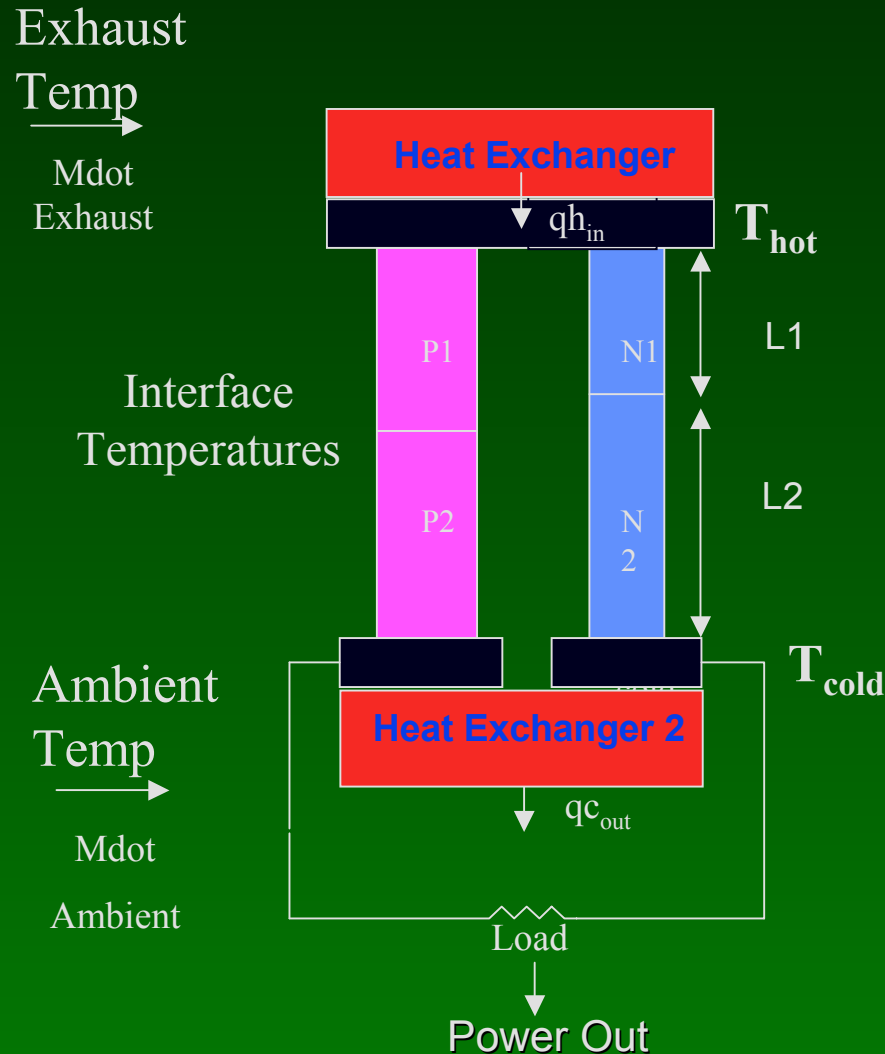


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Advanced Thermoelectric System Design

- Initially Investigated Segmented TE Couple Designs
- Light-Duty & Heavy-Duty Vehicles



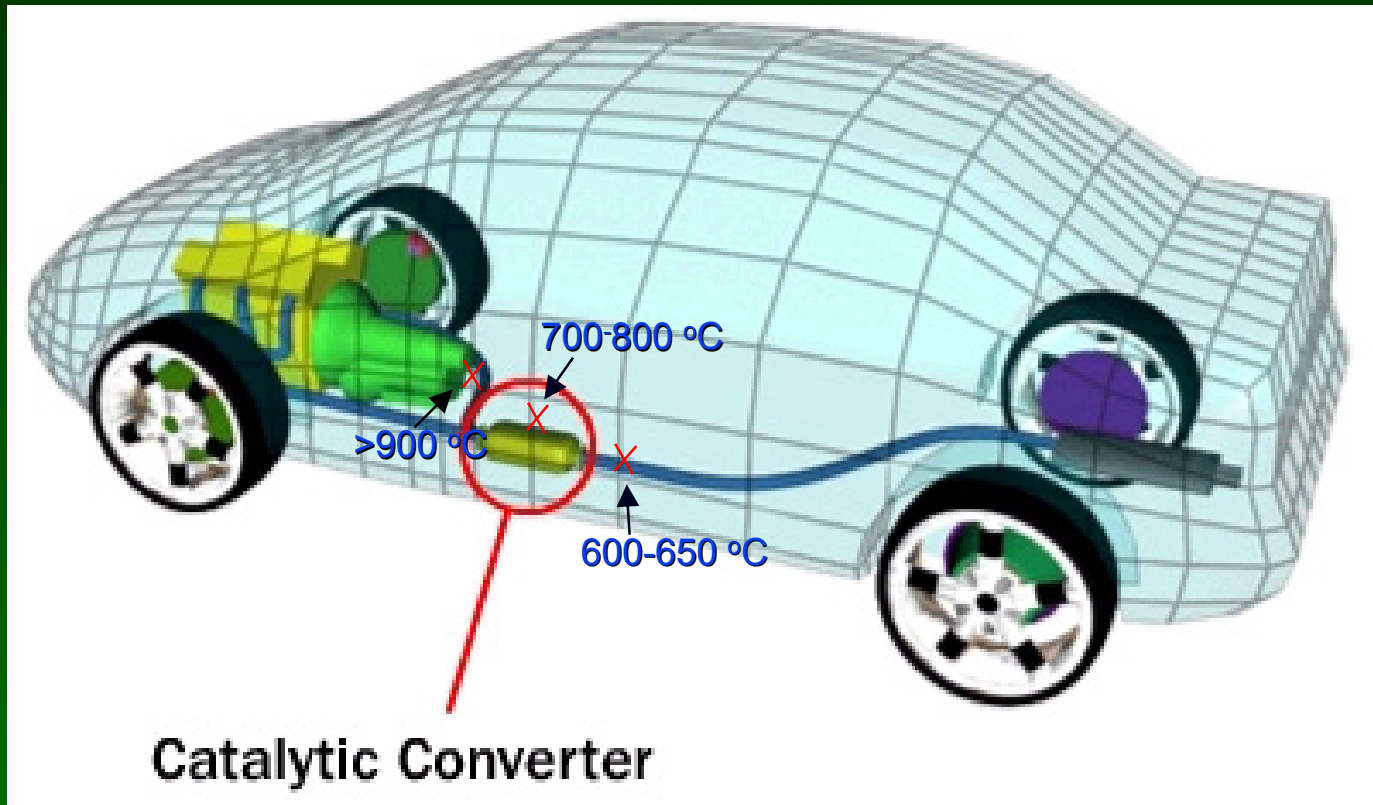
P1=CeFeSb

P2=BiTe

N1=CoSb

N2=BiTe

System Placement



Light Duty Automotive Vehicle Studies



Dodge Neon
Ford Focus
Honda Civic
Saturn S-Series SL

Ave Power = 120 (hp)
Ave Weight = 2500 (lbs)



Buick LeSabre
Cadillac DeVille
Ford Crown Victoria
Lincoln Continental

Ave Power = 250 (hp)
Ave Weight = 3900 (lbs)



Ford Explorer
Toyota 4 Runner
GMC Envoy
Land Rover Discovery

Ave Power = 211 (hp)
Ave Weight = 4300 (lbs)

See Hendricks & Lustbader, 2002, 2003 [1-3]

Advanced Heavy Hybrid Vehicle Applications

Continuing National Security Issue



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Advanced Heavy Hybrid Propulsion Systems (AH²PS)

- **AH²PS Requires High-Grade Electrical Energy Sources from Waste Heat Recovery**
 - Secondary Energy Storage Charging – SOC Maintenance
 - Minimize Engine Use for Energy Storage Charging
 - Powering Auxiliary Loads
- **Long-Term (Phase II) Need for Next-Generation Heavy Hybrid Technology**
 - Advanced Thermoelectric Systems Offer Unique Opportunity
- **Time is Critical – Must Start Now to Have Any Hope of Having Viable Systems in Time to Impact Heavy Vehicle Hybridization**
 - TE Material R&D is Critical
 - Device-Level and System-Level R&D is Critical

