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**OAK RIDGE  
NATIONAL  
LABORATORY**



## **Neutronics Benchmarks of Mixed-Oxide Fuels using the SCALE/CENTRM Sequence**

**D. F. Hollenbach  
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MANAGED AND OPERATED BY  
LOCKHEED MARTIN ENERGY RESEARCH CORPORATION  
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Computational Physics and Engineering Division

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# ABSTRACT

The purpose of this study is to determine and document the reactor physics parameters (multiplication factors, spatially dependent flux ratios, and spatially dependent reaction rates ) for several distinct sets of problems using two distinct resonance cross-section processing techniques. In SCALE, by default, resonances are processed using NITAWL, which utilizes the Nordheim Integral Treatment. The results produced using this sequence are considered to be the base results. A second set of results are produced by replacing NITAWL with CENTRM/PMC. CENTRM produces point-wise fluxes for a given geometry configuration and set of isotopes. Using these fluxes, PMC produces problem-dependent self-shielding cross sections. Both sequences use ENDF/B-V cross-section data.



# 1. INTRODUCTION

This report examines four sets of problems that are used to evaluate the differences between the NITAWL resonance processor and the CENTRM/PMC resonance processor. All the problems are predominantly thermal, with the energy of the average lethargy causing fission (EALCF) being below 1 eV. They are all water-moderated fuel rod lattices of various dimensions and fuel materials. The objective of this report is to compare the differences between the NITAWL and CENTRM/PMC resolved-resonance processors for the class of problems presented in this report. The existence of severe resonance overlap when mixing uranium and plutonium could cause a significant problem with the NITAWL results. CENTRM/PMC does not contain this potential problem, which is a limitation of the Nordheim Integral Treatment.

All problems were processed using SCALE5.0, which allows one to choose which resolved resonance processor will be used to self-shield the nuclides, NITAWL or CENTRM/PMC. SCALE5.0 is a developmental version of the SCALE code system. The current version of SCALE, SCALE4.4, does not contain CENTRM but is essentially the same in all other aspects to SCALE5.0.

SCALE5.0 has the ability to use either NITAWL or CENTRM/PMC as the resolved-resonance processor. All problems were run first using CENTRM/PMC and then using NITAWL. The results were then analyzed and compared.<sup>1,2</sup>

## 1.1 THE SCALE 5.0 SEQUENCES

SCALE 5.0 contains two distinct sequences used for processing cross-section data. The original sequence consisting of the codes CSAS, BONAMI, and NITAWL process all resolved resonance data in NITAWL. The new computational sequence added to SCALE5.0 uses the following sequence to process the cross sections: CSAS, BONAMI, NITAWL, CENTRM, PMC, WORKER. CENTRM/PMC process the resolved resonances cross sections in the unit cell. All other resolved resonance cross sections are processed using NITAWL. To calculate the desired physics parameters, the three experimental benchmark sets then use KENO-V.a and the set of computational benchmarks uses XSDRNPM. Many of the physics parameters are compared with direct experimental data and others are compared only with the same parameters calculated using difference codes and cross sections.

## 1.2 NITAWL

NITAWL performs problem-dependent resonance self-shielding using the Nordheim Integral Treatment, which involves solving for the energy dependence of the neutron flux in a material region containing a resonance absorber and a maximum of two moderating materials. The resonance self-shielding is made with reference to infinite dilution cross-section values. The material region is either infinite or a one-dimensional (1-D) slab, cylinder, or sphere surrounded by moderator. In the moderator, the neutron flux is assumed to be spatially flat and slowly varying with energy. The presence of more than one fuel region in the moderator, such as a lattice, is accounted for using a Dancoff factor.

There are many problems where the Nordheim Integral Treatment may not be appropriate because of the following assumptions:

1. Each resonance nuclide can be treated without consideration of other resonance nuclides present in the system.
2. The neutron flux is spatially uniform in the absorber and moderator regions.
3. Neutron transport into and out of the absorber region can be treated with first-flight escape probabilities.
4. The presence of other absorber lumps in the system can be accounted for with a Dancoff factor which corresponds to the first-flight transmission probability across the moderator. A Dancoff factor of zero corresponds to a single lump in the moderator. A Dancoff factor of 1 corresponds to an infinite medium of the absorber material with no moderator outside the absorber lump.

### 1.3 CENTRM/PMC

The new resolved-resonance processor is composed of two codes that are executed sequentially. The first code, CENTRM, is a discrete-ordinate code that produces a point-wise continuous-energy flux spectrum for a given infinite or 1-D problem. Subsequently, PMC uses this point flux spectrum to collapse point cross sections to a problem-dependent multigroup cross-section set. To generate the flux profile and produce new group cross sections, the two codes use a pointwise continuous cross-section library that contain all the nuclides present in the selected multigroup cross-section library. All the cases in this report were analyzed using the 238-group ENDF/B-V multigroup cross-section library.

CENTRM has several options that determine the range over which the flux spectrum will be generated and the parameters used for generating the flux spectrum. Although pointwise continuous in energy, the flux spectrum is generated on a specified 1-D spacial mesh. For all cases in this report, the spatial mesh is over an infinite cylinder that is automatically generated by the code. The flux spectrum is generated from 20 MeV to  $1.0E-5$  eV over the spatial mesh using a default quadrature of 8. CENTRM uses the specified quadrature to generate Legendre coefficients for the scattering component of the pointwise flux.

CENTRM is capable of using a fixed or fission input source to generate the flux profile. For simplicity and because the benchmarks are fission problems, a spacially flat fission source is assumed as an initial guess. Two other parameters that can affect the flux are the point convergence criterion and the tolerance used for thinning the pointwise cross sections. These parameters are both set to default values of 0.0001 for the convergence criterion and 0.0025 for the thinning tolerance.

In order for CENTRM to generate the flux profile it first combines the pointwise continuous-energy cross sections of all nuclides in each zone. Each zone contains only one material but is divided into many intervals, with each interval being a mesh point where the entire energy spectrum of the flux is calculated. There is no code limit on the number of materials and 1-D zones. However, for large problems involving many materials and zones, computer memory and CPU speed may be a limiting factor.

By default, the flux profile is generated using an  $S_N$  calculation over the entire spectrum. The option exists to perform several other types of calculations independently over the fast, thermal, and



pointwise ranges. Over all energy ranges, scattering for the pointwise continuous cross sections is assumed to be elastic and isotropic in the center of mass system. Consequently, no scattering data are contained in the point library, only 1-D cross sections.

PMC replaces the cross sections for specified nuclides and energy groups in the problem-dependent multigroup library. PMC reads the pointwise flux file, the pointwise continuous cross sections, and the problem-dependent multigroup library; generates new multigroup data from the point data; and finally rewrites the multigroup library with the new multigroup data. PMC can produce multigroup cross sections over three ranges for all nuclides: the entire point library range, the resolved resonance range, or the pointwise flux range. For the problems, in this report PMC produces multigroup cross sections over the resolved resonance range of each nuclide in the unit cell data.

PMC has three methods for computing the scattering component of the new multigroup cross sections. The  $P_N$  components of the original multigroup scattering cross sections can be renormalized to the new 1-D scattering cross sections. The  $P_N$  components of the original multigroup scattering cross sections can be renormalized using the scalar flux. Finally, new  $P_N$  components for the scattering cross section can be computed using the pointwise flux moments. For the problems in this report, the first option of renormalizing the  $P_N$  components using the new 1-D cross sections is used.

A set of pointwise continuous cross sections are available for use by CENTRM and PMC. The point cross sections used in the report were generated using the AMPX code system from the ENDF/B-V nuclear data library. The library contains all the nuclides present in both the 238-group and 44-group ENDF/B-V multigroup libraries. The library contains the total, elastic scattering, and radiative capture cross sections for each nuclide. If a nuclide is fissionable, the fission cross section is also present. Also, if a nuclide contains inelastic data at higher energies, inelastic data are also included in the library. The pointwise continuous library is divided up into files, with each file containing all the cross-section data for one nuclide. The ENDF/B-V pointwise library was generated to be used with the ENDF/B-V multigroup libraries. Using it with any other type of library, such as one generated using ENDF/B-VI data, could produce incorrect results.



## 2. MIX-COMP-THERM-2 (PNL-30 to PNL-35)

### 2.1 DESCRIPTION

This section describes a set of six critical experiments, each consisting of a square-pitched array of mixed plutonium-uranium fuel rods submerged in water surrounded by a water reflector. The water contains boron concentrations from 0.9 to 767.2 ppm. This set of experiments is contained in the *International Handbook of Evaluated Criticality Safety Benchmark Experiments*.<sup>3</sup>

This set of experiments was performed between December 1975 and March 1976 at the Plutonium Recycle Critical Facility at Pacific Northwest Laboratory. The benchmark experiments are light-water-moderated critical assemblies consisting of a core array supported by upper and lower lattice plates. The lattice plates are 2.54 cm thick and located at the top and bottom of the fuel region. The reactor is brought to critical by raising the water level in the tank, thus avoiding the use of control rods. The fuel rods sit on a support plate above the bottom of the tank. The tank is wide enough to assume an infinite moderator on the sides and bottom (~30 cm of water).

All fuel rods have the same physical dimensions. A schematic diagram of the fuel rods and bottom reflector is given in Fig. 2.1. Each fuel rod has an active fuel length of 86.6775 cm, 0.5 cm of UO<sub>2</sub> at the bottom of the fuel, a 0.6985-cm cladding plug on the bottom and a 0.8255-cm cladding plug on the top. The fuel has a radius of 0.64135 cm. The cladding has an outside radius of 0.71755 cm. A 0.3175-cm water gap is located between the top of the aluminum support plate and the bottom of the lower lattice plate. The aluminum support plate is 2.8575 cm thick. There is a 0.889-cm water gap between the bottom of the lead plate and the top of the upper lattice plate. The lead plate is 0.9525 cm thick. The top reflector varies depending on the water level for the particular problem.

The primary differences between the six benchmarks are lattice pitch, number of rods in the lattice, water level, and boron concentrations. All other benchmark characteristics are constant. There are three different lattice pitches, with each pitch used in two problems: 1.778 cm, 2.20914 cm, and 2.51447 cm. The fuel is arranged in a square-pitched lattice. The characteristics of each of the four lattices are given in Table 2.1. Table 2.2 contains the atom densities for all the materials in the problem except B-10 and B-11. The atom densities in Table 2.2 are constant for all benchmarks. Table 2.3 contain the atom densities of B-10 and B-11 for each benchmark. All material temperatures are assumed to be 23°C (295 K).

As shown in Table 2.1, the six benchmark problems change by moderator boron concentration, number of fuel rods, lattice pitch and upper-reflector thickness. To simplify the accumulation of power densities, advantage was taken in the symmetry of the problem whenever possible. The entire problem was explicitly modeled, but instead of having a separate unit for each pin, 1/8th symmetry was used for every problem except PNL-32. Due to an irregular placement of outer rods, this problem needed to be modeled using a unit for each pin. The lattice is then filled from the 1/8th section by inserting additional pins in a mirror image. Figures 2.2 through 2.6 show the lattice map for each problem. Figure 2.4 shows a full-lattice mapping; the other figures contain only 1/8th lattices. The remaining lattice can be extrapolated from these 1/8th sections.

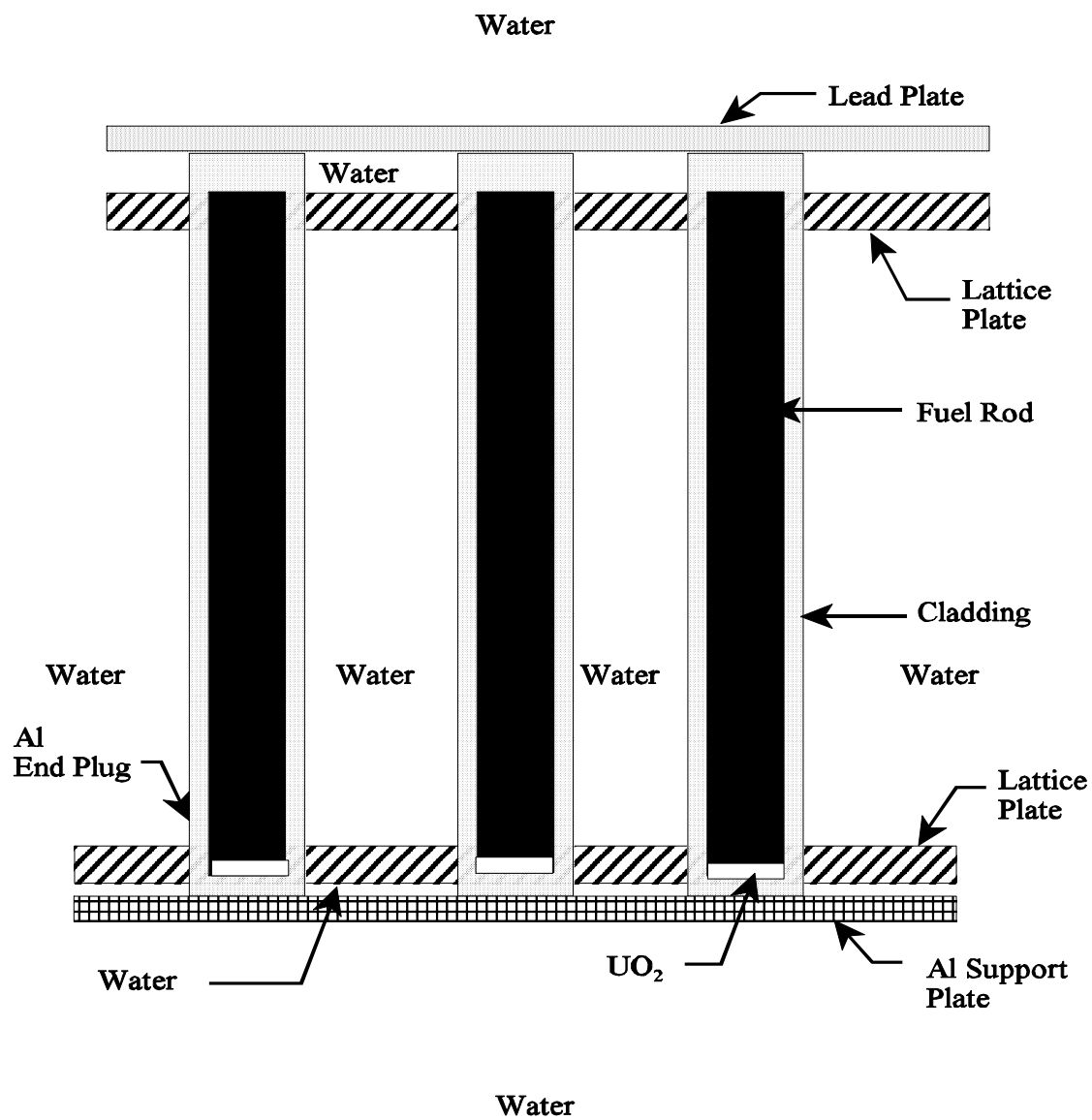


Fig. 2.1. Schematic of the PNL fuel rods with reflector.

Table 2.1. Lattice description for benchmarks

Benchmark No.	Boron con. (ppm)	Critical No. rods	Lattice pitch (cm)	Water level above lead (cm)
30	1.7	469	1.778	13.462
31	687.9	761	1.778	13.462
32	0.9	195	2.20914	3.937
33	1090.4	761	2.20914	13.462
34	1.6	160	2.51447	0.508
35	767.2	689	2.51447	13.462

Table 2.2. Constant benchmark atom densities

Material	Isotope	Atom density (atoms/barn-cm)	Material	Isotope	Atom density (atoms/barn-cm)
Fuel UO <sub>2</sub> -PuO <sub>2</sub> ( 9.54 g/cc )	U-234	$1.2458 \times 10^{-6}$	Lattice plate Support plate	Si	$1.3742 \times 10^{-2}$
	U-235	$1.4886 \times 10^{-4}$		Fe	$4.5919 \times 10^{-2}$
	U-236	$2.0936 \times 10^{-9}$		Cu	$1.1532 \times 10^{-4}$
	U-238	$2.0936 \times 10^{-2}$		Mn	$9.6395 \times 10^{-4}$
	Pu-238	$3.8836 \times 10^{-8}$		Mg	$1.2388 \times 10^{-4}$
	Pu-239	$3.9462 \times 10^{-4}$		Cr	$1.7409 \times 10^{-3}$
	Pu-240	$3.3206 \times 10^{-5}$		Zn	$1.6617 \times 10^{-2}$
	Pu-241	$1.6081 \times 10^{-6}$		Ti	$4.6052 \times 10^{-4}$
	Pu-242	$1.1882 \times 10^{-7}$		Al	$1.5025 \times 10^{-3}$
	Am-241	$1.4954 \times 10^{-6}$			
	O-16	$4.3779 \times 10^{-2}$			
Natural UO <sub>2</sub> ( 9.286 g/cc )	U-234	$1.2406 \times 10^{-6}$	Cladding	Sn	$4.8328 \times 10^{-4}$
	U-235	$1.4824 \times 10^{-4}$		Fe	$9.5642 \times 10^{-5}$
	U-236	$2.0848 \times 10^{-9}$		Cr	$7.6093 \times 10^{-5}$
	U-238	$2.0525 \times 10^{-2}$		Ni	$3.0336 \times 10^{-5}$
	O-16	$4.1943 \times 10^{-2}$		Zr	$4.2621 \times 10^{-2}$
				Lead	Pb

Table 2.3. Moderator atom densities

Benchmark No.	Atom densities ( atoms/barn-cm )			
	H	O	B-10	B-11
PNL-30	$6.6706 \times 10^{-2}$	$3.3353 \times 10^{-2}$	$1.8706 \times 10^{-8}$	$7.5770 \times 10^{-8}$
PNL-31	$6.6605 \times 10^{-2}$	$3.3400 \times 10^{-2}$	$7.5838 \times 10^{-6}$	$3.0718 \times 10^{-5}$
PNL-32	$6.6706 \times 10^{-2}$	$3.3353 \times 10^{-2}$	$9.9034 \times 10^{-9}$	$4.0114 \times 10^{-8}$
PNL-33	$6.6672 \times 10^{-2}$	$3.3427 \times 10^{-2}$	$1.2034 \times 10^{-5}$	$4.8746 \times 10^{-5}$
PNL-34	$6.6706 \times 10^{-2}$	$3.3353 \times 10^{-2}$	$1.7606 \times 10^{-8}$	$7.1313 \times 10^{-8}$
PNL-35	$6.6682 \times 10^{-2}$	$3.3405 \times 10^{-2}$	$8.4597 \times 10^{-5}$	$3.4266 \times 10^{-5}$

## 2.2 ANALYSIS

All six computational benchmarks in this section were processed twice using SCALE 5.0. The set labeled NITAWL uses the NITAWL resonance processor to self-shield the resolved resonance region for all nuclides in the fuel and clad. An identical set, labeled CENTRM, replaces NITAWL with the CENTRM/PMC code sequence for the nuclides in the unit cell. The NITAWL and CENTRM results are then compared.

Table 2.4 contains the  $k_{eff}$  and energy of the average lethargy causing fission (EALCF). The  $k_{eff}$  values for all the benchmark cases are close to 1.0: the worst NITAWL benchmark is 0.90% high, and the worst CENTRM case is 0.68% high. A small negative bias does appear between NITAWL and CENTRM, with the CENTRM cases about 0.25% lower on average than the NITAWL cases.

The EALCF is also shown in this table. The EALCF values listed are from the CENTRM cases. EALCF is the energy of the average lethargy causing fission and is calculated by summing the lethargies of the neutrons that undergo fission, dividing the value by the number of fissions, and converting this value to energy. For all cases, the difference between this value for CENTRM and NITAWL was less than 0.1%. Both CENTRM and NITAWL produce excellent and consistent results for the  $k_{eff}$  and fission energy for this set of problems.

Additional parameters calculated for each problem include: pin-power distributions; absorption,  $\langle G_f \rangle$ , and fission reaction rates and fluxes in the pin fuel, clad, and moderator; and four group cross sections and fluxes for a corner outside pin and the innermost pin. Each of these sets of data are calculated using both CENTRM and NITAWL. All the data for each case are contained in Figs. 2.7a through 2.12b and Tables 2.5 through 2.64.

The pin-power distributions for this problem assumed 1/8th core symmetry with a surrounding reflector for all benchmark cases except PNL-32. Because of a lack of symmetry in two outer pins the entire assembly needed to be modeled. The pin-power data consist of a value and a standard deviation for each pin. The values for the pin powers are actually in units of fissions per  $\text{cm}^3$ -s-source particle  $\times 10^{-5}$ . The value in parentheses is the percent standard deviation of the pin-power value.

In most cases the CENTRM and NITAWL results for each benchmark case fall within 2 standard deviations. The peak-to-low power changes with change in pitch and boron concentration.

The peak-to-low power ratio changed from a low of 1.86 for the smallest pitch with no boron added to a high of 4.19 at the largest pitch with added boron. The addition of boron significantly shifts the flux profile to the center of the assembly by depressing the thermal flux in the moderator.

The reaction rates, total fluxes, and flux ratios for the CENTRM and NITAWL cases of each benchmark case are also in good agreement, seldom varying by more than 1%. These values are included for a corner pin and the center pin for each case. All the reaction rates and fluxes increase as the pins approach the center of the assembly if the outer two layers of the arrays are excluded. The lowest power pin occurs in either the outer layer or the next inner layer of the array. The flux ratios over the fuel, clad, and moderator are relatively constant for a given pitch and boron concentration. However, as the pitch increases, the proportion of the total pin flux in the moderator increases.

Finally, four-group fluxes and cross sections were calculated for selected nuclides in the fuel region of the same corner and center pins. The macroscopic cross sections listed include the radiative capture, fission, and  $\nu$ \*fission cross sections for U-235, U-238, and Pu-239. The four groups are collapsed from the 238-group multigroup cross-section set using the flux profile calculated in KENO-V.a as follows: group 1 is from 20 Mev to 9.5 keV, group 2 is from 9.5 keV to 3.0 eV, group 3 is from 3 eV to 0.4 eV, and group 4 is from 0.4 eV to  $10^{-5}$  eV. The 0.4 eV was chosen as a boundary because it is the cadmium cutoff energy. Groups 2 and 3 contain the resolved resonance regions for most of the nuclides used in these cases. Most of the cross-section data for the CENTRM and NITAWL cases of a given benchmark case agree within 1%.

## 2.3 CONCLUSIONS

For this set of benchmark cases, using either NITAWL and CENTRM as the resonance region processor produces acceptable results of the  $k_{eff}$  values. All other values produced using CENTRM and NITAWL are also consistent with each. For all cases, the  $k_{eff}$ 's produced using CENTRM are slightly lower, ~0.25%, than those produced using NITAWL to do the resonance self-shielding. As a result, the average  $k_{eff}$  of all the CENTRM cases is closer to 1.0 than the average  $k_{eff}$  of all the NITAWL cases for this set of benchmarks. The pin-power distributions, fluxes, reactions rates, and macroscopic cross sections all agree to approximately 1% between CENTRM and NITAWL.

The presence of boron in the moderator depresses the fraction of the flux in the moderator, thus creating a larger difference between the highest- and lowest-power pins. No significant differences were identified between the results produced by NITAWL and CENTRM for these benchmark cases.

Table 2.4. Comparison of  $k_{eff}$  and EALCF from CENTRM and NITAWL

CASE MIX-COMP-THERM- 2	NITAWL $k_{eff} (\pm F)$	CENTRM $k_{eff} (\pm F)$	% DIFF	EALCF ( eV )
PNL-30	1.000 (0.0005) <sup>a</sup>	0.9966 (0.0004)	-0.34	0.575
PNL-31	1.0026 (0.0004)	0.9987 (0.0003)	-0.39	0.768
PNL-32	1.0021 (0.0004)	1.0000 (0.0004)	-0.21	0.193
PNL-33	1.0090 (0.0003)	1.0064 (0.0004)	-0.26	0.282
PNL-34	1.0046 (0.0004)	1.0020 (0.0005)	-0.26	0.138
PNL-35	1.0079 (0.0004)	1.0068 (0.0004)	-0.11	0.182

<sup>a</sup> Values in parentheses is the percent standard deviation.

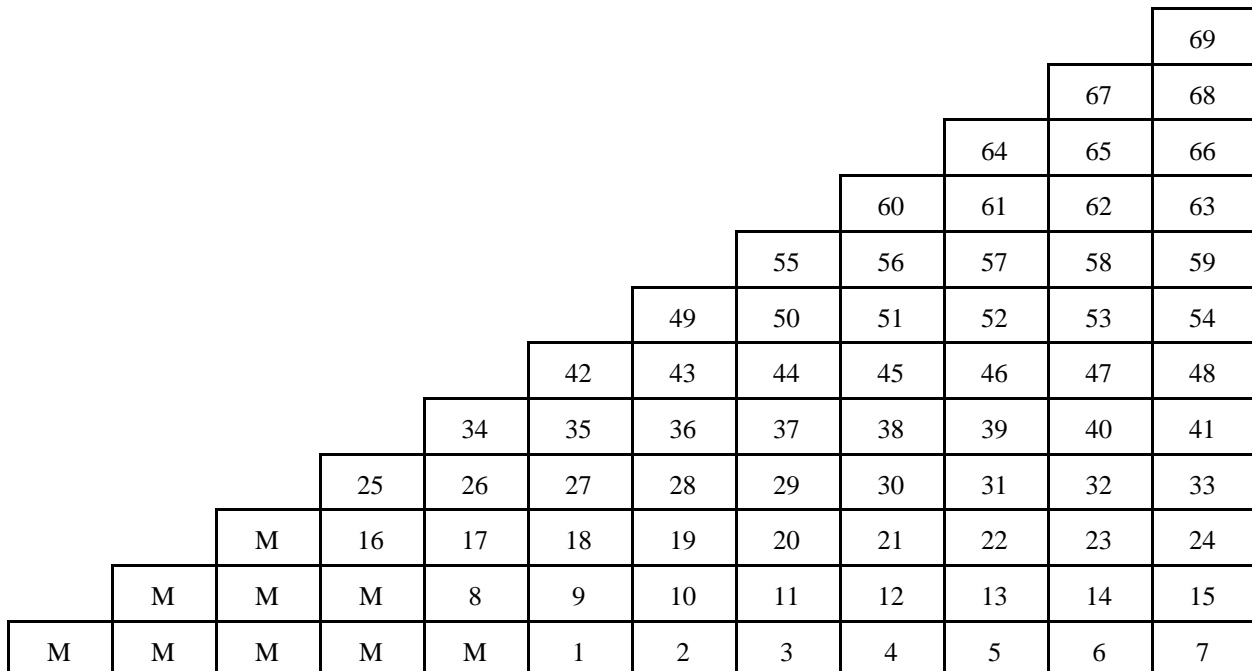


Fig. 2.2. Pin layout of benchmark case PNL-30.



											109
										107	108
									104	105	106
								100	101	102	103
							95	96	97	98	99
						89	90	91	92	93	94
					82	83	84	85	86	87	88
				74	75	76	77	78	79	80	81
			65	66	67	68	69	70	71	72	73
		55	56	57	58	59	60	61	62	63	64
	44	45	46	47	48	49	50	51	52	53	54
32	33	34	35	36	37	38	39	40	41	42	43
M	21	22	23	24	25	26	27	28	29	30	31
M	M	M	12	13	14	15	16	17	18	19	20
M	M	M	M	M	5	6	7	8	9	10	11
M	M	M	M	M	M	M	M	1	2	3	4

Fig. 2.3. Pin layout of benchmark cases PNL-31 and PNL-33.

M	M	M	M	M	M	M	193	194	195	M	M	M	M	M	M	M
M	M	M	M	M	M	187	188	189	190	191	192	M	M	M	M	M
M	M	M	M	178	179	180	181	182	183	184	185	186	M	M	M	M
M	M	M	167	168	169	170	171	172	173	174	175	176	177	M	M	M
M	M	154	155	156	157	158	159	160	161	162	163	164	165	166	M	M
M	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	M
M	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	M
107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123
90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106
73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89
M	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	M
M	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	M
M	M	30	31	32	33	34	35	36	37	38	39	40	41	42	M	M
M	M	M	19	20	21	22	23	24	25	26	27	28	29	M	M	M
M	M	M	M	10	11	12	13	14	15	16	17	18	M	M	M	M
M	M	M	M	M	4	5	6	7	8	9	M	M	M	M	M	M
M	M	M	M	M	M	M	1	2	3	M	M	M	M	M	M	M

Fig. 2.4. Pin layout of benchmark case PNL-32.

																27							
																25	26						
																22	23	24					
																18	19	20	21				
																13	14	15	16	17			
																M	8	9	10	11	12		
																M	M	M	4	5	6	7	
																M	M	M	M	M	M	2	3
																M	M	M	M	M	M	M	1

Fig. 2.5. Pin layout of benchmark case PNL-34.

										99
									97	98
								94	95	96
							90	91	92	93
						85	86	87	88	89
					79	80	81	82	83	84
				72	73	74	75	76	77	78
			64	65	66	67	68	69	70	71
		55	56	57	58	59	60	61	62	63
	45	46	47	48	49	50	51	52	53	54
34	35	36	37	38	39	40	41	42	43	44
M	24	25	26	27	28	29	30	31	32	33
M	M	15	16	17	18	19	20	21	22	23
M	M	M	7	8	9	10	11	12	13	14
M	M	M	M	M	1	2	3	4	5	6

Fig. 2.6. Pin layout of benchmark case PNL-35.

											2.475 (0.91)
										2.458 (0.46)	2.460 (0.46)
									2.413 (0.48)	2.427 (0.31)	2.423 (0.44)
								2.235 (0.48)	2.337 (0.35)	2.354 (0.35)	2.386 (0.43)
							2.095 (0.46)	2.183 (0.35)	2.220 (0.32)	2.275 (0.33)	2.293 (0.46)
						1.883 (0.57)	1.982 (0.35)	2.074 (0.32)	2.127 (0.36)	2.150 (0.35)	2.168 (0.49)
					1.636 (0.58)	1.761 (0.41)	1.860 (0.35)	1.947 (0.35)	1.999 (0.36)	2.033 (0.35)	2.042 (0.49)
				1.423 (0.62)	1.534 (0.40)	1.616 (0.35)	1.707 (0.41)	1.792 (0.38)	1.833 (0.35)	1.874 (0.35)	1.877 (0.50)
			1.530 (0.56)	1.381 (0.46)	1.416 (0.43)	1.483 (0.40)	1.557 (0.42)	1.624 (0.38)	1.670 (0.33)	1.710 (0.38)	1.714 (0.55)
		0	2.213 (0.35)	1.510 (0.44)	1.358 (0.41)	1.367 (0.43)	1.423 (0.42)	1.493 (0.39)	1.530 (0.43)	1.566 (0.39)	1.566 (0.55)
	0	0	0	2.160 (0.37)	1.519 (0.43)	1.391 (0.43)	1.437 (0.44)	1.480 (0.39)	1.539 (0.40)	1.566 (0.39)	1.573 (0.54)
0	0	0	0	0	2.311 (0.40)	2.001 (0.43)	2.035 (0.39)	2.124 (0.40)	2.197 (0.36)	2.225 (0.39)	2.254 (0.57)

Fig. 2.7a. Pin-power distribution for CENTRM benchmark PNL-30. Value in parentheses is the percent standard deviation.

											2.509 (0.86)
										2.465 (0.42)	2.484 (0.42)
									2.402 (0.39)	2.440 (0.32)	2.451 (0.43)
								2.268 (0.48)	2.325 (0.33)	2.350 (0.32)	2.378 (0.46)
							2.115 (0.45)	2.180 (0.36)	2.246 (0.34)	2.285 (0.35)	2.287 (0.44)
						1.891 (0.50)	1.999 (0.35)	2.088 (0.32)	2.138 (0.32)	2.166 (0.36)	2.181 (0.49)
					1.642 (0.55)	1.773 (0.40)	1.865 (0.38)	1.941 (0.32)	1.998 (0.36)	2.033 (0.32)	2.037 (0.47)
				1.424 (0.59)	1.525 (0.40)	1.622 (0.39)	1.734 (0.37)	1.802 (0.35)	1.862 (0.36)	1.885 (0.32)	1.904 (0.53)
			1.511 (0.56)	1.397 (0.41)	1.409 (0.41)	1.491 (0.37)	1.568 (0.41)	1.640 (0.42)	1.686 (0.31)	1.712 (0.39)	1.711 (0.55)
		0	2.211 (0.36)	1.510 (0.38)	1.350 (0.41)	1.372 (0.40)	1.440 (0.39)	1.498 (0.37)	1.544 (0.42)	1.571 (0.39)	1.589 (0.52)
	0	0	0	2.156 (0.35)	1.499 (0.41)	1.405 (0.45)	1.436 (0.39)	1.489 (0.38)	1.550 (0.40)	1.571 (0.39)	1.567 (0.57)
0	0	0	0	0	2.299 (0.39)	2.002 (0.42)	2.039 (0.35)	2.122 (0.36)	2.201 (0.34)	2.231 (0.35)	2.259 (0.50)

Fig. 2.7b. Pin-power distribution for NITAWL benchmark PNL-30. Value in parentheses is the percent standard deviation.

Table 2.5. PNL-30 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.417E-05	2.311E-05	8.244E-06	1.385E-2	0.412
	Clad	2.864E-07	0.0	0.0	2.672E-3	0.079
	Mod.	5.922E-07	0.0	0.0	1.710E-2	0.509
69	Fuel	1.809E-05	2.453E-05	8.727E-06	3.412E-2	0.410
	Clad	4.701E-07	0.0	0.0	6.638E-3	0.080
	Mod.	5.476E-07	0.0	0.0	4.237E-2	0.510

Table 2.6. PNL-30 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.407E-05	2.297E-05	8.192E-06	1.384E-2	0.412
	Clad	2.802E-07	0.0	0.0	2.660E-3	0.079
	Mod.	5.895E-07	0.0	0.0	1.707E-2	0.509
69	Fuel	1.835E-05	2.515E-05	8.948E-06	3.395E-2	0.410
	Clad	4.678E-07	0.0	0.0	6.629E-3	0.080
	Mod.	5.644E-07	0.0	0.0	4.232E-2	0.510

Table 2.7. PNL-30, Pin-1 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	7.308E-05	7.296E-05
2	2.292E-05	2.291E-05
3	5.145E-06	5.269E-06
4	2.251E-05	2.239E-05

Table 2.8. PNL-30, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.31102E-04	5.17496E-04	2.00508E-04	2.30990E-04	5.17470E-04	2.00433E-04
2	5.24167E-03	8.10227E-03	3.32510E-03	5.22152E-03	8.04138E-03	3.30010E-03
3	8.11652E-03	1.64870E-02	6.76610E-03	8.06149E-03	1.64181E-02	6.73784E-03
4	7.34638E-02	1.52885E-01	6.27423E-02	7.34430E-02	1.52842E-01	6.27253E-02

Table 2.9. PNL-30, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	6.78395E-03	1.18456E-02	4.21512E-03	6.78829E-03	1.18801E-02	4.22404E-03
2	4.50410E-02	5.66348E-06	2.34636E-06	4.43898E-02	5.54963E-06	2.29918E-06
3	1.10308E-02	3.81572E-08	1.58093E-08	1.10387E-02	3.82177E-08	1.58343E-08
4	4.21801E-02	1.98117E-07	8.20835E-08	4.21730E-02	1.98085E-07	8.20706E-08

Table 2.10. PNL-30, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.31247E-04	2.10623E-03	6.81955E-04	7.31013E-04	2.10628E-03	6.81768E-04
2	1.46556E-02	2.42259E-02	8.41230E-03	1.42800E-02	2.35796E-02	8.18791E-03
3	4.46091E-02	8.80453E-02	3.05734E-02	4.45318E-02	8.79178E-02	3.05291E-02
4	3.81701E-01	7.65540E-01	2.64839E-01	3.80931E-01	7.64203E-01	2.64376E-01

Table 2.11. PNL-30, Pin-69 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	1.978E-04	1.958E-04
2	7.342E-05	7.309E-05
3	1.445E-05	1.458E-05
4	1.901E-05	1.966E-05

Table 2.12. PNL-30, Pin-69 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	2.40583E-04	5.25394E-04	2.05274E-04	2.40289E-04	5.25082E-04	2.05125E-04
2	5.09194E-03	7.87946E-03	3.23366E-03	4.90525E-03	7.60379E-03	3.12052E-03
3	8.03087E-03	1.62800E-02	6.68118E-03	8.07572E-03	1.64173E-02	6.73752E-03
4	6.44140E-02	1.33756E-01	5.48922E-02	6.49323E-02	1.34838E-01	5.53362E-02

Table 2.13. PNL-30, Pin-69 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	6.48013E-03	1.00639E-02	3.58425E-03	6.50153E-03	1.01355E-02	3.61266E-03
2	4.33496E-02	5.86890E-06	2.43146E-06	4.25035E-02	5.67595E-06	2.35151E-06
3	1.10028E-02	3.78364E-08	1.56763E-08	1.10397E-02	3.81740E-08	1.58162E-08
4	3.74989E-02	1.75656E-07	7.27780E-08	3.77530E-02	1.76873E-07	7.32818E-08

Table 2.14. PNL-30, Pin-69 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	7.34312E-04	2.06900E-03	6.75303E-04	7.34377E-04	2.07025E-03	6.75577E-04
2	1.41486E-02	2.33093E-02	8.09402E-03	1.38472E-02	2.29011E-02	7.95226E-03
3	4.37500E-02	8.64152E-02	3.00072E-02	4.41986E-02	8.73169E-02	3.03204E-02
4	4.24647E-01	8.20289E-01	2.83994E-01	4.24708E-01	8.21267E-01	2.84326E-01



											1.824 (0.90)
										1.821 (0.58)	1.818 (0.53)
									1.780 (0.50)	1.785 (0.32)	1.817 (0.48)
								1.693 (0.56)	1.725 (0.38.)	1.759 (0.36)	1.764 (0.47)
							1.611 (0.55.)	1.650 (0.34)	1.683 (0.35)	1.706 (0.36)	1.687 (0.50)
						1.492 (0.52)	1.535 (0.38)	1.601 (0.35)	1.624 (0.40)	1.633 (0.38)	1.634 (0.52.)
					1.338 (0.58)	1.419 (0.41)	1.476 (0.41)	1.509 (0.35)	1.550 (0.37)	1.562 (0.41)	1.570 (0.57)
				1.202 (0.64.)	1.271 (0.42)	1.332 (0.39)	1.385 (0.40)	1.437 (0.36)	1.460 (0.44)	1.488 (0.40)	1.500 (0.51)
			1.018 (0.65)	1.098 (0.46)	1.175 (0.42)	1.245 (0.48)	1.304 (0.38)	1.346 (0.40)	1.359 (0.40)	1.393 (0.40)	1.393 (0.59)
		0.861 (0.74)	0.930 (0.45)	1.016 (0.48)	1.078 (0.45)	1.139 (0.45)	1.195 (0.46)	1.228 (0.40)	1.261 (0.41)	1.282 (0.45)	1.288 (0.58)
	0.719 (0.74)	0.777 (0.57)	0.849 (0.55)	0.919 (0.46)	0.978 (0.53)	1.026 (0.43)	1.088 (0.43)	1.121 (0.49)	1.157 (0.44)	1.164 (0.45)	1.181 (0.66)
0.924 (0.72)	0.737 (0.59)	0.737 (0.54)	0.771 (0.57)	0.822 (0.52)	0.872 (0.47)	0.918 (0.48)	0.965 (0.46)	1.011 (0.51)	1.043 (0.47)	1.054 (0.45)	1.056 (0.64)
0	0.985 (0.52)	0.860 (0.51)	0.772 (0.55)	0.756 (0.56)	0.787 (0.57)	0.818 (0.53)	0.862 (0.51)	0.888 (0.48)	0.916 (0.53)	0.932 (0.42)	0.944 (0.67)
0	0	0	1.046 (0.49)	0.900 (0.48)	0.789 (0.52)	0.782 (0.57)	0.792 (0.56)	0.788 (0.56)	0.803 (0.49)	0.820 (0.51)	0.821 (0.70)
0	0	0	0	0	1.065 (0.45)	0.946 (0.50)	0.890 (0.55)	0.781 (0.59)	0.745 (0.55)	0.751 (0.60)	0.764 (0.79)
0	0	0	0	0	0	0	0	1.051 (0.45)	0.917 (0.54)	0.911 (0.50)	0.903 (0.77)

Fig. 2.8a. Pin-power distribution for CENTRM benchmark PNL-31. Value in parentheses is percent standard deviation.

											1.829 (1.01)
										1.827 (0.51)	1.832 (0.53)
									1.775 (0.50)	1.798 (0.35)	1.794 (0.52)
								1.722 (0.57)	1.742 (0.35)	1.776 (0.37)	1.785 (0.51)
							1.612 (0.53)	1.666 (0.36)	1.698 (0.38)	1.716 (0.35)	1.724 (0.50)
						1.502 (0.53)	1.549 (0.38)	1.593 (0.40)	1.640 (0.35)	1.644 (0.37)	1.646 (0.56)
					1.353 (0.57)	1.418 (0.43)	1.474 (0.37)	1.525 (0.38)	1.566 (0.38)	1.580 (0.38)	1.572 (0.51)
				1.192 (0.61)	1.274 (0.44)	1.343 (0.39)	1.402 (0.41)	1.435 (0.38)	1.478 (0.41)	1.493 (0.37)	1.486 (0.58)
			1.017 (0.66)	1.107 (0.47)	1.177 (0.43)	1.252 (0.40)	1.299 (0.39)	1.359 (0.42)	1.381 (0.44)	1.384 (0.40)	1.399 (0.55)
		0.860 (0.75)	0.929 (0.51)	1.010 (0.46)	1.079 (0.46)	1.145 (0.45)	1.202 (0.41)	1.245 (0.43)	1.272 (0.39)	1.295 (0.43)	1.297 (0.59)
	0.722 (0.79)	0.771 (0.55)	0.841 (0.55)	0.915 (0.51)	0.977 (0.43)	1.041 (0.47)	1.106 (0.47)	1.131 (0.43)	1.162 (0.43)	1.179 (0.48)	1.181 (0.60)
0.937 (0.68)	0.736 (0.61)	0.728 (0.54)	0.766 (0.58)	0.825 (0.55)	0.880 (0.47)	0.917 (0.49)	0.982 (0.47)	1.013 (0.45)	1.031 (0.46)	1.049 (0.45)	1.064 (0.66)
0	0.991 (0.51)	0.853 (0.52)	0.774 (0.57)	0.771 (0.53)	0.795 (0.53)	0.827 (0.53)	0.866 (0.48)	0.891 (0.52)	0.918 (0.52)	0.925 (0.44)	0.936 (0.67)
0	0	0	1.039 (0.54)	0.888 (0.51)	0.787 (0.50)	0.778 (0.47)	0.787 (0.60)	0.798 (0.55)	0.803 (0.52)	0.811 (0.51)	0.817 (0.72)
0	0	0	0	0	1.064 (0.49)	0.952 (0.45)	0.896 (0.51)	0.782 (0.53)	0.751 (0.55)	0.757 (0.55)	0.744 (0.80)
0	0	0	0	0	0	0	0	1.052 (0.48)	0.917 (0.52)	0.905 (0.49)	0.914 (0.71)

Fig. 2.8b. Pin power distribution for NITAWL benchmark PNL-31. Value in parentheses is percent standard deviation.

Table 2.15. PNL-31 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	6.732E-06	1.0493E-05	3.738E-06	7.748E-3	0.412
	Clad	1.407E-07	0.0	0.0	1.494E-3	0.079
	Mod.	5.801E-07	0.0	0.0	9.563E-3	0.509
109	Fuel	1.352E-05	1.821E-05	6.477E-06	2.577E-2	0.410
	Clad	3.513E-07	0.0	0.0	5.039E-3	0.081
	Mod.	8.806E-07	0.0	0.0	3.197E-2	0.509

Table 2.16. PNL-31 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	6.745E-06	1.049E-05	3.740E-06	7.754E-3	0.412
	Clad	1.404E-07	0.0	0.0	1.500E-3	0.079
	Mod.	5.820E-07	0.0	0.0	9.588E-3	0.509
109	Fuel	1.362E-05	1.838E-05	6.538E-06	2.583E-2	0.411
	Clad	3.478E-07	0.0	0.0	5.033E-3	0.080
	Mod.	8.960E-07	0.0	0.0	3.200E-2	0.509

Table 2.17. PNL-31, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	4.151E-05	4.145E-05
2	1.455E-05	1.468E-05
3	3.350E-06	3.351E-06
4	9.754E-06	9.744E-06

Table 2.18. PNL-31, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	2.34277E-04	5.20559E-04	2.02137E-04	2.34433E-04	5.20890E-04	2.02275E-04
2	5.31166E-03	8.16900E-03	3.35248E-03	5.27939E-03	8.08910E-03	3.31969E-03
3	8.11675E-03	1.65287E-02	6.78319E-03	8.06329E-03	1.64082E-02	6.73381E-03
4	7.08071E-02	1.47273E-01	6.04396E-02	7.10855E-02	1.47857E-01	6.06792E-02

Table 2.19. PNL-31, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	6.72455E-03	1.13885E-02	4.04980E-03	6.74729E-03	1.14467E-02	4.07385E-03
2	4.56936E-02	5.60056E-06	2.32029E-06	4.55851E-02	5.56831E-06	2.30692E-06
3	1.10516E-02	3.83036E-08	1.58698E-08	1.10407E-02	3.82095E-08	1.58309E-08
4	4.08111E-02	1.91551E-07	7.93633E-08	4.09499E-02	1.92215E-07	7.96381E-08

Table 2.20. PNL-31, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	7.32515E-04	2.09589E-03	6.79949E-04	7.32859E-04	2.09690E-03	6.80273E-04
2	1.48948E-02	2.45228E-02	8.51540E-03	1.45238E-02	2.40236E-02	8.34210E-03
3	4.46260E-02	8.81024E-02	3.05931E-02	4.49138E-02	8.86079E-02	3.07687E-02
4	3.92873E-01	7.79195E-01	2.69624E-01	3.93098E-01	7.80112E-01	2.69936E-01

Table 2.21. PNL-31, Pin-109 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	1.485E-04	1.486E-04
2	5.674E-05	5.667E-05
3	1.105E-05	1.126E-05
4	1.379E-05	1.412E-05

Table 2.22. PNL-31, Pin-109 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$
1	2.40011E-04	5.25238E-04	2.05020E-04	2.41044E-04	5.25948E-04	2.05500E-04
2	5.08433E-03	7.90435E-03	3.24387E-03	5.05763E-03	7.83928E-03	3.21717E-03
3	7.87603E-03	1.60055E-02	6.56854E-03	7.93289E-03	1.60894E-02	6.60295E-03
4	6.39052E-02	1.32666E-01	5.44450E-02	6.44026E-02	1.33734E-01	5.48830E-02

Table 2.23. PNL-31, Pin-109 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$
1	6.52904E-03	1.02652E-02	3.65253E-03	6.48723E-03	1.00441E-02	3.57473E-03
2	4.26228E-02	5.78745E-06	2.39771E-06	4.25107E-02	5.49843E-06	2.27798E-06
3	1.10023E-02	3.78561E-08	1.56844E-08	1.09805E-02	3.77877E-08	1.56562E-08
4	3.72074E-02	1.74257E-07	7.21979E-08	3.74882E-02	1.75595E-07	7.27521E-08

Table 2.24. PNL-31, Pin-109 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$
1	7.34579E-04	2.07331E-03	6.76047E-04	7.34616E-04	2.06809E-03	6.74966E-04
2	1.42795E-02	2.36502E-02	8.21241E-03	1.41529E-02	2.32927E-02	8.08827E-03
3	4.25902E-02	8.43169E-02	2.92786E-02	4.25863E-02	8.42498E-02	2.92554E-02
4	4.32807E-01	8.32922E-01	2.88390E-01	4.26617E-01	8.23669E-01	2.85166E-01

0	0	0	0	0	0	0	4.104	3.592	3.967	0	0	0	0	0	0	0
0	0	0	0	0	0	4.526	3.498	3.291	3.407	3.866	4.466	0	0	0	0	0
0	0	0	0	4.931	4.345	3.900	3.723	3.716	3.703	3.685	3.685	4.587	0	0	0	0
0	0	0	4.714	3.978	4.001	4.116	4.282	4.343	4.308	4.142	3.941	3.917	4.729	0	0	0
0	0	4.627	3.919	4.040	4.348	4.602	4.824	4.909	4.867	4.690	4.406	4.053	3.954	4.586	0	0
0	4.571	3.828	3.932	4.394	4.732	5.084	5.314	5.470	5.314	5.046	4.789	4.388	3.947	3.705	4.529	0
0	3.922	3.663	4.307	4.687	5.147	5.525	5.761	5.808	5.730	5.474	5.132	4.724	4.133	3.716	3.894	0
4.157	3.430	3.833	4.318	4.889	5.371	5.758	5.973	6.000	5.910	5.721	5.336	4.926	4.334	3.776	3.452	4.097
3.718	3.346	3.822	4.366	4.891	5.430	5.794	6.009	6.086	6.014	5.818	5.526	4.983	4.389	3.801	3.329	3.647
4.092	3.451	3.831	4.371	4.841	5.391	5.711	5.923	5.990	5.928	5.707	5.408	4.879	4.329	3.765	3.512	4.149
0	3.884	3.703	4.188	4.675	5.207	5.526	5.712	5.786	5.739	5.492	5.143	4.681	4.107	3.701	3.953	0
0	4.583	3.803	4.002	4.472	4.861	5.180	5.299	5.429	5.395	5.173	4.764	4.385	3.921	3.733	4.522	0
0	0	4.695	3.920	4.100	4.404	4.715	4.886	4.992	4.915	4.709	4.402	4.043	3.925	4.545	0	0
0	0	0	4.721	3.921	3.954	4.219	4.362	4.377	4.325	4.198	3.946	3.951	4.748	0	0	0
0	0	0	0	4.639	3.762	3.701	3.821	3.812	3.789	3.926	4.415	4.865	0	0	0	0
0	0	0	0	0	4.516	3.925	3.438	3.393	3.471	4.512	0	0	0	0	0	0
0	0	0	0	0	0	0	4.100	3.642	4.175	0	0	0	0	0	0	0

Fig. 2.9a. Pin-power distribution for CENTRM benchmark PNL-32 with standard deviation between 0.59 and 0.87% of the value.

0	0	0	0	0	0	0	4.193	3.696	4.139	0	0	0	0	0	0	0
0	0	0	0	0	0	4.568	3.565	3.354	3.466	3.987	4.530	0	0	0	0	0
0	0	0	0	4.902	4.409	3.981	3.841	3.804	3.753	3.706	3.767	4.624	0	0	0	0
0	0	0	4.739	3.971	4.071	4.190	4.304	4.352	4.301	4.177	3.952	3.930	4.705	0	0	0
0	0	4.625	3.956	4.080	4.417	4.773	4.884	4.914	4.907	4.720	4.427	4.010	3.991	4.684	0	0
0	4.612	3.769	4.039	4.470	4.913	5.191	5.404	5.433	5.357	5.142	4.790	4.319	3.940	3.779	4.489	0
0	3.884	3.700	4.150	4.792	5.200	5.595	5.759	5.763	5.729	5.484	5.192	4.683	4.164	3.727	3.874	0
4.153	3.500	3.842	4.455	4.989	5.431	5.783	5.974	5.974	5.953	5.726	5.346	4.840	4.324	3.784	3.470	4.059
3.735	3.352	3.825	4.417	4.978	5.524	5.756	6.026	6.099	5.988	5.801	5.425	4.969	4.412	3.818	3.329	3.711
4.211	3.533	3.823	4.416	4.969	5.395	5.781	5.929	5.958	5.856	5.731	5.360	4.817	4.315	3.757	3.404	4.099
0	3.894	3.705	4.182	4.755	5.208	5.492	5.682	5.749	5.595	5.475	5.095	4.677	4.078	3.680	3.876	0
0	4.558	3.742	4.015	4.413	4.846	5.195	5.336	5.383	5.265	5.059	4.737	4.377	3.944	3.712	4.465	0
0	0	4.614	3.980	4.088	4.380	4.731	4.941	4.880	4.853	4.659	4.358	4.024	3.882	4.574	0	0
0	0	0	4.789	3.910	3.973	4.142	4.350	4.423	4.348	4.130	3.973	3.904	4.683	0	0	0
0	0	0	0	4.625	3.768	3.664	3.837	3.803	3.735	3.920	4.301	4.912	0	0	0	0
0	0	0	0	0	4.516	3.907	3.442	3.317	3.414	4.463	0	0	0	0	0	0
0	0	0	0	0	0	0	4.045	3.626	4.106	0	0	0	0	0	0	0

Fig. 2.9b. Pin-power distribution for NITAWL benchmark PNL-32 with standard deviation between 0.57 and 0.90% of the values.

