



Wind Turbine Generator System

Acoustic Noise Test Report

for the

AOC 15/50 Wind Turbine

at the **National Wind Technology Center** Golden, Colorado

by

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4.0 Disclaimer

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NREL is a National Laboratory of the U. S. Department of Energy, and as an adjunct of the U. S. Government, cannot certify wind turbines. The information in this report is limited to NREL's knowledge and understanding as of this date.

5.0 Results

Turbine and background data was collected on March 30, 1999. The following sections show the results of the analysis of the data.

5.1 A-Weighted Sound Power Level

The apparent sound power level was determined using pairs of turbine plus background and pairs of background data between the wind speeds of 6 to 10 m/s. Table 1 gives the calculated apparent sound power level for the four microphone positions. Figure 1 through Figure 4 show the data pairs for microphone positions 1, 2, 3, and 4, respectively.

Table 1. Apparent Sound I over Level	Table 1.	Apparent	Sound	Power	Levels
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Microphone Position	Unit	1	2	3	4
Apparent Sound Power Level	dB	101.1	100.3	98.5	100.0
Uncertainty*	dB	0.6	0.6	0.6	0.6
Number of Turbine plus		58	41	12	50
Background Data Points					
Number of Background Data		14	15	9	8
Points					

* - The uncertainty reported is the worst case.

5.2 Wind Speed Sensitivity

In determining the wind speed dependence, 74 pairs of turbine plus background and 31 pairs of background data was used. The results are shown in Table 2 and Figure 5. The wind speed range for the turbine data pairs was 4.14 to 9.46 m/s and background data pairs was 4.14 to 9.41 m/s.

Bin	Wind Speed Average	Position 1	Uncertainty*
m/s	m/s	dBA	dBA
4	4.26	59.6	1.9
5	5.15	59.6	1.4
6	5.99	62.8	1.5
7	7.20	63.5	1.1
8	8.03	**63.7	1.2
9	9.00	64.7	1.0

 Table 2. Wind Speed Dependence

* The uncertainty reported is the worst case.

**2 data points in background bin, estimate.

5.3 Directivity

In calculating the directivity, the measurements from the four microphone positions were measured simultaneously. The directivity was calculated for positions 2, 3, and 4 in reference to position 1 at a wind speed of 8 m/s. The results are shown in Table 3.

Table 3. Directivity

Position	Units	2	3	4
Directivity	dB	-0.6	-2.6	-0.9
Uncertainty*	dB	0.8	0.8	0.8

* The uncertainty reported is the worst case.

5.4 Octave Spectra

At the reference position, third octave data was also collected. The octave band results for microphone position 1 is shown in Table 4 and Figure 6

Center	20	25	31.5	40	50	63	80	100	125	160	200
Frequency	Hz										
Units	dB										
Position 1	69.0	67.0	65.0	57.0	58.0	59.9	56.7	54.3	53.8	54.1	54.1
Uncertainty	4.1	3.8	3.3	7.2	4.6	2.7	1.8	3.6	1.7	1.6	1.5

Table 4. Third Octave Bands for Microphone Position 1

Center	250	315	400	500	630	800	1000	1250	1600	2000	2500
Frequency	Hz										
Units	dB										
Position 1	52.6	54.1	51.7	53.7	56.8	62.4	52.0	52.0	53.1	47.4	48.8
Uncertainty	1.4	1.7	1.5	1.7	2.4	2.3	1.5	2.1	2.7	1.1	1.4

Center	3150	4000	5000
Frequency	Hz	Hz	Hz
Units	dB	dB	dB
Position 1	45.5	41.0	37.7
Uncertainty	1.3	1.4	1.8

5.5 Tonal Analysis

A tonal analysis was completed for frequencies from 20 to 5000 Hz for 5 integer wind speed bins at the reference microphone position. The sets of unweighted spectra were obtained using the settings shown in Table 5.

Bin	Bandwidth	Frequency	Setup File	Setup File	Number of
		Resolution	Turbine On	Background	Spectra
5	20 - 3200	6	5TAOCNLW	5BAOCNLO	280
5	2500 - 5000	6	5TAOCNHI	5BAOCNHI	280
6	20 - 3200	6	6TAOCNLW	6BAOCNLO	280
6	2500 - 5000	6	6TAOCNHI	6BAOCNHI	280
7	20 - 3200	6	7TAOCNLW	7BAOCNLO	280
7	2500 - 5000	6	7TAOCNHI	7BAOCNHI	280
8	20 - 3200	6	8TAOCNLW	8BAOCNLO	280
8	2500 - 5000	6	8TAOCNHI	8BAOCNHI	280
9	20 - 3200	6	9TAOCNLW	9BAOCNLO	280
9	2500 - 5000	6	9TAOCNHI	9BAOCNHI	280

Table 5. Data Files Created During the Tonal Analysis

5.5.1 Reference Wind Speed

The tonal analysis for the frequency range 20 to 5000 Hz was done with an effective bandwidth of 6 Hz. Figure 10 shows the unweighted spectrum for turbine plus background and background noise. Two critical bands were analyzed. Table 6 shows the results from the critical band analysis.

Table 6. Tonal Analysis at the Reference Wind Speed

Frequency of	Critical	$\Delta L_{tn,max}$	$\Delta L_{\text{tn,avg}}$	U _C
Tone	Band	Difference between the	Difference between the	Combined
		maximum level of tone	average level of the tone	Uncertainty
		and masking level	and masking	
Hz	Hz	dB	dB	dB
488, 492,	432 - 548	7.1	1.8	1.5
496, 500				
1000	916 - 1076	-2.1	-7.8	1.4

5.5.2 Wind Speed Dependence on Tonality

An additional tonal analysis was done for integer wind speed bins from 4 to 9 m/s. Figures 7 through 11 show the spectrums for wind speed bins 5 through 9, respectively. The following tables show the results for the critical band analysis for each wind speed bin.

Critical Band	$\Delta L_{tn,avg}$, Difference between the average level of the tone and masking	ΔL _{a,max} , Tonal Audibility	$\Delta L_{tn,max}$, Difference between the maximum level of tone and masking	U _C Combined Uncertainty
Hz	dB	dB	dB	dB
432 - 548	0.2	9.7	7.4	2.7

Table 7. Tonal Analysis for 5 m/s Wind Speed Bin

Table 8. Tonal Analysis for 6 m/s Wind Speed Bin

Critical	$\Delta L_{tn,avg}$	$\Delta L_{a,max}$	$\Delta L_{tn,max}$	U _C
Band	Difference between	Tonal	Difference between	Combined
	the average level of	Audibility	the maximum level	Uncertainty
	the tone and masking		of tone and masking	
Hz	dB	dB		dB
432 - 548	2.3	11.9	9.6	2.1

Table 9. Tonal Analysis for 7 m/s Wind Speed Bin

Critical	$\Delta L_{tn,avg}$,	$\Delta L_{a,max}$,	$\Delta L_{tn,max}$,	U _C
Band	Difference between	Tonal	Difference between	Combined
	the average level of	Audibility	the maximum level	Uncertainty
	the tone and masking		of tone and masking	
Hz	dB	dB		dB
432 - 548	4.5	12.4	10.1	1.8
916 - 1076	-4.1	4.3	1.5	1.8

Critical	$\Delta L_{tn,avg}$,	$\Delta L_{a,max}$,	$\Delta L_{tn,max}$,	U _C
Band	Difference between	Tonal	Difference between	Combined
	the average level of	Audibility	the maximum level	Uncertainty
	the tone and masking		of tone and masking	
Hz	dB	dB		dB
432 - 548	1.8	9.5	7.1	1.5
916 - 1076	-7.8	0.8	-2.1	1.4

Table 10. Tonal Analysis for 8 m/s Wind Speed Bin

Table 11. Tonal Analysis for 9 m/s Wind Speed Bin

Critical	$\Delta L_{tn,avg}$	$\Delta L_{a,max}$,	$\Delta L_{tn,max}$,	U _C
Band	Difference between	Tonal	Difference between	Combined
	the average level of	Audibility	the maximum level	Uncertainty
	the tone and masking		of tone and masking	
Hz	dB	dB		dB
328 - 436	-2.6	3.2	1.0	7.8
432 - 548	5.4	13.4	11.1	2.0
916 - 1076	1.3	10.3	7.4	2.1





Figure 1. Turbine Plus Background and Background Data For Microphone Position 1



Figure 2. Turbine Plus Background and Background Data For Microphone Position 2







Figure 4. Turbine Plus Background and Background Data For Microphone Position 4





Figure 5. Wind Speed Dependence at Microphone Position 1

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Figure 6. Third Octave Bands for Microphone Position 1



Figure 7. Turbine Plus Background and Background Spectrum for 5 m/s Wind Speed Bin



Figure 8. Turbine Plus Background and Background Spectrum for 6 m/s Wind Speed Bin



Figure 9. Turbine Plus Background and Background Spectrum for 7 m/s Wind Speed Bin



Figure 10. Turbine Plus Background and Background Spectrum for 8 m/s Wind Speed Bin





Figure 11. Turbine Plus Background and Background Spectrum for 9 m/s Wind Speed Bin

6.0 Uncertainty

The combined uncertainty is reported for the apparent sound power level, directivity, wind speed dependence, and tonality. The combined standard uncertainty is the combination of Type A and Type B uncertainties. Type A uncertainty components are evaluated by using statistical methods to a series of repeated measurements. Type B uncertainty components are evaluated through estimations or calibrations. The methods used to evaluate the uncertainty components for the apparent sound power level, directivity, wind speed dependence and tonality will be explained in this section.

6.1 Apparent Sound Pressure Level

The Type A uncertainty for the apparent sound pressure level is the standard error of the estimated L_{Aeq} at the acoustic reference wind speed. This is found from the linear regression analysis.

$$U_A = \sqrt{\frac{\Sigma(y - y_{est})^2}{N - 2}}$$

Equation 10

Parameter	eter Description		Microphone				
		1	2	3	4		
U _A	Type A uncertainty for apparent sound pressure level,	1.1	1.1	0.7	1.2	dB	
у	measured sound pressure level,	-	-	-	-	dB	
Y _{est}	estimated sound pressure level using linear regression,	63.8	63.3	61.5	63.0	dB	
Ν	Number of measurements used in the linear regression.	58	41	12	50	-	

Table 12.	Type A	Apparent Sou	ind Power	Level U	ncertainty	Components
	•/				•/	

The Type B uncertainty components include:

$$U_{B} = \sqrt{U_{B1}^{2} + U_{B2}^{2} + U_{B3}^{2} + U_{B4}^{2} + U_{B5}^{2} + U_{B6}^{2} + U_{B7}^{2} + U_{B8}^{2} + U_{B9}^{2}}$$
 Equation 11

Parameter	Description	Microphone Position		Microphone Position		Unit	Source
		1	2	3	4		
U _B	Type B uncertainty for apparent sound pressure level	0.6	0.6	0.6	0.6	dB	Equation 11
U _{B1}	uncertainty for calibration of the instruments,	0.0	0.0	0.1	0.1	dB	calibrator calibration and the standard error from field calibrating microphones
U _{B2}	uncertainty for tolerances on the chain of acoustic measurement instruments,	0.2	0.2	0.2	0.2	dB	signal analyzer, microphone, microphone adapter, and preamplifier
U _{B3}	uncertainty for acoustic conditions for microphone mounting board,	0.3	0.3	0.3	0.3	dB	estimate
U _{B4}	uncertainty on the distance from microphone to hub,	0.1	0.1	0.1	0.1	dB	estimate
U _{B5}	uncertainty on the acoustic impedance of air,	0.1	0.1	0.1	0.1	dB	estimate
U _{B6}	uncertainty on the acoustic emission of the turbine due to changing weather conditions,	0.3	0.3	0.3	0.3	dB	estimate
U _{B7}	uncertainty on the measured wind speed	0.1	0.1	0.1	0.1	dB	anemometer calibration and estimate of the site effects
U _{B8}	uncertainty on the wind direction measurement,	0.3	0.3	0.3	0.3	dB	Estimate
U _{B9}	uncertainty for the background correction.	0.0	0.0	0.0	0.0	dB	Applied background correction

 Table 13. Type B Apparent Sound Power Level Uncertainty Components

These uncertainties are combined into one standard uncertainty by Equation 12.

$$U_C = \sqrt{U_A^2 + U_B^2}$$
 Equation 12

Parameter	Description		Microphone Positions			
		1	2	3	4	
Uc	Overall standard uncertainty for apparent sound pressure level,	0.6	0.6	0.6	0.6	dB
U _A	Type A uncertainty for apparent sound pressure level,	1.1	1.1	0.7	1.2	dB
U _B	Type B uncertainty for apparent sound pressure level	0.6	0.6	0.6	0.6	dB

Table 14. Overall Uncertainty Components

6.2 Wind Speed Sensitivity

Type A uncertainty for wind speed dependence is found from the from a linear regression analysis. The uncertainty, U_A is calculated for integer wind speeds as the root sum of the squared standard error of the estimated value at the actual wind speed. The squared standard error is given in Equation 13.

$$s_i = \sqrt{\frac{\sum (L_{Aeq} - L_{Aeq,j})^2}{(N-1)^2}}$$

Equation 13

 Table 15. Type A Wind Dependence Uncertainty Components

Parameter	Description	Units
s _i	Type A standard uncertainty for bin i	dB
L _{Aeq}	Average of the sound pressure levels in the bin i	dB
L _{Aeq,i}	sound pressure level in the bin	dB
Ν	number of measurement results in the bin	

The Type B uncertainty for each bin is found using Equation 11.