Critical Technical Issues

➤ **Heat Exchanger / TE Device Integration**

- Potential Electrical Power Available
- Thermal / Power Integration
- Physical Integration
 - How Big Could it Be? How Does It Fit Together?
- Thermal & Structural Interfaces
 - It Is Never Too Early to Start Thinking About This!
- Physical Location on a Vehicle

➤ **Exhaust Mass Flow Effects** — Variation in Flow & Temperature

➤ **Cooling Mass Flow Effects**

- Air-Cooled vs. Water-Cooled

➤ **TE Material Combinations & Effects on Performance**

- What's Best From Performance, Cost, Vehicle Integration

NREL System-Level Investigations in AH²PS Program

➤ **Preliminary Advanced TE System Analyses**

- Exhaust Temperature & Mass Flow Rate Conditions in a Typical AH²PS Vehicle Case
- Realistic Power Estimates
 - Accounting for Integrated Performance Effects
- Preliminary System Sizing
- Vehicle Systems Location Analysis
 - Exhaust Stream
 - Turbo Charger
 - EGR
- Estimate Vehicle-Level Benefits
- Material Property Effects on System Benefits & Performance

➤ **Integrate With AH²PS Project in Out Years**



Table 1 – Thin-Film Multi-Layer Thermoelectric Properties @ 300 °K [5]

	Seebeck Coefficient [10^{-6} V/K]	Electrical Resistivity [Ohm-cm]	Thermal Conductivity [W/m-K]
Si/SiGe n-type	950	0.005	1.0-1.5
Si/SiGe n-type	900	0.0083	1.0-1.5
B ₉ C/B ₄ C p-type	800	0.020	1.0-1.5

(ZT) \approx 1.1-1.6

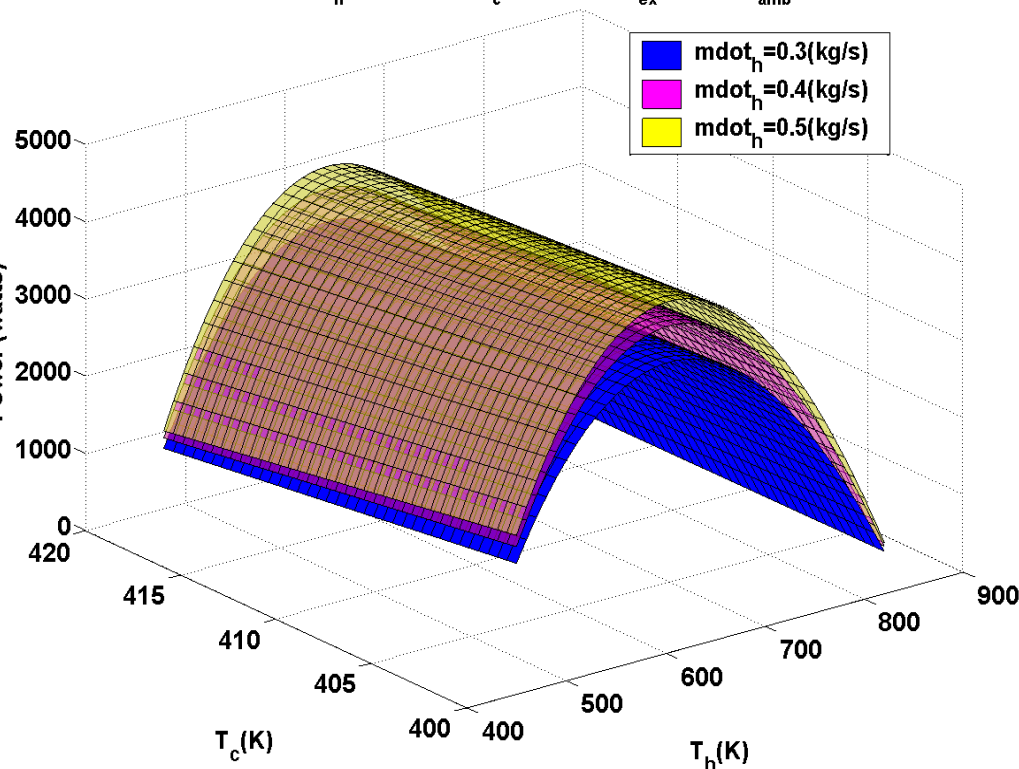
(ZT) \approx 1.4-2.0

Acknowledgement to Peter Martin & L.C. Olsen, PNNL, DEER 2003 , Newport, RI

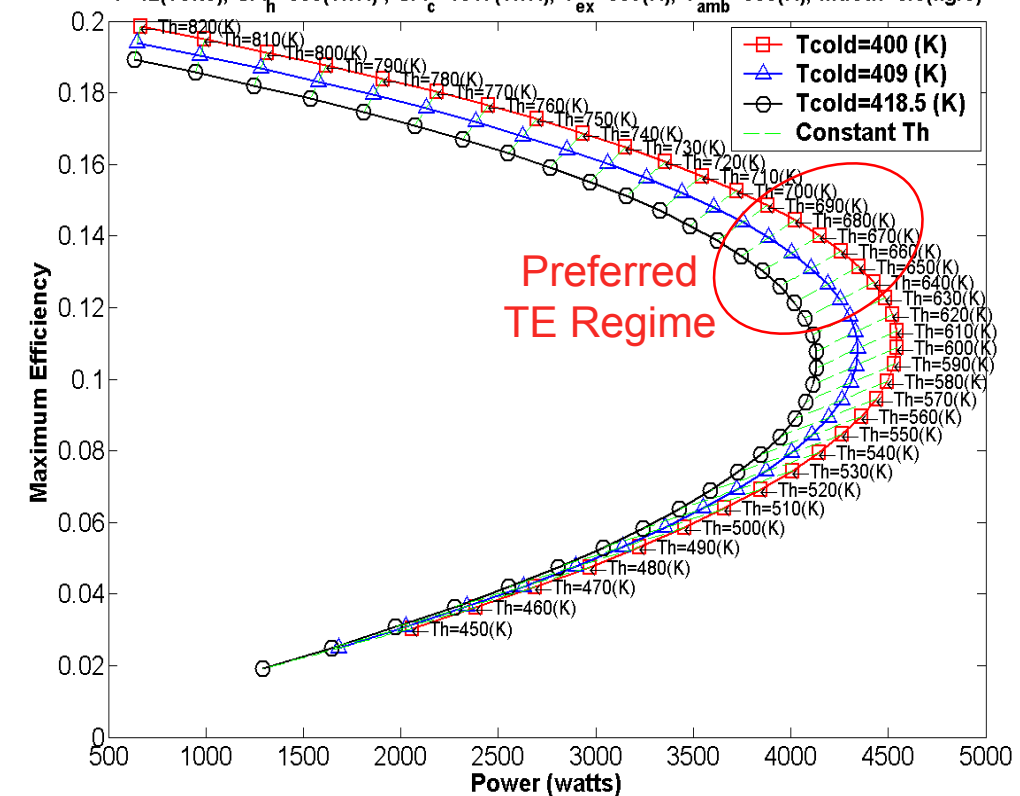
Potential Power Output & Efficiency

- Peak Powers in Optimized Systems: 4000-4500 Watts @ 12%
- Heat Exchanger & TE Device Interaction
- Peak Power & Peak Efficiency At Distinctly Different Points

Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ωm), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=800$ (W/K), $UA_c=1517$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K)

