

# Application of Kronecker products in Fusion Applications \*

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## 1 Introduction

We describe the application of Kronecker product formulation in speeding up key calculations in fusion codes used in the modeling of wave-plasma interaction within the Department of Energy SciDAC (Scientific Discovery through Advanced Computing)<sup>1</sup> program. By taking advantage of the compact representation and efficient matrix-matrix calculations, the Kronecker product formulation leads to an order of magnitude speedup in the matrix assembly in RANT3D (Three Dimensional Recesses Antenna Model) code [1]. Interpolation computed as Kronecker products leads to significant speedup in the ‘WDOT’ power calculation in AORSA2D (All-Orders Spectral Algorithm in Two Dimensions) [4, 5].

## 2 Kronecker Product

Kronecker product (also known as outer product or tensor product) has been successfully used as a framework for understanding different variants of the Fast Fourier Transform [7]. Van Loan [8, 9] has described various interesting properties of Kronecker products and their applications. We shall only briefly review the properties of Kronecker product of matrices.

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<sup>1</sup>For details see [www.osti.gov/scidac](http://www.osti.gov/scidac).

Let matrix  $A$  be  $m_A \times n_A$  and  $B$  be  $m_B \times n_B$ . For convenience, let them be indexed as  $A(ia, ja)$  and  $B(ib, jb)$ . Let  $C = A \otimes B$  (or `kron(A, B)` in MATLAB notation), then matrix  $C$  is size  $(m_A * m_B) \times (n_A * n_B)$ . If matrix  $A$  is  $3 \times 3$ , then

$$C = \begin{bmatrix} a_{11}B & a_{12}B & a_{13}B \\ a_{21}B & a_{22}B & a_{23}B \\ a_{31}B & a_{32}B & a_{33}B \end{bmatrix}$$

Matrix  $C$  can be interpreted as a 4-index array  $C([ib, ia], [jb, ja]) = A(ia, ja) * B(ib, jb)$ , where the composite index  $[ib, ia] = ib + (ia - 1) * m_B$  is the index in Fortran column-wise order. Matrix-vector multiply can be written as very efficient matrix-matrix operations<sup>2</sup>,

$$\begin{aligned} Y([ib, ia]) &= C([ib, ia], [jb, ja]) * X([jb, ja]) \\ &= A(ia, ja) * B(ib, jb) * X([jb, ja]) \\ &= B(ib, jb) * X(jb, ja) * A(ia, ja) \\ Y &= B * X * A^t \end{aligned}$$

Other interesting properties of Kronecker products are summarized below,

$$(A \otimes B) * (E \otimes F) = (A * E) \otimes (B * F) \tag{1}$$

$$(A + B) \otimes E = A \otimes E + B \otimes E \tag{2}$$

$$(A \otimes B) \otimes E = A \otimes (B \otimes E) \tag{3}$$

$$(A \otimes B)^{-1} = (A^{-1} \otimes B^{-1}) \tag{4}$$

$$(A \otimes B)^t = (A^t \otimes B^t) \tag{5}$$

### 3 Interpolation

Kronecker products also arise from interpolation of tabulated function values. Let a matrix  $F = (F_{ij})$  represent tabulated function values for  $F_{ij} = F(x_i, y_j)$ . The function  $F(x, y)$  can be approximated as  $F(x, y) = \sum_{k,\ell} C_{k\ell} \phi_k(x) \phi_\ell(y)$ , where the basis functions  $\phi_k(x)$  may be chosen for example to be B-splines or  $(k - 1)^{th}$  degree Chebyshev polynomials. The coefficients  $C_{k\ell}$  can be computed to satisfy the interpolation conditions

$$F_{ij} = \sum_{k,\ell} C_{k\ell} \phi_k(x_i) \phi_\ell(y_j) \tag{6}$$

The interpolation conditions can be expressed as a Kronecker product,  $F = (T_y \otimes T_x) * C$ , where

$$T_x = \begin{pmatrix} \phi_1(x_1) & \cdots & \phi_n(x_1) \\ \vdots & \ddots & \vdots \\ \phi_1(x_n) & \cdots & \phi_n(x_n) \end{pmatrix}, \quad T_y = \begin{pmatrix} \phi_1(y_1) & \cdots & \phi_n(y_1) \\ \vdots & \ddots & \vdots \\ \phi_1(y_n) & \cdots & \phi_n(y_n) \end{pmatrix}. \tag{7}$$

<sup>2</sup>We blur the distinction between the matrix  $X(jb, ja)$  and vector  $X([jb, ja])$  with composite index.