Parameter	Description	Value	Unit	Source
U _B	Type B uncertainty for bin i	varies by bin	dB	
U _{B1}	uncertainty for calibration of the instruments,	0.1	dB	calibrator calibration and the standard error from field calibrating microphones
U _{B2}	uncertainty for tolerances on the chain of acoustic measurement instruments,	0.2	dB	signal analyzer, microphone, microphone adapter, and preamplifier
U _{B3}	uncertainty for acoustic conditions for microphone mounting board,	0.3	dB	estimate
U _{B4}	uncertainty on the distance from microphone to hub,	0.1	dB	estimate
U _{B5}	uncertainty on the acoustic impedance of air,	0.1	dB	estimate
U _{B6}	uncertainty on the acoustic emission of the turbine due to changing weather conditions,	0.3	dB	estimate
U _{B7}	uncertainty on the measured wind speed	0.1	dB	anemometer calibration and estimate of the site effects
U _{B8}	uncertainty on the wind direction measurement,	0.3	dB	Estimate
U _{B9}	uncertainty for the background correction.	varies by bin	dB	Applied background correction

 Table 16. Type B Wind Dependence Uncertainty Components

6.3 Directivity

An estimate of the standard uncertainty on the directivity is shown in Equation 14.

$$U_D = \sqrt{2} U_C$$

Equation 14

ainty
t

Parameter	Description	Microp	Microphone Position				
		2	3	4			
U _D	Standard uncertainty for directivity,	1.6	1.0	1.7	dB		
Uc	Overall standard uncertainty for apparent sound pressure level.	1.1	0.7	1.2	dB		

6.4 Third Octave Spectra

For the third octave band, U_A for each band is the standard error on the averaged band level. U_A is calculated for each band.

$$U_{A} = \sqrt{\frac{\sum (y - y_{est})^{2}}{N - 1}}$$
 Equation 15

Table 18. Type A Octave Band Uncertainty Components

Parameter	Description	Units
U _A	Type A standard uncertainty for band	dB
у	Sound pressure level of the band	dB
y _{est}	Average sound pressure level of the band	dB
Ν	number of measured spectra	

The Type B uncertainty components are estimated to be the same except for U_{B3} . It will be considered much larger than for L_{WA} , estimated value is 1.2 dB as shown in Table 19.

Parameter	Description	Value	Unit	Source
U _B	Type B uncertainty for octave bands	varies by band	dB	
U _{B1}	uncertainty for calibration of the instruments,	0.1	dB	DAT recorder and calibrator calibration, and the standard error from field calibrating microphones
U _{B2}	uncertainty for tolerances on the chain of acoustic measurement instruments,	0.2	dB	signal analyzer, microphone, microphone adapter, and preamplifier
U _{B3}	uncertainty for acoustic conditions for microphone mounting board,	0.3	dB	estimate
U _{B4}	uncertainty on the distance from microphone to hub,	0.1	dB	estimate
U _{B5}	uncertainty on the acoustic impedance of air,	0.1	dB	estimate
U _{B6}	uncertainty on the acoustic emission of the turbine due to changing weather conditions,	0.3	dB	estimate
U _{B7}	uncertainty on the measured wind speed	varies by band	dB	anemometer calibration and estimate of the site effects
U _{B8}	uncertainty on the wind direction measurement,	0.3	dB	Estimate
U _{B9}	uncertainty for the background correction.	varies by band	dB	Applied background correction

Table 19. Type B Octave Band Uncertainty Components

6.5 Tonal Analysis

For the third octave band, $U_{\rm A}$ for each band is the standard error on the averaged band level. $U_{\rm A}$ is calculated for each band.

$$U_A = \sqrt{\frac{\sum (y - y_{est})^2}{N - 1}}$$

Equation 15

Parameter	Description	Units
U _A	Type A standard uncertainty for tone	dB
У	Maximum sound pressure level of the tone	dB
y _{est}	Average sound pressure level of the band	dB
Ν	number of spectra used	

Table 20. Type A Tonality Uncertainty Components

The Type B uncertainty components are estimated to be the same as shown in Table 19.

Parameter	Description	Value	Unit	Source
U _B	Type B uncertainty for octave bands	varies by band	dB	
U _{B1}	uncertainty for calibration of the instruments,	0.0	dB	DAT recorder and calibrator calibration, and the standard error from field calibrating microphones
U _{B2}	uncertainty for tolerances on the chain of acoustic measurement instruments,	0.2	dB	signal analyzer, DAT recorder
U _{B3}	uncertainty for acoustic conditions for microphone mounting board,	0.3	dB	estimate
U _{B4}	uncertainty on the distance from microphone to hub,	0.1	dB	estimate
U _{B5}	uncertainty on the acoustic impedance of air,	0.1	dB	estimate
U _{B6}	uncertainty on the acoustic emission of the turbine due to changing weather conditions,	0.3	dB	estimate
U _{B7}	uncertainty on the measured wind speed	0.1	dB	anemometer calibration and estimate of the site effects
U _{B8}	uncertainty on the wind direction measurement,	0.3	dB	Estimate

Table 21. Type B Octave Band Uncertainty Components

7.0 Exceptions

7.1 Exceptions to Standard

1. There were no exceptions to the Standard.

7.2 Exceptions to NWTC-CT Quality Assurance System

There were no exceptions to the NWTC-CT Quality Assurance System.

Appendix A Pictures of Test Site



Figure 12. Picture Taken From the Reference Microphone Position (manlift was not present during test)



Figure 13. Picture Taken From the Meteorological Tower (manlift was not present during test)

Appendix B Data Sheets

TURBINE M	EASUREMEN	rs						-2 M	lic 3 M	lic 4
Data File	Time stamp 1	Fime stamp 🛝	Nind Spd Pr	norm I	Pressure	emp Mi	ICI IVII 10	C∠ ⊮ IA d	RA d	RA
	dd/mm/yy h	nh:mm:ss r	n/s k\	N I	Pa K	dE		A U	62 55 62 55	65.07
AOC_C_A2	03.30.99	14:20:51	10.13	53.12	80200	295.5	63.64	62.82	61.36	63.45
AOC_C_A2	03.30.99	14:21:56	8.80	37.50	80200	295.5	62.01	62.77	61.50	63.31
AOC_C_A2	03.30.99	14:23:01	8.98	33.16	80200	293.5	64 19	64.07	63.04	64.91
AOC_C_A2	03.30.99	14:24:06	9.29	52.80	80200	295.5	64.13	64.88	63.35	65.06
AOC_C_A2	03.30.99	14:25:11	10.29	60.01	80200	295.5	64.12	65.18	63.43	65.08
AOC_C_A2	03.30.99	14:26:16	10.27	56.62	80200	293.3	61 73	63.02	61.78	63.12
AOC_C_A2	03.30.99	14:27:21	7.84	25.99	80200	295.5	63 16	63.93	63.51	63.40
AOC_C_A2	03.29.99	14:28:26	8.21	33.87	80200	295.5	57 77	58.12	57.99	57.25
AOC_C_A2	03.30.99	14:29:31	5.25	-1.91	80200	295.5	58.64	59.55	58.54	59.14
AOC_C_A2	03.30.99	14:30:36	6.23	0.00	80200	295.5	60.15	61.53	60.47	61.27
AOC_C_A2	03.30.99	14:31:42	5.60	10.10	80200	295.5	61.04	62.72	61.49	62.55
AOC_C_A2	03.30.99	14:32:47	5.52	10.20	80200	295.5	61.73	63.00	62.22	63.00
AOC_C_A2	03.30.99	14:33:52	10.25	19.32	80200	295.5	64.43	64.86	64.46	63.57
AOC_C_A2	03.30.99	14:34:57	10.20	69.56	80200	295.5	65.79	66.02	65.77	65.08
AOC_C_A2	03.30.99	14:36:02	0.02	11 14	80200	295.5	63.60	64.36	63.59	64.47
AOC_C_A	2 03.30.99	14:37:08	0.90	22.00	80200	295.5	62.61	63.61	62.30	63.84
AOC_C_A	2 03.30.99	14:38:13	10.00	52.03	80200	295.5	64.55	65.14	64.79	64.64
AOC_C_A	<u>2</u> 03.30.99	14:39:18	11.20	63.78	80200	295.5	65.16	65.94	65.16	64.09
AOC_C_A	2 03.30.99	14:40:23	11.44	59.97	80200	295.5	65.51	65.87	65.38	64.25
AOC_C_A	2 03.30.99	14:41:20	12 79	73.57	80200	295.5	66.26	66.27	66.09	65.14
AOC_C_A	2 03.30.99	14:42:33	0.06	11 54	80200	295.5	63.99	64.32	64.16	63.82
AOC_C_A	2 03.30.99	14.43.39	10.32	52.87	80200	295.5	65.11	65.17	65.10	64.22
AOC_C_A	2 03.30.99	14:44:44	0.32	50.68	80200	295.5	64.87	65.28	64.75	63.32
AOC_C_A	2 03.30.99	14:40:49	10.60	59.50	80200	295.5	64.43	65.48	64.84	64.07
AOC_C_A	2 03.30.99	14:40.34	9.85	48.06	80200	295.5	63.68	65.11	64.27	_ 63.35
AOC_C_A	2 03.30.99	14.47.59	7 14	15 71	80200	295.5	61.94	63.09	62.26	61.67
AOC_C_A	2 03.30.99	14.49.04	9 80	31.25	80200	295.5	63.08	64.05	63.29	62.41
AOC_C_A	2 03.30.95	14.30.03	894	38.37	80200	295.5	63.29	64.18	63.66	62.73
AUC_C_A	0 02 20 00		a 7.29	19.74	80200	295.5	62.69	63.60	63.00	62.89
AOC_C_A	2 03.30.95	14.52.10	1 878	37.53	3 80200	295.5	63.80	64.36	63.91	62.93
	2 03.30.8	14:54:20	8 13	26.13	80200	295.5	63.09	63.75	63.35	63.09
	2 03.30.9	a 14:55:36	6 49	15.95	5 80200	295.5	62.03	63.27	62.86	63.58
	2 03.30.90	9 14-56-4	1 7.86	26.70	80200	295.5	62.67	63.55	62.83	63.56
	03.30.9	9 14:57:46	s 10.62	46.37	7 80200	295.5	65.20	65.16	65.18	64.96
	12 03.30.3	0 14·58·5	1 10.29	54.9	1 80200	295.5	65.03	65.23	65.21	64.59
	12 03.00.0	9 14:50:5 9 14:59:5	7 10.82	61.6	1 80200	295.5	65.40	65.65	65.17	65.43
	12 03.30.3 12 03.30.9	g 15:01:0	2 10.60	62.7	8 80200	295.5	66.15	65.95	65.46	66.07
	12 00.00.0 12 03.30.9	9 15:02:0	7 10.35	50.8	5 80200	295.5	64.81	65.24	64.82	65.35
AOC_C_/	2 03.00.0 03.30.9	9 15:03:1:	3 10.11	42.4	3 80200	295.5	64.15	64.77	64.04	64.76
AOC_C_/	A2 03.30.9	9 15:04:1	8 10.06	59.5	5 80200	. 295.5	65.31	65.80	65.19	65.56
A00_0_/	A2 03.30.9	9 15:05:2	3 11.25	66.9	5 80200	295.5	65.98	65.92	65.87	64.73
AOC_C_/	42 03.30.9	9 15:06:2	8 7.20	22.4	8 80200	295.5	62.51	63.36	62.96	63.44
AOC_C_	A2 03.30.9	9 15:07:3	4 6.93	14.2	9 80200	295.5	62.04	63.23	62.53	63.23
AOC_C_	A2 03.30.9	9 15:08:3	9 5,44	. 4.5	9 80200) 295.5	59.91	60.46	60.53	59.93
	A2 03.30.9	9 15:09:4	4 4.28	-4.0	4 8Q200) 295.5	57.43	, 57.54	56.95	57.59
	A2 03.30.9	15:10:4	9 6.38	17.4	5 80200) 295.5	62.69	63.37	62.51	63.65
	Δ2 03.30 S	9 15:11:5	5 8.06	5 25.6	80200) 295.5	62.80	63.54	62.54	63.94
	A2 03.30 9	9 15:13:0	0 7.25	5 28.1	6 80200) 295.5	62.84	63.31	62.26	63.69
	A2 03.30 9	15:14:0)5 7.74	25.0	80200) 295.5	62.93	63.96	62.90) 64.16
	A2 03.30 9	99 15:15:1	10 9.17	7 43.4	18 80200) 295.5	64.00	64.65	63.25	65.04
	A2 03.30 9	9 15:16:1	15 7.40) 34.2	2 80200	0 295.5	63.43	64.28	62.49	64.59
	A2 03.30 g	99 15:17:2	20 6.46	5 4.8	32 80200	0 295.5	61.65	62.13	61.55	5 61.61
	A2 03.30	99 15:18:2	25 5.88	3 5.8	39 80200	0 295.5	61.37	61.84	4 61.8t	5 61.48
AOC_C_	A2 03.30.	99 15:19:	31 7.22	2 11.0	00 8020	0 295.5	62.31	63.02	62.87	62.68