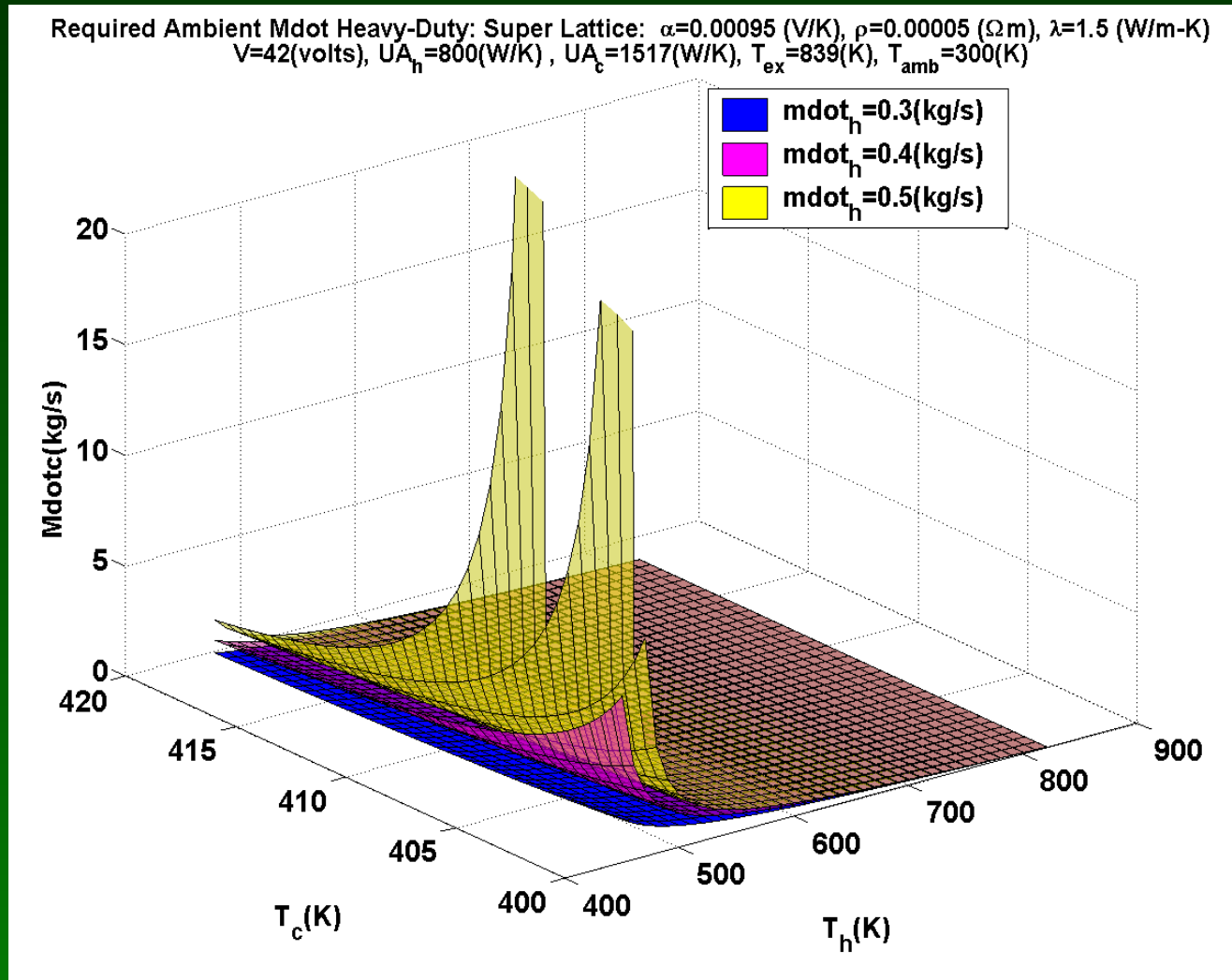


Efficiency At Maximum Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ωm), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=800$ (W/K), $UA_c=1517$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K), $\dot{m}_{th}=0.5$ (kg/s)



