

**Hydraulic Design of Improved Inlets for Culverts
using
Programable Calculators**

MONROE

Compucorp - 325 Scientist

Calculator Design Series #1

October 1980

**U. S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION**

FEDERAL HIGHWAY ADMINISTRATION

Hydraulic Design Publications

The first hydraulic design publications were developed in the early 1960's to aid in the design of highway drainage structures. Since that time, the list of publications has expanded as research results and actual experience became available. Some material is preliminary or tentative, subject to change upon further research. Criticisms and suggestions on material contained in the publications are welcomed.

The publications listed below are available for purchase at the listed prices from the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402. Payment should accompany orders to the Government Printing Office. Stock numbers should be used in ordering the publications.

THIS IS NOT AN ORDER FORM FOR THE GOVERNMENT PRINTING OFFICE (GPO)

Hydraulic Design Series

HDS No. 1 HYDRAULICS OF BRIDGE WATERWAYS - Second Edition - Revised 1978 - \$3.00 (Stock No. 050-001-00133-1)

Hydraulic Engineering Circulars

HEC No. 5 HYDRAULIC CHARTS FOR THE SELECTION OF HIGHWAY CULVERTS - December 1965 - 95 cents (Stock No. 050-002-00010-1)

HEC No. 12 DRAINAGE OF HIGHWAY PAVEMENTS - March 1969 - \$1.55 (Stock No. 050-002-00043-8)

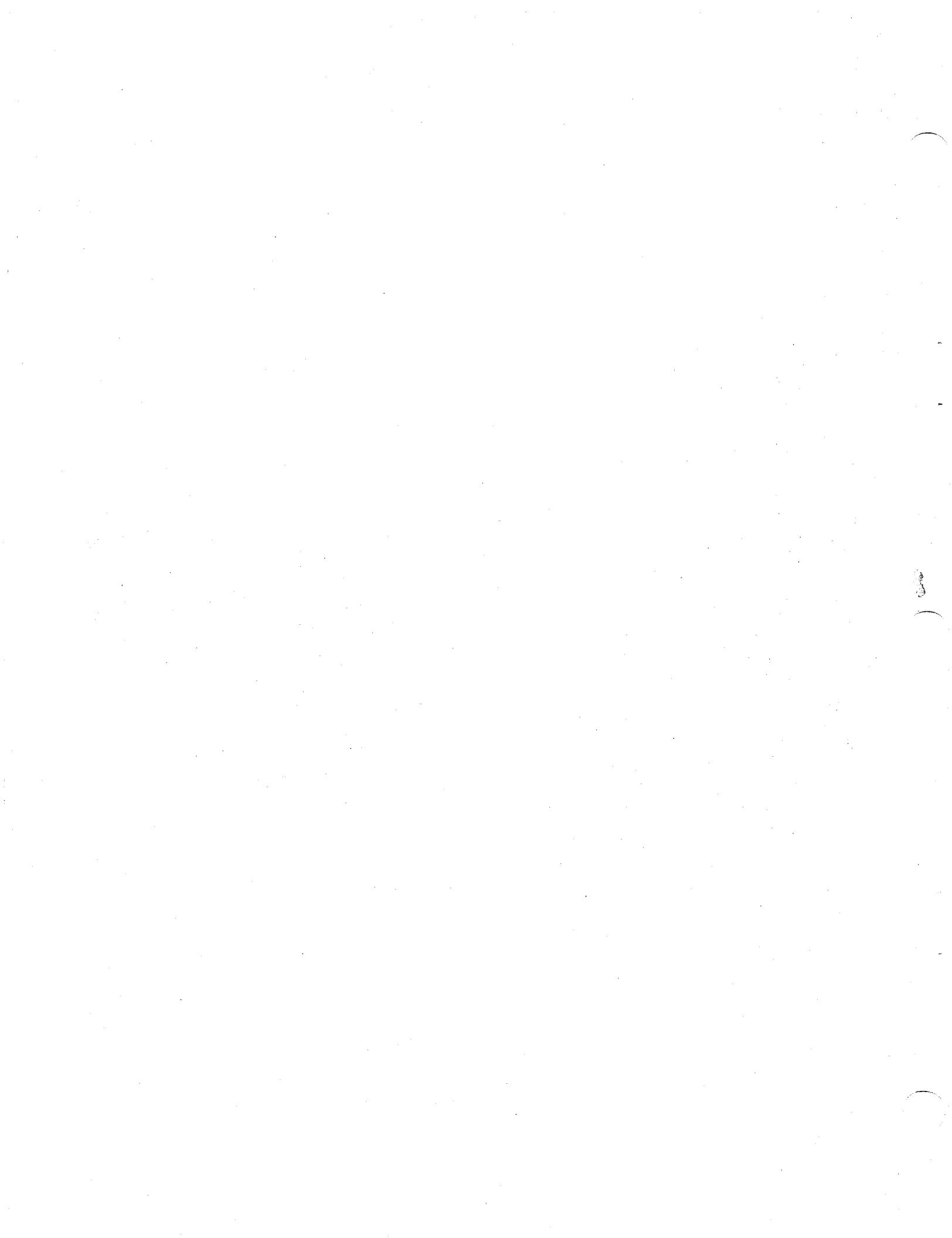
HEC No. 14 HYDRAULIC DESIGN OF ENERGY DISSIPATORS FOR CULVERTS AND CHANNELS - December 1975 - \$4.70 (Stock No. 050-002-00102-7)

HEC No. 15 DESIGN OF STABLE CHANNELS WITH FLEXIBLE LININGS - October 1975 - \$2.75 (Stock No. 050-002-00101-9)

(Continued on inside of back cover)

TABLE OF CONTENTS

	<u>Page</u>
List of Programs.	1
List of Symbols	iii
Introduction.	1
Program Limitations	2
Procedural Outline for Box Culverts	3
Procedural Outline for Pipe Culverts.	12
Example Problems.	21
Equations and Flow Charts Used in Programs.	58
References.	75
Worksheets for Culvert Design	76
Program Listings	83



LIST OF PROGRAMS

For Culvert Design
Using the COMPUCORP 325
(file 2 starts at 38")

File	Block	Description
1	1	Calculates channel tailwater.
1	2	Determines an acceptable box size by calculating H_W_0 .
1	3	Calculates outlet control performance curve data for box culverts.
1	4	Calculates outlet velocity for box culverts in outlet control.
1	5	Calculates the performance of a square-edged inlet with headwalls on a box culvert.
1	6	Calculates the performance of a 45° beveled inlet on a box culvert.
1	7	Calculates the performance of the throat section of a tapered inlet in a box culvert.
1	8	Calculates B_f and L_1 for a side-tapered inlet on a box culvert with favorable face edge conditions. (See Step 7 for definition of favorable conditions).
1	9	Calculates B_f and L_1 for a side-tapered inlet on a box culvert with unfavorable face edge conditions. (See Step 7 for definition of unfavorable conditions).
1	10	Calculates B_f for slope-tapered inlets on culverts with favorable face edge conditions and either a vertical or mitered face.
1	11	Calculates R_f for slope-tapered inlets on culverts with unfavorable face edge conditions and either a vertical or mitered face.
1	12	Calculates L_1 , L_2 , L_3 , L_4 and Taper for a slope-tapered inlet on culverts with either a vertical or mitered face.
1	13	Checks crest control for either a side- or slope-tapered inlet.
1	14	Calculates outlet velocity for box culverts in inlet control.

File Block

- | | | |
|---|----|---|
| 2 | 1 | Determines an acceptable pipe size by computing HW_0 . |
| 2 | 2 | Calculates outlet control performance curve data for pipe culverts. |
| 2 | 3 | Calculates outlet velocity for pipe culverts in outlet control. |
| 2 | 4 | Calculates performance of a thin-edged projecting inlet on a pipe culvert. |
| 2 | 5 | Calculates performance of an inlet with square edges on a pipe culvert. |
| 2 | 6 | Calculates performance of an inlet with 45° bevels on a pipe culvert. |
| 2 | 7 | Calculates the performance of a groove end projecting inlet on a pipe culvert. |
| 2 | 8 | Calculates the performance of a groove end inlet with headwalls on a pipe culvert. |
| 2 | 9 | Calculates performance of a tapered inlet throat in a smooth pipe culvert. |
| 2 | 10 | Calculates the performance of a tapered inlet throat in a rough pipe culvert. |
| 2 | 11 | Calculates B_f and L_1 for a side-tapered inlet on a pipe culvert if the face has projecting thin edges. |
| 2 | 12 | Calculates B_f and L_1 for a side-tapered inlet on a pipe culvert if the face has square edges in a headwall. |
| 2 | 13 | Calculates B_f and L_1 for a side-tapered inlet on a pipe culvert if the face has 45° bevels or a grooved end. |
| 2 | 14 | Calculates outlet velocity for circular pipes in inlet control. |

LIST OF SYMBOLS

<u>Symbol</u>	<u>Units</u>	<u>Description</u>
A	ft. ²	Area of flow in the culvert barrel
Alpha		Energy coefficient used obtain true velocity head
B	ft.	Width of the culvert barrel
BW	ft.	Width of channel bottom
b	ft.	Dimension of side bevel in plane of face
B _f	ft.	Width of face sections of tapered inlets
D	ft.	Height of box culvert or diameter of pipe culvert
d	ft.	Dimension of top bevel in plane of face
d _c	ft.	Critical depth of flow
d _n	ft.	Normal depth of flow in a uniform channel for steady flow
DHW El.	ft.	Design headwater elevation at the culvert entrance
Depth	ft.	A term to indicate the use of either d _n , d _c , TW or D in the calculation of outlet velocity
E	ft.	Height of side-tapered pipe culvert face section, excluding bevel dimension
FALL	ft.	Approximate depression of control section below the stream crossing
H _c	ft.	Depth of pool, or head, above the crest
HW	ft.	Headwater elevation, subscript indicates control section
HW _f	ft.	Headwater elevation required for flow to pass face section in face control
HW _o	ft.	Headwater elevation required for flow to pass face in outlet control
HW _t	ft.	Headwater elevation required for flow to pass throat section in throat control

<u>Symbol</u>	<u>Units</u>	<u>Description</u>
k_e		Entrance energy loss coefficient
L_a	ft.	Approximate total length of culvert, including inlet
L_1, L_2, L_3, L_4	ft.	Dimensions relating to tapered inlets (see sketches in Step 9)
N		Number of barrels
n		Manning roughness coefficient
Q	cu.ft/sec.	Volume rate of flow
R	ft.	Hydraulic radius
S	ft/ft	Slope of culvert barrel
S_f	ft/ft	Slope of FALL for slope-tapered inlets, length : drop
S_o	ft/ft	Slope of natural channel
Taper	ft/ft	Sidewall flare angle, length : offset
TW	ft.	Tailwater depth at outlet of culvert referenced to outlet invert elevation
W	ft.	Width of weir crest for slope-tapered inlet with mitered face, or total weir length for a depressed entrance
X		a factor defined as $\left(\frac{AR^{2/3}}{B^{8/3}}\right)$ or $\left(\frac{AR^{2/3}}{D^{8/3}}\right)$ and used by Chow in determining normal depth
y	ft.	Difference in elevation between crest and face section of a slope-tapered inlet with mitered face
Z_1, Z_2	ft/ft	Horizontal distances per foot of depth for side slopes of channels, cotangent of side slopes

INTRODUCTION

The programmable calculator as a culvert designing tool offers many desirable features. Compared with the hand method, the calculator is more accurate, less time consuming, and eliminates all the searching through charts and nomographs. In one quarter of the time it takes to design one culvert by hand, the designer could use the calculator to design the culvert, checking four or five different sizes to find the best one, while also evaluating several inlet configurations including both side- and slope-tapered inlets.

In an office where it is not feasible to use a computer for culvert design, the programmable calculator becomes a desireable alternative. The accuracy remains the same, and the calculator method offers a segment by segment design approach. This method allows the culvert design parameters to be changed as the design is proceeding along.

The procedure herein covers both box and circular pipe culverts and follows the culvert design methods presented in "Hydraulic Design of Improved Inlets for Culverts," Hydraulic Engineering Circular No. 13 (HEC 13), dated August 1972. The programs begin with the computation of tailwater, proceed through the design of the culvert barrel, and conclude with the design of the culvert inlet most applicable to the site. The programs produce detailed inlet dimensions, performance curve data, and the outlet velocity.

Since the procedure is subdivided into a series of programs, the designer may enter the sequence at any point, provided the necessary input data is available, and obtain the desired design results.

These box and pipe culvert programs have been written for use on the MONROE (formerly Compucorp) - 325 Scientist. It is expected that with the equations, examples, and program listings, a designer will be able to write similar programs for any other calculator he may have available.

Terminology used in this publication assumes that the designer is familiar with HEC 13 and understands the principles and design philosophy expressed therein.

This document was written by Messrs. Patrick D. Wlaschin, Mark M. Chatfield, Albert H. Lowe, and Romeo G. Magalong and was edited by Mr. Philip L. Thompson.

PROGRAM LIMITATIONS

In addition to improved inlets, which include bevel-edged, side-tapered and slope-tapered designs, this procedure includes programs for square-edged entrances for box culverts or thin-edged projecting, square-edged, or groove-edged entrances for circular pipe culverts.

When computing headwater, the upper and lower limits of HW/D for thin-edged projecting, square-edged, groove-edged and beveled inlets should be governed by the limitations of HEC No. 13. Because of the polynomial best-fit equations used, the headwater for improved inlets should be limited to not more than 4.5D or not less than 0.5D.

When designing either a side-tapered or slope-tapered inlet, the number of barrels, N, is limited to two.

Calculations of outlet velocity for box culverts is limited to a maximum D/B of 2.

In programs for circular pipe where d_n/D is greater than 0.89 the program assumes the pipe to be flowing full in calculating velocity.

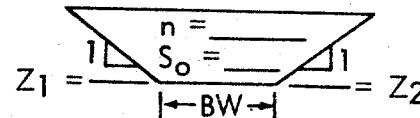
When calculating H in the outlet control performance programs 1-2, 1-3, 2-1, and 2-2, it is assumed that the culvert is flowing full.

PROCEDURAL OUTLINE
FOR BOX CULVERTS

STEP 1

Determine TW elevation from Q and channel geometry if TW is based on normal depth in the natural channel.

Use program #1-1



Enter: n - Manning roughness coefficient for the natural stream

S_o - Slope of natural channel

BW - Width of streambed bottom

Z_1 - Horizontal distance for side slope of channel

Z_2 - Horizontal distance for side slope of channel

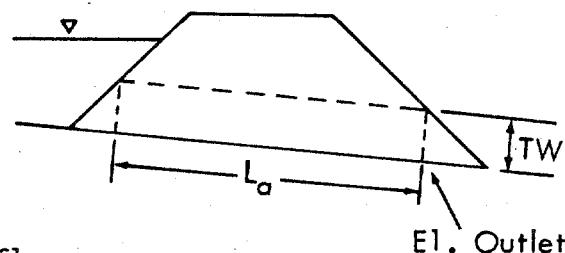
Q - Volume rate of flow

Read: d_n , (TW) - To obtain values of TW for other values of Q , enter Q and press STOP START.

STEP 2

Using a known tailwater or the tailwater calculated in STEP 1, determine an acceptable box culvert size in outlet control.

Use program #1-2



Enter: Q - Volume rate of flow

N - Number of barrels

L_a - Approximate total length of culvert, including inlet

n - Manning roughness coefficient for the barrel

k_e - Entrance energy loss coefficient

TW - Tailwater depth at the outlet of the culvert

Elevation of the outlet invert

B - Width of the box culvert

D - Height of the box culvert

Read: TW or $\frac{d_c + D}{2}$, whichever is controlling

HW_o - Outlet control headwater elevation

If HW_o elevation is not approximately equal to DHW elevation, enter new B and D. Repeat until an acceptable HW_o is obtained.

STEP 3

With the selected box size and entrance configuration, enter the following data to obtain outlet control performance curve data.

Use program #1-3

Enter: L_a - Approximate length of culvert, including inlet
n - Manning roughness coefficient for the culvert barrel
 k_e - Entrance energy loss coefficient
B - Width of box culvert
D - Height of box culvert
Elevation of the outlet invert
TW - Tailwater depth at outlet of culvert
Q/N - Volume rate of flow per barrel

Read: HW_o - Outlet control headwater elevation

To obtain values of HW_o for other values of Q/N, enter TW and Q/N. Repeat for each Q/N.

Since these values of HW_o are used for performance curve data, the different Q/N, values should reflect changes in Q, not N. TW will vary with Q if TW is based on normal depth in the natural channel.

STEP 4

Calculate outlet velocity for box culverts in outlet control.

Use program #1-4

Enter: TW - Tailwater depth at outlet of culvert

D - Height of box culvert

B - Width of box culvert

Q/N - Volume rate of flow per barrel

Read: Velocity - computed differently depending upon

whether d_c , TW or D governs.