The columns of  $T_x$  and  $T_y$  contain the values of the basis functions evaluated as the interpolation knots. The coefficients  $C_{k\ell}$  can be efficiently computed using the property of Kronecker products as

$$C = (T_y \otimes T_x)^{-1} * F = (T_y^{-1} \otimes T_x^{-1}) * F = T_x^{-1} * F * T_y^{-t} \quad (8)$$

Once the coefficients are known, extrapolation at the set of new values  $F(\tilde{x}_m, \tilde{y}_n) = (\tilde{F}_{mn})$  can be computed as Kronecker products,

$$\begin{aligned} \tilde{F} &= T_{\tilde{x}} * C * T_{\tilde{y}}^t = T_{\tilde{x}} * (T_x^{-1} * F * T_y^{-t}) * T_{\tilde{y}}^t, \quad \text{from (8)} \\ \tilde{F} &= (T_{\tilde{x}} * T_x^{-1}) * F * (T_{\tilde{y}} * T_y^{-1})^t \end{aligned} \quad (9)$$

where

$$T_{\tilde{y}} = \begin{pmatrix} \phi_1(\tilde{y}_1) & \cdots & \phi_n(\tilde{y}_1) \\ \vdots & \ddots & \vdots \\ \phi_1(\tilde{y}_n) & \cdots & \phi_n(\tilde{y}_n) \end{pmatrix}. \quad (10)$$

The above can be generalized to higher dimensions. For a 4-variable function indexed as  $F(w, x, y, z)$ , the corresponding interpolation scheme would be

$$F(w, x, y, z) = \sum_{i,j,k,\ell} C_{ijkl} \phi_i(w) \phi_j(x) \phi_k(y) \phi_\ell(z). \quad (11)$$

The interpolation conditions can be written as

$$F = ((T_z \otimes T_y) \otimes (T_x \otimes T_w)) * C \quad (12)$$

so that coefficients  $C_{ijkl}$  can be efficiently computed as

$$C = (T_x \otimes T_w)^{-1} * F * (T_z \otimes T_y)^{-t} \quad (13)$$

$$= (T_x^{-1} \otimes T_w^{-1}) * F * (T_z^{-t} \otimes T_y^{-t}). \quad (14)$$

## 4 RANT3D

The RANT3D [1, 2] antenna modeling code solves Maxwell's equations in two and three dimensions. The antenna geometry is specified in Cartesian coordinates through a series of rectangular recesses and current straps. The code is used in the design of radio-frequency (rf) antenna for heating and current drive in tokamaks. The Kronecker product algebra implemented as matrix-matrix multiply was used for calculating strap impedance matrices. This reduced the time for multiple strap antenna arrays by an order of magnitude.

RANT3D solves Maxwell's equation in vacuum with a generalized plasma boundary

$$\nabla \cdot (\nabla \cdot \mathbf{E}) - \left( \nabla^2 + \frac{\omega^2}{c^2} \right) \mathbf{E} = i\omega\mu_0 \mathbf{J}. \quad (15)$$

Each component of  $\mathbf{E}$  is represented in a variable separable manner by Fourier basis

$$E_c(x, y, z) = \sum_{m,n} E_c^{mn}(x)\eta_c^m(y)\eta_c^n(z), \quad J_c(x, y, z) = \sum_{m,n} J_c^{mn}\eta_c^m(y)\eta_c^n(z) \quad (16)$$

where subscript  $c = x, y, \text{ or } z$ , and the basis functions  $\eta_c^m$  are of the form sin, cos or exp.

The constraints that enforce continuity of tangential electric and magnetic fields lead to repeated evaluations of the form

$$Y(m, n) = \sum_{i,j} B(m, i)X(i, j)A(n, j), \quad \text{for each } m, n. \quad (17)$$

The above computation can be seen to be  $Y = (A \otimes B) * X$  can this form can be evaluated in  $O(2N^3)$  instead of  $O(N^4)$  work. On a model for NSTX (National Spherical Torus Experiment) with 37 recesses, the Kronecker product formulation reduced the time for impedance matrix assembly from about 682 sec to about 55 sec on a 1.3Ghz Power 4.