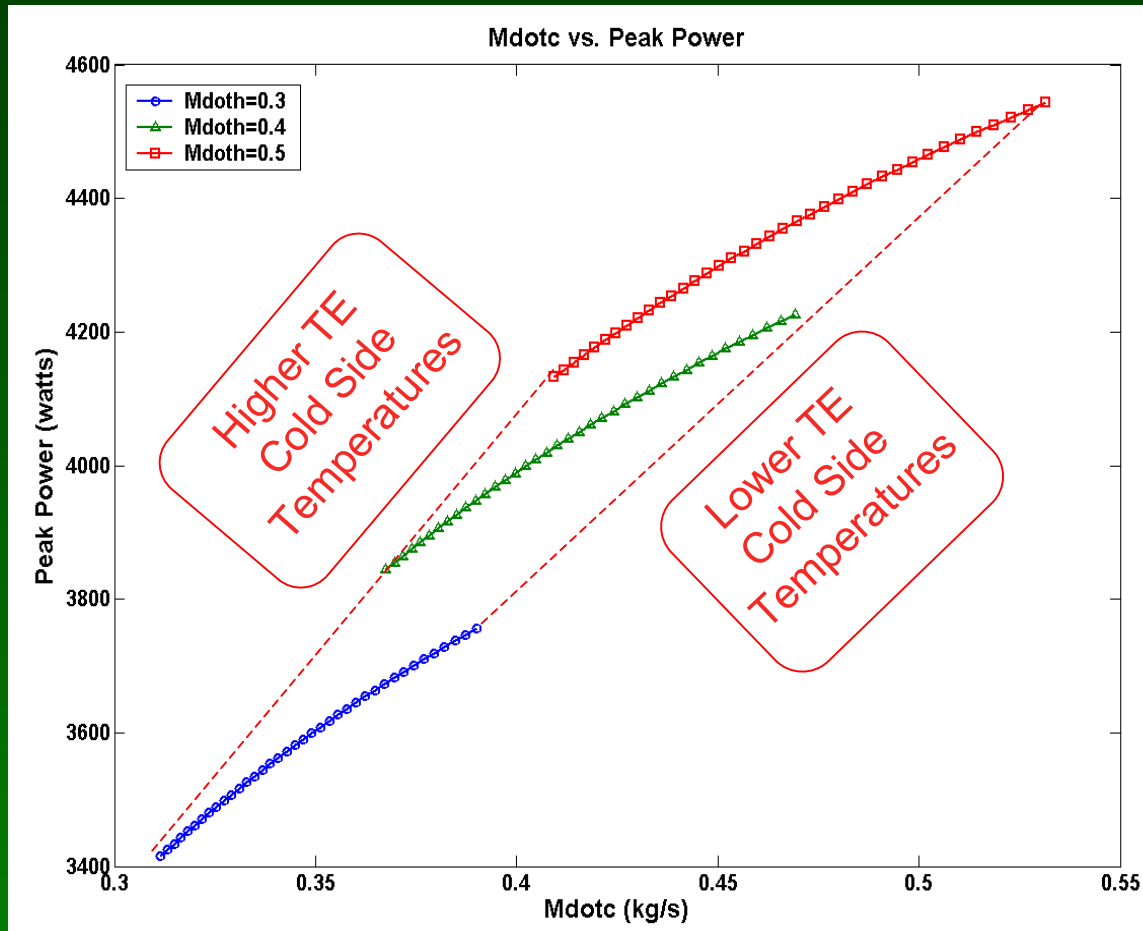
Cold Side Mass Flow Requirements

Preferred Temperature Regimes Due to Cold Side Cooling Requirements



Peak Power / Cooling Mass Flow Relationship

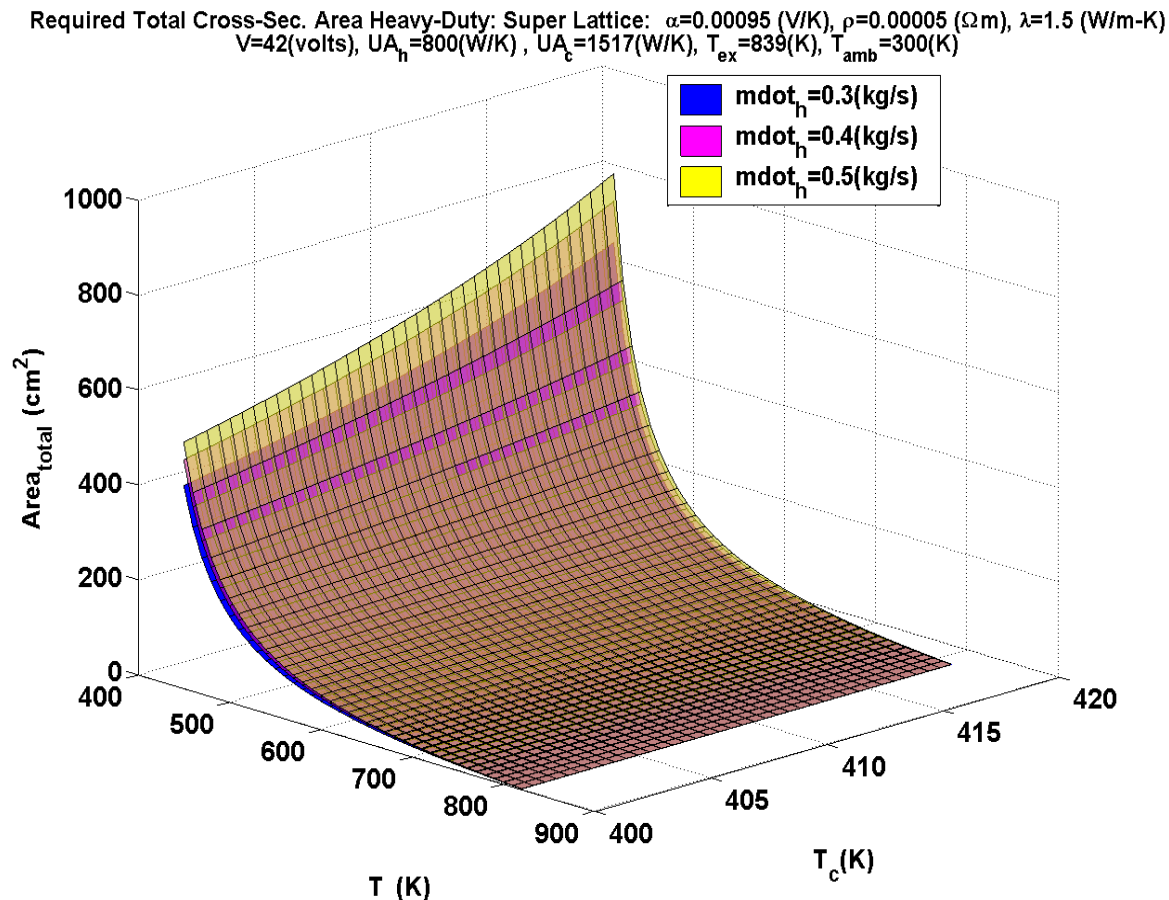
- Peak Power/Cooling Mass Flow Map Driven By TE Temperatures
- Increasing Exhaust Mass Flow Rate \rightarrow Higher Power Output, But Diminishing Returns Are Evident (Application Specific)



Optimum TE Device Area Requirements

- Optimum TE Device Area: Depends on Final Element Lengths (Probably 50-600 cm² at Peak Power Points)
- Heat Exchangers Likely Much Bigger
- Thermal Funneling Effects in System Design

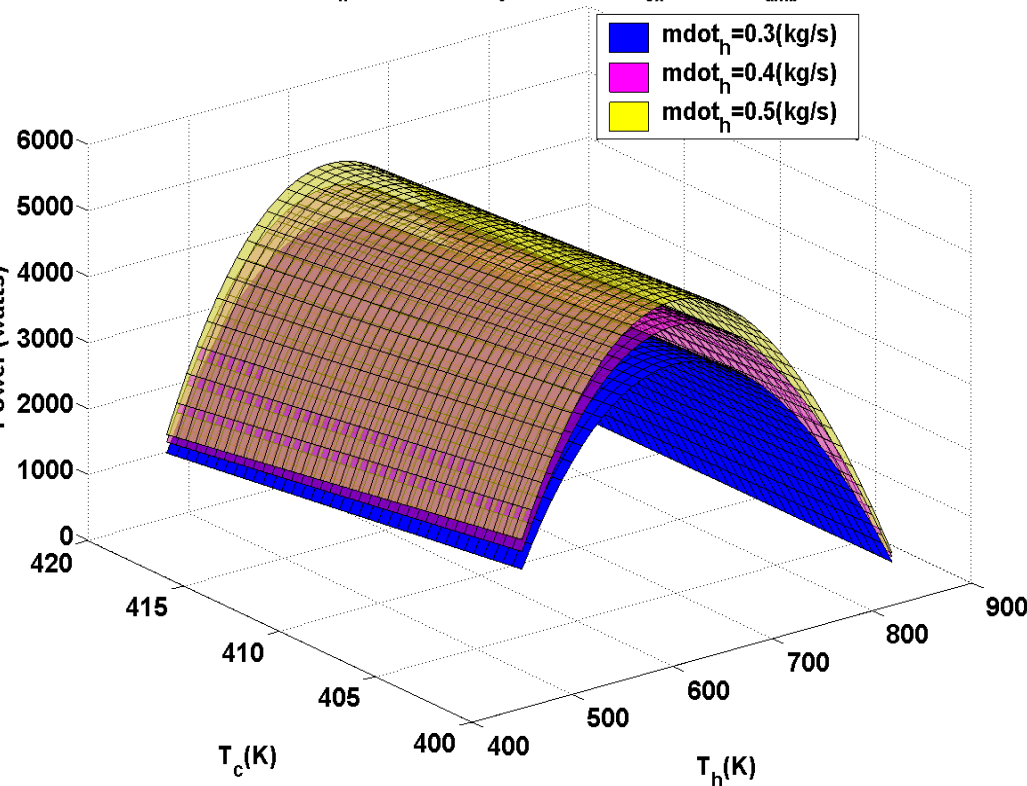
TE Element Length (μm)	Optimum Device Area (cm ²)
100	~50
1000	~500
1250	~625



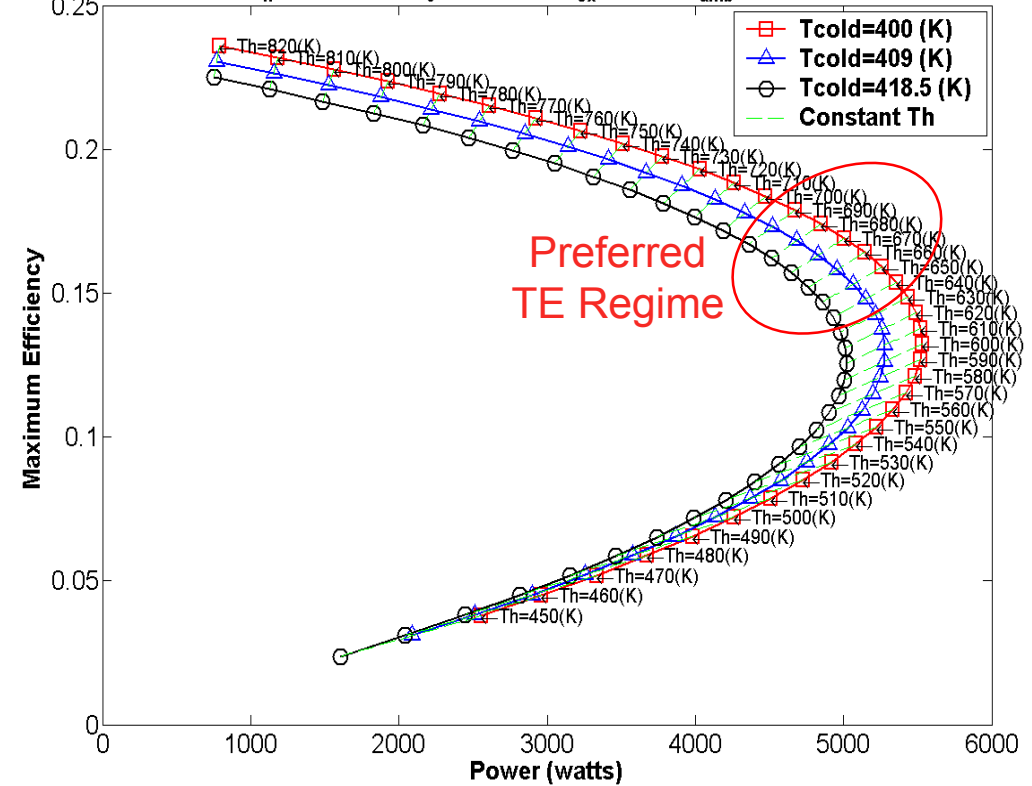
TE Material Thermal Conductivity Effects