TURBINE M	EASUREMEN	NTS		Deser		Dee	0.000	Tomo		Mic 1	Mic 2	Mic 3	Mic 4
Data File	Time stamp	Time stamp	wind spa	Phom	1		ssure	remp		dBA	dBA	dBA	dBA
	dd/mm/yy	hh:mm:ss	m/s = 04	KVV -	7 07	га	00200	20	95.5	62.18	63.00	62.68	62.96
AOC_C_A2	03.30.99	15:20:36	7.94	ו י	1.91		80200	20	95.5	62.96	63.65	60.68	63.72
AOC_C_A2	03.30.99	15:27:25	. 1.11	4	9.20		80200	2	95.5	63.10	64.32	2 61.63	64.48
AOC_C_A2	03.30.99	15:28:30	10.73	· 2	.3.77 88 73		80200	2	95.5	65.99	66.69	64.60	66.71
AOC_C_A2	03.30.99	15:29:35	14.70		200. 11 20 02		80200	2	95.5	65.56	66.32	2 63.29	66.12
AOC_C_A2	03.30.99	15:30:40	0.62		10.00		80100	2	94.7	64.60	65.22	62.05	65.01
AOC_C_A3	03.30.99	15:38:37	9.02 10.36		1 48		80100	2	94.7	66.06	66.14	4 63.63	65.75
AOC_C_A3	03.30.95	15:39:42	12.00		SR 24		80100	2	94.7	66.51	66.62	2 63.88	66.26
AOC_C_A3	03.30.95	15:40.47	10.20	, (3 54		80100	2	94.7	66.00	65.80	63.10	65.11
AOC_C_A3	03.30.98	15:42:57	9.92	, (31.08		80100	2	94.7	65.86	65.94	4 63.64	65.24
AOC_C_A3	03.30.9	9 15:42.57 0 15:44:02	9.3	- -	51.02		80100	2	94.7	65.86	65.9	5 63.29	64.82
AOC_C_A3	03.30.9	3 15·45·07	8.9	<u> </u>	46.24	•	80100	2	94.7	64.83	65.13	2 61.93	64.54
AUC_C_A3	03.30.9	15.46.12	9.3	5	54.85	;	80100	2	94.7	65.48	65.5	4 62.19	65.13
AOC_C_A3	03.30.3	a 15:48:24	10.4	- -	65.06	5	80100	2	94.7	65.83	66.0	3 63.35	65.59
ACC_C_A3	03.30.9	a 15·50·11	7.6	3.	41.01		80100) 2	94.7	63.79	65.0	9 61.74	64.85
	03.30.9	a 15:51:16	6.4	9	21.75	5	80100) 2	94.7	62.63	62.8	0 61.46	63.16
	03.30.9	9 15:52:2	8.1	3	31.60)	80100) 2	294.7	63.22	2 63.9	7 61.87	64.04
	03.30.9	9 15:53:26	5 8.7	5	51.29	3	80100) 2	294.7	64.75	5 65.4	0 62.92	65.67
		9 15:54:3	1 8.2	7.	45.27	7	80100) 2	294.7	64.04	4 65.1	0 62.35	5 65.14
AOC_C_AS	00.00.0	9 15:55:31	6 7.1	4	30.32	2	80100) 2	294.7	62.73	3 64.0	5 61.33	3 64.04
AOC_C_AS	03.30.9	9 15:56:4	1 5.9	8	37.62	2	80100) 2	294.7	7 63.44	4 64.5	9 61.78	64.61
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	3 03 30.9	9 16:02:0	7 8.7	4	49.9	7	8010	0 2	294.	7 65.1	5 65.1	1 62.4	7 64.52
	3 03.30.9	9 16:03:1	2 9.3	3	32.2	4	8010	0;	294.	7 63.7	5 64.5	57 61.2°	7 64.16
AOC C A	3 03.30.9	16:04:1	7 9.0	8	49.1	6	8010	0 :	294.	7 64.9	1 65.3	31 61.8	9 64.65
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	3 03.30.9	9 16:07:3	3 5.9	8	14.2	2	8010	0	294.	7 62.9	1 63.6	59 60.9	3 62.99
	3 03.30.9	99 16:10:5	i0 5.6	64	7.1	7、	8010	0	294.	7 63.6	1 64.2	27 61.8	2 63.27
AOC C A	3 03.30.9	99 16:11:5	5 5.8	33	9.8	6	8010	0	294.	7 62.8	7 63.5	53 61.0	4 63.32
AOC C A	3 03.30.5	99 16:13:0	0.6.	52	23.0)4	8010	0	294.	7 63.0	8 63.6	64 61.1	5 62.58
AOC C A	3 03.30.	99 16:14:0)5 5.0	35	11.0)8	8010	0	294.	7. 62.9	3 63.	71 61.2	7 62.64
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AOC C A	3 03.30.	99 16:16:1	5 8.	30	38.4	19	8010	0	294.	.7 64.6	65.	16 63.0	2 63.21
AOC C A	3 03.30.	99 16:18:2	25 7.1	23	34.7	77	8010	0	294.	.7 64.5	6 64.	68 62.2	8 63.16
AOC C A	3 03.30.	99 16:19:0	30 4.	36	3.0)9	8010	00	294.	.7 60.7	4 61.	05 58.7	3 59.67
AOC C A	.3 03.30.	99 16:20:	35 4.	91	1.0)9	8010)0	294	.7 59.2	<u>21</u> 60.	03 57.4	8 58.71
AOC C A	3 03.30.	99 16:21:4	4ପ୍ 6.	43	21.3	32	8010	00	294	.7 63.3	36 63.	88 61.2	6 62.42
AOC C A	3 03.30.	99 16:22.4	45 6.	84	28.8	34	8010	00	294	.7 63.6	63 63.	99 61.E	62.25
AOC C A	3 03.30.	99 16:23:	50 - 7.	09	26.9	99	8010	00	294	.7 63.8	37 · 64.	09 61.9	5 62.94
AOC C A	3 03.30.	.99 16:24:	55 • 5.	83	10.9	54	8010	00	294	.7 61.3	70; 62.	82 60.4	5 61.20
AOC C A	A3 03.30.	.99 16:26:	00 5.	95	5.0	69	8010	00	294	.7 61.3	31 61.	87 59.5 oo oo oo	51 60.59
AOC_C	43 03.30	.99 16:27:	05 6.	91	32.	16	8010	00	294	.7 63.8	80 64.	29 61.9	
AOC_C /	A3 03.30	.99 16:28:	10 5	72	12.	97	8010	00	294	.7 62.2	29, 63.	U/ 60.9	
	A3 03.30	.99 16:30:	20 5	.71	13.	04	801	00	294	.7 62.4	42 63.	.11 60.6	
AOC_C_/	43 03.30	.99 16:31:	25 4	.14	0.	46	801	00	294	.7 59.	13 59.	.74 58.0	1 29.58

BACKGROU	ND MEASUR	EMENTS	معديد ور	•.	_	T	Min 1	Mic 2	Mic 3	Mic 4
Data File	Time stamp	Time stamp	Wind Spd	Pnorm	Pressure	remp		dBA	dBA	dBA
	dd/mm/yy	hh:mm:ss	m/s	kW	Pa	2015	42 50	41.77	40.49	40.22
AOC_C_A2	03.30.99	11:10:59	7.25	-1.94	80500	291.5	40.32	40.16	38.18	38.78
AOC_C_A2	03.30.99	11:12:04	6.11	-1.99	80300	291.5	39.10	38.86	37.57	38.03
AOC_C_A2	03.30.99	11:13:09	5.57	-1.93	00500	201.5	37.62	37.06	36.38	37.65
AOC_C_A2	03.30.99	11:14:14	4.47	-1.94	00500	291.5	39.65	39.52	38.42	39.17
AOC_C_A2	03.30.99	11:15:20	5.10	-1.94	80300	294.5	42.59	42.32	42.73	44.96
AOC_C_A2	03.30.99	12:31:03	8.97	-1.01	90400	294 5	45.37	44,92	45.29	48.88
AOC_C_A2	03.30.99	12:32:08	7.34	-1.60	00400	294 5	43.66	43,60	43.59	48.92
AOC_C_A2	03.30.99	12:33:13	9.41	-1.04	80400	294.5	39.66	i 38.54	38.99	40.29
AOC_C_A2	03.30.99	12:42:58	8.90) -1.02	90400	294	5 37.13	36.74	37.01	36.99
AOC_C_A2	03.30.99	12:44:04	1.29	f -1.78		294	5 35.79	36.06	36.42	36.55
AOC_C_A2	03.30.99	12:45:09	6.42	2 -1.0	B0400	294 !	5 35.22	35.04	35.45	34.52
AOC_C_A2	03.30.99) 12:46:14	1 0.33	5 -1.75 5 -1.75	5 5040	n 294 !	5 36.45	36.45	i 36.84	36.71
AOC_C_A2	03.30.99) 12:47:1	3 5.0	-1.0	9 8040	0 294	5 37.93	37.09	37.52	38.74
AOC_C_A2	03.30.99	12:48:24	4.90 5 5 01	5 -1.00 5 -1.7	4 BO40	0 294	5 36,58	3 35.89	36.53	35.71
AOC_C_A2	03.30.99	12:49:2	9 5.6	5 -1.7* 6 -1.6*	7 8040	0 294	5 35.95	5 36.26	36.45	35.93
AOC_C_A2	2 03.30.99	12:50:34	4 5.10 n 40	1 -16	7 8040	0 294.	5 36.93	3 36.73	3 37.27	36.79
AOC_C_A2	2 03.30.99	12:51:3	9 4.0 4 E Ê	0 -16	7 8040	0 294.	5 35.04	4 35.21	35.83	34.72
AOC_C_A2	2 03.30.9	9 12:52:4	4 5.0	0 -1.0 2 -1.6	, 0040 8 8040	0 294.	5 36.5	7 36.73	3 37.16	36.37
AOC_C_A2	2 03.30.9	9 12:53:4	9 4.3	7 -17	0 0040 1 8040	0 294	5 42.2	9 41.0	1 41.60	44.61
AOC_C_A2	2 03.30.9	9 12:59:1	0 /./	2 -16	6 8040	0 294	5 40.4	9 39.7	1 40.30	40.13
AOC_C_A	2 03.30.9	9 13:00:2	. /.J	.4 .12	8040	294	5 38.6	3 38.5	7 38.41	38.79
AOC_C_A	2 03.30.9	9 13:22:3	0 50	-1.2	6 8040	294	5 41.0	6 40.5	8 41.14	41.53
AOC_C_A	2 03.30.9	9 13:24:4	-0 J.2 -0 6/	.0 -1.5	5 8040	0 294	.5 39.4	8 39.7	3 40.24	40.86
AOC_C_A	2 03.30.9	9 13:25:5	0.4 0.4		6 8040	0 294	.5 40.5	3 40.2	5 40.40) 41.68
AOC_C_A	2 03.30.9	9 13:29:3	14 J.4 IE 87	n 1.0	19 8040	0 294	.5 40.9	3 40.5	0 40.94	41.35
AOC_C_A	2 03.30.9	9 13:31.4	0 40	,	13 8040	10 294	.5 40.7	9 40.6	5 41.1	7 41.53
AOC_C_A	2 03.30.9	9 13:32:5	50 4.8 NO 4.8	57 -1 55 -1.5	23 8040	294	.5 38.1	0 37.9	5 38.3	2 38.63
AOC_C_A	2 03.30.9	9 13:35:0	JU 4.0	50 -1.	18 8040	294	.5 38.8	1 38.6	8 39.0	0 39.7 9
AOC_C_A	2 03.30.9	13:30:0	,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,	10 -1. 11 -1.	19 804	294	.5 38.7	2 38.2	5 39.4	5 39.53
AOC_C_A	2 03.30.9	JY 13:37:	11 DA 24 EA	/0 -1:	21 804	00 294	.5 38.3	37 38.4	7 39.1	3 39.60
AOC_C_A	2 03.30.9	99 13:39:	21 3.4							

Appendix C Log Sheets


Turbine	
Filename AOC_C_A2	
Comp time: 9:37	
DAT time 10:29	
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Date	Time	DATID	Range	Sensitivity	Action
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 $$\rm C$-2$$ Wind Turbine Generator System Acoustic Noise Test Report for the AOC 15/50 Wind Turbine

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Date 🔬 👘	Time	DATID	Range	Sensitivity	ACTION
mm/dd/vv	hh:mm:ss	1993 2002	mVpke	mVoruV/EU	
03/20/99	(1:10:02	84			Start Meas #1
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Page 38 of 20ge 2 of 2

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Acoustics Test Log

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Turbine	AOC-C-A	3 koc	515/50		
Filename	1				
Comp time		-			
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Wind Turbine Generator System Acoustic Noise Test Report for the AOC 15/50 Wind Turbine

Appendix D Test Plan



Wind Turbine Generator System

Acoustic Emission Test Plan

for the

AOC 15/50 Wind Turbine

at the **National Wind Technology Center** Golden, Colorado

by **National Wind Technology Center** National Renewable Energy Laboratory **1617 Cole Boulevard** Golden, Colorado 80401

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March 1, 1999

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<u>-1 May 99</u> Date <u>4 Mar 99</u>

Date

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4.0 Disclaimer

This report was prepared as an account of work sponsored by an agency of the United States government. The test results documented in this report define the characteristics of the test article as configured and under the conditions tested.

The United States government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Nor do they assume legal liability or responsibility for the performance of the test article or any similarly named article when tested under other conditions or using different test procedures.