STEP 5

Select type of inlet by performing the following inlet control calculations and computing performance curve data.

Use program #1-5 if analyzing a square edged inlet with headwalls.

Use program #1-6 if analyzing a 45° beveled inlet

Use program #1-7 if analyzing the throat section of a tapered inlet.

Enter: DHW Elevation

Elevation of the streambed at the face

B - Width of box culvert

D - Height of box culvert

Q/N - Volume rate of flow per barrel

Read: Elevation of face (or throat) invert - If this value exceeds that of the streambed at the face, the program will assume the elevation of the streambed at the face (zero FALL) in computing the performance curve.

FALL

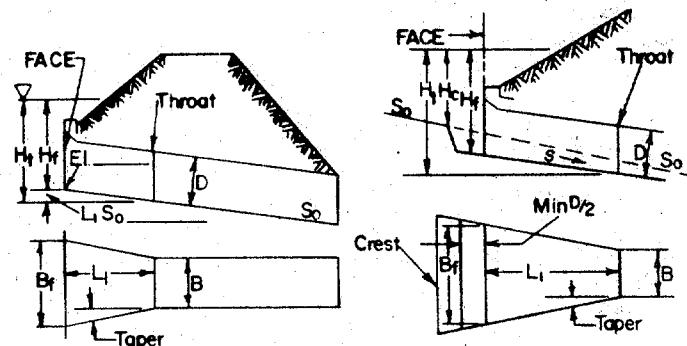
HW_f (or HW_t) - To obtain performance curve data, enter desired Q/N's.

At this point, evaluate the box size chosen. The question should be asked, "Is the minimum FALL excessive for the type of inlet being designed?" If the answer is yes, then return to STEP 2, select a larger box size and proceed through STEPS 3 and 4 again. If the answer is no, the culvert is either adequate or over designed. Use program # 1-13 to check the crest of depressed conventional or beveled designs.

STEP 6

If both the conventional and beveled inlet designs used are inadequate to handle the design Q at the DHW elevation or with a reasonable FALL, and a tapered inlet appears to be both desirable and economical, then design the tapered inlet throat. It is recommended that both side-tapered and slope-tapered designs be analyzed in order that the proper choice be made. To design a side-tapered inlet, proceed as follows. To design a slope-tapered inlet, go to STEP 8.

(SIDE-TAPERED INLET)



Use program #1-8 if the wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides. (Favorable face edge conditions)

Use program #1-9 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)

Enter: HW_f - Headwater elevation with face control
 Elevation of throat invert
 Taper + S - Sidewall flare angle plus
 slope of culvert barrel, $S = (S_0 - FALL/L_a)$
 NxB - Total clear width of culvert
 Q - Volume rate of flow
 D - Height of box culvert

Read: B_f - to round off B_f , enter the new, higher B_f value and press STOP START
 L_1 - Length of improved inlet
 Elevation of the face invert

Step 7

To complete the design of a side-tapered inlet, check crest control.

Use program #1-13

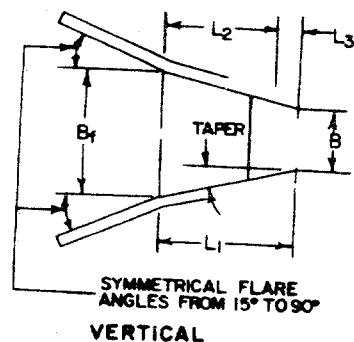
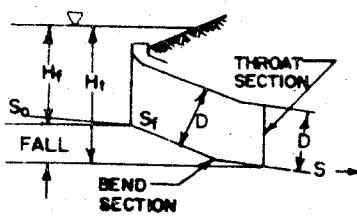
Enter: Q - Volume rate of flow
 N - Number of barrels
 HW_f - Headwater elevation required for flow to pass face section in face control
 W - Weir length = 10 times the FALL

Read: H_c

Maximum crest elevation

STEP 8

Design a slope-tapered inlet for box culvert. If designing a vertical face slope-tapered inlet, proceed as follows. If designing a mitered face slope-tapered inlet, go to STEP 10.



Use program #1-10 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides. (Favorable face edge conditions)

Use program #1-11 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)

Enter: Q - Volume rate of flow

D - Height of box culvert

HW_f - Headwater elevation required for flow to pass face section in face control

Elevation of face invert

y - Difference in elevation between crest and face section of a slope-tapered inlet with mitered face,
= 0 for vertical face

Read: Minimum B_f

Step 9

Calculate design dimensions for slope-tapered inlet with vertical face.

Use program #1-12

Enter: B - Width of box culvert

D - Height of box culvert

N - Number of barrels

B_f - Width of face section of improved inlet (May be rounded up from results of program 1-10 or 1-11)

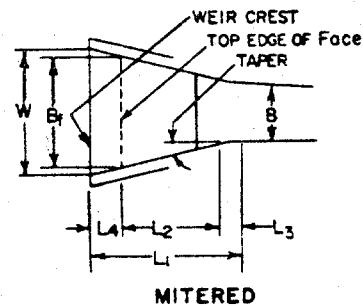
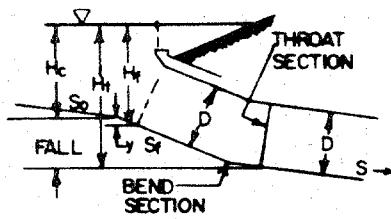
y - Difference in elevation between crest and face section of a slope-tapered inlet with mitered face,
= 0 for vertical face

Taper - Sidewall flare angle
 Elevation crest invert
 Elevation throat invert
 S_f - slope between the face and throat

Read: L_2
 L_3
 L_4
 L_1
 Taper

STEP 10

Mitered face slope-tapered inlet



Use program #1-10 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides.
 (Favorable face edge conditions)

Use program #1-11 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)

Enter: Q - Volume rate of flow
 D - Height of box culvert
 H_{Wf} - Headwater elevation required for flow to pass face section in face control
 Elevation of crest
 y - Difference in elevation between crest and face section of a slope-tapered inlet with mitered face,
 $= (.4D)$

Read: Minimum B_f

Step 11

Calculate design dimensions for slope-tapered inlet with vertical face.

Use program #1-12

Enter: B - Width of box culvert

D - Height of box culvert

N - Number of barrels

B_f - Width of face section of improved inlet (May be rounded up from results of program 1-10 or 1-11)

y - Difference in elevation between crest and face section of a slope-tapered inlet with mitered face,
= (.4D)

Taper - Sidewall flare angle

Elevation crest invert

Elevation throat invert

S_f - Slope between the face and throat

Read: L_2

L_3

L_4

L_1

Taper

STEP 12

Check crest control for a slope-tapered inlet with a mitered face.

Use program #1-13

Enter: Q - Volume rate of flow

N - Number of barrels

HW_f - Headwater elevation required for flow to pass face section in face control

B - Width of box culvert

L_1 - Distance between the throat and face

Taper - Sidewall flare angle

Read: H_c

Maximum crest elevation

Step 13

Calculate outlet velocity for box culverts in inlet control.

Use program #1-14

Enter: D - Height of box culvert

B - Width of box culvert

n - Manning roughness coefficient for culvert
barrel

Q/N - Volume rate of flow per barrel

S - Slope of culvert barrel

Read: d_n/B

Velocity

PROCEDURAL OUTLINE
FOR CIRCULAR PIPE CULVERTS

STEP 1

Determine TW elevation from Q and channel geometry if TW is based on normal depth in the natural channel.

Use program #1-1

$$Z_1 = \frac{1}{n} S_o = \frac{1}{\text{BW}} = Z_2$$

Enter: n - Manning roughness coefficient for the natural stream

S_o - Slope of natural channel

BW - Width of streambed bottom

Z_1 - Horizontal distance for side slope of channel

Z_2 - Horizontal distance for side slope of channel

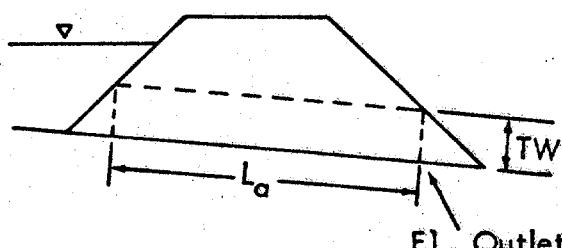
Q - Volume rate of flow

Read: d_n , (TW) - To obtain values of TW for other values of Q, enter Q and press STOP START.

STEP 2

Using a known tailwater or the tailwater calculated in STEP 1, determine an acceptable pipe culvert size in outlet control.

Use program #2-1



Enter: Q - Volume rate of flow

N - Number of barrels

L_a - Approximate total length of culvert, including inlet

n - Manning roughness coefficient for the barrel

k_e - Entrance energy loss coefficient

TW - Tailwater depth at the outlet of the culvert

Elevation of the outlet invert

d_c - Critical depth of flow

D - Diameter of the pipe culvert

Read: TW or $\frac{d_c + D}{2}$, whichever is controlling

HW_o - Outlet control headwater elevation

If HW_o elevation is not approximately equal to DHW elevation, enter new d_c and D. Repeat until an acceptable HW_o is obtained.

The value of d_c may be obtained from charts in Hydraulic Design Series 3, Design Charts for Open-Channel Flow, or any other source that shows critical depth as a function of culvert size and Q. If charts are unavailable, program #2-3 could be used to determine d_c .

STEP 3

With the selected pipe size and entrance configuration, enter the following data to obtain outlet control performance curve data.

Use program #2-2

Enter: L_a - Approximate length of culvert, including inlet
n - Manning roughness coefficient for the culvert barrel
 k_e - Entrance energy loss coefficient
D - Diameter of pipe culvert
Elevation of the outlet invert
TW - Tailwater depth at outlet of culvert
 d_c - Critical depth of flow
Q/N - Volume rate of flow per barrel

Read: HW_o - Outlet control headwater elevation

To obtain values of HW_o for other values of Q/N, enter TW, d_c and Q/N. Repeat for each Q/N.

Since these values of HW_o are used for performance curve data, the different Q/N, values should reflect changes in Q, not N. TW will vary with Q if TW is based on normal depth in the natural channel.

STEP 4

Calculate outlet velocity for pipe culverts in outlet control.

Use program #2-3

Enter: D - Diameter of pipe culvert

Q/N - Volume rate of flow per barrel

Alpha - Energy coefficient

Use 1.04 for concrete pipe

Use 1.12 for corrugated pipe

TW - Tailwater depth at outlet of culvert

Read: Velocity - computed differently depending upon
whether d_c , TW or D governs.

STEP 5

Select type of inlet by performing the following inlet control calculations and computing performance curve data.

Use program #2-4 if analyzing a thin-edged projecting inlet.

Use program #2-5 if analyzing an inlet with square edges.

Use program #2-6 if analyzing a beveled inlet.

Use program #2-7 if analyzing a groove end projecting inlet.

Use program #2-8 if analyzing a groove end inlet and headwalls.

Use program #2-9 if analyzing a tapered inlet throat. (smooth inlet)

Use program #2-10 if analyzing a tapered inlet throat. (rough inlet)

Enter: DHW - Elevation

Elevation of streambed at the face.

D - Diameter pipe culvert

Q/N - Volume rate of flow per barrel

Read: Elevation of face (or throat) invert - If this value exceeds that of the streambed at the face, the program will assume the elevation of the streambed at the face (zero FALL) in computing the performance curve.

FALL

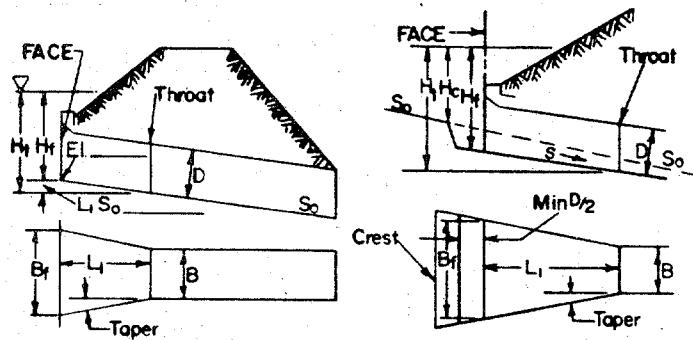
H_{W_f} (or H_{W_t}) - To obtain performance curve data, enter desired Q/N's.

At this point, evaluate the pipe size chosen. The question should be asked, "Is the minimum FALL excessive for the type of inlet being designed?" If the answer is yes, then return to STEP 2, select a larger pipe size and proceed through STEPS 3 and 4 again. If the answer is no, the culvert is either adequate or over designed. Use program # 1-13 to check the crest of depressed conventional or beveled designs.

STEP 6

If both the conventional and beveled inlet designs used are inadequate to handle the design Q at the DHW elevation or with a reasonable FALL, and a tapered inlet appears to be both desirable and economical, then design the tapered inlet throat. It is recommended that both side-tapered and slope-tapered designs be analyzed in order that the proper choice be made. To design a side-tapered inlet, proceed as follows. To design a slope-tapered inlet, go to STEP 8.

(SIDE-TAPERED INLET)



Use program #2-11 if the face has projecting thin edges.

Use program #2-12 if the face has square edges in a headwall.

Use program #2-13 if the face has bevels or a grooved end.

Enter: HW_f - Headwater elevation with face control
 Elevation of throat invert
 Taper + S - Sidewall flare angle plus
 slope of culvert barrel, $S = (S_o - FALL/L_a)$
 NxD - Total clear width of culvert
 Q - Volume rate of flow
 $E - D \leq E \leq 1.1D$

Read: B_f - to round off B_f , enter the new, higher B_f value and press STOP START
 L_1 - Length of improved inlet
 Elevation of the face invert

Step 7

To complete the design of a side-tapered inlet, check crest control.

Use program #1-13

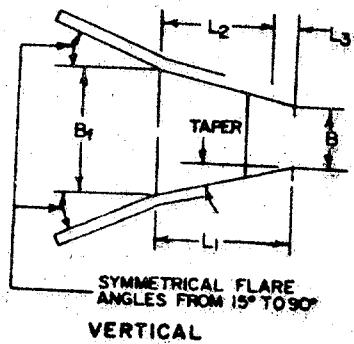
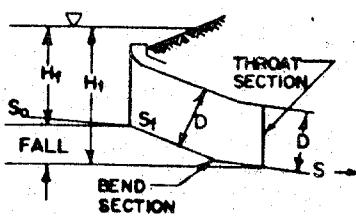
Enter: Q - Volume rate of flow
 N - Number of barrels
 HW_f - Headwater elevation required for flow to pass face section in face control
 W - Weir length = 10 times the FALL

Read: H_c

Maximum crest elevation

STEP 8

Design a slope-tapered inlet for box culvert. If designing a vertical face slope-tapered inlet, proceed as follows. If designing a mitered face slope-tapered inlet, go to STEP 10.



Use program #1-10 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides. (Favorable face edge conditions)

Use program #1-11 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)

Enter: Q - Volume rate of flow

D - Diameter of pipe culvert

HW_f - Headwater elevation required for flow to pass face section in face control

Elevation of face invert

y - Difference in elevation between crest and face

section of a slope-tapered inlet with mitered face,

= 0 for vertical face

Read: Minimum B_f

Step 9

Calculate design dimensions for slope-tapered inlet with vertical face.

Use program #1-12

Enter: B - Width of pipe culvert

D - Diameter of pipe culvert

N - Number of barrels

B_f - Width of face section of improved inlet (May be rounded up from results of program 1-10 or 1-11)

y - Difference in elevation between crest and face section of a slope-tapered inlet with mitered face,

= 0 for vertical face

Taper - Sidewall flare angle
 Elevation, crest invert
 Elevation throat invert
 S_f - slope between the face and throat

Read: L_2

L_3

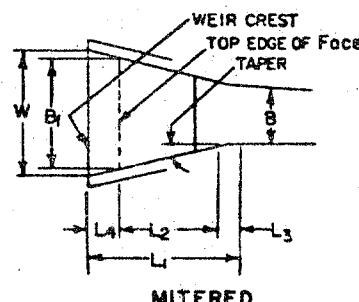
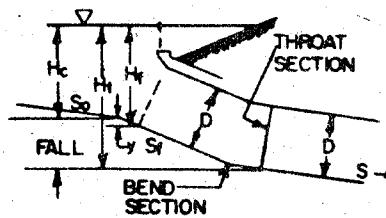
L_4

L_1

Taper

STEP 10

Mitered face slope-tapered inlet



Use program #1-10 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides.
 (Favorable face edge conditions)

Use program #1-11 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)

Enter: Q - Volume rate of flow

D - Diameter of pipe culvert

HW_f - Headwater elevation required for flow to pass face section in face control

Elevation of crest

y - Difference in elevation between crest and face section of a slope-tapered inlet with mitered face,
 $= (.4D)$

Read: Minimum B_f

Step 11

Calculate design dimensions for slope-tapered inlet with vertical face.