Table 2.25. PNL-32 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	2.451E-05	4.086E-05	1.457E-05	2.060E-2	0.267
	Clad	4.627E-07	0.0	0.0	3.943E-3	0.051
	Mod.	1.135E-06	0.0	0.0	5.259E-2	0.682
98	Fuel	3.946E-05	6.076E-05	2.164E-05	4.729E-2	0.266
	Clad	8.113E-07	0.0	0.0	9.173E-3	0.052
	Mod.	1.536E-06	0.0	0.0	1.121E-2	0.682

Table 2.26. PNL-32 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	2.429E-05	4.063E-05	1.449E-05	2.033E-2	0.266
	Clad	4.624E-07	0.0	0.0	3.930E-3	0.051
	Mod.	1.136E-06	0.0	0.0	5.223E-2	0.683
98	Fuel	3.963E-05	6.092E-05	2.169E-05	4.753E-2	0.267
	Clad	8.007E-07	0.0	0.0	9.195E-3	0.052
	Mod.	1.550E-06	0.0	0.0	1.214E-1	0.681



Table 2.27. PNL-32, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	1.048E-04	1.029E-04
2	3.087E-05	3.073E-05
3	7.654E-06	7.310E-06
4	4.050E-05	4.057E-05

Table 2.28. PNL-32, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.28226E-04	5.15645E-04	1.99145E-04	2.28198E-04	5.16018E-04	1.99123E-04
2	5.29819E-03	8.08102E-03	3.31639E-03	5.44312E-03	8.33186E-03	3.41933E-03
3	8.13381E-03	1.64731E-02	6.76041E-03	8.07192E-03	1.63713E-02	6.71862E-03
4	7.46578E-02	1.55396E-01	6.37731E-02	7.43303E-02	1.54714E-01	6.34932E-02

Table 2.29. PNL-32, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	6.95603E-03	1.26008E-02	4.48409E-03	6.96190E-03	1.26902E-02	4.50424E-03
2	4.76213E-02	5.91756E-06	2.45162E-06	4.49401E-02	5.50696E-06	2.28152E-06
3	1.10199E-02	3.80020E-08	1.57448E-08	1.10245E-02	3.79821E-08	1.57367E-08
4	4.27798E-02	2.00991E-07	8.32743E-08	4.26310E-02	2.00282E-07	8.29805E-08

Table 2.30. PNL-32, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.30986E-04	2.12139E-03	6.84695E-04	7.30230E-04	2.12081E-03	6.84023E-04
2	1.53809E-02	2.53859E-02	8.81516E-03	1.48494E-02	2.44809E-02	8.50088E-03
3	4.46591E-02	8.80834E-02	3.05866E-02	4.50509E-02	8.87866E-02	3.08308E-02
4	3.79625E-01	7.64299E-01	2.64388E-01	3.77128E-01	7.59495E-01	2.62726E-01

Table 2.31. PNL-32, Pin-98 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	2.586E-04	2.586E-04
2	8.866E-05	8.976E-05
3	1.956E-05	2.042E-05
4	5.545E-05	5.552E-05

Table 2.32. PNL-32, Pin-98 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	2.34086E-04	5.20599E-04	2.02092E-04	2.34329E-04	5.21021E-04	2.02251E-04
2	5.15153E-03	7.96071E-03	3.26701E-03	5.21152E-03	7.99933E-03	3.28285E-03
3	8.14944E-03	1.65985E-02	6.81186E-03	8.16239E-03	1.66200E-02	6.82071E-03
4	7.06334E-02	1.46886E-01	6.02804E-02	7.03727E-02	1.46337E-01	6.00555E-02

Table 2.33. PNL-32, Pin-98 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	6.75406E-03	1.14805E-02	4.08322E-03	6.78241E-03	1.15393E-02	4.10572E-03
2	4.75024E-02	5.74765E-06	2.38123E-06	4.63517E-02	5.42737E-06	2.24854E-06
3	1.10577E-02	3.83380E-08	1.58842E-08	1.10567E-02	3.83610E-08	1.58937E-08
4	4.07001E-02	1.91006E-07	7.91378E-08	4.05670E-02	1.90373E-07	7.88750E-08

Table 2.34. PNL-32, Pin-98 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	7.32645E-04	2.09793E-03	6.80410E-04	7.32954E-04	2.09852E-03	6.80530E-04
2	1.46368E-02	2.41261E-02	8.37768E-03	1.46065E-02	2.41771E-02	8.39539E-03
3	4.63098E-02	9.11738E-02	3.16598E-02	4.55958E-02	8.98849E-02	3.12122E-02
4	3.98803E-01	7.88748E-01	2.72941E-01	3.99072E-01	7.88716E-01	2.72936E-01

											2.024 (1.15)
										2.037 (0.53)	2.025 (0.53)
									1.958 (0.50)	2.001 (0.40)	2.009 (0.55)
								1.872 (0.50)	1.935 (0.32)	1.955 (0.40)	1.973 (0.54)
							1.783 (0.57)	1.848 (0.41)	1.869 (0.37)	1.905 (0.40)	1.904 (0.51)
						1.626 (0.54)	1.702 (0.39)	1.760 (0.37)	1.801 (0.37)	1.832 (0.41)	1.848 (0.47)
					1.461 (0.56)	1.539 (0.42)	1.624 (0.37)	1.661 (0.37)	1.707 (0.41)	1.721 (0.37)	1.746 (0.55)
				1.275 (0.64)	1.368 (0.47)	1.450 (0.43)	1.509 (0.45)	1.564 (0.43)	1.599 (0.37)	1.636 (0.40)	1.638 (0.55)
			1.065 (0.68)	1.155 (0.47)	1.251 (0.50)	1.341 (0.45)	1.403 (0.43)	1.448 (0.39)	1.485 (0.43)	1.512 (0.41)	1.518 (0.58)
		0.850 (0.79)	0.954 (0.52)	1.040 (0.51)	1.130 (0.51)	1.204 (0.45)	1.258 (0.45)	1.323 (0.45)	1.358 (0.43)	1.373 (0.42)	1.386 (0.60)
	0.639 (0.83)	0.738 (0.57)	0.846 (0.54)	0.910 (0.58)	1.008 (0.49)	1.077 (0.48)	1.137 (0.49)	1.182 (0.53)	1.213 (0.50)	1.231 (0.48)	1.240 (0.72)
0.564 (1.07)	0.554 (0.78)	0.633 (0.62)	0.712 (0.59)	0.793 (0.58)	0.866 (0.60)	0.931 (0.48)	0.991 (0.45)	1.039 (0.53)	1.078 (0.48)	1.092 (0.54)	1.099 (0.62)
0	0.565 (0.69)	0.594 (0.73)	0.618 (0.63)	0.663 (0.64)	0.731 (0.57)	0.786 (0.54)	0.838 (0.57)	0.883 (0.53)	0.932 (0.52)	0.942 (0.51)	0.937 (0.74)
0	0	0	0.621 (0.69)	0.628 (0.59)	0.628 (0.52)	0.658 (0.61)	0.702 (0.63)	0.735 (0.62)	0.761 (0.54)	0.783 (0.62)	0.783 (0.86)
0	0	0	0	0	0.622 (0.64)	0.618 (0.65)	0.639 (0.63)	0.619 (0.63)	0.623 (0.66)	0.641 (0.63)	0.659 (0.97)
0	0	0	0	0	0	0	0	0.610 (0.66)	0.570 (0.66)	0.585 (0.75)	0.604 (0.90)

Fig. 2.10a. Pin-power distribution for CENTRM benchmark PNL-33. Value in parentheses is percent standard deviation.

											2.037 (0.95)
										2.052 (0.57)	2.057 (0.51)
									2.004 (0.50)	2.007 (0.40)	2.018 (0.53)
								1.884 (0.57)	1.950 (0.36)	1.981 (0.38)	1.981 (0.51)
							1.783 (0.53)	1.833 (0.41)	1.883 (0.35)	1.917 (0.38)	1.917 (0.54)
						1.646 (0.55)	1.711 (0.38)	1.772 (0.37)	1.804 (0.40)	1.823 (0.40)	1.827 (0.49)
					1.466 (0.59)	1.553 (0.39)	1.610 (0.40)	1.670 (0.43)	1.718 (0.41)	1.736 (0.37)	1.751 (0.50)
				1.245 (0.60)	1.362 (0.43)	1.456 (0.39)	1.527 (0.40)	1.572 (0.41)	1.604 (0.41)	1.643 (0.40)	1.638 (0.54)
			1.067 (0.72)	1.155 (0.45)	1.257 (0.46)	1.330 (0.48)	1.403 (0.43)	1.447 (0.43)	1.491 (0.43)	1.509 (0.42)	1.528 (0.55)
		0.839 (0.75)	0.943 (0.60)	1.050 (0.52)	1.135 (0.48)	1.220 (0.47)	1.283 (0.45)	1.321 (0.48)	1.371 (0.47)	1.393 (0.45)	1.391 (0.60)
	0.632 (0.82)	0.731 (0.65)	0.824 (0.57)	0.919 (0.50)	1.004 (0.50)	1.069 (0.49)	1.141 (0.47)	1.181 (0.52)	1.220 (0.44)	1.247 (0.44)	1.249 (0.63.)
0.565 (0.98)	0.561 (0.63)	0.631 (0.62)	0.703 (0.54)	0.788 (0.53)	0.880 (0.54)	0.938 (0.51)	0.990 (0.53)	1.042 (0.53)	1.071 (0.53)	1.099 (0.50)	1.088 (0.73)
0	0.566 (0.64)	0.586 (0.69)	0.617 (0.62)	0.672 (0.68)	0.729 (0.58)	0.795 (0.53)	0.845 (0.55)	0.886 (0.53)	0.922 (0.55)	0.941 (0.55)	0.947 (0.78)
0	0	0	0.619 (0.69)	0.618 (0.67)	0.625 (0.68)	0.665 (0.63)	0.708 (0.54)	0.737 (0.61)	0.763 (0.54)	0.776 (0.62)	0.797 (0.82)
0	0	0	0	0	0.621 (0.67)	0.619 (0.68)	0.637 (0.67)	0.618 (0.65)	0.629 (0.68)	0.634 (0.69)	0.642 (0.97)
0	0	0	0	0	0	0	0	0.608 (0.65)	0.579 (0.62)	0.588 (0.72)	0.590 (0.96)

Fig. 2.10b. Pin-power distribution for NITAWL benchmark PNL-33. Value in parentheses is percent standard deviation.

Table 2.35. PNL-33 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	3.818E-06	6.043E-06	2.152E-06	3.853E-3	0.267
	Clad	7.376E-08	0.0	0.0	7.423E-4	0.051
	Mod.	4.770E-07	0.0	0.0	9.836E-3	0.682
109	Fuel	1.360E-05	2.034E-05	7.243E-06	1.705E-2	0.265
	Clad	2.788E-07	0.0	0.0	3.401E-3	0.051
	Mod.	1.498E-06	0.0	0.0	4.516E-2	0.684

Table 2.36. PNL-33 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	3.812E-06	6.048E-06	2.155E-06	3.867E-3	0.267
	Clad	7.253E-08	0.0	0.0	7.426E-4	0.052
	Mod.	4.787E-07	0.0	0.0	9.858E-3	0.681
109	Fuel	1.375E-05	2.067E-05	7.357E-06	1.779E-2	0.268
	Clad	2.783E-07	0.0	0.0	3.442E-3	0.052
	Mod.	1.505E-06	0.0	0.0	4.521E-2	0.680

Table 2.37. PNL-33, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.014E-05	2.016E-05
2	6.869E-06	6.908E-06
3	1.672E-06	1.719E-06
4	5.718E-06	5.745E-06

Table 2.38. PNL-33, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.31933E-04	5.20055E-04	2.01129E-04	2.31159E-04	5.18686E-04	2.00672E-04
2	5.35943E-03	8.22495E-03	3.37546E-03	5.34155E-03	8.22719E-03	3.37636E-03
3	8.26154E-03	1.68721E-02	6.92416E-03	8.25026E-03	1.68098E-02	6.89860E-03
4	7.10700E-02	1.47828E-01	6.06675E-02	7.10641E-02	1.47819E-01	6.06639E-02

Table 2.39. PNL-33, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	6.93024E-03	1.22507E-02	4.34474E-03	6.91791E-03	1.22576E-02	4.35689E-03
2	4.93469E-02	5.63616E-06	2.33504E-06	4.72956E-02	5.71788E-06	2.36889E-06
3	1.10965E-02	3.87293E-08	1.60462E-08	1.10697E-02	3.84758E-08	1.59412E-08
4	4.09384E-02	1.92170E-07	7.96200E-08	4.09467E-02	1.92207E-07	7.96350E-08

Table 2.40. PNL-33, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.32468E-04	2.11213E-03	6.82512E-04	7.31890E-04	2.11186E-03	6.82669E-04
2	1.55242E-02	2.53875E-02	8.81569E-03	1.47320E-02	2.43541E-02	8.45686E-03
3	4.75761E-02	9.35353E-02	3.24798E-02	4.58342E-02	9.03415E-02	3.13708E-02
4	3.92576E-01	7.79160E-01	2.69612E-01	3.91025E-01	7.76590E-01	2.68717E-01

Table 2.41. PNL-33, Pin-109 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	9.567E-05	9.796E-05
2	3.454E-05	3.486E-05
3	8.083E-06	7.903E-06
4	1.794E-05	1.809E-05

Table 2.42. PNL-33, Pin-109 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	2.35819E-04	5.23015E-04	2.03090E-04	2.36391E-04	5.23032E-04	2.03334E-04
2	5.23295E-03	8.08842E-03	3.31943E-03	5.36724E-03	8.21076E-03	3.36962E-03
3	8.20877E-03	1.67738E-02	6.88382E-03	8.26627E-03	1.68900E-02	6.93152E-03
4	6.90920E-02	1.43635E-01	5.89465E-02	6.84549E-02	1.42274E-01	5.83881E-02

Table 2.43. PNL-33, Pin-109 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	6.78959E-03	1.14474E-02	4.06739E-03	6.75365E-03	1.12640E-02	4.00886E-03
2	4.77122E-02	5.87328E-06	2.43327E-06	4.72083E-02	5.94071E-06	2.46121E-06
3	1.10759E-02	3.86960E-08	1.60324E-08	1.11162E-02	3.88436E-08	1.60936E-08
4	3.99038E-02	1.87192E-07	7.75574E-08	3.95563E-02	1.85520E-07	7.68646E-08

Table 2.44. PNL-33, Pin-109 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	7.33828E-04	2.09652E-03	6.79997E-04	7.33983E-04	2.09254E-03	6.79479E-04
2	1.54018E-02	2.52039E-02	8.75191E-03	1.50735E-02	2.48369E-02	8.62447E-03
3	4.51535E-02	8.91184E-02	3.09459E-02	4.89102E-02	9.59904E-02	3.33323E-02
4	4.06251E-01	7.98367E-01	2.76308E-01	4.12182E-01	8.07020E-01	2.79323E-01

								7.799 (0.66)
							7.518 (0.37)	7.649 (0.35)
						6.835 (0.40)	7.190 (0.27)	7.306 (0.37)
					5.772 (0.44)	6.293 (0.30)	6.617 (0.26)	6.772 (0.35)
				4.766 (0.47)	5.125 (0.31)	5.558 (0.30)	5.878 (0.29)	5.991 (0.39)
			0	5.095 (0.29)	4.633 (0.33)	4.852 (0.31)	5.064 (0.30)	5.107 (0.46)
		0	0	0	5.015 (0.27)	4.688 (0.34)	4.382 (0.33)	4.282 (0.47)
	0	0	0	0	0	0	4.431 (0.34)	3.764 (0.52)
0	0	0	0	0	0	0	0	4.082 (0.48)

Fig. 2.11a. Pin-power distribution for CENTRM benchmark PNL-34. Value in parentheses is percent standard deviation.



								7.789 (0.58)
							7.559 (0.29)	7.692 (0.25)
						6.856 (0.30)	7.211 (0.20)	7.342 (0.28)
					5.778 (0.31)	6.319 (0.21)	6.661 (0.21)	6.794 (0.32)
				4.790 (0.33)	5.142 (0.25)	5.607 (0.23)	5.928 (0.22)	5.991 (0.32)
			0	5.108 (0.24)	4.634 (0.25)	4.865 (0.21)	5.047 (0.23)	5.134 (0.33)
		0	0	0	5.009 (0.25)	4.689 (0.24)	4.367 (0.26)	4.295 (0.36)
	0	0	0	0	0	0	4.412 (0.26)	3.775 (0.40)
0	0	0	0	0	0	0	0	4.055 (0.41)

Fig. 2.11b. Pin-power distribution for NITAWL benchmark PNL-34. Value in parentheses is percent standard deviation.

Table 2.45. PNL-34 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	2.378E-05	4.072E-05	1.453E-05	1.638E-2	0.205
	Clad	4.283E-07	0.0	0.0	3.115E-3	0.039
	Mod.	1.208E-06	0.0	0.0	6.042E-2	0.756
27	Fuel	4.850E-05	7.778E-05	2.772E-05	4.812E-2	0.206
	Clad	9.350E-07	0.0	0.0	9.315E-3	0.039
	Mod.	2.117E-06	0.0	0.0	1.767E-1	0.755

Table 2.46. PNL-34 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	2.359E-05	4.048E-05	1.444E-05	1.632E-2	0.205
	Clad	4.263E-07	0.0	0.0	3.103E-3	0.039
	Mod.	1.204E-06	0.0	0.0	6.010E-2	0.756
27	Fuel	4.865E-05	7.795E-5	2.778E-05	4.833E-2	0.206
	Clad	9.241E-07	0.0	0.0	9.314E-3	0.040
	Mod.	2.122E-06	0.0	0.0	1.768E-1	0.754

Table 2.47. PNL-34, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	7.853E-05	7.833E-05
2	2.067E-05	2.085E-05
3	5.292E-06	5.285E-06
4	4.175E-05	4.127E-05

Table 2.48. PNL-34, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.24131E-04	5.12577E-04	1.97109E-04	2.23704E-04	5.11854E-04	1.96816E-04
2	5.42283E-03	8.35085E-03	3.42710E-03	5.42556E-03	8.28643E-03	3.40068E-03
3	8.31740E-03	1.69753E-02	6.96653E-03	8.31298E-03	1.69590E-02	6.95981E-03
4	7.54771E-02	1.57143E-01	6.44898E-02	7.58120E-02	1.57838E-01	6.47754E-02

Table 2.49. PNL-34, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.08275E-03	1.34026E-02	4.75965E-03	7.06095E-03	1.33747E-02	4.74910E-03
2	5.08244E-02	6.00968E-06	2.48979E-06	4.81132E-02	5.51775E-06	2.28598E-06
3	1.11012E-02	3.87466E-08	1.60534E-08	1.11191E-02	3.89584E-08	1.61412E-08
4	4.32220E-02	2.03118E-07	8.41557E-08	4.33792E-02	2.03865E-07	8.44652E-08

Table 2.50. PNL-34, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.29345E-04	2.13767E-03	6.87363E-04	7.28644E-04	2.13663E-03	6.86999E-04
2	1.53106E-02	2.52664E-02	8.77363E-03	1.54151E-02	2.54295E-02	8.83026E-03
3	4.67356E-02	9.20261E-02	3.19556E-02	4.76683E-02	9.37614E-02	3.25584E-02
4	3.72031E-01	7.53188E-01	2.60517E-01	3.73795E-01	7.56765E-01	2.61754E-01

Table 2.51. PNL-34, Pin-27 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.549E-04	2.550E-04
2	8.111E-05	8.287E-05
3	1.947E-05	1.947E-05
4	7.406E-05	7.415E-05

Table 2.52. PNL-34, Pin-27 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	2.32268E-04	5.19584E-04	2.01251E-04	2.31678E-04	5.19278E-04	2.00931E-04
2	5.33129E-03	8.13383E-03	3.33805E-03	5.40039E-03	8.25888E-03	3.38937E-03
3	8.21787E-03	1.67382E-02	6.86918E-03	8.24787E-03	1.68440E-02	6.91263E-03
4	7.26200E-02	1.51090E-01	6.20057E-02	7.26900E-02	1.51227E-01	6.20624E-02

Table 2.53. PNL-34, Pin-27 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	6.87156E-03	1.19877E-02	4.26261E-03	6.88984E-03	1.21250E-02	4.30392E-03
2	4.88942E-02	5.93992E-06	2.46088E-06	4.94199E-02	5.55323E-06	2.30068E-06
3	1.10643E-02	3.83905E-08	1.59059E-08	1.11102E-02	3.88583E-08	1.60997E-08
4	4.17166E-02	1.95887E-07	8.11600E-08	4.17541E-02	1.96065E-07	8.12334E-08

Table 2.54. PNL-34, Pin-27 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	7.32585E-04	2.10845E-03	6.82303E-04	7.32086E-04	2.11047E-03	6.82341E-04
2	1.52932E-02	2.51849E-02	8.74535E-03	1.50659E-02	2.45838E-02	8.53662E-03
3	4.71772E-02	9.27560E-02	3.22091E-02	4.72429E-02	9.29723E-02	3.22843E-02
4	3.90512E-01	7.78732E-01	2.69434E-01	3.90550E-01	7.78815E-01	2.69459E-01

										2.316 (1.24)
									2.296 (0.53)	2.287 (0.52)
								2.231 (0.55)	2.256 (0.39)	2.273 (0.58)
							2.099 (0.52)	2.175 (0.40)	2.223 (0.43)	2.208 (0.54)
						1.961 (0.55)	2.034 (0.41)	2.098 (0.41)	2.134 (0.38)	2.135 (0.61)
					1.756 (0.64)	1.872 (0.43)	1.941 (0.42)	1.996 (0.39)	2.057 (0.38)	2.047 (0.55)
				1.554 (0.67)	1.667 (0.45)	1.768 (0.42)	1.831 (0.46)	1.888 (0.45)	1.915 (0.41)	1.936 (0.60)
			1.322 (0.73)	1.441 (0.50)	1.550 (0.43)	1.640 (0.45)	1.704 (0.46)	1.742 (0.40)	1.797 (0.43)	1.788 (0.57)
		1.050 (0.80)	1.196 (0.58)	1.301 (0.46)	1.414 (0.47)	1.498 (0.52)	1.567 (0.46)	1.606 (0.46)	1.640 (0.43)	1.640 (0.61)
	0.798 (0.83)	0.924 (0.60)	1.047 (0.60)	1.159 (0.53)	1.254 (0.49)	1.331 (0.51)	1.400 (0.49)	1.441 (0.49)	1.475 (0.45)	1.488 (0.64)
0.657 (0.98)	0.680 (0.66)	0.780 (0.67)	0.888 (0.60)	1.002 (0.60)	1.099 (0.58)	1.163 (0.52)	1.236 (0.55)	1.270 (0.55)	1.299 (0.48)	1.291 (0.76)
0	0.645 (0.64)	0.667 (0.70)	0.755 (0.71)	0.838 (0.66)	0.926 (0.58)	1.004 (0.57)	1.052 (0.58)	1.091 (0.50)	1.122 (0.56)	1.114 (0.73)
0	0	0.605 (0.73)	0.620 (0.71)	0.685 (0.66)	0.759 (0.64)	0.821 (0.68)	0.868 (0.53)	0.902 (0.62)	0.924 (0.56)	0.929 (0.81)
0	0	0	0.562 (0.81)	0.591 (0.78)	0.617 (0.75)	0.649 (0.79)	0.696 (0.66)	0.736 (0.69)	0.753 (0.64)	0.760 (0.98)
0	0	0	0	0	0.553 (0.78)	0.558 (0.83)	0.591 (0.70)	0.619 (0.71)	0.642 (0.75)	0.645 (1.12)

Fig. 2.12a. Pin-power distribution for CENTRM benchmark PNL-35. Value in parentheses is percent standard deviation.

										2.333 (0.98)
									2.308 (0.50)	2.324 (0.46)
								2.251 (0.49)	2.275 (0.36)	2.283 (0.54)
							2.133 (0.50)	2.193 (0.36)	2.202 (0.36)	2.210 (0.48)
						1.973 (0.50)	2.044 (0.36)	2.110 (0.35)	2.131 (0.37)	2.142 (0.54)
					1.790 (0.55)	1.887 (0.38)	1.950 (0.40)	2.004 (0.36)	2.038 (0.35)	2.050 (0.48)
				1.583 (0.60)	1.688 (0.41)	1.765 (0.40)	1.827 (0.40)	1.890 (0.38)	1.916 (0.37)	1.941 (0.52)
			1.329 (0.66)	1.460 (0.45)	1.552 (0.42)	1.636 (0.38)	1.692 (0.38)	1.766 (0.39)	1.772 (0.40)	1.802 (0.60)
		1.065 (0.73)	1.212 (0.48)	1.315 (0.50)	1.409 (0.45)	1.482 (0.42)	1.566 (0.44)	1.603 (0.42)	1.622 (0.42)	1.645 (0.59)
	8.130 (0.80)	9.340 (0.58)	1.060 (0.54)	1.164 (0.47)	1.252 (0.50)	1.329 (0.47)	1.391 (0.45)	1.433 (0.44)	1.479 (0.41)	1.488 (0.61)
6.750 (0.89)	6.790 (0.62)	7.980 (0.63)	9.02 (0.55)	1.011 (0.53)	1.095 (0.48)	1.159 (0.50)	1.220 (0.46)	1.258 (0.46)	1.301 (0.47)	1.315 (0.61)
0	0.651 (0.64)	0.663 (0.67)	0.742 (0.60)	0.837 (0.60)	0.927 (0.54)	0.994 (0.54)	1.033 (0.52)	1.087 (0.53)	1.101 (0.49)	1.123 (0.72)
0	0	0.607 (0.74)	0.616 (0.66)	0.677 (0.65)	0.765 (0.57)	0.819 (0.56)	0.870 (0.59)	0.900 (0.53)	0.920 (0.59)	0.921 (0.77)
0	0	0	0.565 (0.68)	0.591 (0.65)	0.606 (0.66)	0.653 (0.63)	0.686 (0.66)	0.717 (0.59)	0.744 (0.59)	0.755 (0.87)
0	0	0	0	0	0.557 (0.69)	0.554 (0.69)	0.600 (0.73)	0.615 (0.71)	0.640 (0.70)	0.650 (0.96)

Fig. 2.12b. Pin-power distribution for NITAWL benchmark PNL-35. Value in parentheses is percent standard deviation.

Table 2.55. PNL-35 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	3.409E-06	5.555E-06	1.980E-06	3.018E-3	0.205
	Clad	6.266E-08	0.0	0.0	5.795E-4	0.039
	Mod.	3.753E-07	0.0	0.0	1.113E-2	0.756
99	Fuel	1.478E-05	2.314E-05	8.243E-06	1.578E-2	0.206
	Clad	2.862E-07	0.0	0.0	3.049E-3	0.039
	Mod.	1.467E-06	0.0	0.0	5.794E-2	0.755

Table 2.56. PNL-35 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	3.418E-06	5.589E-06	1.992E-06	3.030E-3	0.206
	Clad	6.288E-08	0.0	0.0	5.820E-4	0.040
	Mod.	3.743E-07	0.0	0.0	1.107E-2	0.754
99	Fuel	1.486E-05	2.341E-05	8.338E-06	1.603E-2	0.207
	Clad	2.817E-07	0.0	0.0	3.073E-3	0.040
	Mod.	1.487E-06	0.0	0.0	5.834E-2	0.753

Table 2.57. PNL-35, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	1.534E-05	1.545E-05
2	4.935E-06	4.897E-06
3	1.254E-06	1.264E-06
4	5.413E-06	5.443E-06

Table 2.58. PNL-35, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.29059E-04	5.17093E-04	1.99589E-04	2.29390E-04	5.17691E-04	1.99788E-04
2	5.45929E-03	8.37664E-03	3.43769E-03	5.46541E-03	8.36718E-03	3.43382E-03
3	8.30534E-03	1.69238E-02	6.94538E-03	8.28758E-03	1.68623E-02	6.92012E-03
4	7.30078E-02	1.51919E-01	6.23460E-02	7.27680E-02	1.51408E-01	6.21367E-02

Table 2.59. PNL-35, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	6.96200E-03	1.25983E-02	4.46724E-03	6.97774E-03	1.26269E-02	4.47453E-03
2	5.05345E-02	5.59431E-06	2.31769E-06	4.85328E-02	5.78528E-06	2.39681E-06
3	1.11140E-02	3.88695E-08	1.61043E-08	1.10876E-02	3.87287E-08	1.60460E-08
4	4.19366E-02	1.96955E-07	8.16021E-08	4.18109E-02	1.96348E-07	8.13505E-08

Table 2.60. PNL-35, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.31004E-04	2.12002E-03	6.83898E-04	7.31003E-04	2.11949E-03	6.83599E-04
2	1.57027E-02	2.57978E-02	8.95814E-03	1.48272E-02	2.46432E-02	8.55722E-03
3	4.68010E-02	9.21946E-02	3.20143E-02	4.68134E-02	9.21519E-02	3.19994E-02
4	3.84903E-01	7.69989E-01	2.66394E-01	3.86636E-01	7.72458E-01	2.67253E-01



Table 2.61. PNL-35, Pin-99 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	8.383E-05	8.501E-05
2	2.858E-05	2.911E-05
3	6.805E-06	7.098E-06
4	2.163E-05	2.187E-05

Table 2.62. PNL-35, Pin-99 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.33860E-04	5.21028E-04	2.02116E-04	2.31754E-04	5.19152E-04	2.00942E-04
2	5.36679E-03	8.26977E-03	3.39384E-03	5.36675E-03	8.27252E-03	3.39496E-03
3	8.17348E-03	1.67070E-02	6.85640E-03	8.15523E-03	1.66066E-02	6.81524E-03
4	7.08756E-02	1.47418E-01	6.04988E-02	7.06159E-02	1.46859E-01	6.02693E-02

Table 2.63. PNL-35, Pin-99 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	6.85097E-03	1.17780E-02	4.19479E-03	6.87710E-03	1.20714E-02	4.28595E-03
2	5.03681E-02	5.57278E-06	2.30878E-06	4.60701E-02	5.75479E-06	2.38419E-06
3	1.10871E-02	3.86935E-08	1.60313E-08	1.10723E-02	3.85789E-08	1.59839E-08
4	4.08300E-02	1.91640E-07	7.94004E-08	4.06994E-02	1.91015E-07	7.91408E-08

Table 2.64. PNL-35, Pin-99 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	7.33474E-04	2.10363E-03	6.81678E-04	7.31953E-04	2.10893E-03	6.82076E-04
2	1.48751E-02	2.48097E-02	8.61505E-03	1.48705E-02	2.44772E-02	8.49959E-03
3	4.59681E-02	9.06342E-02	3.14723E-02	4.52842E-02	8.93873E-02	3.10394E-02
4	3.95694E-01	7.84138E-01	2.71343E-01	3.95679E-01	7.83429E-01	2.71097E-01



## 3. MIX-COMP-THERM-3 (SAXTON-1 TO SAXTON-6)

### 3.1 DESCRIPTION

This section describes a set of six critical experiments, each consisting of a square-pitched array of mixed plutonium-uranium fuel rods submerged in water surrounded by a water reflector. The fuel rods are identical in all cases. Criticality is controlled by varying the number of rods, rod pitch, boron in water, and water level. This set of experiments is contained in the *International Handbook of Evaluated Criticality Safety Benchmark Experiments*.<sup>3</sup>

This set of experiments was performed in 1965 at the in the Critical Reactor Experiment Facility at the Westinghouse Reactor Evaluation Center. The benchmark experiments are light-water-moderated critical assemblies consisting of a core array supported by upper, middle, and lower lattice plates. The lower and middle lattice plates are 0.635 cm thick. The upper lattice plate is 1.27 cm thick. The middle lattice plate was not included in the models to facilitate the accumulation of pin-power distributions. The reactor is brought to critical by raising the water level in the tank, thus avoiding the use of control rods. The fuel rods sit on a support plate above the bottom of the tank. The tank is wide enough to assume an infinite moderator on the sides and bottom (~30 cm of water).

All fuel rods have the same physical dimensions. A schematic diagram of the fuel rods and bottom reflector is given in Fig. 3.1. Each fuel rod has an active fuel length of 92.964 cm, a 1.905-cm-long cladding plug on the bottom and a 4.320-cm-long cladding plug on the top. The fuel has a diameter of 0.856996 cm. The cladding outside diameter is 0.99314 cm with a 0.059055-cm-thick wall. This leaves a 0.009017-cm gap between the fuel and cladding.

The bottom of the fuel rod and lower lattice plate rest on a 2.54-cm aluminum support plate. Between the bottom of the aluminum support plate and the top of a 5.08-cm aluminum slab is 6.35 cm of water. The space between the top of the lower lattice plate and bottom of the middle lattice plate is 46.99 cm. The space between the top of the middle lattice plate and bottom of the top lattice plate is 47.625 cm. To simplify the problem the middle lattice plate was removed and replaced with water. The water level varies with each problem but is always between the middle and upper lattice plates. The tank is large enough to assume an infinite water reflector on the sides and bottom. An infinite water reflector can be effectively modeled using 30 cm of water, which is used to model the reflector for this set of benchmarks.

The primary differences between the six benchmarks are lattice pitch, number of rods in the lattice, water level, and for problem 3, boron density in the water. The physical characteristics of each benchmark case, including moderator temperature, are given in Table 3.1. The atom densities for all the materials in the problem except B-10, B-11 H, and O in the moderator are contained in Table 3.2. The atom densities in Table 3.2 are constant for all benchmarks. Table 3.3 contain the atom densities of B-10, B-11, H, and O in the moderator for each benchmark.

The lattice is filled from the 1/8th or 1/4th section by inserting additional pins in a mirror image. Figures 3.2 through 3.6 show the lattice map for each problem. Figure 3.2 shows a 1/4th lattice mapping while the other figures contain only 1/8th lattices. This difference exists because SAXTON-1 contains a different number of pins in the X and Y directions.

Table 3.1. Lattice description for SAXTON benchmark cases

Benchmark No.	Boron con. (ppm)	Lattice	Lattice pitch (cm)	Water level from bottom of fuel (cm)	Water temp. (°C)
1	0.0	22 × 23	1.3208	82.90	25.8
2	0.0	19 × 19	1.4224	80.80	17.0
3	337	21 × 21	1.4224	88.06	18.0
4	0.0	13 × 13	1.86789	68.41	24.1
5	0.0	12 × 12	2.01158	76.76	16.1
6	0.0	11 × 11	2.6416	79.50	19.9

Table 3.2. Constant benchmark atom densities

Material	Isotope	Atom density (atoms/barn-cm)	Material	Isotope	Atom density (atoms/barn-cm)
Fuel UO <sub>2</sub> -PuO <sub>2</sub>	U-234	$4.6590 \times 10^{-6}$	Cladding and end plugs	Sn	$4.6590 \times 10^{-4}$
	U-235	$1.5301 \times 10^{-4}$		Fe	$1.4148 \times 10^{-4}$
	U-238	$2.1097 \times 10^{-2}$		Cr	$7.5977 \times 10^{-5}$
	Pu-239	$1.3526 \times 10^{-3}$		O	$2.9630 \times 10^{-4}$
	Pu-240	$1.2759 \times 10^{-4}$		Zr	$4.2517 \times 10^{-2}$
	Pu-241	$1.1407 \times 10^{-5}$	Al lattice plate, Al support plate, Al slab (2.69 gm/cc)	Al	$6.0039 \times 10^{-2}$
	Pu-242	$6.0318 \times 10^{-7}$			
	Am-241	$1.7783 \times 10^{-6}$			
	O-16	$4.3779 \times 10^{-2}$			

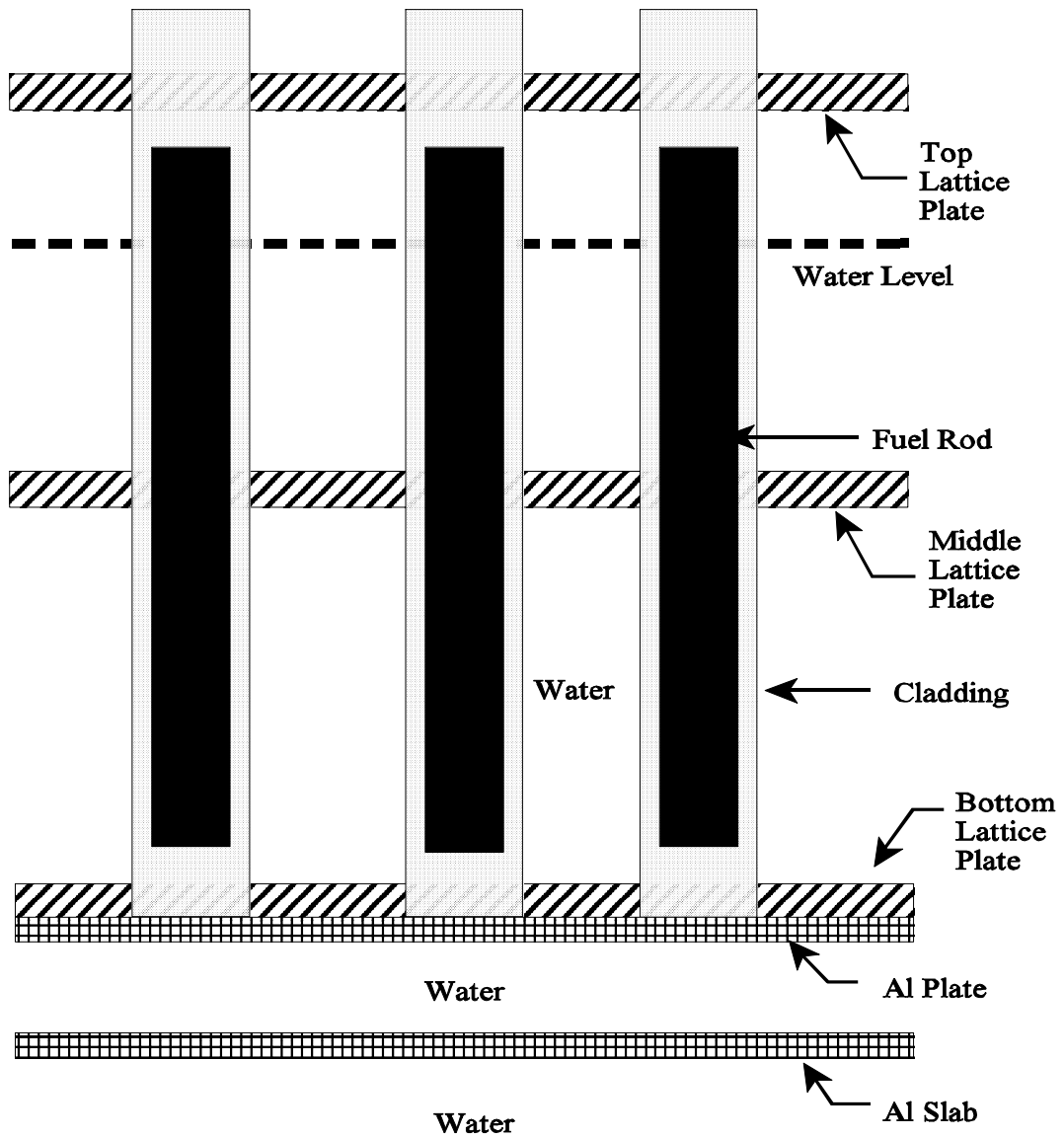


Fig. 3.1. Schematic of the SAXTON fuel rods with reflector.

Table 3.3. Moderator atom densities

Benchmark No.	Atom densities ( atoms/barn-cm )			
	H	O	B-10	B-11
SAXTON-1	$6.6643 \times 10^{-2}$	$3.3322 \times 10^{-2}$	0.0	0.0
SAXTON-2	$6.6781 \times 10^{-2}$	$3.3390 \times 10^{-2}$	0.0	0.0
SAXTON-3	$6.6751 \times 10^{-2}$	$3.3404 \times 10^{-2}$	$3.7338 \times 10^{-6}$	$1.5029 \times 10^{-5}$
SAXTON-4	$6.6673 \times 10^{-2}$	$3.3336 \times 10^{-2}$	0.0	0.0
SAXTON-5	$6.6783 \times 10^{-2}$	$3.3392 \times 10^{-2}$	0.0	0.0
SAXTON-6	$6.6737 \times 10^{-2}$	$3.3368 \times 10^{-2}$	0.0	0.0

## 3.2 ANALYSIS

All six computational benchmarks in this section were processed twice using SCALE 5.0. The set labeled NITAWL uses the NITAWL resonance processor to self-shield the resolved resonance region for all nuclides in the unit cell. An identical set, labeled CENTRM, replaces NITAWL with the CENTRM/PMC code sequence. The NITAWL and CENTRM results are then compared.

Table 3.4 contains the  $k_{eff}$  and Energy of the Average Lethargy Causing Fission (EALCF). The  $k_{eff}$  values for all the benchmark cases are very close to 1.0, the worst NITAWL benchmark being 0.68% high and the worst CENTRM case being 0.59% high. There appears to be a small negative bias between NITAWL and CENTRM, the CENTRM cases being about 0.3% lower on average than the NITAWL cases. The EALCF values listed are from the CENTRM cases. For all cases, the difference between this value for CENTRM and NITAWL was less than 0.1%. Both CENTRM and NITAWL produce excellent results for the  $k_{eff}$  and EALCF for this set of problems.

Also, calculated for each problem are the pin-power distributions; absorption,  $\langle G_f \rangle$ , and fission reaction rates and fluxes in the pin fuel, clad, and moderator; and four group cross sections and fluxes for a corner outside pin and the center pin. Each set of data is calculated using both CENTRM and NITAWL. All the data for each case are contained in the following Figs. 3.7a through 3.12b and Tables 3.5 through 3.64.

The pin-power distributions for the first problem assume 1/4th core symmetry, the pin-power distributions for the remaining problems assume 1/8th core symmetry, with a surrounding reflector in all problems. The pin-power data consist of a value and a standard deviation for each pin. The values for the pin power are actually in units of fissions per  $\text{cm}^3$ -source particle  $\times 10^{-5}$ . The value in parentheses is the percent standard deviation of the pin-power value. The pin-power distributions in the 1/8th or full-core representations are the portion of the pin covered by water. The value off to the side in the pin-power distributions represents all the fuel not covered by water. Separating the fuel rod was necessary to model this in KENO-V.a.

In most cases the CENTRM and NITAWL results for each benchmark case agree within 2 standard deviations. The peak-to-low power changes with respect to pitch. The peak-to-low power ratio initially decreased with increasing pitch, starting with a high of 2.6 for SAXTON-1 and decreasing to a low of 1.8 for SAXTON-5. A further increase in pitch, as shown in SAXTON-6,

increases the ratio to 2.5. The small pitch in SAXTON-1 and -2 cause the array to be under moderated. This under moderation results in the highest power pin being on the edge of the array and the lowest power pin being several pins in from the edge where the thermal flux is low due to lack of moderator and the fast flux is also low because it is not deep within the array.

The total fluxes, and flux ratios for the CENTRM and NITAWL cases of each benchmark case, are also in good agreement, seldom varying by more than 1%. These values are included for a corner pin and the center pin for each case. The reaction rates in the fuel and cladding are also in good agreement. However, the reaction rates for the moderator appear to be significantly different, with the CENTRM value being almost a factor of 2 higher for all cases.

Finally, four-group fluxes and cross sections were calculated for selected nuclides in the fuel region of the same corner and center pins. The macroscopic cross sections listed include the radiative capture, fission, and  $\nu$ \*fission cross sections for U-235, U-238, and Pu-239. The four groups are collapsed from the 238-group multigroup cross-section set using the flux profile calculated in KENO-V.a as follows: group 1 is from 20 MeV to 9.5 keV, group 2 is from 9.5 keV to 3.0 eV, group 3 is from 3 eV to 0.4 eV, and group 4 is from 0.4 eV to  $10^{-5}$  eV. The 0.4 eV was chosen as a boundary because it is the cadmium cutoff energy. Groups 2 and 3 contain the resolved resonance regions for most of the nuclides used in these cases. Most of the cross-section data for the CENTRM and NITAWL cases of a given benchmark case agree within 1%.

### 3.3 CONCLUSIONS

For this set of benchmark cases using either NITAWL and CENTRM as the resonance region processor produces acceptable results of the  $k_{eff}$  values. All other values produced using CENTRM and NITAWL are also consistent with each. For all cases, the  $k_{eff}$ 's produced using CENTRM are slightly lower (~0.3%) than those produced using NITAWL to do the resonance self-shielding. As a result the average  $k_{eff}$  of all the CENTRM cases is closer to 1.0 than the average  $k_{eff}$  of all the NITAWL cases for this set of benchmarks. The pin-power distributions, fluxes, most reactions rates, and macroscopic cross sections generally agree to approximately 1% between CENTRM and NITAWL. The only significant discrepancy is the absorption reaction rate for the moderator. CENTRM calculates a value that is about a factor of 2 higher than the same value using NITAWL.

Table 3.4 Comparison of  $k_{eff}$  and EALCF from CENTRM and NITAWL<sup>a</sup>

CASE MIX-COMP-THERM-3	NITAWL $k_{eff} (\pm F)$	CENTRM $k_{eff} (\pm F)$	% DIFF	EALCF ( eV )
SAXTON-1	1.0046 (0.0005)	1.0007 (0.0004)	-0.39	0.881
SAXTON-2	1.0058 (0.0004)	1.0012 (0.0004)	-0.46	0.537
SAXTON-3	1.0054 (0.0004)	1.0017 (0.0004)	-0.37	0.633
SAXTON-4	1.0056 (0.0004)	1.0029 (0.0004)	-0.27	0.186
SAXTON-5	1.0062 (0.0004)	1.0035 (0.0004)	-0.27	0.154
SAXTON-6	1.0068 (0.0005)	1.0059 (0.0004)	-0.09	0.100

<sup>a</sup>Value in parentheses is percent standard deviation.



121	122	123	124	125	126	127	128	129	130	131	132
109	110	111	112	113	114	115	116	117	118	119	120
97	98	99	100	101	102	103	104	105	106	107	108
85	86	87	88	89	90	91	92	93	94	95	96
73	74	75	76	77	78	79	80	81	82	83	84
61	62	63	64	65	66	67	68	69	70	71	72
49	50	51	52	53	54	55	56	57	58	59	60
37	38	39	40	41	42	43	44	45	46	47	48
25	26	27	28	29	30	31	32	33	34	35	36
13	14	15	16	17	18	19	20	21	22	23	24
1	2	3	4	5	6	7	8	9	10	11	12

Fig.3.2. Pin layout of benchmark case SAXTON-1.

									55
								53	54
							50	51	52
						46	47	48	49
					41	42	43	44	45
			35	36	37	38	39	40	
		28	29	30	31	32	33	34	
	20	21	22	23	24	25	26	27	
	11	12	13	14	15	16	17	18	19
1	2	3	4	5	6	7	8	9	10

Fig. 3.3. Pin layout of benchmark case SAXTON-2.

										66
									64	65
								61	62	63
							57	58	59	60
						52	53	54	55	56
				46	47	48	49	50	51	
			39	40	41	42	43	44	45	
		31	32	33	34	35	36	37	38	
		22	23	24	25	26	27	28	29	30
	12	13	14	15	16	17	18	19	20	21
1	2	3	4	5	6	7	8	9	10	11

Fig. 3.4. Pin layout of benchmark case SAXTON-3.

						28
					26	27
				23	24	25
			19	20	21	22
		14	15	16	17	18
	8	9	10	11	12	13
1	2	3	4	5	6	7

Fig. 3.5. Pin layout of benchmark case SAXTON-4.

					21
				19	20
			16	17	18
		12	13	14	15
	7	8	9	10	11
1	2	3	4	5	6

Fig. 3.6. Pin layout of benchmark cases SAXTON-5 and 6.

						0.150 (0.73)						
6.485 (0.53)	3.658 (0.59)	3.513 (0.64)	3.704 (0.60)	3.968 (0.55)	4.199 (0.57)	4.486 (0.55)	4.633 (0.49)	4.770 (0.54)	4.894 (0.55)	4.914 (0.50)	4.971 (0.73)	
6.446 (0.50)	3.716 (0.58)	3.461 (0.61)	3.693 (0.61)	3.957 (0.59)	4.222 (0.55)	4.421 (0.57)	4.570 (0.57)	4.687 (0.51)	4.871 (0.51)	4.858 (0.53)	4.962 (0.66)	
6.319 (0.48)	3.630 (0.63)	3.434 (0.62)	3.601 (0.61)	3.837 (0.54)	4.133 (0.57)	4.381 (0.56)	4.493 (0.49)	4.664 (0.56)	4.782 (0.56)	4.846 (0.52)	4.847 (0.71)	
6.148 (0.50)	3.531 (0.62)	3.368 (0.59)	3.524 (0.66)	3.729 (0.56)	3.986 (0.58)	4.175 (0.52)	4.397 (0.55)	4.503 (0.50)	4.649 (0.51)	4.680 (0.52)	4.705 (0.75)	
5.884 (0.49)	3.410 (0.63)	3.176 (0.67)	3.433 (0.59)	3.686 (0.59)	3.876 (0.58)	4.087 (0.61)	4.247 (0.55)	4.338 (0.54)	4.491 (0.54)	4.514 (0.53)	4.556 (0.75)	
5.635 (0.50)	3.234 (0.67)	3.058 (0.64)	3.231 (0.66)	3.496 (0.60)	3.668 (0.54)	3.879 (0.60)	4.029 (0.57)	4.171 (0.52)	4.254 (0.57)	4.283 (0.51)	4.344 (0.75)	
5.340 (0.53)	3.066 (0.66)	2.898 (0.63)	3.037 (0.71)	3.280 (0.62)	3.477 (0.56)	3.662 (0.61)	3.794 (0.59)	3.908 (0.61)	4.018 (0.57)	4.067 (0.56)	4.085 (0.75)	
4.988 (0.55)	2.822 (0.70)	2.693 (0.72)	2.864 (0.66)	3.054 (0.70)	3.264 (0.61)	3.412 (0.61)	3.552 (0.61)	3.652 (0.59)	3.747 (0.59)	3.772 (0.58)	3.830 (0.84)	
4.609 (0.58)	4.609 (0.67)	2.520 (0.72)	2.716 (0.71)	2.878 (0.67)	3.057 (0.67)	3.187 (0.62)	3.360 (0.58)	3.473 (0.62)	3.531 (0.59)	3.574 (0.70)	3.571 (0.88)	
4.611 (0.62)	2.773 (0.75)	2.701 (0.67)	2.827 (0.68)	3.079 (0.65)	3.255 (0.69)	3.427 (0.66)	3.557 (0.63)	3.717 (0.60)	3.757 (0.54)	3.81 (0.62)	3.815 (0.88)	
6.090 (0.50)	4.599 (0.56)	4.683 (0.52)	5.010 (0.56)	5.313 (0.51)	5.712 (0.53)	5.943 (0.52)	6.227 (0.49)	6.425 (0.51)	6.539 (0.50)	6.636 (0.48)	6.635 (0.67)	

Fig. 3.7a. Pin-power distribution for CENTRM benchmark SAXTON-1. Value in parentheses is the percent standard deviation.

