

Appendix 6
HISTORIC DATA

+ Flood information outside that in the systematic record can often be used to extend the record of the largest events to a historic period much longer than that of the systematic record. In such a situation, the following analytical techniques are used to compute a historically adjusted log-Pearson Type III frequency curve. +

1. Historic knowledge is used to define the historically longer period of "H" years. The number "Z" of events that are known to be the largest in the historically longer period "H" are given a weight of 1.0. The remaining "N" events from the systematic record are given a weight of $(H-Z)/(N+L)$ on the assumption that their distribution is representative of the (H-Z) remaining years of the historically longer period. *

2. The computations can be done directly by applying the weights to each individual year's data using equations 6-1, 6-2a, 6-3a, and 6-4a. Figure 6-1 is an example of this procedure in which there are 44 years of systematic record and the 1897, 1919 and 1927 floods are known to be the three largest floods in the 77 year period 1897 to 1973. If statistics have been previously computed for the current continuous record, they can be adjusted to give the equivalent historically adjusted values using equations 6-1, 6-2b, 6-3b, and 6-4b, as illustrated in Figure 6-2. +

+ 3. The historically adjusted frequency curve is sketched on logarithmic-probability paper through points established by use of equation 6-5. The individual flood events should also be plotted for comparison. The historically adjusted plotting positions for the individual flood events are computed by use of equation 6-8, in which the historically adjusted order number of each event "m" is computed from equations 6-6 and 6-7. The computations are illustrated in Figures 6-1 and 6-2, and the completed plotting is shown in Figure 6-3. *

+ 4. The following example illustrates the steps in application of the historic peak adjustment only. It does not include the final step of weighting with the generalized skew. The historically adjusted skew developed by this procedure is appropriate to use in developing a generalized skew. +

DEFINITION OF SYMBOLS

- E = event number when events are ranked in order from greatest magnitude to smallest magnitude. The event numbers "E" will range from 1 to (Z + N).
- + X = logarithmic magnitude of systematic peaks excluding zero flood events, peaks below base, high or low outliers
- X_z = logarithmic magnitude of a historic peak including a high outlier that has historic information
- N = number of X's +
- + M = mean of X's
- \tilde{M} = historically adjusted mean
- \tilde{m} = historically adjusted order number of each event for use in formulas to compute the plotting position on probability paper +
- S = standard deviation of the X's
- \tilde{S} = historically adjusted standard deviation +
- G = skew coefficient of the X's
- + \tilde{G} = historically adjusted skew coefficient +
- K = Pearson Type III coordinate expressed in number of standard deviations from the mean for a specified recurrence interval or percent chance
- Q = computed flood flow for a selected recurrence interval or percent chance
- \tilde{P} = plotting position in percent
- * \tilde{P} = probability that any peak will exceed the truncation level (used in step 1, Appendix 5) *
- + Z = number of historic peaks including high outliers that have historic information +
- * H = number of years in historic period *
- + L = number of low values to be excluded, such as: number of zeros, number of incomplete record years (below measurable base), and low outliers which have been identified +
- * a = constant that is characteristic of a given plotting position formula. For Weibull formula, a = 0; for Beard formula, a = 0.3; and for Hazen formula, a = 0.5 *
- * W = systematic record weight *

EQUATIONS

$$+ W = \frac{H - Z}{N + L} \quad (6-1)$$

$$\tilde{M} = \frac{W \sum X + \sum X_z}{H - WL} \quad (6-2a)$$

$$\tilde{S}^2 = \frac{W \sum (X - \tilde{M})^2 + \sum (X_z - \tilde{M})^2}{(H - WL - 1)} \quad (6-3a)$$

$$\tilde{G} = \frac{H - WL}{(H - WL - 1)(H - WL - 2)} \left[\frac{W \sum (X - \tilde{M})^3 + \sum (X_z - \tilde{M})^3}{\tilde{S}^3} \right] \quad (6-4a)$$

$$\tilde{M} = \frac{WNM + \sum X_z}{H - WL} \quad (6-2b)$$

$$\tilde{S}^2 = \frac{W(N - 1)S^2 + WN(M - \tilde{M})^2 + \sum (X_z - \tilde{M})^2}{(H - WL - 1)} \quad (6-3b)$$

$$\tilde{G} = \frac{H - WL}{(H - WL - 1)(H - WL - 2)\tilde{S}^3} \left[\frac{W(N - 1)(N - 2)S^3 \tilde{G} + 3W(N - 1)(M - \tilde{M})S^2}{N} + WN(M - \tilde{M})^3 + \sum (X_z - \tilde{M})^3 \right] \quad (6-4b) +$$