## 5 Power Calculations

The AORSA2D code [3, 4, 5] uses a spectral representation to model the response of plasma to radio frequency (rf) waves in a tokamak geometry by solving the inhomogeneous wave equation or Helmholtz equation,

$$-\nabla \times \nabla \times \mathbf{E} + \frac{\omega^2}{c^2} \left( \mathbf{E} + \frac{i}{\omega\epsilon_0} \mathbf{J}_p \right) = -i\omega\mu_0 \mathbf{J}_{ant}, \quad (18)$$

where  $\mathbf{E}$  is the wave electric field and  $\mathbf{J}_{ant}$  is a specified external antenna current. Most of the complication in (18) arises from the response of the plasma to the electromagnetic wave field, which is included through the plasma current,  $\mathbf{J}_p$ . The rf electric field  $\mathbf{E}$  and plasma current  $\mathbf{J}_p$  are expanded in Fourier harmonics of the radial dimension as

$$\mathbf{E}(x, y) = \sum_{n,m} \mathbf{E}_{nm} e^{i(k_n x + k_m y)} = \sum_{n,m} \mathbf{E}_{nm} e^{i\vec{k}_n \cdot \mathbf{r}}, \quad (19)$$

$$\mathbf{J}_p(x) = \sum_{n,m} \sigma(x, y, k_n, k_m) \cdot \mathbf{E}_{nm} e^{i(k_n x + k_m y)}. \quad (20)$$

The tensor  $\sigma(x, y, k_n, k_m)$  can be derived from the first-order rf distribution function given by Stix [6]. It depends on the Fourier mode  $k_n, k_m$  and is a complicated function of modified Bessel functions and plasma  $Z$  functions. AORSA2D uses the method of collocation and constructs a large dense complex linear system that is solved in parallel by ScaLAPACK. For example, with  $200 \times 200$  Fourier modes, it is necessary to solve 120,000 coupled complex equations, and the storage required for the resulting matrix is about 230 GBytes and require about 1.3 Tflops-hour of computation.

One costly computation is the calculation of the local energy absorption at every grid point in the plasma, after  $\mathbf{E}(x, y)$  is available,

$$\dot{W} = \frac{\partial W(\vec{k}_n, \vec{k}_m)}{\partial t} \quad (21)$$

$$= \frac{1}{2} \text{Re} \sum_{n,m} e^{i(\vec{k}_n - \vec{k}_m) \cdot \vec{r}} \sum_{\ell=-\infty}^{\infty} \mathbf{E}_m^* \cdot W_\ell \cdot \mathbf{E}_n \quad (22)$$

$$= \frac{1}{2} \text{Re} \sum_{n,m} e^{-i\vec{k}_m \cdot \vec{r}} \mathbf{E}_m^* \cdot \left( \sum_{\ell=-\infty}^{\infty} W_\ell \right) \cdot \mathbf{E}_n e^{i\vec{k}_n \cdot \vec{r}} \quad (23)$$

where  $W(x, y, \vec{k}_n, \vec{k}_m)$  involve costly evaluation of modified Bessel functions,

$$W_\ell = C * \begin{pmatrix} \frac{\ell^2 I_\ell}{\Gamma} Z_\ell & -i\ell \left( \frac{\Gamma_n}{\Gamma} I_\ell - I'_\ell \right) Z_\ell & -k_{\perp,n} \frac{\ell I_\ell}{\Gamma} \frac{\alpha Z'_\ell}{2\Omega} \\ i\ell \left( \frac{\Gamma_m}{\Gamma} I_\ell - I'_\ell \right) Z_\ell & \left[ \frac{\ell^2}{\Gamma} I_\ell + 2\tilde{\Gamma} I_\ell - 2\bar{\Gamma} I'_\ell \right] Z_\ell & -i(k_{\perp,m} I_\ell - k_{\perp,n} I'_\ell) \frac{\alpha Z'_\ell}{2\Omega} \\ -k_{\perp,m} \frac{\ell I_\ell}{\Gamma} \frac{\alpha Z'_\ell}{2\Omega} & i(k_{\perp,n} I_\ell - k_{\perp,m} I'_\ell) \frac{\alpha Z'_\ell}{2\Omega} & -\zeta_\ell I_\ell Z'_\ell \end{pmatrix},$$

$$I_\ell = I_\ell(\tilde{\Gamma}), \quad I'_\ell = I'_\ell(\tilde{\Gamma}), \quad C = -i\epsilon_0 \frac{\omega_p^2}{k_{\perp}\alpha} e^{-\Gamma} \quad (24)$$

$$\tilde{\Gamma} = \sqrt{\Gamma_n \Gamma_m}, \quad \bar{\Gamma} = \frac{1}{2}(\Gamma_n + \Gamma_m), \quad \Gamma_n = \frac{1}{2}(k_{\perp,n}\alpha/\Omega)^2. \quad (25)$$

Here  $I_\ell$  is the modified Bessel function of order  $\ell$ ,  $Z_\ell$  is the plasma dispersion function with arguments  $\zeta_\ell = (\omega - \ell\Omega)/|k_{\perp}|\alpha$ , and derivative of  $Z_\ell$  is  $Z'_\ell(\zeta_\ell) = -2[1 + \zeta_\ell Z(\zeta_\ell)]$ . There is an additional ‘Swanson’s rotation’ to transform  $\mathbf{E}(x, y)$  and other quantities between the ‘Stix frame’ and local coordinate aligned to the magnetic field.