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NREL is a National Laboratory of the U. S. Department of Energy, and as an adjunct of the U. S. Government, cannot certify wind turbines. The information in this report is limited to NREL's knowledge and understanding as of this date.

5.0 Test Objective

The objective of the test is to characterize the noise emissions of the AOC 15/50 wind turbine in a manner suitable for certification. To meet this objective, the test was conducted in accordance with the IEC draft standard for acoustic noise measurement techniques, IEC 61400-11 (Ref. 1). This report documents the measurement techniques, test equipment, analysis procedures, results, and uncertainty for the following quantities:

- apparent sound power level,
- dependence on wind speed,
- directivity,
- octave band levels,
- tonality.

6.0 Test Turbine

The test turbine was a model AOC 15/50 wind turbine manufactured by Atlantic Orient Corporation and installed at the National Wind Technology Center just south of Boulder, Colorado. The turbine has no serial number but was the third turbine of this type to be manufactured by Atlantic Orient Corporation.

The AOC 15/50 wind turbine is shown in Figure 1 and its configuration is detailed in Table 1. The turbine is a horizontal-axis, downwind, free-yaw, fixed-pitch machine. Hub height is 25 m (82 ft). Rotational energy is converted to electrical power in the nacelle, which contains a gearbox and a generator. Operation of the turbine is controlled from a programmable logic controller (PLC) located in a control shed on the ground. Wind speed data, required for operation of the wind turbine, is gathered from instrumentation located on the turbine tower.

The blades are lofted from NREL S825/S809/S810 thick-airfoil sections, and are made of woodepoxy laminates, reinforced with carbon fiber. The rotor is a three-bladed, fixed-pitch, stallregulated design. It has a diameter of 15 m (49.2 ft) and has a nominal speed of 65 rpm. For the present performance test, the blade pitch is set to 0.09°, where the pitch is measured at the blade tip, and positive pitch angles are towards feather. The rotor is connected directly to the gearbox main shaft, and the gearbox increases the main shaft speed to 1800 rpm, driving a three-phase, 60 Hz, 480 volt, induction generator.

The tower is a 24.4 m (80 ft) high free-standing, steel lattice, three-legged structure. The machine is controlled by a PLC that is located in a control house adjacent to the tower. This PLC communicates with the PLC in the nacelle and provides performance and maintenance diagnostic information. Connection to the grid is made at the switchboard enclosure in the control house.

A complete description of the AOC 15/50 control system is available in the AOC 15/50 Operations and Maintenance Manual (Ref. 2).



Figure 1. AOC 15/50 Test Turbine

	Test Turbine
General Configuration:	
Make and Model	Atlantic Orient Corporation, AOC 15/50
Rotation Axis (H / V)	Horizontal
Orientation (upwind / downwind)	Downwind
Number of Blades	3
Rotor Hub Type	Rigid
Rotor Diameter (m)	15.0
Hub Height (m)	25
Performance:	
Rated Electrical Power (kW)	50
Rated Wind Speed (m/s)	12
Cut-in Wind Speed (m/s)	4.9
Cut-out Wind Speed (m/s)	22.4
Extreme Wind Speed (m/s)	59.5
Rotor:	
Swept Area (m ²)	177
Rotational Speed (rpm)	65
Rotational Speed at reference wind speed	65
(rpm)	
Rotational Speed at rated power (rpm)	65
Coning Angle (deg)	6
Tilt Angle (deg)	0
Blade Pitch Angle (deg)	0.09
Power Regulation	Stall
Overspeed Control	Failsafe redundant aerodynamic tips and high-speed
	shaft brake
Drive Train:	
Gearbox Make, Type, Ratio	AOC Custom-made, Planetary, 28.25:1
Generator: Make, Type, Speed, Voltage,	Magnetek, 3-Phase Induction, 1800 rpm, 480 V, 60 Hz
Frequency	
Yaw System:	
Wind Direction Sensor	None
Yaw Control Method	Free
Tower:	
Туре	Lattice
Height	24.4
Control / Electrical System:	
Controller: Make, Type	Koyo Direct Logic 205, PLC
Power Converter: Make, Type	None
Logic System	PLC Ladder
Monitoring System	None
Electrical Output: Voltage, Frequency,	480 V, 60 Hz, 3-phase
Number of Phases	

Table 1. Test Turbine Configuration

7.0 Test Site

The test turbine is located at NREL's National Wind Technology Center, located off Colorado State Highway 128, approximately 8.1 km (5 miles) south of Boulder, Colorado. The turbine site, as shown in Figure 2, is at an approximate elevation of 1849 m (6065 ft).

Power connection is made to the wind site 13.8 kV main collector line via a cable from the site control house to a pad-mounted transformer (D68215) and breaker panel. The main collector line connects to the Public Service of Colorado's 69 kV distributor line, which represents an infinite load to the wind turbine.

The test site terrain is flat, farm land with an estimated roughness of 0.5 m. Table 2 lists the structures close to the test turbine. The turbine shed is located upwind of the microphone positions and its wake does not influence wind speed measurements or microphone measurements. The Bergey 850 W wind turbine noise does not influence microphone measurements.

Description	Bearing From Turbine	Distance From Test	Tower Or Structure Height	Rotor Diameter Or Structure Width	Operating Status
Turbing abod	240	22.7	2.0	2.5	
Turbine sneu	540	23.7	3.0	2.3	-
Whisper 3000	190	71.3	32.0	4.5	Operating

Table 2. Structures Close to AOC 15/50 Test Turbine

The existing meteorological tower is located 35.7 meters from the test turbine at a bearing of 292° true. This distance is 2.38 rotor diameters from the test turbine and within the range between 2 and 4 rotor diameters specified in the IEC standard.



Figure 2. Location of AOC 15/50 Test Turbine

8.0 Test Equipment

8.1 Equipment Description

Table 3 shows the list of equipment used for the test. All instruments met the requirements defined by the Standard.

Instrument	Manufacturer	Model Number	Serial Number	Calibration Due
Signal Analyzer	Hewlett Packard	35670A	3431A01613	8/14/00
Microphone 1	ACO Japan	7012	19037	1/29/00
Microphone 2	ACO Japan	7012	19014	1/29/00
Microphone 3	ACO Japan	7012	19017	1/29/00
Microphone 4	ACO Japan	7012	19035	1/29/00
Preamplifier 1	ACO Pacific	4012	79900503	1/29/00
Preamplifier 2	ACO Pacific	4012	96049	1/29/00
Preamplifier 3	ACO Pacific	4012	79900502	1/29/00
Preamplifier 4	ACO Pacific	4012	79900504	1/29/00
Acoustic Calibrator	Bruel & Kjaer	4230	861619	4/22/99
Digital Recorder	Sony	PC208AX	U3538	8/25/00
Anemometer	Met One	010C	T2346	10/29/99
Wind Vane	Met One	020C	U1475	12/18/99
Pressure Sensor	Omega	HHP-102	046/21	9/14/99
Temperature Sensor	Omega	869	T171111	9/14/99
GPIB Card	National	PCMCIA-	A2B275	n/a
	Instruments	GPIB		
DAQ Card	National	AI-16XE-50	A4CBCC	n/a
	Instruments			
Laptop Computer	Panasonic	CF-25	7DkSA01050	n/a
Campbell Datalogger	Campbell	CR23X	1214	10/16/00
	Scientific			

 Table 3. Equipment List for Acoustic Test

The data acquisition system synchronizes the acoustic measurements with the meteorological measurements. This system is run from a laptop computer. From the laptop, two PCMCIA (Personal Computer Memory Card International Association) cards are used. One card, a GPIB (General Purpose Interface Bus) card, controls and downloads one-minute acoustic data from the signal analyzer. The other card, a DAQ (Data Acquisition) card, records samples of wind speed, wind direction, and power data. The wind speed signal is shared with the power performance datalogger, pre-scaled to 1 Volt equals 360° and 1 Volt approximately equals 120 kW These signals are sent to the National Instruments DAQ card from the power performance datalogger continuous analog out ports. All meteorological signals are updated once a second. A Microsoft Visual Basic program AcoustDAQ Version 1.2 averages the meteorological data and synchronizes with the acoustic averages. The program also records, graphs, and updates the user on all incoming data.



Figure 3. Microphone Positions

8.2 Instrumentation Locations

Figure 3 shows the layout of the microphones. The radius, R_0 is determined by Equation 1.

$$R_o = H + \frac{D}{2}$$
 Equation 1

Table 4. Variables for Determining the Distance Detween the Turbine and Microphon	ones
---	------

Parameter	Description	Value	Units
R _o	reference distance,	32.5	m
Η	vertical distance from the ground to the rotor center,	25	m
D	diameter of the rotor.	15	m

Microphones were located 32.5 m from the center of the tower with positions as shown in Figure 3. Measurements from three microphones will be placed at microphone positions 1A, 1B, and 1C will meet the requirements for the reference microphone position shown in Table 5. One additional microphone will be moved between microphone positions 2, 3, and 4 to meet the requirements for these positions as shown in Table 5. No adjustments from the nominal microphone positions were required to avoid reflecting surfaces or to obtain allowable grazing angles.

The microphones were placed on a reflecting surface. The reflecting boards were 1 m diameter circular plywood boards with a thickness of approximately 13 mm. In addition, microphone primary windscreens were used. The primary windscreen was one half of an open cell foam sphere with a diameter of approximately 90 mm.

The anemometer was located on a meteorological tower at the turbine's hub height. The meteorological tower was located 35.7 m (2.38 rotor diameters) from the turbine at a bearing of 292° true.

To meet the requirements of the Standard, the NWTC-CT quality assurance document, AI05, is used to define allowable wind directions. With an anemometer height equal to turbine hub height and anemometer position 2.38 rotor diameters from the turbine, the tolerance on wind direction due to anemometer placement is 57°.

9.0 Measurement Procedures

9.1 Test Conduct

During the test, the temperature and pressure was read from the Campbell Scientific data logger and manually entered into laptop computer. Temperature and pressure were updated at least every 2 hours. Also, the microphone calibrations were documented on the log sheet, included in Appendix B. Changes to analyzer settings were also documented on the log sheet.

After the data acquisition and related equipment was checked out, the data acquisition program, AcoustDAQ, was initiated. AcoustDAQ requires the operator to start a new project file and enter general test information, such as turbine information and site characteristics. The operator enters some data, such as air pressure and temperature and the reference microphone position, at the beginning of each measurement session. A session is started when the turbine is stopped for background measurements, when it is started for operating measurements, and when microphone positions are changed.

The four microphones were calibrated through a procedure in AcoustDAQ. During the calibration process, the sensitivity factors to calibrate the microphone transducers were entered on the test log sheet (Appendix B). The microphones were also recalibrated at the start and end of each measurement session.

After the microphones were calibrated, a measurement session was started. AcoustDAQ initiated and triggered the signal analyzer that acquired and averaged four channels of microphone data. The program also acquired and averaged one-minute of wind speed and wind direction data. Wind speed averages were corrected to a reference height of 10 m using Equation 2. The data were accepted if the wind speed and wind direction were in the acceptable range. If the data were acceptable, the wind speed and wind direction averages were synchronized with the microphone averages and recorded in a data file along with pressure and temperature readings. One-minute octave averages were also downloaded from the analyzer, synchronized with the corrected wind speed, and stored in a separate data file.

AcoustDAQ also tracked how much data was collected. Different counts were kept of acceptable data sets according to wind speed. The number of data sets overall, with wind speed between 4 and 8 m/s, with wind speed between 8 and rated wind speed, and with wind speed between 6 and 10 m/s was tracked. The counts were kept for both turbine and background data sets.

9.2 Test Completion

The test was complete when all requirements listed in Table 5 are fulfilled.

Measurement Type	Microphon • Desition	Requirements
	e Position	
Overall measurements	1*	At least 30 one-minute averages.
Overall measurements	2, 3, and 4	At least 10 one-minute averages taken during a wind speed not differing more than 2 m/s from the acoustic reference wind speed.
For A-weighted sound pressure level:	1*	At least 10 measurements taken during a wind speed not differing more than 2 m/s from the acoustic reference wind speed (8 m/s).
		At least 8 of the measurements below the acoustic reference wind speed.
		At least 8 of the measurements above the acoustic reference wind speed.
For octave or third octave band measurements:	1*	At least 5 one-minute averaged spectra measured with wind speeds differing less than 2 m/s from the acoustic reference wind speed.
Narrow band measurements	1*	At least 2 minutes of measurements taken each for 4 integer wind speeds including the acoustic reference wind speed (8 m/s)

Table 5. Data Requirements for Turbine and Background Measurements

* - This position includes microphone positions 1A, 1B, and 1C.