Use program #1-12

Enter: B - Width of pipe culvert

D - Diameter of pipe culvert

N - Number of barrels

B_f - Width of face section of improved inlet (May be rounded up from results of program 1-10 or 1-11)

y - Difference in elevation between crest and face section of a slope-tapered inlet with mitered face,
= (.4D)

Taper - Sidewall flare angle

Elevation crest invert

Elevation throat invert

S_f - Slope between the face and throat

Read: L_2

L_3

L_4

L_1

Taper

STEP 12

Check crest control for a slope-tapered inlet with a mitered face.

Use program #1-13

Enter: Q - Volume rate of flow

N - Number of barrels

H_{Wf} - Headwater elevation required for flow to pass face section in face control

D - Diameter of pipe culvert

L_1 - Distance between the throat and face

Taper - Sidewall flare angle

Read: H_c

Maximum crest elevation

Step 13

Calculate outlet velocity for pipe culverts in inlet control.

Use program #2-14

Enter: D - Diameter of pipe culvert

B - Width of pipe culvert

n - Manning roughness coefficient for culvert
barrel

Q/N - Volume rate of flow per barrel

S - Slope of culvert barrel

Read: Velocity

Example Problems

BOX CULVERT EXAMPLE NO. 1

Given: Design Discharge (Q) = 1,000 cfs, for a 50-year recurrence interval

Slope of stream bed (S_0) = 0.05 ft./ft.

Allowable Headwater Elevation = 200

Elevation Outlet Invert = 172.5

Culvert Length (L_a) = 350 ft.

Downstream channel approximates an 8' wide trapezoidal channel with 2:1 side slopes and a Manning's "n" of 0.03.

Requirements: This box culvert will be located in a rural area where the Allowable Headwater Elevation is not too critical; that is, the damages are low due to exceeding that elevation at infrequent times. Thus, the culvert should have the smallest possible barrel to pass design Q without exceeding AHW El. Use a reinforced concrete box with $n = 0.012$.

WORKSHEET FOR CULVERT DESIGN

PROJECT: EXAMPLE #1DESIGNER: PDW

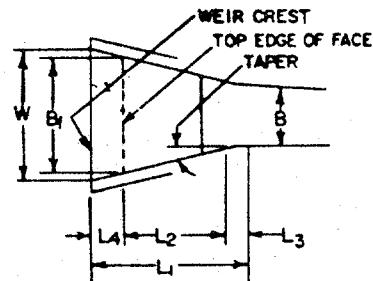
STATION: _____

DATE: 6/1/79

INITIAL DATA

Design Q 50 = 1000 cfs Channel Slope, S_o = 0.05 ft./ft.AHW Elevation = 200 ft. El. Stream bed at Face 190 ft.Approx. Culvert length, L_o = 350 ft. Barrel Shape BoxEl. Outlet Invert = 172.5 ft. Barrel Material REINF. CONC.

(See page 2 for natural stream data)

SUMMARY INFORMATION
FOR
SELECTED DESIGNBarrel Shape and Material REINF. CONC. BOX CULVERTFace Edge Description 45° BEVELSType of Improved Inlet SLOPE-TAPERED INLETWidth of box, B = 7 ft. Inlet length, L_1 = 15.22 ft.Depth or Diameter, D = 6 ft. Face to Bend, L_2 = 11.72 ft.Width of face, B_f = 14 ft. Bend to Throat, L_3 = 3.50 ft.No. of Barrels, N = 1 Crest to Face, L_4 = — ft.Inlet fall, FALL = 5.85 ft. Side Taper = 4.34 : 1Barrel Slope, S = 0.033 ft./ft. Crest Length, W = — ft.Top bevel height, d = 3 in. Side bevel width, b = 3.5 in.Outlet velocity, V = 34.43 ft./sec.COMMENTS ON DESIGN: _____

STEP 1
CALCULATE TAILWATER

Use file 1, block 1

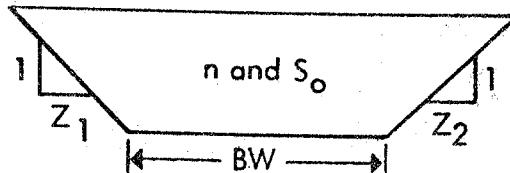
Enter: 1. $n = 0.03$ (channel)

2. $S_o = 0.05$

3. BW = 8

4. $Z_1 = 2$

5. $Z_2 = 2$



(Enter) 6. Q	(Read) TW, Based on d_n	COMMENTS
1000	3.51	
800	3.14	
600	2.71	
1200	3.85	

STEP 2

DETERMINE AN ACCEPTABLE CULVERT SIZE

Use file 1, block 2 if designing a box culvert.

~~Use file 2, block 1 if designing a circular pipe culvert.~~

Enter: 1. $Q = 1000$

2. $N = 1$

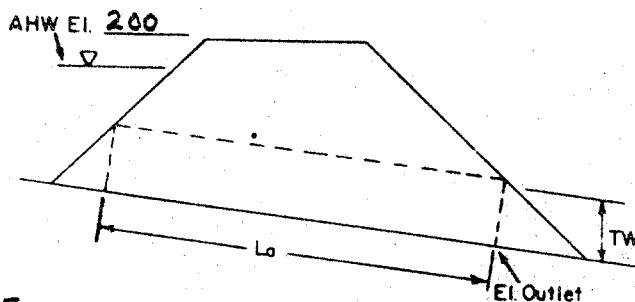
3. $L_a = 350$

4. $n = 0.012$ (Barrel)

5. $k_e = 0.2$

6. $TW = 3.51$

7. Elev. outlet invert = 172.5



(Enter) 8. B - If box (1) d_c - If pipe	(Enter) 9. D	(Read) $\frac{d_c + D}{2}$ or TW	(Read) H_W_o	COMMENTS
7	7	7.00	191.74	OK - but try smaller size
7	6	6.00	195.85	OK - USE
6	6	6.0	203.07	Exceeds AHW EI.

(1) d_c values taken from Design Charts For Open-Channel Flow,
Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 3

OUTLET CONTROL PERFORMANCE CURVE DATA

Use file 1, block 3 if designing a box culvert

~~Use file 2, block 2 if designing a pipe culvert~~

ENTER: 1. $L_a = \underline{350}$
 2. $n = \underline{0.012}$ (Barrel)
 3. $k_e = \underline{0.2}$
 4. $B = \underline{7}$ (for box only)
 5. $D = \underline{6}$
 6. Elev. outlet invert = 172.5

7. (2) (Enter) TW	8. (3) (Enter) d_c pipe only	9. (Enter) Q/N	(Read) HW _o	COMMENTS
3.51	—	1000	195.85	
3.14	—	800	189.60	
2.71	—	600	184.74	
3.85	—	1200	203.48	

Note: Plot outlet control performance curve

(2) Obtain values from Step 1

(3) d_c obtained from Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 4

OUTLET VELOCITY WHEN CULVERT IS IN OUTLET CONTROL

If designing a Box Culvert

Use file 1, block 4

Enter: 1. TW = 3.51
 2. D = 6.0
 3. B = 7.0
 4. Q/N = 1000

(Read):
Velocity
23.80

If designing a pipe culvert

Use file 2, block 3

Enter: 1. D = _____
 2. Q/N = _____
 3. Alpha = _____ (1.04 for RCP, 1.12 for CMP)
 4. TW = _____

(Read):
Velocity

STEP 5

INLET CONTROL CALCULATIONS AND PERFORMANCE CURVE DATA

(BOX CULVERTS)

Use file 1, block 5 if analyzing a square-edge inlet with headwalls.

Use file 1, block 6 if analyzing a 45° beveled inlet.

Use file 1, block 7 if analyzing a tapered inlet throat.

(PIPE CULVERTS)

~~Use file 2, block 4 if analyzing a thin-edged projecting inlet.~~

~~Use file 2, block 5 if analyzing an inlet with square edges in a headwall.~~

~~Use file 2, block 7 if analyzing a groove end projecting inlet.~~

~~Use file 2, block 8 if analyzing a groove end inlet and headwalls.~~

~~Use file 2, block 6 if analyzing a beveled intef.~~

~~Use file 2, block 9 if analyzing a tapered inlet throat. (Smooth inlet)~~

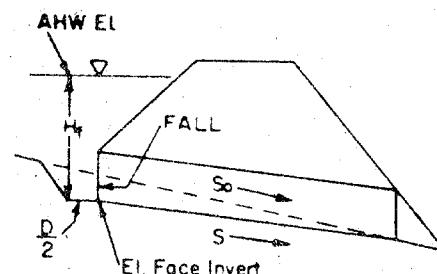
~~Use file 2, block 10 if analyzing a tapered inlet throat. (Rough inlet)~~

Enter: 1. AHW Elev. = 200

2. E1. Stream bed at face = 190

$$3. B = \frac{7}{(D, \text{ if pipe})}$$

$$4. D = \underline{\hspace{2cm}} 6$$



CONVENTIONAL or BEVELED

Q	5. (Enter) Q/N	(Read) E1. Face invert	(Read) FALL	(Read) HW _f	Note: Use Upper headings for Con- ventional or beveled face; Lower headings for tapered inlet throat. COMMENTS
		E1. Throat invert		HW _t	
Program No. <u>1-6</u> ,		Inlet and Edge Description <u>45° BEVELS</u>			
1000	1000	177.33	12.66	200.00	FALL IS TOO LARGE - TRY TAPERED THROAT INLET
Program No. <u>1-7</u> ,		Inlet and Edge Description <u>TAPERED INLET THROAT</u>			
1000	1000	184.14	5.85	200.00	OK - DRAW PERFORMANCE CURVES
800	800			196.41	
600	600			193.58	
1200	1200			204.48	

Note: Plot inlet control section performance curve

STEP 6 & 7
SIDE-TAPERED INLET AND CREST CHECK

(BOX CULVERTS)

Use file 1, block 8 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides. (Favorable face edge conditions)
 Use file 1, block 9 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)

(PIPE CULVERTS)

Use file 2, block 11 if the face has projecting thin edges.
 Use file 2, block 12 if the face has square edges in a headwall.
 Use file 2, block 13 if the face has bevels or a groove end.

(CREST CHECK)

Use file 1, block 13 for crest check on a conventional, beveled or side-tapered inlet.

Enter: 1. $HW_f = 200$

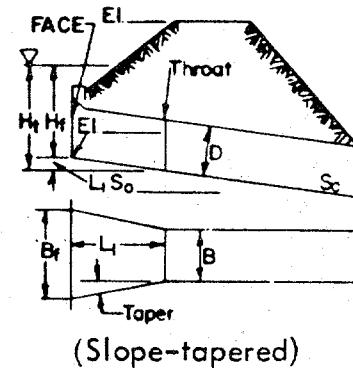
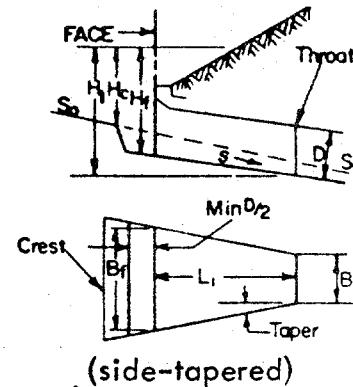
2. EI . Throat Invert = 184.14

3. $(Taper + S) = 4.033$ (Taper is 4:1 to 6:1), ($S \approx S_o - FALL/L_a$)

4. $N \times B = 7$ ($N \times D$ for pipe)

5. $Q = 1000$

6. $D = 6$ (E for pipe, where $D \leq E \leq 1.1 D$)



(4) (Read) Min. B_f	B_f Used	(Read) L_1	(Read) EI . face invert	COMMENTS
10.28	10.50	7.00	184.37	

(4) To use a B_f that is rounded off enter new B_f and press START STOP

Enter: (Crest Check)

1. $Q = 1000$ 2. $N = 1$ 3. $HW_f = 200$ 4. $W = 58.5$

5. $B = 0$ 6. $L_1 = 0$ 7. Taper = 0

Crest Check: (Read) $H_c = 3.31$, (Read) Max. Crest $EI. = 196.68$

STEP 8 THROUGH 12
SLOPE-TAPERED INLET AND CREST CHECK

Use file 1, block 10 for B_f if face has favorable edge conditions as in STEP 5.

Use file 1, block 11 for B_f if face has unfavorable edge conditions as in STEP 5.

Enter: 1. $Q = \underline{1000}$

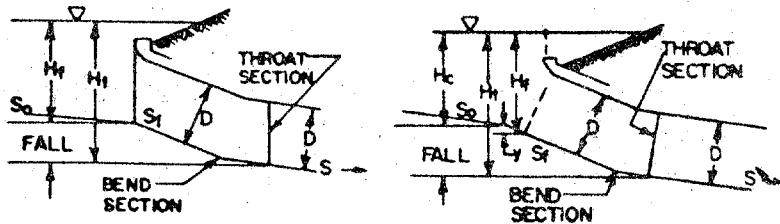
2. $D = \underline{6}$

3. $HW_f = \underline{200}$

4. E1. Streambed at face = 190 (if vertical face)

E1. Crest = _____ (if mitered face)

5. $y = \underline{0}$



(Read) Min. B_f , or higher rounded value	Type of Face
<u>13.72</u> (USE 14.0)	Vertical, $y = 0$
	Mitered, $y = .4D$

Use file 1, block 12 for L dimensions of an inlet with a vertical face.

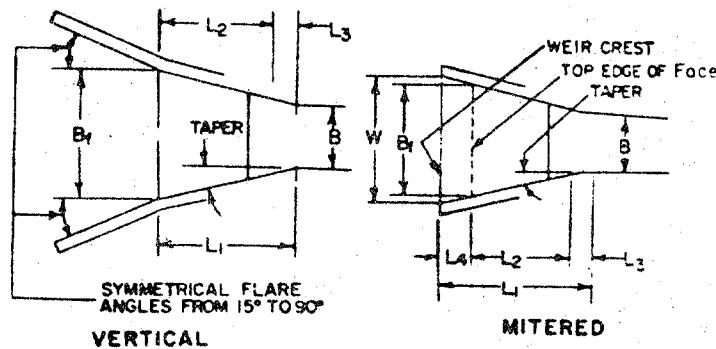
Enter: 1. $B = \underline{7}$ 6. Taper = 4 : 1

2. $D = \underline{6}$ 7. E1. Crest Inv. = 190

3. $N = \underline{1}$ 8. E1. Throat Inv. = 184.14

4. $B_f = \underline{14}$ 9. $S_f = \underline{2}$: 1
(2:1 to 3:1)

5. $y = \underline{0}$



(Read) L_2	(Read) L_3	(Read) L_4	(Read) L_1	(Read) Taper	Type of Face
<u>11.72</u>	<u>3.50</u>	<u>0</u>	<u>15.22</u>	<u>4.34</u>	Vertical, $y = 0$
					Mitered, $y = .4D$

Use file 1, block 13 for crest check on a slope-tapered inlet with mitered face.