						4.967 (0.78)						
6.502 (0.50)	3.746 (0.64)	3.555 (0.60)	3.711 (0.62)	4.013 (0.54)	4.274 (0.56)	4.457 (0.58)	4.689 (0.54)	4.801 (0.55)	4.913 (0.55)	4.997 (0.49)	4.967 (0.78)	
6.441 (0.49)	3.706 (0.59)	3.493 (0.67)	3.699 (0.65)	3.939 (0.63)	4.244 (0.56)	4.422 (0.53)	4.641 (0.55)	4.780 (0.55)	4.840 (0.51)	4.917 (0.49)	4.912 (0.74)	
6.347 (0.45)	3.634 (0.54)	3.368 (0.65)	3.599 (0.59)	3.884 (0.61)	4.115 (0.57)	4.390 (0.51)	4.502 (0.52)	4.684 (0.54)	4.757 (0.56)	4.854 (0.51)	4.879 (0.78)	
6.197 (0.52)	3.522 (0.63)	3.356 (0.64)	3.356 (0.59)	3.836 (0.60)	4.052 (0.56)	4.279 (0.57)	4.446 (0.54)	4.547 (0.54)	4.614 (0.55)	4.711 (0.49)	4.737 (0.76)	
5.882 (0.52)	3.391 (0.62)	3.212 (0.63)	3.408 (0.64)	3.685 (0.61)	3.868 (0.56)	4.112 (0.57)	4.229 (0.55)	4.343 (0.49.)	4.500 (0.54)	4.497 (0.57)	4.520 (0.76)	
5.619 (0.54)	3.243 (0.70)	3.060 (0.66)	3.260 (0.61)	3.477 (0.64)	3.708 (0.59)	3.880 (0.57)	4.050 (0.60)	4.189 (0.60)	4.265 (0.55)	4.321 (0.58)	4.305 (0.71)	
5.353 (0.51)	3.065 (0.67)	2.880 (0.64)	3.041 (0.64)	3.296 (0.66)	3.479 (0.62)	3.650 (0.59)	3.879 (0.60)	3.922 (0.67)	3.990 (0.52)	4.087 (0.54)	4.126 (0.78)	
4.982 (0.54)	2.844 (0.73)	2.673 (0.69)	2.857 (0.73)	3.063 (0.66)	3.264 (0.62)	3.422 (0.68)	3.577 (0.62)	3.698 (0.59)	3.787 (0.62)	3.847 (0.59)	3.823 (0.83)	
4.689 (0.60)	2.684 (0.76)	2.526 (0.71)	2.697 (0.68)	2.904 (0.69)	3.064 (0.68)	3.243 (0.65)	3.361 (0.64)	3.478 (0.62)	3.538 (0.61)	3.578 (0.63)	3.626 (0.89)	
4.621 (0.58)	2.801 (0.72)	2.677 (0.75)	2.839 (0.78)	3.079 (0.61)	3.258 (0.64)	3.417 (0.65)	3.558 (0.61)	3.735 (0.53)	3.801 (0.60)	3.882 (0.63)	3.872 (0.86)	
6.047 (0.48)	4.602 (0.56)	4.618 (0.58)	4.932 (0.58)	5.360 (0.51)	5.681 (0.53)	6.037 (0.46)	6.282 (0.44)	6.440 (0.48)	6.562 (0.47)	6.694 (0.48)	6.750 (0.68)	

Fig. 3.7b. Pin-power distribution for NITAWL benchmark SAXTON-1. Value in parentheses is the percent standard deviation.

Table 3.5. SAXTON-1 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	3.400E-05	6.075E-05	2.123E-05	7.209E-03	0.344
	Clad	3.137E-07	0.0	0.0	2.114E-03	0.101
	Mod.	1.303E-06	0.0	0.0	1.162E-02	0.555
132	Fuel	3.446E-05	5.001E-05	1.747E-05	1.905E-02	0.339
	Clad	5.304E-07	0.0	0.0	5.690E-03	0.101
	Mod.	9.171E-07	0.0	0.0	3.141E-02	0.559

Table 3.6. SAXTON-1 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	3.407E-05	6.097E-05	2.131E-05	7.160E-03	0.344
	Clad	3.038E-07	0.0	0.0	2.102E-03	0.101
	Mod.	6.505E-07	0.0	0.0	1.157E-02	0.556
132	Fuel	3.445E-05	4.998E-05	1.746E-05	1.895E-02	0.338
	Clad	5.131E-07	0.0	0.0	5.682E-03	0.101
	Mod.	4.648E-07	0.0	0.0	3.143E-02	0.561

Table 3.7. SAXTON-1, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^2 \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^2 \cdot \text{s}^{-1}$ )
1	9.920E-05	9.850E-05
2	2.598E-05	2.555E-05
3	5.448E-06	5.416E-06
4	2.012E-05	2.026E-05

Table 3.8. SAXTON-1, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.32297E-04	5.28702E-04	2.03588E-04	2.31560E-04	5.28129E-04	2.03214E-04
2	5.36940E-03	8.29315E-03	3.40344E-03	5.43045E-03	8.32423E-03	3.41618E-03
3	7.84363E-03	1.58948E-02	6.52311E-03	7.88612E-03	1.60166E-02	6.57304E-03
4	7.43305E-02	1.54727E-01	6.34985E-02	7.41841E-02	1.54426E-01	6.33751E-02

Table 3.9. SAXTON-1, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.21435E-03	1.34429E-02	4.77316E-03	7.22446E-03	1.35539E-02	4.80883E-03
2	5.31239E-02	5.82914E-06	2.41498E-06	5.09276E-02	5.71143E-06	2.36622E-06
3	1.12361E-02	3.85156E-08	1.59577E-08	1.12440E-02	3.86270E-08	1.60039E-08
4	4.26642E-02	2.00382E-07	8.30224E-08	4.25934E-02	2.00045E-07	8.28825E-08

Table 3.10. SAXTON-1, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.51521E-03	7.34395E-03	2.36412E-03	2.51413E-03	7.35233E-03	2.36542E-03
2	4.31528E-02	7.26582E-02	2.52301E-02	4.23284E-02	7.17029E-02	2.48984E-02
3	1.42157E-01	2.82164E-01	9.79800E-02	1.43048E-01	2.83783E-01	9.85430E-02
4	1.26177E+00	2.54082E+00	8.78966E-01	1.25963E+00	2.53651E+00	8.77483E-01

Table 3.11. SAXTON-1, Pin-132 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.750E-04	2.726E-04
2	9.570E-05	9.640E-05
3	1.651E-05	1.607E-05
4	1.110E-05	1.112E-05

Table 3.12. SAXTON-1, Pin-132 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	2.45122E-04	5.39109E-04	2.10038E-04	2.44993E-04	5.38844E-04	2.09938E-04
2	5.15441E-03	7.97880E-03	3.27443E-03	5.09111E-03	7.85028E-03	3.22168E-03
3	7.58571E-03	1.52693E-02	6.26638E-03	7.63367E-03	1.54170E-02	6.32701E-03
4	6.21247E-02	1.28918E-01	5.29069E-02	6.23526E-02	1.29385E-01	5.30985E-02

Table 3.13. SAXTON-1, Pin-132 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	6.80382E-03	1.10027E-02	3.91622E-03	6.78188E-03	1.09576E-02	3.89839E-03
2	4.89435E-02	6.26429E-06	2.59527E-06	4.75272E-02	6.04762E-06	2.50550E-06
3	1.11343E-02	3.75412E-08	1.55540E-08	1.11699E-02	3.77752E-08	1.56510E-08
4	3.63750E-02	1.70185E-07	7.05107E-08	3.64831E-02	1.70704E-07	7.07262E-08

Table 3.14. SAXTON-1, Pin-132 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	2.52991E-03	7.17411E-03	2.33467E-03	2.52913E-03	7.17146E-03	2.33393E-03
2	4.10734E-02	6.89915E-02	2.39569E-02	3.95781E-02	6.68722E-02	2.32210E-02
3	1.30973E-01	2.61059E-01	9.06517E-02	1.35790E-01	2.70087E-01	9.37866E-02
4	1.45288E+00	2.78304E+00	9.63703E-01	1.45769E+00	2.79201E+00	9.66808E-01



									7.032 (0.91)
								7.088 (0.42)	7.085 (0.46)
							6.809 (0.46)	6.904 (0.32)	6.960 (0.49)
						6.408 (0.49)	6.587 (0.33)	6.701 (0.33)	6.721 (0.48)
				5.874 (0.49)	6.137 (0.35)	6.268 (0.37)	6.459 (0.35)	6.431 (0.48)	
			5.267 (0.53)	5.498 (0.34)	5.807 (0.36)	5.922 (0.34)	6.082 (0.36)	6.127 (0.49)	
		4.501 (0.61)	4.877 (0.40)	5.169 (0.39)	5.362 (0.37)	5.580 (0.37)	5.629 (0.38)	5.695 (0.52)	
	3.937 (0.61)	4.239 (0.41)	4.533 (0.40)	4.826 (0.42)	5.017 (0.39)	5.191 (0.39)	5.256 (0.37)	5.308 (0.56)	
	4.056 (0.65)	4.036 (0.42)	4.308 (0.40)	4.628 (0.40)	4.898 (0.37)	5.101 (0.39)	5.261 (0.38)	5.374 (0.35)	5.422 (0.51)
7.779 (0.47)	6.169 (0.37)	6.394 (0.34)	6.876 (0.36)	7.378 (0.34)	7.815 (0.30)	8.167 (0.33)	8.417 (0.30)	8.574 (0.31)	8.669 (0.41)

Fig. 3.8a. Pin-power distribution for CENTRM benchmark SAXTON-2. Value in parentheses is percent standard deviation.

0.172 (0.72)									7.111 (0.85)
								7.073 (0.45)	7.107 (0.46)
							6.803 (0.46)	6.929 (0.32)	7.015 (0.47)
						6.476 (0.49)	6.655 (0.35)	6.786 (0.34)	6.773 (0.44)
				5.890 (0.52)	6.194 (0.36)	6.362 (0.34)	6.449 (0.34)	6.504 (0.46)	
			5.255 (0.53)	5.527 (0.39)	5.826 (0.36)	5.985 (0.35)	6.159 (0.37)	6.139 (0.50)	
		4.556 (0.57)	4.871 (0.39)	5.198 (0.36)	5.449 (0.38)	5.562 (0.37)	5.690 (0.38)	5.706 (0.48)	
	3.988 (0.57)	4.229 (0.40)	4.534 (0.40)	4.839 (0.40)	5.022 (0.42)	5.209 (0.39)	5.298 (0.39)	5.338 (0.54)	
	4.073 (0.62)	3.989 (0.46)	4.314 (0.38)	4.651 (0.40)	4.909 (0.36)	5.172 (0.39)	5.260 (0.40)	5.401 (0.36)	5.401 (0.48)
7.878 (0.40)	6.193 (0.34)	6.355 (0.33)	6.870 (0.34)	7.353 (0.32)	7.839 (0.32)	8.201 (0.30)	8.457 (0.29)	8.657 (0.29)	8.684 (0.44)

Fig. 3.8b. Pin-power distribution for NITAWL benchmark SAXTON-2. Value in parentheses is percent standard deviation.

Table 3.15. SAXTON-2 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	4.361E-05	7.811E-05	2.729E-05	8.590E-03	0.296
	Clad	3.882E-07	0.0	0.0	2.531E-03	0.087
	Mod.	1.731E-06	0.0	0.0	1.793E-02	0.617
55	Fuel	4.675E-05	7.033E-05	2.457E-05	2.148E-02	0.293
	Clad	6.310E-07	0.0	0.0	6.403E-03	0.087
	Mod.	1.351E-06	0.0	0.0	4.552E-02	0.620

Table 3.16. SAXTON-2 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	4.393E-05	7.895E-05	2.759E-05	8.596E-03	0.296
	Clad	3.874E-07	0.0	0.0	2.523E-03	0.087
	Mod.	8.732E-07	0.0	0.0	1.790E-02	0.617
55	Fuel	4.723E-05	7.130E-05	2.491E-05	2.145E-02	0.292
	Clad	6.079E-07	0.0	0.0	6.411E-03	0.087
	Mod.	6.803E-07	0.0	0.0	4.565E-02	0.621

Table 3.17. SAXTON-2, Pin-1 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	1.210E-04	1.209E-04
2	3.068E-05	3.075E-05
3	6.650E-06	6.426E-06
4	2.598E-05	2.635E-05

Table 3.18. SAXTON-2, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	2.31295E-04	5.28168E-04	2.03137E-04	2.31046E-04	5.27611E-04	2.02942E-04
2	5.50818E-03	8.46995E-03	3.47598E-03	5.34062E-03	8.20683E-03	3.36800E-03
3	7.88307E-03	1.60481E-02	6.58600E-03	7.88335E-03	1.59830E-02	6.55932E-03
4	7.48945E-02	1.55911E-01	6.39846E-02	7.47985E-02	1.55708E-01	6.39009E-02

Table 3.19. SAXTON-2, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	7.27299E-03	1.37200E-02	4.87017E-03	7.25772E-03	1.36913E-02	4.86098E-03
2	5.45685E-02	6.04055E-06	2.50257E-06	5.15366E-02	5.85011E-06	2.42368E-06
3	1.12498E-02	3.86744E-08	1.60235E-08	1.12126E-02	3.84197E-08	1.59180E-08
4	4.29376E-02	2.01691E-07	8.35643E-08	4.28896E-02	2.01461E-07	8.34691E-08

Table 3.20. SAXTON-2, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	2.51538E-03	7.36394E-03	2.36798E-03	2.51302E-03	7.35725E-03	2.36609E-03
2	4.36441E-02	7.27138E-02	2.52495E-02	4.25694E-02	7.20315E-02	2.50126E-02
3	1.44153E-01	2.85821E-01	9.92499E-02	1.40219E-01	2.78403E-01	9.66744E-02
4	1.26117E+00	2.54337E+00	8.79827E-01	1.26115E+00	2.54272E+00	8.79601E-01

Table 3.21. SAXTON-2, Pin-55 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	3.168E-04	3.145E-04
2	1.074E-04	1.086E-04
3	1.945E-05	1.953E-05
4	1.722E-05	1.751E-05

Table 3.22 SAXTON-2, Pin-55 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$
1	2.42818E-04	5.37235E-04	2.08871E-04	2.42331E-04	5.36480E-04	2.08578E-04
2	5.28301E-03	8.16913E-03	3.35254E-03	5.21227E-03	8.02944E-03	3.29521E-03
3	7.65558E-03	1.53980E-02	6.31918E-03	7.58530E-03	1.53401E-02	6.29544E-03
4	6.42364E-02	1.33386E-01	5.47403E-02	6.47836E-02	1.34511E-01	5.52022E-02

Table 3.23. SAXTON-2, Pin-55 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$
1	6.89564E-03	1.14866E-02	4.08747E-03	6.87320E-03	1.14586E-02	4.07844E-03
2	5.10445E-02	5.98081E-06	2.47782E-06	5.07872E-02	5.96084E-06	2.46955E-06
3	1.11261E-02	3.76231E-08	1.55879E-08	1.11419E-02	3.76606E-08	1.56035E-08
4	3.74682E-02	1.75440E-07	7.26882E-08	3.77212E-02	1.76632E-07	7.31816E-08

Table 3.24. SAXTON-2, Pin-55 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$	$\underline{G_a}$	$\langle G_f \rangle$	$\underline{G_f}$
1	2.52700E-03	7.20417E-03	2.33954E-03	2.52549E-03	7.20372E-03	2.33961E-03
2	4.23034E-02	7.11892E-02	2.47201E-02	4.01978E-02	6.76656E-02	2.34965E-02
3	1.33769E-01	2.66117E-01	9.24077E-02	1.31144E-01	2.61407E-01	9.07727E-02
4	1.41690E+00	2.73612E+00	9.47311E-01	1.43265E+00	2.76589E+00	9.57596E-01

0.186 (0.99)										5.900 (0.99)
									5.929 (0.48)	5.958 (0.50)
								5.672 (0.51)	5.819 (0.31)	5.884 (0.49)
							5.436 (0.48)	5.585 (0.33)	5.666 (0.33)	5.630 (0.49)
						5.000 (0.54)	5.206 (0.35)	5.373 (0.33)	5.425 (0.33)	5.486 (0.55)
				4.473 (0.49)	4.718 (0.35)	4.935 (0.37)	5.060 (0.34)	5.148 (0.34)	5.191 (0.55)	
			3.921 (0.58)	4.189 (0.42)	4.440 (0.38)	4.590 (0.38)	4.750 (0.36)	4.833 (0.34)	4.836 (0.52)	
		3.331 (0.66)	3.599 (0.45)	3.842 (0.38)	4.096 (0.43)	4.271 (0.41)	4.357 (0.41)	4.399 (0.42)	4.447 (0.52)	
	2.821 (0.75)	3.029 (0.47)	3.314 (0.50)	3.555 (0.43)	3.722 (0.39)	3.898 (0.40)	3.976 (0.39)	4.078 (0.39)	4.096 (0.57)	
	2.693 (0.80)	2.750 (0.51)	2.987 (0.44)	3.235 (0.47)	3.464 (0.40)	3.672 (0.41)	3.860 (0.41)	3.906 (0.40)	3.977 (0.41)	3.972 (0.56)
4.495 (0.57)	3.726 (0.48)	3.956 (0.41)	4.320 (0.37)	4.667 (0.37)	5.028 (0.37)	5.272 (0.37)	5.506 (0.38)	5.679 (0.38)	5.763 (0.36)	5.781 (0.51)

Fig. 3.9a. Pin-power distribution for CENTRM benchmark SAXTON-3. Value in parentheses is percent standard deviation.

0.187 (1.06)										5.920 (1.07)
									5.932 (0.47)	5.983 (0.45)
								5.779 (0.48)	5.826 (0.33)	5.906 (0.48)
							5.446 (0.46)	5.598 (0.33)	5.704 (0.33)	5.705 (0.45)
						5.019 (0.56)	5.257 (0.36)	5.406 (0.36)	5.478 (0.36)	5.496 (0.47)
					4.482 (0.54)	4.743 (0.40)	4.946 (0.34)	5.088 (0.35)	5.205 (0.34)	5.195 (0.51)
				3.988 (0.58)	4.209 (0.38)	4.447 (0.36)	4.582 (0.37)	4.738 (0.36)	4.822 (0.36)	4.866 (0.54)
			3.317 (0.60)	3.625 (0.44)	3.856 (0.39)	4.081 (0.38)	4.245 (0.37)	4.400 (0.36)	4.439 (0.34)	4.515 (0.51)
		2.787 (0.67)	3.058 (0.48)	3.340 (0.44)	3.557 (0.45)	3.734 (0.42)	3.912 (0.43)	4.022 (0.39)	4.049 (0.41)	4.134 (0.59)
	2.676 (0.74)	2.740 (0.51)	3.007 (0.46)	3.254 (0.49)	3.491 (0.42)	3.663 (0.47)	3.821 (0.42)	3.954 (0.42)	4.004 (0.43)	4.050 (0.61)
4.515 (0.53)	3.758 (0.45)	3.949 (0.41)	4.335 (0.40)	4.695 (0.39)	5.019 (0.36)	5.313 (0.36)	5.493 (0.38)	5.685 (0.38)	5.746 (0.34)	5.823 (0.46)

Fig. 3.9b. Pin-power distribution for NITAWL benchmark SAXTON-3. Value in parentheses is percent standard deviation.

Table 3.25. SAXTON-3 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	2.543E-05	4.469E-05	1.562E-05	6.051E-03	0.295
	Clad	2.340E-07	0.0	0.0	1.781E-03	0.087
	Mod.	1.588E-06	0.0	0.0	1.266E-02	0.618
66	Fuel	3.944E-05	5.901E-05	2.061E-05	1.985E-02	0.292
	Clad	5.323E-07	0.0	0.0	5.950E-03	0.087
	Mod.	1.782E-06	0.0	0.0	4.227E-02	0.621

Table 3.26. SAXTON-3 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	2.574E-05	4.529E-05	1.589E-05	6.060E-03	0.295
	Clad	2.313E-07	0.0	0.0	1.785E-03	0.087
	Mod.	7.923E-07	0.0	0.0	1.270E-02	0.618
66	Fuel	3.956E-05	5.952E-05	2.079E-05	1.999E-02	0.293
	Clad	5.281E-07	0.0	0.0	5.968E-03	0.087
	Mod.	8.857E-07	0.0	0.0	4.235E-02	0.620



Table 3.27. SAXTON-3, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	7.796E-05	7.800E-05
2	2.181E-05	2.192E-05
3	4.829E-06	4.689E-06
4	1.453E-05	1.470E-05

Table 3.28. SAXTON-3, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$G_a$	$\langle G_f \rangle$	$G_f$	$G_a$	$\langle G_f \rangle$	$G_f$
1	2.32521E-04	5.28612E-04	2.03658E-04	2.32862E-04	5.29454E-04	2.03931E-04
2	5.50005E-03	8.43228E-03	3.46053E-03	5.39193E-03	8.28878E-03	3.40165E-03
3	7.92452E-03	1.60789E-02	6.59865E-03	7.90441E-03	1.60146E-02	6.57223E-03
4	7.31686E-02	1.52279E-01	6.24939E-02	7.33599E-02	1.52663E-01	6.26517E-02

Table 3.29. SAXTON-3, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$G_a$	$\langle G_f \rangle$	$G_f$	$G_a$	$\langle G_f \rangle$	$G_f$
1	7.20136E-03	1.33762E-02	4.75174E-03	7.23290E-03	1.34483E-02	4.77628E-03
2	5.41784E-02	5.69922E-06	2.36116E-06	5.29886E-02	5.86670E-06	2.43054E-06
3	1.12448E-02	3.86080E-08	1.59959E-08	1.12161E-02	3.84319E-08	1.59231E-08
4	4.20736E-02	1.97550E-07	8.18486E-08	4.21529E-02	1.97922E-07	8.20034E-08

Table 3.30. SAXTON-3, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$G_a$	$\langle G_f \rangle$	$G_f$	$G_a$	$\langle G_f \rangle$	$G_f$
1	2.51444E-03	7.33436E-03	2.36219E-03	2.51691E-03	7.34278E-03	2.36421E-03
2	4.43213E-02	7.47680E-02	2.59628E-02	4.17771E-02	7.10830E-02	2.46832E-02
3	1.44573E-01	2.86496E-01	9.94842E-02	1.40383E-01	2.78776E-01	9.68036E-02
4	1.27177E+00	2.55010E+00	8.82257E-01	1.28214E+00	2.56855E+00	8.88646E-01

Table 3.31. SAXTON-3, Pin-66 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	2.666E-04	2.684E-04
2	9.313E-05	9.364E-05
3	1.707E-05	1.685E-05
4	1.407E-05	1.456E-05

Table 3.32. SAXTON-3, Pin-66 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.42733E-04	5.37472E-04	2.08870E-04	2.43387E-04	5.37876E-04	2.09178E-04
2	5.30011E-03	8.16540E-03	3.35100E-03	5.27422E-03	8.12879E-03	3.33598E-03
3	7.70943E-03	1.55532E-02	6.38289E-03	7.67703E-03	1.54383E-02	6.33579E-03
4	6.52259E-02	1.35439E-01	5.55832E-02	6.49576E-02	1.34906E-01	5.53641E-02

Table 3.33. SAXTON-3, Pin-66 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	6.92119E-03	1.15793E-02	4.11808E-03	6.86967E-03	1.13727E-02	4.04314E-03
2	5.09692E-02	6.02439E-06	2.49588E-06	4.92231E-02	6.08021E-06	2.51901E-06
3	1.11677E-02	3.78609E-08	1.56865E-08	1.11602E-02	3.77671E-08	1.56476E-08
4	3.79241E-02	1.77598E-07	7.35821E-08	3.78323E-02	1.77181E-07	7.34093E-08

Table 3.34. SAXTON-3, Pin-66 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.52720E-03	7.21032E-03	2.34053E-03	2.52750E-03	7.19788E-03	2.33835E-03
2	4.12518E-02	6.95573E-02	2.41534E-02	4.03271E-02	6.74581E-02	2.34245E-02
3	1.37500E-01	2.73101E-01	9.48330E-02	1.37757E-01	2.73564E-01	9.49941E-02
4	1.43800E+00	2.77757E+00	9.61635E-01	1.41120E+00	2.73126E+00	9.45577E-01

						0.218 (0.73)														18.89 (0.69)						
																				18.60 (0.33)	18.82 (0.36)					
																				17.23 (0.35)	17.81 (0.24)	18.18 (0.33)				
																				14.90 (0.35)	16.09 (0.26)	16.9 (0.26)	16.95 (0.35)			
																				12.39 (0.38)	13.62 (0.29)	14.58 (0.24)	15.18 (0.25)	15.37 (0.38)		
																				10.54 (0.30)	11.44 (0.28)	12.55 (0.28)	13.40 (0.26)	13.91 (0.27)	14.11 (0.40)	
																				13.71 (0.41)	12.57 (0.29)	13.86 (0.29)	15.06 (0.26)	16.18 (0.25)	16.83 (0.25)	17.04 (0.30)

Fig. 3.10a. Pin-power distribution for CENTRM benchmark SAXTON-4. Value in parentheses is percent standard deviation.

																																							19.22 (0.63)						
																																						18.69 (0.34)	18.74 (0.33)						
																																						17.22 (0.35)	17.97 (0.23)	18.11 (0.32)					
																																						15.01 (0.37)	16.06 (0.26)	16.70 (0.24)	16.94 (0.35)				
																																							12.38 (0.42)	13.63 (0.29)	14.56 (0.25)	15.19 (0.26)	15.46 (0.37)		
																																							10.58 (0.45)	11.45 (0.28)	12.55 (0.30)	13.47 (0.29)	14.02 (0.27)	14.19 (0.39)	
																																							13.72 (0.38)	12.61 (0.27)	13.89 (0.27)	15.18 (0.25)	16.16 (0.28)	16.86 (0.24)	17.12 (0.33)

Fig. 3.10b. Pin-power distribution for NITAWL benchmark SAXTON-4. Value in parentheses is percent standard deviation.

Table 3.35. SAXTON-4 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	7.531E-05	1.363E-04	4.765E-05	1.085E-02	0.172
	Clad	6.208E-07	0.0	0.0	3.159E-03	0.050
	Mod.	3.325E-06	0.0	0.0	4.911E-02	0.778
28	Fuel	1.133E-04	1.888E-04	6.597E-05	2.644E-02	0.170
	Clad	1.093E-06	0.0	0.0	7.857E-03	0.051
	Mod.	4.152E-06	0.0	0.0	1.212E-01	0.779

Table 3.36. SAXTON-4 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	7.555E-05	1.372E-04	4.796E-05	1.091E-02	0.172
	Clad	6.298E-07	0.0	0.0	3.186E-03	0.050
	Mod.	1.677E-06	0.0	0.0	4.926E-02	0.778
28	Fuel	1.153E-04	1.923E-04	6.721E-05	2.661E-02	0.171
	Clad	1.090E-06	0.0	0.0	7.874E-03	0.050
	Mod.	2.076E-06	0.0	0.0	1.214E-01	0.779

Table 3.37. SAXTON-4, Pin-1 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	1.767E-04	1.772E-04
2	4.238E-05	4.314E-05
3	9.788E-06	9.606E-06
4	4.606E-05	4.644E-05

Table 3.38. SAXTON-4, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.28768E-04	5.25936E-04	2.01824E-04	2.28888E-04	5.26218E-04	2.01905E-04
2	5.58388E-03	8.56052E-03	3.51317E-03	5.50211E-03	8.45190E-03	3.46859E-03
3	8.12596E-03	1.65337E-02	6.78529E-03	8.00644E-03	1.62619E-02	6.67374E-03
4	7.52875E-02	1.56735E-01	6.43226E-02	7.54139E-02	1.57003E-01	6.44324E-02

Table 3.39. SAXTON-4, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.34533E-03	1.41658E-02	5.02602E-03	7.35536E-03	1.41852E-02	5.03150E-03
2	5.77836E-02	6.06902E-06	2.51437E-06	5.53505E-02	5.94471E-06	2.46287E-06
3	1.12800E-02	3.90072E-08	1.61613E-08	1.12638E-02	3.87636E-08	1.60605E-08
4	4.31348E-02	2.02633E-07	8.39546E-08	4.31960E-02	2.02927E-07	8.40764E-08

Table 3.40. SAXTON-4, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.51088E-03	7.39032E-03	2.37191E-03	2.51148E-03	7.39283E-03	2.37221E-03
2	4.48570E-02	7.50776E-02	2.60703E-02	4.28458E-02	7.19822E-02	2.49954E-02
3	1.48740E-01	2.94317E-01	1.02200E-01	1.46544E-01	2.90227E-01	1.00780E-01
4	1.25958E+00	2.54316E+00	8.79726E-01	1.25886E+00	2.54285E+00	8.79615E-01

Table 3.41. SAXTON-4, Pin-28 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	4.435E-04	4.456E-04
2	1.401E-04	1.409E-04
3	2.995E-05	2.997E-05
4	5.644E-05	5.789E-05

Table 3.42. SAXTON-4, Pin-28 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.37576E-04	5.33610E-04	2.06345E-04	2.36654E-04	5.32933E-04	2.05880E-04
2	5.42624E-03	8.34946E-03	3.42656E-03	5.49204E-03	8.44613E-03	3.46621E-03
3	8.00180E-03	1.62249E-02	6.65856E-03	7.91521E-03	1.60134E-02	6.57174E-03
4	7.09472E-02	1.47553E-01	6.05542E-02	7.02795E-02	1.46150E-01	5.99789E-02

Table 3.43. SAXTON-4, Pin-28 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	7.11109E-03	1.26244E-02	4.48453E-03	7.14856E-03	1.28317E-02	4.55624E-03
2	5.52425E-02	5.99818E-06	2.48502E-06	5.40680E-02	5.89807E-06	2.44355E-06
3	1.12522E-02	3.86845E-08	1.60276E-08	1.12054E-02	3.82593E-08	1.58516E-08
4	4.09068E-02	1.91933E-07	7.95213E-08	4.05719E-02	1.90337E-07	7.88606E-08

Table 3.44. SAXTON-4, Pin-28 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.52286E-03	7.28582E-03	2.35416E-03	2.52139E-03	7.29800E-03	2.35595E-03
2	4.55287E-02	7.65767E-02	2.65909E-02	4.36759E-02	7.33527E-02	2.54713E-02
3	1.45672E-01	2.88541E-01	1.00195E-01	1.41609E-01	2.80817E-01	9.75128E-02
4	1.32655E+00	2.62741E+00	9.09199E-01	1.32947E+00	2.62807E+00	9.09471E-01



Table 3.45. SAXTON-5 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	7.340E-05	1.334E-04	4.665E-05	1.142E-02	0.148
	Clad	6.001E-07	0.0	0.0	3.327E-03	0.043
	Mod.	3.369E-06	0.0	0.0	6.246E-02	0.809
21	Fuel	1.175E-04	2.005E-04	7.008E-05	2.753E-02	0.147
	Clad	1.081E-06	0.0	0.0	8.169E-03	0.043
	Mod.	4.571E-06	0.0	0.0	1.519E-01	0.810

Table 3.46. SAXTON-5 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	7.276E-05	1.326E-04	4.636E-05	1.134E-02	0.147
	Clad	5.939E-07	0.0	0.0	3.314E-03	0.043
	Mod.	1.683E-06	0.0	0.0	6.233E-02	0.810
21	Fuel	1.185E-04	2.024E-04	7.072E-05	2.776E-02	0.147
	Clad	1.081E-06	0.0	0.0	8.220E-03	0.044
	Mod.	2.306E-06	0.0	0.0	1.528E-01	0.809



Table 3.47. SAXTON-5, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	1.642E-04	1.632E-04
2	3.938E-05	3.897E-05
3	9.086E-06	8.830E-06
4	4.517E-05	4.505E-05

Table 3.48. SAXTON-5, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.28516E-04	5.26334E-04	2.01776E-04	2.28104E-04	5.25678E-04	2.01507E-04
2	5.57692E-03	8.53438E-03	3.50244E-03	5.57593E-03	8.52166E-03	3.49720E-03
3	8.00912E-03	1.62733E-02	6.67842E-03	7.98496E-03	1.61621E-02	6.63276E-03
4	7.58687E-02	1.57957E-01	6.48244E-02	7.56584E-02	1.57516E-01	6.46433E-02

Table 3.49. SAXTON-5, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	7.40499E-03	1.43721E-02	5.09562E-03	7.36961E-03	1.43170E-02	5.07374E-03
2	6.01938E-02	6.08276E-06	2.52006E-06	5.60690E-02	5.89946E-06	2.44412E-06
3	1.12744E-02	3.88600E-08	1.61004E-08	1.12557E-02	3.87165E-08	1.60410E-08
4	4.34215E-02	2.04004E-07	8.45229E-08	4.33185E-02	2.03512E-07	8.43190E-08

Table 3.50. SAXTON-5, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	2.51193E-03	7.40536E-03	2.37431E-03	2.51011E-03	7.40294E-03	2.37356E-03
2	4.59985E-02	7.75008E-02	2.69116E-02	4.40523E-02	7.41950E-02	2.57639E-02
3	1.50511E-01	2.97520E-01	1.03313E-01	1.47223E-01	2.91456E-01	1.01207E-01
4	1.25860E+00	2.54527E+00	8.80429E-01	1.25753E+00	2.54209E+00	8.79338E-01

Table 3.51. SAXTON-5, Pin-21 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	4.092E-04	4.112E-04
2	1.239E-04	1.261E-04
3	2.677E-05	2.696E-05
4	6.193E-05	6.260E-05

Table 3.52. SAXTON-5, Pin-21 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.36162E-04	5.32867E-04	2.05677E-04	2.35623E-04	5.32179E-04	2.05354E-04
2	5.48935E-03	8.40097E-03	3.44768E-03	5.44674E-03	8.35559E-03	3.42905E-03
3	7.96989E-03	1.61823E-02	6.64109E-03	7.98750E-03	1.62231E-02	6.65779E-03
4	7.21016E-02	1.49992E-01	6.15555E-02	7.19091E-02	1.49587E-01	6.13891E-02

Table 3.53. SAXTON-5, Pin-21 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	7.19130E-03	1.30115E-02	4.61767E-03	7.19283E-03	1.30642E-02	4.63670E-03
2	5.75995E-02	6.14358E-06	2.54525E-06	5.55646E-02	6.04202E-06	2.50319E-06
3	1.12575E-02	3.87725E-08	1.60642E-08	1.12617E-02	3.87641E-08	1.60607E-08
4	4.14883E-02	1.94726E-07	8.06790E-08	4.13946E-02	1.94278E-07	8.04931E-08

Table 3.54. SAXTON-5, Pin-21 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.52182E-03	7.31114E-03	2.35818E-03	2.52033E-03	7.31286E-03	2.35814E-03
2	4.59107E-02	7.65671E-02	2.65875E-02	4.38622E-02	7.38489E-02	2.56436E-02
3	1.46728E-01	2.90546E-01	1.00891E-01	1.47469E-01	2.91907E-01	1.01364E-01
4	1.31306E+00	2.61230E+00	9.03898E-01	1.31380E+00	2.61230E+00	9.03907E-01

0.349 (1.00)						26.71 (0.54)
					25.24 (0.26)	26.06 (0.27)
				22.18 (0.30)	23.68 (0.19)	24.15 (0.28)
		17.62 (0.35)	19.75 (0.21)	21.10 (0.19)	21.46 (0.29)	
		12.89 (0.35)	15.03 (0.22)	16.85 (0.22)	17.95 (0.20)	18.30 (0.31)
10.69 (0.39)	11.87 (0.28)	13.89 (0.26)	15.51 (0.25)	16.58 (0.23)	16.92 (0.35)	

Fig. 3.12a. Pin-power distribution for CENTRM benchmark SAXTON-6. Value in parentheses is percent standard deviation.

0.341 (1.01)						26.34 (0.53)
					25.27 (0.28)	25.86 (0.27)
				22.14 (0.31)	23.68 (0.20)	24.16 (0.27)
		17.65 (0.32)	19.77 (0.21)	21.15 (0.19)	21.58 (0.30)	
		12.84 (0.40)	15.03 (0.24)	16.86 (0.23)	17.98 (0.20)	18.46 (0.31)
10.75 (0.42)	11.84 (0.27)	13.94 (0.26)	15.58 (0.24)	16.62 (0.23)	16.94 (0.30)	

Fig. 3.12b. Pin-power distribution for NITAWL benchmark SAXTON-6. Value in parentheses is percent standard deviation.

Table 3.55. SAXTON-6 CENTRM reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	5.801E-05	1.068E-04	3.734E-05	8.227E-03	0.085
	Clad	4.571E-07	0.0	0.0	2.381E-03	0.024
	Mod.	2.974E-06	0.0	0.0	8.646E-02	0.891
21	Fuel	1.483E-04	2.649E-04	9.259E-05	2.605E-02	0.085
	Clad	1.224E-06	0.0	0.0	7.665E-03	0.025
	Mod.	6.914E-06	0.0	0.0	2.718E-01	0.890

Table 3.56. SAXTON-6 NITAWL reaction rates and fluxes

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	5.849E-05	1.078E-04	3.768E-05	8.318E-03	0.085
	Clad	4.597E-07	0.0	0.0	2.405E-03	0.025
	Mod.	1.489E-06	0.0	0.0	8.696E-02	0.890
21	Fuel	1.484E-04	2.656E-04	9.284E-05	2.592E-02	0.085
	Clad	1.212E-06	0.0	0.0	7.589E-03	0.025
	Mod.	3.439E-06	0.0	0.0	2.708E-01	0.890

Table 3.57. SAXTON-6, Pin-1 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	1.127E-04	1.136E-04
2	2.431E-05	2.487E-05
3	5.596E-06	5.708E-06
4	3.680E-05	3.720E-05

Table 3.58. SAXTON-6, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	2.25419E-04	5.23524E-04	2.00192E-04	2.25627E-04	5.23460E-04	2.00250E-04
2	5.64554E-03	8.59223E-03	3.52618E-03	5.66043E-03	8.68922E-03	3.56598E-03
3	8.10920E-03	1.64809E-02	6.76363E-03	8.14676E-03	1.65761E-02	6.80268E-03
4	7.66356E-02	1.59575E-01	6.54883E-02	7.61884E-02	1.58640E-01	6.51043E-02

Table 3.59. SAXTON-6, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	7.46961E-03	1.48484E-02	5.26453E-03	7.45908E-03	1.47830E-02	5.24259E-03
2	6.30267E-02	6.27162E-06	2.59830E-06	5.76920E-02	5.74105E-06	2.37850E-06
3	1.12849E-02	3.89762E-08	1.61485E-08	1.13126E-02	3.92234E-08	1.62510E-08
4	4.38120E-02	2.05877E-07	8.52986E-08	4.35935E-02	2.04834E-07	8.48667E-08

Table 3.60. SAXTON-6, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle \underline{G}_f \rangle$	$\underline{G}_f$
1	2.50829E-03	7.44201E-03	2.38103E-03	2.50741E-03	7.43347E-03	2.37922E-03
2	4.78379E-02	8.01259E-02	2.78233E-02	4.63764E-02	7.75412E-02	2.69258E-02
3	1.52214E-01	3.00611E-01	1.04386E-01	1.54150E-01	3.04373E-01	1.05692E-01
4	1.24949E+00	2.53488E+00	8.76780E-01	1.24891E+00	2.53120E+00	8.75527E-01

Table 3.61. SAXTON-6, Pin-21 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	3.626E-04	3.592E-04
2	9.528E-05	9.575E-05
3	2.230E-05	2.206E-05
4	8.798E-05	8.816E-05

Table 3.62. SAXTON-6, Pin-21 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.30565E-04	5.27350E-04	2.02688E-04	2.30477E-04	5.28068E-04	2.02763E-04
2	5.63375E-03	8.59935E-03	3.52909E-03	5.56879E-03	8.53534E-03	3.50283E-03
3	8.06789E-03	1.64302E-02	6.74278E-03	8.03178E-03	1.64159E-02	6.73694E-03
4	7.49118E-02	1.55931E-01	6.39925E-02	7.47374E-02	1.55564E-01	6.38420E-02

Table 3.63. SAXTON-6, Pin-21 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	7.31139E-03	1.38701E-02	4.92308E-03	7.34112E-03	1.40133E-02	4.96478E-03
2	6.04901E-02	6.16474E-06	2.55402E-06	5.89630E-02	6.22799E-06	2.58023E-06
3	1.12898E-02	3.90791E-08	1.61912E-08	1.12885E-02	3.90972E-08	1.61987E-08
4	4.29311E-02	2.01652E-07	8.35480E-08	4.28370E-02	2.01200E-07	8.33613E-08

Table 3.64. SAXTON-6, Pin-21 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	2.51210E-03	7.36437E-03	2.36645E-03	2.51355E-03	7.37904E-03	2.36928E-03
2	4.63848E-02	7.74581E-02	2.68969E-02	4.49666E-02	7.52761E-02	2.61392E-02
3	1.47063E-01	2.91411E-01	1.01191E-01	1.47665E-01	2.92500E-01	1.01570E-01
4	1.27191E+00	2.56133E+00	8.86051E-01	1.27598E+00	2.56709E+00	8.88067E-01

## 4. MIX-COMP-THERM-4 (TCA-1 TO TCA-11)

### 4.1 DESCRIPTION

This section describes a set of 11 critical experiments, each consisting of a square-pitched array of mixed Plutonium-Uranium fuel rods partially submerged in water surrounded by a water reflector. The water-to-fuel ratios for the arrays range from 2.4 to 5.6. This set of experiments is contained in the *International Handbook of Evaluated Criticality Safety Benchmark Experiments*.<sup>3</sup>

This set of experiments was performed between 1972 and 1975 at the Tokai Research Establishment of JAERI. The Tank-Type Critical Assembly (TCA) benchmark cases are light-water moderated critical assemblies, consisting of a core array supported by upper, middle, and lower grid plates. The grid plates do not pass through the fuel region. The fuel is sufficiently long such that the water level is below the top of the fuel region in all cases. The reactor is brought to critical by raising the water level in the tank, thus avoiding the use of control rods. The fuel rods sit on a support plate above the bottom of the tank. The tank is wide enough to assume an infinite moderator on the sides (~30 cm of water).

All fuel rods have the same physical dimensions. A schematic diagram of the fuel rods and bottom reflector is given in Fig. 4.1. Each fuel rod has an active fuel length of 70.6 cm and a 16.83-cm-long bottom aluminum end plug that sits on a 1.27-cm-thick aluminum support plate. The fuel has a radius of 0.5325 cm. The cladding has an outside radius of 0.6115 cm. For the calculation, the cladding is extended 9.97 cm above the active fuel to the bottom of the middle grid plate. The middle grid plate and everything above are assumed to be insignificant and thus excluded from the model. The fuel lattice is surrounded by 30 cm of water on the four sides from the bottom of the tank to the top of the critical water level.

From the top of the aluminum support plate is a 4.445-cm water gap and 0.601-cm lower aluminum grid plate. Below the aluminum support plate is a 2.2-cm-thick stainless steel (SS) support plate, a 13.8-cm water gap, 0.5-cm-thick SS tank liner and 37.0 cm of concrete.

The primary differences between the 11 benchmarks are lattice pitch, number of rods in the lattice, water level, and Pu-241 and Am-241 number densities. All other benchmark characteristics are constant. The 11 benchmarks are divided into four different lattice pitches: 1.825 cm, 1.956 cm, 2.225 cm, and 2.474 cm. For a given pitch, the number of pins in the lattice is given. The fuel is arranged in a square-pitched square lattice. The characteristics of each of the four lattices are given in Table 4.1. The critical fuel height variations are due to the changes in Pu-241 and Am-241 atom densities. Table 4.2 contains the atom densities for all the materials in the problem except Pu-241 and Am-241. The atom densities in Table 4.2 are constant for all benchmarks. Table 4.3 contains the atom densities for Pu-241 and Am-241 for each benchmark. All material temperatures are assumed to be 20°C.

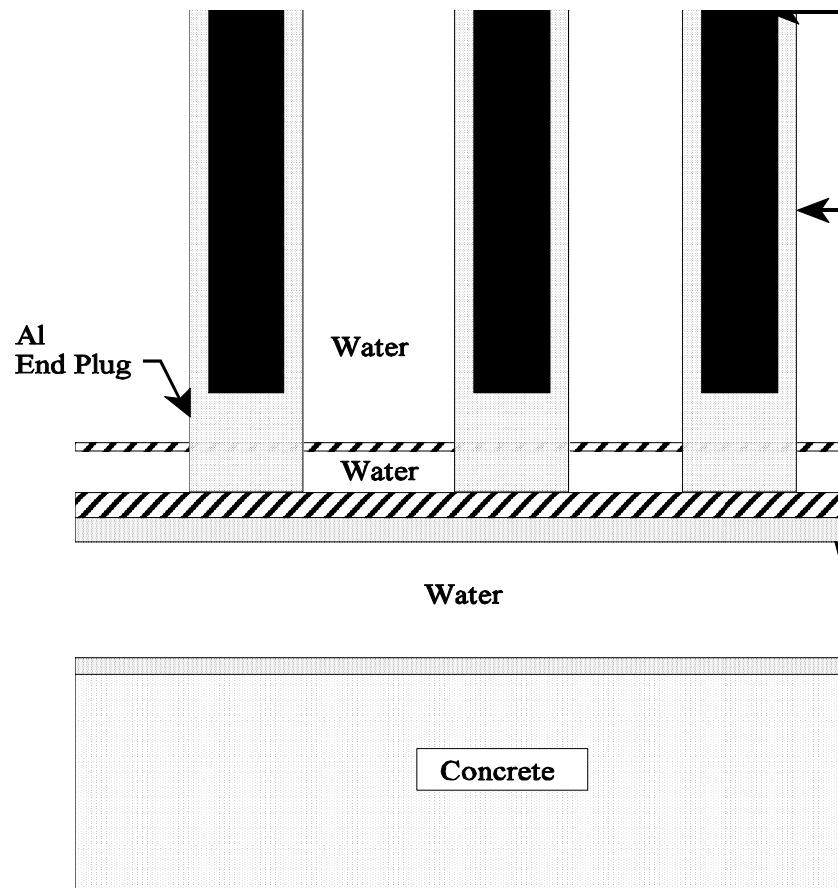


Fig. 4.1. Schematic of the TCA fuel rods and bottom reflector.



Table 4.1. Lattice description for benchmarks

Benchmark No.	Water/Fuel volume ratio (H/Pu ratio)	Lattice pitch (cm)	Number of rods on a Side	Lattice side dimension (cm)	Critical water level (cm)
1					59.5
2	2.42 (402)	1.825	23	41.975	91.90
3					64.06
4					61.50
5	2.98 (494)	1.956	21	41.076	64.40
6					69.40
7					60.32
8	4.24 (703)	2.225	20	44.500	62.99
9					65.63
10	5.55 (921)	2.474	21	51.954	62.05
11					64.53

The first three benchmarks; TCA-1, TCA-2, and TCA-3 have a pitch of 1.825 cm and  $23 \times 23$  pin lattice. This pitch produces a water-to-fuel volume ratio of 2.42 cm and a H/Pu ratio of 402. To simplify the production of the lattice pin-power distribution and improve the statistics, the lattice advantage is taken of the lattice symmetry. Only 1/8th of the lattice needs to be modeled precisely to produce the pin-power distribution. The lattice is then filled from the 1/8th section by inserting additional pins in a mirror image. Figure 4.2 is a lattice map of the pin locations.

The same approach is used for the next three benchmarks: TCA-4, TCA-5, and TCA-6. These benchmarks have a pitch of 1.956 cm and  $21 \times 21$  pin lattice. This pitch produces a water-to-fuel volume ratio of 2.98 cm and a H/Pu ratio of 494. The symmetry of the lattice is used in the same way it was used in the first three benchmarks. One-eighth of the lattice is filled, and the remaining lattice is filled assuming a mirror image. Figure 4.3 is a lattice map of the pin locations.

The next three benchmark problems TCA-7, TCA-8, and TCA-9 again use the same approach. These benchmarks have a pitch of 2.225 cm and a  $20 \times 20$  pin lattice. This pitch produces a water-to-fuel volume ratio of 4.24 cm and a H/Pu ratio of 703. Figure 4.4 is a lattice map of the pin locations.

The last benchmark problems TCA-10 and TCA-11 have the same lattice arrangement as the second set of benchmarks (see Fig. 4.3). However, these benchmarks have of pitch of 2.474 cm which produces a water-to-fuel volume ratio of 5.55 cm and a H/Pu ratio of 921. The input files for each of the benchmark problems can be found in Appendix C.

## 4.2 ANALYSIS

All 11 computational benchmarks in this section were processed twice using SCALE 5.0. The set labeled NITAWL uses the NITAWL resonance processor to self-shield the resolved resonance region for all nuclides in the fuel and clad. An identical set, labeled CENTRM, replaces NITAWL with the CENTRM/PMC code sequence. The NITAWL and CENTRM results are then compared.

Table 4.4 contains the  $k_{eff}$  and Energy of the Average Lethargy Causing Fission (EALCF). The  $k_{eff}$  values for all the benchmark cases are very close to 1.0: the worst NITAWL benchmark is 0.26% high, and the worst CENTRM case is 0.37% low. There does appear to be a small negative bias between NITAWL and CENTRM, the CENTRM cases being about 0.2% lower on average than the NITAWL cases. The EALCF values listed are from the CENTRM cases. For all cases the difference between this value for CENTRM and NITAWL was less than 0.1%. Both CENTRM and NITAWL produce excellent results for the  $k_{eff}$  and fission energy for this set of problems.

Also, calculated for each problem is the: pin-power distributions; absorption,  $\langle G_f \rangle$ , and fission reaction rates and fluxes in the pin fuel, clad, and moderator; and four group cross sections and fluxes for a corner outside pin and the innermost pin. Each of these sets of data are calculated using both CENTRM and NITAWL. The data for each case are contained in Figs. 4.5a through 4.15b and Tables 4.5 through 4.114.

The pin-power distributions for this problem assumed 1/8th core symmetry with a surrounding reflector. The pin-power data consist of a value and a standard deviation for each pin. The values for the pin-powers are actually in units of fissions per  $\text{cm}^3\text{-s-source particle} \times 10^{-5}$ . The value in parentheses is the percent standard deviation of the pin-power value. In most cases, the CENTRM and NITAWL results for each benchmark case agree within 2 standard deviations. The pin-power distributions represent that portion of the pin covered by water. The value off to the side in the pin-power distributions represents all the fuel not covered by water. The peak-to-low power changed with respect to pitch. The peak-to-low-power ratio changed from a low of 2.7 for the smallest pitch to a high of 4.9 at the largest pitch.

The reaction rates, total fluxes, and flux ratios for the CENTRM and NITAWL cases of each benchmark case are also in good agreement, seldom varying by more than 1%. These values are included for a corner pin and the center pin for each case. The flux ratios over the fuel, clad, and moderator stay relatively constant for a given pitch. However, as the pitch increases the proportion of the total pin flux in the moderator increases.

Finally, four-group fluxes and cross sections were calculated for selected nuclides in the fuel region of the same corner and center pins. The macroscopic cross sections include the radiative capture, fission, and  $\nu^*\text{fission}$  cross sections for U-235, U-238, and Pu-239. The four groups are collapsed from the 238-group multigroup cross-section set using the flux profile calculated in KENO-V.a as follows: group 1 is from 20 Mev to 9.5 keV, group 2 is from 9.5 keV to 3.0 eV, Group 3 is from 3 eV to 0.4 eV, and group 4 is from 0.4 eV to  $10^{-5}$  eV. The 0.4 eV was chosen as a boundary because it is the cadmium cutoff energy. Groups 2 and 3 contain the resolved resonance regions for most of the nuclides used in these cases. Most of the cross-section data for the CENTRM and NITAWL cases of a given benchmark case agree within 1%.

### 4.3 CONCLUSIONS

For this set of benchmark cases, using either NITAWL and CENTRM as the resonance region processor produces acceptable results of the  $k_{eff}$  values. All other values produced using CENTRM and NITAWL are also consistent with each. The  $k_{eff}$  values are slightly lower,  $\sim 0.2\%$ , for all CENTRM cases. The pin-power distributions, fluxes, reaction rates, and macroscopic cross sections generally agree within approximately 1% between CENTRM and NITAWL. No significant differences were identified between the results produced by NITAWL and CENTRM for these benchmark cases.