- λ Reduced From 1.5 W/m-K \rightarrow 1.0 W/m-K
- Peak Powers for Optimized Systems: 5000-5500 W @ 14-15%
- Quantifies the Effect of Materials R&D Focus in this Area

Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ωm), $\lambda=1.0$ (W/m-K)
 $V=42$ (volts), $UA_h=800$ (W/K), $UA_c=1454$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K)



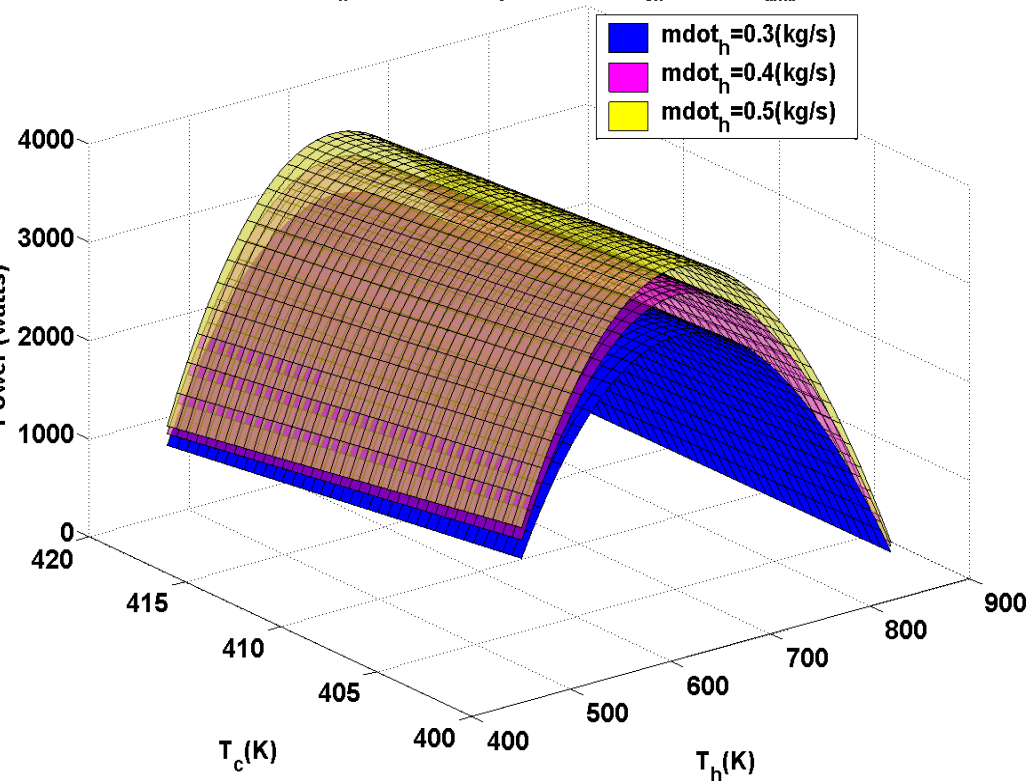
Efficiency At Maximum Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ωm), $\lambda=1.0$ (W/m-K)
 $V=42$ (volts), $UA_h=800$ (W/K), $UA_c=1454$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K), $\dot{m}_h=0.5$ (kg/s)



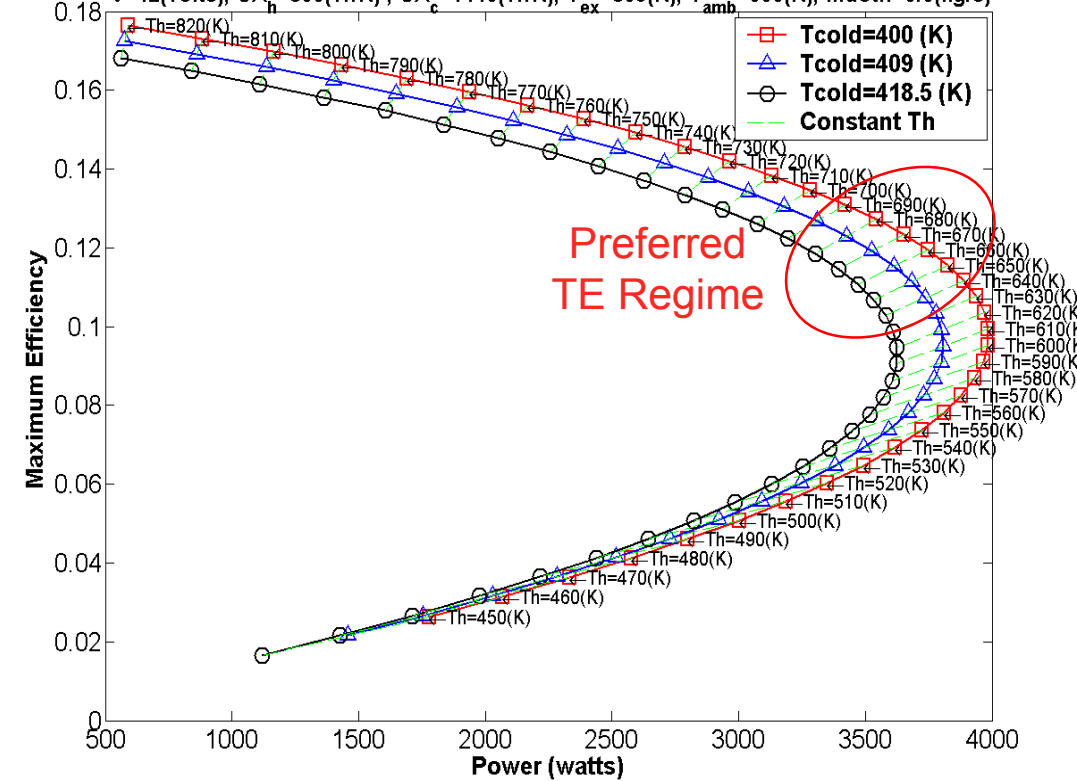
Higher Electrical Resistivity Effects

- ρ Increased from $0.005 \text{ } \Omega\text{-cm}$ \rightarrow $0.0083 \text{ } \Omega\text{-cm}$
- Peak Powers in Optimized Design: $3500\text{-}4000 \text{ W @ } 10\%$
- Quantifies the Effect of Materials R&D Focus in this Area

Power Heavy-Duty: Super Lattice: $\alpha=0.0009 \text{ (V/K)}$, $\rho=0.000083 \text{ (}\Omega\text{m)}$, $\lambda=1.5 \text{ (W/m-K)}$
 $V=42 \text{ (volts)}$, $UA_h=800 \text{ (W/K)}$, $UA_c=1443 \text{ (W/K)}$, $T_{ex}=839 \text{ (K)}$, $T_{amb}=300 \text{ (K)}$



Efficiency At Maximum Power Heavy-Duty: Super Lattice: $\alpha=0.0009 \text{ (V/K)}$, $\rho=0.000083 \text{ (}\Omega\text{m)}$, $\lambda=1.5 \text{ (W/m-K)}$
 $V=42 \text{ (volts)}$, $UA_h=800 \text{ (W/K)}$, $UA_c=1443 \text{ (W/K)}$, $T_{ex}=839 \text{ (K)}$, $T_{amb}=300 \text{ (K)}$, $\dot{m}_h=0.5 \text{ (kg/s)}$