$$* \text{Log } Q = \tilde{M} + K\tilde{S} \quad (6-5)$$

$$\tilde{m} = E; \text{ when: } 1 \leq E \leq Z \quad (6-6) *$$

$$+ \tilde{m} = WE - (W - 1)(Z + 0.5); \text{ when: } (Z + 1) \leq E \leq (Z + N + L) \quad (6-7) +$$

$$P\tilde{P} = \frac{\tilde{m} - a}{H + 1 - 2a} 100 \quad (6-8)$$

Figure 6-1. HISTORICALLY WEIGHTED LOG PEARSON TYPE III - ANNUAL PEAKS

Station: 3-6065, Big Sandy River at Bruceton, TN. D. A. 205 square miles
 Record: 1897, 1919, 1927, 1930-1973 (47 years)
 Historical period: 1897-1973 (77 years)
 N = 44; Z = 3; W = 77

Year	Q (ft ³ / s) = Y	Log Y = X	Deviation from mean log x = (X-M)	Weight = W	Event Number = E	Weighted order Number = m	Plotting position (Weibull) P _P
1897	25,000	4.39794	0.68212	1.00	1	1.00	1.28
1919	21,000	4.32222	0.60640	1.00	2	2.00	2.56
1927	18,500	4.26717	0.55136	1.00	3	3.00	3.85
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1935	17,000	4.23045	0.51464	1.68182	4	4.34	5.56
1937	13,800	4.13988	0.42407	1.68182	5	6.02	7.72
1946	12,000	4.07918	0.36337		6	7.71	9.88
1972	12,000	4.07918	0.36337		7	9.39	12.04
1956	11,800	4.07188	0.35607		8	11.07	14.19
1942	10,100	4.00432	0.28851		9	12.75	16.35
1950	9,880	3.99475	0.27895		10	14.43	18.50
1930	9,100	3.95904	0.24323		11	16.12	20.67
1967	9,060	3.95713	0.24132		12	17.80	22.82
1932	7,820	3.89321	0.17740		13	19.48	24.97
1973	7,640	3.88309	0.16728		14	21.16	27.13
1962	7,480	3.87390	0.15809		15	22.84	29.28
1965	7,180	3.85612	0.14031		16	24.53	31.45
1936	6,740	3.82866	0.11285		17	26.21	33.60
1948	6,130	3.78746	0.07165		18	27.89	35.76
1939	5,940	3.77379	0.05798		19	29.57	37.91
1945	5,630	3.75051	0.03470		20	31.25	40.06
1934	5,580	3.74663	0.03082		21	32.94	42.23
1955	5,480	3.73878	0.02297		22	34.62	44.38
1944	5,340	3.72754	0.01173	23	36.30	46.54	
1951	5,230	3.71850	0.00269	24	37.98	48.69	
1957	5,150	3.71181	-0.00400	25	39.66	50.85	
1971	5,080	3.70586	-0.00995	26	41.35	53.01	
1953	5,000	3.69897	-0.01684	27	43.03	55.17	
1949	4,740	3.67578	-0.04003	28	44.71	57.32	
1970	4,330	3.63649	-0.07932	29	46.39	59.47	
1938	4,270	3.63043	-0.08538	30	48.07	61.62	
1952	4,260	3.62941	-0.08640	31	49.76	63.79	
1947	3,980	3.59988	-0.11593	32	51.44	65.95	
1943	3,780	3.57749	-0.13832	33	53.12	68.10	
1961	3,770	3.57634	-0.13947	34	54.80	70.25	
1958	3,350	3.52504	-0.19077	35	56.49	72.42	
1954	3,320	3.52114	-0.19467	36	58.17	74.58	
1933	3,220	3.50786	-0.20795	37	59.85	76.73	
1964	3,100	3.49136	-0.22445	38	61.53	78.88	
1968	3,080	3.48855	-0.22725	39	63.21	81.04	
1969	2,800	3.44716	-0.26865	40	64.90	83.21	
1963	2,740	3.43775	-0.27806	41	66.58	85.36	
1959	2,400	3.38021	-0.33560	42	68.26	87.51	
1931	2,060	3.31387	-0.40194	43	69.94	89.67	
1966	1,920	3.28330	-0.43251	44	71.62	91.82	
1940	1,680	3.22531	-0.49050	45	73.31	93.99	
1960	1,460	3.16435	-0.55146	46	74.99	96.14	
1941	1,200	3.07918	-0.63663	1.68182	47	76.67	98.29



Figure 6-1. HISTORICALLY WEIGHTED LOG PEARSON-TYPE III - ANNUAL PEAKS (Continued)