Enter: 1. $Q = \underline{\quad}$ 3. $HW_f = \underline{\quad}$ 6. $L_1 = \underline{\quad}$

2. $N = \underline{\quad}$ 4. $W = \underline{0}$ 7. Taper = : 1

5. $B = \underline{\quad}$

Crest Check: (Read) $H_c = \underline{\quad}$, (Read) Max, Crest E1. =

STEP 13
OUTLET VELOCITY WHEN CULVERT IS IN INLET CONTROL

Use file 1, block 14 if designing a box culvert
 Use file 2, block 14 if designing a pipe culvert

- Enter:
1. D = 6
 2. B = 7 (Use D if designing a pipe)
 3. n = 0.012
 4. Q/N = 1000
 5. S = 0.033 = $(S_o - \text{FALL}/L_a)$

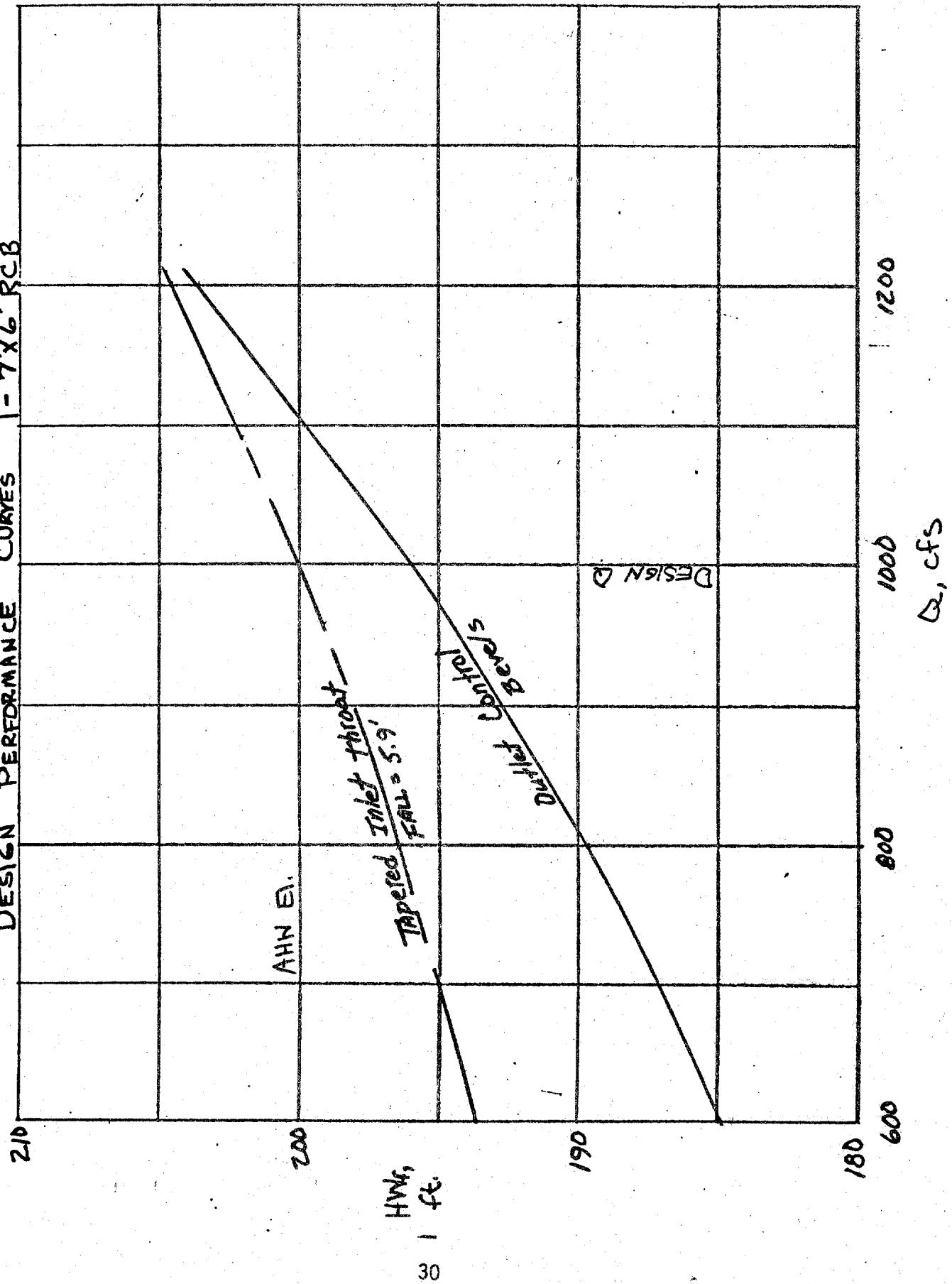
(READ) d/n/B	(READ) Velocity
0.59	34.43

For Box Culvert

(READ) Velocity

For pipe culvert

DESIGN PERFORMANCE CURVES - 7'x6' RCB



PIPE CULVERT EXAMPLE NO. 2

Given: Same as example no. 1

Requirements: Use a concrete pipe with $n = 0.012$

WORKSHEET FOR CULVERT DESIGN

PROJECT: EXAMPLE #2DESIGNER: PDW

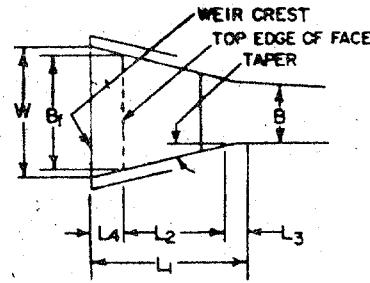
STATION: _____

DATE: 6/1-79

INITIAL DATA

Design Q 50 = 1000 cfs Channel Slope, S_0 = 0.05 ft./ft.AHW Elevation = 200 ft. El. Stream bed at Face 190 ft.Approx. Culvert length, L_a = 350 ft. Barrel Shape CIRCULAR PIPEEl. Outlet Invert = 172.5 ft. Barrel Material REINF. CONC.

(See page 2 for natural stream data)

SUMMARY INFORMATION
FOR
SELECTED DESIGNBarrel Shape and Material REINF. CONC. CIRC. PIPEFace Edge Description 45° BEVELSType of Improved Inlet SLOPE-TAPERED INLETWidth of box, B = — ft. Inlet length, L_1 = 24.78 ft.Depth or Diameter, D = 7 ft. Face to Bend, L_2 = 21.28 ft.Width of face, B_f = 13.0 ft. Bend to Throat, L_3 = 3.50 ft.No. of Barrels, N = 1 Crest to Face, L_4 = — ft.Inlet fall, FALL = 10.63 ft. Side Taper = 8.26 : 1Barrel Slope, S = 0.020 ft./ft. Crest Length, W = — ft.Top bevel height, d = 3.5 in. Side bevel width, b = 6.5 in.Outlet velocity, V = 29.14 ft./sec.

COMMENTS ON DESIGN: _____

STEP 1
CALCULATE TAILWATER

Use file 1, block 1

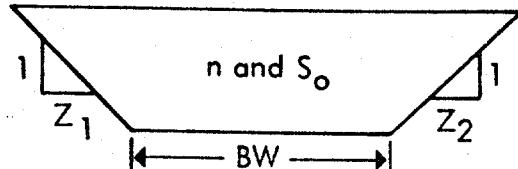
Enter: 1. $n = 0.03$ (channel)

2. $S_o = 0.05$

3. BW = 8

4. $Z_1 = 2$

5. $Z_2 = 2$



(Enter) 6. Q	(Read) TW, Based on d_n	COMMENTS
1000	3.51	
800	3.14	
600	2.71	
1200	3.85	

STEP 2

DETERMINE AN ACCEPTABLE CULVERT SIZE

~~Use file 1, block 2 if designing a box culvert.~~

Use file 2, block 1 if designing a circular pipe culvert.

Enter: 1. $Q = 1000$

2. $N = 1$

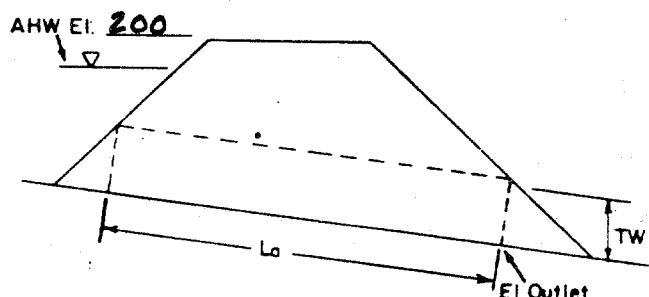
3. $L_a = 350$

4. $n = 0.012$ (Barrel)

5. $k_e = 0.2$

6. $TW = 3.5$

7. Elev. outlet invert = 172.5



8. (Enter) (1) d_c - If pipe	9. (Enter) D	(Read) $\frac{d_c + D}{2}$ or TW	(Read) HW _o	COMMENTS
> 7	7	7.0	199.34	OK - USE
7.73	8	7.86	191.30	
> 6.5	6.5	6.5	206.71	EXCEEDS AHW EI.

(1) d_c values taken from Design Charts For Open-Channel Flow,
Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 3

OUTLET CONTROL PERFORMANCE CURVE DATA

~~Use file 1, block 3 if designing a box culvert~~

Use file 2, block 2 if designing a pipe culvert

ENTER: 1. $L_a = \underline{350}$
 2. $n = \underline{0.012}$ (Barrel)
 3. $k_e = \underline{0.2}$
 4. $B = \underline{\quad}$ (for box only)
 5. $D = \underline{7}$
 6. Elev. outlet invert = 172.5

7. (2) (Enter) TW	8. (3) (Enter) d_c - pipe only	9. (Enter) Q/N	(Read) HW _o	COMMENTS
3.51	> 7	1000	199.34	
3.14	> 7	800	192.20	
2.71	6.3	600	186.29	
3.85	> 7	1200	208.08	

Note: Plot outlet control performance curve

(2) Obtain values from Step 1

(3) d_c obtained from Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 4

OUTLET VELOCITY WHEN CULVERT IS IN OUTLET CONTROL

If designing a Box Culvert

~~Use file 1, block 4~~

Enter: 1. TW = _____
 2. D = _____
 3. B = _____
 4. Q/N = _____

(Read):
Velocity

If designing a pipe culvert

~~Use file 2, block 3~~

Enter: 1. D = 7
 2. Q/N = 1000
 3. Alpha = 1.04 (1.04 for RCP, +.12 for CMP)
 4. TW = 3.51

(Read):
Velocity
26.06

STEP 5

INLET CONTROL CALCULATIONS AND PERFORMANCE CURVE DATA

(BOX CULVERTS)

~~Use file 1, block 5 if analyzing a square-edge inlet with headwalls.~~

~~Use file 1, block 6 if analyzing a 45° beveled inlet.~~

~~Use file 1, block 7 if analyzing a tapered inlet throat.~~

(PIPE CULVERTS)

~~Use file 2, block 4 if analyzing a thin-edged projecting inlet.~~

~~Use file 2, block 5 if analyzing an inlet with square edges in a headwall.~~

~~Use file 2, block 7 if analyzing a groove end projecting inlet.~~

~~Use file 2, block 8 if analyzing a groove end inlet and headwalls.~~

Use file 2, block 6 if analyzing a beveled inlet.

Use file 2, block 9 if analyzing a tapered inlet throat. (Smooth inlet)

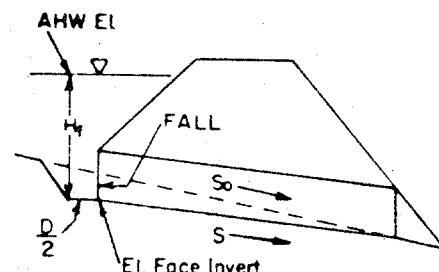
Use file 2, block 10 if analyzing a tapered inlet throat. (Smooth inlet)

Enter: 1. AHW Elev. = 200

2. E1. Stream bed at face = 190

3. B = 7 (D, if pipe)

$$4. D = 7$$



CONVENTIONAL or BEVELED

Q	5. (Enter) Q/N	(Read) E1. Face invert	(Read)	(Read) HW _f	Note: Use Upper headings for Con- ventional or beveled face: Lower headings for tapered inlet throat. COMMENTS
		E1. Throat invert	FALL	HW _t	
Program No.	2-6	Inlet and Edge Description	45° BEVELS		
1000	1000	172.27	17.72	200.00	FALL TOO LARGE
Program No.	2-9	Inlet and Edge Description	TAPERED INLET - SMOOTH THROAT		
1000	1000	179.36	10.63	200.00	FALL ≈ 1.5 D - OK
800	800			194.84	
600	600			190.79	DRAW PERFORMANCE CURVES
1200	1200			205.92	

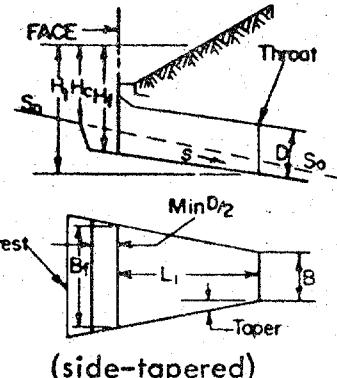
Note: Plot inlet control section performance curve

STEP 6 & 7

SIDE-TAPERED INLET AND CREST CHECK

(BOX CULVERTS)

~~Use file 1, block 8 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides. (Favorable face edge conditions)~~
~~Use file 1, block 9 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)~~



(PIPE CULVERTS)

~~Use file 2, block 11 if the face has projecting thin edges.~~
~~Use file 2, block 12 if the face has square edges in a headwall.~~
~~Use file 2, block 13 if the face has bevels or a groove end.~~

(CREST CHECK)

Use file 1, block 13 for crest check on a conventional, beveled or side-tapered inlet.

Enter: 1. $HW_f = 200$

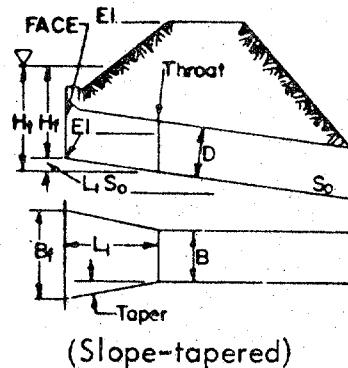
2. EI . Throat Invert = 179.36

3. $(Taper + S) = 4.020$ (Taper is 4:1 to 6:1), ($S \approx S_o - \text{FALL} / L_a$)

4. $N \times B = 7$ ($N \times D$ for pipe)

5. $Q = 1000$

6. $D = 7$ (E for pipe, where $D \leq E \leq 1.1 D$)



(Slope-tapered)

(4) (Read) Min. B_f	B_f Used	(Read) L_1	(Read) EI . face invert	COMMENTS
9.42	10.00	6.0	179.48	

(4) To use a B_f that is rounded off enter new B_f and press START STOP

Enter: (Crest Check)

1. $Q = 1000$ 2. $N = 1$ 3. $HW_f = 200$ 4. $W = 106.30$

5. $B = 0$ 6. $L_1 = 0$ 7. Taper = 0

Crest Check: (Read) $H_c = 2.22$, (Read) Max. Crest $EI. = 197.77$

STEP 8 THROUGH 12
SLOPE-TAPERED INLET AND CREST CHECK

Use file 1, block 10 for B_f if face has favorable edge conditions as in STEP 5.
 Use file 1, block 11 for B_f if face has unfavorable edge conditions as in STEP 5.

Enter: 1. $Q = \underline{1000}$

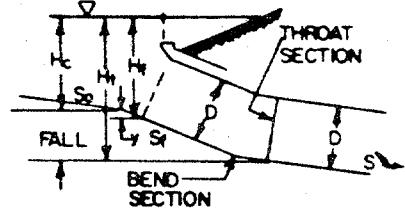
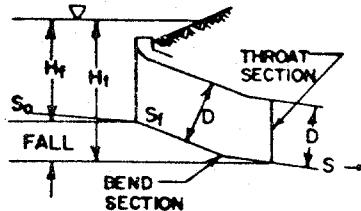
2. $D = \underline{7}$

3. $HW_f = \underline{200}$

4. E1. Streambed at face = 190 (if vertical face)

~~E1. Crest = _____~~ (if mitered face)

5. $y = \underline{0}$



(Read) Min. B_f , or higher rounded value	Type of Face
12.56 (USE 13.0)	Vertical, $y = 0$
	Mitered, $y = .4D$

Use file 1, block 12 for L dimensions of an inlet with a vertical face.

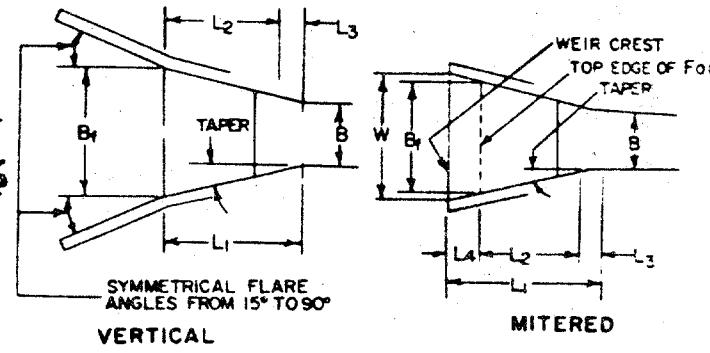
Enter: 1. $B = \underline{7}$ 6. Taper = 4 : 1

2. $D = \underline{7}$ 7. E1. Crest Inv. = 190

3. $N = \underline{1}$ 8. E1. Throat Inv. = 179.36

4. $B_f = \underline{13}$ 9. $S_f = \underline{2}$: 1
(2:1 to 3:1)

5. $y = \underline{0}$



(Read) L_2	(Read) L_3	(Read) L_4	(Read) L_1	(Read) Taper	Type of Face
21.28	3.50	0	24.78	8.26	Vertical, $y = 0$
					Mitered, $y = .4D$

Use file 1, block 13 for crest check on a slope-tapered inlet with mitered face.