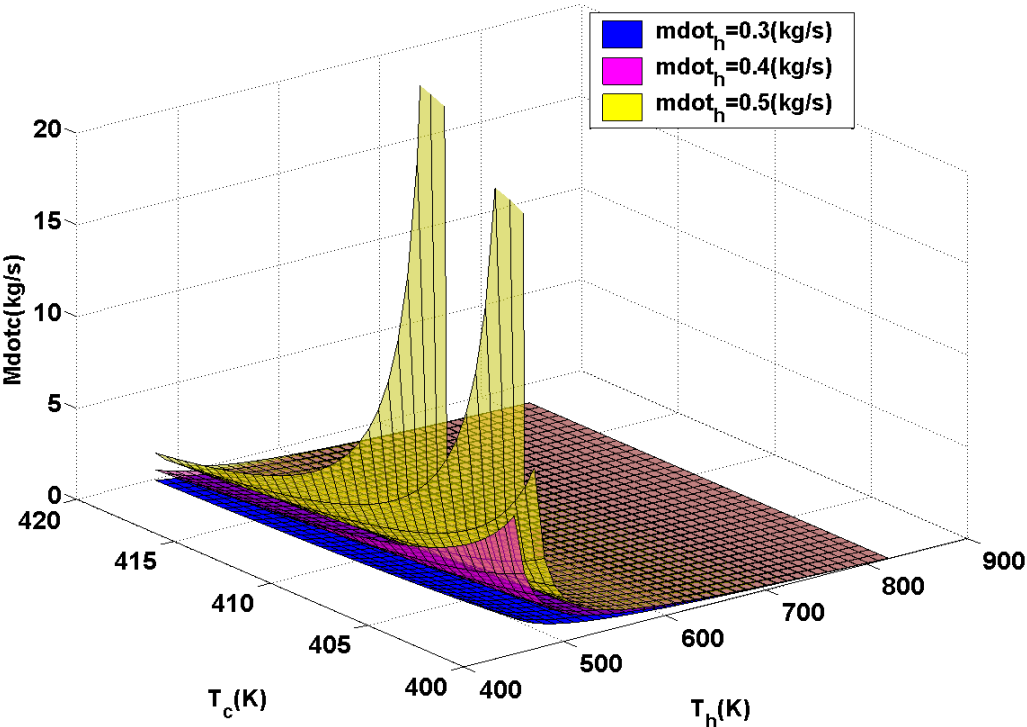


Resistivity Effect on Cold Side Mass Flow Requirements

- And the Cold Side Mass Flow Requirements Get More Severe & Tenuous

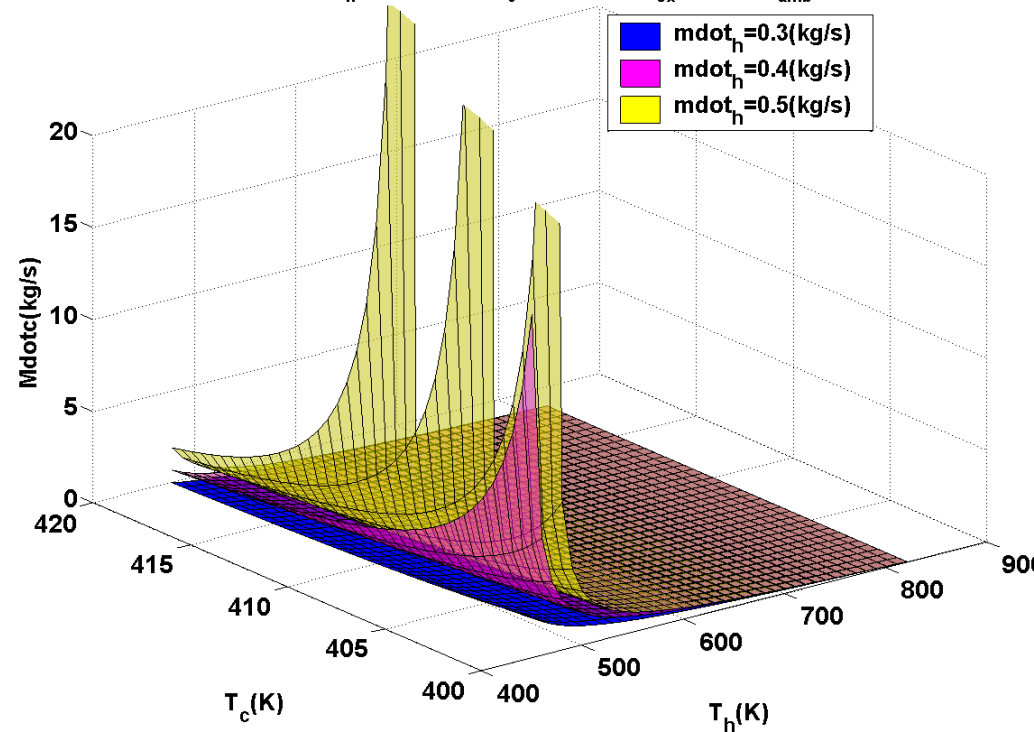
Lower Resistivity Case

Required Ambient Mdot Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ωm), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=800$ (W/K), $UA_c=1517$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K)



Higher Resistivity Case

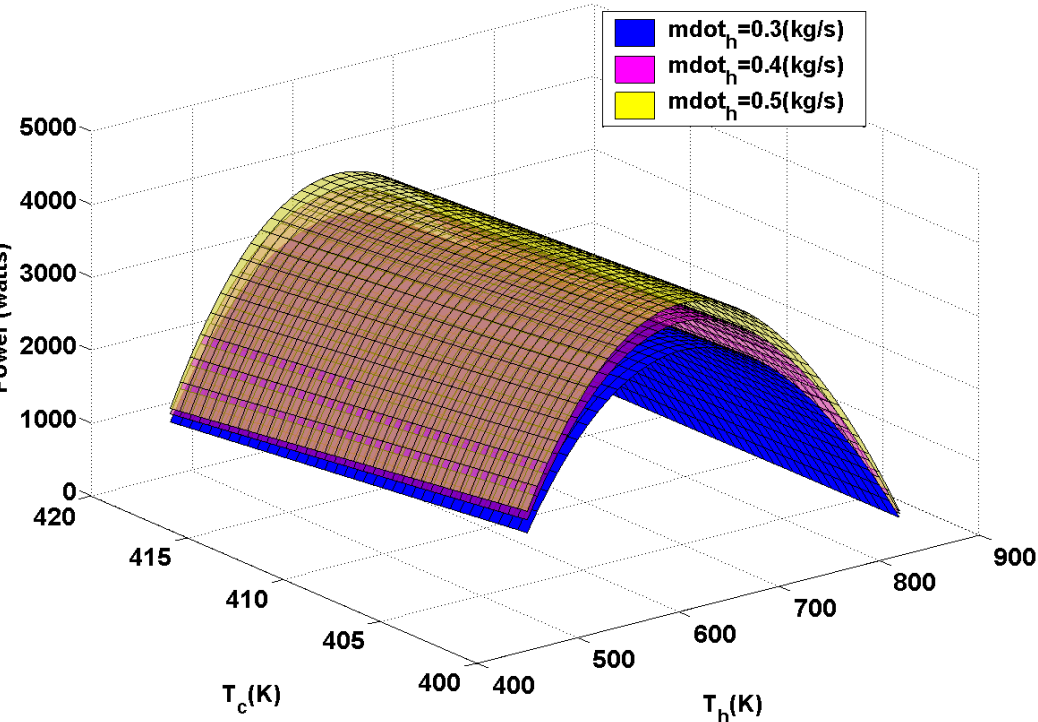
Required Ambient Mdot Heavy-Duty: Super Lattice: $\alpha=0.0009$ (V/K), $\rho=0.000083$ (Ωm), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=800$ (W/K), $UA_c=1443$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K)