Two simplifying assumptions are used to reduce the cost for computing  $\dot{W}$ . The first is to truncate the expansion of  $W_\ell$  typically to  $-2 \leq \ell \leq 2$ . The second is to restrict the evaluation to a smaller number of local Fourier modes (say 32 modes instead of 96 modes) and with some overlap with neighboring nodes. Even with these simplifications for the evaluation of  $\dot{W}$ , the relative error in evaluation is typically less than 5%.

This costly evaluation can be further reduced by using interpolation and extrapolation expressed as Kronecker products in (9). We shall consider, for example, the evaluation of the (1,1) component in  $\dot{W}$ . The evaluation of other entries can be similarly derived. The main contribution is

$$\sum_{m,n} u_m \left( \sum_{\ell} \ell^2 I_\ell Z_\ell \right) v_n, \quad (26)$$

where  $u_m = e^{-i\vec{k}_m \cdot \vec{r}} \mathbf{E}_m / \sqrt{\Gamma_m}$ ,  $v_n = e^{i\vec{k}_n \cdot \vec{r}} \mathbf{E}_n / \sqrt{\Gamma_n}$  (with  $\tilde{\Gamma} = \sqrt{\Gamma_n \Gamma_m}$ ). This can be interpreted as the algebraic evaluation of a vector product,  $u^t * \tilde{F} * v$  where entries in matrix  $\tilde{F}$ ,  $\tilde{F}_{n,m} = \sum_{\ell} \ell^2 I_\ell(\sqrt{\Gamma_n \Gamma_m}) Z_\ell$  are costly to compute.

As entries in the matrix  $\tilde{F}$  (size  $M \times M$ ) are smooth functions of modified Bessel functions and plasma  $Z$  dispersion functions, we can consider approximating matrix  $\tilde{F}$  by evaluating only a  $m \times m$  submatrix  $F$  and performing interpolation. Using equations (8) and (9), we have

$$u^t \tilde{F} v = u^t * (T_{\tilde{x}} * T_x^{-1}) * F * (T_{\tilde{y}} * T_y^{-1})^t * v \quad (27)$$

$$= (u^t * T_{\tilde{x}} * T_x^{-1}) * F * (T_y^{-t} T_{\tilde{y}}^t v) \quad (28)$$

$$= \tilde{u}^t * F * \tilde{v}, \quad \text{where } \tilde{u} = T_x^{-t} * T_{\tilde{x}}^t * u, \tilde{v} = T_y^{-t} * T_{\tilde{y}}^t * v. \quad (29)$$

Since the evaluation of  $\tilde{W}$  is repeated many times at each grid point in the plasma, we can amortize the cost for precomputing the transformation matrices

$$\hat{T}_y = T_y^{-t} * T_{\tilde{y}}^t, \quad \hat{T}_x = T_x^{-t} * T_{\tilde{x}}^t. \quad (30)$$

The overall approximate computation of  $u^t * \tilde{F} * v$  can be arranged as (i) evaluation of a submatrix  $F$ , (ii) transform vectors  $\tilde{u} = \hat{T}_y * u, \tilde{v} = \hat{T}_x * v$  (in  $O(2mM)$  work) and (iii) final evaluation of  $\tilde{u}^t * F * \tilde{v}$  (in  $O(2m^2)$  work). Note that explicit computation of the interpolation coefficients by (8) (in  $O(2m^3)$  work) and evaluation of  $\tilde{F}$  by (9) (in  $O(mM^2)$  work) to evaluate  $u^t * \tilde{F} * v$  (in  $O(2M^2)$  work) would be more costly.

This approximate evaluation of  $\tilde{W}$  has been incorporated into the AORSA2D code. For one typical computation with  $96 \times 96$  modes, the time for evaluating  $\tilde{W}$  using 32 local Fourier modes required about 78.3 min while the Kronecker version that evaluated a  $9 \times 9$  submatrix (instead of  $32 \times 32$  matrix for each component) reduced the time to about 7.1 minutes with less than 3% difference in the results.

There is an on-going effort to incorporate similar Kronecker technology for evaluate of  $\tilde{W}$  in the three-dimensional version of AORSA.

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