Table 4.2. Benchmark atom densities

Material	Isotope	Atom density (atoms/barn-cm)	Material	Isotope	Atom density (atoms/barn-cm)
Fuel	U-234	$7.1749 \times 10^{-7}$	Ordinary concrete	H	$1.3742 \times 10^{-2}$
	U-235	$9.3926 \times 10^{-5}$		O	$4.5919 \times 10^{-2}$
	U-238	$1.2951 \times 10^{-2}$		C	$1.1532 \times 10^{-4}$
	Pu-238	$2.0003 \times 10^{-6}$		Na	$9.6395 \times 10^{-4}$
	Pu-239	$2.7491 \times 10^{-4}$		Mg	$1.2388 \times 10^{-4}$
	Pu-240	$8.8417 \times 10^{-5}$		Al	$1.7409 \times 10^{-3}$
	Pu-241	(See Table 3.3)		Si	$1.6617 \times 10^{-2}$
	Pu-242	$8.1234 \times 10^{-6}$		K	$4.6052 \times 10^{-4}$
	Am-241	(See Table 3.3)		Ca	$1.5025 \times 10^{-3}$
	O-16	$2.7837 \times 10^{-2}$		Fe	$3.4492 \times 10^{-4}$
	B-10	$6.0418 \times 10^{-8}$			
B-11	$2.4319 \times 10^{-7}$				
Cladding + Air gap	Zr	$3.7772 \times 10^{-2}$	Stainless steel (SS-304L)	C	$1.1928 \times 10^{-4}$
	Sn	$4.3737 \times 10^{-4}$		Si	$1.7003 \times 10^{-3}$
	Fe	$8.8570 \times 10^{-5}$		Mn	$1.7385 \times 10^{-3}$
	Cr	$6.6119 \times 10^{-5}$		P	$6.9381 \times 10^{-5}$
	Ni	$3.5864 \times 10^{-5}$		S	$4.4673 \times 10^{-5}$
			Ni	$8.9506 \times 10^{-3}$	
			Cr	$1.7450 \times 10^{-2}$	
			Fe	$5.7202 \times 10^{-2}$	
Water (20° C) 0.9982 g/cc	H	$6.6735 \times 10^{-2}$	Aluminum	Al	$6.0224 \times 10^{-2}$
	O	$3.3368 \times 10^{-2}$			

Table 4.3. Pu-241 and Am-241 atom densities

Benchmark No.	Atom densities ( atoms/barn-cm )	
	Pu-241	Am-241
1	$2.7923 \times 10^{-5}$	$1.3531 \times 10^{-6}$
2	$2.6701 \times 10^{-5}$	$2.5812 \times 10^{-6}$
3	$2.5447 \times 10^{-5}$	$3.8361 \times 10^{-6}$
4	$2.8003 \times 10^{-5}$	$1.2793 \times 10^{-6}$
5	$2.6670 \times 10^{-5}$	$2.6129 \times 10^{-6}$
6	$2.4228 \times 10^{-5}$	$5.0543 \times 10^{-6}$
7	$2.8133 \times 10^{-5}$	$1.1498 \times 10^{-6}$
8	$2.6649 \times 10^{-5}$	$2.6340 \times 10^{-6}$
9	$2.5373 \times 10^{-5}$	$3.9098 \times 10^{-6}$
10	$2.8077 \times 10^{-5}$	$1.2053 \times 10^{-6}$
11	$2.6617 \times 10^{-5}$	$2.6656 \times 10^{-6}$

Table 4.4. Comparison of  $k_{eff}$  and EALCF from CENTRM and NITAWL<sup>a</sup>

Benchmark identification	CENTRM $k_{eff} (\pm F)$	NITAWL $k_{eff} (\pm F)$	EALF (eV)	$k_{eff}$ % DIFF
TCA-1	0.9963 (0.0005)	0.9993 (0.0004)	0.145	-0.3
TCA-2	0.9969 (0.0004)	1.0001 (0.0004)	0.144	-0.32
TCA-3	0.9985 (0.0005)	1.0002 (0.0004)	0.143	-0.17
TCA-4	0.9973 (0.0004)	0.9995 (0.0004)	0.119	-0.22
TCA-5	0.9982 (0.0004)	1.0008 (0.0004)	0.118	-0.26
TCA-6	0.9988 (0.0004)	1.0003 (0.0003)	0.117	-0.15
TCA-7	0.9994 (0.0004)	1.0016 (0.0004)	0.0927	-0.22
TCA-8	1.0002 (0.0004)	1.0017 (0.0003)	0.0923	-0.15
TCA-9	1.0009 (0.0004)	1.0024 (0.0004)	0.0916	-0.15
TCA-10	1.0003 (0.0003)	1.0020 (0.0004)	0.0797	-0.17
TCA-11	1.0010 (0.0004)	1.0026 (0.0004)	0.0792	-0.16

<sup>a</sup> Value in parentheses is percent standard deviation.

											78
										76	77
									73	74	75
								69	70	71	72
							64	65	66	67	68
						58	59	60	61	62	63
					51	52	53	54	55	56	57
				43	44	45	46	47	48	49	50
			34	35	36	37	38	39	40	41	42
		24	25	26	27	28	29	30	31	32	33
	13	14	15	16	17	18	19	20	21	22	23
1	2	3	4	5	6	7	8	9	10	11	12

Fig. 4.2. Pin layout of benchmark cases TCA-1, TCA-2, and TCA-3.

											66
										64	65
									61	62	63
								57	58	59	60
							52	53	54	55	56
						46	47	48	49	50	51
					39	40	41	42	43	44	45
				31	32	33	34	35	36	37	38
			22	23	24	25	26	27	28	29	30
		12	13	14	15	16	17	18	19	20	21
1	2	3	4	5	6	7	8	9	10	11	

Fig. 4.3. Pin layout of benchmark cases TCA-4, TCA-5 ,TCA-6, TCA-10, and TCA-11.

									55
								53	54
							50	51	52
						46	47	48	49
					41	42	43	44	45
				35	36	37	38	39	40
			28	29	30	31	32	33	34
		20	21	22	23	24	25	26	27
	11	12	13	14	15	16	17	18	19
1	2	3	4	5	6	7	8	9	10

Fig. 4.4. Pin layout of benchmark cases TCA-7, TCA-8, and TCA-9.

											5.299 (0.91)
										5.191 (0.46)	5.175 (0.48)
									4.954 (0.48)	5.104 (0.36)	5.242 (0.48)
								4.722 (0.51)	4.871 (0.33)	4.971 (0.34)	4.937 (0.48)
							4.426 (0.51)	4.601 (0.33)	4.697 (0.36)	4.759 (0.36)	4.815 (0.54)
						3.982 (0.50)	4.212 (0.39)	4.340 (0.37)	4.479 (0.36)	4.554 (0.33)	4.551 (0.44)
					3.535 (0.54)	3.766 (0.44)	3.934 (0.40)	4.068 (0.40)	4.184 (0.38)	4.252 (0.38)	4.286 (0.53)
				3.058 (0.60)	3.295 (0.43)	3.456 (0.45)	3.650 (0.35)	3.781 (0.36)	3.895 (0.37)	3.942 (0.39)	3.989 (0.53)
			2.518 (0.75)	2.769 (0.48)	2.963 (0.45)	3.180 (0.44)	3.354 (0.46)	3.457 (0.41)	3.555 (0.38)	3.617 (0.40)	3.640 (0.56)
		2.104 (0.83)	2.321 (0.51)	2.533 (0.48)	2.736 (0.45)	2.893 (0.47)	3.058 (0.39)	3.159 (0.41)	3.257 (0.42)	3.271 (0.41)	3.331 (0.58)
	1.889 (0.78)	1.980 (0.57)	2.223 (0.55)	2.402 (0.51)	2.624 (0.50)	2.789 (0.41)	2.917 (0.41)	3.037 (0.47)	3.092 (0.45)	3.150 (0.42)	3.184 (0.65)
2.329 (0.66)	2.178 (0.54)	2.356 (0.50)	2.589 (0.47)	2.844 (0.47)	3.066 (0.41)	3.258 (0.42)	3.398 (0.43)	3.576 (0.39)	3.644 (0.44)	3.710 (0.40)	3.729 (0.57)

Fig. 4.5a. Pin-power distribution for CENTRM benchmark TCA-1. Value in parentheses is percent standard deviation.



											5.219 (0.86)
										5.153 (0.50)	5.235 (0.47)
									5.022 (0.49)	5.083 (0.36)	5.140 (0.46)
								4.775 (0.48)	4.893 (0.35)	4.968 (0.38)	5.010 (0.49)
							4.453 (0.54)	4.607 (0.35)	4.712 (0.36)	4.779 (0.33)	4.840 (0.50)
						4.006 (0.55)	4.225 (0.41)	4.384 (0.36)	4.474 (0.36)	4.594 (0.35)	4.547 (0.53)
					3.541 (0.55)	3.807 (0.39)	3.978 (0.41)	4.086 (0.36)	4.200 (0.39)	4.270 (0.37)	4.341 (0.47)
				3.013 (0.60)	3.298 (0.40)	3.496 (0.39)	3.645 (0.42)	3.821 (0.38)	3.921 (0.43)	3.981 (0.37)	3.948 (0.55)
			2.552 (0.65)	2.767 (0.46)	2.999 (0.44)	3.200 (0.40)	3.362 (0.36)	3.471 (0.38)	3.581 (0.41)	3.631 (0.41)	3.624 (0.59)
		2.113 (0.73)	2.284 (0.48)	2.509 (0.50)	2.749 (0.46)	2.906 (0.47)	3.036 (0.42)	3.153 (0.42)	3.238 (0.41)	3.276 (0.44)	3.329 (0.53)
	1.911 (0.77)	1.997 (0.47)	2.202 (0.57)	2.417 (0.51)	2.623 (0.44)	2.768 (0.46)	2.927 (0.46)	3.029 (0.40)	3.071 (0.44)	3.176 (0.41)	3.180 (0.65)
2.279 (0.69)	2.171 (0.53)	2.347 (0.50)	2.571 (0.48)	2.845 (0.43)	3.066 (0.47)	3.274 (0.39)	3.446 (0.41)	3.601 (0.38)	3.673 (0.38)	3.729 (0.41)	3.776 (0.55)

Fig. 4.5b. Pin-power distribution for NITAWL benchmark TCA-1. Value in parentheses is percent standard deviation.

Table 4.5. Selected reaction rates for CENTRM case TCA-1

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.400E-05	2.320E-05	8.219E-06	5.406E-03	0.271
	Clad	2.686E-07	0.0	0.0	1.687E-03	0.085
	Mod.	7.396E-07	0.0	0.0	1.285E-02	0.644
78	Fuel	3.547E-05	5.287E-05	1.869E-05	2.162E-02	0.270
	Clad	7.404E-07	0.0	0.0	6.840E-03	0.085
	Mod.	1.542E-06	0.0	0.0	5.169E-02	0.645

Table 4.6. Selected reaction rates for NITAWL case TCA-1

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.386E-05	2.292E-05	8.121E-06	5.354E-03	0.271
	Clad	2.641E-07	0.0	0.0	1.665E-03	0.084
	Mod.	7.348E-07	0.0	0.0	1.277E-02	0.645
78	Fuel	3.457E-05	5.164E-05	1.827E-05	2.134E-02	0.268
	Clad	7.151E-07	0.0	0.0	6.771E-03	0.085
	Mod.	1.529E-06	0.0	0.0	5.146E-02	0.647

Table 4.7. TCA-1, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	5.205E-05	5.150E-05
2	1.550E-05	1.533E-05
3	3.677E-06	3.705E-06
4	3.068E-05	3.040E-05

Table 4.8. TCA-1, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	1.43276E-04	3.25948E-04	1.25443E-04	1.43133E-04	3.25491E-04	1.25308E-04
2	3.47383E-03	5.32334E-03	2.18465E-03	3.41501E-03	5.21704E-03	2.14103E-03
3	5.07797E-03	1.03603E-02	4.25178E-03	5.13482E-03	1.05164E-02	4.31584E-03
4	4.86542E-02	1.01291E-01	4.15691E-02	4.83612E-02	1.00680E-01	4.13181E-02

Table 4.9. TCA-1, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	4.48868E-03	8.37908E-03	2.97182E-03	4.45235E-03	8.27583E-03	2.93388E-03
2	3.79279E-02	3.70803E-06	1.53622E-06	3.78200E-02	3.60508E-06	1.49357E-06
3	6.96274E-03	2.42790E-08	1.00592E-08	6.99725E-03	2.45979E-08	1.01914E-08
4	2.76422E-02	1.29929E-07	5.38321E-08	2.75005E-02	1.29251E-07	5.35513E-08

Table 4.10. TCA-1, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	5.12119E-04	1.49477E-03	4.80859E-04	5.11680E-04	1.49305E-03	4.80499E-04
2	1.13759E-02	1.87090E-02	6.49658E-03	1.06255E-02	1.76083E-02	6.11439E-03
3	3.27337E-02	6.44523E-02	2.23808E-02	3.35760E-02	6.60534E-02	2.29368E-02
4	2.66846E-01	5.40163E-01	1.86831E-01	2.66855E-01	5.39595E-01	1.86638E-01

Table 4.11. TCA-1, Pin-78 four-group fluxes

Group	CENTRM M ( cm <sup>2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>2</sup> - s <sup>-1</sup> )
1	2.399E-04	2.360E-04
2	8.524E-05	8.507E-05
3	1.867E-05	1.851E-05
4	6.380E-05	6.276E-05

Table 4.12. TCA-1, Pin-78 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G_a}$	$\langle G_f \rangle$	$\overline{G_f}$	$\overline{G_a}$	$\langle G_f \rangle$	$\overline{G_f}$
1	1.48131E-04	3.30102E-04	1.27921E-04	1.47652E-04	3.28787E-04	1.27540E-04
2	3.33968E-03	5.12318E-03	2.10251E-03	3.40930E-03	5.23865E-03	2.14990E-03
3	5.10391E-03	1.04015E-02	4.26869E-03	5.13030E-03	1.04663E-02	4.29526E-03
4	4.54602E-02	9.45345E-02	3.87961E-02	4.53139E-02	9.42388E-02	3.86748E-02

Table 4.13. TCA-1, Pin-78 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G_a}$	$\langle G_f \rangle$	$\overline{G_f}$	$\overline{G_a}$	$\langle G_f \rangle$	$\overline{G_f}$
1	4.34327E-03	7.48462E-03	2.65627E-03	4.30530E-03	7.37008E-03	2.62250E-03
2	3.98175E-02	3.68536E-06	1.52683E-06	3.74190E-02	3.60909E-06	1.49523E-06
3	6.98275E-03	2.43235E-08	1.00777E-08	6.98957E-03	2.44139E-08	1.01151E-08
4	2.59889E-02	1.21997E-07	5.05458E-08	2.59301E-02	1.21719E-07	5.04304E-08

Table 4.14. TCA-1, Pin-78 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G_a}$	$\langle G_f \rangle$	$\overline{G_f}$	$\overline{G_a}$	$\langle G_f \rangle$	$\overline{G_f}$
1	5.14181E-04	1.47485E-03	4.77461E-04	5.13292E-04	1.47159E-03	4.76847E-04
2	1.06372E-02	1.75772E-02	6.10359E-03	1.08006E-02	1.79107E-02	6.21938E-03
3	3.42975E-02	6.73203E-02	2.33768E-02	3.44553E-02	6.76072E-02	2.34764E-02
4	2.85886E-01	5.65284E-01	1.95610E-01	2.82398E-01	5.59148E-01	1.93483E-01

											4.965 (0.99)
										4.937 (0.46)	4.994 (0.49)
									4.776 (0.50)	4.866 (0.34)	4.932 (0.47)
								4.569 (0.53)	4.688 (0.32)	4.750 (0.35)	4.781 (0.47)
							4.283 (0.57)	4.402 (0.38)	4.527 (0.36)	4.600 (0.35)	4.677 (0.48)
						3.846 (0.55)	4.048 (0.38)	4.205 (0.37)	4.302 (0.36)	4.359 (0.34)	4.376 (0.50)
					3.405 (0.57)	3.636 (0.43)	3.795 (0.37)	3.946 (0.36)	4.058 (0.34)	4.111 (0.39)	4.125 (0.49)
				2.910 (0.64)	3.171 (0.47)	3.388 (0.42)	3.532 (0.36)	3.649 (0.41)	3.739 (0.41)	3.822 (0.40)	3.849 (0.55)
			2.455 (0.64)	2.666 (0.48)	2.882 (0.43)	3.063 (0.42)	3.207 (0.41)	3.324 (0.42)	3.449 (0.41)	3.489 (0.42)	3.486 (0.55)
		2.021 (0.74)	2.222 (0.54)	2.433 (0.46)	2.634 (0.46)	2.808 (0.47)	2.906 (0.42)	3.043 (0.45)	3.141 (0.44)	3.166 (0.45)	3.189 (0.61)
	1.841 (0.80)	1.935 (0.54)	2.120 (0.48)	2.324 (0.52)	2.503 (0.44)	2.645 (0.46)	2.825 (0.44)	2.902 (0.43)	2.982 (0.43)	3.040 (0.46)	3.036 (0.61)
2.226 (0.69)	2.099 (0.51)	2.276 (0.50)	2.506 (0.50)	2.739 (0.44)	2.952 (0.41)	3.138 (0.43)	3.341 (0.35)	3.425 (0.39)	3.533 (0.37)	3.606 (0.40)	3.590 (0.59)

Fig. 4.6a. Pin-power distribution for CENTRM benchmark TCA-2. Value in parentheses is percent standard deviation.

											5.023 (0.99)
										4.960 (0.46)	5.042 (0.47)
									4.835 (0.48)	4.922 (0.33)	4.929 (0.47)
								4.569 (0.52)	4.721 (0.32)	4.780 (0.36)	4.776 (0.48)
							4.250 (0.50)	4.420 (0.35)	4.521 (0.36)	4.608 (0.35)	4.612 (0.50)
						3.803 (0.58)	4.057 (0.34)	4.179 (0.39)	4.303 (0.35)	4.406 (0.35)	4.409 (0.51)
					3.430 (0.58)	3.641 (0.41)	3.836 (0.39)	3.972 (0.37)	4.049 (0.39)	4.121 (0.37)	4.127 (0.54)
				2.949 (0.66)	3.164 (0.42)	3.374 (0.41)	3.549 (0.43)	3.649 (0.40)	3.775 (0.38)	3.806 (0.42)	3.858 (0.53)
			2.447 (0.66)	2.659 (0.43)	2.876 (0.44)	3.101 (0.45)	3.229 (0.44)	3.359 (0.40)	3.459 (0.38)	3.487 (0.43)	3.504 (0.59)
		2.029 (0.71)	2.232 (0.51)	2.431 (0.48)	2.644 (0.45)	2.793 (0.49)	2.940 (0.44)	3.042 (0.45)	3.132 (0.39)	3.194 (0.43)	3.205 (0.58)
	1.837 (0.75)	1.930 (0.56)	2.140 (0.51)	2.325 (0.53)	2.522 (0.47)	2.677 (0.44)	2.816 (0.44)	2.936 (0.40)	3.008 (0.44)	3.035 (0.40)	3.064 (0.61)
2.222 (0.68)	2.106 (0.51)	2.274 (0.52)	2.527 (0.47)	2.756 (0.43)	2.976 (0.41)	3.149 (0.44)	3.323 (0.39)	3.477 (0.38)	3.562 (0.38)	3.583 (0.41)	3.598 (0.59)

Fig. 4.6b. Pin-power distribution for NITAWL benchmark TCA-2. Value in parentheses is percent standard deviation.

Table 4.15. Selected reaction rates for CENTRM case TCA-2

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.356E-05	2.236E-05	7.923E-06	5.453E-03	0.270
	Clad	2.613E-07	0.0	0.0	1.705E-03	0.085
	Mod.	7.206E-07	0.0	0.0	1.301E-02	0.645
78	Fuel	3.394E-05	5.051E-05	1.786E-05	2.155E-02	0.269
	Clad	7.023E-07	0.0	0.0	6.812E-03	0.085
	Mod.	1.495E-06	0.0	0.0	5.179E-02	0.646

Table 4.16. Selected reaction rates for NITAWL case TCA-2

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.356E-05	2.241E-05	7.942E-06	5.429E-03	0.271
	Clad	2.591E-07	0.0	0.0	1.693E-03	0.084
	Mod.	7.211E-07	0.0	0.0	1.293E-02	0.645
78	Fuel	3.354E-05	5.009E-05	1.771E-05	2.137E-02	0.268
	Clad	6.772E-07	0.0	0.0	6.756E-03	0.084
	Mod.	1.478E-06	0.0	0.0	5.172E-02	0.648

Table 4.17. TCA-2, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	5.046E-05	5.017E-05
2	1.503E-05	1.485E-05
3	3.705E-06	3.620E-06
4	2.970E-05	2.981E-05

Table 4.18. TCA-2, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	1.43119E-04	3.25379E-04	1.25277E-04	1.42796E-04	3.25595E-04	1.25157E-04
2	3.53013E-03	5.42307E-03	2.22558E-03	3.53101E-03	5.37976E-03	2.20780E-03
3	5.06839E-03	1.03472E-02	4.24642E-03	5.21793E-03	1.06593E-02	4.37445E-03
4	4.85643E-02	1.01103E-01	4.14919E-02	4.86105E-02	1.01201E-01	4.15317E-02

Table 4.19. TCA-2, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	4.44405E-03	8.24665E-03	2.92378E-03	4.49711E-03	8.46895E-03	2.99705E-03
2	3.85408E-02	3.81629E-06	1.58108E-06	3.63117E-02	3.48554E-06	1.44405E-06
3	6.97263E-03	2.42518E-08	1.00480E-08	6.99494E-03	2.45706E-08	1.01801E-08
4	2.75966E-02	1.29711E-07	5.37418E-08	2.76225E-02	1.29835E-07	5.37930E-08

Table 4.20. TCA-2, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	5.11583E-04	1.49239E-03	4.80303E-04	5.11437E-04	1.49567E-03	4.80666E-04
2	1.10651E-02	1.80525E-02	6.26864E-03	1.07872E-02	1.76378E-02	6.12465E-03
3	3.33360E-02	6.55390E-02	2.27581E-02	3.37318E-02	6.63232E-02	2.30304E-02
4	2.67093E-01	5.40384E-01	1.86909E-01	2.66605E-01	5.39661E-01	1.86656E-01



Table 4.21. TCA-2, Pin-78 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.302E-04	2.272E-04
2	8.173E-05	8.176E-05
3	1.759E-05	1.791E-05
4	6.122E-05	6.071E-05

Table 4.22. TCA-2, Pin-78 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	1.47775E-04	3.29361E-04	1.27654E-04	1.47727E-04	3.29384E-04	1.27666E-04
2	3.40270E-03	5.23267E-03	2.14744E-03	3.44284E-03	5.28022E-03	2.16695E-03
3	5.19904E-03	1.06173E-02	4.35723E-03	5.12518E-03	1.04631E-02	4.29398E-03
4	4.56001E-02	9.48282E-02	3.89167E-02	4.54184E-02	9.44484E-02	3.87607E-02

Table 4.23. TCA-2, Pin-78 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	4.32970E-03	7.46321E-03	2.65044E-03	4.32945E-03	7.46893E-03	2.65359E-03
2	3.93173E-02	3.71651E-06	1.53973E-06	3.66084E-02	3.70903E-06	1.53663E-06
3	7.00819E-03	2.46566E-08	1.02156E-08	6.99481E-03	2.44808E-08	1.01429E-08
4	2.60606E-02	1.22341E-07	5.06882E-08	2.59687E-02	1.21901E-07	5.05058E-08

Table 4.24. TCA-2, Pin-78 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	5.13614E-04	1.47354E-03	4.77076E-04	5.13794E-04	1.47461E-03	4.77474E-04
2	1.10415E-02	1.82425E-02	6.33460E-03	1.06940E-02	1.76497E-02	6.12879E-03
3	3.48073E-02	6.83161E-02	2.37224E-02	3.39004E-02	6.66510E-02	2.31443E-02
4	2.84748E-01	5.63652E-01	1.95041E-01	2.85625E-01	5.64792E-01	1.95441E-01

											4.889 (1.00)
										4.823 (0.45)	4.841 (0.48)
									4.680 (0.49)	4.775 (0.35)	4.801 (0.51)
								4.418 (0.49)	4.556 (0.35)	4.662 (0.34)	4.671 (0.44)
							4.131 (0.53)	4.290 (0.37)	4.381 (0.40)	4.473 (0.37)	4.486 (0.50)
						3.736 (0.54)	3.929 (0.37)	4.067 (0.37)	4.181 (0.37)	4.232 (0.35)	4.253 (0.47)
					3.282 (0.51)	3.485 (0.38)	3.672 (0.38)	3.812 (0.35)	3.911 (0.36)	3.997 (0.36)	4.014 (0.57)
				2.803 (0.63)	3.040 (0.42)	3.236 (0.40)	3.429 (0.41)	3.556 (0.41)	3.634 (0.40)	3.682 (0.39)	3.716 (0.53)
			2.356 (0.60)	2.576 (0.50)	2.763 (0.42)	2.948 (0.40)	3.121 (0.39)	3.244 (0.43)	3.319 (0.40)	3.364 (0.43)	3.384 (0.59)
		1.962 (0.81)	2.133 (0.49)	2.338 (0.47)	2.571 (0.43)	2.695 (0.42)	2.838 (0.44)	2.947 (0.47)	3.038 (0.46)	3.085 (0.43)	3.097 (0.55)
	1.782 (0.78)	1.874 (0.52)	2.046 (0.52)	2.263 (0.47)	2.423 (0.44)	2.573 (0.48)	2.708 (0.46)	2.819 (0.40)	2.891 (0.44)	2.907 (0.42)	2.936 (0.54)
2.156 (0.74)	2.021 (0.52)	2.204 (0.50)	2.429 (0.49)	2.663 (0.44)	2.876 (0.42)	3.083 (0.41)	3.215 (0.40)	3.338 (0.42)	3.414 (0.40)	3.474 (0.33)	3.480 (0.59)

Fig. 4.7a. Pin-power distribution for CENTRM benchmark TCA-3. Value in parentheses is percent standard deviation.

											4.857 (1.00)
										4.845 (0.46)	4.826 (0.50)
									4.692 (0.49)	4.713 (0.37)	4.814 (0.46)
								4.430 (0.53)	4.565 (0.34)	4.635 (0.34)	4.646 (0.48)
							4.145 (0.54)	4.284 (0.39)	4.400 (0.36)	4.464 (0.36)	4.512 (0.50)
						3.718 (0.51)	3.929 (0.35)	4.066 (0.38)	4.195 (0.37)	4.262 (0.33)	4.242 (0.50)
					3.318 (0.57)	3.525 (0.36)	3.701 (0.40)	3.836 (0.37)	3.934 (0.37)	3.997 (0.35)	4.006 (0.51)
				2.807 (0.61)	3.095 (0.41)	3.287 (0.39)	3.406 (0.41)	3.538 (0.40)	3.646 (0.36)	3.714 (0.36)	3.704 (0.49)
			2.365 (0.67)	2.589 (0.48)	2.799 (0.44)	2.975 (0.41)	3.132 (0.41)	3.230 (0.40)	3.314 (0.41)	3.391 (0.39)	3.396 (0.59)
		1.949 (0.76)	2.150 (0.51)	2.363 (0.47)	2.541 (0.48)	2.706 (0.45)	2.838 (0.44)	2.977 (0.42)	3.035 (0.43)	3.082 (0.43)	3.092 (0.55)
	1.762 (0.77)	1.861 (0.58)	2.063 (0.49)	2.238 (0.53)	2.433 (0.47)	2.572 (0.46)	2.729 (0.48)	2.840 (0.40)	2.894 (0.44)	2.944 (0.42)	2.962 (0.59)
2.155 (0.76)	2.037 (0.53)	2.194 (0.47)	2.420 (0.50)	2.654 (0.46)	2.866 (0.42)	3.058 (0.41)	3.225 (0.40)	3.315 (0.41)	3.430 (0.39)	3.480 (0.37)	3.483 (0.58)

Fig. 4.7b. Pin-power distribution for NITAWL benchmark TCA-3. Value in parentheses is percent standard deviation.

Table 4.25. Selected reaction rates for CENTRM case TCA-3

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.307E-05	2.156E-05	7.643E-06	5.476E-03	0.271
	Clad	2.496E-07	0.0	0.0	1.701E-03	0.085
	Mod.	6.938E-07	0.0	0.0	1.300E-02	0.644
78	Fuel	3.318E-05	4.938E-05	1.747E-05	2.182E-02	0.269
	Clad	6.794E-07	0.0	0.0	6.875E-03	0.085
	Mod.	1.442E-06	0.0	0.0	5.233E-02	0.646

Table 4.26. Selected reaction rates for NITAWL case TCA-3

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.296E-05	2.142E-05	7.591E-06	5.418E-03	0.272
	Clad	2.463E-07	0.0	0.0	1.676E-03	0.084
	Mod.	6.886E-07	0.0	0.0	1.285E-02	0.644
78	Fuel	3.290E-05	4.896E-05	1.732E-05	2.172E-02	0.269
	Clad	6.746E-07	0.0	0.0	6.861E-03	0.085
	Mod.	1.449E-06	0.0	0.0	5.222E-02	0.646

Table 4.27. TCA-3, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	4.915E-05	4.860E-05
2	1.453E-05	1.440E-05
3	3.519E-06	3.300E-06
4	2.876E-05	2.864E-05

Table 4.28. TCA-3, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	1.42818E-04	3.25054E-04	1.25124E-04	1.43107E-04	3.25739E-04	1.25325E-04
2	3.36929E-03	5.19745E-03	2.13299E-03	3.46178E-03	5.31513E-03	2.18128E-03
3	5.17928E-03	1.05930E-02	4.34726E-03	5.19818E-03	1.06224E-02	4.35933E-03
4	4.86050E-02	1.01190E-01	4.15275E-02	4.84951E-02	1.00958E-01	4.14323E-02

Table 4.29. TCA-3, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	4.44993E-03	8.27601E-03	2.93516E-03	4.47772E-03	8.36366E-03	2.96352E-03
2	3.65872E-02	3.54715E-06	1.46957E-06	3.65101E-02	3.54449E-06	1.46847E-06
3	7.01523E-03	2.46279E-08	1.02038E-08	7.00700E-03	2.46391E-08	1.02084E-08
4	2.76173E-02	1.29810E-07	5.37830E-08	2.75642E-02	1.29555E-07	5.36770E-08

Table 4.30. TCA-3, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	5.11491E-04	1.49361E-03	4.80637E-04	5.11798E-04	1.49459E-03	4.80689E-04
2	1.09264E-02	1.82048E-02	6.32153E-03	1.06379E-02	1.74194E-02	6.04882E-03
3	3.56962E-02	6.99270E-02	2.42818E-02	3.44527E-02	6.76673E-02	2.34972E-02
4	2.66921E-01	5.40191E-01	1.86841E-01	2.66795E-01	5.39735E-01	1.86684E-01

Table 4.31. TCA-3, Pin-78 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.243E-04	2.215E-04
2	8.038E-05	8.190E-05
3	1.810E-05	1.765E-05
4	5.962E-05	5.956E-05

Table 4.32. TCA-3, Pin-78 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	1.47728E-04	3.29228E-04	1.27610E-04	1.47738E-04	3.29429E-04	1.27667E-04
2	3.36825E-03	5.14716E-03	2.11235E-03	3.40828E-03	5.21512E-03	2.14023E-03
3	5.12983E-03	1.04660E-02	4.29517E-03	5.13172E-03	1.04717E-02	4.29747E-03
4	4.59777E-02	9.56112E-02	3.92380E-02	4.54550E-02	9.45238E-02	3.87918E-02

Table 4.33. TCA-3, Pin-78 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	4.31758E-03	7.42746E-03	2.63695E-03	4.34475E-03	7.50781E-03	2.66748E-03
2	3.69603E-02	3.91179E-06	1.62064E-06	3.60504E-02	3.75949E-06	1.55755E-06
3	6.98884E-03	2.44361E-08	1.01243E-08	6.98652E-03	2.44809E-08	1.01429E-08
4	2.62422E-02	1.23201E-07	5.10444E-08	2.59876E-02	1.21988E-07	5.05418E-08

Table 4.34. TCA-3, Pin-78 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	5.13304E-04	1.47258E-03	4.76835E-04	5.13774E-04	1.47465E-03	4.77404E-04
2	1.08802E-02	1.78741E-02	6.20669E-03	1.05497E-02	1.73471E-02	6.02371E-03
3	3.36764E-02	6.62210E-02	2.29950E-02	3.26723E-02	6.44142E-02	2.23675E-02
4	2.87561E-01	5.69182E-01	1.96949E-01	2.86127E-01	5.65714E-01	1.95759E-01

										6.107 (0.90)
									6.067 (0.43)	6.093 (0.43)
								5.865 (0.43)	5.933 (0.35)	5.977 (0.46)
							5.480 (0.46)	5.673 (0.35)	5.759 (0.31)	5.797 (0.43)
						4.989 (0.43)	5.244 (0.34)	5.447 (0.34)	5.513 (0.35)	5.571 (0.47)
					4.464 (0.56)	4.722 (0.35)	4.957 (0.33)	5.109 (0.36)	5.207 (0.35)	5.226 (0.47)
				3.839 (0.55)	4.125 (0.38)	4.412 (0.33)	4.611 (0.35)	4.762 (0.32)	4.805 (0.34)	4.824 (0.46)
			3.152 (0.60)	3.489 (0.40)	3.765 (0.38)	3.994 (0.35)	4.201 (0.34)	4.308 (0.38)	4.384 (0.35)	4.402 (0.52)
		2.601 (0.64)	2.827 (0.45)	3.120 (0.42)	3.374 (0.40)	3.577 (0.41)	3.735 (0.37)	3.861 (0.39)	3.933 (0.37)	3.954 (0.56)
	2.180 (0.76)	2.373 (0.47)	2.634 (0.45)	2.897 (0.44)	3.116 (0.42)	3.317 (0.44)	3.488 (0.39)	3.597 (0.37)	3.641 (0.41)	3.642 (0.57)
2.423 (0.70)	2.365 (0.50)	2.614 (0.49)	2.928 (0.42)	3.239 (0.43)	3.492 (0.39)	3.697 (0.36)	3.883 (0.36)	3.998 (0.39)	4.081 (0.36)	4.134 (0.53)

Fig. 4.8a. Pin-power distribution for CENTRM benchmark TCA-4. Value in parentheses is percent standard deviation.

										6.212 (0.86)
									6.114 (0.44)	6.159 (0.45)
								5.831 (0.44)	5.974 (0.31)	5.984 (0.46)
							5.529 (0.46)	5.708 (0.33)	5.770 (0.31)	5.819 (0.41)
						5.102 (0.47)	5.229 (0.35)	5.445 (0.32)	5.522 (0.33)	5.533 (0.42)
					4.470 (0.51)	4.777 (0.34)	4.968 (0.33)	5.140 (0.35)	5.202 (0.33)	5.243 (0.45)
				3.832 (0.54)	4.116 (0.40)	4.387 (0.37)	4.630 (0.35)	4.727 (0.32)	4.837 (0.33)	4.850 (0.46)
			3.129 (0.62)	3.495 (0.38)	3.735 (0.41)	4.030 (0.39)	4.197 (0.38)	4.309 (0.34)	4.374 (0.35)	4.458 (0.50)
		2.582 (0.69)	2.840 (0.45)	3.132 (0.46)	3.388 (0.42)	3.581 (0.39)	3.754 (0.40)	3.870 (0.38)	3.961 (0.38)	3.971 (0.51)
	2.185 (0.71)	2.350 (0.49)	2.643 (0.44)	2.904 (0.44)	3.128 (0.43)	3.330 (0.42)	3.500 (0.40)	3.601 (0.40)	3.672 (0.39)	3.710 (0.48)
2.436 (0.71)	2.386 (0.49)	2.626 (0.48)	2.916 (0.44)	3.228 (0.44)	3.505 (0.41)	3.706 (0.43)	3.883 (0.39)	3.981 (0.41)	4.062 (0.38)	4.100 (0.55)

Fig. 4.8b. Pin-power distribution for NITAWL benchmark TCA-4. Value in parentheses is percent standard deviation.



Table 4.35. Selected reaction rates for CENTRM case TCA-4

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.440E-05	2.393E-05	8.480E-06	5.581E-03	0.235
	Clad	2.746E-07	0.0	0.0	1.739E-03	0.073
	Mod.	7.889E-07	0.0	0.0	1.642E-02	0.692
66	Fuel	4.055E-05	6.181E-05	2.186E-05	2.281E-02	0.235
	Clad	8.066E-07	0.0	0.0	7.166E-03	0.074
	Mod.	1.867E-06	0.0	0.0	6.712E-02	0.691

Table 4.36. Selected reaction rates for NITAWL case TCA-4

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.464E-05	2.446E-05	8.665E-06	5.642E-03	0.236
	Clad	2.772E-07	0.0	0.0	1.754E-03	0.073
	Mod.	7.942E-07	0.0	0.0	1.652E-02	0.691
66	Fuel	4.061E-05	6.263E-05	2.216E-05	2.295E-02	0.234
	Clad	8.106E-07	0.0	0.0	7.227E-03	0.074
	Mod.	1.885E-06	0.0	0.0	6.790E-02	0.692

Table 4.37. TCA-4, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	5.137E-05	5.198E-05
2	1.508E-05	1.488E-05
3	3.637E-06	3.684E-06
4	3.178E-05	3.244E-05

Table 4.38. TCA-4, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	1.42972E-04	3.25729E-04	1.25284E-04	1.42717E-04	3.25108E-04	1.25072E-04
2	3.54777E-03	5.40060E-03	2.21636E-03	3.49262E-03	5.32638E-03	2.18590E-03
3	5.19612E-03	1.06384E-02	4.36591E-03	5.19563E-03	1.06220E-02	4.35917E-03
4	4.87823E-02	1.01563E-01	4.16806E-02	4.89171E-02	1.01845E-01	4.17962E-02

Table 4.39. TCA-4, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	4.51308E-03	8.46385E-03	3.00241E-03	4.47482E-03	8.38222E-03	2.97205E-03
2	3.86113E-02	3.72395E-06	1.54282E-06	3.54513E-02	3.52350E-06	1.45977E-06
3	7.00737E-03	2.46436E-08	1.02103E-08	7.01355E-03	2.47048E-08	1.02357E-08
4	2.77151E-02	1.30278E-07	5.39767E-08	2.77735E-02	1.30557E-07	5.40922E-08

Table 4.40. TCA-4, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	5.12178E-04	1.49692E-03	4.81232E-04	5.11274E-04	1.49406E-03	4.80446E-04
2	1.11540E-02	1.83841E-02	6.38377E-03	1.08239E-02	1.78689E-02	6.20489E-03
3	3.46250E-02	6.79736E-02	2.36035E-02	3.48586E-02	6.84167E-02	2.37574E-02
4	2.65578E-01	5.38310E-01	1.86183E-01	2.66229E-01	5.39667E-01	1.86654E-01

Table 4.41. TCA-4, Pin-66 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.378E-04	2.383E-04
2	8.358E-05	8.422E-05
3	1.882E-05	1.898E-05
4	7.623E-05	7.746E-05

Table 4.42. TCA-4, Pin-66 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	1.47181E-04	3.29323E-04	1.27404E-04	1.47030E-04	3.28757E-04	1.27281E-04
2	3.46397E-03	5.28525E-03	2.16902E-03	3.45056E-03	5.27803E-03	2.16605E-03
3	5.05350E-03	1.03193E-02	4.23494E-03	5.07799E-03	1.03695E-02	4.25556E-03
4	4.64067E-02	9.65304E-02	3.96152E-02	4.62458E-02	9.61957E-02	3.94779E-02

Table 4.43. TCA-4, Pin-66 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	4.36716E-03	7.64672E-03	2.70927E-03	4.35812E-03	7.61288E-03	2.70342E-03
2	4.02182E-02	3.82265E-06	1.58372E-06	3.67393E-02	3.69650E-06	1.53144E-06
3	6.96068E-03	2.41878E-08	1.00214E-08	6.97476E-03	2.43271E-08	1.00792E-08
4	2.64749E-02	1.24324E-07	5.15096E-08	2.63939E-02	1.23940E-07	5.13506E-08

Table 4.44. TCA-4, Pin-66 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	5.13616E-04	1.47840E-03	4.77839E-04	5.13256E-04	1.47677E-03	4.77633E-04
2	1.11268E-02	1.82952E-02	6.35292E-03	1.07160E-02	1.75431E-02	6.09175E-03
3	3.23976E-02	6.38268E-02	2.21636E-02	3.30910E-02	6.51217E-02	2.26133E-02
4	2.81830E-01	5.60508E-01	1.93933E-01	2.81951E-01	5.60363E-01	1.93887E-01

										5.973 (0.85)
									5.841 (0.44)	5.875 (0.49)
								5.617 (0.45)	5.723 (0.34)	5.821 (0.42)
							5.245 (0.44)	5.464 (0.33)	5.537 (0.33)	5.623 (0.44)
						4.824 (0.47)	5.071 (0.31)	5.205 (0.30)	5.288 (0.29)	5.352 (0.47)
				4.271 (0.53)	4.523 (0.33)	4.753 (0.30)	4.916 (0.31)	4.981 (0.34)	5.050 (0.44)	
			3.643 (0.55)	3.966 (0.37)	4.187 (0.38)	4.389 (0.35)	4.507 (0.34)	4.630 (0.34)	4.648 (0.50)	
		3.029 (0.59)	3.330 (0.42)	3.604 (0.41)	3.798 (0.40)	3.987 (0.38)	4.110 (0.36)	4.165 (0.36)	4.228 (0.48)	
	2.450 (0.65)	2.713 (0.44)	2.973 (0.41)	3.230 (0.39)	3.385 (0.41)	3.574 (0.39)	3.709 (0.42)	3.777 (0.37)	3.781 (0.56)	
	2.050 (0.75)	2.254 (0.48)	2.522 (0.47)	2.750 (0.45)	2.981 (0.46)	3.176 (0.38)	3.331 (0.38)	3.429 (0.35)	3.508 (0.41)	3.534 (0.55)
2.283 (0.66)	2.260 (0.50)	2.500 (0.47)	2.828 (0.43)	3.060 (0.41)	3.331 (0.40)	3.528 (0.37)	3.725 (0.37)	3.815 (0.39)	3.867 (0.37)	3.921 (0.50)

Fig. 4.9a. Pin-power distribution for CENTRM benchmark TCA-5. Value in parentheses is percent standard deviation.

										5.872 (0.90)
									5.824 (0.44)	5.930 (0.43)
								5.663 (0.47)	5.775 (0.33)	5.815 (0.46)
							5.278 (0.44)	5.523 (0.31)	5.575 (0.32)	5.572 (0.46)
						4.844 (0.50)	5.069 (0.31)	5.219 (0.32)	5.311 (0.31)	5.323 (0.47)
				4.326 (0.49)	4.538 (0.35)	4.742 (0.33)	4.945 (0.33)	5.011 (0.32)	5.054 (0.46)	
			3.679 (0.54)	3.942 (0.34)	4.189 (0.36)	4.400 (0.36)	4.534 (0.35)	4.638 (0.33)	4.691 (0.53)	
		3.002 (0.59)	3.342 (0.40)	3.606 (0.38)	3.840 (0.35)	4.021 (0.35)	4.138 (0.38)	4.209 (0.38)	4.213 (0.54)	
	2.468 (0.64)	2.720 (0.49)	2.999 (0.42)	3.225 (0.45)	3.440 (0.39)	3.582 (0.41)	3.702 (0.40)	3.771 (0.38)	3.783 (0.53)	
	2.075 (0.66)	2.259 (0.54)	2.518 (0.45)	2.768 (0.45)	3.015 (0.41)	3.168 (0.43)	3.345 (0.39)	3.455 (0.40)	3.474 (0.39)	3.504 (0.54)
2.297 (0.69)	2.263 (0.45)	2.480 (0.49)	2.792 (0.42)	3.046 (0.38)	3.316 (0.41)	3.535 (0.39)	3.708 (0.38)	3.801 (0.38)	3.876 (0.36)	3.904 (0.55)

Fig. 4.9b. Pin-power distribution for NITAWL benchmark TCA-5. Value in parentheses is percent standard deviation.

Table 4.45. Selected reaction rates for CENTRM case TCA-5

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.374E-05	2.280E-05	8.078E-06	5.603E-03	0.235
	Clad	2.618E-07	0.0	0.0	1.747E-03	0.074
	Mod.	7.503E-07	0.0	0.0	1.646E-02	0.691
66	Fuel	3.907E-05	5.970E-05	2.112E-05	2.311E-02	0.235
	Clad	7.783E-07	0.0	0.0	7.263E-03	0.074
	Mod.	1.793E-06	0.0	0.0	6.806E-02	0.691

Table 4.46. Selected reaction rates for NITAWL case TCA-5

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.378E-05	2.293E-05	8.127E-06	5.603E-03	0.235
	Clad	2.619E-07	0.0	0.0	1.745E-03	0.074
	Mod.	7.543E-07	0.0	0.0	1.646E-02	0.691
66	Fuel	3.868E-05	5.889E-05	2.084E-05	2.304E-02	0.234
	Clad	7.727E-07	0.0	0.0	7.281E-03	0.074
	Mod.	1.803E-06	0.0	0.0	6.824E-02	0.692

Table 4.47. TCA-5, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	4.939E-05	4.938E-05
2	1.446E-05	1.412E-05
3	3.466E-06	3.579E-06
4	3.035E-05	3.059E-05

Table 4.48. TCA-5, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	1.42994E-04	3.26070E-04	1.25328E-04	1.43122E-04	3.25555E-04	1.25325E-04
2	3.42309E-03	5.26214E-03	2.15954E-03	3.47849E-03	5.29943E-03	2.17484E-03
3	5.14146E-03	1.04884E-02	4.30436E-03	5.22434E-03	1.06706E-02	4.37913E-03
4	4.87407E-02	1.01475E-01	4.16445E-02	4.86829E-02	1.01355E-01	4.15953E-02

Table 4.49. TCA-5, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	4.50583E-03	8.47688E-03	2.99982E-03	4.48281E-03	8.35527E-03	2.96632E-03
2	3.83667E-02	3.84273E-06	1.59203E-06	3.62671E-02	3.53982E-06	1.46653E-06
3	7.00150E-03	2.45134E-08	1.01563E-08	7.02110E-03	2.47448E-08	1.02522E-08
4	2.76871E-02	1.30144E-07	5.39213E-08	2.76564E-02	1.30000E-07	5.38614E-08

Table 4.50. TCA-5, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	5.12069E-04	1.49754E-03	4.81215E-04	5.11841E-04	1.49393E-03	4.80664E-04
2	1.09615E-02	1.82420E-02	6.33444E-03	1.10261E-02	1.81861E-02	6.31503E-03
3	3.50990E-02	6.88148E-02	2.38956E-02	3.48620E-02	6.84733E-02	2.37771E-02
4	2.66585E-01	5.39901E-01	1.86737E-01	2.66263E-01	5.39232E-01	1.86508E-01

Table 4.51. TCA-5, Pin-66 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.303E-04	2.296E-04
2	8.041E-05	8.059E-05
3	1.804E-05	1.799E-05
4	7.411E-05	7.336E-05

Table 4.52. TCA-5, Pin-66 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	1.47516E-04	3.29683E-04	1.27617E-04	1.46906E-04	3.28595E-04	1.27226E-04
2	3.45804E-03	5.28540E-03	2.16908E-03	3.42799E-03	5.19278E-03	2.13107E-03
3	5.21778E-03	1.06625E-02	4.37578E-03	5.17950E-03	1.05856E-02	4.34425E-03
4	4.63091E-02	9.63284E-02	3.95323E-02	4.61333E-02	9.59635E-02	3.93825E-02

Table 4.53. TCA-5, Pin-66 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	4.38259E-03	7.65041E-03	2.71517E-03	4.35318E-03	7.60571E-03	2.70175E-03
2	3.76966E-02	3.76282E-06	1.55892E-06	3.76657E-02	3.47384E-06	1.43920E-06
3	7.01397E-03	2.46319E-08	1.02054E-08	6.99839E-03	2.45177E-08	1.01581E-08
4	2.64310E-02	1.24116E-07	5.14236E-08	2.63412E-02	1.23688E-07	5.12462E-08

Table 4.54. TCA-5, Pin-66 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	5.14155E-04	1.47850E-03	4.78094E-04	5.13349E-04	1.47737E-03	4.77888E-04
2	1.09920E-02	1.80785E-02	6.27768E-03	1.06624E-02	1.75079E-02	6.07953E-03
3	3.48251E-02	6.83614E-02	2.37382E-02	3.45711E-02	6.78516E-02	2.35613E-02
4	2.81194E-01	5.59228E-01	1.93491E-01	2.80259E-01	5.57291E-01	1.92823E-01



										5.446 (0.87)
									5.462 (0.45)	5.433 (0.42)
								5.225 (0.40)	5.327 (0.30)	5.357 (0.42)
							4.915 (0.44)	5.049 (0.30)	5.160 (0.34)	5.185 (0.43)
						4.477 (0.48)	4.691 (0.37)	4.860 (0.33)	4.954 (0.36)	4.957 (0.47)
					3.976 (0.52)	4.231 (0.37)	4.430 (0.37)	4.569 (0.33)	4.651 (0.31)	4.688 (0.46)
				3.440 (0.56)	3.685 (0.42)	3.916 (0.36)	4.084 (0.36)	4.239 (0.34)	4.317 (0.35)	4.338 (0.50)
			2.811 (0.62)	3.097 (0.39)	3.347 (0.37)	3.552 (0.34)	3.704 (0.36)	3.855 (0.39)	3.900 (0.33)	3.925 (0.48)
		2.272 (0.65)	2.533 (0.42)	2.797 (0.37)	3.010 (0.43)	3.216 (0.43)	3.339 (0.40)	3.445 (0.33)	3.528 (0.38)	3.528 (0.59)
	1.928 (0.76)	2.090 (0.51)	2.327 (0.47)	2.570 (0.45)	2.789 (0.40)	2.962 (0.40)	3.081 (0.42)	3.182 (0.38)	3.274 (0.42)	3.260 (0.56)
2.123 (0.72)	2.094 (0.47)	2.324 (0.47)	2.602 (0.41)	2.847 (0.39)	3.072 (0.40)	3.294 (0.40)	3.461 (0.41)	3.543 (0.36)	3.638 (0.36)	3.680 (0.54)

Fig. 4.10a. Pin-power distribution for CENTRM benchmark TCA-6. Value in parentheses is percent standard deviation.

										5.535 (0.82)
									5.433 (0.45)	5.485 (0.41)
								5.208 (0.43)	5.336 (0.30)	5.380 (0.44)
							4.903 (0.45)	5.056 (0.32)	5.155 (0.31)	5.224 (0.42)
						4.478 (0.50)	4.745 (0.32)	4.840 (0.32)	4.949 (0.31)	5.009 (0.47)
					3.945 (0.51)	4.219 (0.35)	4.437 (0.34)	4.592 (0.34)	4.656 (0.35)	4.662 (0.46)
				3.402 (0.55)	3.677 (0.37)	3.935 (0.36)	4.103 (0.36)	4.259 (0.35)	4.279 (0.33)	4.347 (0.51)
			2.808 (0.56)	3.096 (0.43)	3.349 (0.38)	3.556 (0.37)	3.711 (0.36)	3.858 (0.35)	3.908 (0.35)	3.932 (0.47)
		2.286 (0.62)	2.545 (0.44)	2.795 (0.38)	3.014 (0.42)	3.211 (0.41)	3.340 (0.38)	3.434 (0.35)	3.501 (0.39)	3.547 (0.56)
	1.930 (0.79)	2.114 (0.47)	2.328 (0.48)	2.571 (0.47)	2.784 (0.43)	2.977 (0.38)	3.106 (0.36)	3.198 (0.41)	3.269 (0.38)	3.308 (0.52)
2.129 (0.65)	2.105 (0.45)	2.328 (0.49)	2.622 (0.41)	2.861 (0.43)	3.096 (0.38)	3.292 (0.40)	3.450 (0.38)	3.563 (0.40)	3.618 (0.35)	3.656 (0.57)

Fig. 4.10b. Pin-power distribution for NITAWL benchmark TCA-6. Value in parentheses is percent standard deviation.