10.0 Analysis Methods

10.1 Data Selection

The first step in the data analysis procedure is to reject all data obtained during the following circumstances:

- Interrupting noise sources such as a passing vehicle or airplane
- Failure of test equipment
- Wind direction is outside of allowable range
- Wind speed is outside of allowable range
- Turbine failure
- Adverse weather conditions

10.2 Wind Speed Correction

Wind speed was corrected to the reference condition of an anemometer height of 10 meters using Equation 2.

$$V_{\rm s} = V_{z} \left[\frac{\ln \frac{z_{ref}}{z_{oref}} \ln \frac{H}{z_{o}}}{\ln \frac{H}{z_{oref}} \ln \frac{z}{z_{o}}} \right]$$
Equation 2

Parameter	Description	Value	Units
Vs	corrected wind speed	-	m/s
Vz	wind speed measured at anemometer height z	-	m/s
Zoref	reference roughness length of 0.05 m	0.05	m
Zo	roughness length	0.05	m
Н	rotor center height	25	m
Z _{ref}	reference height 10 m	10	m
Z	anemometer height	25	m

Table 6. Variables for Standardizing Wind Speed

10.3 A-Weighted Sound Power Level

A linear regression analysis will be done with at least 10 pairs of equivalent continuous sound pressure levels from the microphone at the reference positions and the corrected wind speed. These pairs were selected to cover wind speeds that differ less than 2 m/s from the acoustic reference wind speed of 8 m/s or wind speeds between 6 and 10 m/s. The reference position sound pressure level, L_{Aeq} , is the value of the regression line at the acoustic reference wind speed. A similar analysis yields the background noise level at the acoustic reference wind speed. If the sound pressure level is less than 6 dB but more than 3 dB higher than the background sound pressure level, the turbine sound pressure level is corrected for background by subtracting 1.3 dB and marked by an asterisk, "*". These corrected sound pressure levels would not be used in calculating the apparent sound power level or directivity. If the difference was less than 3 dB, no data will be reported and it will be reported the turbine noise was less than the background noise. If the turbine sound pressure level was more than 6 dB above the background sound pressure levels, Equation 3 corrects the measured turbine noise level for background noise and provides the corrected sound pressure level at the reference was pressure levels. Laeq.

$$L_{Aeq,c} = 10 * \log \left[10^{(0.1L_{s+n})} - 10^{(0.1L_n)} \right]$$
 Equation 3

Parameter	Description	Units
L _{Aeq,c}	sound pressure level of the turbine operating alone	dB
L _{s+n}	sound pressure level of the turbine plus background	dB
L _n	sound pressure level of the background	dB

Table 7. Variables for Determining Equivalent Sound Pressure Level

Finally, we calculated the apparent sound power level, L_{WA} , from the corrected sound pressure level using Equation 4.

$$L_{WA} = L_{Aeq,c} - 6 + 10 * \log\left(\frac{4\pi R_1^2}{S_0}\right)$$

Equation 4

Table 8.	Variables in	Calculating the	Apparent Sound	Power Level
----------	--------------	-----------------	----------------	-------------

Parameter	Description	Units
L _{Aeq,c}	background-corrected, A-weighted, sound pressure level at the	
	acoustic reference wind speed under reference conditions,	
R ₁	slant distance from the rotor center to the microphone	m
So	reference area $S_0 = 1 m^2$	m^2

10.4 Wind Speed Sensitivity

In addition to the scatter plot obtained from the procedure in Section 8.4.3, the IEC Standard requires that wind speed sensitivity be defined by binning the reference microphone data into integer values of corrected wind speed. For each bin, the reference position sound pressure level was corrected for that bin's background noise as described above.

10.5 Directivity

Directivity, Δ_i , is the difference in A-weighted sound pressure levels at Positions 2, 3, and 4 compared to the A-weighted sound pressure levels at the reference position. The sound pressure levels at the reference wind speed of 8 m/s were corrected for background noise using the methods described in Section 8.4.3. In addition, corrections were made for differences in slant distances. (Slant distance is the distance from the microphone to the center of the turbine's rotor.) The directivity at each position is calculated by Equation 5.

$$\Delta_i = L_{Aeq,i} - L_{Aeq,1} + 20 * \log\left(\frac{R_i}{R_1}\right).$$
 Equation 5

Parameter Description Units A-weighted sound pressure level at positions 2, 3, or 4, corrected dB L_{Aeq.i} for background noise in the same position, A-weighted sound pressure level at the reference position, dB L_{Aeq,1} measured simultaneously with $L_{\mbox{\scriptsize Aeq,I}}$ and also corrected for background noise, slant distance between the rotor center and positions 2, 3, or 4 Ri m slant distance between the rotor center and the reference position. R_1 m

Table 9. Variables in Determining the Directivity

10.6 Octave Spectra

Spectral content of the noise signal at the reference microphone is obtained using the spectrum analyzer's octave analysis setting.

10.7 Tonal Analysis

10.7.1 Tonality at the Acoustic Reference Wind Speed (8 m/s)

Quantification of the tonal characteristics is the final analysis activity. The first step in this analysis is to identify a data set where wind speed is close to 8 m/s for a minimum of 2 minutes. The signal analyzer was set to perform Fast Fourier Transforms (FFTs) using a Hanning window in the time domain and 800 lines resolution. The unweighted noise data from the reference position microphone were played back from the DAT recorder to the signal analyzer.

The frequency resolution accounted for a 50 percent decrease in resolution resulting from use of a Hanning window, calculated by Equation 6. (The frequency resolution used in this analysis is much finer than the 20-57 hertz required by the Standard.) The spectra were RMS-averaged and saved as files listed in the table above. The files are imported into an Exceltm spreadsheet for plotting. The plots allow the analyst to identify suspected tones.

Effective NoiseBandwidth =
$$\frac{Band}{Number of lines}$$
 *Window Factor Equation 6

Next, each suspected tone was compared to the masking level of its neighboring frequencies. The range of neighboring frequencies that was considered was called the "critical band" and was defined as follows:

- 1. If the suspected tone is between 20 and 500 hertz, the critical band spans 100 hertz.
- 2. If the suspected tone is above 500 hertz, the critical band spans 20% of the tone frequency.

If a suspected tone is single peak, the critical band is located to center the peak. If the suspected tone consists of multiple peaks closely spaced, the critical band is located to include the largest possible number of the most prominent peaks. If the suspected tone is between 20 and 70 hertz, the critical band is 20 to 120 hertz.

Each line in the critical band was then classified according to the following criteria:

- 1. A peak is classed as a tone if its RMS-averaged level is:
 - more than 6 dB above the average masking level. The average masking level is the logarithmic average of the sound pressure levels of the rest of the lines in the critical band but excluding one line each side of the peak.
- 2. Lines adjacent to a tone are also classified as a tones if their RMS-averaged levels are:
 - within 10dB of the peak and
 - more than 6 dB above the average masking level.
- 3. Lines adjacent to a tone are classified as neither tones nor masking if their RMS-averaged levels are:
 - more than 10dB below the peak level and
 - more than 6 dB above the average masking level.
- 4. Lines are classified as masking if their RMS-averaged levels are less than 6 dB above the average masking level.

Because classifying a line as a tone means it can no longer be counted as masking, an iterative procedure is required for the proper identification of tones and masking. A spreadsheet analysis method is used for this iteration. For more information, refer to the NWTC-CT quality assurance document, AI09.

This process was repeated for every suspected tone in the spectrum. The result was that within each critical band every spectral line was classified as tone energy, masking energy or neither. The frequency of each tone was also determined during this part of the analysis.

The next step in tonal analysis was to determine the maximum sound pressure level of the tone(s). The sound data were again played from the DAT recorder into the signal analyzer. This time the analyzer was programmed to display the spectra as a "waterfall." The analyst used analyzer functions to slice through the waterfall-displayed spectra at single frequency bins (frequency lines). Sound pressure levels of the tone in each spectrum were saved in files whose names correspond with the frequency of the tone. These files were imported into an Exceltm spreadsheet and sorted to enable the analyst to identify and arithmetically-average the maximum 25% of the sound pressure levels of each tone. Finally, if multiple tones were present within the critical band, they are energy-summed to determine the overall tone level, L_{pt} .

Next the analyst determined the sound pressure level of the masking noise, L_{pn} , in the critical bands. Masking energy was calculated from the same 2-minute data set as used to determine the tone level. The short-term spectra were RMS-averaged into a single, 2-minute spectrum. The masking level was corrected for the reduction in the number of lines due to the exclusion of tones and for the Hanning window using Equation 7.

$$L_{pn} = L_{pn,avg} + 10 * \log\left(\frac{bandwidth \ of \ critical \ band}{effective \ noise \ bandwidth}\right)$$
Equation 7

Table 10.	Variables in Determining the Masking Noise Level
-----------	--

Parameter	Description	Units
L _{pn}	Sound pressure level of masking noise within a critical band,	dB
L _{pn,avg}	energy averaged measured masking noise determined by	dB
	averaging the masking noise separate from any tones within the	
	critical band.	

The analyst determined if background noise affected the masking noise level by performing an FFT of background noise obtained under similar wind conditions to those used for the turbine operating noise analysis. First, the analyst verified that the background noise does not contain the same tone as the turbine noise. Next, the analyst determined the background noise level for the same critical band as used for each tone. Equation 3 was used to correct the masking noise level of each critical band for background noise. If background noise level was within 6 dB of the masking noise, then the report states that the masking noise was affected by background noise.

The analyst determined the tone level difference, $\Delta L_{tn,max}$, between the maximum tone level and the background-corrected masking noise level using Equation 8.

$$\Delta L_{tn,\max} = L_{pt} - L_{pn}$$

Equation 8

Table 11. Variable in Determining the Tone Level Difference

Parameter	Description	Units
$\Delta L_{tn,max}$	Tone level difference,	dB
L _{pt}	maximum tone level within the critical band,	dB
L _{pn}	total masking noise within the critical band.	dB

Tone levels were subjected to a final check for audibility by determining the minimum tone level, $\Delta L_{tm,crit}$, that an average listener would be able to hear using Equation 9.

$$\Delta L_{tn,crit} = -2 - \log \left[1 + \left(\frac{f}{502}\right)^{2.5} \right]$$

Equation 9

Table 12.	Variables in	Determining the	Masking Threshold

Parameter	Description	Units
$\Delta L_{tn,crit}$	Masking threshold for tones in noise,	dB
f	frequency at the center of the critical band.	dB

If the tone level difference, $\Delta L_{tn,max}$, is less than $\Delta L_{tm, crit}$, the tone is not reported.

For each value of $\Delta L_{tn,max}$ a frequency dependent correction must be applied to compensate for the response of the human ear to tones of different frequency.

The 'tonal audibility', $\Delta L_{a,max}$, is defined as:

$$\Delta L_{a,\max} = \Delta L_{tn,\max} - L_{ac}$$
 Equation 10

Where L_a is the frequency dependent audibility criterion, defined as:

$$L_a = -2 - \log_{10} \left[1 + \left(\frac{f}{502}\right)^{2.5} \right]$$
 Equation 11

A corresponding value of $\Delta L_{a,max}$ must be calculated for each value of $\Delta L_{tn,max}$. For tonal audibilities meeting the condition:

$$\Delta L_{a,\max} \ge 0$$
 Equation 12

the values of $\Delta L_{a,max}$ must be reported. According to the criterion curve defined above, a 'typical' listener would consider such tones as being 'audible'. For tonal audibilities not meeting this condition, there is no requirement to report the values. According to the criterion curve defined above, a 'typical' listener would consider such tones as being 'inaudible'.

10.7.2 Wind Speed Dependence of Tonality

The wind speed and spectra are averaged over a two-minute period for acoustic/wind speed data pairs and binned into integer wind speed bins. The bins must cover at least a 4 m/s wind speed range including the acoustic reference wind speed (8 m/s). A tonal analysis will be done on measurements in each bin as detailed in the previous section.

11.0 Uncertainty

The combined uncertainty is reported for the apparent sound power level, directivity, wind speed dependence, and tonality. The combined standard uncertainty is the combination of type A and type B uncertainties. Type A uncertainty components are evaluated by using statistical methods to a series of repeated measurements. Type B uncertainty components are evaluated through estimations or calibrations. The methods used to evaluate the uncertainty components for the apparent sound power level, directivity, wind speed dependence and tonality will be explained in this section.

11.1 A-Weighted Sound Power Level

The type A uncertainty for the apparent sound pressure level is the standard error of the estimated L_{Aeq} at the acoustic reference wind speed. This is found from the linear regression analysis.

$$U_A = \sqrt{\frac{\Sigma(y - y_{est})^2}{N - 2}}$$

Equation 13

Parameter	Description	Units
U _A	Type A uncertainty for apparent sound pressure level,	dB
у	measured sound pressure level,	dB
y _{est}	estimated sound pressure level using linear regression,	dB
Ν	Number of measurements used in the linear regression.	