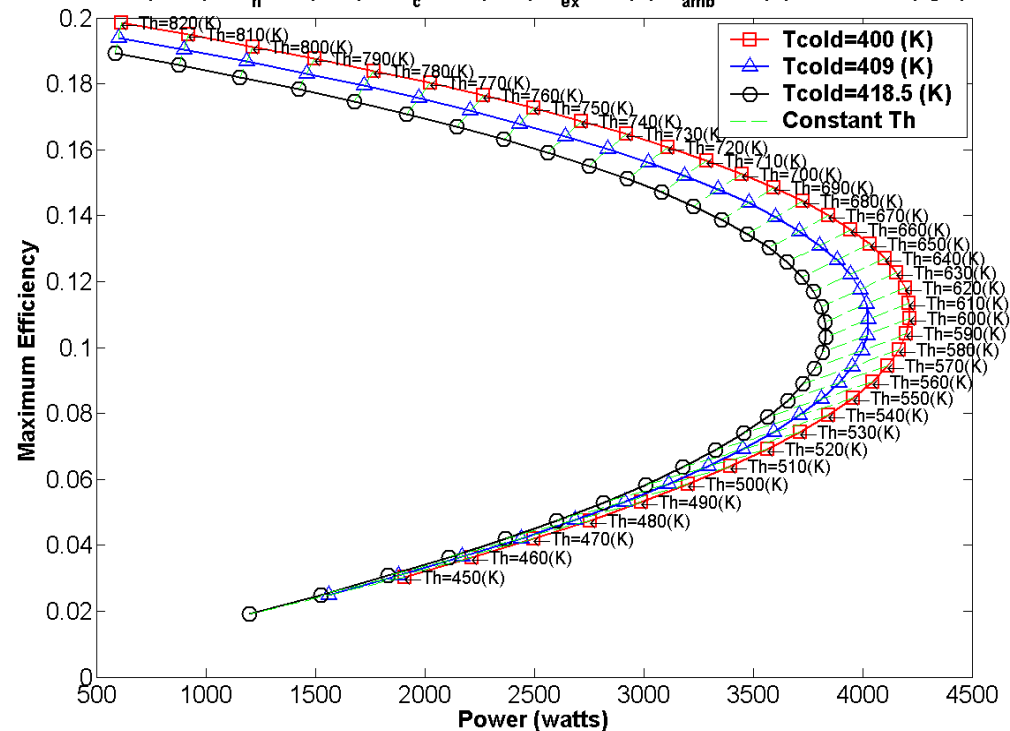
Hot Side Heat Exchanger UA Effects

- Hot Side UA Reduced From 800 W/K \rightarrow 600 W/K
- Peak Powers in Optimized Systems: 3700-4200 W @ 11-12 %
- Quantifies the Effect of Heat Exchanger R&D As Critical Enabling Technology

Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ωm), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=600$ (W/K), $UA_c=1349$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K)



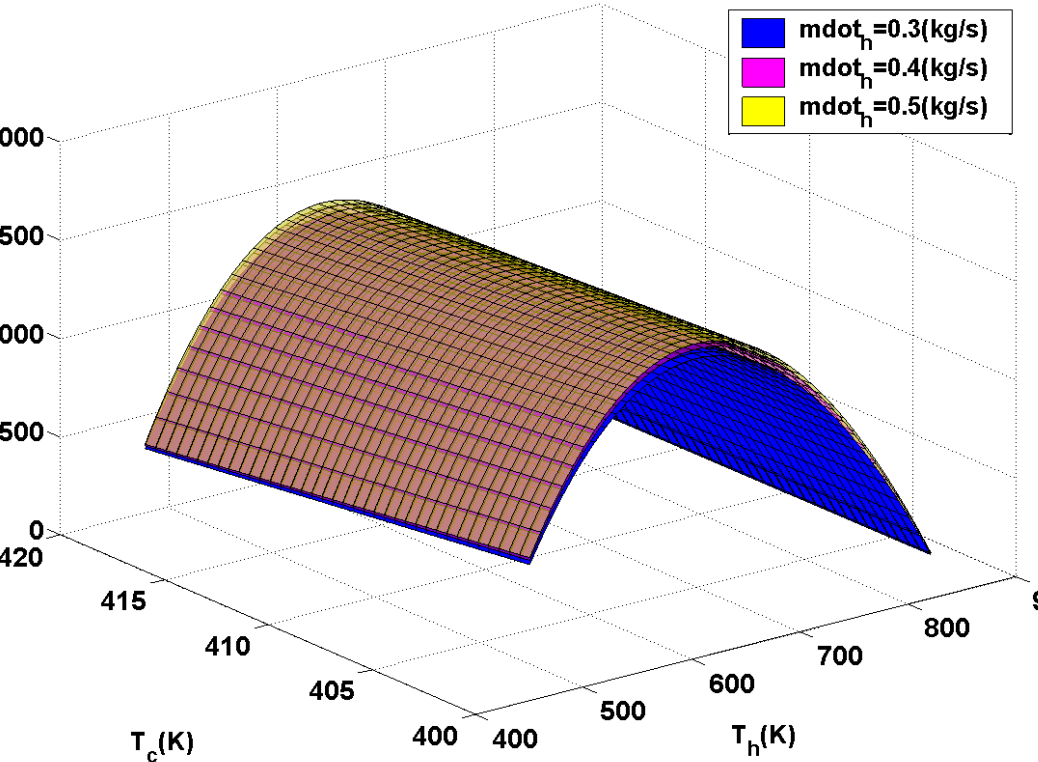
Efficiency At Maximum Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ωm), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=600$ (W/K), $UA_c=1349$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K), $\dot{m}_h=0.5$ (kg/s)



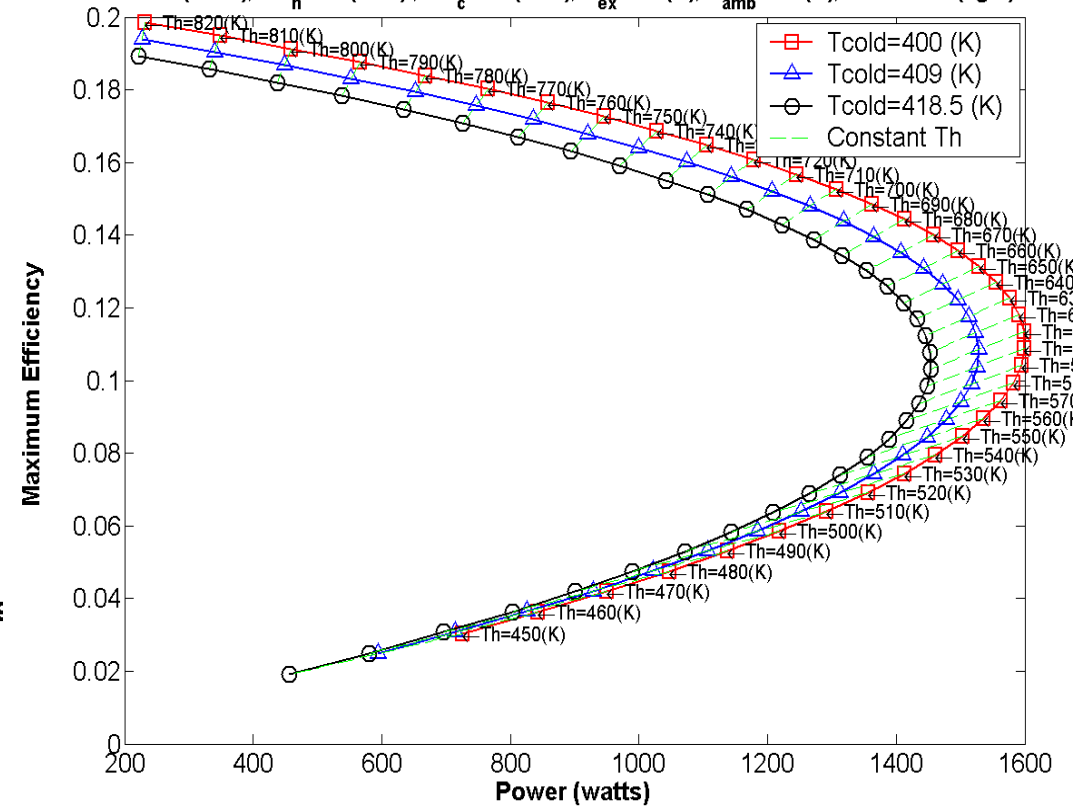
Hot Side Heat Exchanger UA Effects

- Hot Side UA Reduced From 800 W/K \rightarrow 100 W/K
- Devastating Impact on Power Output: 1400-1600 W @ 11-12%
- Optimum TE Device Area Drops to 250-300 cm² @ Peak Powers

Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ω m), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=100$ (W/K), $UA_c=386$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K)

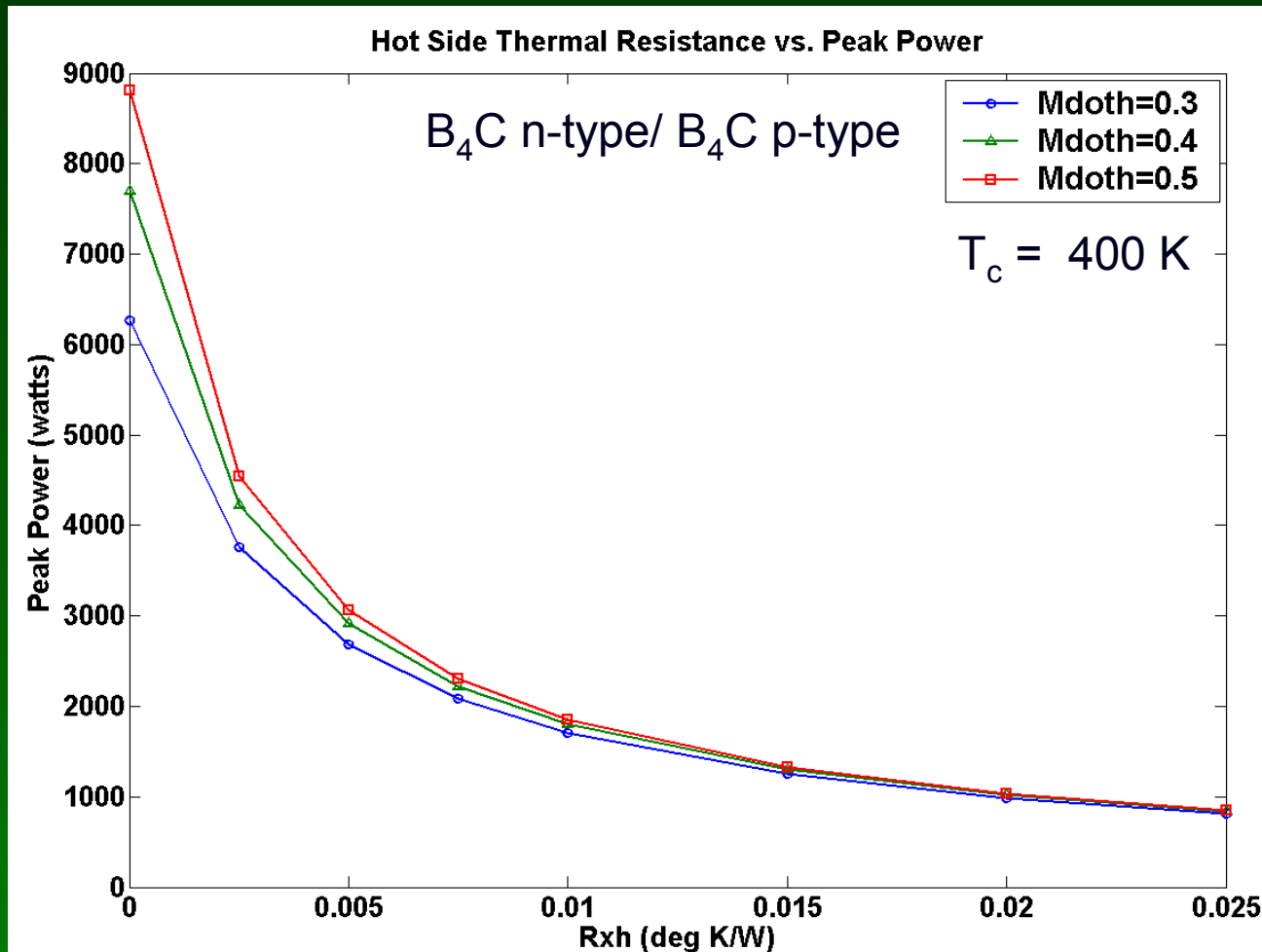


Efficiency At Maximum Power Heavy-Duty: Super Lattice: $\alpha=0.00095$ (V/K), $\rho=0.00005$ (Ω m), $\lambda=1.5$ (W/m-K)
 $V=42$ (volts), $UA_h=100$ (W/K), $UA_c=386$ (W/K), $T_{ex}=839$ (K), $T_{amb}=300$ (K), $\dot{m}_h=0.5$ (kg/s)



Hot Side Thermal Resistance Effects

- Device-to-Heat Exchanger Thermal Resistance Will Have Large Effect on Peak Power Available
- R_{thermal} Can Dominate If Interface Designed Poorly
- Mass Flow Rate Effect
Large at Low R_{thermal}



Potential Heavy Hybrid Vocations/Markets



Marketing / Commercialization Thoughts

- Different Devices/Systems Than Previously Dealt With
 - TE Device Not That Big for 3.5 – 5.0 kW Powers
 - Thermal Funneling
 - Could Be Ultra-Thin TE Devices
- Advanced Heat Exchangers Key Enabler
- Preferred Temperature Regimes Definitely Exist
 - Maximum TE Power
 - System Cooling
- Coupled TE Materials and System-Level R&D Required
- Heavy-Duty Markets Present Larger Power Opportunity Than Light-Duty Markets
- Device/System Characterization, Verification, & Validation
- Heat Exchanger / TE System is the Key!

Technical Challenges in LD & HD Applications

- **Cost**
- **Material Interface Contacts**
 - Electrical Resistance
 - Structural Ruggedness - Shock & Vibration
 - Thermal Expansion
 - Thermal Diffusion
- **Tailor TEG Systems to Vehicle Systems & Requirements**
 - Design/Fabricate For New TE Materials
 - Thermal Funneling
 - Establish TE System Cost Basis
- **Location for Optimal Heat Recovery**
- **Maintaining Relatively Constant Cold Side Temperatures**
- **Maximum Power Output is at Maximum Engine Output**
 - Not Necessarily Synchronized With Times of Maximum Power Requirement
 - Requires Energy Storage (e.g., batteries)
- **Establish Supplier Infrastructure**
 - TE Materials, System Fabrication, System Testing

Conclusions

- **WHR Applications Currently In Light-Duty & Heavy-Duty Vehicles**
 - Automotive Exhaust Waste Heat Recovery
 - Heavy Hybrid Vehicle Program Applications - Truck Electrification & SOC Maintenance
- **Heat Exchanger / Thermoelectric Device Design Must Be Analyzed & Optimized Simultaneously Within Vehicle-Level Studies (ADVISOR)**
- **Coupled TE Materials & System-Level R&D Required**
- **Heat Exchanger / TE Device Tradeoffs**
 - Heavy Duty Power Potential Higher Than Light Duty Vehicle Power
 - Maximum Power Near $T_h = 625$ K
 - Cold Side Mass Flow Rates Could Be Challenging
 - Optimum Design Regimes Exist (TE Performance & Cold Mass Flow Reasons)
 - Thermal Funneling Will Be A Design Issue
 - TE Materials Strongly Impact Thermal System Design
 - Thermal Interfaces & Thermal Losses Could Limit Power Potential (Be Smart!)

Acknowledgements

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References

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NREL System-Level Investigations

➤ Advanced TE System Analyses Required

- Knowing Material ZT is Critical & Necessary, but Not Sufficient
- TE System Performance & Benefits Dependent on System Temperatures Likely in Actual Operating Systems
- Accurately Quantifying Requires a Full System Analysis Approach
- Focus & Direct TE Material R&D to Most Beneficial Opportunities & Material Combinations