Table 4.55. Selected reaction rates for CENTRM case TCA-6

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.298E-05	2.136E-05	7.574E-06	5.637E-03	0.235
	Clad	2.474E-07	0.0	0.0	1.759E-03	0.073
	Mod.	7.049E-07	0.0	0.0	1.659E-02	0.692
66	Fuel	3.599E-05	5.470E-05	1.936E-05	2.295E-02	0.234
	Clad	7.226E-07	0.0	0.0	7.268E-03	0.074
	Mod.	1.669E-06	0.0	0.0	6.776E-02	0.692

Table 4.56. Selected reaction rates for NITAWL case TCA-6

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.301E-05	2.152E-05	7.630E-06	5.677E-03	0.236
	Clad	2.482E-07	0.0	0.0	1.771E-03	0.073
	Mod.	7.104E-07	0.0	0.0	1.663E-02	0.691
66	Fuel	3.641E-05	5.549E-05	1.964E-05	2.328E-02	0.235
	Clad	7.250E-07	0.0	0.0	7.322E-03	0.074
	Mod.	1.692E-06	0.0	0.0	6.857E-02	0.691

Table 4.57. TCA-6, Pin-1 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	4.562E-05	4.614E-05
2	1.353E-05	1.361E-05
3	3.260E-06	3.167E-06
4	2.877E-05	2.891E-05

Table 4.58. TCA-6, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	1.43180E-04	3.25454E-04	1.25334E-04	1.42890E-04	3.25301E-04	1.25170E-04
2	3.45574E-03	5.26068E-03	2.15894E-03	3.46874E-03	5.30446E-03	2.17691E-03
3	5.12187E-03	1.04432E-02	4.28580E-03	5.18636E-03	1.05942E-02	4.34774E-03
4	4.87091E-02	1.01408E-01	4.16173E-02	4.87392E-02	1.01468E-01	4.16413E-02

Table 4.59. TCA-6, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	4.44759E-03	8.24022E-03	2.92337E-03	4.46693E-03	8.35598E-03	2.96179E-03
2	3.90256E-02	3.50820E-06	1.45343E-06	3.57765E-02	3.56985E-06	1.47897E-06
3	6.98181E-03	2.44734E-08	1.01398E-08	7.00395E-03	2.46168E-08	1.01992E-08
4	2.76742E-02	1.30082E-07	5.38954E-08	2.76818E-02	1.30118E-07	5.39104E-08

Table 4.60. TCA-6, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	5.11662E-04	1.49257E-03	4.80489E-04	5.11324E-04	1.49329E-03	4.80338E-04
2	1.13135E-02	1.86601E-02	6.47963E-03	1.07085E-02	1.75213E-02	6.08419E-03
3	3.39736E-02	6.67666E-02	2.31844E-02	3.36473E-02	6.62052E-02	2.29895E-02
4	2.66162E-01	5.39117E-01	1.86465E-01	2.67553E-01	5.41501E-01	1.87294E-01

Table 4.61. TCA-6, Pin-66 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	2.129E-04	2.141E-04
2	7.322E-05	7.593E-05
3	1.668E-05	1.698E-05
4	6.844E-05	6.955E-05

Table 4.62. TCA-6, Pin-66 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	1.46734E-04	3.28401E-04	1.27150E-04	1.47522E-04	3.29450E-04	1.27598E-04
2	3.38204E-03	5.17330E-03	2.12307E-03	3.41355E-03	5.23610E-03	2.14885E-03
3	5.13990E-03	1.04899E-02	4.30497E-03	5.04984E-03	1.02714E-02	4.21529E-03
4	4.64337E-02	9.65915E-02	3.96403E-02	4.61970E-02	9.60939E-02	3.94361E-02

Table 4.63. TCA-6, Pin-66 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	4.34898E-03	7.60907E-03	2.70457E-03	4.36295E-03	7.58351E-03	2.69381E-03
2	3.85262E-02	3.68752E-06	1.52772E-06	3.74174E-02	3.59244E-06	1.48833E-06
3	6.99508E-03	2.44889E-08	1.01462E-08	6.96908E-03	2.42193E-08	1.00345E-08
4	2.64864E-02	1.24380E-07	5.15332E-08	2.63675E-02	1.23812E-07	5.12979E-08

Table 4.64. TCA-6, Pin-66 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	5.13250E-04	1.47784E-03	4.78051E-04	5.13989E-04	1.47716E-03	4.77940E-04
2	1.13093E-02	1.84779E-02	6.41636E-03	1.07147E-02	1.76559E-02	6.13092E-03
3	3.39521E-02	6.67206E-02	2.31683E-02	3.32187E-02	6.53557E-02	2.26946E-02
4	2.81522E-01	5.60045E-01	1.93774E-01	2.81843E-01	5.60105E-01	1.93799E-01

									7.308 (0.44)
								7.112 (0.39)	7.241 (0.35)
							6.694 (0.43)	6.907 (0.26)	7.038 (0.31)
						6.068 (0.46)	6.408 (0.30)	6.595 (0.30)	6.694 (0.30)
					5.368 (0.55)	5.743 (0.35)	6.028 (0.33)	6.153 (0.34)	6.308 (0.29)
				4.563 (0.47)	4.998 (0.34)	5.297 (0.35)	5.515 (0.33)	5.710 (0.30)	5.792 (0.32)
			3.708 (0.54)	4.107 (0.38)	4.467 (0.38)	4.726 (0.34)	4.996 (0.34)	5.135 (0.34)	5.182 (0.36)
		2.884 (0.72)	3.250 (0.41)	3.615 (0.38)	3.950 (0.39)	4.203 (0.34)	4.373 (0.37)	4.511 (0.36)	4.579 (0.39)
	2.218 (0.76)	2.524 (0.48)	2.866 (0.44)	3.179 (0.45)	3.463 (0.41)	3.694 (0.41)	3.852 (0.37)	3.966 (0.40)	4.027 (0.40)
2.112 (0.73)	2.218 (0.54)	2.550 (0.48)	2.879 (0.44)	3.211 (0.40)	3.481 (0.45)	3.706 (0.38)	3.893 (0.38)	4.026 (0.39)	4.085 (0.37)

Fig. 4.11a. Pin-power distribution for CENTRM benchmark TCA-7. Value in parentheses is percent standard deviation.

									7.408 (0.42)
								7.147 (0.41)	7.221 (0.26)
							6.690 (0.44)	6.948 (0.30)	7.021 (0.30)
						6.147 (0.44)	6.439 (0.33)	6.607 (0.32)	6.750 (0.30)
					5.413 (0.49)	5.784 (0.37)	6.036 (0.33)	6.174 (0.32)	6.317 (0.30)
				4.575 (0.52)	5.009 (0.37)	5.294 (0.35)	5.496 (0.34)	5.716 (0.32)	5.817 (0.31)
			3.668 (0.55)	4.106 (0.38)	4.503 (0.34)	4.750 (0.37)	4.980 (0.35)	5.1116 (0.36)	5.231 (0.33)
		2.847 (0.66)	3.251 (0.41)	3.587 (0.40)	3.919 (0.38)	4.192 (0.41)	4.381 (0.40)	4.515 (0.36)	4.586 (0.37)
	2.218 (0.66)	2.533 (0.50)	2.857 (0.45)	3.206 (0.44)	3.499 (0.42)	3.700 (0.35)	3.863 (0.35)	3.987 (0.43)	4.057 (0.39)
2.101 (0.67)	2.211 (0.53)	2.557 (0.45)	2.878 (0.46)	3.214 (0.43)	3.494 (0.40)	3.723 (0.40)	3.929 (0.39)	4.019 (0.36)	4.082 (0.39)

Fig. 4.11b. Pin-power distribution for NITAWL benchmark TCA-7. Value in parentheses is percent standard deviation.

Table 4.65. Selected reaction rates for CENTRM case TCA-7

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.250E-05	2.098E-05	7.436E-06	4.475E-03	0.181
	Clad	2.338E-07	0.0	0.0	1.390E-03	0.056
	Mod.	7.159E-07	0.0	0.0	1.884E-02	0.763
55	Fuel	4.638E-05	7.357E-05	2.604E-05	2.167E-02	0.182
	Clad	8.926E-07	0.0	0.0	6.796E-03	0.057
	Mod.	2.331E-06	0.0	0.0	9.081E-02	0.761

Table 4.66. Selected reaction rates for NITAWL case TCA-7

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.239E-05	2.081E-05	7.375E-06	4.405E-03	0.181
	Clad	2.328E-07	0.0	0.0	1.370E-03	0.056
	Mod.	7.088E-07	0.0	0.0	1.861E-02	0.763
55	Fuel	4.646E-05	7.384E-05	2.619E-05	2.180E-02	0.182
	Clad	8.849E-07	0.0	0.0	6.807E-03	0.057
	Mod.	2.324E-06	0.0	0.0	9.112E-02	0.761



Table 4.67. TCA-7, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	4.076E-05	4.002E-05
2	1.156E-05	1.122E-05
3	2.916E-06	2.849E-06
4	2.805E-05	2.789E-05

Table 4.68. TCA-7, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	1.42491E-04	3.25106E-04	1.25005E-04	1.41299E-04	3.24300E-04	1.24414E-04
2	3.44975E-03	5.22773E-03	2.14542E-03	3.47152E-03	5.26026E-03	2.15876E-03
3	5.21159E-03	1.06607E-02	4.37503E-03	5.27529E-03	1.08126E-02	4.43738E-03
4	4.89248E-02	1.01867E-01	4.18053E-02	4.88655E-02	1.01743E-01	4.17544E-02

Table 4.69. TCA-7, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	4.51148E-03	8.48982E-03	3.01170E-03	4.53551E-03	8.70929E-03	3.08361E-03
2	3.80608E-02	3.86401E-06	1.60085E-06	3.81145E-02	3.57483E-06	1.48104E-06
3	7.01523E-03	2.46902E-08	1.02296E-08	7.02506E-03	2.48652E-08	1.03021E-08
4	2.77876E-02	1.30626E-07	5.41212E-08	2.77567E-02	1.30480E-07	5.40602E-08

Table 4.70. TCA-7, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	5.11889E-04	1.49757E-03	4.81327E-04	5.11022E-04	1.50238E-03	4.81994E-04
2	1.09768E-02	1.79177E-02	6.22185E-03	1.09889E-02	1.81187E-02	6.29163E-03
3	3.46245E-02	6.80175E-02	2.36188E-02	3.47959E-02	6.83577E-02	2.37369E-02
4	2.64817E-01	5.37348E-01	1.85848E-01	2.63994E-01	5.35812E-01	1.85317E-01

Table 4.71. TCA-7, Pin-55 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.186E-04	2.205E-04
2	7.342E-05	7.405E-05
3	1.743E-05	1.715E-05
4	9.388E-05	9.404E-05

Table 4.72. TCA-7, Pin-55 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	1.46008E-04	3.28325E-04	1.26835E-04	1.45867E-04	3.28061E-04	1.26745E-04
2	3.45407E-03	5.28814E-03	2.17020E-03	3.44685E-03	5.26736E-03	2.16167E-03
3	5.22363E-03	1.06689E-02	4.37843E-03	5.15115E-03	1.05143E-02	4.31500E-03
4	4.73673E-02	9.85703E-02	4.04524E-02	4.74047E-02	9.86425E-02	4.04820E-02

Table 4.73. TCA-7, Pin-55 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	4.42752E-03	7.91693E-03	2.81011E-03	4.41279E-03	7.88612E-03	2.79909E-03
2	3.99843E-02	3.82517E-06	1.58476E-06	3.88724E-02	3.70637E-06	1.53553E-06
3	7.01291E-03	2.46832E-08	1.02267E-08	6.99207E-03	2.45220E-08	1.01599E-08
4	2.69759E-02	1.26733E-07	5.25080E-08	2.69906E-02	1.26799E-07	5.25354E-08

Table 4.74. TCA-7, Pin-55 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	5.13362E-04	1.48414E-03	4.78998E-04	5.13238E-04	1.48384E-03	4.78975E-04
2	1.13505E-02	1.86607E-02	6.47983E-03	1.09736E-02	1.80388E-02	6.26385E-03
3	3.48495E-02	6.84159E-02	2.37571E-02	3.38470E-02	6.65440E-02	2.31071E-02
4	2.74694E-01	5.50591E-01	1.90475E-01	2.75966E-01	5.52786E-01	1.91235E-01

									7.058 (0.42)
								6.778 (0.45)	6.930 (0.30)
							6.434 (0.40)	6.596 (0.28)	6.745 (0.31)
						5.871 (0.47)	6.133 (0.33)	6.327 (0.30)	6.451 (0.29)
					5.168 (0.48)	5.489 (0.32)	5.742 (0.35)	5.939 (0.31)	6.053 (0.31)
				4.377 (0.49)	4.767 (0.33)	5.039 (0.34)	5.336 (0.33)	5.465 (0.33)	5.519 (0.32)
			3.520 (0.56)	3.936 (0.40)	4.294 (0.38)	4.552 (0.35)	4.754 (0.36)	4.920 (0.32)	4.979 (0.34)
		2.777 (0.66)	3.119 (0.45)	3.500 (0.39)	3.787 (0.45)	4.040 (0.37)	4.186 (0.35)	4.325 (0.33)	4.397 (0.36)
	2.148 (0.70)	2.439 (0.51)	2.772 (0.46)	3.062 (0.39)	3.330 (0.39)	3.540 (0.40)	3.714 (0.42)	3.803 (0.37)	3.857 (0.39)
2.037 (0.75)	2.140 (0.50)	2.445 (0.49)	2.777 (0.46)	3.109 (0.42)	3.342 (0.42)	3.553 (0.38)	3.728 (0.41)	3.851 (0.40)	3.923 (0.39)

Fig. 4.12a. Pin-power distribution for CENTRM benchmark TCA-8. Value in parentheses is percent standard deviation.

									7.087 (0.46)
								6.790 (0.41)	6.919 (0.28)
							6.419 (0.42)	6.669 (0.27)	6.737 (0.32)
						5.900 (0.43)	6.151 (0.30)	6.328 (0.27)	6.378 (0.33)
					5.179 (0.50)	5.512 (0.31)	5.799 (0.30)	5.942 (0.31)	6.021 (0.31)
				4.388 (0.53)	4.751 (0.35)	5.082 (0.35)	5.308 (0.31)	5.501 (0.31)	5.566 (0.31)
			3.547 (0.55)	3.954 (0.39)	4.305 (0.40)	4.595 (0.33)	4.764 (0.36)	4.941 (0.34)	4.987 (0.34)
		2.717 (0.67)	3.141 (0.42)	3.469 (0.43)	3.797 (0.38)	4.026 (0.36)	4.223 (0.36)	4.326 (0.36)	4.387 (0.37)
	2.140 (0.71)	2.434 (0.47)	2.753 (0.43)	3.061 (0.44)	3.313 (0.40)	3.540 (0.40)	3.695 (0.40)	3.832 (0.42)	3.886 (0.38)
2.055 (0.75)	2.128 (0.49)	2.452 (0.45)	2.780 (0.44)	3.082 (0.44)	3.377 (0.39)	3.615 (0.40)	3.740 (0.39)	3.859 (0.40)	3.928 (0.38)

Fig. 4.12b. Pin-power distribution for NITAWL benchmark TCA-8. Value in parentheses is percent standard deviation.

Table 4.75. Selected reaction rates for CENTRM case TCA-8

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.219E-05	2.033E-05	7.204E-06	4.521E-03	0.182
	Clad	2.267E-07	0.0	0.0	1.397E-03	0.056
	Mod.	6.904E-07	0.0	0.0	1.890E-02	0.762
55	Fuel	4.454E-05	7.082E-05	2.507E-05	2.182E-02	0.182
	Clad	8.569E-07	0.0	0.0	6.833E-03	0.057
	Mod.	2.247E-06	0.0	0.0	9.140E-02	0.761

Table 4.76. Selected reaction rates for NITAWL case TCA-8

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.228E-05	2.056E-05	7.288E-06	4.508E-03	0.182
	Clad	2.273E-07	0.0	0.0	1.396E-03	0.056
	Mod.	6.917E-07	0.0	0.0	1.890E-02	0.762
55	Fuel	4.442E-05	7.058E-05	2.499E-05	2.172E-02	0.182
	Clad	8.512E-07	0.0	0.0	6.810E-03	0.057
	Mod.	2.244E-06	0.0	0.0	9.104E-02	0.761

Table 4.77. TCA-8, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	3.944E-05	3.890E-05
2	1.103E-05	1.116E-05
3	2.823E-06	2.632E-06
4	2.727E-05	2.765E-05

Table 4.78. TCA-8, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{<G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{<G}_f$	$\underline{G}_f$
1	1.42334E-04	3.25312E-04	1.24980E-04	1.42088E-04	3.25219E-04	1.24828E-04
2	3.53127E-03	5.35172E-03	2.19630E-03	3.46204E-03	5.26653E-03	2.16133E-03
3	5.12848E-03	1.04583E-02	4.29199E-03	5.21250E-03	1.06698E-02	4.37876E-03
4	4.88629E-02	1.01736E-01	4.17514E-02	4.88872E-02	1.01784E-01	4.17714E-02

Table 4.79. TCA-8, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{<G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{<G}_f$	$\underline{G}_f$
1	4.53489E-03	8.60396E-03	3.05003E-03	4.52758E-03	8.62663E-03	3.05064E-03
2	4.11256E-02	3.90524E-06	1.61793E-06	3.90452E-02	3.64034E-06	1.50818E-06
3	6.97793E-03	2.43563E-08	1.00913E-08	7.01079E-03	2.46993E-08	1.02334E-08
4	2.77529E-02	1.30460E-07	5.40521E-08	2.77661E-02	1.30523E-07	5.40785E-08

Table 4.80. TCA-8, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{<G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{<G}_f$	$\underline{G}_f$
1	5.11790E-04	1.49952E-03	4.81643E-04	5.11429E-04	1.50018E-03	4.81447E-04
2	1.15051E-02	1.87178E-02	6.49966E-03	1.06573E-02	1.75647E-02	6.09924E-03
3	3.42439E-02	6.71877E-02	2.33306E-02	3.42088E-02	6.72576E-02	2.33550E-02
4	2.65649E-01	5.38621E-01	1.86291E-01	2.65522E-01	5.38441E-01	1.86228E-01

Table 4.81. TCA-8, Pin-55 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.110E-04	2.107E-04
2	7.037E-05	6.962E-05
3	1.673E-05	1.667E-05
4	9.070E-05	9.010E-05

Table 4.82. TCA-8, Pin-55 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	1.45480E-04	3.27674E-04	1.26526E-04	1.45435E-04	3.27709E-04	1.26510E-04
2	3.39048E-03	5.20276E-03	2.13517E-03	3.47111E-03	5.30325E-03	2.17640E-03
3	5.13229E-03	1.04562E-02	4.29112E-03	5.19965E-03	1.06013E-02	4.35069E-03
4	4.74630E-02	9.87671E-02	4.05332E-02	4.77188E-02	9.92999E-02	4.07518E-02

Table 4.83. TCA-8, Pin-55 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	4.41327E-03	7.93014E-03	2.81274E-03	4.42132E-03	7.95819E-03	2.82199E-03
2	3.87344E-02	3.80772E-06	1.57752E-06	3.76439E-02	3.63710E-06	1.50684E-06
3	6.98380E-03	2.43899E-08	1.01051E-08	7.00174E-03	2.45717E-08	1.01805E-08
4	2.70204E-02	1.26942E-07	5.25946E-08	2.71446E-02	1.27535E-07	5.28402E-08

Table 4.84. TCA-8, Pin-55 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	5.12787E-04	1.48453E-03	4.78981E-04	5.12848E-04	1.48514E-03	4.79084E-04
2	1.11398E-02	1.83762E-02	6.38104E-03	1.10696E-02	1.81030E-02	6.28615E-03
3	3.39692E-02	6.67376E-02	2.31743E-02	3.43528E-02	6.74775E-02	2.34313E-02
4	2.75637E-01	5.52375E-01	1.91090E-01	2.76264E-01	5.53948E-01	1.91632E-01

									6.747 (0.46)
								6.520 (0.40)	6.616 (0.30)
							6.164 (0.40)	6.297 (0.32)	6.417 (0.30)
						5.649 (0.43)	5.915 (0.30)	6.064 (0.29)	6.158 (0.28)
					4.974 (0.43)	5.311 (0.34)	5.553 (0.30)	5.732 (0.31)	5.793 (0.30)
				4.210 (0.48)	4.568 (0.33)	4.907 (0.35)	5.111 (0.33)	5.265 (0.31)	5.318 (0.33)
			3.447 (0.56)	3.807 (0.37)	4.124 (0.34)	4.379 (0.38)	4.589 (0.34)	4.729 (0.33)	4.777 (0.33)
		2.642 (0.62)	2.995 (0.40)	3.353 (0.42)	3.657 (0.39)	3.869 (0.38)	4.027 (0.38)	4.147 (0.35)	4.236 (0.38)
	2.049 (0.75)	2.330 (0.49)	2.663 (0.46)	3.948 (0.44)	3.206 (0.42)	3.412 (0.41)	3.586 (0.37)	3.704 (0.39)	3.745 (0.38)
1.975 (0.75)	2.076 (0.52)	2.378 (0.48)	2.685 (0.44)	2.993 (0.43)	3.228 (0.41)	3.452 (0.36)	3.579 (0.39)	3.723 (0.38)	3.736 (0.38)

Fig. 4.13a. Pin-power distribution for CENTRM benchmark TCA-9. Value in parentheses is percent standard deviation.



									6.800 (0.46)
								6.580 (0.38)	6.670 (0.31)
							6.176 (0.41)	6.363 (0.29)	6.453 (0.30)
						5.635 (0.47)	5.898 (0.29)	6.091 (0.28)	6.195 (0.30)
					5.005 (0.45)	5.293 (0.32)	5.511 (0.31)	5.719 (0.32)	5.831 (0.31)
				4.282 (0.51)	4.566 (0.35)	4.892 (0.32)	5.110 (0.33)	5.264 (0.32)	5.384 (0.35)
			3.411 (0.61)	3.800 (0.41)	4.089 (0.37)	4.402 (0.33)	4.609 (0.32)	4.756 (0.36)	4.821 (0.34)
		2.650 (0.64)	3.001 (0.39)	3.317 (0.42)	3.641 (0.39)	3.876 (0.38)	4.059 (0.39)	4.143 (0.33)	4.226 (0.35)
	2.086 (0.76)	2.348 (0.51)	2.677 (0.50)	3.966 (0.40)	3.202 (0.42)	3.410 (0.40)	3.561 (0.40)	3.662 (0.37)	3.742 (0.39)
1.957 (0.65)	2.055 (0.51)	2.361 (0.51)	2.691 (0.44)	3.012 (0.43)	3.213 (0.43)	3.430 (0.40)	3.584 (0.37)	3.714 (0.37)	3.782 (0.39)

Fig. 4.13b. Pin-power distribution for NITAWL benchmark TCA-9. Value in parentheses is percent standard deviation.

Table 4.85. Selected reaction rates for CENTRM case TCA-9

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.197E-05	1.995E-05	7.072E-06	4.613E-03	0.183
	Clad	2.247E-07	0.0	0.0	1.425E-03	0.056
	Mod.	6.729E-07	0.0	0.0	1.919E-02	0.761
55	Fuel	4.255E-05	6.730E-05	2.383E-05	2.168E-02	0.181
	Clad	8.192E-07	0.0	0.0	6.794E-03	0.057
	Mod.	2.155E-06	0.0	0.0	9.111E-02	0.762

Table 4.86. Selected reaction rates for NITAWL case TCA-9

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	1.173E-05	1.955E-05	6.931E-06	4.554E-03	0.182
	Clad	2.206E-07	0.0	0.0	1.420E-03	0.056
	Mod.	6.680E-07	0.0	0.0	1.910E-02	0.762
55	Fuel	4.279E-05	6.771E-05	2.398E-05	2.188E-02	0.182
	Clad	8.213E-07	0.0	0.0	6.844E-03	0.057
	Mod.	2.172E-06	0.0	0.0	9.168E-02	0.761

Table 4.87. TCA-9, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	3.851E-05	3.808E-05
2	1.088E-05	1.068E-05
3	2.665E-06	2.690E-06
4	2.684E-05	2.644E-05

Table 4.88. TCA-9, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$G_a$	$\langle G_f \rangle$	$G_f$	$G_a$	$\langle G_f \rangle$	$G_f$
1	1.42657E-04	3.25414E-04	1.25101E-04	1.41875E-04	3.24320E-04	1.24670E-04
2	3.42835E-03	5.22619E-03	2.14479E-03	3.51588E-03	5.33745E-03	2.19045E-03
3	5.02206E-03	1.01901E-02	4.18195E-03	5.22963E-03	1.07319E-02	4.40428E-03
4	4.91554E-02	1.02344E-01	4.20007E-02	4.86914E-02	1.01377E-01	4.16040E-02

Table 4.89. TCA-9, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$G_a$	$\langle G_f \rangle$	$G_f$	$G_a$	$\langle G_f \rangle$	$G_f$
1	4.50192E-03	8.46604E-03	2.99920E-03	4.50218E-03	8.53582E-03	3.03046E-03
2	4.14411E-02	3.76574E-06	1.56013E-06	3.83075E-02	3.58055E-06	1.48341E-06
3	6.94867E-03	2.40724E-08	9.97362E-09	7.02602E-03	2.48603E-08	1.03001E-08
4	2.78966E-02	1.31143E-07	5.43353E-08	2.76690E-02	1.30061E-07	5.38869E-08

Table 4.90 TCA-9, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$G_a$	$\langle G_f \rangle$	$G_f$	$G_a$	$\langle G_f \rangle$	$G_f$
1	5.11763E-04	1.49708E-03	4.81127E-04	5.10995E-04	1.49750E-03	4.81258E-04
2	1.10924E-02	1.84326E-02	6.40062E-03	1.10329E-02	1.80993E-02	6.28488E-03
3	3.20870E-02	6.32248E-02	2.19544E-02	3.47840E-02	6.83283E-02	2.37267E-02
4	2.66228E-01	5.40183E-01	1.86826E-01	2.64971E-01	5.37118E-01	1.85773E-01

Table 4.91. TCA-9, Pin-55 four-group fluxes

Group	CENTRM M ( cm <sup>-2</sup> - s <sup>-1</sup> )	NITAWL M ( cm <sup>-2</sup> - s <sup>-1</sup> )
1	2.010E-04	2.034E-04
2	6.739E-05	6.769E-05
3	1.576E-05	1.591E-05
4	8.667E-05	8.728E-05

Table 4.92. TCA-9, Pin-55 four-group U-235 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	1.45454E-04	3.27423E-04	1.26486E-04	1.45607E-04	3.27771E-04	1.26597E-04
2	3.41193E-03	5.23067E-03	2.14662E-03	3.48574E-03	5.30232E-03	2.17602E-03
3	5.17154E-03	1.05678E-02	4.33692E-03	5.13163E-03	1.04658E-02	4.29508E-03
4	4.74074E-02	9.86494E-02	4.04848E-02	4.74735E-02	9.87892E-02	4.05423E-02

Table 4.93. TCA-9, Pin-55 four-group U-238 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	4.40327E-03	7.89249E-03	2.80210E-03	4.40840E-03	7.90103E-03	2.80352E-03
2	3.82984E-02	3.87376E-06	1.60488E-06	3.80297E-02	3.68119E-06	1.52510E-06
3	6.99689E-03	2.45553E-08	1.01737E-08	6.98259E-03	2.44124E-08	1.01145E-08
4	2.69919E-02	1.26807E-07	5.25386E-08	2.70262E-02	1.26972E-07	5.26067E-08

Table 4.94. TCA-9, Pin-55 four-group Pu-239 cross sections

Group	CENTRM cross sections ( cm <sup>-1</sup> )			NITAWL cross sections ( cm <sup>-1</sup> )		
	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$	$\overline{G}_a$	$\langle G_f \rangle$	$\overline{G}_f$
1	5.12642E-04	1.48335E-03	4.78804E-04	5.12945E-04	1.48419E-03	4.78995E-04
2	1.10458E-02	1.82405E-02	6.33394E-03	1.08837E-02	1.78922E-02	6.21299E-03
3	3.38276E-02	6.65209E-02	2.30991E-02	3.35685E-02	6.60145E-02	2.29233E-02
4	2.75620E-01	5.52218E-01	1.91037E-01	2.75080E-01	5.51449E-01	1.90770E-01

										6.856 (0.85)
									6.768 (0.41)	6.823 (0.42)
								6.535 (0.43)	6.644 (0.30)	6.692 (0.44)
							6.073 (0.44)	6.278 (0.31)	6.452 (0.32)	6.462 (0.48)
						5.443 (0.46)	5.760 (0.35)	5.984 (0.30)	6.074 (0.35)	6.161 (0.44)
					4.729 (0.48)	5.080 (0.34)	5.339 (0.33)	5.561 (0.32)	5.648 (0.33)	5.659 (0.48)
				3.888 (0.57)	4.322 (0.37)	4.641 (0.36)	4.858 (0.32)	5.062 (0.33)	5.192 (0.34)	5.200 (0.49)
			3.115 (0.64)	3.500 (0.43)	3.840 (0.39)	4.093 (0.37)	4.339 (0.38)	4.483 (0.39)	4.605 (0.39)	4.604 (0.53)
		2.358 (0.72)	2.681 (0.47)	3.033 (0.43)	3.323 (0.38)	3.532 (0.43)	3.760 (0.40)	3.875 (0.42)	3.955 (0.37)	3.936 (0.55)
	1.684 (0.85)	1.983 (0.56)	2.291 (0.51)	2.553 (0.46)	2.823 (0.46)	3.029 (0.41)	3.208 (0.45)	3.286 (0.41)	3.384 (0.39)	3.418 (0.59)
1.428 (0.77)	1.569 (0.61)	1.859 (0.57)	2.158 (0.49)	2.398 (0.51)	2.643 (0.49)	2.831 (0.45)	2.995 (0.47)	3.099 (0.42)	3.141 (0.43)	3.185 (0.58)

Fig. 4.14a. Pin-power distribution for CENTRM benchmark TCA-10. Value in parentheses is percent standard deviation.

										6.908 (0.85)
									6.810 (0.41)	6.858 (0.43)
								6.535 (0.42)	6.640 (0.31)	6.685 (0.43)
							6.057 (0.47)	6.279 (0.33)	6.387 (0.31)	6.470 (0.43)
						5.486 (0.45)	5.776 (0.31)	6.008 (0.31)	6.085 (0.33)	6.152 (0.45)
					4.750 (0.51)	5.094 (0.33)	5.371 (0.31)	5.545 (0.30)	5.669 (0.34)	5.702 (0.44)
				3.961 (0.55)	4.306 (0.33)	4.671 (0.38)	4.906 (0.32)	5.079 (0.34)	5.159 (0.36)	5.240 (0.48)
			3.100 (0.59)	3.517 (0.38)	3.850 (0.40)	4.088 (0.40)	4.342 (0.36)	4.512 (0.35)	4.599 (0.34)	4.621 (0.50)
		2.323 (0.70)	2.712 (0.44)	3.010 (0.46)	3.318 (0.45)	3.576 (0.42)	3.745 (0.40)	3.898 (0.41)	3.962 (0.39)	4.025 (0.59)
	1.667 (0.84)	2.010 (0.56)	2.295 (0.51)	2.584 (0.45)	2.808 (0.48)	3.022 (0.46)	3.184 (0.45)	3.312 (0.43)	3.374 (0.41)	3.412 (0.57)
1.422 (0.85)	1.576 (0.65)	1.865 (0.58)	2.122 (0.51)	2.401 (0.50)	2.644 (0.46)	2.824 (0.47)	2.996 (0.45)	3.102 (0.39)	3.155 (0.44)	3.217 (0.56)

Fig. 4.14b. Pin-power distribution for NITAWL benchmark TCA-10. Value in parentheses is percent standard deviation.

Table 4.95. Selected reaction rates for CENTRM case TCA-10

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	8.487E-06	1.430E-05	5.068E-06	2.952E-03	0.146
	Clad	1.587E-07	0.0	0.0	9.168E-04	0.046
	Mod.	4.949E-07	0.0	0.0	1.630E-02	0.808
66	Fuel	4.238E-05	6.861E-05	2.429E-05	1.833E-02	0.147
	Clad	8.072E-07	0.0	0.0	5.748E-03	0.046
	Mod.	2.263E-06	0.0	0.0	1.007E-01	0.807

Table 4.96. Selected reaction rates for NITAWL case TCA-10

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	8.415E-06	1.413E-05	5.006E-06	2.931E-03	0.146
	Clad	1.562E-07	0.0	0.0	9.141E-04	0.046
	Mod.	4.895E-07	0.0	0.0	1.618E-02	0.808
66	Fuel	4.266E-05	6.930E-05	2.454E-05	1.832E-02	0.147
	Clad	8.014E-07	0.0	0.0	5.729E-03	0.045
	Mod.	2.297E-06	0.0	0.0	1.009E-01	0.808

Table 4.97. TCA-10, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.547E-05	2.512E-05
2	7.003E-06	7.231E-06
3	1.709E-06	1.737E-06
4	1.922E-05	1.894E-05

Table 4.98. TCA-10, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	1.40788E-04	3.23363E-04	1.24110E-04	1.41106E-04	3.24338E-04	1.24311E-04
2	3.64170E-03	5.55391E-03	2.27928E-03	3.51527E-03	5.32391E-03	2.18488E-03
3	5.30350E-03	1.08803E-02	4.46517E-03	5.18458E-03	1.06225E-02	4.35935E-03
4	4.91298E-02	1.02298E-01	4.19822E-02	4.92076E-02	1.02458E-01	4.20476E-02

Table 4.99. TCA-10, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	4.53168E-03	8.72356E-03	3.09660E-03	4.53467E-03	8.75482E-03	3.09219E-03
2	4.29217E-02	3.81724E-06	1.58147E-06	4.01630E-02	3.94182E-06	1.63309E-06
3	7.03335E-03	2.49018E-08	1.03173E-08	7.00443E-03	2.45869E-08	1.01868E-08
4	2.78924E-02	1.31130E-07	5.43293E-08	2.79251E-02	1.31284E-07	5.43933E-08

Table 4.100. TCA-10, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	5.10742E-04	1.50232E-03	4.82148E-04	5.10768E-04	1.50322E-03	4.81907E-04
2	1.13157E-02	1.86831E-02	6.48763E-03	1.14534E-02	1.87359E-02	6.50593E-03
3	3.56099E-02	6.98250E-02	2.42465E-02	3.42803E-02	6.73431E-02	2.33847E-02
4	2.63607E-01	5.35739E-01	1.85285E-01	2.64216E-01	5.36885E-01	1.85682E-01



Table 4.101. TCA-10, Pin-66 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	1.721E-04	1.716E-04
2	5.659E-05	5.611E-05
3	1.360E-05	1.336E-05
4	8.928E-05	9.041E-05

Table 4.102. TCA-10, Pin-66 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	1.44765E-04	3.27146E-04	1.26179E-04	1.44207E-04	3.26568E-04	1.25881E-04
2	3.42458E-03	5.21627E-03	2.14071E-03	3.45678E-03	5.26794E-03	2.16191E-03
3	5.10952E-03	1.04097E-02	4.27204E-03	5.28578E-03	1.08415E-02	4.44925E-03
4	4.80156E-02	9.99418E-02	4.10152E-02	4.77411E-02	9.93647E-02	4.07783E-02

Table 4.103. TCA-10, Pin-66 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	4.43964E-03	8.07600E-03	2.86439E-03	4.43787E-03	8.12821E-03	2.88138E-03
2	3.89892E-02	3.80924E-06	1.57815E-06	3.85192E-02	3.58239E-06	1.48417E-06
3	6.97667E-03	2.43379E-08	1.00837E-08	7.03071E-03	2.48865E-08	1.03109E-08
4	2.73091E-02	1.28331E-07	5.31703E-08	2.71792E-02	1.27709E-07	5.29124E-08

Table 4.104. TCA-10, Pin-66 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$	$\underline{G_a}$	$\underline{\langle G_f \rangle}$	$\underline{G_f}$
1	5.12740E-04	1.48833E-03	4.79719E-04	5.12294E-04	1.48952E-03	4.79891E-04
2	1.11449E-02	1.83349E-02	6.36671E-03	1.12214E-02	1.84762E-02	6.41579E-03
3	3.30546E-02	6.50683E-02	2.25947E-02	3.57615E-02	7.00931E-02	2.43396E-02
4	2.70972E-01	5.45716E-01	1.88771E-01	2.70533E-01	5.44404E-01	1.88319E-01

										6.654 (0.79)
									6.562 (0.44)	6.611 (0.46)
								6.263 (0.44)	6.409 (0.32)	6.449 (0.43)
							5.818 (0.46)	6.026 (0.31)	6.170 (0.31)	6.207 (0.44)
						5.216 (0.46)	5.552 (0.35)	5.746 (0.30)	5.878 (0.30)	5.943 (0.39)
					4.527 (0.58)	4.898 (0.35)	5.157 (0.31)	5.351 (0.31)	5.483 (0.32)	5.471 (0.45)
				3.745 (0.51)	4.139 (0.38)	4.467 (0.35)	4.724 (0.35)	4.888 (0.33)	5.001 (0.33)	4.991 (0.49)
			3.030 (0.65)	3.377 (0.41)	3.691 (0.40)	3.991 (0.38)	4.178 (0.39)	4.331 (0.34)	4.457 (0.36)	4.431 (0.50)
		2.212 (0.70)	2.576 (0.52)	2.912 (0.43)	3.174 (0.42)	3.439 (0.38)	3.611 (0.39)	3.748 (0.36)	3.825 (0.40)	3.884 (0.50)
	1.604 (0.82)	1.905 (0.50)	2.200 (0.49)	2.472 (0.45)	2.710 (0.48)	2.905 (0.41)	3.084 (0.47)	3.215 (0.41)	3.268 (0.43)	3.263 (0.55)
1.350 (0.84)	1.492 (0.56)	1.764 (0.57)	2.050 (0.50)	2.302 (0.49)	2.553 (0.45)	2.722 (0.44)	2.886 (0.45)	2.980 (0.46)	3.036 (0.44)	3.092 (0.56)

Fig. 4.15a. Pin-power distribution for CENTRM benchmark TCA-11. Value in parentheses is percent standard deviation.

										6.756 (0.82)
									6.609 (0.41)	6.637 (0.39)
								6.358 (0.42)	6.453 (0.31)	6.510 (0.44)
							5.866 (0.43)	6.087 (0.31)	6.184 (0.31)	6.208 (0.44)
						5.248 (0.45)	5.518 (0.31)	5.748 (0.29)	5.874 (0.31)	5.922 (0.43)
					4.565 (0.51)	4.901 (0.35)	5.149 (0.31)	5.364 (0.31)	5.480 (0.32)	5.535 (0.47)
				3.782 (0.57)	4.171 (0.39)	4.444 (0.38)	4.672 (0.37)	4.911 (0.33)	4.984 (0.30)	5.039 (0.47)
			2.969 (0.61)	3.380 (0.38)	3.683 (0.38)	3.961 (0.37)	4.175 (0.40)	4.337 (0.35)	4.431 (0.36)	4.489 (0.53)
		2.266 (0.73)	2.599 (0.49)	2.912 (0.47)	3.209 (0.40)	3.419 (0.44)	3.625 (0.39)	3.746 (0.38)	3.823 (0.39)	3.855 (0.60)
	1.628 (0.86)	1.918 (0.54)	2.205 (0.51)	2.470 (0.48)	2.727 (0.45)	2.946 (0.52)	3.062 (0.42)	3.184 (0.42)	3.282 (0.42)	3.293 (0.59)
1.376 (0.81)	1.498 (0.61)	1.770 (0.54)	2.049 (0.51)	2.320 (0.50)	2.536 (0.45)	2.723 (0.45)	2.861 (0.49)	2.983 (0.44)	3.037 (0.42)	3.032 (0.61)

Fig. 4.15b. Pin-power distribution for NITAWL benchmark TCA-11. Value in parentheses is percent standard deviation.

Table 4.105. Selected reaction rates for CENTRM case TCA-11

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	7.995E-06	1.342E-05	4.759E-06	2.922E-03	0.146
	Clad	1.494E-07	0.0	0.0	8.994E-04	0.046
	Mod.	4.727E-07	0.0	0.0	1.613E-02	0.808
66	Fuel	4.112E-05	6.652E-05	2.356E-05	1.831E-02	0.147
	Clad	7.801E-07	0.0	0.0	5.719E-03	0.045
	Mod.	2.193E-06	0.0	0.0	1.009E-01	0.808

Table 4.106. Selected reaction rates for NITAWL case TCA-11

Pin	Region	$G_a M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$\langle G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$G_f M$ ( $\text{cm}^{-3} - \text{s}^{-1}$ )	$M$ ( $\text{cm} - \text{s}^{-1}$ )	$M/M_t$
1	Fuel	8.237E-06	1.382E-05	4.898E-06	2.946E-03	0.146
	Clad	1.536E-07	0.0	0.0	9.201E-04	0.046
	Mod.	4.780E-07	0.0	0.0	1.632E-02	0.808
66	Fuel	4.210E-05	6.785E-05	2.403E-05	1.881E-02	0.149
	Clad	7.944E-07	0.0	0.0	5.881E-03	0.045
	Mod.	2.226E-06	0.0	0.0	1.019E-01	0.805

Table 4.107. TCA-11, Pin-1 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	2.428E-05	2.418E-05
2	6.754E-06	6.771E-06
3	1.616E-06	1.716E-06
4	1.818E-05	1.859E-05

Table 4.108. TCA-11, Pin-1 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	1.41872E-04	3.24906E-04	1.24701E-04	1.41020E-04	3.23700E-04	1.24222E-04
2	3.59017E-03	5.46494E-03	2.24276E-03	3.58779E-03	5.48985E-03	2.25299E-03
3	5.18994E-03	1.06233E-02	4.35970E-03	5.10914E-03	1.04368E-02	4.28316E-03
4	4.91039E-02	1.02248E-01	4.19618E-02	4.92082E-02	1.02458E-01	4.20477E-02

Table 4.109. TCA-11, Pin-1 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	4.53707E-03	8.65445E-03	3.06352E-03	4.50757E-03	8.64413E-03	3.06142E-03
2	3.77442E-02	3.89227E-06	1.61256E-06	4.14119E-02	3.44468E-06	1.42711E-06
3	6.97847E-03	2.44523E-08	1.01310E-08	6.97541E-03	2.44034E-08	1.01108E-08
4	2.78818E-02	1.31080E-07	5.43088E-08	2.79222E-02	1.31269E-07	5.43873E-08

Table 4.110. TCA-11, Pin-1 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$	$\underline{G}_a$	$\underline{\langle G}_f$	$\underline{G}_f$
1	5.11446E-04	1.50099E-03	4.81647E-04	5.10571E-04	1.50108E-03	4.81762E-04
2	1.15859E-02	1.88543E-02	6.54708E-03	1.15115E-02	1.90902E-02	6.62899E-03
3	3.43188E-02	6.73416E-02	2.33841E-02	3.42125E-02	6.71562E-02	2.33196E-02
4	2.62911E-01	5.34534E-01	1.84867E-01	2.65492E-01	5.39053E-01	1.86434E-01

Table 4.111. TCA-11, Pin-66 four-group fluxes

Group	CENTRM M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )	NITAWL M ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )
1	1.657E-04	1.701E-04
2	5.293E-05	5.558E-05
3	1.316E-05	1.301E-05
4	8.674E-05	8.849E-05

Table 4.112. TCA-11, Pin-66 four-group U-235 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	1.44711E-04	3.27220E-04	1.26172E-04	1.44755E-04	3.27436E-04	1.26225E-04
2	3.46220E-03	5.28876E-03	2.17045E-03	3.45516E-03	5.25847E-03	2.15802E-03
3	5.16589E-03	1.05595E-02	4.33352E-03	5.18064E-03	1.05839E-02	4.34357E-03
4	4.81825E-02	1.00288E-01	4.11571E-02	4.80322E-02	9.99713E-02	4.10273E-02

Table 4.113. TCA-11, Pin-66 four-group U-238 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	4.47467E-03	8.17996E-03	2.90346E-03	4.47739E-03	8.19447E-03	2.90690E-03
2	3.91615E-02	3.93752E-06	1.63130E-06	4.02064E-02	3.76053E-06	1.55797E-06
3	6.99303E-03	2.44910E-08	1.01470E-08	6.99198E-03	2.45410E-08	1.01678E-08
4	2.73917E-02	1.28724E-07	5.33326E-08	2.73197E-02	1.28377E-07	5.31893E-08

Table 4.114. TCA-11, Pin-66 four-group Pu-239 cross sections

Group	CENTRM cross sections ( $\text{cm}^{-1}$ )			NITAWL cross sections ( $\text{cm}^{-1}$ )		
	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$	$\underline{G}_a$	$\langle G_f \rangle$	$\underline{G}_f$
1	5.12696E-04	1.48906E-03	4.79759E-04	5.13031E-04	1.49057E-03	4.80148E-04
2	1.14152E-02	1.88409E-02	6.54241E-03	1.11940E-02	1.81913E-02	6.31686E-03
3	3.48957E-02	6.84264E-02	2.37608E-02	3.45817E-02	6.78782E-02	2.35705E-02
4	2.71706E-01	5.47283E-01	1.89309E-01	2.72174E-01	5.47792E-01	1.89488E-01

## 5. CALCULATIONAL BENCHMARKS

### 5.1 DESCRIPTION

The calculational benchmarks examined in this report are divided into two distinct geometric sets of cases. The first set of cases consists of an infinitely long pin in an infinite triangular-pitched lattice. The second set of cases consists of a buckled pin in an infinite triangular-pitched lattice. The radii of the fuel, clad, and moderator are all the same for all variants and states. Also, the buckling height is the same in all buckled problems. All variants and states are calculated in both geometric configurations. The state parameters are given in Table 5.1.<sup>4</sup>

The calculational benchmarks in each geometric set are divided into variants, with five states in each of the variants. The variants differ only by the isotopic composition of the fuel. Within each variant, the fuel composition is the same for each state, with the exception of the presence or absence of <sup>135</sup>Xe and <sup>149</sup>Sm. The differences in the states are due to the presence or absence of <sup>135</sup>Xe and <sup>149</sup>Sm in the fuel, the fuel temperature, and the type of moderator.

There are four basic types of fuel: fresh uranium fuel, fresh MOX fuel, spent uranium fuel and fresh MOX fuel containing Pu recycled from a reactor. The spent uranium fuel is used in two variants: variant V3 uses spent uranium fuel with only the actinides, whereas variant V4 uses spent uranium fuel with actinides and fission products. There are also four variations of the fresh MOX fuel: fresh MOX fuel, MOX fuel with only <sup>239</sup>Pu, MOX fuel with only <sup>240</sup>Pu, and MOX fuel with only <sup>241</sup>Pu. The basic fuel material isotopic composition for each variant is given in Table 5.2.

There are four nonfuel material compositions in the set of calculational benchmarks: 1 clad composition, which is common to all problems, and 3 moderator material compositions. The variations in the moderator compositions are due to the presence or absence of <sup>10</sup>B and <sup>11</sup>B, the clad and moderator temperature, and the moderator density. The material isotopic compositions for the clad and each moderator are given in Table 5.3.

Table 5.1. State parameters for the calculational benchmark variants

State	Fuel zone temp (K)	Nonfuel zone temp (K)	<sup>135</sup> Xe, <sup>149</sup> Sm in fuel	<sup>10</sup> B, <sup>11</sup> B in moderator	Moderator material
S1	1027	579	Yes	Yes	MOD1
S3	1027	579	Yes	No	MOD2
S4	1027	579	No	Yes	MOD1
S5	579	579	No	Yes	MOD1
S6	300	300	No	Yes	MOD3

Table 5.2. Basic fuel isotopic composition for each computational benchmark variant

Variant	Comment	Isotope	Atom density ( $10^{-24} \text{ cm}^{-3}$ )	Isotope e	Atom density ( $10^{-24} \text{ cm}^{-3}$ )
V1	Fresh uranium fuel	$^{235}\text{U}$	$8.7370 \times 10^{-4}$	$^{16}\text{O}$	$3.9235 \times 10^{-2}$
		$^{238}\text{U}$	$1.8744 \times 10^{-2}$		
V2	Fresh MOX fuel	$^{235}\text{U}$	$3.8393 \times 10^{-5}$	$^{239}\text{Pu}$	$6.5875 \times 10^{-4}$
		$^{238}\text{U}$	$1.8917 \times 10^{-2}$	$^{240}\text{Pu}$	$4.2323 \times 10^{-5}$
		$^{16}\text{O}$	$4.1707 \times 10^{-2}$	$^{41}\text{Pu}$	$7.0246 \times 10^{-4}$
V3	Spent uranium fuel with no fission products ( actinides only )	$^{235}\text{U}$	$3.7843 \times 10^{-4}$	$^{242}\text{Pu}$	$4.7576 \times 10^{-6}$
		$^{236}\text{U}$	$8.6365 \times 10^{-5}$	$^{241}\text{Am}$	$4.9491 \times 10^{-7}$
		$^{238}\text{U}$	$1.8327 \times 10^{-2}$	$^{242\text{m}}\text{Am}$	$7.9194 \times 10^{-9}$
		$^{237}\text{Np}$	$2.4823 \times 10^{-5}$	$^{243}\text{Am}$	$6.6925 \times 10^{-7}$
		$^{238}\text{Pu}$	$6.7254 \times 10^{-6}$	$^{242}\text{Cm}$	$1.2582 \times 10^{-7}$
		$^{239}\text{Np}$	$1.8332 \times 10^{-6}$	$^{243}\text{Cm}$	$2.0629 \times 10^{-9}$
		$^{239}\text{Pu}$	$1.3111 \times 10^{-4}$	$^{244}\text{Cm}$	$1.2387 \times 10^{-7}$
		$^{240}\text{Pu}$	$3.6233 \times 10^{-5}$	$^{16}\text{O}$	$3.9235 \times 10^{-2}$
		$^{241}\text{Pu}$	$2.1701 \times 10^{-5}$		
V4	Spent uranium fuel ( actinides + fission products ) ( V3 + listed isotopes )	$^{103}\text{Rh}$	$1.8890 \times 10^{-4}$	$^{145}\text{Nd}$	$1.9975 \times 10^{-6}$
		$^{131}\text{Xe}$	$1.4255 \times 10^{-5}$	$^{153}\text{Eu}$	$2.4801 \times 10^{-7}$
		$^{143}\text{Nd}$	$2.6692 \times 10^{-2}$	$^{109}\text{Ag}$	$2.2037 \times 10^{-9}$
		$^{147}\text{Pm}$	$6.1574 \times 10^{-5}$	$^{155}\text{Eu}$	$9.6857 \times 10^{-7}$
		$^{133}\text{Cs}$	$3.5974 \times 10^{-6}$	$^{95}\text{Mo}$	$3.3720 \times 10^{-7}$
		$^{99}\text{Tc}$	$3.3320 \times 10^{-6}$	$^{154}\text{Eu}$	$5.1189 \times 10^{-9}$
		$^{152}\text{Sm}$	$2.6842 \times 10^{-4}$	$^{101}\text{Ru}$	$3.1134 \times 10^{-7}$
		$^{151}\text{Sm}$	$3.0757 \times 10^{-5}$		
V7	Fresh MOX fuel with $^{239}\text{Pu}$ as only Pu	$^{235}\text{U}$	$3.8393 \times 10^{-5}$	$^{239}\text{Pu}$	$6.5875 \times 10^{-4}$
		$^{238}\text{U}$	$1.8917 \times 10^{-2}$	$^{16}\text{O}$	$4.1707 \times 10^{-2}$
V8	Fresh MOX fuel with $^{240}\text{Pu}$ as only Pu	$^{235}\text{U}$	$6.9714 \times 10^{-4}$	$^{240}\text{Pu}$	$4.2323 \times 10^{-5}$
		$^{238}\text{U}$	$1.8917 \times 10^{-2}$	$^{16}\text{O}$	$4.1707 \times 10^{-2}$
V9	Fresh MOX fuel with $^{241}\text{Pu}$ as only Pu	$^{235}\text{U}$	$3.8393 \times 10^{-5}$	$^{41}\text{Pu}$	$6.6577 \times 10^{-4}$
		$^{238}\text{U}$	$1.8917 \times 10^{-2}$	$^{16}\text{O}$	$4.1707 \times 10^{-2}$
V10	Fresh MOX fuel with recycled reactor Pu	$^{235}\text{U}$	$5.0000 \times 10^{-5}$	$^{240}\text{Pu}$	$4.9000 \times 10^{-4}$
		$^{238}\text{U}$	$2.2100 \times 10^{-2}$	$^{241}\text{Pu}$	$1.9000 \times 10^{-4}$
		$^{16}\text{O}$	$4.6300 \times 10^{-2}$	$^{242}\text{Pu}$	$1.0500 \times 10^{-4}$
		$^{238}\text{Pu}$	$3.0000 \times 10^{-5}$	$^{241}\text{Am}$	$2.5000 \times 10^{-5}$
		$^{239}\text{Pu}$	$1.1600 \times 10^{-3}$		



Table 5.3. Nonfuel material isotopic composition

Material	Comment	Isotope	Atom density ( $10^{-24} \text{ cm}^{-3}$ )	Isotope	Atom density ( $10^{-24} \text{ cm}^{-3}$ )
Clad	Cladding	Zr	$4.2300 \times 10^{-2}$		
MOD1	Hot moderator with boric acid	H	$4.7830 \times 10^{-2}$	$^{10}\text{B}$	$4.7344 \times 10^{-6}$
		$^{16}\text{O}$	$2.3910 \times 10^{-2}$	$^{11}\text{B}$	$1.9177 \times 10^{-5}$
MOD2	Hot moderator without boric acid	H	$4.7830 \times 10^{-2}$		
		$^{16}\text{O}$	$2.3910 \times 10^{-2}$		
MOD3	Cold moderator with boric acid	H	$6.6940 \times 10^{-2}$	$^{10}\text{B}$	$6.6262 \times 10^{-6}$
		$^{16}\text{O}$	$3.3470 \times 10^{-2}$	$^{11}\text{B}$	$2.6839 \times 10^{-5}$

## 5.2 ANALYSIS

All computational benchmarks were processed using SCALE 5.0. The cases labeled NITAWL utilize the following sequence: CSAS, BONAMI, NITAWL, XSDRNPM. The cases labeled CENTRM utilize the following sequence: CSAS, BONAMI, NITAWL, CENTRM, PMC, WORKER, XSDRNPM. In the NITAWL cases the resolved resonance region is self-shielded using NITAWL. In the CENTRM cases the resolved resonance region is self-shielded using CENTRM and PMC, which removes the limitations of the Nordheim Integral Treatment. Table 5.4 contains the results for the infinite arrays, and Table 5.5 contains the results for the buckled arrays.