Enter: 1. $Q = \underline{\hspace{2cm}}$

3. $HW_f = \underline{\hspace{2cm}}$

6. $L_1 = \underline{\hspace{2cm}}$

2. $N = \underline{\hspace{2cm}}$

4. $W = \underline{0}$

7. Taper = _____ : 1

5. $B = \underline{\hspace{2cm}}$

Crest Check: (Read) $H_c = \underline{\hspace{2cm}}$, (Read) Max, Crest E1. = <u>_____</u>
--	--

STEP 13

OUTLET VELOCITY WHEN CULVERT IS IN INLET CONTROL

Use file 1, block 14 if designing a box culvert
 Use file 2, block 14 if designing a pipe culvert

Enter: 1. D = 7

2. B = 7 (Use D if designing a pipe)

3. n = 0.012

4. Q/N = 1000

5. S = 0.02 = $(S_o - \text{FALL}/L_a)$

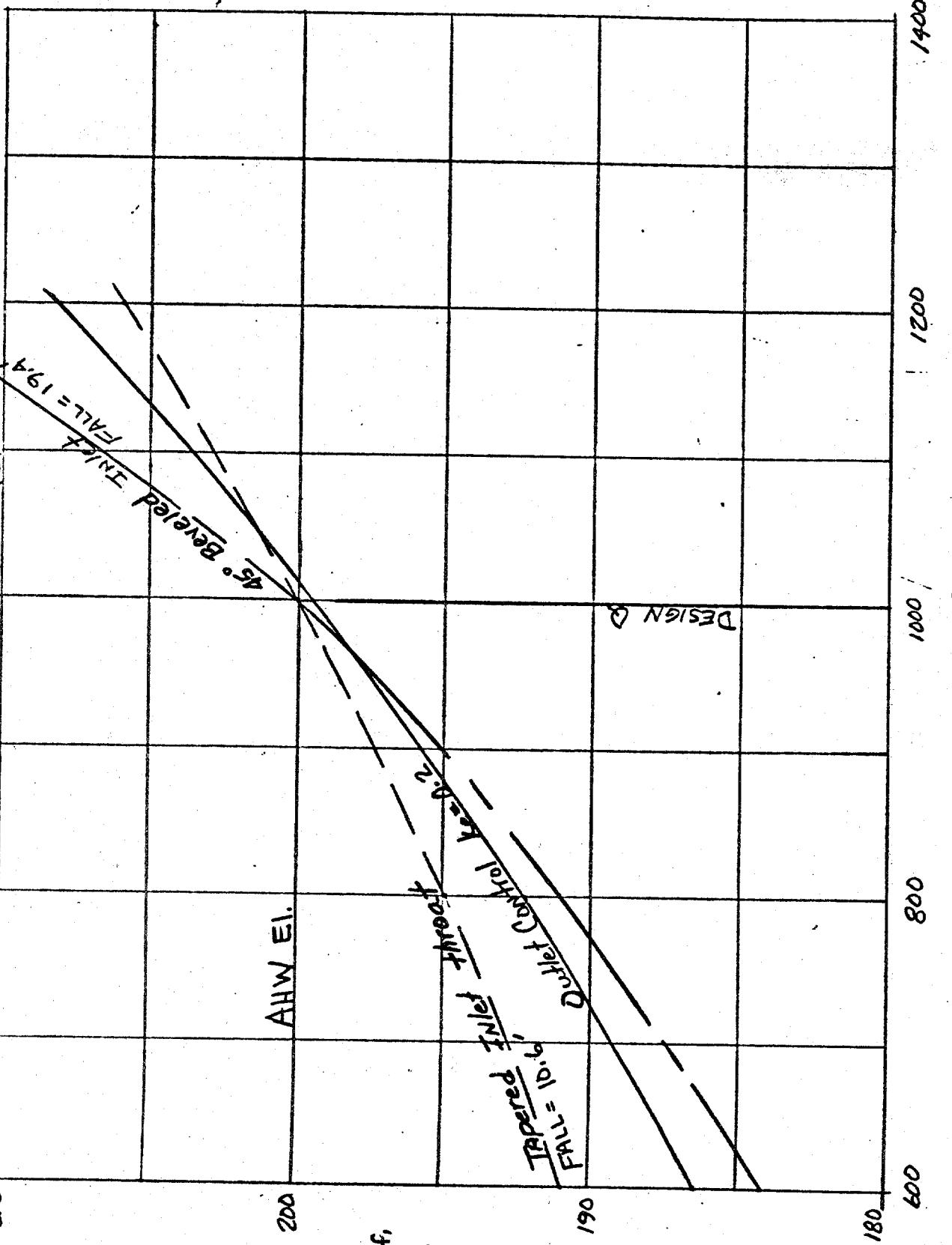
(READ) d/n/B	(READ) Velocity

For Box Culvert

(READ) Velocity
29.14

For pipe culvert

DESIGN PERFORMANCE CURVES 1-7' RCP



BOX CULVERT EXAMPLE NO. 3

Given: Same as example no. 1 except

Slope of stream bed (S_o) = 0.005 ft./ft.

Elevation Outlet Invert = 188.25

Requirements: Same as example no. 1

WORKSHEET FOR CULVERT DESIGN

PROJECT: EXAMPLE #3DESIGNER: PDW

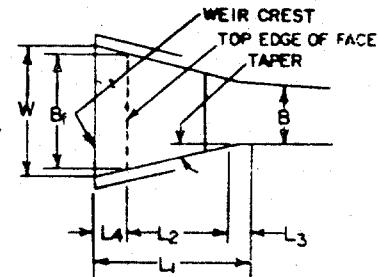
STATION: _____

DATE: 6/1/79

INITIAL DATA

Design Q 50 = 1000 cfs Channel Slope, S_o = 0.005 ft./ft.AHW Elevation = 200 ft. El. Stream bed at Face 190 ft.Approx. Culvert length, Barrel Shape Box L_a = 350 ft. Barrel Material REINF. CONC.El. Outlet Invert = 188.25 ft. Barrel Roughness, n. 0.012

(See page 2 for natural stream data)

SUMMARY INFORMATION
FOR
SELECTED DESIGNBarrel Shape and Material REINF. CONC. Box CULVERTFace Edge Description 45° BEVELSType of Improved Inlet NONEWidth of box, B = 10 ft. Inlet length, L₁ = — ft.Depth or Diameter, D = 9 ft. Face to Bend, L₂ = — ft.Width of face, B_f = — ft. Bend to Throat, L₃ = — ft.No. of Barrels, N = 1 Crest to Face, L₄ = — ft.Inlet fall, FALL = 0.92 ft. Side Taper = — : 1Barrel Slope, S = 0.005 ft./ft. Crest Length, W = — ft.Top bevel height, d = 4.5 in. Side bevel width, b = 5 in.Outlet velocity, V = 16.97 ft./sec.

COMMENTS ON DESIGN: _____

STEP 1
CALCULATE TAILWATER

Use file 1, block 1

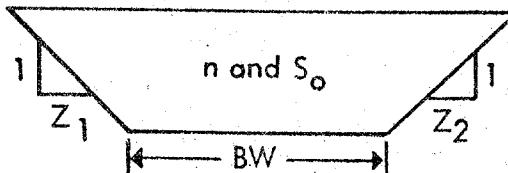
Enter: 1. $n = 0.03$ (channel)

2. $S_o = 0.005$

3. BW = 8

4. $Z_1 = 2$

5. $Z_2 = 2$



(Enter) 6. Q	(Read) TW, Based on d_n	COMMENTS
1000	6.11	
800	5.51	
600	4.81	
1200	6.65	

STEP 2
DETERMINE AN ACCEPTABLE CULVERT SIZE

Use file 1, block 2 if designing a box culvert.

Use file 2, block 1 if designing a circular pipe culvert.

Enter: 1. $Q = 1000$

2. $N = 1$

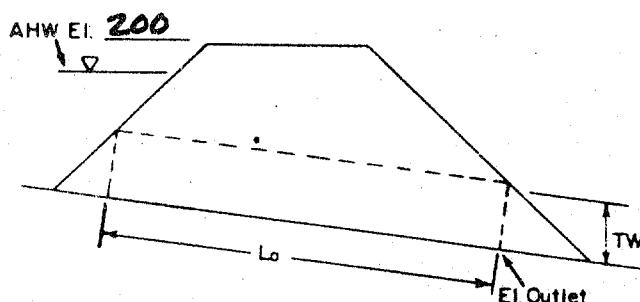
3. $L_a = 350$

4. $n = 0.012$ (Barrel)

5. $k_e = 0.5 \& 0.2$

6. $TW = 6.11$

7. Elev. outlet invert = 188.25



(Enter) 8. B - If box (1) d_c - If pipe	(Enter) 9. D	(Read) $\frac{d_c + D}{2}$ or TW	(Read) H_W	COMMENTS
8	8	7.93	204.07	EXCEEDS AHWEL. $k_e = .5$
9	9	8.14	200.40	EXCEEDS AHWEL $k_e = .2$
10	9	7.89	199.33	OK - USE $k_e = .2$

(1) d_c values taken from Design Charts For Open-Channel Flow,
Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 3

OUTLET CONTROL PERFORMANCE CURVE DATA

Use file 1, block 3 if designing a box culvert
 Use file 2, block 2 if designing a pipe culvert

ENTER: 1. $L_a = \underline{350}$
 2. $n = \underline{0.012}$ (Barrel)
 3. $k_e = \underline{0.2}$
 4. $B = \underline{10}$ (for box only)
 5. $D = \underline{9}$
 6. Elev. outlet invert = 188.25

7. (2) (Enter) TW	8. (3) (Enter) d_c - pipe only	9. (Enter) Q/N	(Read) HW _o	COMMENTS
6.11	—	1000	199.33	
5.51	—	800	197.71	
4.81	—	600	196.31	
6.65	—	1200.	201.17	

Note: Plot outlet control performance curve

(2) Obtain values from Step 1

(3) d_c obtained from Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 4

OUTLET VELOCITY WHEN CULVERT IS IN OUTLET CONTROL

If designing a Box Culvert

Use file 1, block 4

Enter: 1. TW = 6.11
 2. D = 9
 3. B = 10
 4. Q/N = 1000

(Read):
Velocity
14.73

If designing a pipe culvert

Use file 2, block 3

Enter: 1. D = _____
 2. Q/N = _____
 3. Alpha = _____ (1.04 for RCP, 1.12 for CMP)
 4. TW = _____

(Read):
Velocity

STEP 5

INLET CONTROL CALCULATIONS AND PERFORMANCE CURVE DATA

(BOX CULVERTS)

Use file 1, block 5 if analyzing a square-edge inlet with headwalls.

Use file 1, block 6 if analyzing a 45° beveled inlet.

Use file 1, block 7 if analyzing a tapered inlet throat.

(PIPE CULVERTS)

Use file 2, block 4 if analyzing a thin-edged projecting inlet.

Use file 2, block 5 if analyzing an inlet with square edges in a headwall.

Use file 2, block 7 if analyzing a groove-end projecting inlet.

Use file 2, block 8 if analyzing a groove-end inlet and headwalls.

Use file 2, block 6 if analyzing a beveled inlet.

Use file 2, block 9 if analyzing a tapered inlet throat. (Smooth inlet)

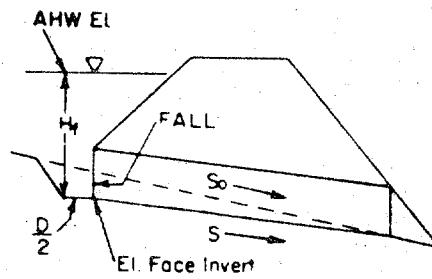
Use file 2, block 10 if analyzing a tapered inlet throat. (Rough inlet)

Enter: 1. AHW Elev. = 200

2. El. Stream bed at face = 190

3. B = 10 (D, if pipe)

4. D = 9



CONVENTIONAL or BEVELED

Q	5. (Enter) Q/N	(Read) El. Face invert	(Read) FALL	(Read) HW _f	Note: Use Upper headings for Conventional or beveled face: Lower headings for tapered inlet throat. COMMENTS
		El. Throat invert	HW _t		

Program No. 1-5, Inlet and Edge Description SQ. EDGES W/ HEADWALLS

1000	1000	188.05	1.94	200.00	TRY BEVELED INLET
800	800			198.03	
600	600			196.20	
1200	1200			202.22	

Program No. 1-6, Inlet and Edge Description 45° BEVELS

1000	1000	189.07	0.92	200.00	FALL IS MINOR - NOT NECESSARY
800	800			198.27	TO INCREASE SIZE JUST TO
600	600			196.59	ELIMINATE FALL
1200	1200			201.87	DRAW PERFORMANCE CURVES

Note: Plot inlet control section performance curve

STEP 13
OUTLET VELOCITY WHEN CULVERT IS IN INLET CONTROL

Use file 1, block 14 if designing a box culvert
~~Use file 2, block 14 if designing a pipe culvert~~

Enter: 1. D = 9

2. B = 10 (Use D if designing a pipe)

3. n = 0.012

4. Q/N = 1000

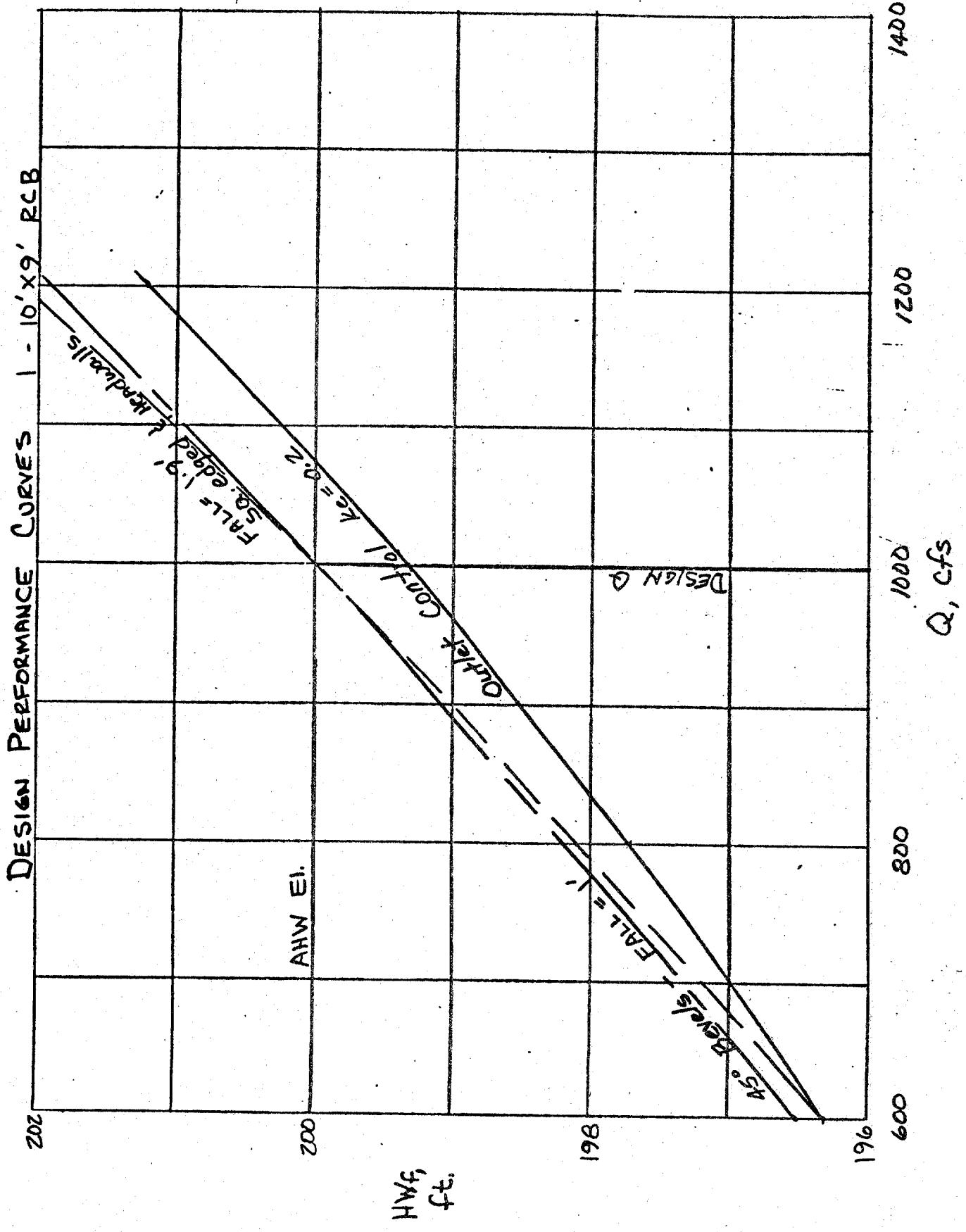
5. S = 0.005 = $(S_o - \text{FALL}/L_a)$

(READ) d/n/B	(READ) Velocity
.58	16.97

For Box Culvert

(READ) Velocity

For pipe culvert



BOX CULVERT EXAMPLE NO. 4

Given: An existing box culvert built on a rock foundation requires modification to handle higher than anticipated flows.

Original Design: Box size = 7' x 6'

Design discharge, $Q_{50} = 350 \text{ cfs}$

Allowable headwater elevation = 100

Elevation outlet invert = 75.0

Elevation inlet invert = 92.5

Culvert length = 350 ft.