Solving (Eq. 6-2a)

$$\begin{aligned} \Sigma X &= 162.40155 \\ W \Sigma X &= 273.13018 \\ \Sigma X_z &= \frac{12.98733}{286.11751} \end{aligned}$$

$$\bar{M} = 286.11751/77 = \underline{\underline{3.71581}}$$

Solving (Eq. 6-3a)

$$\begin{aligned} \Sigma x^2 &= 3.09755 \\ W \Sigma x^2 &= 5.20952 \\ \Sigma x_z^2 &= \frac{1.13705}{6.34657} \end{aligned}$$

$$\bar{S}^2 = 6.34657/(77 - 1) = 0.08351$$

$$\bar{S} = \underline{\underline{0.28898}} \quad \bar{S}^3 = 0.02413$$

Solving (Eq. 6-4a)

$$\begin{aligned} \Sigma x^3 &= -0.37648 \\ W \Sigma x^3 &= -0.63317 \\ \Sigma x_z^3 &= \frac{0.70802}{0.07485} \end{aligned}$$

$$\bar{G} = \frac{(77) (0.07485)}{(76) (75) (0.02413)} = \underline{\underline{0.0418}}$$

Solving (Eq. 6, Page 13)

$$N = 77$$

$$A = -0.33 + 0.08 (0.0418) = -0.32666$$

$$B = 0.94 - 0.26 (0.0418) = 0.92913$$

$$MSE_G = 10[-0.32666 - 0.92913[0.88649]] = 10[-1.150325] = 0.07074$$

Solving (Eq. 9.5, Page 12)

$$G_w = \frac{0.302(0.0418) + 0.07074(-0.2)}{.302 + 0.07074} = -0.00409$$

Solving (Eq. 6-5)

%	K $G_w = -0.00409$	(S) (K) $\bar{S} = .28898$	$\bar{M} + (\bar{S}) (K) = \text{Log } Q$ $\bar{M} = 3.71581$	Q (ft ³ /s)
99	-2.32934	-0.67313	3.04269	1,103
95	-1.64599	-0.47566	3.24014	1,738
90	-1.28196	-0.37046	3.34535	2,215
80	-0.84141	-0.24315	3.47266	2,969
50	0.00067	0.00019	3.71600	5,200
20	0.84180	0.24326	3.95907	9,100
10	1.28110	0.37021	4.08602	12,190
4	1.74929	0.50551	4.22132	16,646
2	2.05159	0.59289	4.30868	20,355
1	2.32340	0.67142	4.38723	24,391
.1	3.08455	0.89138	4.60719	40,475
.01	3.71054	1.07227	4.78808	61,387

Solving (Eq. 6-6)

$$\begin{aligned} Z &= 3 \\ \text{For } E &= 1; \bar{m} = E = 1 \\ \text{For } E &= 2; \bar{m} = E = 2 \\ \text{For } E &= 3; \bar{m} = E = 3 \end{aligned}$$

Solving (Eq. 6-8)

$$\text{For Weibull: } a = 0. \bar{P}P = (100) (\bar{m})/(78)$$

Solving (Eq. 6-7)

$$\begin{aligned} (Z + 1) &= 4 \\ (Z + N) &= 47 \\ \text{For } 4 \leq E \leq 47: \\ \bar{m} &= (1.682) (E) - (0.682) (3.5) \\ \bar{m} &= (1.682) (E) - 2.387 \end{aligned}$$



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Figure 6-2. HISTORICALLY WEIGHTED LOG-PEARSON TYPE III - ANNUAL PEAKS

Results of Standard Computation for the Current Continuous Record

Big Sandy River at Bruceton, TN. DA - 205 square miles
 #3-6065 (44 years)

N = number of observations used = 44

M = mean of logarithms = 3.69094

S = standard deviation of logarithms = 0.26721

S² = 0.07140 S³ = 0.01908

G = coefficient of skewness (logs) = -0.18746

Adjustment to Historically Weighted 77 Years

Historic Peaks (Z = 3 Years)					
Year	Y _Z (ft ³ /s)	Log Y _Z = X _Z	X _Z - \tilde{M}	(X _Z - \tilde{M}) ²	(X _Z - \tilde{M}) ³
1897	25,000	4.39794	0.68213	0.46531	0.31740
1919	21,000	4.32222	0.60641	0.36774	0.22300
1927	18,500	4.26717	0.55136	0.30400	0.16762
Summation		12.98733	1.83990	1.13705	0.70802

N = 44 Z = 3 H = 77

Solving (Eq. 6-1): W = (77-3)/44 = 1.68182

Solving (Eq. 6-2b): $\tilde{M} = \frac{(1.68182)(44)(3.69094) + (12.98733)}{77} = 3.71581$

Solving (Eq. 6-3b):

(M - \tilde{M}) = -0.02487; (M - \tilde{M})² = 0.000619; (M - \tilde{M})³ = -0.0000154