Table 13. Type A Apparent Sound Power Level Uncertainty Components

The Type B uncertainty is found using Equation 14. It components are listed in Table 14:

$$U_{B} = \sqrt{U_{B1}^{2} + U_{B2}^{2} + U_{B3}^{2} + U_{B4}^{2} + U_{B5}^{2} + U_{B6}^{2} + U_{B7}^{2} + U_{B8}^{2} + U_{B9}^{2}}$$
 Equation 14

Parameter	Description	Unit	Source
U _B	Type B uncertainty for apparent sound pressure level	dB	
U _{B1}	uncertainty for calibration of the instruments,	dB	calibrator calibration and the standard error from field calibrating microphones
U _{B2}	uncertainty for tolerances on the chain of acoustic measurement instruments,	dB	signal analyzer, microphone, microphone adapter, and preamplifier
U _{B3}	uncertainty for acoustic conditions for microphone mounting board,	dB	estimate
U _{B4}	uncertainty on the distance from microphone to hub,	dB	estimate
U _{B5}	uncertainty on the acoustic impedance of air,	dB	estimate
U _{B6}	uncertainty on the acoustic emission of the turbine due to changing weather conditions,	dB	estimate
U _{B7}	uncertainty on the measured wind speed	dB	anemometer calibration and estimate of the site effects
U _{B8}	uncertainty on the wind direction measurement,	dB	Estimate
U _{B9}	uncertainty for the background correction.	dB	Applied background correction

Table 14. Type B Apparent Sound Power Level Uncertainty Components

These uncertainties are combined into one standard uncertainty using Equation 15.

$$U_C = \sqrt{U_A^2 + U_B^2}$$

Equation 15

Table 15.	Overall	Uncertainty	Components
-----------	---------	-------------	-------------------

Parameter	Description	Units
U _C	Overall standard uncertainty for apparent sound pressure level,	dB
U _A	Type A uncertainty for apparent sound pressure level,	dB
U _B	Type B uncertainty for apparent sound pressure level	dB

11.2 Wind Speed Sensitivity

Type A uncertainty for wind speed dependence is found from the from a linear regression analysis. The uncertainty, U_A is calculated for integer wind speeds as the root sum of the squared standard error of the estimated value at the actual wind speed. The squared standard error is given by Equation 16.

$$s_i = \sqrt{\frac{\sum (L_{Aeq} - L_{Aeq,j})^2}{(N-1)^2}}$$

Equation 16

Table 16.	Type A	Wind De	pendence	Uncertainty	Components
					1

Parameter	Description	Units
Si	Type A standard uncertainty for bin i	dB
L _{Aeq}	Average of the sound pressure levels in the bin i	dB
L _{Aeq,i}	sound pressure level in the bin	dB
N	number of measurement results in the bin	

The type B uncertainty for each bin is found by combining the components listed in Table 17 and the square root of the some of the squares.

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Parameter	Description	Unit	Source
U _B	Type B uncertainty for bin i	dB	
U _{B1}	uncertainty for calibration of the instruments,	dB	calibrator calibration and the standard error from field calibrating microphones
U _{B2}	uncertainty for tolerances on the chain of acoustic measurement instruments,	dB	signal analyzer, microphone, microphone adapter, and preamplifier
U _{B3}	uncertainty for acoustic conditions for microphone mounting board,	dB	estimate
U _{B4}	uncertainty on the distance from microphone to hub,	dB	estimate
U _{B5}	uncertainty on the acoustic impedance of air,	dB	estimate
U _{B6}	uncertainty on the acoustic emission of the turbine due to changing weather conditions,	dB	estimate
U _{B7}	uncertainty on the measured wind speed	dB	anemometer calibration and estimate of the site effects
U _{B8}	uncertainty on the wind direction measurement,	dB	Estimate
U _{B9}	uncertainty for the background correction.	dB	Applied background correction

 Table 17. Type B Wind Dependence Uncertainty Components

11.3 Directivity

An estimate of the standard uncertainty on the directivity is shown in Equation 17.

$$U_D = \sqrt{2} U_C$$
 Equation 17

Table 18. Variables for Estimating Directivity Uncertainty

Parameter	Description	Unit
UD	Standard uncertainty for directivity,	dB
U _C	Overall standard uncertainty for apparent sound pressure	dB
	level.	

11.4 Octave Spectra

For the third octave band, U_A for each band is the standard error on the averaged band level.

$$U_A = \sqrt{\frac{\sum (y - y_{est})^2}{N - 1}}$$
 Equation 18

Parameter	Description	Units
U _A	Type A standard uncertainty for band	dB
У	Sound pressure level of the band	dB
Y _{est}	Average sound pressure level of the band	dB
N	number of measured spectra	

Table 19. Type A Octave Band Uncertainty Components

The type B uncertainty components are estimated to be the same except for U_{B3} . It will be considered much larger than for L_{WA} , estimated value is 1.2 dB as shown in Table 20.

Parameter	Description	Unit	Source
U _B	Type B uncertainty for octave bands	dB	
U _{B1}	uncertainty for calibration of the instruments,	dB	calibrator calibration and the standard error from field calibrating microphones
U _{B2}	uncertainty for tolerances on the chain of acoustic measurement instruments,	dB	signal analyzer, microphone, microphone adapter, and preamplifier
U _{B3}	uncertainty for acoustic conditions for microphone mounting board,	dB	estimate
U _{B4}	uncertainty on the distance from microphone to hub,	dB	estimate
U _{B5}	uncertainty on the acoustic impedance of air,	dB	estimate
U _{B6}	uncertainty on the acoustic emission of the turbine due to changing weather conditions,	dB	estimate
U _{B7}	uncertainty on the measured wind speed	dB	anemometer calibration and estimate of the site effects
U _{B8}	uncertainty on the wind direction measurement,	dB	Estimate
U _{B9}	uncertainty for the background correction.	dB	Applied background correction

Table 20. Type B Octave Band Uncertainty Components

12.0 Reporting

After the test has been completed to the above requirements and NREL has analyzed the data, a test report will be generated. This report will consist of two main volumes. The first is the test results, which will consist of the following sections:

- A-weighted sound power level
- Wind speed sensitivity (graphically and tabularly)
- Plots of all data and regression lines
- Directivity
- Octave spectra (graphically and tabularly)
- Tonal analysis including wind speed dependence of tonality

- Uncertainty
- Exceptions to the test plan

The goal of Volume 1 of the test report is that the client will have a small and easily usable summary of the acoustic noise test done on their turbine. Volume 2 of the test report is the Test Plan, where all the details of the turbine and test equipment are listed.

13.0 Roles and Responsibilities

Table 21 lists the test team and identifies roles and responsibilities for each team member.

Test Team	Person (Employer)	Roles and Responsibility
Title		
Test Manager	Hal Link - NREL	Overall test management and responsibility.
		Customer contact person. Authorization for
		any deviations from planned test procedures.
		Reviews and approves test plan and test
		report.
Test Engineer	Arlinda Huskey – NREL	Supervision of acoustic test set-up, checkout,
and Analyst		and conduct. Periodic review of test data.
		Review and report test results. Primary point
		of contact between test technician and the test
		site manager.
Test Technician	Mark Meadors – NREL	Responsible for installation and maintenance
		of test equipment. Also assists in execution of
		test.
Site Technician	Mark Meadors – NREL	Provide on-site assistance to test, responsible
		for turning on/off surrounding turbines and
		test turbine. Must be available during regular
		working hours and off-hours.

 Table 21. Roles and Responsibilities

14.0 References

- 1. IEC 61400-11: Wind Turbine Generator Systems, Part 11: Acoustic Noise Measurement Techniques, 88/67/FDIS, International Electrotechnical Commission, Netherlands, 1995 as corrected by TJ Dubois Jan 1998.
- 2. AOC 15/50 Wind Turbine Operation & Maintenance Manual, Atlantic Orient Corporation, Revision 1.1, 1995.

15.0 Appendix A: Calibration Sheets

Microphone 1 calibration s/n 19037 Microphone 2 calibration s/n 19014 Microphone 3 calibration s/n 19017 Microphone 4 calibration s/n 19035 Preamplifier 1 calibration s/n 79900503 Preamplifier 2 calibration s/n 96049 Preamplifier 3 calibration s/n 79900502 Preamplifier 4 calibration s/n 79900504 Signal Analyzer Acoustic Calibrator DAT Recorder Anemometer Wind vane Pressure Sensor **Temperature Sensor** Campbell Datalogger

Costa Mesa, CA 92626 714-540-0169						
	CER	r I P I	CATE	OF CAI	LIBRATION	
Customer 1	Name: IN	STRUMENI	REPAIR LAB	S, INC	Dept :	
	II	NSTR	UMENT	INFORM	ATION	
Manufactu	rer : ACO	O PACIFI	C	Report # :	15608-1	
Model #	: 70	12		Cust P.O.# :	015726	
Asset #	: 190	033		Date Recvd :	01/25/99	
Serial #	: 190	US7 CDODUONE	7	Accuracy :	±.12DB	
Descriptio	on : Mit	/20/00	5	Tomporature.	21	
Date Due	· 01	/29/00		Humidity ·	49	
Interval	: 12	, 25, 00		Employee # :	17	
	COND	ITIC) N I NS'	CRUMENT	RECEIVED	
Condition	Receive	d: In 7	Colerance			
Remarks :	UNIT SE	NSATIVII	TY FOUND TO I	BE -34.5DB RI	E IV/PA	
	COND	ITIC)N INS'	r u m b n t	RETURNED	
Condition	Returned	d : In 7	Colerance			
Remarks :	SEE ATT	ACHED CH	LART FOR FRE	QUENCY CURVE.		
OTHER STAN	NDARDS U	SED: 595	5, 051			
****************************					•	
	Manufac	turor i	Model #		Description	Due Date
631	BRIJEL &	KJAER	1023	MFR SPECS	SINE/RADNOM GENER	12/23/99
632	BRUEL &	KTAER	2706	MFR. SPECS.	POWER AMPLIFIER	12/23/99
653	BRUEL &	KJEAR	2610	MFR. SPECS.	MEASURING AMPLIFI	04/09/99
654	BRUEL &	KJAER	2307	MFR. SPECS.	LEVEL RECORDER	03/30/99
655	BRUEL &	KJAER	4142	MFR. SPECS.	MIC CAL APPARATUS	04/10/99
089	BRUEL &	KJAER	4228	.09 dB	PISTONPHONE	09/05/99
593	BRUEL &	KJAER	4165	±.12 DB	MICROPHONE	06/19/99

Excalibur Engineering Inc. 3198-C Airport Loop Dr.

Excalibur Engineering Inc. certifies that the instrument specified above meets the manufacturer's specifications and has been calibrated using standards and instruments also listed above whose accuracies are traceable to the National Institute of Standards and Technology (NIST), and the calibration systems and records are in compliance to ISO-10012 and ANSI Z540-1. This document cannot be reproduced without prior approval.

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Microphone 2 Calibration Sheet for s/n 19014

Excalibur Engineering Inc. 3198-C Airport Loop Dr. Costa Mesa, CA 92626 714-540-0169							
C E	RTIFICATE	OF CA	LIBRATION				
Customer Name: Manufacturer : Model # : Asset # : Serial # : Description : Date Cal : Date Due : Interval :	INSTRUMENT REPAIR I N S T R U M E N ACO PACIFIC 7012 19035 19014 MICROPHONE 01/29/99 01/29/00 12	LABS, INC T INFORM Report # : Cust P.O.# : Date Recvd : Accuracy : Maint. Proc: Temperature: Humidity : Employee # :	Dept : A T I O N 15608-3 015726 01/25/99 ±.12DB 1371 21 49 17				
C O Condition Rece Remarks : UNIT	NDITION II vived : In Tolerance SENSATIVITY FOUND	STRUMENT S TO BE -33.23DB	R B C B I V B D RE IV/PA				

CONDITION INSTRUMENT RETURNED Condition Returned : In Tolerance Remarks : OTHER STANDARDS USED: 595, 051

		STANDAI	RDS USBI)	
ID #	Manufacturer	Model #	Accuracy	Description	Due Date
631	BRUEL & KJAER	1023	MFR. SPECS.	SINE/RADNOM GENER	12/23/99
632	BRUEL & KJAER	2706	MFR. SPECS.	POWER AMPLIFIER	12/23/99
653	BRUEL & KJEAR	2610	MFR. SPECS.	MEASURING AMPLIFI	04/09/99
654	BRUEL & KJAER	2307	MFR. SPECS.	LEVEL RECORDER	03/30/99
655	BRUEL & KJAER	4142	MFR. SPECS.	MIC CAL APPARATUS	04/10/99
089	BRUEL & KJAER	4228	.09 dB	PISTONPHONE	09/05/99
593	BRUEL & KJAER	4165	±.12 DB	MICROPHONE	06/19/99

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Microphone 3 Calibration Sheet for s/n 19017

Excalibur Engineering Inc. 3198-C Airport Loop Dr. Costa Mesa, CA 92626 714-540-0169 CALIBRATION CERTIFICATE OF Customer Name: INSTRUMENT REPAIR LABS, INC Dept : INSTRUMENT INFORMATION Manufacturer : ACO PACIFIC Report # : 15608-2 Model # Cust P.O.# : 015726 : 7012 Date Recvd : 01/25/99 Asset ₩ : 19036 Serial # : 19017 Accuracy : ±.12DB Description : MICROPHONE Maint. Proc: 1371 Date Cal : 01/29/99 Temperature: 21 : 49 Date Due : 01/29/00 Humidity : 12 Employee # : 17 Interval CONDITION INSTRUMENT RECEIVED Condition Received : In Tolerance Remarks : UNIT SENSATIVITY FOUND TO BE -34.95DB RE IV/PA CONDITION INSTRUMENT RETURNED Condition Returned : In Tolerance Remarks : SEE ATTACHED CHART FOR FREQUENCY CURVE. OTHER STANDARDS USED: 595, 051 STANDARDS USED Model # Due Date ID # Manufacturer Accuracy Description MFR. SPECS. SINE/RADNOM GENER 12/23/99 631 BRUEL & KJAER 1023 632 BRUEL & KJAER 2706 MFR. SPECS. POWER AMPLIFIER 12/23/99 653 BRUEL & KJEAR 2610 MFR. SPECS. MEASURING AMPLIFI 04/09/99 MFR. SPECS. 03/30/99 BRUEL & KJAER LEVEL RECORDER 654 2307 MIC CAL APPARATUS 04/10/99 655 BRUEL & KJAER 4142 MFR. SPECS. 089 BRUEL & KJAER 4228 .09 dB PISTONPHONE 09/05/99 MICROPHONE 06/19/99 ±.12 DB 593 BRUEL & KJAER 4165 Excalibur Engineering Inc. certifies that the instrument specified above

meets the manufacturer's specifications and has been calibrated using standards and instruments also listed above whose accuracies are traceable to the National Institute of Standards and Technology (NIST), and the calibration systems and records are in compliance to ISO-10012 and ANSI Z540-1. This document cannot be reproduced without prior approval.