For each variant and state, the differences between the NITAWL and CENTRM multiplication factors ( $k_4$  and buckled  $k_4$ ) and the energy of the average lethargy causing fission (EALCF) are almost identical for the infinite and buckled geometries as shown in Tables 5.4 and 5.5. The differences in the multiplication between the CENTRM and NITAWL cases range from -0.09% to -0.55%. Trends are apparent based on both fuel material and temperature. The smallest difference occurs for variant V4, state S6, which is spent uranium fuel with actinides and fission products at room temperature. The largest difference occurs for variant V9, state S1, which is fresh MOX fuel with all the Pu as  $^{241}\text{Pu}$  at reactor temperatures.

The selection and number of nuclides in the fuel has little effect on the difference between NITAWL and CENTRM, at most ~0.25%, which occurs when the amount of  $^{241}\text{Pu}$  is at its maximum. The effects of resonance overlap do not seem to be significant. The lowest difference at any given temperature occurs for spent uranium fuel with actinides and fission products. The amount of absorbers in the fuel ( $^{135}\text{Xe}$  and  $^{149}\text{Sm}$ ) and in the moderator ( $^{10}\text{B}$ ) also does not affect the differences.

Fuel and moderator temperature have the most obvious, albeit still small, effect on the difference between NITAWL and CENTRM results. For a given variant, the largest difference always occurs with the fuel at 1027 K and the moderator at 579 K. Decreasing the fuel temperature to 579 K always decreases the difference, as much as 0.1%. Further decreasing the fuel and moderator temperature to 300 K always further decreases the difference, as much as another 0.1%. Both NITAWL and

CENTRM interpolate data between temperatures.

The EALCF is also calculated for each variant and state. The differences in the average-energy between the NITAWL and CENTRM cases range from a low of -0.41% to a high of 1.66%. Trends are apparent based only on temperature. The smallest differences with each variant occur in state S6, and the largest differences occurs for states 1, 2, and 3. As the pin temperature drops, the differences between the CSAS and CENTRM results lessen.

### 5.3 CONCLUSIONS

For this set of cases using either NITAWL or CENTRM as the resonance region processor produces consistent results. The  $k_{eff}$  values are slightly lower, ~0.3%, for all CENTRM cases. The nuclides selected do not appear to have an effect on the difference, but the temperature of the system does have a slight effect: the point library has temperature data well above that available in the multigroup library. The approximations used to process the resolved resonance data in NITAWL do not significantly affect the results, as shown by the good agreement with the CENTRM results.

Table 5.4a.  $k_4$  and EALCF values and differences for the variant cases

VARIANTS V1 - V4	NITAWL $k_4$	CENTRM $k_4$	$k_4$ % DIFF	NITAWL EALCF (eV)	CENTRM EALCF (eV)	EALCF % DIFF
V1S1	1.2593	1.2541	-0.41	0.7766	0.7806	0.52
V1S3	1.3144	1.3090	-0.41	0.6984	0.7019	0.5
V1S4	1.3069	1.3015	-0.41	0.7052	0.7087	0.5
V1S5	1.3249	1.3205	-0.33	0.6846	0.6877	0.45
V1S6	1.3669	1.3634	-0.26	0.2808	0.2819	0.39
V2S1	1.2074	1.2017	-0.47	1.5678	1.5873	1.24
V2S3	1.2360	1.2300	-0.49	1.4690	1.4871	1.23
V2S4	1.2270	1.2212	-0.47	1.4907	1.5090	1.23
V2S5	1.2474	1.2428	-0.37	1.4305	1.4460	1.08
V2S6	1.3256	1.3210	-0.35	0.5514	0.5568	0.98
V3S1	1.0821	1.0767	-0.5	0.9976	1.0064	0.88
V3S3	1.1267	1.1210	-0.51	0.8982	0.9058	0.85
V3S4	1.1218	1.1162	-0.5	0.9027	0.9103	0.84
V3S5	1.1412	1.1357	-0.48	0.8694	0.877	0.87
V3S6	1.1902	1.1862	-0.34	0.3271	0.3289	0.55
V4S1	1.0158	1.0140	-0.18	1.1496	1.1532	0.31
V4S3	1.0558	1.0536	-0.21	1.0346	1.0385	0.38
V4S4	1.0510	1.0490	-0.19	1.0411	1.0442	0.3
V4S5	1.0688	1.0669	-0.18	1.0081	1.0055	-0.26
V4S6	1.1197	1.1187	-0.09	0.3678	0.368	0.05

Table 5.4b.  $k_4$  and EALCF values and differences for the variant cases (cont.)

VARIANTS V7 - V10	CSAS $k_4$	CENTRM $k_4$	$k_4$ % DIFF	CSAS EALCF (eV)	CENTRM EALCF (eV)	EALCF % DIFF
V7S1	1.3047	1.2984	-0.48	1.2704	1.2851	1.16
V7S3	1.3372	1.3307	-0.49	1.1922	1.2058	1.14
V7S4	1.3270	1.3206	-0.48	1.2090	1.2228	1.14
V7S5	1.3459	1.3404	-0.41	1.1687	1.1816	1.1
V7S6	1.4112	1.4067	-0.32	0.4793	0.4835	0.88
V8S1	1.0904	1.0859	-0.41	0.8038	0.8083	0.56
V8S3	1.1442	1.1395	-0.41	0.7108	0.7146	0.53
V8S4	1.1399	1.1351	-0.42	0.7147	0.7186	0.55
V8S5	1.1596	1.1557	-0.34	0.6881	0.6912	0.45
V8S6	1.2115	1.2084	-0.26	0.2694	0.2704	0.37
V9S1	1.5290	1.5207	-0.54	1.4193	1.4140	-0.37
V9S3	1.5644	1.5561	-0.53	1.3346	1.3293	-0.4
V9S4	1.5515	1.5432	-0.53	1.3585	1.3529	-0.41
V9S5	1.5736	1.5668	-0.43	1.3191	1.3181	-0.08
V9S6	1.6195	1.6140	-0.34	0.5601	0.5602	0.02
V10S1	1.0952	1.0902	-0.46	9.5809	9.7345	1.6
V10S3	1.1078	1.1027	-0.46	9.118	9.2636	1.6
V10S4	1.1010	1.0958	-0.47	9.3374	9.4863	1.59
V10S5	1.1196	1.1160	-0.32	8.7717	8.8831	1.27
V10S6	1.1937	1.1917	-0.17	2.614	2.6373	0.89

Table 5.5a. Buckled  $k_4$  and EALCF values and differences for the variant cases

VARIANTS V1 - V4	CSAS buckled $k_4$	CENTRM buckled $k_4$	$k_4$ % DIFF	CSAS EALCF (eV)	CENTRM EALCF (eV)	EALCF % DIFF
V1S1	1.0802	1.0757	-0.42	0.8408	0.8455	0.56
V1S3	1.1266	1.1218	-0.43	0.755	0.7592	0.56
V1S4	1.1201	1.1154	-0.42	0.7628	0.7670	0.55
V1S5	1.1353	1.1314	-0.34	0.7402	0.7438	0.49
V1S6	1.2286	1.2253	-0.27	0.2932	0.2944	0.41
V2S1	1.0396	1.0346	-0.48	1.6927	1.7146	1.29
V2S3	1.0638	1.0586	-0.49	1.5847	1.605	1.28
V2S4	1.0562	1.0511	-0.48	1.6086	1.6293	1.29
V2S5	1.1050	1.1007	-0.39	1.5477	1.5659	1.18
V2S6	1.2167	1.2125	-0.35	0.5755	0.5814	1.03
V3S1	0.9547	0.9499	-0.5	1.0872	1.0973	0.93
V3S3	0.9932	0.9882	-0.5	0.9775	0.9863	0.9
V3S4	0.9889	0.9839	-0.51	0.9827	0.9917	0.92
V3S5	1.0059	1.0011	-0.48	0.9457	0.9542	0.9
V3S6	1.0887	1.0850	-0.34	0.3425	0.3445	0.58
V4S1	0.8975	0.8958	-0.19	1.2555	1.2600	0.36
V4S3	0.9322	0.9301	-0.23	1.1285	1.1334	0.43
V4S4	0.9279	0.9261	-0.19	1.1361	1.1400	0.34
V4S5	0.9435	0.9418	-0.18	1.0923	1.0963	0.37
V4S6	1.0253	1.0242	-0.11	0.3847	0.3858	0.29

Table 5.5b. Buckled  $k_4$  and EALCF values and differences for the variant cases (cont.)

VARIANTS V7 - V10	CSAS buckled $k_4$	CENTRM buckled $k_4$	$k_4$ % DIFF	CSAS EALCF (eV)	CENTRM EALCF (eV)	EALCF % DIFF
V7S1	1.1560	1.1504	-0.48	1.3698	1.3865	1.22
V7S3	1.1844	1.1786	-0.49	1.2846	1.300	1.2
V7S4	1.1755	1.1697	-0.49	1.3031	1.3187	1.2
V7S5	1.1920	1.1870	-0.42	1.2589	1.2734	1.15
V7S6	1.2955	1.2913	-0.32	0.4991	0.5037	0.92
V8S1	0.9628	0.9588	-0.42	0.8777	0.8831	0.62
V8S3	1.0093	1.0050	-0.43	0.7748	0.7794	0.59
V8S4	1.0055	1.0012	-0.43	0.7794	0.7841	0.6
V8S5	1.0227	1.0192	-0.34	0.7496	0.7534	0.51
V8S6	1.1095	1.1066	-0.26	0.2819	0.2829	0.35
V9S1	1.3591	1.3515	-0.56	1.5135	1.5087	-0.32
V9S3	1.3901	1.3825	-0.55	1.4225	1.4177	-0.34
V9S4	1.3788	1.3712	-0.55	1.4481	1.4431	-0.35
V9S5	1.3982	1.3920	-0.44	1.4055	1.4052	-0.02
V9S6	1.4906	1.4855	-0.34	0.5802	0.5803	0.02
V10S1	0.9876	0.9831	-0.46	10.483	10.657	1.66
V10S3	0.9988	0.9941	-0.47	9.9769	10.142	1.65
V10S4	0.9927	0.9881	-0.46	10.216	10.385	1.65
V10S5	1.0094	1.0061	-0.33	9.5901	9.7165	1.32
V10S6	1.1087	1.1069	-0.16	2.7455	2.7705	0.91

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**APPENDIX A**  
**SCALE INPUT OF MIX-COMP-THERM-2 PROBLEM SET**



## APPENDIX A SCALE INPUT OF MIX-COMP-THERM-2 PROBLEM SET

This appendix contains the CENTRM inputs for the six MIX-COMP-THERM-02 cases, PNL30 , PNL31, PNL32, PNL33, PNL34, and PNL35. The inputs can be changed to standard CSAS cases by replacing the =CSASC5 record with =CSAS25. The input for the cases are listed below.

```

=csasc5      parm=(size=2000000)
              pnl-30 fuel
              238group latticecell
              'PNL30 - MOX fuel
u-235  1 0 1.4886-4 295 end
u-238  1 0 2.0611-2 295 end
o      1 0 4.3779-2 295 end
u-234  1 0 1.2458-6 295 end
u-236  1 0 2.0936-9 295 end
pu-238 1 0 3.8836-8 295 end
pu-239 1 0 3.9262-4 295 end
pu-240 1 0 3.3206-5 295 end
pu-241 1 0 1.6081-6 295 end
pu-242 1 0 1.1882-7 295 end
am-241 1 0 1.4891-6 295 end
              'clad (ZR-2)
zr      2 0 4.2621-2 295 end
sn      2 0 4.8328-4 295 end
ni      2 0 3.0336-5 295 end
cr      2 0 7.6093-5 295 end
fe      2 0 9.5642-5 295 end
              'water(Reflector)
h       3 0 6.6706-2 295 end
o       3 0 3.3353-2 295 end
b-10   3 0 1.8706-8 295 end
b-11   3 0 7.5770-8 295 end
              'Lattice Grid
si      4 0 3.4607-4 295 end
fe      4 0 1.0152-4 295 end
cu      4 0 6.3731-5 295 end
mn      4 0 2.2115-5 295 end
mg      4 0 6.6651-4 295 end
cr      4 0 6.2310-5 295 end
ti      4 0 2.5375-5 295 end
al      4 0 5.8433-2 295 end
              'UO2
u-234   5 0 1.2406-6 295 end
u-235   5 0 1.4824-4 295 end
u-236   5 0 2.0848-9 295 end
u-238   5 0 2.0525-2 295 end
o       5 0 4.1943-2 295 end
              'Aluminum
si      6 0 3.4607-4 295 end
fe      6 0 1.0152-4 295 end
cu      6 0 6.3731-5 295 end
mn      6 0 2.2115-5 295 end
mg      6 0 6.6651-4 295 end
              cr  6 0 6.2310-5 295 end
              ti  6 0 2.5375-5 295 end
              al  6 0 5.8433-2 295 end
              'lead
pb      7 0 3.2174-2 295 end
              end comp
squarepitch 1.778 1.2827 1 2 1.4351 3 end
              more data
limcen=20000000
              end more
              PNL-30
              read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
              res=225
              plt=no lng=2000000
              end param
              read geometry
              '
              unit 1
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              '
              unit 2
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              '
              unit 3
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              '
              unit 4
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              '
              unit 5
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0

```







```

,
    unit 63
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
    unit 64
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
    unit 65
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
    unit 66
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
    unit 67
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
    unit 68
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
    unit 69
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
    unit 81
com='Fuel - Lower Clad + Moderator'
cylinder 2 1 0.7176 0.3175 0.0
cuboid 3 1 4p0.889 0.3175 0.0
,
    unit 82
com='Fuel - Lower PuO2/UO2 + UO2 + Clad + Moderator
+ Lattice Grid'
cylinder 1 1 0.6414 2.54 0.881
cylinder 5 1 0.6414 2.54 0.381
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p0.73025 2.54 0.0
cuboid 4 1 4p0.889 2.54 0.0
,
    unit 83
com='Fuel - Upper PuO2/UO2 + Clad + Moderator +
Lattice Grid'
cylinder 1 1 0.6414 2.54 0.0
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p0.73025 2.54 0.0
cuboid 4 1 4p0.889 2.54 0.0
,
    unit 84
com='Fuel - Upper PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 0.0635 0.0
cylinder 2 1 0.7176 0.0635 0.0
cuboid 3 1 4p0.889 0.0635 0.0
,
    unit 85
com='Reflector - Lower Moderator'
cuboid 3 1 4p0.889 0.3175 0.0
,
    unit 86
com='Reflector - Lower Moderator + Lattice Grid'
cuboid 3 1 4p0.73025 2.54 0.0
cuboid 4 1 4p0.889 2.54 0.0
,
    unit 87
com='Reflector - Upper Moderator + Lattice Grid'
cuboid 3 1 4p0.73025 2.54 0.0
cuboid 4 1 4p0.889 2.54 0.0
,
    unit 88
com='Reflector - Upper Moderator'
cuboid 3 1 4p0.889 0.0635 0.0
,
    unit 90
com='Reflector'
cuboid 3 1 4p0.889 86.6775 0.0
,
    global unit 100
com='Cells in assembly'
array 1 -20.447 -20.447 0
cuboid 6 1 4p20.447 92.9640 -2.8575
cuboid 7 1 4p20.447 93.9165 -2.8575
replicate 3 2 6*3.0 4
replicate 3 6 4*3.0 1.462 3.0 1
replicate 3 7 4*3.0 0.0 3.0 5
end geometry
read array
ara=1 nux=23 nuy=23 nuz=5
fill
'Lower Cladding and Moderator
85 85 85 85 85 81 81 81 81 81 81 81 1b11
85 85 85 85 81 81 81 81 81 81 81 81 1b11
85 85 85 81 81 81 81 81 81 81 81 81 1b11
85 85 81 81 81 81 81 81 81 81 81 81 1b11
85 81 81 81 81 81 81 81 81 81 81 81 1b11
81 81 81 81 81 81 81 81 81 81 81 81 1b11
81 81 81 81 81 81 81 81 81 81 81 81 1b11
81 81 81 81 81 81 81 81 81 81 81 81 1b11

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81 81 81 81 81 81 81 81 81 81 81 81 1b11
81 81 81 81 81 81 81 81 81 81 81 81 1b11
81 81 81 81 81 81 81 81 81 81 81 81 1b11
81 81 81 81 81 81 81 81 81 81 81 81 1b264
    'Lower Lattice Grid
86 86 86 86 86 82 82 82 82 82 82 82 1b11
86 86 86 86 82 82 82 82 82 82 82 82 1b11
86 86 86 82 82 82 82 82 82 82 82 82 1b11
86 86 82 82 82 82 82 82 82 82 82 82 1b11
86 82 82 82 82 82 82 82 82 82 82 82 1b11
82 82 82 82 82 82 82 82 82 82 82 82 1b11
82 82 82 82 82 82 82 82 82 82 82 82 1b11
82 82 82 82 82 82 82 82 82 82 82 82 1b11
82 82 82 82 82 82 82 82 82 82 82 82 1b11
82 82 82 82 82 82 82 82 82 82 82 82 1b11
82 82 82 82 82 82 82 82 82 82 82 82 1b11
82 82 82 82 82 82 82 82 82 82 82 82 1b264
    'Fuel and Reflector
    90 90 90 90 90 1 2 3 4 5 6 7 1b11
    90 90 90 90 8 9 10 11 12 13 14 15 1b11
    90 90 90 16 17 18 19 20 21 22 23 24 1b11
    90 90 16 25 26 27 28 29 30 31 32 33 1b11
    90 8 17 26 34 35 36 37 38 39 40 41 1b11
    1 9 18 27 35 42 43 44 45 46 47 48 1b11
    2 10 19 28 36 43 49 50 51 52 53 54 1b11
    3 11 20 29 37 44 50 55 56 57 58 59 1b11
    4 12 21 30 38 45 51 56 60 61 62 63 1b11
    5 13 22 31 39 46 52 57 61 64 65 66 1b11
    6 14 23 32 40 47 53 58 62 65 67 68 1b11
    7 15 24 33 41 48 54 59 63 66 68 69 1b264
    'Upper Lattice Grid
87 87 87 87 87 83 83 83 83 83 83 83 1b11
87 87 87 87 83 83 83 83 83 83 83 83 1b11
87 87 87 83 83 83 83 83 83 83 83 83 1b11
87 87 83 83 83 83 83 83 83 83 83 83 1b11
87 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b11
83 83 83 83 83 83 83 83 83 83 83 83 1b264
    'Upper Cladding and Moderator
88 88 88 88 88 84 84 84 84 84 84 84 1b11
88 88 88 88 84 84 84 84 84 84 84 84 1b11
88 88 88 84 84 84 84 84 84 84 84 84 1b11
88 88 84 84 84 84 84 84 84 84 84 84 1b11
88 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b11
84 84 84 84 84 84 84 84 84 84 84 84 1b264
end fill

```

```

end array
read bias id=500 2 11 end bias
read plot
    ttl='x-z plot at y=0.0'
    xul=-50.0 yul=0. zul=110
    xlr=50.0 ylr=0. zlr=-10.
    uax=1.0 wdn=-1.0
    nax=600 end plt0
    ttl='x-y plot at z=25.0'
    pic=mix
    xul=-30.0 yul=30. zul=25.
    xlr=30.0 ylr=-30. zlr=25.
    uax=1.0 vdn=-1.0
    nax=600 end plt1
end plot
end data
end
=shell
cp ft04f001 $RTNDR/pnl30.xs04
cp ft64f001 $RTNDR/pnl30.rs64
end
=kmart
read initial kunit=64
    xunit=4
    actbygrp
    rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92236 27 92236 18 92236 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
40000 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
28000 27
24000 27
26000 27
5010 27
5011 27
8016 27
1001 27
end activity

```



```

read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=(size=2000000)
              pnl-31 fuel
              238group latticecell
              'MOX fuel
u-235  1 0 1.4886-4 295 end
u-238  1 0 2.0611-2 295 end
o      1 0 4.3779-2 295 end
u-234  1 0 1.2458-6 295 end
u-236  1 0 2.0936-9 295 end
pu-238 1 0 3.8836-8 295 end
pu-239 1 0 3.9262-4 295 end
pu-240 1 0 3.3206-5 295 end
pu-241 1 0 1.6081-6 295 end
pu-242 1 0 1.1882-7 295 end
am-241 1 0 1.4891-6 295 end
              'clad (ZR-2)
zr     2 0 4.2621-2 295 end
sn     2 0 4.8328-4 295 end
ni     2 0 3.0336-5 295 end
cr     2 0 7.6093-5 295 end
fe     2 0 9.5642-5 295 end
              'water(Reflector)
h      3 0 6.6685-2 295 end
o      3 0 3.3400-2 295 end
b-10   3 0 7.5838-6 295 end
b-11   3 0 3.0718-5 295 end
              'Lattice Grid
si     4 0 3.4607-4 295 end
fe     4 0 1.0152-4 295 end
cu     4 0 6.3731-5 295 end
mn     4 0 2.2115-5 295 end
mg     4 0 6.6651-4 295 end
cr     4 0 6.2310-5 295 end
ti     4 0 2.5375-5 295 end
al     4 0 5.8433-2 295 end
              'UO2
u-234  5 0 1.2406-6 295 end
u-235  5 0 1.4824-4 295 end
u-236  5 0 2.0848-9 295 end
u-238  5 0 2.0525-2 295 end
o      5 0 4.1943-2 295 end
              'Aluminum
si     6 0 3.4607-4 295 end
fe     6 0 1.0152-4 295 end
cu     6 0 6.3731-5 295 end
mn     6 0 2.2115-5 295 end
mg     6 0 6.6651-4 295 end

cr     6 0 6.2310-5 295 end
ti     6 0 2.5375-5 295 end
al     6 0 5.8433-2 295 end
              'lead
pb     7 0 3.2174-2 295 end
              end comp
squarepitch 1.778 1.2827 1 2 1.4351 3 end
              more data
              limcen=20000000
              end more
              PNL-31
              read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
              res=225
              plt=no lng=2000000
              end param
              read geometry
              ,
              unit 1
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              ,
              unit 2
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              ,
              unit 3
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              ,
              unit 4
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              ,
              unit 5
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              ,
              unit 6
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
              ,
              unit 7
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0

```









cylinder 2 1 0.7176 86.6775 0.0	
cuboid 3 1 4p0.889 86.6775 0.0	
	unit 93
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 94
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 95
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 96
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 97
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 98
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 99
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 100
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 101
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0
	cylinder 2 1 0.7176 86.6775 0.0
	cuboid 3 1 4p0.889 86.6775 0.0
	unit 102
	com='PuO2/UO2 + Clad + Moderator'
	cylinder 1 1 0.6414 86.6775 0.0

```

cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 103
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 104
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 105
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 106
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 107
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 108
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 109
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p0.889 86.6775 0.0
,
unit 111
com='Fuel - Lower Clad + Moderator'
cylinder 2 1 0.7176 0.3175 0.0
cuboid 3 1 4p0.889 0.3175 0.0
,
unit 112
com='Fuel - Lower PuO2/UO2 + UO2 + Clad + Moderator
+ Lattice Grid'
cylinder 1 1 0.6414 2.54 0.881
cylinder 5 1 0.6414 2.54 0.381
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p0.73025 2.54 0.0
,
cuboid 4 1 4p0.889 2.54 0.0
,
unit 113
com='Fuel - Upper PuO2/UO2 + Clad + Moderator +
Lattice Grid'
cylinder 1 1 0.6414 2.54 0.0
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p0.73025 2.54 0.0
cuboid 4 1 4p0.889 2.54 0.0
,
unit 114
com='Fuel - Upper PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 0.0635 0.0
cylinder 2 1 0.7176 0.0635 0.0
cuboid 3 1 4p0.889 0.0635 0.0
,
unit 115
com='Reflector - Lower Moderator'
cuboid 3 1 4p0.889 0.3175 0.0
,
unit 116
com='Reflector - Lower Moderator + Lattice Grid'
cuboid 3 1 4p0.73025 2.54 0.0
cuboid 4 1 4p0.889 2.54 0.0
,
unit 117
com='Reflector - Upper Moderator + Lattice Grid'
cuboid 3 1 4p0.73025 2.54 0.0
cuboid 4 1 4p0.889 2.54 0.0
,
unit 118
com='Reflector - Upper Moderator'
cuboid 3 1 4p0.889 0.0635 0.0
,
unit 120
com='Moderator'
cuboid 3 1 4p0.889 86.6775 0.0
,
global unit 130
com='Cells in assembly'
array 1 -27.559 -27.559 0
cuboid 6 1 4p27.559 92.9640 -2.8575
cuboid 7 1 4p27.559 93.9165 -2.8575
replicate 3 2 6*3.0 4
replicate 3 6 4*3.0 1.462 3.0 1
replicate 3 7 4*3.0 0.0 3.0 5
end geometry
read array
ara=1 nux=31 nuy=31 nuz=5
fill
'Lower Cladding and Moderator
115 115 115 115 115 115 115 115 115 115 115 115 111
111 111 111 1b15
115 115 115 115 115 115 115 115 115 111 111 111 111
111 111 111 1b15
115 115 115 115 115 115 111 111 111 111 111 111
111 111 111 1b15

```

115 115 115 115 115 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 115 115 115 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 115 115 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 115 115 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 115 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 115 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 111 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 111 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 115 111 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 111 111 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 111 111 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b15  
 111 111 111 111 111 111 111 111 111 111 111 111 111  
     111 111 111 1b480  
     'Lower Lattice Grid  
 116 116 116 116 116 116 116 116 116 116 116 116 112  
     112 112 112 1b15  
 116 116 116 116 116 116 116 116 116 112 112 112 112  
     112 112 112 1b15  
 116 116 116 116 116 116 116 112 112 112 112 112 112  
     112 112 112 1b15  
 116 116 116 116 116 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 116 116 116 116 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 116 116 116 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 116 116 116 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 116 116 112 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 116 112 112 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 116 112 112 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 112 112 112 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 112 112 112 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15  
 112 112 112 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b15

112 112 112 112 112 112 112 112 112 112 112 112 112  
     112 112 112 1b480  
     'Fuel and Reflector  
 120 120 120 120 120 120 120 120 120 120 120 120 1 2  
     3 4 1b15  
 120 120 120 120 120 120 120 120 120 5 6 7 8 9 10  
     11 1b15  
 120 120 120 120 120 120 120 12 13 14 15 16 17 18  
     19 20 1b15  
 120 120 120 120 120 21 22 23 24 25 26 27 28 29 30  
     31 1b15  
 120 120 120 120 32 33 34 35 36 37 38 39 40 41 42  
     43 1b15  
 120 120 120 21 33 44 45 46 47 48 49 50 51 52 53  
     54 1b15  
 120 120 120 22 34 45 55 56 57 58 59 60 61 62 63  
     64 1b15  
 120 120 12 23 35 46 56 65 66 67 68 69 70 71 72  
     73 1b15  
 120 120 13 24 36 47 57 66 74 75 76 77 78 79 80  
     81 1b15  
 120 5 14 25 37 48 58 67 75 82 83 84 85 86 87 88  
     1b15  
 120 6 15 26 38 49 59 68 76 83 89 90 91 92 93 94  
     1b15  
 120 7 16 27 39 50 60 69 77 84 90 95 96 97 98 99  
     1b15  
 1 8 17 28 40 51 61 70 78 85 91 96 100 101 102  
     103 1b15  
 2 9 18 29 41 52 62 71 79 86 92 97 101 104 105  
     106 1b15  
 3 10 19 30 42 53 63 72 80 87 93 98 102 105 107  
     108 1b15  
 4 11 20 31 43 54 64 73 81 88 94 99 103 106 108  
     109 1b480  
     'Upper Lattice Grid  
 117 117 117 117 117 117 117 117 117 117 117 117 113  
     113 113 113 1b15  
 117 117 117 117 117 117 117 117 117 113 113 113 113  
     113 113 113 1b15  
 117 117 117 117 117 117 117 113 113 113 113 113 113  
     113 113 113 1b15  
 117 117 117 117 117 113 113 113 113 113 113 113 113  
     113 113 113 1b15  
 117 117 117 113 113 113 113 113 113 113 113 113 113  
     113 113 113 1b15  
 117 117 117 113 113 113 113 113 113 113 113 113 113  
     113 113 113 1b15  
 117 117 113 113 113 113 113 113 113 113 113 113 113  
     113 113 113 1b15  
 117 117 113 113 113 113 113 113 113 113 113 113 113  
     113 113 113 1b15  
 117 113 113 113 113 113 113 113 113 113 113 113 113  
     113 113 113 1b15  
 117 113 113 113 113 113 113 113 113 113 113 113 113



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113 113 113 1b15
117 113 113 113 113 113 113 113 113 113 113 113 113
113 113 113 1b15
113 113 113 113 113 113 113 113 113 113 113 113
113 113 113 1b15
113 113 113 113 113 113 113 113 113 113 113 113
113 113 113 1b15
113 113 113 113 113 113 113 113 113 113 113 113
113 113 113 1b480
'Upper Cladding and Moderator
114 114 114 114 114 114 114 114 114 114 114 114 118
118 118 118 1b15
114 114 114 114 114 114 114 114 114 118 118 118 118
118 118 118 1b15
114 114 114 114 114 114 118 118 118 118 118 118 118
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118 118 118 118 118 118 118 118 118 118 118 118 118
118 118 118 1b15
118 118 118 118 118 118 118 118 118 118 118 118 118
118 118 118 1b480
end fill
end array
read bias id=500 2 11 end bias
read plot
ttl='x-z plot at y=0.0'
xul=-50.0 yul=0. zul=110
xlr=50.0 ylr=0. zlr=-10.
uax=1.0 wdn=-1.0
nax=600 end plt0
ttl='x-y plot at z=25.0'
pic=mix
xul=-30.0 yul=30. zul=25.
xlr=30.0 ylr=-30. zlr=25.

```

```

uax=1.0 vdn=-1.0
nax=600 end plt1
end plot
end data
end
=shell
cp ft04f001 $RTNDIR/pnl31.xs04
cp ft64f001 $RTNDIR/pnl31.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92236 27 92236 18 92236 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
40000 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
28000 27
24000 27
26000 27
5010 27
5011 27
8016 27
1001 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5 parm=(size=1000000)
pnl-32 fuel

```

```

238group latticecell
  'MOX fuel
u-235 1 0 1.4886-4 295 end
u-238 1 0 2.0611-2 295 end
o 1 0 4.3779-2 295 end
u-234 1 0 1.2458-6 295 end
u-236 1 0 2.0936-9 295 end
pu-238 1 0 3.8836-8 295 end
pu-239 1 0 3.9262-4 295 end
pu-240 1 0 3.3206-5 295 end
pu-241 1 0 1.6081-6 295 end
pu-242 1 0 1.1882-7 295 end
am-241 1 0 1.4891-6 295 end
  'clad (ZR-2)
zr 2 0 4.2621-2 295 end
sn 2 0 4.8328-4 295 end
ni 2 0 3.0336-5 295 end
cr 2 0 7.6093-5 295 end
fe 2 0 9.5642-5 295 end
  'water(Reflector)
h 3 0 6.6706-2 295 end
o 3 0 3.3353-2 295 end
b-10 3 0 9.9034-9 295 end
b-11 3 0 4.0114-8 295 end
  'Lattice Grid
si 4 0 3.4607-4 295 end
fe 4 0 1.0152-4 295 end
cu 4 0 6.3731-5 295 end
mn 4 0 2.2115-5 295 end
mg 4 0 6.6651-4 295 end
cr 4 0 6.2310-5 295 end
ti 4 0 2.5375-5 295 end
al 4 0 5.8433-2 295 end
  'UO2
u-234 5 0 1.2406-6 295 end
u-235 5 0 1.4824-4 295 end
u-236 5 0 2.0848-9 295 end
u-238 5 0 2.0525-2 295 end
o 5 0 4.1943-2 295 end
  'Aluminum
si 6 0 3.4607-4 295 end
fe 6 0 1.0152-4 295 end
cu 6 0 6.3731-5 295 end
mn 6 0 2.2115-5 295 end
mg 6 0 6.6651-4 295 end
cr 6 0 6.2310-5 295 end
ti 6 0 2.5375-5 295 end
al 6 0 5.8433-2 295 end
  'lead
pb 7 0 3.2174-2 295 end
end comp
squarepitch 2.20914 1.2827 1 2 1.4351 3 end
  more data
  limcen=20000000
  end more
  PNL-32
  read param

```

```

gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
plt=no lng=2000000
end param
read geometry
  ,
  unit 1
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 2
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 3
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 4
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 5
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 6
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 7
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 8
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.10457 86.6775 0.0
  ,
  unit 9
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0

```





















cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 181  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 182  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 183  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 184  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 185  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 186  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 187  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 188  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 189  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,

unit 190  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 191  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 192  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 193  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 194  
 com='1PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 195  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.10457 86.6775 0.0  
 ,  
 unit 201  
 com='Fuel - Lower Clad + Moderator'  
 cylinder 2 1 0.7176 0.3175 0.0  
 cuboid 3 1 4p1.10457 0.3175 0.0  
 ,  
 unit 202  
 com='Fuel - Lower PuO2/UO2 + UO2 + Clad + Moderator  
 + Lattice Grid'  
 cylinder 1 1 0.6414 2.54 0.881  
 cylinder 5 1 0.6414 2.54 0.381  
 cylinder 2 1 0.7176 2.54 0.0  
 cuboid 3 1 4p1.02329 2.54 0.0  
 cuboid 4 1 4p1.10457 2.54 0.0  
 ,  
 unit 203  
 com='Fuel - Upper PuO2/UO2 + Clad + Moderator +  
 Lattice Grid'  
 cylinder 1 1 0.6414 2.54 0.0  
 cylinder 2 1 0.7176 2.54 0.0  
 cuboid 3 1 4p1.02329 2.54 0.0  
 cuboid 4 1 4p1.10457 2.54 0.0

	201 201 201 201
unit 204	201 201 201 201 201 201 201 201 201 201 201 201 201 201
com='Fuel - Upper PuO2/UO2 + Clad + Moderator'	201 201 201 201
cylinder 1 1 0.6414 0.0635 0.0	201 201 201 201 201 201 201 201 201 201 201 201 201 201
cylinder 2 1 0.7176 0.0635 0.0	201 201 201 201
cuboid 3 1 4p1.10457 0.0635 0.0	205 201 201 201 201 201 201 201 201 201 201 201 201 201
	201 201 201 205
unit 205	205 201 201 201 201 201 201 201 201 201 201 201 201 201
com='Reflector - Lower Moderator'	201 201 201 205
cuboid 3 1 4p1.10457 0.3175 0.0	205 205 201 201 201 201 201 201 201 201 201 201 201 201
	201 201 205 205
unit 206	205 205 205 201 201 201 201 201 201 201 201 201 201 201
com='Reflector - Lower Moderator + Lattice Grid'	201 205 205 205
cuboid 3 1 4p1.02329 2.54 0.0	205 205 205 205 201 201 201 201 201 201 201 201 201 201
cuboid 4 1 4p1.10457 2.54 0.0	205 205 205 205
	205 205 205 205 205 201 201 201 201 201 201 205 205
unit 207	205 205 205 205
com='Reflector - Upper Moderator + Lattice Grid'	205 205 205 205 205 205 205 201 201 201 201 205 205 205
cuboid 3 1 4p1.02329 2.54 0.0	205 205 205 205
cuboid 4 1 4p1.10457 2.54 0.0	'Lower Lattice Grid
	206 206 206 206 206 206 206 202 202 202 206 206 206
unit 208	206 206 206 206
com='Reflector - Upper Moderator'	206 206 206 206 206 206 202 202 202 202 202 202 202 206
cuboid 3 1 4p1.10457 0.0635 0.0	206 206 206 206
	206 206 206 206 202 202 202 202 202 202 202 202 202
unit 210	206 206 206 202
com='Moderator'	202 202 202 202 202 202 202 202 202 202 202 202
cuboid 3 1 4p1.10457 86.6775 0.0	202 206 206 206
	206 206 202 202 202 202 202 202 202 202 202 202 202
global unit 220	202 202 206 206
com='Cells in assembly'	206 202 202 202 202 202 202 202 202 202 202 202 202 202
array 1 -18.77769 -18.77769 0	202 202 202 206
cuboid 6 1 4p18.77769 92.9640 -2.8575	206 202 202 202 202 202 202 202 202 202 202 202 202 202
cuboid 7 1 4p18.77769 93.9165 -2.8575	202 202 202 206
replicate 3 2 4*3.0 3.937 3.0 1	202 202 202 202 202 202 202 202 202 202 202 202 202 202
replicate 3 3 4*3.0 0.0 3.0 9	202 202 202 202
cuboid 3 1 4p48.77769 97.8535 -32.8575	202 202 202 202 202 202 202 202 202 202 202 202 202 202
end geometry	202 202 202 202
read array	202 202 202 202 202 202 202 202 202 202 202 202 202 202
ara=1 nux=17 nuy=17 nuz=5	202 202 202 202
fill	206 202 202 202 202 202 202 202 202 202 202 202 202 202
'Lower Cladding and Moderator	202 202 202 206
205 205 205 205 205 205 205 201 201 201 205 205 205	206 202 202 202 202 202 202 202 202 202 202 202 202 202
205 205 205 205	202 202 202 206
205 205 205 205 205 205 201 201 201 201 201 201 205	206 206 202 202 202 202 202 202 202 202 202 202 202 202
205 205 205 205	202 202 206 206
205 205 205 205 201 201 201 201 201 201 201 201 201 201	206 206 206 202 202 202 202 202 202 202 202 202 202 202
205 205 205 205	202 206 206 206
205 205 205 201 201 201 201 201 201 201 201 201 201 201	206 206 206 206 202 202 202 202 202 202 202 202 202 202
205 205 201 201 201 201 201 201 201 201 201 201 201 201	206 206 206 206
201 201 205 205	206 206 206 206
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205 201 201 201 201 201 201 201 201 201 201 201 201 201	206 206 206 206
201 201 201 201 201 201 201 201 201 201 201 201 201 201	'Fuel and Reflector
	210 210 210 210 210 210 210 193 194 195 210 210 210
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    210 210 210 210
210 210 210 210 178 179 180 181 182 183 184 185 186
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    177 210 210 210
210 210 154 155 156 157 158 159 160 161 162 163 164
    165 166 210 210
210 139 140 141 142 143 144 145 146 147 148 149 150
    151 152 153 210
210 124 125 126 127 128 129 130 131 132 133 134 135
    136 137 138 210
107 108 109 110 111 112 113 114 115 116 117 118 119
    120 121 122 123
90 91 92 93 94 95 96 97 98 99 100 101 102 103 104
    105 106
73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88
    89
210 58 59 60 61 62 63 64 65 66 67 68 69 70 71
    72 210
210 43 44 45 46 47 48 49 50 51 52 53 54 55 56
    57 210
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    210 210 210
    'Upper Lattice Grid
207 207 207 207 207 207 207 203 203 203 207 207 207
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    207 207 207 207
    'Upper Cladding and Moderator
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208 208 208 208 208 208 208 204 204 204 208 208 208
    208 208 208 208
    end fill
    end array
read bias id=500 2 11 end bias
read plot
ttl='x-z plot at y=0.0'
xul=-30.0 yul=0. zul=110
xlr=30.0 ylr=0. zlr=-10.
uax=1.0 wdn=-1.0
nax=600 end plt0
ttl='x-y plot at z=25.0'
pic=mix
xul=-30.0 yul=30. zul=25.

```

```

xlr=30.0 ylr=-30. zlr=25.
uax=1.0 vdn=-1.0
nax=600 end plt1
end plot
end data
end
=shell
cp ft04f001 $RTNDR/pnl32.xs04
cp ft64f001 $RTNDR/pnl32.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92236 27 92236 18 92236 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
40000 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
28000 27
24000 27
26000 27
5010 27
5011 27
8016 27
1001 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5      parm=(size=1000000)

```

```

pnl-33 fuel
238group latticecell
'MOX fuel
u-235 1 0 1.4886-4 295 end
u-238 1 0 2.0611-2 295 end
o 1 0 4.3779-2 295 end
u-234 1 0 1.2458-6 295 end
u-236 1 0 2.0936-9 295 end
pu-238 1 0 3.8836-8 295 end
pu-239 1 0 3.9262-4 295 end
pu-240 1 0 3.3206-5 295 end
pu-241 1 0 1.6081-6 295 end
pu-242 1 0 1.1882-7 295 end
am-241 1 0 1.4891-6 295 end
'clad (ZR-2)
zr 2 0 4.2621-2 295 end
sn 2 0 4.8328-4 295 end
ni 2 0 3.0336-5 295 end
cr 2 0 7.6093-5 295 end
fe 2 0 9.5642-5 295 end
'water(Reflector)
h 3 0 6.6672-2 295 end
o 3 0 3.3427-2 295 end
b-10 3 0 1.2034-5 295 end
b-11 3 0 4.8746-5 295 end
'Lattice Grid
si 4 0 3.4607-4 295 end
fe 4 0 1.0152-4 295 end
cu 4 0 6.3731-5 295 end
mn 4 0 2.2115-5 295 end
mg 4 0 6.6651-4 295 end
cr 4 0 6.2310-5 295 end
ti 4 0 2.5375-5 295 end
al 4 0 5.8433-2 295 end
'UO2
u-234 5 0 1.2406-6 295 end
u-235 5 0 1.4824-4 295 end
u-236 5 0 2.0848-9 295 end
u-238 5 0 2.0525-2 295 end
o 5 0 4.1943-2 295 end
'Aluminum
si 6 0 3.4607-4 295 end
fe 6 0 1.0152-4 295 end
cu 6 0 6.3731-5 295 end
mn 6 0 2.2115-5 295 end
mg 6 0 6.6651-4 295 end
cr 6 0 6.2310-5 295 end
ti 6 0 2.5375-5 295 end
al 6 0 5.8433-2 295 end
'lead
pb 7 0 3.2174-2 295 end
end comp
squarepitch 2.20914 1.2827 1 2 1.4351 3 end
more data
limcen=20000000
end more
PNL-33

```

```

read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
plt=no lng=2000000
end param
read geometry
,
unit 1
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 2
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 3
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 4
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 5
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 6
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 7
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 8
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 9
com='PuO2/UO2 + Clad + Moderator'

```

```

cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 10
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 11
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 12
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 13
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 14
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 15
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 16
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 17
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 18
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0

```











```

,
unit 95
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 96
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 97
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 98
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 99
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 100
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 101
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 102
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 103
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 104
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 105
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 106
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 107
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 108
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 109
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.1046 86.6775 0.0
,
unit 111
com='Fuel - Lower Clad + Moderator'
cylinder 2 1 0.7176 0.3175 0.0
cuboid 3 1 4p1.1046 0.3175 0.0
,
unit 112
com='Fuel - Lower PuO2/UO2 + UO2 + Clad + Moderator
+ Lattice Grid'
cylinder 1 1 0.6414 2.54 0.881
cylinder 5 1 0.6414 2.54 0.381
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p1.02329 2.54 0.0
cuboid 4 1 4p1.1046 2.54 0.0
,
unit 113
com='Fuel - Upper PuO2/UO2 + Clad + Moderator +
Lattice Grid'
cylinder 1 1 0.6414 2.54 0.0
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p1.02329 2.54 0.0
cuboid 4 1 4p1.1046 2.54 0.0
,
unit 114

```



```

120 120 120 120 32 33 34 35 36 37 38 39 40 41 42
      43 lb15
120 120 120 21 33 44 45 46 47 48 49 50 51 52 53
      54 lb15
120 120 120 22 34 45 55 56 57 58 59 60 61 62 63
      64 lb15
120 120 12 23 35 46 56 65 66 67 68 69 70 71 72
      73 lb15
120 120 13 24 36 47 57 66 74 75 76 77 78 79 80
      81 lb15
120 5 14 25 37 48 58 67 75 82 83 84 85 86 87 88
      lb15
120 6 15 26 38 49 59 68 76 83 89 90 91 92 93 94
      lb15
120 7 16 27 39 50 60 69 77 84 90 95 96 97 98 99
      lb15
  1 8 17 28 40 51 61 70 78 85 91 96 100 101 102
      103 lb15
  2 9 18 29 41 52 62 71 79 86 92 97 101 104 105
      106 lb15
  3 10 19 30 42 53 63 72 80 87 93 98 102 105 107
      108 lb15
  4 11 20 31 43 54 64 73 81 88 94 99 103 106 108
      109 lb480
      'Upper Lattice Grid
117 117 117 117 117 117 117 117 117 117 117 117 113
      113 113 113 lb15
117 117 117 117 117 117 117 117 117 113 113 113 113
      113 113 113 lb15
117 117 117 117 117 117 117 113 113 113 113 113 113
      113 113 113 lb15
117 117 117 117 117 113 113 113 113 113 113 113 113
      113 113 113 lb15
117 117 117 117 113 113 113 113 113 113 113 113 113
      113 113 113 lb15
117 117 113 113 113 113 113 113 113 113 113 113 113
      113 113 113 lb15
117 113 113 113 113 113 113 113 113 113 113 113 113
      113 113 113 lb15
117 113 113 113 113 113 113 113 113 113 113 113 113
      113 113 113 lb15
113 113 113 113 113 113 113 113 113 113 113 113 113
      113 113 113 lb15
113 113 113 113 113 113 113 113 113 113 113 113 113
      113 113 113 lb15
113 113 113 113 113 113 113 113 113 113 113 113 113
      113 113 113 lb480

```

```

      'Upper Cladding and Moderator
114 114 114 114 114 114 114 114 114 114 114 114 118
      118 118 118 lb15
114 114 114 114 114 114 114 114 114 118 118 118 118
      118 118 118 lb15
114 114 114 114 114 114 114 118 118 118 118 118 118
      118 118 118 lb15
114 114 114 114 114 118 118 118 118 118 118 118 118
      118 118 118 lb15
114 114 114 114 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
114 114 114 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
114 114 114 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
114 114 118 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
114 118 118 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
114 118 118 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
114 118 118 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
118 118 118 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
118 118 118 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb15
118 118 118 118 118 118 118 118 118 118 118 118 118
      118 118 118 lb480
      end fill
      end array
read bias id=500 2 11 end bias
read plot
  ttl='x-z plot at y=0.0'
  xul=-50.0 yul=0. zul=110
  xlr=50.0 ylr=0. zlr=-10.
  uax=1.0 wdn=-1.0
  max=600 end plt0
  ttl='x-y plot at z=25.0'
  pic=mix
  xul=-30.0 yul=30. zul=25.
  xlr=30.0 ylr=-30. zlr=25.
  uax=1.0 vdn=-1.0
  max=600 end plt1
  end plot
  end data
  end
  =shell
cp ft04f001 $RTNDIR/pnl33.xs04
cp ft64f001 $RTNDIR/pnl33.rs64
  end
  =kmart
read initial kunit=64

```

```

xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92236 27 92236 18 92236 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
40000 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
28000 27
24000 27
26000 27
5010 27
5011 27
8016 27
1001 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=(size=1000000)
pnl-34 fuel
238group latticecell
'MOX fuel
u-235 1 0 1.4886-4 295 end
u-238 1 0 2.0611-2 295 end
o 1 0 4.3779-2 295 end
u-234 1 0 1.2458-6 295 end
u-236 1 0 2.0936-9 295 end
pu-238 1 0 3.8836-8 295 end
pu-239 1 0 3.9262-4 295 end
pu-240 1 0 3.3206-5 295 end
pu-241 1 0 1.6081-6 295 end

pu-242 1 0 1.1882-7 295 end
am-241 1 0 1.4891-6 295 end
'clad (ZR-2)
zr 2 0 4.2621-2 295 end
sn 2 0 4.8328-4 295 end
ni 2 0 3.0336-5 295 end
cr 2 0 7.6093-5 295 end
fe 2 0 9.5642-5 295 end
'water(Reflector)
h 3 0 6.6706-2 295 end
o 3 0 3.3353-2 295 end
b-10 3 0 1.7606-8 295 end
b-11 3 0 7.1313-8 295 end
'Lattice Grid
si 4 0 3.4607-4 295 end
fe 4 0 1.0152-4 295 end
cu 4 0 6.3731-5 295 end
mn 4 0 2.2115-5 295 end
mg 4 0 6.6651-4 295 end
cr 4 0 6.2310-5 295 end
ti 4 0 2.5375-5 295 end
al 4 0 5.8433-2 295 end
'UO2
u-234 5 0 1.2406-6 295 end
u-235 5 0 1.4824-4 295 end
u-236 5 0 2.0848-9 295 end
u-238 5 0 2.0525-2 295 end
o 5 0 4.1943-2 295 end
'Aluminum
si 6 0 3.4607-4 295 end
fe 6 0 1.0152-4 295 end
cu 6 0 6.3731-5 295 end
mn 6 0 2.2115-5 295 end
mg 6 0 6.6651-4 295 end
cr 6 0 6.2310-5 295 end
ti 6 0 2.5375-5 295 end
al 6 0 5.8433-2 295 end
'lead
pb 7 0 3.2174-2 295 end
end comp
squarepitch 2.51447 1.2827 1 2 1.4351 3 end
more data
limcen=20000000
end more
PNL-34
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
plt=no lng=2000000
end param
read geometry
'
unit 1
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0

```





```

unit 21
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
,
unit 22
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
,
unit 23
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
,
unit 24
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
,
unit 25
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
,
unit 26
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
,
unit 27
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
,
unit 31
com='Fuel - Lower Clad + Moderator'
cylinder 2 1 0.7176 0.3175 0.0
cuboid 3 1 4p1.257235 0.3175 0.0
,
unit 32
com='Fuel - Lower PuO2/UO2 + UO2 + Clad + Moderator
+ Lattice Grid'
cylinder 1 1 0.6414 2.54 0.881
cylinder 5 1 0.6414 2.54 0.381
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p0.939735 2.54 0.0
cuboid 4 1 4p1.257235 2.54 0.0
,
unit 33
com='Fuel - Upper PuO2/UO2 + Clad + Moderator +
Lattice Grid'
cylinder 1 1 0.6414 2.54 0.0
cylinder 2 1 0.7176 2.54 0.0
cuboid 3 1 4p0.939735 2.54 0.0
cuboid 4 1 4p1.257235 2.54 0.0
,
unit 34
com='Fuel - Upper PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 0.0635 0.0
cylinder 2 1 0.7176 0.0635 0.0
cuboid 3 1 4p1.257235 0.0635 0.0
,
unit 35
com='Reflector - Lower Moderator'
cuboid 3 1 4p1.257235 0.3175 0.0
,
unit 36
com='Reflector - Lower Moderator + Lattice Grid'
cuboid 3 1 4p0.939735 2.54 0.0
cuboid 4 1 4p1.257235 2.54 0.0
,
unit 37
com='Reflector - Upper Moderator + Lattice Grid'
cuboid 3 1 4p0.939735 2.54 0.0
cuboid 4 1 4p1.257235 2.54 0.0
,
unit 38
com='Reflector - Upper Moderator'
cuboid 3 1 4p1.257235 0.0635 0.0
,
unit 40
com='Moderator'
cuboid 3 1 4p1.257235 86.6775 0.0
,
global unit 50
com='Cells in assembly'
array 1 -21.372995 -21.372995 0
cuboid 6 1 4p21.372995 92.9640 -2.8575
cuboid 7 1 4p21.372995 93.9165 -2.8575
replicate 3 2 4*3.0 0.508 3.0 1
replicate 3 3 4*3.0 0.0 3.0 9
end geometry
read array
ara=1 nux=17 nuy=17 nuz=5
fill
'Lower Cladding and Moderator
35 35 35 35 35 35 35 35 31 1b8
35 35 35 35 35 35 35 35 31 31 1b8
35 35 35 35 35 35 31 31 31 31 1b8
35 35 35 35 31 31 31 31 31 31 1b8
35 35 35 31 31 31 31 31 31 31 1b8
35 35 31 31 31 31 31 31 31 31 1b8
35 31 31 31 31 31 31 31 31 31 1b8
31 31 31 31 31 31 31 31 31 31 1b144