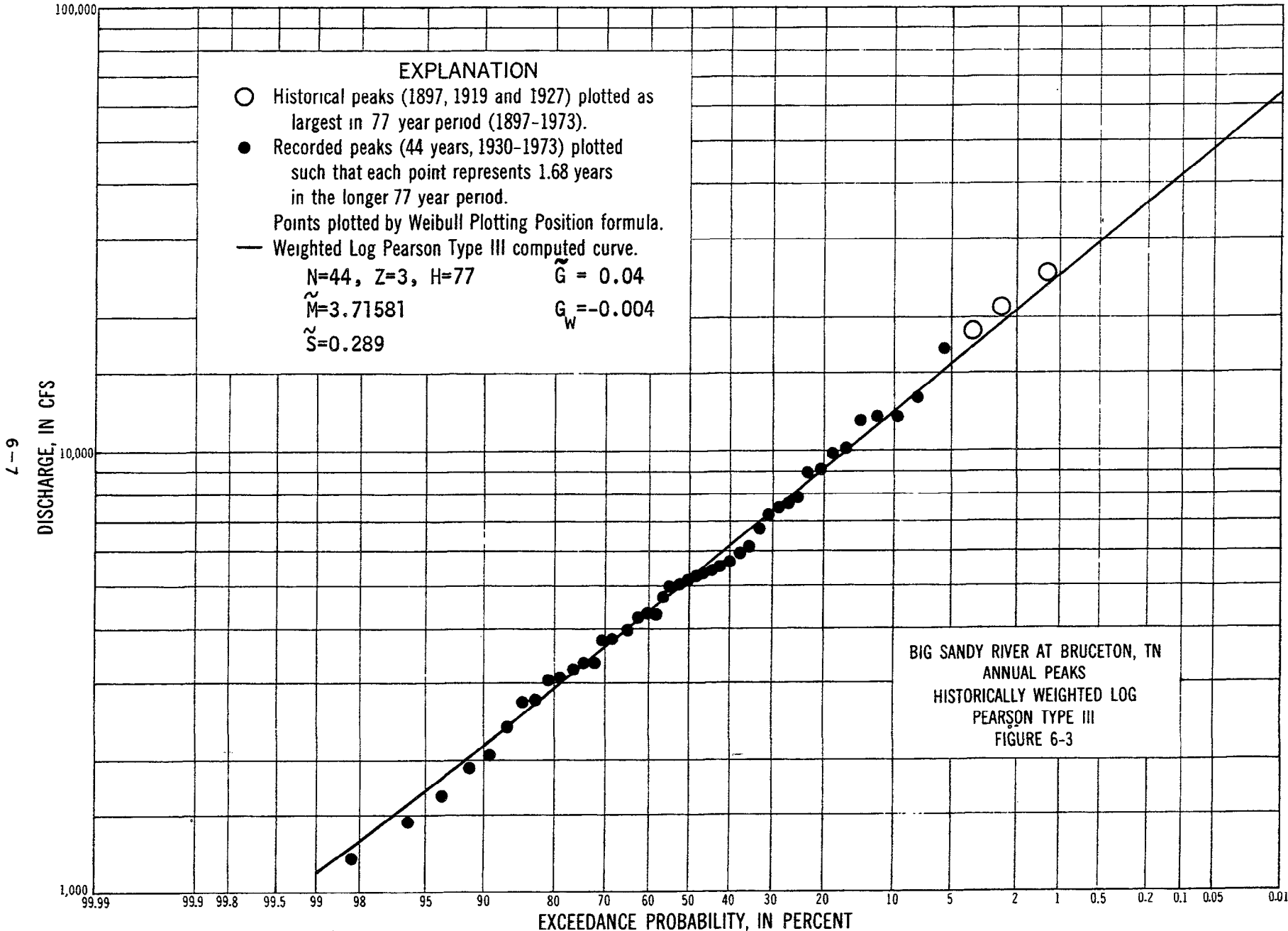
$\tilde{S}^2 = \frac{(1.68182)(43)(0.07140) + (1.68182)(44)(0.000619) + (1.13705)}{76} = 0.08351$

$\tilde{S}^2 = 0.08351$ $\tilde{S} = 0.28898$ $\tilde{S}^3 = 0.02413$

Solving (Eq. 6-4b):

$\tilde{G} = \frac{77}{(76)(75)(0.02413)} \left[\frac{(1.68182)(43)(42)(0.01908)(-0.18746)}{44} + (3)(1.68182)(43)(-0.02487)(0.07140) + (1.68182)(44)(-0.0000154) + (0.70802) \right]$
 $\tilde{G} = 0.0418$

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L-9

DISCHARGE, IN CFS

EXCEEDANCE PROBABILITY, IN PERCENT