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Microphone 4 Calibration Sheet for s/n 19035

Excalibur Engineering Inc. 3198-C Airport Loop Dr. Costa Mesa, CA 92626 714-540-0169 CERTIFICATE OF CALIBRATION Customer Name: INSTRUMENT REPAIR LABS, INC Dept : INSTRUMENT INFORMATION Manufacturer : ACO PACIFIC Report # : 15608-4 Cust P.O.# : 015726 Model # : 7012 Asset # Serial # : 19034 Date Recvd : 01/25/99 : 19035 Accuracy : ±.12DB Description : MICROPHONE Maint. Proc: MFIB Temperature: 21 Humidity : 49 : 01/29/99 Date Cal Date Due : 01/29/00 Employee # : 17 Interval : 12 CONDITION INSTRUMENT RECEIVED Condition Received : In Tolerance Remarks : UNSIT SENSATIVITY FOUND TO BE -34.23DB CONDITION INSTRUMENT RETURNED Condition Returned : In Tolerance Remarks : OTHER STANDARDS USED: 595, 051

			8	S T A N D A H	t d s	USBE)	
ID #	Manufa	ict	urer	Model #	Accui	cacy	Description	Due Date
631	BRUEL	&	KJAER	1023	MFR.	SPECS.	SINE/RADNOM GENER	12/23/99
632	BRUEL	&	KJAER	2706	MFR.	SPECS.	POWER AMPLIFIER	12/23/99
653	BRUEL	&	KJEAR	2610	MFR.	SPECS.	MEASURING AMPLIFI	04/09/99
654	BRUEL	&	KJAER	2307	MFR.	SPECS.	LEVEL RECORDER	03/30/99
655	BRUEL	&	KJAER	4142	MFR.	SPECS.	MIC CAL APPARATUS	04/10/99
089	BRUEL	&	KJAER	4228	.09 d	lB	PISTONPHONE	09/05/99
593	BRUEL	&	KJAER	4165	±.12	DB	MICROPHONE	06/19/99

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Preamplifier 1 Calibration Sheet for s/n 79900503

Excalibur Engineering Inc. 3198-C Airport Loop Dr. Costa Mesa, CA 92626 714-540-0169							
CB	RTIFICATE	OF CAI	LIBRATION				
Customer Name: Manufacturer : Model # : Asset # : Serial # : Description : Date Cal : Date Due : Interval :	INSTRUMENT REPAIR INSTRUMEN ACO PACIFIC 4012 NAN L79900503 1/2" MIKE PREAMP. 01/29/99 01/29/00 12	LABS, INC T INFORM Report # : Cust P.O.# : Date Recvd : Accuracy : Maint. Proc: Temperature: Humidity : Employee # :	Dept : A T 1 O N 15608-9 015726 01/25/99 MFR. SPECS. MFIB 21 49 17				
CONDITION INSTRUMENT RECEIVED Condition Received : In Tolerance Remarks :							
CONDITION INSTRUMENT RETURNED Condition Returned : In Tolerance Remarks :							

		STANDA	RDS USE	D	
ID #	Manufacturer	Model #	Accuracy	Description	Due Date
595	HEWLETT PACKAR	8903B	MFR SPECS	AUDIO ANALYZER	06/17/99

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Excalibur Engineering Inc. 3198-C Airport Loop Dr. Costa Mesa, CA 92626 714-540-0169							
CERTIFICATE OF CALIBRATION							
Customer	Name: INSTRUMENT REPAID	R LABS, INC	Dept :				
Manufactu Model # Asset # Serial # Descripti Date Cal Date Due Interval	INSTRUMEI rer: ACO PACIFIC : 4012 : NAN : XX96049 on : 1/2" MIKE PREAMP : 01/29/99 : 01/29/00 : 12	T INFORM Report# : Cust P.O.# : Date Recvd : Accuracy : Maint. Proc: Temperature: Humidity : Employee # :	A T I O N 15608-8 015726 01/25/99 MFR. SPECS. MFIB 21 49 17				
Condition Remarks :	CONDITION I Received : In Tolerand	NSTRUMENT ce	RECEIVE	D			
Condition Remarks :	CONDITION E Returned : In Tolerand	NSTRUMENT ce	BETURNE.	D			
	STAN	DARDS USE	D				
1D # 595	Manufacturer Model HEWLETT PACKAR 8903B	ACCUTACY MFR SPECS	Description AUDIO ANALYZER	Due Date 06/17/99			

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Preamplifier 3 Calibration Sheet for s/n 79900502

3198-C Airport Loop Dr. Costa Mesa, CA 92626 714-540-0169					
CERTIFICATE	OF CALIBRATION				
Customer Name: INSTRUMENT REPAIR LABS I N S T R U M E N T Manufacturer : ACO PACIFIC Model # : 4012 Asset # : NAN Serial # : L79900502 Description : 1/2" MIKE PREAMP. Date Cal : 01/29/99 Date Due : 01/29/00 Interval : 12	, INC Dept : INFORMATION Report # : 15608-6 Cust P.O.# : 015726 Date Recvd : 01/25/99 Accuracy : MFR. SPECS. Maint. Proc: MFIB Temperature: 21 Humidity : 49 Employee # : 17				
CONDITION INST Condition Received : In Tolerance Remarks :	RUMENT RECEIVED				
CONDITION INST Condition Returned : In Tolerance Remarks :	RUMENT RETURNED				
ID # Manufacturer Model # . 595 HEWLETT PACKAR 8903B 1	Accuracy Description Due Date MFR SPECS AUDIO ANALYZER 06/17/99				
Excalibur Engineering Inc. certifies meets the manufacturer's specifi using standards and instruments al	that the instrument specified above cations and has been calibrated so listed above whose accuracies are				

Excalibur Engineering Inc.

traceable to the National Institute of Standards and Technology (NIST), and the calibration systems and records are in compliance to ISO-10012 and ANSI Z5401. This document cannot be reproduced without prior approval.

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Excalibur Engineering Inc. 3198-C Airport Loop Dr. Costa Mesa, CA 92626 714-540-0169					
C I	BRTIFICATE	OF CA	LIBRATION		
Customer Name:	INSTRUMENT REPAIR LA	BS, INC	Dept :		
Manufacturer : Model # : Asset # : Serial # : Description : Date Cal : Date Due : Interval :	ACO PACIFIC : 4012 : NAN : L79900504 : 1/2" MIKE PREAMP. : 01/29/99 : 01/29/00 : 12	Report # : Cust P.O.# : Date Recvd : Accuracy : Maint. Proc: Temperature: Humidity : Employee # :	A 1 0 A 15608-10 015726 01/25/99 MFR. SPECS. MFIB 21 49 17		
C O Condition Rece Remarks :	NDITION INS sived : In Tolerance	ITRUMENT	RECEIVED		
C O Condition Retu Remarks :	NDITION INS arned : In Tolerance	TRUMENT:	RETURNBD		
ID # Manu 595 HEWI	S T A N D 3 lfacturer Model # LETT PACKAR 8903B	A CCUTACY MFR SPECS	Description Du AUDIO ANALYZER 00	ue Date 6/17/99	

Excalibur Engineering Inc. certifies that the instrument specified above meets the manufacturer's specifications and has been calibrated using standards and instruments also listed above whose accuracies are traceable to the National Institute of Standards and Technology (NIST), and the calibration systems and records are in compliance to ISO-10012 and ANSI Z549 1. This document cannot be reproduced without prior approval.

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Signal Analyzer Calibration Sheet

С	ertificate Of Calibration
Model No:	35670A
Serial No:	3431A01613
Description:	DYNAMIC SIGNAL ANALYZER
Customer Name:	NATIONAL RENEWABLE ENERGY LABORATORY
Agreement No.	VISA/ARLINDA HUSKEI
Certificate No: Customer ID No:	2452K947701 123502
At the time of calibration applicable Hewlett-Packar	a, this certifies that the above product was calibrated in accordance w
At planned intervals, Hew measurement against nat ratio type measurements	vlett-Packard measurement standards are calibrated by comparison to ional standards, natural physical constants, consensus standards, or using self-calibrating techniques.
National Standards are ad other recognized national	lministered by NIST (National Institute of Standards and Technology standards laboratories.
Initial testing found your ensure performance to pu	instrument was IN-SPECIFICATION. No adjustment was necessary blished operating specifications where tested.
Supporting documentatio request.	n relative to traceability is on file and is available for examination u
The calibration interval fo is 14-Aug-1999.	or this unit is 12 months and the calibration due date based on this inter
Temperature: 21.6 °C	Relative Humidity: 4
Remarks or special requir	rements:
STE 9000 TEST PROGR	AM HP35670A/REV.A.00.03.
Calibration Date: 14-Aug	-1998 Dave McCarthy, Calify Mana

,

	C	ertificate Of Calil	oration	FS 2324
Model No: Serial No: Descriptio Customer Agreemen Certificate Customer	n: Name: P.O. No: t No: No: ID No:	35670A 3431A01613 DYNAMIC SIGNAL ANALYZER NATIONAL RENEWABLE ENEI VISA/ARLINDA HUSKEY 2452K947701 123502	RGY LABORA	TORY
Calibration Model	n Equipme Model D	ent Used:	Trace Number	Cal Due Date
FLU5700A 3325A 3325B 3458A	AC DC C. SYNTHE: SYNTHE: SYSTEM	ALIBRATOR SIZER/FUNCTION GENERATOR SIZER/FUNCTION GENERATOR MULTIMETER	5700A15016 3325A01121 3325B01972 3458A01113	05-Mar-1999 01-Apr-1999 27-Sep-1998 25-Sep-1998

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FOR BR	ÜFL&K.IÆR	
Sound Level	Calibrator Type 4230	
The Sound Pressure Level has been	The calibrator type 4230	
measured by comparison with Standard	ID #: 00787C	
Reference Pistonphone.	Serial number 861619	
Type: 4220 serial number 1510240	has been found to be within the spec	ifications
and	listed below.	
Type: 4220 serial number 1048795	Sound Programs I and produced in th	
Calibrated by: SN (BRÜEL & KJÆR)	terminated by a loading volume of 1.	.333 cm ³ :
Date of Calibration: 18 AUG 1997	94.0	± 0.3 dB
Re-calibration Due: 18 AUG 1998	Frequency: 100	0 <u>+</u> 15 Hz
UNCERTAINTY OF MEASUREMENT:	Equivalent Coupler Volume: V > 14	% 0 cm3
A: Estimated Uncertainty of comparison:+/-0.09dB	Equivalent Couplet Volume. V > 14	о сш-
at 99% Confidence Level B: Estimated Uncertainty of Ref. 4220: +/-0 10 dB	ENVIRONMENTAL CONDITION	NS:
at 99% Confidence Level	Ambient Pressure 986.93	hPa
C: Total Uncertainty 0.13 dB (calculated as the	Temperature 239	РС
square root of the summed squares of A and B)	Relative Humidity 38	%
at 99% Confidence Level	Re-calibration due on 22 APR 19 Calibration procedure: Brilel & Kier 4230 Rev. 181	998 999 Nov 1997
	Certificate No.: 6922-7 PO# Verbal - A. Huskey For: National Renewable Energy Lab, Golden, CC	y) 80403
	Frequency 997.4 Hz	
	SPL 93.89 dB Volume Check -0.04 dB	
	Distortion 0.55 % Battery Voltage 8.8 VOLT	
	Was frequency and SPL adjusted for improvement? Was battery replaced with new alkaline type?	Yes-SPL! Yes!
	FINAL PERFORMANCE:	
	Frequency 997.4 Hz SPL 93.98 dB	
	Volume Check -0.02 dB Distortion 0.65 %	
	Note: This calibrator was within Mfg specifications	as received.
	ODIN METROLOGY. Inc.	
Performed on a test system which operates in compliance with ANSI/NCSI 7540-1	A BRÜEL & KJÆR, DIV.OF SPECTRIS TECHNOLOGY, AUTHORIZED CALIDDATION CENTED	. INC.,
Reference standards 4220 No.; 1510240 and 4228	3533 OLD CONEJO ROAD, SUITE # 125	
with, NIST test no.822/258435-97. Signed:	1HOUSAND OAKS, CA 91520 PHONE: (805) 375-0830 FAX: (805) 375-0405	5
Torben Ehlert Quality Assumance Man		
LOI NEH EMITTI , Quanty Assurance Mgr.		Daga 1 of 7

Sony Precision Technology America, Inc.