```

```

'Lower Lattice Grid
36 36 36 36 36 36 36 36 32 1b8
36 36 36 36 36 36 36 32 32 1b8
36 36 36 36 36 32 32 32 32 1b8
36 36 36 36 32 32 32 32 32 1b8
36 36 36 32 32 32 32 32 32 1b8
36 36 32 32 32 32 32 32 32 1b8
36 36 32 32 32 32 32 32 32 1b8
36 32 32 32 32 32 32 32 32 1b8
32 32 32 32 32 32 32 32 32 1b144
'Fuel and Reflector
40 40 40 40 40 40 40 40 1 1b8
40 40 40 40 40 40 40 2 3 1b8
40 40 40 40 40 4 5 6 7 1b8
40 40 40 40 8 9 10 11 12 1b8
40 40 40 8 13 14 15 16 17 1b8
40 40 4 9 14 18 19 20 21 1b8
40 40 5 10 15 19 22 23 24 1b8
40 2 6 11 16 20 23 25 26 1b8
1 3 7 12 17 21 24 26 27 1b144
'Upper Lattice Grid
37 37 37 37 37 37 37 37 33 1b8
37 37 37 37 37 37 37 33 33 1b8
37 37 37 37 37 33 33 33 33 1b8
37 37 37 37 33 33 33 33 33 1b8
37 37 33 33 33 33 33 33 33 1b8
37 37 33 33 33 33 33 33 33 1b8
37 33 33 33 33 33 33 33 33 1b8
33 33 33 33 33 33 33 33 33 1b144
'Upper Cladding and Moderator
38 38 38 38 38 38 38 38 34 1b8
38 38 38 38 38 38 38 34 34 1b8
38 38 38 38 38 34 34 34 34 1b8
38 38 38 38 34 34 34 34 34 1b8
38 38 38 34 34 34 34 34 34 1b8
38 38 34 34 34 34 34 34 34 1b8
38 38 34 34 34 34 34 34 34 1b8
38 34 34 34 34 34 34 34 34 1b8
34 34 34 34 34 34 34 34 34 1b144
end fill
end array
read bias id=500 2 11 end bias
read plot
ttl='x-z plot at y=0.0'
xul=-30.0 yul=0. zul=110
xlr=30.0 ylr=0. zlr=-10.
uax=1.0 wdn=-1.0
nax=600 end plt0
ttl='x-y plot at z=25.0'
pic=mix
xul=-30.0 yul=30. zul=25.
xlr=30.0 ylr=-30. zlr=25.
uax=1.0 vdn=-1.0
nax=600 end plt1
end plot
end data

end
=shell
cp ft04f001 $RTNDIR/pnl34.xs04
cp ft64f001 $RTNDIR/pnl34.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92236 27 92236 18 92236 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
40000 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
28000 27
24000 27
26000 27
5010 27
5011 27
8016 27
1001 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5 parm=(size=1000000)
pnl-35 fuel
238group latticecell
'MOX fuel
u-235 1 0 1.4886-4 295 end
u-238 1 0 2.0611-2 295 end

```

```

o 1 0 4.3779-2 295 end
u-234 1 0 1.2458-6 295 end
u-236 1 0 2.0936-9 295 end
pu-238 1 0 3.8836-8 295 end
pu-239 1 0 3.9262-4 295 end
pu-240 1 0 3.3206-5 295 end
pu-241 1 0 1.6081-6 295 end
pu-242 1 0 1.1882-7 295 end
am-241 1 0 1.4891-6 295 end
'clad (ZR-2)
zr 2 0 4.2621-2 295 end
sn 2 0 4.8328-4 295 end
ni 2 0 3.0336-5 295 end
cr 2 0 7.6093-5 295 end
fe 2 0 9.5642-5 295 end
'water(Reflector)
h 3 0 6.6682-2 295 end
o 3 0 3.3405-2 295 end
b-10 3 0 8.4597-6 295 end
b-11 3 0 3.4266-5 295 end
'Lattice Grid
si 4 0 3.4607-4 295 end
fe 4 0 1.0152-4 295 end
cu 4 0 6.3731-5 295 end
mn 4 0 2.2115-5 295 end
mg 4 0 6.6651-4 295 end
cr 4 0 6.2310-5 295 end
ti 4 0 2.5375-5 295 end
al 4 0 5.8433-2 295 end
'UO2
u-234 5 0 1.2406-6 295 end
u-235 5 0 1.4824-4 295 end
u-236 5 0 2.0848-9 295 end
u-238 5 0 2.0525-2 295 end
o 5 0 4.1943-2 295 end
'Aluminum
si 6 0 3.4607-4 295 end
fe 6 0 1.0152-4 295 end
cu 6 0 6.3731-5 295 end
mn 6 0 2.2115-5 295 end
mg 6 0 6.6651-4 295 end
cr 6 0 6.2310-5 295 end
ti 6 0 2.5375-5 295 end
al 6 0 5.8433-2 295 end
'lead
pb 7 0 3.2174-2 295 end
end comp
squarepitch 2.51447 1.2827 1 2 1.4351 3 end
more data
limcen=20000000
end more
PNL-35
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
plt=no lng=2000000
end param

read geometry
'
unit 1
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 2
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 3
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 4
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 5
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 6
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 7
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 8
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 9
com='PuO2/UO2 + Clad + Moderator'
cylinder 1 1 0.6414 86.6775 0.0
cylinder 2 1 0.7176 86.6775 0.0
cuboid 3 1 4p1.257235 86.6775 0.0
'
unit 10

```











com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 87  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 88  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 89  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 90  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 91  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 92  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 93  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 94  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 95  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0

cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 96  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 97  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 98  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 99  
 com='PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 86.6775 0.0  
 cylinder 2 1 0.7176 86.6775 0.0  
 cuboid 3 1 4p1.257235 86.6775 0.0  
 ,  
 unit 100  
 com='Fuel - Lower Clad + Moderator'  
 cylinder 2 1 0.7176 0.3175 0.0  
 cuboid 3 1 4p1.257235 0.3175 0.0  
 ,  
 unit 101  
 com='Fuel - Lower PuO2/UO2 + UO2 + Clad + Moderator  
 + Lattice Grid'  
 cylinder 1 1 0.6414 2.54 0.881  
 cylinder 5 1 0.6414 2.54 0.381  
 cylinder 2 1 0.7176 2.54 0.0  
 cuboid 3 1 4p0.939735 2.54 0.0  
 cuboid 4 1 4p1.257235 2.54 0.0  
 ,  
 unit 102  
 com='Fuel - Upper PuO2/UO2 + Clad + Moderator +  
 Lattice Grid'  
 cylinder 1 1 0.6414 2.54 0.0  
 cylinder 2 1 0.7176 2.54 0.0  
 cuboid 3 1 4p0.939735 2.54 0.0  
 cuboid 4 1 4p1.257235 2.54 0.0  
 ,  
 unit 103  
 com='Fuel - Upper PuO2/UO2 + Clad + Moderator'  
 cylinder 1 1 0.6414 0.0635 0.0  
 cylinder 2 1 0.7176 0.0635 0.0  
 cuboid 3 1 4p1.257235 0.0635 0.0  
 ,  
 unit 104  
 com='Reflector - Lower Moderator'  
 cuboid 3 1 4p1.257235 0.3175 0.0

```

          ,
          unit 106
com='Reflector - Lower Moderator + Lattice Grid'
  cuboid 3 1 4p0.939735 2.54 0.0
  cuboid 4 1 4p1.257235 2.54 0.0
          ,
          unit 107
com='Reflector - Upper Moderator + Lattice Grid'
  cuboid 3 1 4p0.939735 2.54 0.0
  cuboid 4 1 4p1.257235 2.54 0.0
          ,
          unit 108
com='Reflector - Upper Moderator'
  cuboid 3 1 4p1.257235 0.0635 0.0
          ,
          unit 110
com='Moderator'
  cuboid 3 1 4p1.257235 86.6775 0.0
          ,
          global unit 120
com='Cells in assembly'
  array 1 -36.459815 -36.459815 0
  cuboid 6 1 4p36.459815 92.9640 -2.8575
  cuboid 7 1 4p36.459815 93.9165 -2.8575
  replicate 3 2 6*3.0 4
  replicate 3 6 4*3.0 1.462 3.0 1
  replicate 3 7 4*3.0 0.0 3.0 5
  end geometry
  read array
  ara=1 nux=29 nuy=29 nuz=5
  fill
  'Lower Cladding and Moderator
105 105 105 105 105 105 105 105 105 101 101 101 101
  101 101 1b14
105 105 105 105 105 105 105 101 101 101 101 101 101
  101 101 1b14
105 105 105 105 105 105 101 101 101 101 101 101 101
  101 101 1b14
105 105 105 105 105 101 101 101 101 101 101 101 101
  101 101 1b14
105 105 105 105 101 101 101 101 101 101 101 101 101
  101 101 1b14
105 105 105 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
105 105 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
105 105 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
105 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
105 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
          ,
          101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
101 101 101 101 101 101 101 101 101 101 101 101 101
  101 101 1b14
          ,
          'Lower Lattice Grid
106 106 106 106 106 106 106 106 106 106 102 102 102 102
  102 102 1b14
106 106 106 106 106 106 106 106 102 102 102 102 102 102
  102 102 1b14
106 106 106 106 106 106 106 102 102 102 102 102 102 102
  102 102 1b14
106 106 106 106 106 106 102 102 102 102 102 102 102 102
  102 102 1b14
106 106 106 106 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
106 106 106 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
106 106 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
106 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
106 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
102 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
102 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
102 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
102 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
102 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
102 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
102 102 102 102 102 102 102 102 102 102 102 102 102 102
  102 102 1b14
          ,
          'Fuel and Reflector
110 110 110 110 110 110 110 110 110 1 2 3 4 5 6
  1b14
110 110 110 110 110 110 110 110 7 8 9 10 11 12 13 14
  1b14
110 110 110 110 110 110 15 16 17 18 19 20 21 22 23
  1b14
110 110 110 110 110 24 25 26 27 28 29 30 31 32 33
  1b14
110 110 110 110 34 35 36 37 38 39 40 41 42 43 44
  1b14
110 110 110 24 35 45 46 47 48 49 50 51 52 53 54
  1b14
110 110 15 25 36 46 55 56 57 58 59 60 61 62 63
  1b14
110 7 16 26 37 47 56 64 65 66 67 68 69 70 71
  1b14
110 8 17 27 38 48 57 65 72 73 74 75 76 77 78
  1b14
1 9 18 28 39 49 58 66 73 79 80 81 82 83 84
  1b14

```



50115 27  
50116 27  
50117 27  
50118 27  
50119 27  
50120 27  
50122 27  
50124 27  
28000 27  
24000 27  
26000 27  
5010 27  
5011 27  
8016 27  
1001 27  
end activity  
read collapse  
factor=1.0  
lastg=57  
lastg=148  
lastg=204  
lastg=238  
end collapse  
end

**APPENDIX B**

**SCALE INPUT OF MIX-COMP-THERM-3 PROBLEM SET**



## APPENDIX B

### SCALE INPUT OF MIX-COMP-THERM-3 PROBLEM SET

This appendix contains the CENTRM inputs for the six MIX-COMP-THERM-03 cases, SAXTON01, SAXTON02, SAXTON03, SAXTON04, SAXTON05, and SAXTON06. The inputs can be changed to standard CSAS cases by replacing the =CSASC5 record with =CSAS25.

The input for the cases are listed below.

<pre> =csasc5      parm=size=1000000               saxton 1 fuel               238group latticecell               'MOX fuel pu-239 1 0 1.3526-3 299 end pu-240 1 0 1.2759-4 299 end pu-241 1 0 1.1407-5 299 end pu-242 1 0 6.0318-7 299 end am-241 1 0 1.7783-6 299 end u-234 1 0 1.1688-6 299 end u-235 1 0 1.5301-4 299 end u-238 1 0 2.1097-2 299 end o 1 0 4.5155-2 299 end               'clad (ZR-2) zr 2 0 4.2517-2 299 end sn 2 0 4.6590-4 299 end cr 2 0 7.5977-5 299 end fe 2 0 1.4148-4 299 end o 2 0 2.9630-4 299 end               'water(Reflector) h 3 0 6.6643-2 299 end o 3 0 3.3322-2 299 end 'b-10 3 0 1.7606-8 299 end 'b-11 3 0 7.1313-8 299 end               'Middle Grid and H2O al 4 .8004 299 end h2o 4 .1996 299 end               'Aluminum al 5 0 6.0039-2 295 end               end comp squarepitch 1.3208 .856996 1 2 .99314 3 .87503 0 end               more data               limcen=20000000               end more               saxton 1               read param gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64               res=225               lng=2000000               end param               read geometry               '               unit 1 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 cylinder 0 1 0.437515 82.90 0.00 cylinder 2 1 0.49657 82.90 0.00 </pre>	<pre> cylinder 2 1 0.49657 82.90 -1.27 cuboid 3 1 4p.6604 82.90 -1.27               unit 2 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 cylinder 0 1 0.437515 82.90 0.00 cylinder 2 1 0.49657 82.90 0.00 cylinder 2 1 0.49657 82.90 -1.27 cuboid 3 1 4p.6604 82.90 -1.27               unit 3 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 cylinder 0 1 0.437515 82.90 0.00 cylinder 2 1 0.49657 82.90 0.00 cylinder 2 1 0.49657 82.90 -1.27 cuboid 3 1 4p.6604 82.90 -1.27               unit 4 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 cylinder 0 1 0.437515 82.90 0.00 cylinder 2 1 0.49657 82.90 0.00 cylinder 2 1 0.49657 82.90 -1.27 cuboid 3 1 4p.6604 82.90 -1.27               unit 5 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 cylinder 0 1 0.437515 82.90 0.00 cylinder 2 1 0.49657 82.90 0.00 cylinder 2 1 0.49657 82.90 -1.27 cuboid 3 1 4p.6604 82.90 -1.27               unit 6 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 cylinder 0 1 0.437515 82.90 0.00 cylinder 2 1 0.49657 82.90 0.00 cylinder 2 1 0.49657 82.90 -1.27 cuboid 3 1 4p.6604 82.90 -1.27               unit 7 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 cylinder 0 1 0.437515 82.90 0.00 cylinder 2 1 0.49657 82.90 0.00 cylinder 2 1 0.49657 82.90 -1.27 cuboid 3 1 4p.6604 82.90 -1.27               unit 8 com='Fuel + Gap + Clad + Moderator' cylinder 1 1 0.428498 82.90 0.00 </pre>
------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

















```

cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 123
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 124
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 125
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 126
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 127
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 128
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 129
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 130
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 131
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 132
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 82.90 0.00
cylinder 0 1 0.437515 82.90 0.00
cylinder 2 1 0.49657 82.90 0.00
cylinder 2 1 0.49657 82.90 -1.27
cuboid 3 1 4p.6604 82.90 -1.27
unit 141
com='Clad + Mod + AL Grid'
cylinder 2 1 0.49657 0.635 0.0
cylinder 3 1 0.50419 0.635 0.0
cuboid 5 1 4p.6604 0.635 0.0
unit 143
com='Fuel + Gap + Clad + Air'
cylinder 1 1 0.428498 10.064 0.0
cylinder 0 1 0.437515 10.064 0.0
cylinder 2 1 0.49657 10.064 0.0
cuboid 0 1 4p.6604 10.064 0.0
unit 144
com='Top Clad + Void'
cylinder 2 1 0.49657 1.016 0.0
cuboid 0 1 4p.6604 1.016 0.0
unit 145
com='Top Clad + Void + AL grid'
cylinder 2 1 0.49657 1.27 0.0
cylinder 0 1 0.50419 1.27 0.0
cuboid 5 1 4p.6604 1.27 0.0
unit 151
com='array of Clad + Mod + AL Grid + Reflector'
array 1 -15.1892 -14.5288 0.0
cuboid 4 1 2p45.1892 2p44.5288 0.635 0.0
unit 152
com='array of Fuel + Gap + Clad + Moderator + Reflector'
array 2 -15.1892 -14.5288 -1.27
cuboid 3 1 2p45.1892 2p44.5288 82.90 -1.27
unit 153
com='array of Fuel + Gap + Clad + Air'
array 3 -15.1892 -14.5288 0.0
cuboid 0 1 2p45.1892 2p44.5288 10.064 0.0

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unit 154
com='array of Top Clad + Void'
array 4 -15.1892 -14.5288 0.0
cuboid 0 1 2p45.1892 2p44.5288 1.016 0.0

unit 155
com='array of Top Clad + Void + AL grid'
array 5 -15.1892 -14.5288 0.0
cuboid 4 1 2p45.1892 2p44.5288 1.27 0.0

global unit 160
com='array of arrays of fuel element sections + reflector'
array 6 -45.1892 -44.5288 0.0
cuboid 5 1 2p45.1892 2p44.5288 97.155 -2.54
cuboid 3 1 2p45.1892 2p44.5288 97.155 -8.89
cuboid 5 1 2p45.1892 2p44.5288 97.155 -13.97
cuboid 3 1 2p45.1892 2p44.5288 97.155 -43.97
end geom

read array
ara=1 nux=23 nuy=22 nuz=1
fill f141 end fill
ara=2 nux=23 nuy=22 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 12 1b11
13 14 15 16 17 18 19 20 21 22 23 24 1b11
25 26 27 28 29 30 31 32 33 34 35 36 1b11
37 38 39 40 41 42 43 44 45 46 47 48 1b11
49 50 51 52 53 54 55 56 57 58 59 60 1b11
61 62 63 64 65 66 67 68 69 70 71 72 1b11
73 74 75 76 77 78 79 80 81 82 83 84 1b11
85 86 87 88 89 90 91 92 93 94 95 96 1b11
97 98 99 100 101 102 103 104 105 106 107 108 1b11
109 110 111 112 113 114 115 116 117 118 119 120 1b11
121 122 123 124 125 126 127 128 129 130 131 132 1b11
1n253
end fill
ara=3 nux=23 nuy=22 nuz=1
fill f143 end fill
ara=4 nux=23 nuy=22 nuz=1
fill f144 end fill
ara=5 nux=23 nuy=22 nuz=1
fill f145 end fill
ara=6 nux=1 nuy=1 nuz=5
fill 151 152 153 154 155 end fill
end array
read plot
ttl='simple plot 1'
lpi=10 scr=yes pic=mix nax=400
xul= -20.0 yul= 0.6 zul= 100
xlr= 20.0 ylr= 0.6 zlr= -10
uax=1.0 wdn=-1.0 end plt0
ttl='simple plot 2'
pic=mix nax=400
xul= -20.0 yul= 20. zul= 25.
xlr= 20.0 ylr= -20. zlr= 25.
uax=1.0 vdn=-1.0 end plt1

end plot
end data
end
=shell
cp ft04f001 $RTNDIR/sax01.xs04
cp ft64f001 $RTNDIR/sax01.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5 parm=size=1000000
saxton 2 fuel
238group latticecell
'MOX fuel
pu-239 1 0 1.3526-3 290 end
pu-240 1 0 1.2759-4 290 end
pu-241 1 0 1.1407-5 290 end

```



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pu-242 1 0 6.0318-7 290 end
am-241 1 0 1.7783-6 290 end
u-234 1 0 1.1688-6 290 end
u-235 1 0 1.5301-4 290 end
u-238 1 0 2.1097-2 290 end
o 1 0 4.5155-2 290 end
'clad (ZR-2)
zr 2 0 4.2517-2 290 end
sn 2 0 4.6590-4 290 end
cr 2 0 7.5977-5 290 end
fe 2 0 1.4148-4 290 end
o 2 0 2.9630-4 290 end
'water(Reflector)
h 3 0 6.6781-2 290 end
o 3 0 3.3390-2 290 end
'b-10 3 0 1.7606-8 290 end
'b-11 3 0 7.1313-8 290 end
'Middle Grid and H2O
al 4 .8458 290 end
h2o 4 .1542 290 end
'Aluminum
al 5 0 6.0039-2 290 end
end comp
squarepitch 1.4224 .856996 1 2 .99314 3 .87503 0 end
more data
limcen=20000000
end more
saxton 2
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
'
unit 1
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 2
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 3
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 4
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 5
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 6
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 7
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 8
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 9
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 10
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 11
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 80.80 0.00
cylinder 0 1 0.437515 80.80 0.00
cylinder 2 1 0.49657 80.80 0.00
cylinder 2 1 0.49657 80.80 -1.27
cuboid 3 1 4p.7112 80.80 -1.27
unit 12
com='Fuel + Gap + Clad + Moderator'

```





cuboid 3 1 4p.7112 80.80 -1.27  
 unit 45  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 46  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 47  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 48  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 49  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 50  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 51  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 52  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27

unit 53  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 54  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 55  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 80.80 0.00  
 cylinder 0 1 0.437515 80.80 0.00  
 cylinder 2 1 0.49657 80.80 0.00  
 cylinder 2 1 0.49657 80.80 -1.27  
 cuboid 3 1 4p.7112 80.80 -1.27  
 unit 71  
 com='Clad + Mod + AL Grid'  
 cylinder 2 1 0.49657 0.635 0.0  
 cylinder 3 1 0.50419 0.635 0.0  
 cuboid 5 1 4p.7112 0.635 0.0  
 unit 73  
 com='Fuel + Gap + Clad + Air'  
 cylinder 1 1 0.428498 12.164 0.0  
 cylinder 0 1 0.437515 12.164 0.0  
 cylinder 2 1 0.49657 12.164 0.0  
 cuboid 0 1 4p.7112 12.164 0.0  
 unit 74  
 com='Top Clad + Void'  
 cylinder 2 1 0.49657 1.016 0.0  
 cuboid 0 1 4p.7112 1.016 0.0  
 unit 75  
 com='Top Clad + Void + AL grid'  
 cylinder 2 1 0.49657 1.27 0.0  
 cylinder 0 1 0.50419 1.27 0.0  
 cuboid 5 1 4p.7112 1.27 0.0  
 unit 81  
 com='array of Clad + Mod + AL Grid + Reflector'  
 array 1 -13.5128 -13.5128 0.0  
 cuboid 4 1 4p43.5128 0.635 0.0  
 unit 82  
 com='array of Fuel + Gap + Clad + Moderator + Reflector'  
 array 2 -13.5128 -13.5128 -1.27  
 cuboid 3 1 4p43.5128 80.80 -1.27  
 unit 83

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com='array of Fuel + Gap + Clad + Air'
  array 3 -13.5128 -13.5128 0.0
  cuboid 0 1 4p43.5128 12.164 0.0
  ,
  unit 84
  com='array of Top Clad + Void'
  array 4 -13.5128 -13.5128 0.0
  cuboid 0 1 4p43.5128 1.016 0.0
  ,
  unit 85
com='array of Top Clad + Void + AL grid'
  array 5 -13.5128 -13.5128 0.0
  cuboid 4 1 4p43.5128 1.27 0.0
  ,
  global unit 100
com='array of arrays of fuel element sections + reflector'
  array 6 -43.5128 -43.5128 0.0
  cuboid 5 1 4p43.5128 97.155 -2.54
  cuboid 3 1 4p43.5128 97.155 -8.89
  cuboid 5 1 4p43.5128 97.155 -13.97
  cuboid 3 1 4p43.5128 97.155 -43.97
  end geom
  ,
  read array
  ara=1 nux=19 nuy=19 nuz=1
  fill f71 end fill
  ara=2 nux=19 nuy=19 nuz=1
  fill
  1 2 3 4 5 6 7 8 9 10 1b9
  2 11 12 13 14 15 16 17 18 19 1b9
  3 12 20 21 22 23 24 25 26 27 1b9
  4 13 21 28 29 30 31 32 33 34 1b9
  5 14 22 29 35 36 37 38 39 40 1b9
  6 15 23 30 36 41 42 43 44 45 1b9
  7 16 24 31 37 42 46 47 48 49 1b9
  8 17 25 32 38 43 47 50 51 52 1b9
  9 18 26 33 39 44 48 51 53 54 1b9
  10 19 27 34 40 45 49 52 54 55 1b180
  end fill
  ara=3 nux=19 nuy=19 nuz=1
  fill f73 end fill
  ara=4 nux=19 nuy=19 nuz=1
  fill f74 end fill
  ara=5 nux=19 nuy=19 nuz=1
  fill f75 end fill
  ara=6 nux=1 nuy=1 nuz=5
  fill 81 82 83 84 85 end fill
  end array
  read plot
  ttl='simple plot 1'
  lpi=10 scr=yes pic=mix nax=400
  xul= -20.0 yul= 0.0 zul= 100
  xlr= 20.0 ylr= 0.0 zlr= -10
  uax=1.0 wdn=-1.0 end plt0
  ttl='simple plot 2'
  pic=mix nax=400
  xul= -20.0 yul= 20. zul= 25.

xlr= 20.0 ylr= -20. zlr= 25.
uax=1.0 vdn=-1.0 end plt1
end plot
end data
end
=shell
cp ft04f001 $RTNDIR/sax02.xs04
cp ft64f001 $RTNDIR/sax02.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5 parm=size=1000000
saxton 3 fuel
238group latticecell
'MOX fuel
pu-239 1 0 1.3526-3 291 end

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pu-240 1 0 1.2759-4 291 end
pu-241 1 0 1.1407-5 291 end
pu-242 1 0 6.0318-7 291 end
am-241 1 0 1.7783-6 291 end
u-234 1 0 1.1688-6 291 end
u-235 1 0 1.5301-4 291 end
u-238 1 0 2.1097-2 291 end
o 1 0 4.5155-2 291 end
'clad (ZR-2)
zr 2 0 4.2517-2 291 end
sn 2 0 4.6590-4 291 end
cr 2 0 7.5977-5 291 end
fe 2 0 1.4148-4 291 end
o 2 0 2.9630-4 291 end
'water(Reflector)
h 3 0 6.6751-2 291 end
o 3 0 3.3404-2 291 end
b-10 3 0 3.7338-6 291 end
b-11 3 0 1.5029-5 291 end
'Middle Grid and H2O
al 4 .8458 291 end
h2o 4 .1542 291 end
'Aluminum
al 5 0 6.0039-2 291 end
end comp
squarepitch 1.4224 .856996 1 2 .99314 3 .87503 0 end
more data
limcen=20000000
end more
saxton 3
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 2
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 3
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 4
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 5
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 6
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 7
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 8
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 9
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 10
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 11
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 12

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unit 61
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 62
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 63
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 64
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 65
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 66
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 88.06 0.00
cylinder 0 1 0.437515 88.06 0.00
cylinder 2 1 0.49657 88.06 0.00
cylinder 2 1 0.49657 88.06 -1.27
cuboid 3 1 4p.7112 88.06 -1.27
unit 71
com='Clad + Mod + AL Grid'
cylinder 2 1 0.49657 0.635 0.0
cylinder 3 1 0.50419 0.635 0.0
cuboid 5 1 4p.7112 0.635 0.0
unit 73
com='Fuel + Gap + Clad + Air'
cylinder 1 1 0.428498 4.904 0.0
cylinder 0 1 0.437515 4.904 0.0
cylinder 2 1 0.49657 4.904 0.0
cuboid 0 1 4p.7112 4.904 0.0
unit 74

```

```

com='Top Clad + Void'
cylinder 2 1 0.49657 1.016 0.0
cuboid 0 1 4p.7112 1.016 0.0
unit 75
com='Top Clad + Void + AL grid'
cylinder 2 1 0.49657 1.27 0.0
cylinder 0 1 0.50419 1.27 0.0
cuboid 5 1 4p.7112 1.27 0.0
unit 81
com='array of Clad + Mod + AL Grid + Reflector'
array 1 -14.9499 -14.9499 0.0
cuboid 4 1 4p44.9499 0.635 0.0
unit 82
com='array of Fuel + Gap + Clad + Moderator + Reflector'
array 2 -14.9499 -14.9499 -1.27
cuboid 3 1 4p44.9499 88.06 -1.27
unit 83
com='array of Fuel + Gap + Clad + Air'
array 3 -14.9499 -14.9499 0.0
cuboid 0 1 4p44.9499 4.904 0.0
unit 84
com='array of Top Clad + Void'
array 4 -14.9499 -14.9499 0.0
cuboid 0 1 4p44.9499 1.016 0.0
unit 85
com='array of Top Clad + Void + AL grid'
array 5 -14.9499 -14.9499 0.0
cuboid 4 1 4p44.9499 1.27 0.0
global unit 100
com='array of arrays of fuel element sections + reflector'
array 6 -44.9499 -44.9499 0.0
cuboid 5 1 4p44.9499 97.155 -2.54
cuboid 3 1 4p44.9499 97.155 -8.89
cuboid 5 1 4p44.9499 97.155 -13.97
cuboid 3 1 4p44.9499 97.155 -43.97
end geom
read array
ara=1 nux=21 nuy=21 nuz=1
fill f71 end fill
ara=2 nux=21 nuy=21 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 1b 10
2 12 13 14 15 16 17 18 19 20 21 1b 10
3 13 22 23 24 25 26 27 28 29 30 1b 10
4 14 23 31 32 33 34 35 36 37 38 1b 10
5 15 24 32 39 40 41 42 43 44 45 1b 10
6 16 25 33 40 46 47 48 49 50 51 1b 10
7 17 26 34 41 47 52 53 54 55 56 1b 10
8 18 27 35 42 48 53 57 58 59 60 1b 10

```

```

9 19 28 36 43 49 54 58 61 62 63 1b 10
10 20 29 37 44 50 55 59 62 64 65 1b 10
11 21 30 38 45 51 56 60 63 65 66 1b 220
    end fill
    ara=3 nux=21 nuy=21 nuz=1
        fill f73 end fill
    ara=4 nux=21 nuy=21 nuz=1
        fill f74 end fill
    ara=5 nux=21 nuy=21 nuz=1
        fill f75 end fill
    ara=6 nux=1 nuy=1 nuz=5
        fill 81 82 83 84 85 end fill
    end array
    read plot
    ttl='simple plot 1'
lpi=10 scr=yes pic=mix nax=400
xul= -20.0 yul= 0.0 zul= 100
xlr= 20.0 ylr= 0.0 zlr= -10
uax=1.0 wdn=-1.0 end plt0
    ttl='simple plot 2'
    pic=mix nax=400
xul= -20.0 yul= 20. zul= 25.
xlr= 20.0 ylr= -20. zlr= 25.
uax=1.0 vdn=-1.0 end plt1
    end plot
    end data
    end
    =shell
cp ft04f001 $RTNDIR/sax03.xs04
cp ft64f001 $RTNDIR/sax03.rs64
    end
    =kmart
    read initial kunit=64
        xunit=4
        actbygrp
        rrpvol
    end initial
    read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
    5010 27
    5011 27
    8016 27
    40000 27
    24000 27
    26000 27
    1001 27
    50112 27
    50114 27
    50115 27
    50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5    parm=size=1000000
           saxton 4 fuel
           238group latticecell
           'MOX fuel
pu-239 1 0 1.3526-3 297 end
pu-240 1 0 1.2759-4 297 end
pu-241 1 0 1.1407-5 297 end
pu-242 1 0 6.0318-7 297 end
am-241 1 0 1.7783-6 297 end
u-234 1 0 1.1688-6 297 end
u-235 1 0 1.5301-4 297 end
u-238 1 0 2.1097-2 297 end
o 1 0 4.5155-2 297 end
   'clad (ZR-2)
zr 2 0 4.2517-2 297 end
sn 2 0 4.6590-4 297 end
cr 2 0 7.5977-5 297 end
fe 2 0 1.4148-4 297 end
o 2 0 2.9630-4 297 end
   'water(Reflector)
h 3 0 6.6673-2 297 end
o 3 0 3.3336-2 297 end
'b-10 3 0 3.7338-6 297 end
'b-11 3 0 1.5029-5 297 end
   'Middle Grid and H2O
al 4 .93 297 end
h2o 4 .07 297 end
   'Aluminum
al 5 0 6.0039-2 297 end
end comp
squarepitch 1.8679 .856996 1 2.99314 3 .87503 0 end
    more data
    limcen=20000000
    end more
    saxton 4
    read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
    res=225
    lng=2000000
    end param

```



unit 17  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 18  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 19  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 20  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 21  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 22  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 23  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 24  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 25

com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 26  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 27  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 28  
 com='Fuel + Gap + Clad + Moderator'  
 cylinder 1 1 0.428498 68.41 0.00  
 cylinder 0 1 0.437515 68.41 0.00  
 cylinder 2 1 0.49657 68.41 0.00  
 cylinder 2 1 0.49657 68.41 -1.27  
 cuboid 3 1 4p.93395 68.41 -1.27

unit 71

com='Clad + Mod + AL Grid'  
 cylinder 2 1 0.49657 0.635 0.0  
 cylinder 3 1 0.50419 0.635 0.0  
 cuboid 5 1 4p.93395 0.635 0.0

unit 73

com='Fuel + Gap + Clad + Air'  
 cylinder 1 1 0.428498 24.554 0.0  
 cylinder 0 1 0.437515 24.554 0.0  
 cylinder 2 1 0.49657 24.554 0.0  
 cuboid 0 1 4p.93395 24.554 0.0

unit 74

com='Top Clad + Void'  
 cylinder 2 1 0.49657 1.016 0.0  
 cuboid 0 1 4p.93395 1.016 0.0

unit 75

com='Top Clad + Void + AL grid'  
 cylinder 2 1 0.49657 1.27 0.0  
 cylinder 0 1 0.50419 1.27 0.0  
 cuboid 5 1 4p.93395 1.27 0.0

unit 81

com='array of Clad + Mod + AL Grid + Reflector'  
 array 1 -12.14135 -12.14135 0.0  
 cuboid 4 1 4p42.14135 0.635 0.0

```

unit 82
com='array of Fuel + Gap + Clad + Moderator + Reflector'
array 2 -12.14135 -12.14135 -1.27
cuboid 3 1 4p42.14135 68.41 -1.27
,
unit 83
com='array of Fuel + Gap + Clad + Air'
array 3 -12.14135 -12.14135 0.0
cuboid 0 1 4p42.14135 24.554 0.0
,
unit 84
com='array of Top Clad + Void'
array 4 -12.14135 -12.14135 0.0
cuboid 0 1 4p42.14135 1.016 0.0
,
unit 85
com='array of Top Clad + Void + AL grid'
array 5 -12.14135 -12.14135 0.0
cuboid 4 1 4p42.14135 1.27 0.0
,
global unit 100
com='array of arrays of fuel element sections + reflector'
array 6 -42.14135 -42.14135 0.0
cuboid 0 1 4p42.14135 97.15501 0.00
cuboid 5 1 4p42.14135 97.15501 -2.54
cuboid 3 1 4p42.14135 97.15501 -8.89
cuboid 5 1 4p42.14135 97.15501 -13.97
cuboid 3 1 4p42.14135 97.15501 -43.97
end geom
,
read array
ara=1 nux=13 nuy=13 nuz=1
fill f71 end fill
ara=2 nux=13 nuy=13 nuz=1
fill
1 2 3 4 5 6 7 1b6
2 8 9 10 11 12 13 1b6
3 9 14 15 16 17 18 1b6
4 10 15 19 20 21 22 1b6
5 11 16 20 23 24 25 1b6
6 12 17 21 24 26 27 1b6
7 13 18 22 25 27 28 1b84
end fill
ara=3 nux=13 nuy=13 nuz=1
fill f73 end fill
ara=4 nux=13 nuy=13 nuz=1
fill f74 end fill
ara=5 nux=13 nuy=13 nuz=1
fill f75 end fill
ara=6 nux=1 nuy=1 nuz=5
fill 81 82 83 84 85 end fill
end array
read plot
ttl='simple plot 1'
lpi=10 scr=yes pic=mix nax=400
xul= -20.0 yul= 0.0 zul= 100
xlr= 20.0 ylr= 0.0 zlr= -10

```

```

uax=1.0 wdn=-1.0 end plt0
ttl='simple plot 2'
pic=mix nax=400
xul= -20.0 yul= 20. zul= 25.
xlr= 20.0 ylr= -20. zlr= 25.
uax=1.0 vdn=-1.0 end plt1
end plot
end data
end
=shell
cp ft04f001 $RTNDIR/sax04.xs04
cp ft64f001 $RTNDIR/sax04.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5 parm=size=1000000

```

```

saxton 5 fuel
238group latticecell
'MOX fuel
pu-239 1 0 1.3526-3 289 end
pu-240 1 0 1.2759-4 289 end
pu-241 1 0 1.1407-5 289 end
pu-242 1 0 6.0318-7 289 end
am-241 1 0 1.7783-6 289 end
u-234 1 0 1.1688-6 289 end
u-235 1 0 1.5301-4 289 end
u-238 1 0 2.1097-2 289 end
o 1 0 4.5155-2 289 end
'clad (ZR-2)
zr 2 0 4.2517-2 289 end
sn 2 0 4.6590-4 298 end
cr 2 0 7.5977-5 289 end
fe 2 0 1.4148-4 289 end
o 2 0 2.9630-4 289 end
'water(Reflector)
h 3 0 6.6783-2 289 end
o 3 0 3.3392-2 289 end
'Middle Grid and H2O
al 4 .942 289 end
h2o 4 .058 289 end
'Aluminum
al 5 0 6.0039-2 289 end
end comp
squarepitch 2.01158 .856996 1 2 .99314 3 .87503 0
end
more data
limcen=20000000
end more
saxton 5
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
'
unit 1
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 2
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 3
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00

```

```

cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 4
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 5
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 6
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 7
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 8
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 9
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 10
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00
cylinder 2 1 0.49657 76.76 0.00
cylinder 2 1 0.49657 76.76 -1.27
cuboid 3 1 4p1.00579 76.76 -1.27
unit 11
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 76.76 0.00
cylinder 0 1 0.437515 76.76 0.00

```

cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 12  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 13  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 14  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 15  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 16  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 17  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 18  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 19  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00

cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 20  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 21  
com='Fuel + Gap + Clad + Moderator'  
cylinder 1 1 0.428498 76.76 0.00  
cylinder 0 1 0.437515 76.76 0.00  
cylinder 2 1 0.49657 76.76 0.00  
cylinder 2 1 0.49657 76.76 -1.27  
cuboid 3 1 4p1.00579 76.76 -1.27  
unit 71  
com='Clad + Mod + AL Grid'  
cylinder 2 1 0.49657 0.635 0.0  
cylinder 3 1 0.50419 0.635 0.0  
cuboid 5 1 4p1.00579 0.635 0.0  
unit 73  
com='Fuel + Gap + Clad + Air'  
cylinder 1 1 0.428498 16.204 0.0  
cylinder 0 1 0.437515 16.204 0.0  
cylinder 2 1 0.49657 16.204 0.0  
cuboid 0 1 4p1.00579 16.204 0.0  
unit 74  
com='Top Clad + Void'  
cylinder 2 1 0.49657 1.016 0.0  
cuboid 0 1 4p1.00579 1.016 0.0  
unit 75  
com='Top Clad + Void + AL grid'  
cylinder 2 1 0.49657 1.27 0.0  
cylinder 0 1 0.50419 1.27 0.0  
cuboid 5 1 4p1.00579 1.27 0.0  
unit 81  
com='array of Clad + Mod + AL Grid + Reflector'  
array 1 -12.06948 -12.06948 0.0  
cuboid 4 1 4p42.06948 0.635 0.0  
unit 82  
com='array of Fuel + Gap + Clad + Moderator + Reflector'  
array 2 -12.06948 -12.06948 -1.27  
cuboid 3 1 4p42.06948 76.76 -1.27  
unit 83  
com='array of Fuel + Gap + Clad + Air'  
array 3 -12.06948 -12.06948 0.0  
cuboid 0 1 4p42.06948 16.204 0.0  
unit 84



```

com='array of Top Clad + Void'
array 4 -12.06948 -12.06948 0.0
cuboid 0 1 4p42.06948 1.016 0.0
    ,
        unit 85
com='array of Top Clad + Void + AL grid'
array 5 -12.06948 -12.06948 0.0
cuboid 4 1 4p42.06948 1.27 0.0
    ,
        global unit 100
com='array of arrays of fuel element sections + reflector'
array 6 -42.06948 -42.06948 0.0
cuboid 5 1 4p42.06948 97.15500 -2.54
cuboid 3 1 4p42.06948 97.15500 -8.89
cuboid 5 1 4p42.06948 97.15500 -13.97
cuboid 3 1 4p42.06948 97.15500 -43.97
    end geom
    ,
        read array
ara=1 nux=12 nuy=12 nuz=1
    fill f71 end fill
ara=2 nux=12 nuy=12 nuz=1
    fill
        1 2 3 4 5 6 n6
        2 7 8 9 10 11 n6
        3 8 12 13 14 15 n6
        4 9 13 16 17 18 n6
        5 10 14 17 19 20 n6
        6 11 15 18 20 21 n6
        n72
    end fill
ara=3 nux=12 nuy=12 nuz=1
    fill f73 end fill
ara=4 nux=12 nuy=12 nuz=1
    fill f74 end fill
ara=5 nux=12 nuy=12 nuz=1
    fill f75 end fill
ara=6 nux=1 nuy=1 nuz=5
    fill 81 82 83 84 85 end fill
    end array
    read plot
    ttl='simple plot 1'
lpi=10 scr=yes pic=mix nax=400
xul= -20.0 yul= 1.006 zul= 100
xlr= 20.0 ylr= 1.006 zlr= -10
uax=1.0 wdn=-1.0 end plt0
    ttl='simple plot 2'
    pic=mix nax=400
xul= -20.0 yul= 20. zul= 25.
xlr= 20.0 ylr= -20. zlr= 25.
uax=1.0 vdn=-1.0 end plt1
    end plot
    end data
    end
    =shell
cp ft04f001 $RTNDIR/sax05.xs04
cp ft64f001 $RTNDIR/sax05.rs64

end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5    parm=size=1000000
saxton 6 fuel
238group latticecell
'MOX fuel
pu-239 1 0 1.3526-3 293 end
pu-240 1 0 1.2759-4 293 end
pu-241 1 0 1.1407-5 293 end
pu-242 1 0 6.0318-7 293 end
am-241 1 0 1.7783-6 293 end
u-234 1 0 1.1688-6 293 end
u-235 1 0 1.5301-4 293 end
u-238 1 0 2.1097-2 293 end
o 1 0 4.5155-2 293 end

```

```

        'clad (ZR-2)
zr  2 0 4.2517-2 293 end
sn  2 0 4.6590-4 293 end
cr  2 0 7.5977-5 293 end
fe  2 0 1.4148-4 293 end
o   2 0 2.9630-4 293 end
        'water(Reflector)
h   3 0 6.6737-2 293 end
o   3 0 3.3368-2 293 end
        'Middle Grid and H2O
al  4 .969      293 end
h2o 4 .031      293 end
        'Aluminum
al  5 0 6.0039-2 293 end
        end comp
squarepitch 2.6416 .856996 1 2 .99314 3 .87503 0 end
        more data
limcen=20000000
        end more
        saxton 6
        read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
        res=225
        lng=2000000
        end param
        read geometry
        ,
        unit 1
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 2
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 3
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 4
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 5
com='Fuel + Gap + Clad + Moderator'

```

```

cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 6
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 7
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 8
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 9
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 10
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 11
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 12
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00
cylinder 0 1 0.437515 79.50 0.00
cylinder 2 1 0.49657 79.50 0.00
cylinder 2 1 0.49657 79.50 -1.27
cuboid 3 1 4p1.3208 79.50 -1.27
        unit 13
com='Fuel + Gap + Clad + Moderator'
cylinder 1 1 0.428498 79.50 0.00

```



```

cuboid 5 1 4p1.3208 0.635 0.0
,
unit 73
com='Fuel + Gap + Clad + Air'
cylinder 1 1 0.428498 13.464 0.0
cylinder 0 1 0.437515 13.464 0.0
cylinder 2 1 0.49657 13.464 0.0
cuboid 0 1 4p1.3208 13.464 0.0
,
unit 74
com='Top Clad + Void'
cylinder 2 1 0.49657 1.016 0.0
cuboid 0 1 4p1.3208 1.016 0.0
,
unit 75
com='Top Clad + Void + AL grid'
cylinder 2 1 0.49657 1.27 0.0
cylinder 0 1 0.50419 1.27 0.0
cuboid 5 1 4p1.3208 1.27 0.0
,
unit 81
com='array of Clad + Mod + AL Grid + Reflector'
array 1 -14.5288 -14.5288 0.0
cuboid 4 1 4p44.5288 0.635 0.0
,
unit 82
com='array of Fuel + Gap + Clad + Moderator + Reflector'
array 2 -14.5288 -14.5288 -1.27
cuboid 3 1 4p44.5288 79.50 -1.27
,
unit 83
com='array of Fuel + Gap + Clad + Air'
array 3 -14.5288 -14.5288 0.0
cuboid 0 1 4p44.5288 13.464 0.0
,
unit 84
com='array of Top Clad + Void'
array 4 -14.5288 -14.5288 0.0
cuboid 0 1 4p44.5288 1.016 0.0
,
unit 85
com='array of Top Clad + Void + AL grid'
array 5 -14.5288 -14.5288 0.0
cuboid 4 1 4p44.5288 1.27 0.0
,
global unit 100
com='array of arrays of fuel element sections + reflector'
array 6 -44.5288 -44.5288 0.0
cuboid 5 1 4p44.5288 97.15500 -2.54
cuboid 3 1 4p44.5288 97.15500 -8.89
cuboid 5 1 4p44.5288 97.15500 -13.97
cuboid 3 1 4p44.5288 97.15500 -43.97
end geom
,
read array
ara=1 nux=11 nuy=11 nuz=1
fill f71 end fill

ara=2 nux=11 nuy=11 nuz=1
fill
1 2 3 4 5 6 1b5
2 7 8 9 10 11 1b5
3 8 12 13 14 15 1b5
4 9 13 16 17 18 1b5
5 10 14 17 19 20 1b5
6 11 15 18 20 21 1b60
end fill
ara=3 nux=11 nuy=11 nuz=1
fill f73 end fill
ara=4 nux=11 nuy=11 nuz=1
fill f74 end fill
ara=5 nux=11 nuy=11 nuz=1
fill f75 end fill
ara=6 nux=1 nuy=1 nuz=5
fill 81 82 83 84 85 end fill
end array
read plot
ttl='simple plot 1'
lpi=10 scr=yes pic=mix nax=400
xul= -20.0 yul= 0.0 zul= 100
xlr= 20.0 ylr= 0.0 zlr= -10
uax=1.0 wdn=-1.0 end plt0
ttl='simple plot 2'
pic=mix nax=400
xul= -20.0 yul= 20. zul= 25.
xlr= 20.0 ylr= -20. zlr= 25.
uax=1.0 vdn=-1.0 end plt1
end plot
end data
end
=shell
cp ft04f001 $RTNDIR/sax06.xs04
cp ft64f001 $RTNDIR/sax06.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27

```

```
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
```



**APPENDIX C**

**SCALE INPUT OF MIX-COMP-THERM-4 PROBLEM SET**





## APPENDIX C

### SCALE INPUT OF MIX-COMP-THERM-4 PROBLEM SET

This appendix contains the CENTRM inputs for the eleven MIX-COMP-THERM-04 cases, TCA01, TCA02, TCA03, TCA04, TCA05, TCA06, TCA07, TCA08, TCA09, TCA10, and TCA11. The inputs can be changed to standard CSAS cases by replacing the =CSASC5 record with =CSAS25.

```

=csasc5      parm=size=1000000
tca          *****case 1 *****
238group latticecell
'MOX fuel
u-234  1 0 7.1749-7 293 end
u-235  1 0 9.3926-5 293 end
u-238  1 0 1.2951-2 293 end
pu-238  1 0 2.0003-6 293 end
pu-239  1 0 2.7491-4 293 end
pu-240  1 0 8.8417-5 293 end
*****      pu-241 varies *****
pu-241  1 0 2.7923-5 293 end
pu-242  1 0 8.1234-6 293 end
*****am-241 varies*****
am-241  1 0 1.3531-6 293 end
o      1 0 2.7837-2 293 end
b-10   1 0 6.0418-8 293 end
b-11   1 0 2.4319-7 293 end
'clad (ZR-2)
zr      2 0 3.7772-2 293 end
sn      2 0 4.3737-4 293 end
cr      2 0 8.8570-5 293 end
fe      2 0 6.6119-5 293 end
o      2 0 3.5864-5 293 end
'water(Reflector)
h      3 0 6.6735-2 293 end
o      3 0 3.3368-2 293 end
'Al
Al      4 0 6.0224-2 293 end
'Stainless Steel
c      5 0 1.1928-4 293 end
si     5 0 1.7003-3 293 end
mn     5 0 1.7385-3 293 end
p      5 0 6.9381-5 293 end
s      5 0 4.4673-5 293 end
ni     5 0 8.9506-3 293 end
cr     5 0 1.7450-2 293 end
fe     5 0 5.7202-2 293 end
'ordinary concrete
h      6 0 1.3742-2 293 end
o      6 0 4.5919-2 293 end
c      6 0 1.1532-4 293 end
na     6 0 9.6395-4 293 end
mg     6 0 1.2388-4 293 end
al     6 0 1.7409-3 293 end
si     6 0 1.6617-2 293 end
k      6 0 4.6052-4 293 end

ca      6 0 1.5025-3 293 end
fe      6 0 3.4492-4 293 end
end comp
squarepitch 1.825 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-1
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 6
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 7
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0

```







```

unit 76
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 77
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 78
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 59.55 0.0
cylinder 2 1 0.6115 59.55 0.0
cuboid 3 1 4p0.9125 59.55 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p.9125 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p.9125 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 11.05 0.0
cylinder 2 1 .6115 11.05 0.0
cuboid 0 1 4p.9125 11.05 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p0.9125 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p50.9875 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -20.9875 -20.9875 0.0
cuboid 0 1 4p50.9875 11.05 0.0
unit 104
com='array of void+Clad+void'
array 4 -20.9875 -20.9875 0.0
cuboid 0 1 4p50.9875 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 59.55 0.0
global unit 110

com='array of arrays of fuel element sections + reflector'
array 6 -50.9875 -50.9875 0
cuboid 4 1 4p50.9875 97.40 -1.27
cuboid 5 1 4p50.9875 97.40 -3.47
cuboid 3 1 4p50.9875 97.40 -17.27
cuboid 5 1 4p50.9875 97.40 -17.77
cuboid 6 1 4p50.9875 97.40 -54.77
end geometry
read array
ara=1 nux=23 nuy=23 nuz=1
fill f81 end fill
ara=2 nux=23 nuy=23 nuz=1
fill f82 end fill
ara=3 nux=23 nuy=23 nuz=1
fill f83 end fill
ara=4 nux=23 nuy=23 nuz=1
fill f84 end fill
ara=5 nux=23 nuy=23 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 12 1b 11
2 13 14 15 16 17 18 19 20 21 22 23 1b 11
3 14 24 25 26 27 28 29 30 31 32 33 1b 11
4 15 25 34 35 36 37 38 39 40 41 42 1b 11
5 16 26 35 43 44 45 46 47 48 49 50 1b 11
6 17 27 36 44 51 52 53 54 55 56 57 1b 11
7 18 28 37 45 52 58 59 60 61 62 63 1b 11
8 19 29 38 46 53 59 64 65 66 67 68 1b 11
9 20 30 39 47 54 60 65 69 70 71 72 1b 11
10 21 31 40 48 55 61 66 70 73 74 75 1b 11
11 22 32 41 49 56 62 67 71 74 76 77 1b 11
12 23 33 42 50 57 63 68 72 75 77 78 1b 264
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp ft04f001 $RTNDR/tca01.xs04
cp ft64f001 $RTNDR/tca01.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452