Barrel Slope, $S = 0.05 \text{ ft./ft.}$

Channel Slope, $S_0 = 0.05 \text{ ft./ft.}$

Manning $n = 0.012$

Entrance configuration = square edges with headwalls

Downstream channel approximates a 6' wide trapezoidal channel with 2:1 side slopes and a Manning's "n" of 0.03

Requirements: Modify box culvert to handle $Q_{50} = 425 \text{ cfs.}$

WORKSHEET FOR CULVERT DESIGN

PROJECT: EXAMPLE #4

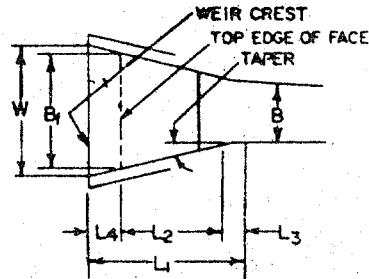
STATION: _____

DESIGNER: PDWDATE: 6/1/79

INITIAL DATA

Design Q 50 = 350 cfs Channel Slope, s_o = 0.05 ft./ft.AHW Elevation = 100 ft. El. Stream bed at Face 92.5 ft.Approx. Culvert length, L_a = 350 ft. Barrel Shape BoxBarrel Material REINF. CONC.El. Outlet Invert = 75 ft. Barrel Roughness, n. 0.012

(See page 2 for natural stream data)

SUMMARY INFORMATION
FOR
SELECTED DESIGNBarrel Shape and Material REINF. CONC. BOX CULVERTFace Edge Description 45° BEVELSType of Improved Inlet SIDE-TAPERED INLETWidth of box, B = 7 ft. Inlet length, L_1 = 8 ft.Depth or Diameter, D = 6 ft. Face to Bend, L_2 = — ft.Width of face, B_f = 11 ft. Bend to Throat, L_3 = — ft.No. of Barrels, N = 1 Crest to Face, L_4 = — ft.Inlet fall, FALL = 0 ft. Side Taper = 4 : 1Barrel Slope, S = 0.05 ft./ft. Crest Length, W = — ft.Top bevel height, d = 3 in. Side bevel width, b = 3.5 in.Outlet velocity, V = 32.27 ft./sec.COMMENTS ON DESIGN: BUILD SIDE-TAPERED INLET AS
AN EXTENSION OF THE EXISTING BOX CULVERT.

STEP 1
CALCULATE TAILWATER

Use file 1, block 1

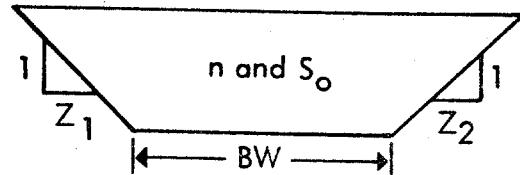
Enter: 1. $n = \underline{0.03}$ (channel)

2. $S_o = \underline{0.05}$

3. BW = 6

4. $Z_1 = \underline{2}$

5. $Z_2 = \underline{2}$



(Enter) 6. Q	(Read) TW, Based on d_n	COMMENTS
350	2.28	
300	2.11	
400	2.44	
500	2.73	

STEP 2
DETERMINE AN ACCEPTABLE CULVERT SIZE

Use file 1, block 2 if designing a box culvert.

Use file 2, block 1 if designing a circular pipe culvert.

Enter: 1. $Q = \underline{\hspace{2cm}}$

2. $N = \underline{\hspace{2cm}}$

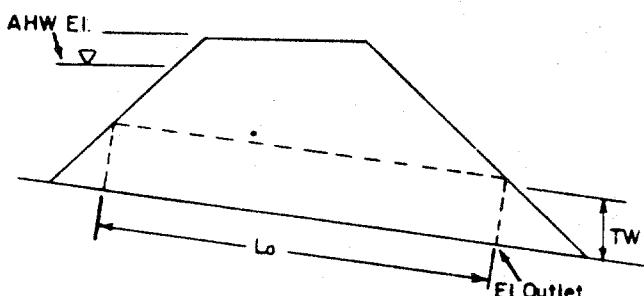
3. $L_a = \underline{\hspace{2cm}}$

4. $n = \underline{\hspace{2cm}}$ (Barrel)

5. $k_e = \underline{\hspace{2cm}}$

6. $TW = \underline{\hspace{2cm}}$

7. Elev. outlet invert =



(Enter) 8. B - If box (1) d_c - If pipe	(Enter) 9. D	(Read) $\frac{d_c + D}{2}$ or TW	(Read) H_w	COMMENTS
<i>Since we already know the culvert size, STEP #2 is unnecessary. However, it is good to plot the outlet and inlet control performance curves for the existing culvert.</i>				

(1) d_c values taken from Design Charts For Open-Channel Flow,
Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 3

OUTLET CONTROL PERFORMANCE CURVE DATA

Use file 1, block 3 if designing a box culvert

~~Use file 2, block 2 if designing a pipe culvert~~

ENTER: 1. $L_a = \underline{350}$
 2. $n = \underline{0.012}$ (Barrel)
 3. $k_e = \underline{0.5}$
 4. $B = \underline{7}$ (for box only)
 5. $D = \underline{6}$
 6. Elev. outlet invert = 75

7. (2) (Enter) TW	8. (3) (Enter) $d_c = \text{pipe only}$	9. (Enter) Q/N	(Read) HW _o	COMMENTS
2.28	—	350	82.85	
2.15	—	300	81.92	
2.47	—	400	83.88	
2.76	—	500	86.25	

Note: Plot outlet control performance curve

(2) Obtain values from Step 1

(3) d_c obtained from Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 4

OUTLET VELOCITY WHEN CULVERT IS IN OUTLET CONTROL

If designing a Box Culvert

Use file 1, block 4

Enter: 1. TW = 2.28
 2. D = 6
 3. B = 7
 4. Q/N = 350

(Read):
Velocity
11.69

If designing a pipe culvert

~~Use file 2, block 3~~

Enter: 1. D = _____
 2. Q/N = _____
 3. Alpha = _____ (1.04 for RCP, 1.12 for CMP)
 4. TW = _____

(Read):
Velocity

STEP 5

INLET CONTROL CALCULATIONS AND PERFORMANCE CURVE DATA

(BOX CULVERTS)

~~Use file 1, block 5 if analyzing a square-edge inlet with headwalls.~~

~~Use file 1, block 6 if analyzing a 45° beveled inlet.~~

~~Use file 1, block 7 if analyzing a tapered inlet throat.~~

(PIPE CULVERTS)

~~Use file 2, block 4 if analyzing a thin-edged projecting inlet.~~

~~Use file 2, block 5 if analyzing an inlet with square edges in a headwall.~~

~~Use file 2, block 7 if analyzing a groove end projecting inlet.~~

~~Use file 2, block 8 if analyzing a groove end inlet and headwalls.~~

~~Use file 2, block 6 if analyzing a beveled inlet.~~

~~Use file 2, block 9 if analyzing a tapered inlet throat. (Smooth inlet)~~

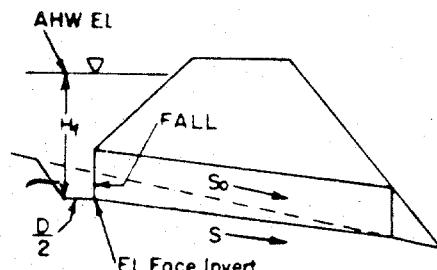
~~Use file 2, block 10 if analyzing a tapered inlet throat. (Rough inlet)~~

Enter: 1. AHW Elev. = 100

2. El. Stream bed at face = 92.5

3. B = 7 (D, if pipe)

4. D = 6



CONVENTIONAL or BEVELED

Q	5. (Enter) Q/N	(Read) El. Face invert	(Read) FALL	(Read) HW _f	Note: Use Upper headings for Conventional or beveled face: Lower headings for tapered inlet throat. COMMENTS
		El. Throat invert	HW _t		
Program No.	<u>1-5</u>		Inlet and Edge Description	<u>SQ. EDGES w/ HEADWALLS</u>	
350	350	92.50	0.00	99.91	DRAW PERFORMANCE CURVES
300	300			99.07	
400	400			100.81	
500	500			102.88	
Program No.	<u>1-6</u>		Inlet and Edge Description	<u>45° BEVELS</u>	
360	350	92.50	0.00	99.30	USE
300	300			98.55	DRAW PERFORMANCE CURVE
400	400			100.08	
500	500			101.79	TRY SIDE-TAPERED INLET

Note: Plot inlet control section performance curve

STEP 5

INLET CONTROL CALCULATIONS AND PERFORMANCE CURVE DATA

(BOX CULVERTS)

Use file 1, block 5 if analyzing a square-edge inlet with headwalls.

Use file 1, block 6 if analyzing a 45° beveled inlet.

Use file 1, block 7 if analyzing a tapered inlet throat.

(PIPE CULVERTS)

Use file 2, block 4 if analyzing a thin-edged projecting inlet.

Use file 2, block 5 if analyzing an inlet with square edges in a headwall.

Use file 2, block 7 if analyzing a groove end projecting inlet.

Use file 2, block 8 if analyzing a groove end inlet and headwalls.

Use file 2, block 6 if analyzing a beveled inlet.

Use file 2, block 9 if analyzing a tapered inlet throat. (Smooth inlet)

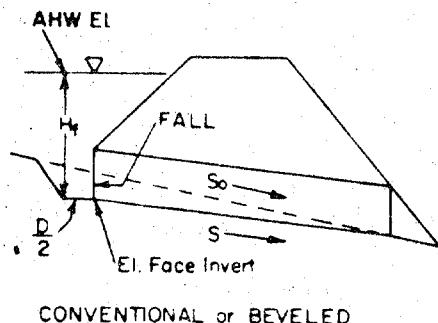
Use file 2, block 10 if analyzing a tapered inlet throat. (Rough inlet)

Enter: 1. AHW Elev. = 100

2. El. Stream bed at face = 92.5

3. B = 7 (D, if pipe)

4. D = 6



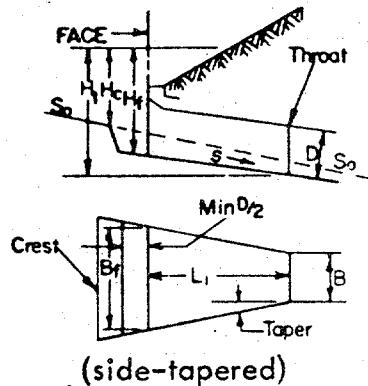
Q	5. (Enter) Q/N	(Read) El. Face invert	(Read) FALL	(Read) HW _f	Note: Use Upper headings for Conventional or beveled face; Lower headings for tapered inlet throat. COMMENTS
		El. Throat invert	HW _t		
Program No. <u>1-7</u>			Inlet and Edge Description <u>TAPERED INLET</u>		
<u>350</u>	<u>350</u>	<u>92.50</u>	<u>0.00</u>	<u>98.89</u>	<u>DRAW CURVE</u>
<u>300</u>	<u>300</u>			<u>98.26</u>	
<u>400</u>	<u>400</u>			<u>99.50</u>	
<u>500</u>	<u>500</u>			<u>100.70</u>	
Program No. <u> </u>		Inlet and Edge Description <u> </u>			

Note: Plot inlet control section performance curve

STEP 6 & 7
SIDE-TAPERED INLET AND CREST CHECK

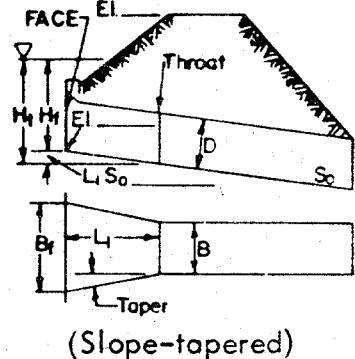
(BOX CULVERTS)

Use file 1, block 8 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides. (Favorable face edge conditions)
 Use file 1, block 9 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)



(PIPE CULVERTS)

Use file 2, block 11 if the face has projecting thin edges.
 Use file 2, block 12 if the face has square edges in a headwall.
 Use file 2, block 13 if the face has bevels or a groove end.



(CREST CHECK)

Use file 1, block 13 for crest check on a conventional, beveled or side-tapered inlet.

Enter: 1. $HW_f = 100$

2. EI . Throat Invert = 92.5

3. $(Taper + S) = 4.05$ (Taper is 4:1 to 6:1), ($S \approx S_o - \text{FALL} / L_a$)

4. $N \times B = 7$ ($N \times D$ for pipe)

5. $Q = 445$ FROM PERFORMANCE CURVE

6. $D = 6$ (E for pipe, where $D \leq E \leq 1.1 D$)

(4) (Read) Min. B_f	B_f Used	(Read) L_1	(Read) EI . face invert	COMMENTS
10.86	11.00	8.0	92.90	FACE DESIGNED FOR LARGER FLOWRATE.

(4) To use a B_f that is rounded off enter new B_f and press START STOP RECOMPUTE OUTLET CONTROL PERFORMANCE CURVE FOR CULVERT Enter: (Crest Check) WITH ADDITIONAL 8 FEET AND AN IMPROVED INLET.
 $L_a = 358$, $K_e = .2$

1. $Q =$ 2. $N =$ 3. $HW_f =$ 4. $W =$

5. $B =$ 0 6. $L_1 =$ 0 7. Taper = 0

Crest Check: (Read) $H_c =$ _____, (Read) Max. Crest $EI. =$ _____

STEP 3

OUTLET CONTROL PERFORMANCE CURVE DATA

Use file 1, block 3 if designing a box culvert

~~Use file 2, block 2 if designing a pipe culvert~~

ENTER: 1. $L_a = \underline{358}$
 2. $n = \underline{0.012}$ (Barrel)
 3. $k_e = \underline{0.2}$
 4. $B = \underline{7}$ (for box only)
 5. $D = \underline{6}$
 6. Elev. outlet invert = 75

READJUSTED FOR
NEW L_a , k_e

7. (2) (Enter) TW	8. (3) (Enter) d_c - pipe only	9. (Enter) Q/N	(Read) HW _o	COMMENTS
2.28	—	350	81.80	
2.15	—	300	81.15	
2.47	—	400	82.51	
2.76	—	500	84.11	DRAW PERFORMANCE CURVE

Note: Plot outlet control performance curve

(2) Obtain values from Step 1

(3) d_c obtained from Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 4

OUTLET VELOCITY WHEN CULVERT IS IN OUTLET CONTROL

If designing a Box Culvert

Use file 1, block 4

Enter: 1. TW = 2.58 @ 445 cfs
 2. D = 6
 3. B = 7
 4. Q/N = 445

(Read):
Velocity
12.67

~~If designing a pipe culvert~~

~~Use file 2, block 3~~

Enter: 1. D = _____
 2. Q/N = _____
 3. Alpha = _____ (1.04 for RCP, 1.12 for CMP)
 4. TW = _____

(Read):
Velocity

STEP 13
OUTLET VELOCITY WHEN CULVERT IS IN INLET CONTROL

Use file 1, block 14 if designing a box culvert
 Use file 2, block 14 if designing a pipe culvert