137 West Bristol Lane, Orange, CA 92865 Telephone: (714) 921-0630 Fax: (714) 921-1162

stomer Name: National Renewable Energy Laborato	ry Date: August 25, 1998
Instrument Info	ormation
Model No. PC208Ax	Report No. 145401-1
Serial No. U3538	Cust. P.O. VISA Card
Asset No. 124037	Date Recvd. 08/18/98
Date Cal. 08/24/98	Accuracy: Mfr. Spece
Date Due: 08/24/99	Maint. Prco: 1341
Interval: 12	Temperature: 23
Description: Data Recorder	Humidity: 47

Condition Instrument Received / Returned

Condition Received: In Tolerance Remarks:

Condition Returned: In Tolerance Remarks: Calibrated

Standards Used

<u>ID #</u>	Manufacturer	Model No.	Accuracy	Description	Due Date
569	Hewlett Packard	3325A	Mfr. Specs	Sweep Generator	11/14/98
533	Keithley	2000	Mfr. Specs	6 1/2 Digit DMM	03/20/99
616	Fluke	5500A/SC	Mfr. Specs	Multi Calibrator	10/14/98
643	Bruel & Kiaer	2032	Mfr. Specs	FFT Signal Analyze	02/11/99
595	Hewlett Packard	8903B	Mfr. Specs	Audio Analyzer	06/17/99

Sony Precision Technology America, Inc. certifies that the instrument specified above meets the manufacture's specifications and has been calibrated using standards and instruments also listed above whose accuracy's are traceable to the National Institute of Standards and Technology (N.I.S.T.), and the calibration systems and records are in compliance to ISO-10012 and ANSI Z540-1. This document cannot be reproduced without prior approval.

Approved by: Shan of 25/98

SONY

Anemometer Calibration Sheet

Annemometer Calibration Report

Calibration Laboratory: National Wind Technology Center - Cert. Team National Renewable Energy Laboratory Customer: National Wind Technology Center - Certification Team National Renewable Energy Laboratory 1617 Cole Boulevard 1617 Cole Boulevard Golden, Colorado 80401 Golden, Colorado 80401 Dates of Calibration: Test Start: 1 Calibration Location: 1-Oct-98 National Wind Technology Center Side-by-Side Anemometer Calibration Facility Test End: 28-Oct-98 6-Nov-98 Report: Report Number: CR-anno-98-4-T3 Procedure: Page: 1 of 1 NWTC-CT: GI21-98237, Field Calibrate Anemometers Item Calibrated: Deviations from procedure; Manufacturer Met One Instruments, Inc None Model 010C Cup Serial Number T2346 Results: Cup Material Aluminum Slope: 0.0399 m/s/hertz Condition Refurbished 15 Sep 98 Offset: 0.3247 m/s Estimated Uncertainty: Traceability: Vwind Cres UncerTotal Uncert: Reference Cup: Met One, 010C, s/n: U2645 4 - 5 m/s 0.083 0.096 Calibrated by: CRES, Pikermi, Greece 5 - 10 m/s 0.067 0.083 Calibration date: 11-Mar-98 10 - 15 m/s 0.078 0.092 <u>6Nov98</u> Date Approved Hal Link 0.8 20 18 0.6 (m/s) 16 0.4 14 (m/s) 0.2 Wind Speed 12 uals 10 0.0 Residu 8 -0.2 6 Ref. -0.4 4 -0.6 2 0 -0.8 400 0 100 200 300 500 Signal Frequency (hz)

Wind Vane Calibration Sheet

		INSI KU DEDA ID	MENT		
			LADS		
	Gertif	icate of	^c Galil	bration	
	COI CEF CALIBRATIC	MPANY NAME: TIFICATION #:	National 98102319 IRL Depo	Renewable Energ 2 t	y Lab
	MANUFACTURER	MODEL N		P.O. NUMBER	
	SERIAL NUMBER U1475	CALIBRATI 178	ON ID # 1.5	CUSTOMER ID #	
L				· · · · · · · · · · · · · · · · · · ·	
	RECEIVED E v	/ithin Tolerance Out Of Tolerance	Oper Oper Phys	rational Failure ical Damage	
	RETURNED	Vithin Tolerance	🗌 Limit	ed	
		2ther	11/03/9	9	
	STANDARD(S) Used MD1 FL8				
			MFGR Cal	Procedure	
ł					
	meets or exceeds all r	nanufacturer's or	agreed upon	ocal specifications. The	
	N.I.S.T. within the limit	ation of their cali	bration service	s, or have been derived	
	from accepted values Requirements″ satisfy /	of natural physic NSI/NCSL Z540,	al constants. C MIL-STD-456	Dur "Calibration System 62A, FDA GMP 820.61	
	and ISO Guide 25. The unless otherwise noted	calibration envir . This report is	onment was 70 not to be repr	<pre>0°F ½ 5°F and <70% RH roduced, except in full,</pre>	
	without the written app	roval of Instrumen	t Repair Labs ['] (Quality Manager.	
			RV.	Mark Shann	
TÜV	C	ATE CALIBRAT	ED:	11/03/98	
	\QL	ALITY MANAC	ER:	BILL HEDRICK	
ISO 9002					
	2100	W. 6th Ave. • Br	oomfield, CO	80020	



Report of Calibration

INSTRUMENT REPAIR LABS						
Report of Calibration						
Customer <u>NREL</u>	Manufacture	<u> MET の NE</u> Calibration # 9 <u>8/0 3/9 2</u>				
Model #のスのこ	Serial # <u>14</u> _	75 / /78/5 Tech 18				
Date <u>// - 3 - 98</u>	Due <u>//-3-99</u>	Ambient°F % RH				
	🕿 As Received	🙇 As Returned				
READINGS						
SVDC OUTPUT	READING	2. 5VDC OUTPOT READING				
MARK ALIGNED	2.5069	1,2542				
CW 900	3,7527	1,9012				
CW 180°	4,9995	2,5026				
CW 270°	1,2539	6.6025				
C W 360°	2.5023	1,2515				
MARK ALIGNED	2,5005	1.2495				
CCW 270°	1,2540	16072				
CCW 180°	5,0039	2.5010				
CCW 90°	3,7573	1,8999				
ccw o°	2.5009	1,2495				
TOLERAN	$c = \tau/-3$	0				
SV OUTPU	$T = \frac{+}{-}, 0$	421				
2. SV OUTPU	r = t/-, 0	$z_{I}V$				

SVDC OUTPUT	READING	2. SYDC OUTPOT READING
MARK ALIGNED	2.5069	1,2542
CW 900	3,7527	1,9012
CW 180°	4,9995	2.5026
CW 270°	1,2539	6.6025
C W 360°	2.5023	1,2515
MARK ALIGNED	2,5005	1.2495
CCW 270°	1,2540	16072
CCW 180°	5,0039	2.5010
CCW 900	3.7573	1,8999
cciv o°	2.5009	1. 2495
TOLERANC	E = T/-3	0

TOLERANCE	=	$T/-3^{\circ}$
SV OUTPUT	ž	+1- ,042V
2. SV OUTPUT	5	+/- ,021V

2100 W. 6th Ave. • Broomfield, CO 80020 (303) 469-5375 or (800) 345-6140 FAX (303) 469-5378

2 - 62 page

Pressure Sensor Calibration Sheet

	INSTRUMENT	
	REPAIR LABS	
	Contificate of Calibuation	
	Certy icute of Cattoria	
	COMPANY NAME: National Renewable Energy CERTIFICATION #: 980911237 IRL Depot	Lab
	MANUFACTURER MODEL NUMBER P.O. NUMBER	
	SERIAL NUMBER CALIBRATION ID # CUSTOMER ID # 046/21 17304	
	RECEIVED Out Of Tolerance Deperational Failure Out Of Tolerance Physical Damage	
	T Within Tolerance Limited	
	□ Other	
	CALIBRATION Due	
	STANDARD(S) Used	
	CALIBRATION PROCEDURE USED	
	Instrument Repair Labs, Inc. does hereby certify that the above listed instrument meets or exceeds all manufacturer's or agreed upon local specifications. The instrument has been calibrated using standards whose accuracies are traceable to N.I.S.T. within the limitation of their calibration services, or have been derived from accepted values of natural physical constants. Our "Calibration System Requirements" satisfy ANSI/NCSL Z540, MIL-STD-45662A, FDA GMP 820.61 and ISO Guide 25. The calibration environment was 70°F ½ 5°F and <70% RH unless otherwise noted. This report is not to be reproduced, except in full, without the written approval of Instrument Repair Labs' Quality Manager.	
	CERTIFIED BY: Ronald Horton	
	DATE CALIBRATED: 09/14/98	
	QUALITY MANAGER: BILL HEDRICK	
ISU YUU2 INSTRUMENT REPAIR LABS	2100 W. 6th Ave. • Broomfield, CO 80020 (303) 469-5375 or (800) 345-6140 FAX (303) 469-5378	



Temperature Sensor Calibration Sheet

			2
	DEDATE I	<u>LN</u> I A DC	
		INC.	
Gertif.	icate of C	Salib	ration
COI		tional	Renewable Energy L
CEF CALIBRATIC	TIFICATION #: 98 N LOCATION: IR	L Depot	3
MANUFACTURER	MODEL NUMB	ER	P.O. NUMBER
SERIAL NUMBER	CALIBRATION II)#	CUSTOMER ID #
		1	·····
RECEIVED 🗵 V	/ithin Tolerance Out Of Tolerance	Opera Opera Physic	ational Failure cal Damage
	/ithin Tolerance	🗌 Limite	ed
	Other		
CALIBRATION D	0ue 0	9/14/99	9
STANDARD(S) U	sedF	L11, HS	31
CALIBRATION PROCE	DURE USEDMF	GR Cal	Procedure
Instrument Repair Labs, meets or exceeds all r instrument has been cal N.I.S.T. within the limit from accepted values Requirements" satisfy A and ISO Guide 25, The unless otherwise notec without the written app	Inc. does hereby certi nanufacturer's or agree ibrated using standards ation of their calibratio of natural physical co NNSI/NCSL Z540, MIL e calibration environme I. This report is not t roval of Instrument Rep	fy that the ed upon 1d whose acc on services instants. O -STD-4566 ent was 70 o be repro air Labs' Q	above listed instrument ocal specifications. The curacies are traceable to , or have been derived ur "Calibration System 2A, FDA GMP 820.61 °F ½ 5°F and <70% RH oduced, except in full, Quality Manager.
	CERTIFIED BY:	Ror	ald Horton
	ATE CALIBRATED:		09/14/98
	ALITY MANAGER:		BILL HEDRICK
NSTRUMENT REPAIR LASS 2 2100	W. 6th Ave. • Broom	field, CO	80020

	INSTRUME REPAIR LA	n to the second	
	Report of C	alibration	
Customer <u>NREL</u>	Manufacturer	OMEGA	Calibration # <u>9809112</u>
Model # <u>869</u>	Serial # <u>7-17111</u>	1 / 17305IRL	Tech
Date <u>7-14-98</u>	Due <u>9-14-99</u>	Ambient//	<u>A-</u> ºF <u>N/A</u> %₿
Q	As Received	C As Returned	3
	READI	NGS	
	Actual (ST) READ	רעעד)
SIMULATED TEST	100.00R = 0.0	°C 0.0)°C
·	174.00 N = 195.0)°C[95,0)°C
	313,591 = 600,	D°C 600.0	?°С
	ACTUAL (STD)	READ	(UVT)
PROBE COMP. TEST	25.0°C	25,0	°C
	·· ·		
		·····-	
(202)	2100 W. 6th Ave. • Brod	omfield, CO 80020	70
(303)	45-5373 Ur (000) 345-6	170 FAA (303) 409-33	/0

Campbell Datalogger Calibration Sheet

CSI DATALOGGER MODEL: CR23X Item #10517 FINAL DATALOGGER TEST REPORT AND CALIBRATION CERTIFICATION

Serial # **1214** Test Panel Position 12

TEST	ANALOG INPUTS	PASS/F	AIL IN	PUT M	EASU	RED	*	TEST
#				<u>v</u> .	mv.		ERROR	TEMP
1	Diff. Range 5 (+-0.05%)	FSR) P		5 4	996.9)	.03	-25 C
2		-		5	5000.7	/	.01	+50 C
3	Channel Multiplexing	P						
4	Panel Temperature	P						
5	Battery Voltage	Р						
	ANALOG OUTPUTS	_		_				
6 7	Switched (+-0.05% FSR)	Р		5	999.9	1 Э	.02	-25 C +50 C
8	Continuous (+-0.05% FSR)) P		5	001.2	2	.01	-25 C
9		, -		4	999.6	5	.00	+50 C
10	Excit. Multiplexing	P		•		-		
11	CAO Channels	P						
12	PULSE COUNTERS	P						
13	DIGITAL CONTROL OUT	Р						
	CPU AND INTERFACE							<u> </u>
14	Memory	Р						
15	Serial I/O	Р						
16	Clock	Р						
	SYSTEM POWER			MEASU	RED			
17	Outorcont (2, 2m) turn)	в		1 010)			
10	Monguromont (loaded)	r D		97 0) m2			
10	(70 m) turn 150 m) londor			0/.5	, mer			
	(70 MA Cyp., 150 MA 10ade							
	TEMPERATURE RANGE		INPUT	MEAS	URED	*	T	EST
			v.	V	7.	ERRO	R TI	EMP.
19	Diff Range 5 Cold (Derat	ted)	5					
20	Diff Range 5 Hot (Dera	ted)	5					
NOTE:	The collective measurement	nt unce	rtaintv	of th	le cal	libra	tion	
	process exceeds a 4:1 ac	curácy	ratio.					
TEST :	STANDARDS USED:							
	Test Procedure TST10517C	Rev.9						
1	Environmental Chamber:							
	DC Calibrator S/N A02120	5	(Trace	able t	O NIS	ST 239	96111)
	Oscillatek S/N 205345	фсхо	(Trace	able t	O NIS	ST 014	41/WW	VB)
inal <i>(</i>	Report Validation By							
Α	Tili				10/10	6/98		

A. PARKINSON