```

```

5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=size=1000000
tca          *****case 2 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.6701-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 2.5812-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end

'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 1.825 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-2
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0

```









```

cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 75
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 76
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 77
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 78
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.90 0.0
cylinder 2 1 0.6115 61.90 0.0
cuboid 3 1 4p0.9125 61.90 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p.9125 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p.9125 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 8.7 0.0
cylinder 2 1 .6115 8.7 0.0
cuboid 0 1 4p.9125 8.7 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p0.9125 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p50.9875 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -20.9875 -20.9875 0.0
cuboid 0 1 4p50.9875 8.7 0.0
unit 104

com='array of void+Clad+void'
array 4 -20.9875 -20.9875 0.0
cuboid 0 1 4p50.9875 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 61.90 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -50.9875 -50.9875 0.0
cuboid 4 1 4p50.9875 97.40 -1.27
cuboid 5 1 4p50.9875 97.40 -3.47
cuboid 3 1 4p50.9875 97.40 -17.27
cuboid 5 1 4p50.9875 97.40 -17.77
cuboid 6 1 4p50.9875 97.40 -54.77
end geometry
read array
ara=1 nux=23 nuy=23 nuz=1
fill f81 end fill
ara=2 nux=23 nuy=23 nuz=1
fill f82 end fill
ara=3 nux=23 nuy=23 nuz=1
fill f83 end fill
ara=4 nux=23 nuy=23 nuz=1
fill f84 end fill
ara=5 nux=23 nuy=23 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 12 1b 11
2 13 14 15 16 17 18 19 20 21 22 23 1b 11
3 14 24 25 26 27 28 29 30 31 32 33 1b 11
4 15 25 34 35 36 37 38 39 40 41 42 1b 11
5 16 26 35 43 44 45 46 47 48 49 50 1b 11
6 17 27 36 44 51 52 53 54 55 56 57 1b 11
7 18 28 37 45 52 58 59 60 61 62 63 1b 11
8 19 29 38 46 53 59 64 65 66 67 68 1b 11
9 20 30 39 47 54 60 65 69 70 71 72 1b 11
10 21 31 40 48 55 61 66 70 73 74 75 1b 11
11 22 32 41 49 56 62 67 71 74 76 77 1b 11
12 23 33 42 50 57 63 68 72 75 77 78 1b 264
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp ft04f001 $RTNDR/tca02.xs04
cp ft64f001 $RTNDR/tca02.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452

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92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=size=1000000
tca          *****case 3 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.5447-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 3.8361-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end

cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 1.825 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-3
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 4
com='(Fuel+Clad+H2O)'

```







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cuboid 3 1 4p0.9125 64.06 0.0
unit 73
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 74
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 75
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 76
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 77
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 78
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.06 0.0
cylinder 2 1 0.6115 64.06 0.0
cuboid 3 1 4p0.9125 64.06 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p.9125 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p.9125 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 6.54 0.0
cylinder 2 1 .6115 6.54 0.0
cuboid 0 1 4p.9125 6.54 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p0.9125 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p50.9875 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 4.445 0.0
unit 102

com='array of h2o and end plugs above Al grid plate '
array 2 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -20.9875 -20.9875 0.0
cuboid 0 1 4p50.9875 6.54 0.0
unit 104
com='array of void+Clad+void'
array 4 -20.9875 -20.9875 0.0
cuboid 0 1 4p50.9875 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -20.9875 -20.9875 0.0
cuboid 3 1 4p50.9875 64.06 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -50.9875 -50.9875 0.0
cuboid 4 1 4p50.9875 97.40 -1.27
cuboid 5 1 4p50.9875 97.40 -3.47
cuboid 3 1 4p50.9875 97.40 -17.27
cuboid 5 1 4p50.9875 97.40 -17.77
cuboid 6 1 4p50.9875 97.40 -54.77
end geometry
read array
ara=1 nux=23 nuy=23 nuz=1
fill f81 end fill
ara=2 nux=23 nuy=23 nuz=1
fill f82 end fill
ara=3 nux=23 nuy=23 nuz=1
fill f83 end fill
ara=4 nux=23 nuy=23 nuz=1
fill f84 end fill
ara=5 nux=23 nuy=23 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 12 1b 11
2 13 14 15 16 17 18 19 20 21 22 23 1b 11
3 14 24 25 26 27 28 29 30 31 32 33 1b 11
4 15 25 34 35 36 37 38 39 40 41 42 1b 11
5 16 26 35 43 44 45 46 47 48 49 50 1b 11
6 17 27 36 44 51 52 53 54 55 56 57 1b 11
7 18 28 37 45 52 58 59 60 61 62 63 1b 11
8 19 29 38 46 53 59 64 65 66 67 68 1b 11
9 20 30 39 47 54 60 65 69 70 71 72 1b 11
10 21 31 40 48 55 61 66 70 73 74 75 1b 11
11 22 32 41 49 56 62 67 71 74 76 77 1b 11
12 23 33 42 50 57 63 68 72 75 77 78 1b 264
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp fit04f001 $RTNDIR/tca03.xs04
cp fit64f001 $RTNDIR/tca03.rs64
end

```

```

=kmart
read initial kunit=64
      xunit=4
      actbygrp
      rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=size=1000000
tca          *****case 4 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.8003-5 293 end
pu-242 1 0 8.1234-6 293 end

*****am-241 varies*****
am-241 1 0 1.2793-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 1.956 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-4
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0

```







```

cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 49
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 50
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 51
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 52
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 53
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 54
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 55
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 56
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 57
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 58
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 59
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 60
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 61
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 62
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 63
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 64
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 65
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 66
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 61.50 0.0
cylinder 2 1 0.6115 61.50 0.0
cuboid 3 1 4p0.978 61.50 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p.978 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p.978 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 9.1 0.0
cylinder 2 1 .6115 9.1 0.0
cuboid 0 1 4p.978 9.1 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p0.978 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p50.538 .601 0.0

```

```

unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -20.538 -20.538 0.0
cuboid 3 1 4p50.538 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 -20.538 -20.538 0.0
cuboid 3 1 4p50.538 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -20.538 -20.538 0.0
cuboid 0 1 4p50.538 9.1 0.0
unit 104
com='array of void+Clad+void'
array 4 -20.538 -20.538 0.0
cuboid 0 1 4p50.538 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -20.538 -20.538 0.0
cuboid 3 1 4p50.538 61.50 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -50.538 -50.538 0.0
cuboid 4 1 4p50.538 97.40 -1.27
cuboid 5 1 4p50.538 97.40 -3.47
cuboid 3 1 4p50.538 97.40 -17.27
cuboid 5 1 4p50.538 97.40 -17.77
cuboid 6 1 4p50.538 97.40 -54.77
end geometry
read array
ara=1 nux=21 nuy=21 nuz=1
fill f81 end fill
ara=2 nux=21 nuy=21 nuz=1
fill f82 end fill
ara=3 nux=21 nuy=21 nuz=1
fill f83 end fill
ara=4 nux=21 nuy=21 nuz=1
fill f84 end fill
ara=5 nux=21 nuy=21 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 1b 10
2 12 13 14 15 16 17 18 19 20 21 1b 10
3 13 22 23 24 25 26 27 28 29 30 1b 10
4 14 23 31 32 33 34 35 36 37 38 1b 10
5 15 24 32 39 40 41 42 43 44 45 1b 10
6 16 25 33 40 46 47 48 49 50 51 1b 10
7 17 26 34 41 47 52 53 54 55 56 1b 10
8 18 27 35 42 48 53 57 58 59 60 1b 10
9 19 28 36 43 49 54 58 61 62 63 1b 10
10 20 29 37 44 50 55 59 62 64 65 1b 10
11 21 30 38 45 51 56 60 63 65 66 1b 220
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end

```

```

=shell
cp ft04f001 $RTNDIR/tca04.xs04
cp ft64f001 $RTNDIR/tca04.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5 parm=size=1000000
tca *****case 5 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end

```

```

pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.6670-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 2.6129-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 1.956 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-5
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0

```

```

unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 6
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 7
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 8
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 9
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 10
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 11
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 12
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 13
com='(Fuel+Clad+H2O)'

```





```

unit 59
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 60
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 61
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 62
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 63
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 64
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 65
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 66
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.40 0.0
cylinder 2 1 0.6115 64.40 0.0
cuboid 3 1 4p0.978 64.40 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p.978 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p.978 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 6.2 0.0
cylinder 2 1 .6115 6.2 0.0
cuboid 0 1 4p.978 6.2 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p0.978 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p50.538 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 0 0 0
cuboid 3 1 4p50.538 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 0 0 0
cuboid 3 1 4p50.538 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 0 0 0
cuboid 0 1 4p50.538 6.2 0.0
unit 104
com='array of void+Clad+void'
array 4 0 0 0
cuboid 0 1 4p50.538 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 0 0 0
cuboid 3 1 4p50.538 64.40 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -50.538 -50.538 0
cuboid 4 1 4p50.538 97.40 -1.27
cuboid 5 1 4p50.538 97.40 -3.47
cuboid 3 1 4p50.538 97.40 -17.27
cuboid 5 1 4p50.538 97.40 -17.77
cuboid 6 1 4p50.538 97.40 -54.77
end geometry
read array
ara=1 nux=21 nuy=21 nuz=1
fill f81 end fill
ara=2 nux=21 nuy=21 nuz=1
fill f82 end fill
ara=3 nux=21 nuy=21 nuz=1
fill f83 end fill
ara=4 nux=21 nuy=21 nuz=1
fill f84 end fill
ara=5 nux=21 nuy=21 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 1b 10
2 12 13 14 15 16 17 18 19 20 21 1b 10
3 13 22 23 24 25 26 27 28 29 30 1b 10
4 14 23 31 32 33 34 35 36 37 38 1b 10
5 15 24 32 39 40 41 42 43 44 45 1b 10
6 16 25 33 40 46 47 48 49 50 51 1b 10
7 17 26 34 41 47 52 53 54 55 56 1b 10
8 18 27 35 42 48 53 57 58 59 60 1b 10
9 19 28 36 43 49 54 58 61 62 63 1b 10
10 20 29 37 44 50 55 59 62 64 65 1b 10
11 21 30 38 45 51 56 60 63 65 66 1b 220
end fill
ara=6 nux=1 nuy=1 nuz=6

```



```

fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp ft04f001 $RTNDIR/tca05.xs04
cp ft64f001 $RTNDIR/tca05.rs64
end
=kmart
read initial kunit=64
      xunit=4
      actbygrp
      rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5      parm=size=1000000
tca          *****case 6 *****
238group latticecell
'MOX fuel

```

```

u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.4228-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 5.0543-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 1.956 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-6
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry

```





```

cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 47
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 48
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 49
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 50
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 51
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 52
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 53
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 54
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 55
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 56
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 57
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 58
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 59
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 60
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 61
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 62
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 63
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 64
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 65
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 66
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 69.40 0.0
cylinder 2 1 0.6115 69.40 0.0
cuboid 3 1 4p0.978 69.40 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p.978 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p.978 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 1.2 0.0

```

```

cylinder 2 1 .6115 1.2 0.0
cuboid 0 1 4p.978 1.2 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p0.978 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p50.538 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 0 0 0
cuboid 3 1 4p50.538 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 0 0 0
cuboid 3 1 4p50.538 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 0 0 0
cuboid 0 1 4p50.538 1.2 0.0
unit 104
com='array of void+Clad+void'
array 4 0 0 0
cuboid 0 1 4p50.538 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 0 0 0
cuboid 3 1 4p50.538 69.40 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -50.538 -50.538 0
cuboid 4 1 4p50.538 97.40 -1.27
cuboid 5 1 4p50.538 97.40 -3.47
cuboid 3 1 4p50.538 97.40 -17.27
cuboid 5 1 4p50.538 97.40 -17.77
cuboid 6 1 4p50.538 97.40 -54.77
end geometry
read array
ara=1 nux=21 nuy=21 nuz=1
fill f81 end fill
ara=2 nux=21 nuy=21 nuz=1
fill f82 end fill
ara=3 nux=21 nuy=21 nuz=1
fill f83 end fill
ara=4 nux=21 nuy=21 nuz=1
fill f84 end fill
ara=5 nux=21 nuy=21 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 1b 10
2 12 13 14 15 16 17 18 19 20 21 1b 10
3 13 22 23 24 25 26 27 28 29 30 1b 10
4 14 23 31 32 33 34 35 36 37 38 1b 10
5 15 24 32 39 40 41 42 43 44 45 1b 10
6 16 25 33 40 46 47 48 49 50 51 1b 10
7 17 26 34 41 47 52 53 54 55 56 1b 10
8 18 27 35 42 48 53 57 58 59 60 1b 10
9 19 28 36 43 49 54 58 61 62 63 1b 10
10 20 29 37 44 50 55 59 62 64 65 1b 10
11 21 30 38 45 51 56 60 63 65 66 1b 220
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp ft04f001 $RTNDIR/tca06.xs04
cp ft64f001 $RTNDIR/tca06.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

```

```

=csasc5      parm=size=1000000
tca          *****case 7 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.8133-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 1.1498-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 2.225 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-7
read param

```

```

gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 6
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 7
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 8
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 9
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 10
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 60.32 0.0
cylinder 2 1 0.6115 60.32 0.0
cuboid 3 1 4p1.1125 60.32 0.0
unit 11
com='(Fuel+Clad+H2O)'

```







```

com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p1.1125 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 10.28 0.0
cylinder 2 1 .6115 10.28 0.0
cuboid 0 1 4p1.1125 10.28 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p1.1125 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p52.25 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -22.25 -22.25 0.0
cuboid 0 1 4p52.25 10.28 0.0
unit 104
com='array of void+Clad+void'
array 4 -22.25 -22.25 0.0
cuboid 0 1 4p52.25 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 60.32 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -52.25 -52.25 0.0
cuboid 4 1 4p52.25 97.40 -1.27
cuboid 5 1 4p52.25 97.40 -3.47
cuboid 3 1 4p52.25 97.40 -17.27
cuboid 5 1 4p52.25 97.40 -17.77
cuboid 6 1 4p52.25 97.40 -54.77
end geometry
read array
ara=1 nux=20 nuy=20 nuz=1
fill f81 end fill
ara=2 nux=20 nuy=20 nuz=1
fill f82 end fill
ara=3 nux=20 nuy=20 nuz=1
fill f83 end fill
ara=4 nux=20 nuy=20 nuz=1
fill f84 end fill
ara=5 nux=20 nuy=20 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 n 10
2 11 12 13 14 15 16 17 18 19 n 10
3 12 20 21 22 23 24 25 26 27 n 10
4 13 21 28 29 30 31 32 33 34 n 10
5 14 22 29 35 36 37 38 39 40 n 10
6 15 23 30 36 41 42 43 44 45 n 10
7 16 24 31 37 42 46 47 48 49 n 10
8 17 25 32 38 43 47 50 51 52 n 10
9 18 26 33 39 44 48 51 53 54 n 10
10 19 27 34 40 45 49 52 54 55 n 10
n200
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp ft04f001 $RTNDIR/tca07.xs04
cp ft64f001 $RTNDIR/tca07.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57

```

```

lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=size=1000000
TCA          *****case 8 *****
238group latticecell
'MOX fuel
u-234  1 0 7.1749-7 293 end
u-235  1 0 9.3926-5 293 end
u-238  1 0 1.2951-2 293 end
pu-238  1 0 2.0003-6 293 end
pu-239  1 0 2.7491-4 293 end
pu-240  1 0 8.8417-5 293 end
*****      pu-241 varies *****
pu-241  1 0 2.6649-5 293 end
pu-242  1 0 8.1234-6 293 end
*****      am-241 varies *****
am-241  1 0 2.6340-6 293 end
o  1 0 2.7837-2 293 end
b-10  1 0 6.0418-8 293 end
b-11  1 0 2.4319-7 293 end
'clad (ZR-2)
zr  2 0 3.7772-2 293 end
sn  2 0 4.3737-4 293 end
cr  2 0 8.8570-5 293 end
fe  2 0 6.6119-5 293 end
o  2 0 3.5864-5 293 end
'water(Reflector)
h  3 0 6.6735-2 293 end
o  3 0 3.3368-2 293 end
'Al
Al  4 0 6.0224-2 293 end
'Stainless Steel
c  5 0 1.1928-4 293 end
si  5 0 1.7003-3 293 end
mn  5 0 1.7385-3 293 end
p  5 0 6.9381-5 293 end
s  5 0 4.4673-5 293 end
ni  5 0 8.9506-3 293 end
cr  5 0 1.7450-2 293 end
fe  5 0 5.7202-2 293 end
'ordinary concrete
h  6 0 1.3742-2 293 end
o  6 0 4.5919-2 293 end
c  6 0 1.1532-4 293 end
na  6 0 9.6395-4 293 end
mg  6 0 1.2388-4 293 end
al  6 0 1.7409-3 293 end
si  6 0 1.6617-2 293 end
k  6 0 4.6052-4 293 end
ca  6 0 1.5025-3 293 end
fe  6 0 3.4492-4 293 end
end comp

squarepitch 2.225  1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-8
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 6
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 7
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 8
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 9
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.99 0.0
cylinder 2 1 0.6115 62.99 0.0
cuboid 3 1 4p1.1125 62.99 0.0
unit 10

```





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cuboid 3 1 4p1.1125 62.99 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p1.1125 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p1.1125 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 7.61 0.0
cylinder 2 1 .6115 7.61 0.0
cuboid 0 1 4p1.1125 7.61 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p1.1125 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p52.25 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate'
array 2 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -22.25 -22.25 0.0
cuboid 0 1 4p52.25 7.61 0.0
unit 104
com='array of void+Clad+void'
array 4 -22.25 -22.25 0.0
cuboid 0 1 4p52.25 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 62.99 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -52.25 -52.25 0.0
cuboid 4 1 4p52.25 97.40 -1.27
cuboid 5 1 4p52.25 97.40 -3.47
cuboid 3 1 4p52.25 97.40 -17.27
cuboid 5 1 4p52.25 97.40 -17.77
cuboid 6 1 4p52.25 97.40 -54.77
end geometry
read array
ara=1 nux=20 nuy=20 nuz=1
fill f81 end fill
ara=2 nux=20 nuy=20 nuz=1
fill f82 end fill
ara=3 nux=20 nuy=20 nuz=1

```

```

fill f83 end fill
ara=4 nux=20 nuy=20 nuz=1
fill f84 end fill
ara=5 nux=20 nuy=20 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 n 10
2 11 12 13 14 15 16 17 18 19 n 10
3 12 20 21 22 23 24 25 26 27 n 10
4 13 21 28 29 30 31 32 33 34 n 10
5 14 22 29 35 36 37 38 39 40 n 10
6 15 23 30 36 41 42 43 44 45 n 10
7 16 24 31 37 42 46 47 48 49 n 10
8 17 25 32 38 43 47 50 51 52 n 10
9 18 26 33 39 44 48 51 53 54 n 10
10 19 27 34 40 45 49 52 54 55 n 10
n200
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp fit04f001 $RTNDIR/tca08.xs04
cp fit64f001 $RTNDIR/tca08.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27

```

```

50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=size=1000000
TCA          *****case 9 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.5373-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 3.9098-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end

al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 2.225 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-9
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 6
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 7
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 8
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0

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cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 55
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 65.63 0.0
cylinder 2 1 0.6115 65.63 0.0
cuboid 3 1 4p1.1125 65.63 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p1.1125 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p1.1125 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 4.97 0.0
cylinder 2 1 .6115 4.97 0.0
cuboid 0 1 4p1.1125 4.97 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p1.1125 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p52.25 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -22.25 -22.25 0.0
cuboid 0 1 4p52.25 4.97 0.0
unit 104
com='array of void+Clad+void'
array 4 -22.25 -22.25 0.0
cuboid 0 1 4p52.25 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -22.25 -22.25 0.0
cuboid 3 1 4p52.25 65.63 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -52.25 -52.25 0.0
cuboid 4 1 4p52.25 97.40 -1.27
cuboid 5 1 4p52.25 97.40 -3.47
cuboid 3 1 4p52.25 97.40 -17.27
cuboid 5 1 4p52.25 97.40 -17.77
cuboid 6 1 4p52.25 97.40 -54.77
end geometry

```

```

read array
ara=1 nux=20 nuy=20 nuz=1
fill f81 end fill
ara=2 nux=20 nuy=20 nuz=1
fill f82 end fill
ara=3 nux=20 nuy=20 nuz=1
fill f83 end fill
ara=4 nux=20 nuy=20 nuz=1
fill f84 end fill
ara=5 nux=20 nuy=20 nuz=1
fill
  1 2 3 4 5 6 7 8 9 10 n 10
  2 11 12 13 14 15 16 17 18 19 n 10
  3 12 20 21 22 23 24 25 26 27 n 10
  4 13 21 28 29 30 31 32 33 34 n 10
  5 14 22 29 35 36 37 38 39 40 n 10
  6 15 23 30 36 41 42 43 44 45 n 10
  7 16 24 31 37 42 46 47 48 49 n 10
  8 17 25 32 38 43 47 50 51 52 n 10
  9 18 26 33 39 44 48 51 53 54 n 10
  10 19 27 34 40 45 49 52 54 55 n 10
n200
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp fit04f001 $RTNDIR/tca09.xs04
cp fit64f001 $RTNDIR/tca09.rs64
end
=kmart
read initial kunit=64
      xunit=4
      actbygrp
      rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27
26000 27
1001 27
50112 27
50114 27

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```

50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end

=csasc5      parm=size=1000000
TCA          *****case 10 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.8077-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 1.2053-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end
s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end

'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 2.474 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-10
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 6
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 7
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0

```





```

cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 54
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 55
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 56
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 57
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 58
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 59
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 60
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 61
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 62
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 63
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 64
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 65
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 66
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 62.05 0.0
cylinder 2 1 0.6115 62.05 0.0
cuboid 3 1 4p1.237 62.05 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p1.237 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p1.237 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 8.55 0.0
cylinder 2 1 .6115 8.55 0.0
cuboid 0 1 4p1.237 8.55 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p1.237 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p55.977 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -25.977 -25.977 0.0
cuboid 3 1 4p55.977 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 -25.977 -25.977 0.0
cuboid 3 1 4p55.977 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -25.977 -25.977 0.0
cuboid 0 1 4p55.977 8.55 0.0
unit 104
com='array of void+Clad+void'
array 4 -25.977 -25.977 0.0
cuboid 0 1 4p55.977 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -25.977 -25.977 0.0
cuboid 3 1 4p55.977 62.05 0.0
global unit 110
com='array of arrays of fuel element sections + reflector'
array 6 -55.977 -55.977 0.0
cuboid 4 1 4p55.977 97.40 -1.27
cuboid 5 1 4p55.977 97.40 -3.47

```

```

cuboid 3 1 4p55.977 97.40 -17.27
cuboid 5 1 4p55.977 97.40 -17.77
cuboid 6 1 4p55.977 97.40 -54.77
end geometry
read array
ara=1 nux=21 nuy=21 nuz=1
fill f81 end fill
ara=2 nux=21 nuy=21 nuz=1
fill f82 end fill
ara=3 nux=21 nuy=21 nuz=1
fill f83 end fill
ara=4 nux=21 nuy=21 nuz=1
fill f84 end fill
ara=5 nux=21 nuy=21 nuz=1
fill
  1 2 3 4 5 6 7 8 9 10 11 1b 10
  2 12 13 14 15 16 17 18 19 20 21 1b 10
  3 13 22 23 24 25 26 27 28 29 30 1b 10
  4 14 23 31 32 33 34 35 36 37 38 1b 10
  5 15 24 32 39 40 41 42 43 44 45 1b 10
  6 16 25 33 40 46 47 48 49 50 51 1b 10
  7 17 26 34 41 47 52 53 54 55 56 1b 10
  8 18 27 35 42 48 53 57 58 59 60 1b 10
  9 19 28 36 43 49 54 58 61 62 63 1b 10
  10 20 29 37 44 50 55 59 62 64 65 1b 10
  11 21 30 38 45 51 56 60 63 65 66 1b 220
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp ft04f001 $RTNDIR/tca10.xs04
cp ft64f001 $RTNDIR/tca10.rs64
end
=kmart
read initial kunit=64
      xunit=4
      actbygrp
      rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27
5011 27
8016 27
40000 27
24000 27

```

```

26000 27
1001 27
50112 27
50114 27
50115 27
50116 27
50117 27
50118 27
50119 27
50120 27
50122 27
50124 27
end activity
read collapse
factor=1.0
lastg=57
lastg=148
lastg=204
lastg=238
end collapse
end
=csasc5      parm=size=1000000
TCA          *****case 11 *****
238group latticecell
'MOX fuel
u-234 1 0 7.1749-7 293 end
u-235 1 0 9.3926-5 293 end
u-238 1 0 1.2951-2 293 end
pu-238 1 0 2.0003-6 293 end
pu-239 1 0 2.7491-4 293 end
pu-240 1 0 8.8417-5 293 end
***** pu-241 varies *****
pu-241 1 0 2.6617-5 293 end
pu-242 1 0 8.1234-6 293 end
*****am-241 varies*****
am-241 1 0 2.6656-6 293 end
o 1 0 2.7837-2 293 end
b-10 1 0 6.0418-8 293 end
b-11 1 0 2.4319-7 293 end
'clad (ZR-2)
zr 2 0 3.7772-2 293 end
sn 2 0 4.3737-4 293 end
cr 2 0 8.8570-5 293 end
fe 2 0 6.6119-5 293 end
o 2 0 3.5864-5 293 end
'water(Reflector)
h 3 0 6.6735-2 293 end
o 3 0 3.3368-2 293 end
'Al
Al 4 0 6.0224-2 293 end
'Stainless Steel
c 5 0 1.1928-4 293 end
si 5 0 1.7003-3 293 end
mn 5 0 1.7385-3 293 end
p 5 0 6.9381-5 293 end

```

```

s 5 0 4.4673-5 293 end
ni 5 0 8.9506-3 293 end
cr 5 0 1.7450-2 293 end
fe 5 0 5.7202-2 293 end
'ordinary concrete
h 6 0 1.3742-2 293 end
o 6 0 4.5919-2 293 end
c 6 0 1.1532-4 293 end
na 6 0 9.6395-4 293 end
mg 6 0 1.2388-4 293 end
al 6 0 1.7409-3 293 end
si 6 0 1.6617-2 293 end
k 6 0 4.6052-4 293 end
ca 6 0 1.5025-3 293 end
fe 6 0 3.4492-4 293 end
end comp
squarepitch 2.474 1.065 1 2 1.223 3 end
more data
limcen=17000000
end more
tca-11
read param
gen=225 nsk=25 npg=20000 fdn=yes flx=yes wrs=64
res=225
lng=2000000
end param
read geometry
unit 1
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 2
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 3
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 4
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 5
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 6
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0

```

```

unit 7
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 8
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 9
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 10
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 11
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 12
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 13
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 14
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 15
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 16
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 17
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 18
com='(Fuel+Clad+H2O)'

```







```

unit 64
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 65
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 66
com='(Fuel+Clad+H2O)'
cylinder 1 1 0.5325 64.53 0.0
cylinder 2 1 0.6115 64.53 0.0
cuboid 3 1 4p1.237 64.53 0.0
unit 81
com='h2o and end plug below Al grid plate - fill array 1'
cylinder 4 1 0.6115 4.445 0.0
cuboid 3 1 4p1.237 4.445 0.0
unit 82
com='h2o and end plug above Al grid plate - fill array 2'
cylinder 4 1 0.6115 11.784 0.0
cuboid 3 1 4p1.237 11.784 0.0
unit 83
com='(Fuel+Clad+Void) - fill array 3'
cylinder 1 1 .5325 6.07 0.0
cylinder 2 1 .6115 6.07 0.0
cuboid 0 1 4p1.237 6.07 0.0
unit 84
com='(void+Clad+void)'
cylinder 0 1 0.5325 9.97 0.0
cylinder 2 1 0.6115 9.97 0.0
cuboid 0 1 4p1.237 9.97 0.0
unit 100
com='Lower Al grid plate'
cuboid 4 1 4p55.977 .601 0.0
unit 101
com='array of h2o and end plugs below Al grid plate'
array 1 -25.977 -25.977 0.0
cuboid 3 1 4p55.977 4.445 0.0
unit 102
com='array of h2o and end plugs above Al grid plate '
array 2 -25.977 -25.977 0.0
cuboid 3 1 4p55.977 11.784 0.0
unit 103
com='array of Fuel+Clad+Void'
array 3 -25.977 -25.977 0.0
cuboid 0 1 4p55.977 6.07 0.0
unit 104
com='array of void+Clad+void'
array 4 -25.977 -25.977 0.0
cuboid 0 1 4p55.977 9.97 0.0
unit 105
com='array of Fuel+Clad+H2O'
array 5 -25.977 -25.977 0.0
cuboid 3 1 4p55.977 64.53 0.0
global unit 110

com='array of arrays of fuel element sections + reflector'
array 6 -55.977 -55.977 0.0
cuboid 4 1 4p55.977 97.40 -1.27
cuboid 5 1 4p55.977 97.40 -3.47
cuboid 3 1 4p55.977 97.40 -17.27
cuboid 5 1 4p55.977 97.40 -17.77
cuboid 6 1 4p55.977 97.40 -54.77
end geometry
read array
ara=1 nux=21 nuy=21 nuz=1
fill f81 end fill
ara=2 nux=21 nuy=21 nuz=1
fill f82 end fill
ara=3 nux=21 nuy=21 nuz=1
fill f83 end fill
ara=4 nux=21 nuy=21 nuz=1
fill f84 end fill
ara=5 nux=21 nuy=21 nuz=1
fill
1 2 3 4 5 6 7 8 9 10 11 1b 10
2 12 13 14 15 16 17 18 19 20 21 1b 10
3 13 22 23 24 25 26 27 28 29 30 1b 10
4 14 23 31 32 33 34 35 36 37 38 1b 10
5 15 24 32 39 40 41 42 43 44 45 1b 10
6 16 25 33 40 46 47 48 49 50 51 1b 10
7 17 26 34 41 47 52 53 54 55 56 1b 10
8 18 27 35 42 48 53 57 58 59 60 1b 10
9 19 28 36 43 49 54 58 61 62 63 1b 10
10 20 29 37 44 50 55 59 62 64 65 1b 10
11 21 30 38 45 51 56 60 63 65 66 1b 220
end fill
ara=6 nux=1 nuy=1 nuz=6
fill 101 100 102 105 103 104 end fill
end array
end data
end
=shell
cp ft04f001 $RTNDR/tca11.xs04
cp ft64f001 $RTNDR/tca11.rs64
end
=kmart
read initial kunit=64
xunit=4
actbygrp
rrpvol
end initial
read activity
92234 27 92234 18 92234 1452
92235 27 92235 18 92235 1452
92238 27 92238 18 92238 1452
94238 27 94238 18 94238 1452
94239 27 94239 18 94239 1452
94240 27 94240 18 94240 1452
94241 27 94241 18 94241 1452
94242 27 94242 18 94242 1452
95241 27 95241 18 95241 1452
5010 27

```

5011 27  
8016 27  
40000 27  
24000 27  
26000 27  
1001 27  
50112 27  
50114 27  
50115 27  
50116 27  
50117 27  
50118 27  
50119 27  
50120 27  
50122 27  
50124 27  
end activity  
read collapse  
factor=1.0  
lastg=57  
lastg=148  
lastg=204  
lastg=238  
end collapse  
end



**APPENDIX D**  
**SCALE INPUT OF VARIANTS PROBLEM SET**



## APPENDIX D SCALE INPUT OF VARIANTS PROBLEM SET

This appendix contains the CENTRM inputs for the forty variant/state computational benchmark cases. There are 8 variant groups: V1, V2, V3, V4, V7, V8, V9, and V10. In each variant group there are 5 states: S1, S3, S4, S5, and S6. Each combination of variant and state represents a case. The inputs can be changed to standard CSAS cases by replacing the =CSASC5 record with =CSAS25. The inputs for the cases are listed below.

```
=csasc1x   parm=size=1000000
FMDP V10 S1 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S3 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S4 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S5 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 579 end
u-238 1 0 2.2100-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S6 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S7 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S8 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S9 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V10 S10 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 1027 end
u-238 1 0 2.2100-2 1027 end
o-16 1 0 4.63-2 1027 end
pu-238 1 0 3.0-5 1027 end
pu-239 1 0 1.1600-3 1027 end
pu-240 1 0 4.9-4 1027 end
pu-241 1 0 1.9-4 1027 end
pu-242 1 0 1.05-4 1027 end
am-241 1 0 2.5-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end
```

```

o-16 1 0 4.63-2 579 end
pu-238 1 0 3.0-5 579 end
pu-239 1 0 1.1600-3 579 end
pu-240 1 0 4.9-4 579 end
pu-241 1 0 1.9-4 579 end
pu-242 1 0 1.05-4 579 end
am-241 1 0 2.5-5 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V10 S6 pin-cell case---
238group latticecell
u-235 1 0 5.0-5 300 end
u-238 1 0 2.2100-2 300 end
o-16 1 0 4.63-2 300 end
pu-238 1 0 3.0-5 300 end
pu-239 1 0 1.1600-3 300 end
pu-240 1 0 4.9-4 300 end
pu-241 1 0 1.9-4 300 end
pu-242 1 0 1.05-4 300 end
am-241 1 0 2.5-5 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end
b-11 3 0 2.6839-5 300 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V1 S1 pin-cell case---
238group latticecell
u-235 1 0 8.7370-4 1027 end

```

```

u-238 1 0 1.8744-2 1027 end
o-16 1 0 3.9235-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
iim=40 icm=50
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V1 S3 pin-cell case---
238group latticecell
u-235 1 0 8.7370-4 1027 end
u-238 1 0 1.8744-2 1027 end
o-16 1 0 3.9235-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
'b-10 3 0 4.7344-6 579 end
'b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V1 S4 pin-cell case---
238group latticecell
u-235 1 0 8.7370-4 1027 end
u-238 1 0 1.8744-2 1027 end
o-16 1 0 3.9235-2 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data

```



```

ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V1 S5 pin-cell case---
238group latticecell
u-235 1 0 8.7370-4 579 end
u-238 1 0 1.8744-2 579 end
o-16 1 0 3.9235-2 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V1 S6 pin-cell case---
238group latticecell
u-235 1 0 8.7370-4 300 end
u-238 1 0 1.8744-2 300 end
o-16 1 0 3.9235-2 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end
b-11 3 0 2.6839-5 300 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=8000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V2 S1 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-239 1 0 6.5875-4 1027 end
pu-240 1 0 4.2323-5 1027 end
pu-241 1 0 7.0246-6 1027 end
o-16 1 0 3.9235-2 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end

ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V2 S3 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-239 1 0 6.5875-4 1027 end
pu-240 1 0 4.2323-5 1027 end
pu-241 1 0 7.0246-6 1027 end
o-16 1 0 3.9235-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
'b-10 3 0 4.7344-6 579 end
'b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V2 S4 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-239 1 0 6.5875-4 1027 end
pu-240 1 0 4.2323-5 1027 end
pu-241 1 0 7.0246-6 1027 end
o-16 1 0 3.9235-2 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end

```

```

zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=17000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V2 S5 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 579 end
u-238 1 0 1.8917-2 579 end
pu-239 1 0 6.5875-4 579 end
pu-240 1 0 4.2323-5 579 end
pu-241 1 0 7.0246-6 579 end
o-16 1 0 3.9235-2 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=17000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V2 S6 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 300 end
u-238 1 0 1.8917-2 300 end
pu-239 1 0 6.5875-4 300 end
pu-240 1 0 4.2323-5 300 end
pu-241 1 0 7.0246-6 300 end
o-16 1 0 3.9235-2 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end
b-11 3 0 2.6839-5 300 end

```

```

end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=17000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V3 S1 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 1027 end
u-236 1 0 8.6365-5 1027 end
u-238 1 0 1.8327-2 1027 end
np-237 1 0 2.4823-5 1027 end
pu-238 1 0 6.7254-6 1027 end
'np-239 1 0 1.8332-6 1027 end
pu-239 1 0 1.3111-4 1027 end
pu-240 1 0 3.6233-5 1027 end
pu-241 1 0 2.1701-5 1027 end
pu-242 1 0 4.7576-6 1027 end
am-241 1 0 4.949-7 1027 end
am-242m 1 0 7.9194-9 1027 end
am-243 1 0 6.6925-7 1027 end
cm-242 1 0 1.2582-7 1027 end
cm-243 1 0 2.0629-9 1027 end
cm-244 1 0 1.2387-7 1027 end
o-16 1 0 3.9235-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V3 S3 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 1027 end
u-236 1 0 8.6365-5 1027 end
u-238 1 0 1.8327-2 1027 end
np-237 1 0 2.4823-5 1027 end
pu-238 1 0 6.7254-6 1027 end
'np-239 1 0 1.8332-6 1027 end
pu-239 1 0 1.3111-4 1027 end

```

```

pu-240 1 0 3.6233-5 1027 end
pu-241 1 0 2.1701-5 1027 end
pu-242 1 0 4.7576-6 1027 end
am-241 1 0 4.949-7 1027 end
am-242m 1 0 7.9194-9 1027 end
am-243 1 0 6.6925-7 1027 end
cm-242 1 0 1.2582-7 1027 end
cm-243 1 0 2.0629-9 1027 end
cm-244 1 0 1.2387-7 1027 end
o-16 1 0 3.9235-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
'b-10 3 0 4.7344-6 579 end
'b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V3 S4 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 1027 end
u-236 1 0 8.6365-5 1027 end
u-238 1 0 1.8327-2 1027 end
np-237 1 0 2.4823-5 1027 end
pu-238 1 0 6.7254-6 1027 end
'np-239 1 0 1.8332-6 1027 end
pu-239 1 0 1.3111-4 1027 end
pu-240 1 0 3.6233-5 1027 end
pu-241 1 0 2.1701-5 1027 end
pu-242 1 0 4.7576-6 1027 end
am-241 1 0 4.949-7 1027 end
am-242m 1 0 7.9194-9 1027 end
am-243 1 0 6.6925-7 1027 end
cm-242 1 0 1.2582-7 1027 end
cm-243 1 0 2.0629-9 1027 end
cm-244 1 0 1.2387-7 1027 end
o-16 1 0 3.9235-2 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data

```

```

limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V3 S5 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 579 end
u-236 1 0 8.6365-5 579 end
u-238 1 0 1.8327-2 579 end
np-237 1 0 2.4823-5 579 end
pu-238 1 0 6.7254-6 579 end
'np-239 1 0 1.8332-6 579 end
pu-239 1 0 1.3111-4 579 end
pu-240 1 0 3.6233-5 579 end
pu-241 1 0 2.1701-5 579 end
pu-242 1 0 4.7576-6 579 end
am-241 1 0 4.949-7 579 end
am-242m 1 0 7.9194-9 579 end
am-243 1 0 6.6925-7 579 end
cm-242 1 0 1.2582-7 579 end
cm-243 1 0 2.0629-9 579 end
cm-244 1 0 1.2387-7 579 end
o-16 1 0 3.9235-2 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V3 S6 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 300 end
u-236 1 0 8.6365-5 300 end
u-238 1 0 1.8327-2 300 end
np-237 1 0 2.4823-5 300 end
pu-238 1 0 6.7254-6 300 end
'np-239 1 0 1.8332-6 300 end
pu-239 1 0 1.3111-4 300 end
pu-240 1 0 3.6233-5 300 end
pu-241 1 0 2.1701-5 300 end
pu-242 1 0 4.7576-6 300 end

```

```

am-241 1 0 4.949-7 300 end
am-242m 1 0 7.9194-9 300 end
am-243 1 0 6.6925-7 300 end
cm-242 1 0 1.2582-7 300 end
cm-243 1 0 2.0629-9 300 end
cm-244 1 0 1.2387-7 300 end
o-16 1 0 3.9235-2 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end
b-11 3 0 2.6839-5 300 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V4 S1 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 1027 end
u-236 1 0 8.6365-5 1027 end
u-238 1 0 1.8327-2 1027 end
np-237 1 0 2.4823-5 1027 end
pu-238 1 0 6.7254-6 1027 end
'np-239 1 0 1.8332-6 1027 end
pu-239 1 0 1.3111-4 1027 end
pu-240 1 0 3.6233-5 1027 end
pu-241 1 0 2.1701-5 1027 end
rh-103 1 0 1.8890-5 1027 end
xe-131 1 0 1.4255-5 1027 end
nd-143 1 0 2.6692-5 1027 end
pm-147 1 0 6.1574-6 1027 end
cs-133 1 0 3.5974-5 1027 end
tc-99 1 0 3.3320-5 1027 end
sm-152 1 0 2.6842-6 1027 end
sm-151 1 0 3.0757-7 1027 end
pu-242 1 0 4.7576-6 1027 end
am-241 1 0 4.9491-7 1027 end
am-242m 1 0 7.9194-9 1027 end
am-243 1 0 6.6925-7 1027 end
cm-242 1 0 1.2582-7 1027 end
cm-243 1 0 2.0629-9 1027 end
cm-244 1 0 1.2387-7 1027 end
o-16 1 0 3.9235-2 1027 end
nd-145 1 0 1.9975-5 1027 end
eu-153 1 0 2.4801-6 1027 end
ag-109 1 0 2.2037-6 1027 end
eu-155 1 0 9.6857-8 1027 end
mo-95 1 0 3.3720-5 1027 end

```

```

eu-154 1 0 5.1189-7 1027 end
ru-101 1 0 3.1134-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=20000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V4 S3 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 1027 end
u-236 1 0 8.6365-5 1027 end
u-238 1 0 1.8327-2 1027 end
np-237 1 0 2.4823-5 1027 end
pu-238 1 0 6.7254-6 1027 end
'np-239 1 0 1.8332-6 1027 end
pu-239 1 0 1.3111-4 1027 end
pu-240 1 0 3.6233-5 1027 end
pu-241 1 0 2.1701-5 1027 end
rh-103 1 0 1.8890-5 1027 end
xe-131 1 0 1.4255-5 1027 end
nd-143 1 0 2.6692-5 1027 end
pm-147 1 0 6.1574-6 1027 end
cs-133 1 0 3.5974-5 1027 end
tc-99 1 0 3.3320-5 1027 end
sm-152 1 0 2.6842-6 1027 end
sm-151 1 0 3.0757-7 1027 end
pu-242 1 0 4.7576-6 1027 end
am-241 1 0 4.9491-7 1027 end
am-242m 1 0 7.9194-9 1027 end
am-243 1 0 6.6925-7 1027 end
cm-242 1 0 1.2582-7 1027 end
cm-243 1 0 2.0629-9 1027 end
cm-244 1 0 1.2387-7 1027 end
o-16 1 0 3.9235-2 1027 end
nd-145 1 0 1.9975-5 1027 end
eu-153 1 0 2.4801-6 1027 end
ag-109 1 0 2.2037-6 1027 end
eu-155 1 0 9.6857-8 1027 end
mo-95 1 0 3.3720-5 1027 end
eu-154 1 0 5.1189-7 1027 end
ru-101 1 0 3.1134-5 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end

```

```

h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
'b-10 3 0 4.7344-6 579 end
'b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=20000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x   parm=size=1000000
FMDP V4 S4 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 1027 end
u-236 1 0 8.6365-5 1027 end
u-238 1 0 1.8327-2 1027 end
np-237 1 0 2.4823-5 1027 end
pu-238 1 0 6.7254-6 1027 end
'np-239 1 0 1.8332-6 1027 end
pu-239 1 0 1.3111-4 1027 end
pu-240 1 0 3.6233-5 1027 end
pu-241 1 0 2.1701-5 1027 end
rh-103 1 0 1.8890-5 1027 end
xe-131 1 0 1.4255-5 1027 end
nd-143 1 0 2.6692-5 1027 end
pm-147 1 0 6.1574-6 1027 end
cs-133 1 0 3.5974-5 1027 end
tc-99 1 0 3.3320-5 1027 end
sm-152 1 0 2.6842-6 1027 end
sm-151 1 0 3.0757-7 1027 end
pu-242 1 0 4.7576-6 1027 end
am-241 1 0 4.9491-7 1027 end
am-242m 1 0 7.9194-9 1027 end
am-243 1 0 6.6925-7 1027 end
cm-242 1 0 1.2582-7 1027 end
cm-243 1 0 2.0629-9 1027 end
cm-244 1 0 1.2387-7 1027 end
o-16 1 0 3.9235-2 1027 end
nd-145 1 0 1.9975-5 1027 end
eu-153 1 0 2.4801-6 1027 end
ag-109 1 0 2.2037-6 1027 end
eu-155 1 0 9.6857-8 1027 end
mo-95 1 0 3.3720-5 1027 end
eu-154 1 0 5.1189-7 1027 end
ru-101 1 0 3.1134-5 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp

```

```

triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=20000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x   parm=size=1000000
FMDP V4 S5 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 579 end
u-236 1 0 8.6365-5 579 end
u-238 1 0 1.8327-2 579 end
np-237 1 0 2.4823-5 579 end
pu-238 1 0 6.7254-6 579 end
'np-239 1 0 1.8332-6 579 end
pu-239 1 0 1.3111-4 579 end
pu-240 1 0 3.6233-5 579 end
pu-241 1 0 2.1701-5 579 end
rh-103 1 0 1.8890-5 579 end
xe-131 1 0 1.4255-5 579 end
nd-143 1 0 2.6692-5 579 end
pm-147 1 0 6.1574-6 579 end
cs-133 1 0 3.5974-5 579 end
tc-99 1 0 3.3320-5 579 end
sm-152 1 0 2.6842-6 579 end
sm-151 1 0 3.0757-7 579 end
pu-242 1 0 4.7576-6 579 end
am-241 1 0 4.9491-7 579 end
am-242m 1 0 7.9194-9 579 end
am-243 1 0 6.6925-7 579 end
cm-242 1 0 1.2582-7 579 end
cm-243 1 0 2.0629-9 579 end
cm-244 1 0 1.2387-7 579 end
o-16 1 0 3.9235-2 579 end
nd-145 1 0 1.9975-5 579 end
eu-153 1 0 2.4801-6 579 end
ag-109 1 0 2.2037-6 579 end
eu-155 1 0 9.6857-8 579 end
mo-95 1 0 3.3720-5 579 end
eu-154 1 0 5.1189-7 579 end
ru-101 1 0 3.1134-5 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=20000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001

```

```

end more
end data
end

=csasc1x   parm=size=1000000
FMDP V4 S6 pin-cell case---
238group latticecell
u-235 1 0 3.7843-4 300 end
u-236 1 0 8.6365-5 300 end
u-238 1 0 1.8327-2 300 end
np-237 1 0 2.4823-5 300 end
pu-238 1 0 6.7254-6 300 end
'np-239 1 0 1.8332-6 300 end
pu-239 1 0 1.3111-4 300 end
pu-240 1 0 3.6233-5 300 end
pu-241 1 0 2.1701-5 300 end
rh-103 1 0 1.8890-5 300 end
xe-131 1 0 1.4255-5 300 end
nd-143 1 0 2.6692-5 300 end
pm-147 1 0 6.1574-6 300 end
cs-133 1 0 3.5974-5 300 end
tc-99 1 0 3.3320-5 300 end
sm-152 1 0 2.6842-6 300 end
sm-151 1 0 3.0757-7 300 end
pu-242 1 0 4.7576-6 300 end
am-241 1 0 4.9491-7 300 end
am-242m 1 0 7.9194-9 300 end
am-243 1 0 6.6925-7 300 end
cm-242 1 0 1.2582-7 300 end
cm-243 1 0 2.0629-9 300 end
cm-244 1 0 1.2387-7 300 end
o-16 1 0 3.9235-2 300 end
nd-145 1 0 1.9975-5 300 end
eu-153 1 0 2.4801-6 300 end
ag-109 1 0 2.2037-6 300 end
eu-155 1 0 9.6857-8 300 end
mo-95 1 0 3.3720-5 300 end
eu-154 1 0 5.1189-7 300 end
ru-101 1 0 3.1134-5 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end
b-11 3 0 2.6839-5 300 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=20000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000

```

```

FMDP V4 S6 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-239 1 0 6.5875-4 1027 end
o-16 1 0 4.1707-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x   parm=size=1000000
FMDP V7 S3 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-239 1 0 6.5875-4 1027 end
o-16 1 0 4.1707-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
'b-10 3 0 4.7344-6 579 end
'b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x   parm=size=1000000
FMDP V7 S4 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-239 1 0 6.5875-4 1027 end
o-16 1 0 4.1707-2 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end

```

```

h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V7 S5 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 579 end
u-238 1 0 1.8917-2 579 end
pu-239 1 0 6.5875-4 579 end
o-16 1 0 4.1707-2 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V7 S6 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 300 end
u-238 1 0 1.8917-2 300 end
pu-239 1 0 6.5875-4 300 end
o-16 1 0 4.1707-2 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end
b-11 3 0 2.6839-5 300 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=16000000
ixtr3=3

```

```

szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V8 S1 pin-cell case---
238group latticecell
u-235 1 0 6.9714-4 1027 end
u-238 1 0 1.8917-2 1027 end
pu-240 1 0 4.2323-5 1027 end
o-16 1 0 4.1707-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V8 S3 pin-cell case---
238group latticecell
u-235 1 0 6.9714-4 1027 end
u-238 1 0 1.8917-2 1027 end
pu-240 1 0 4.2323-5 1027 end
o-16 1 0 4.1707-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
'b-10 3 0 4.7344-6 579 end
'b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V8 S4 pin-cell case---
238group latticecell
u-235 1 0 6.9714-4 1027 end

```

```

u-238 1 0 1.8917-2 1027 end
pu-240 1 0 4.2323-5 1027 end
o-16 1 0 4.1707-2 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V8 S5 pin-cell case---
238group latticecell
u-235 1 0 6.9714-4 579 end
u-238 1 0 1.8917-2 579 end
pu-240 1 0 4.2323-5 579 end
o-16 1 0 4.1707-2 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V8 S6 pin-cell case---
238group latticecell
u-235 1 0 6.9714-4 300 end
u-238 1 0 1.8917-2 300 end
pu-240 1 0 4.2323-5 300 end
o-16 1 0 4.1707-2 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end

```

```

b-11 3 0 2.6839-5 300 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V9 S1 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-241 1 0 6.6577-4 1027 end
o-16 1 0 4.1707-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```

```

=csasc1x parm=size=1000000
FMDP V9 S3 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-241 1 0 6.6577-4 1027 end
o-16 1 0 4.1707-2 1027 end
xe-135 1 0 9.4581-9 1027 end
sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
'b-10 3 0 4.7344-6 579 end
'b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data

```



```

end

=csasc1x   parm=size=1000000
FMDP V9 S5 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 1027 end
u-238 1 0 1.8917-2 1027 end
pu-241 1 0 6.6577-4 1027 end
o-16 1 0 4.1707-2 1027 end
'xe-135 1 0 9.4581-9 1027 end
'sm-149 1 0 7.3667-8 1027 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V9 S6 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 579 end
u-238 1 0 1.8917-2 579 end
pu-241 1 0 6.6577-4 579 end
o-16 1 0 4.1707-2 579 end
'xe-135 1 0 9.4581-9 579 end
'sm-149 1 0 7.3667-8 579 end
zr 2 0 4.23-2 579 end
h 3 0 4.783-2 579 end
o-16 3 0 2.391-2 579 end
b-10 3 0 4.7344-6 579 end
b-11 3 0 1.9177-5 579 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

=csasc1x   parm=size=1000000
FMDP V9 S6 pin-cell case---
238group latticecell
u-235 1 0 3.8393-5 300 end
u-238 1 0 1.8917-2 300 end
pu-241 1 0 6.6577-4 300 end
o-16 1 0 4.1707-2 300 end
'xe-135 1 0 9.4581-9 300 end
'sm-149 1 0 7.3667-8 300 end
zr 2 0 4.23-2 300 end
h 3 0 6.694-2 300 end
o-16 3 0 3.347-2 300 end
b-10 3 0 6.6262-6 300 end
b-11 3 0 2.6839-5 300 end
end comp
triangpitch 1.27500 0.772 1 3 0.9164 2 end
more data
limcen=12000000
ixtr3=3
szf=.75 isn=16 eps=.00001 ptc=.00001
end more
end data
end

```



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