Enter: 1. D = 6

2. B = 7 (Use D if designing a pipe)

3. n = 0.012

4. Q/N = 445

5. S = 0.05 = $(S_o - \text{FALL}/L_o)$

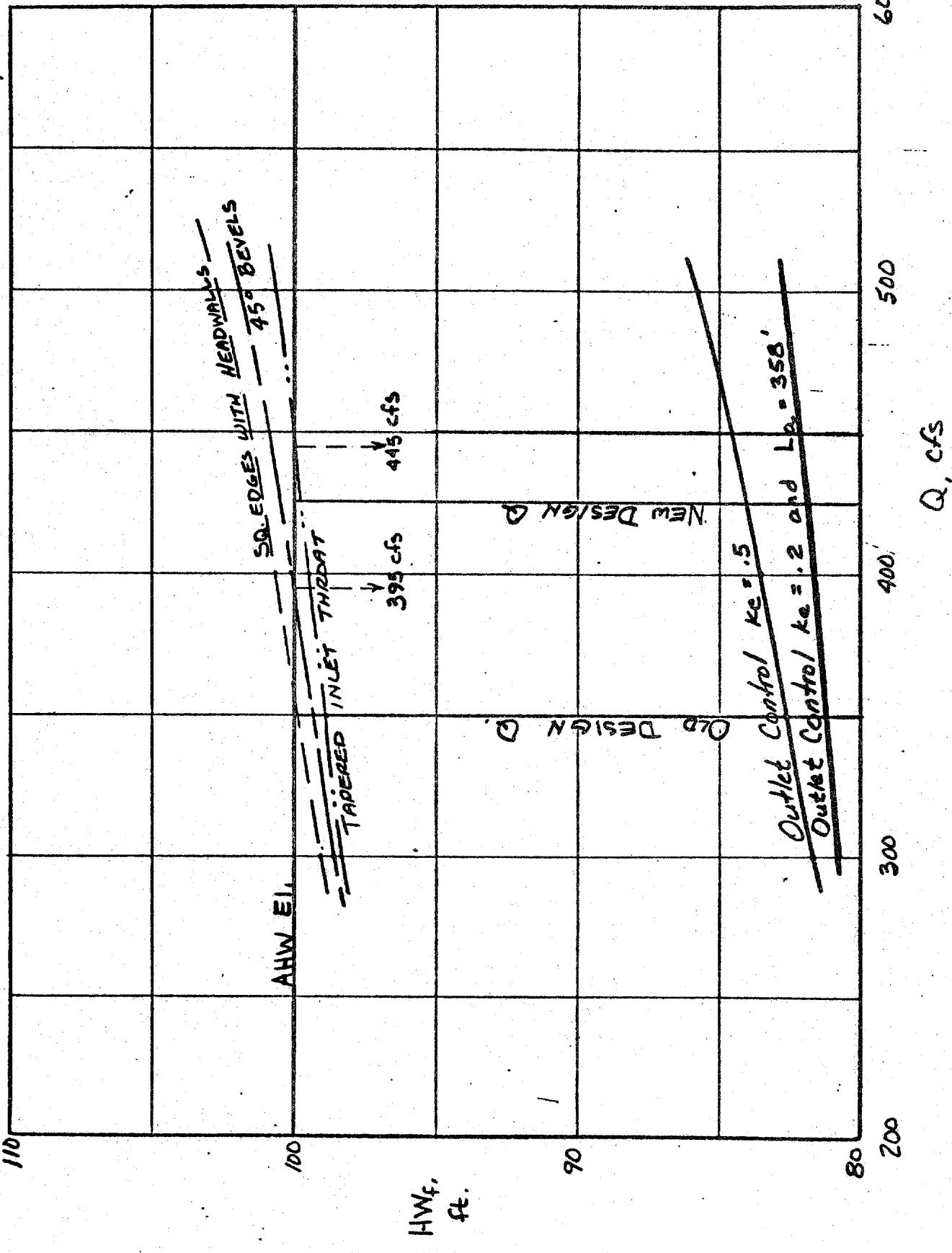
(READ) d_n/B	(READ) Velocity
.28	32.27

For Box Culvert

(READ) Velocity

For pipe culvert

DESIGN PERFORMANCE Curves 1-7'x6' REINF. CONC. BOX, zero fall



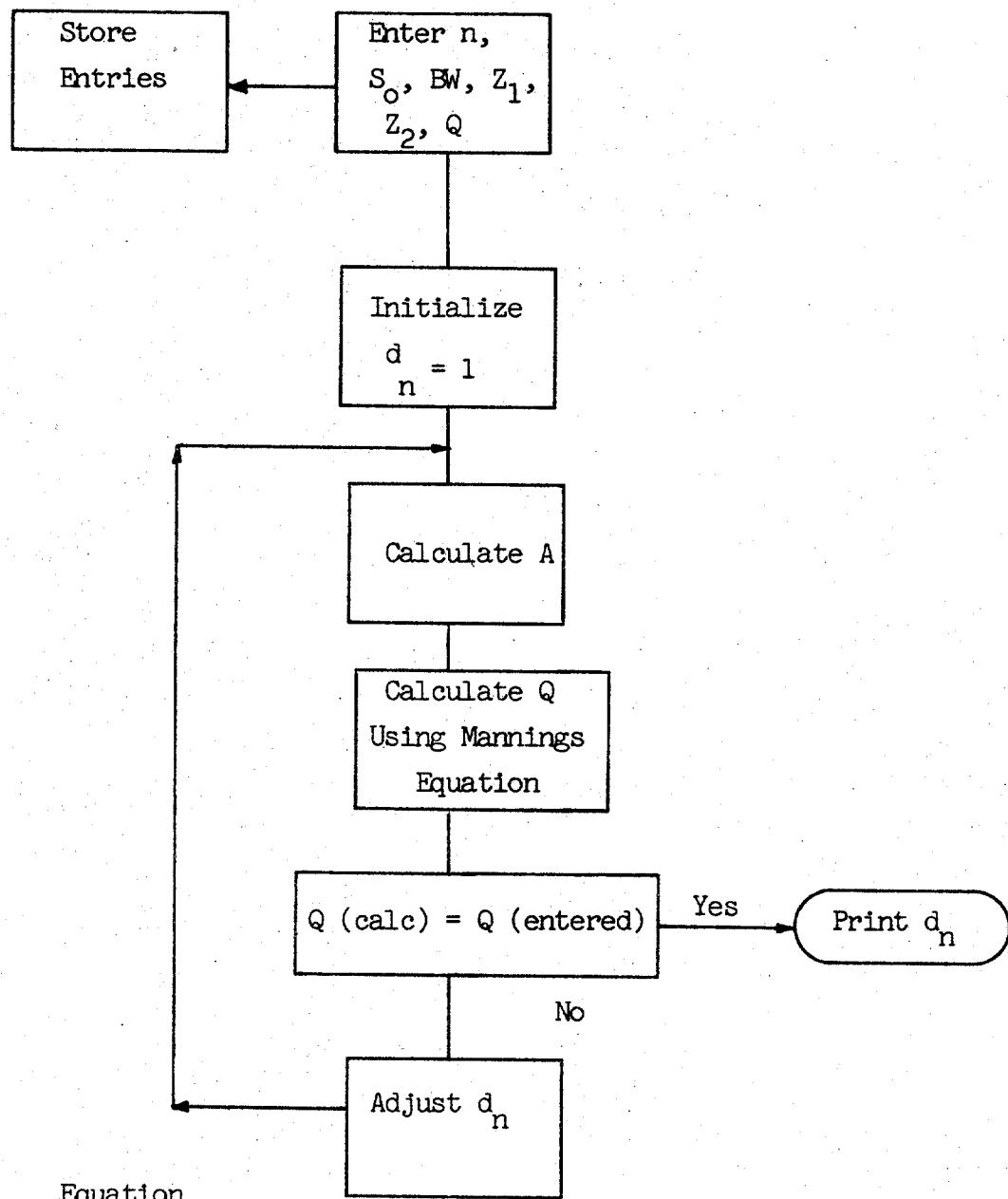
Conclusion - Example Problem No. 4

From the performance curves it can be seen that the addition of bevels does not satisfy the Q_{50} of 425 cfs at the AHW elevation. It is also seen that the addition of a side-tapered inlet increases the capacity of the culvert to 445 cfs at the AHW elevation of 100 feet. This increase is obtained with the side-tapered inlet built at the same slope as the existing barrel and channel. The side-tapered inlet is the least costly type of modification that will handle the increase flow.

EQUATIONS AND FLOW CHARTS

USED IN PROGRAMS

Program 1-1



$$Q = \frac{1.486}{n} AR^{2/3} S_o^{1/2} \quad (\text{Basic Equation})$$

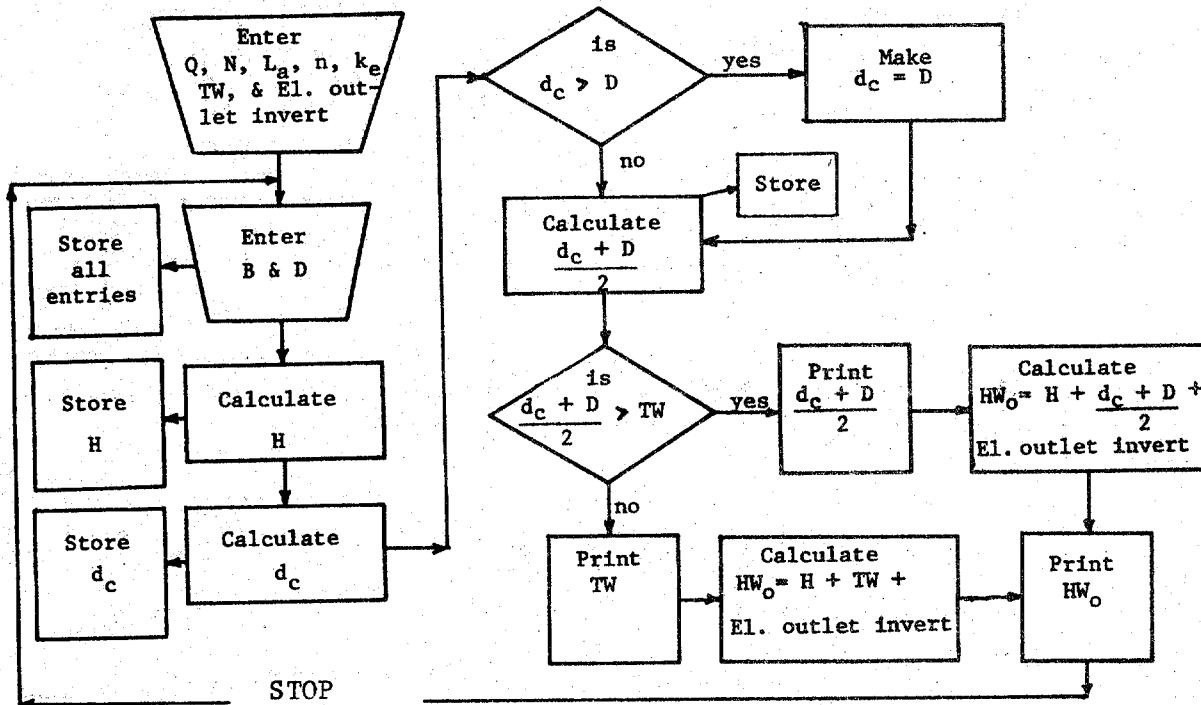
$$R = A/WP$$

$$A = BW d_n + \frac{1}{2} Z_1 d_n^2 + \frac{1}{2} Z_2 d_n^2$$

$$WP = BW + d_n \sqrt{Z_1^2 + 1} + d_n \sqrt{Z_2^2 + 1}$$

d_n is calculated to $\pm .0001$

Program 1-2



$$HW_o = H + h_o + \text{Elev. Outlet invert} \quad (\text{Basic Equation}) \quad (2)$$

where

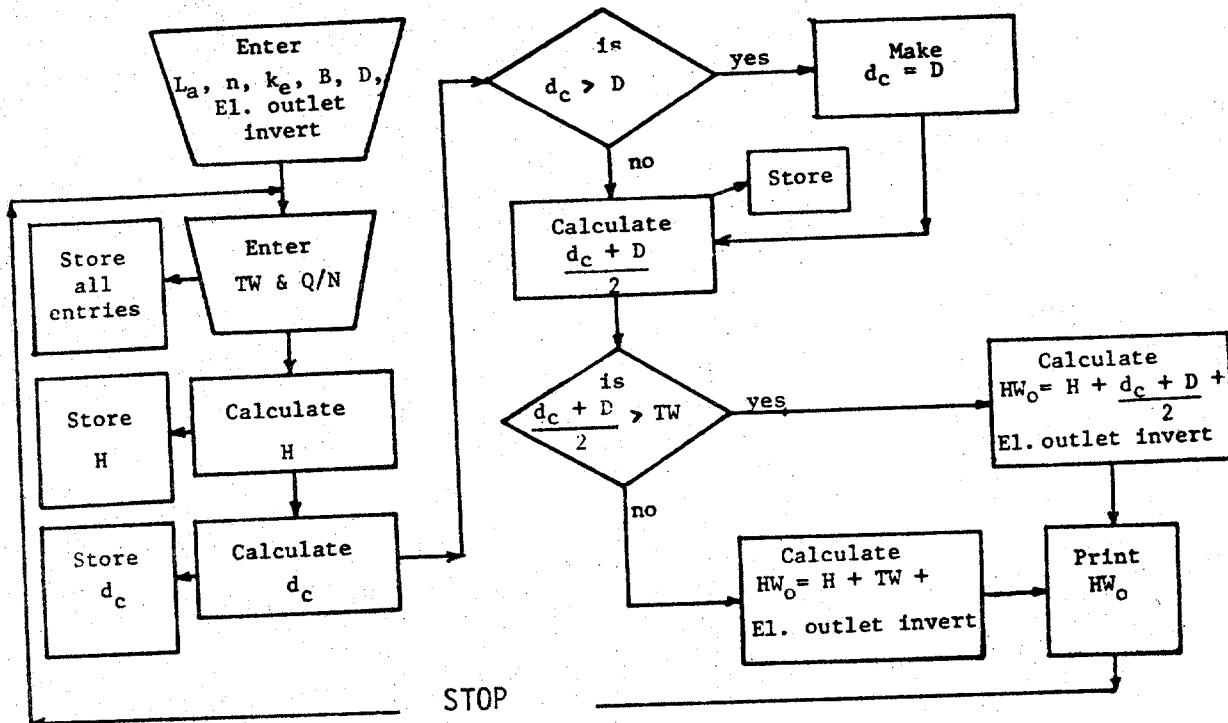
$$H = \left[n + k_e + \frac{29n^2 L_a}{BD} \left(\frac{1.33}{2(B+D)} \right) \right] \frac{(Q/NBD)^2}{64.4} \quad (2)$$

$$h_o = \frac{d_c + D}{2} \text{ or } TW, \text{ whichever is greater} \quad (2)$$

$$\text{and } d_c = 0.315 \left(\frac{Q}{NB} \right)^{2/3} \quad (2)$$

Note: d_c cannot exceed D

Program 1-3



$$HW_o = H + h_o + \text{Elev. Outlet invert} \quad (\text{Basic Equation}) \quad (2)$$

where

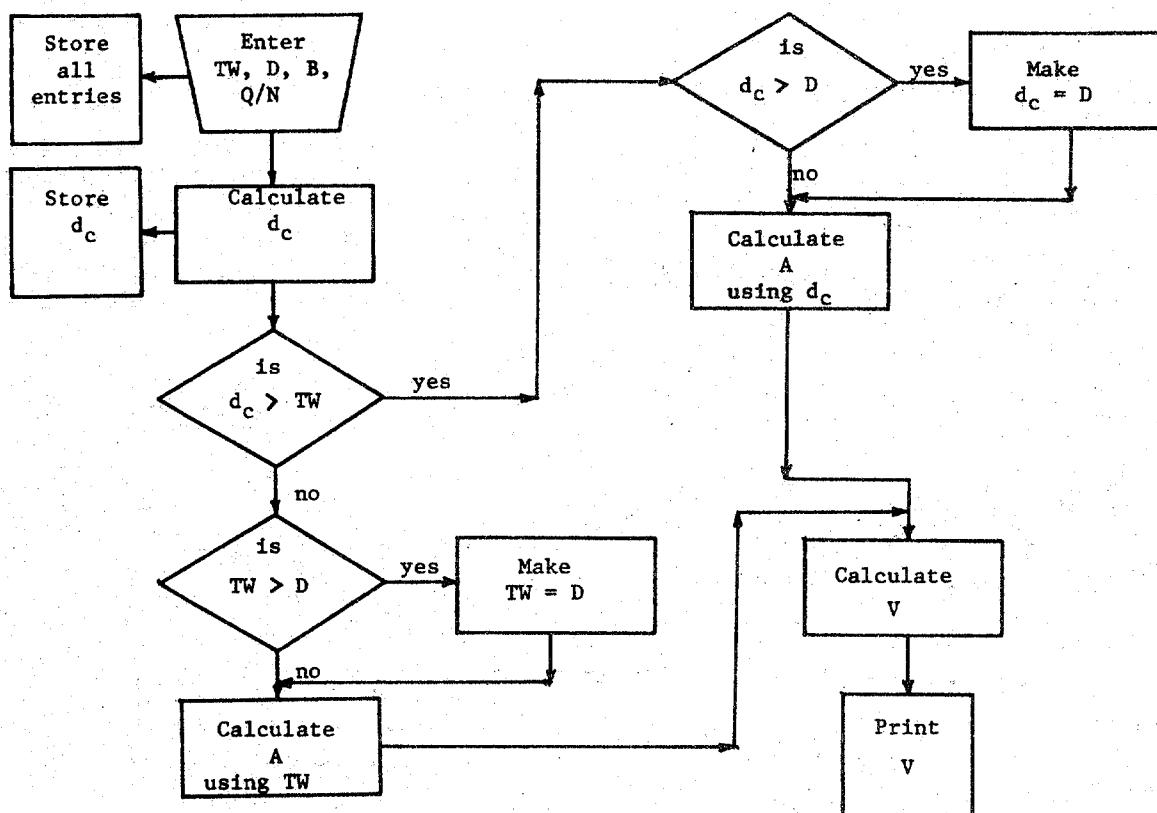
$$H = \left[1 + k_e + \frac{29n^2 L_a}{BD} \right] \frac{(Q/NBD)^2}{1.33} \quad (2)$$

$$h_o = \frac{d_c + D}{2} \text{ or } TW, \text{ whichever is greater} \quad (2)$$

$$\text{and } d_c = 0.315 \left(\frac{Q}{NB} \right)^{2/3} \quad (2)$$

Note: d_c cannot exceed D

Program 1-4



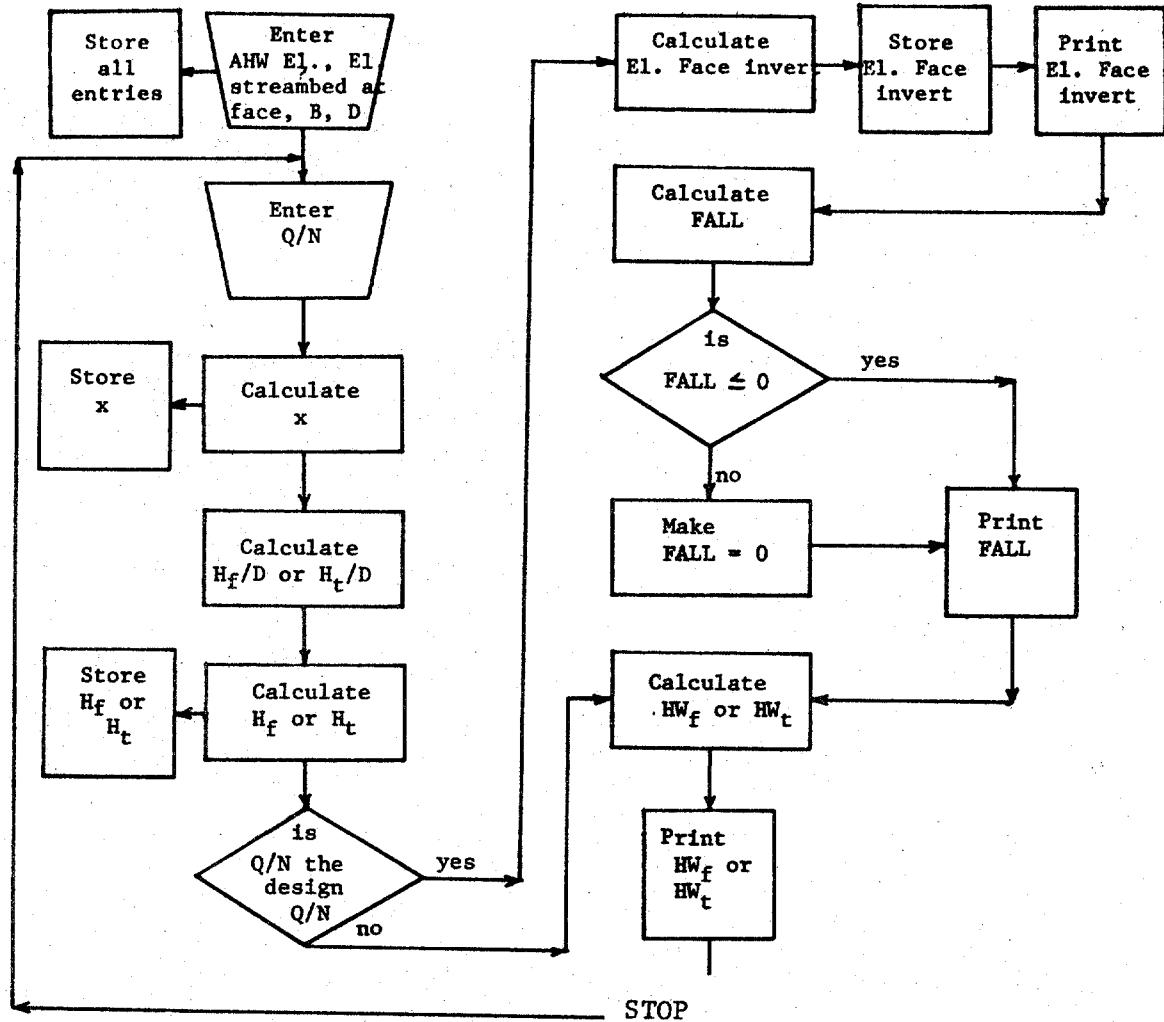
$$V = \frac{Q}{A \times N} \text{ and } A = B \times \text{depth of water, } (d_c, TW, \text{ or } D)$$

$$d_c = 0.315 \left(\frac{Q}{N} \right)^{2/3}$$

TW is based on program #1

To find area use d_c or TW, whichever is greater, but not to exceed D

Program 1-5, 1-6, & 1-7



(Square edge in headwall)

$$\frac{H_f}{D} = .122117 + .505435x - .10856x^2 + .0207809x^3 - .00136757x^4 + .00003456x^5 \quad (3)$$

(45° Bevels)

$$\frac{H_f}{D} = .1566086 + .3989353x - .0640392x^2 + .01120135x^3 - .0006449x^4 + .000014566x^5 \quad (4)$$

(Tapered inlet throat)

$$\frac{H_t}{D} = .1295033 + .3789445x - .0437778x^2 + .00426329x^3 - .000106358x^4 \quad (4)$$

Where $x = \frac{Q}{NBD^{3/2}}$ and

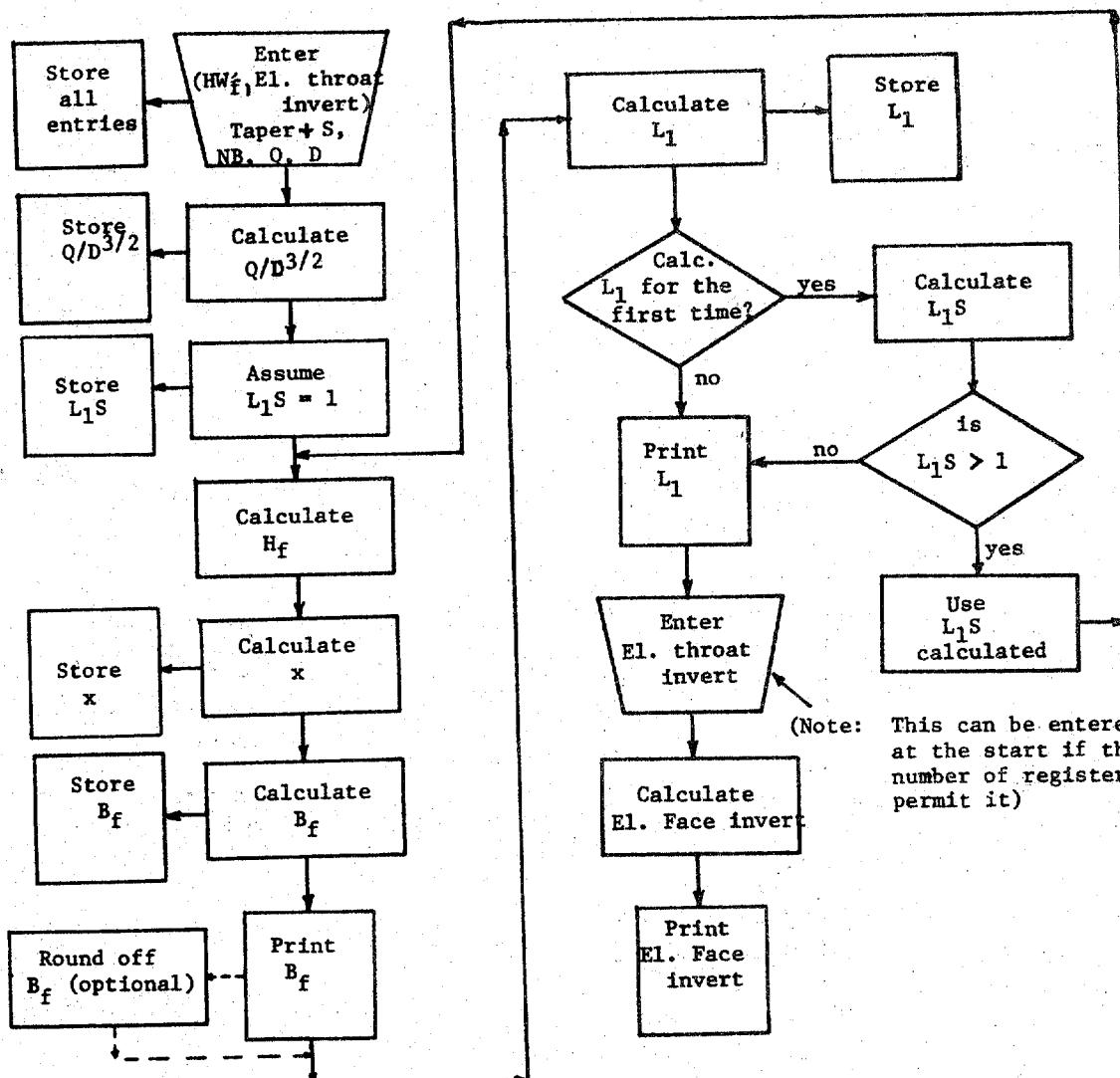
$$AHW \text{ Elev.} - H_f = \text{Elev. face invert}$$

$$(AHW \text{ ELEV.} - H_f) - \text{Elev. Streambed at face} = \text{FALL}$$

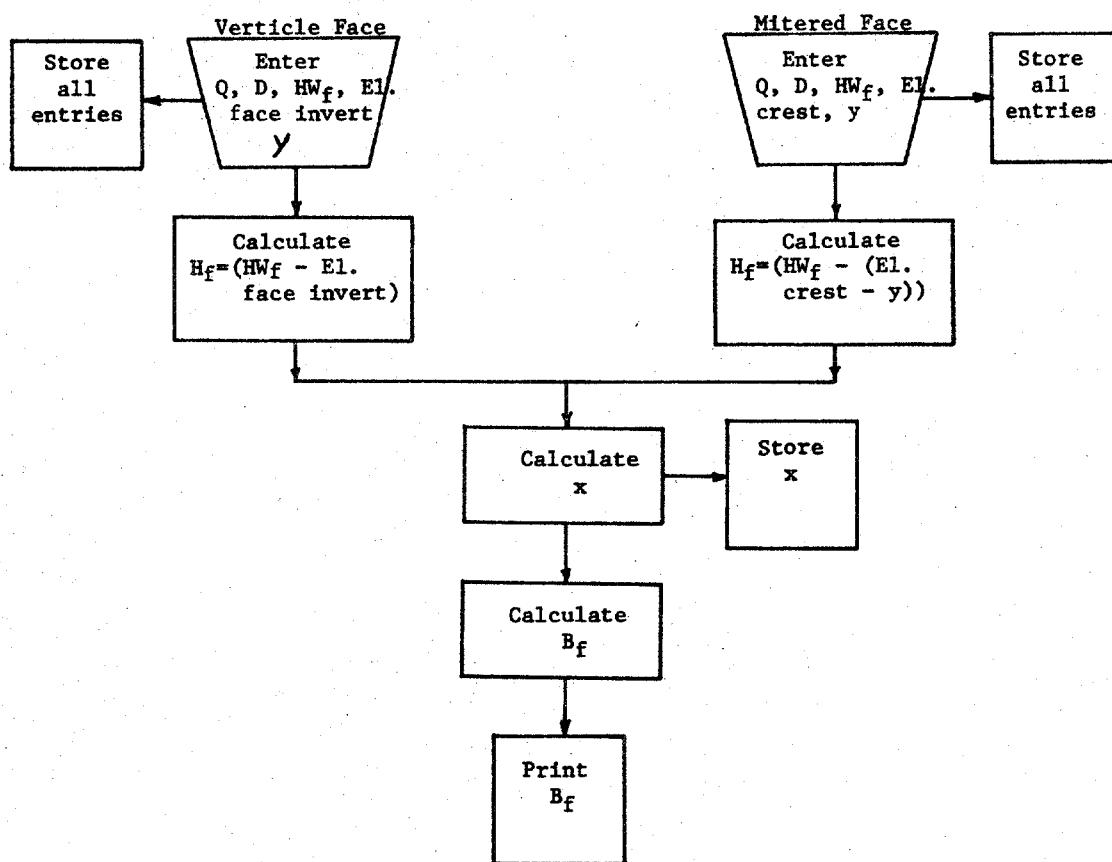
$$\text{Elev. face invert} + H_f = H_w$$

(Same procedure for H_t)

Program 1-8, 1-9



Program 1-10, 1-11



(Solid Curve - Favorable edges)

$$B_f = \frac{Q}{D^{3/2}} [-2.265863 + 7.942441x - 4.0352094x^2 + 1.619481x^3 - .3458214x^4 + .028146767x^5]$$

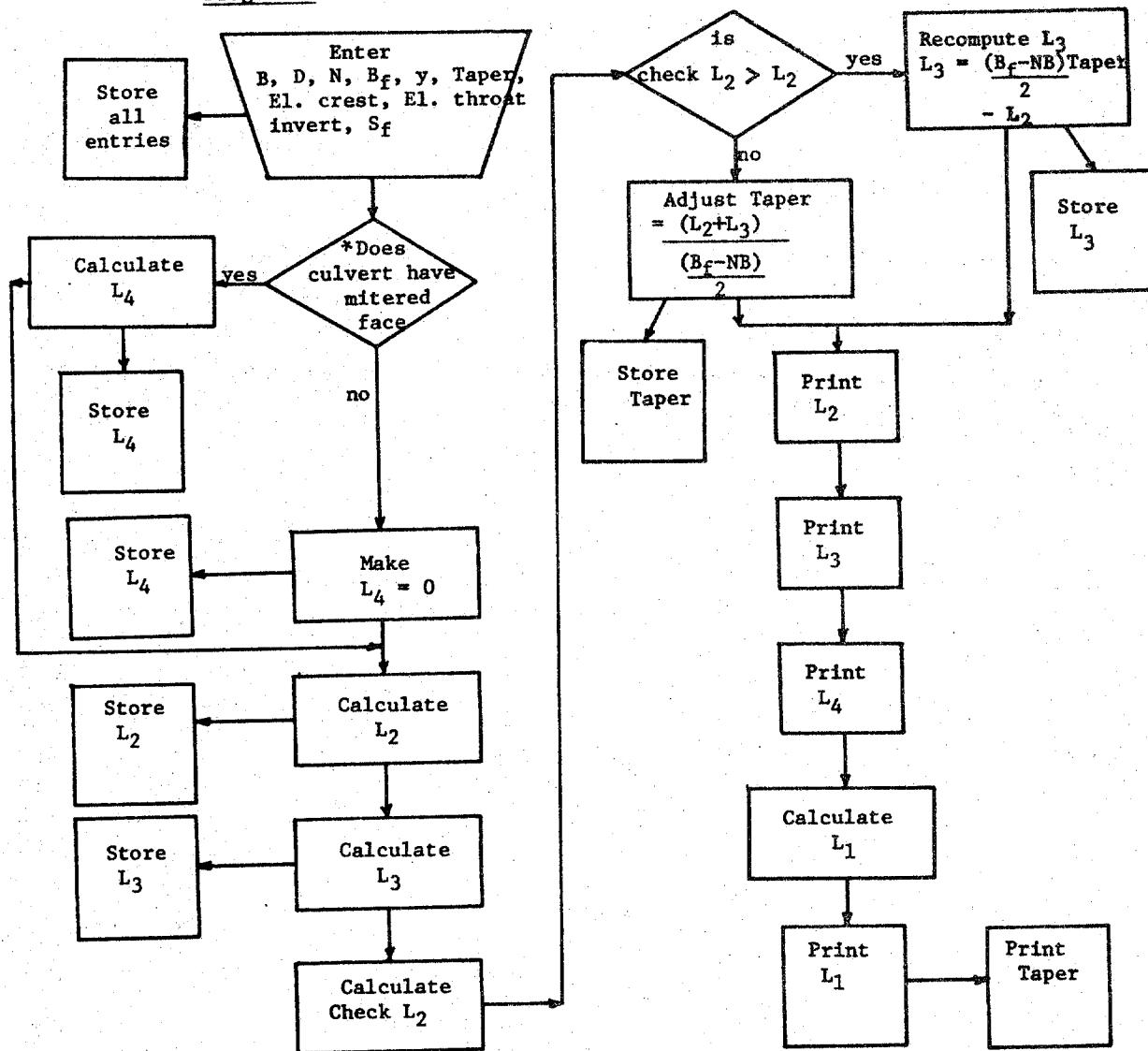
(Dashed Curve - Unfavorable edges)

$$B_f = \frac{Q}{D^{3/2}} : [-1.353 + 5.150x - 1.131x^2 + .1578x^3 - .0144x^4 + .0011x^5](4)$$

where $x = H_f/D$; $H_f = (HW_f - El. face invert)$ for verticle face

$H_f = (HW_f - (El. crest - y))$ for mitered face

Program 1-12



$$\text{Min } L_3 = 0.5NB \quad (5)$$

$$L_4 \approx S_f y + D/S_f \quad (5)$$

$$L_2 \approx (\text{El. Crest Invert} - \text{El. Throat Invert})S_f - L_4 \quad (5)$$

$$L_1 = L_2 + L_3 + L_4 \quad (5)$$

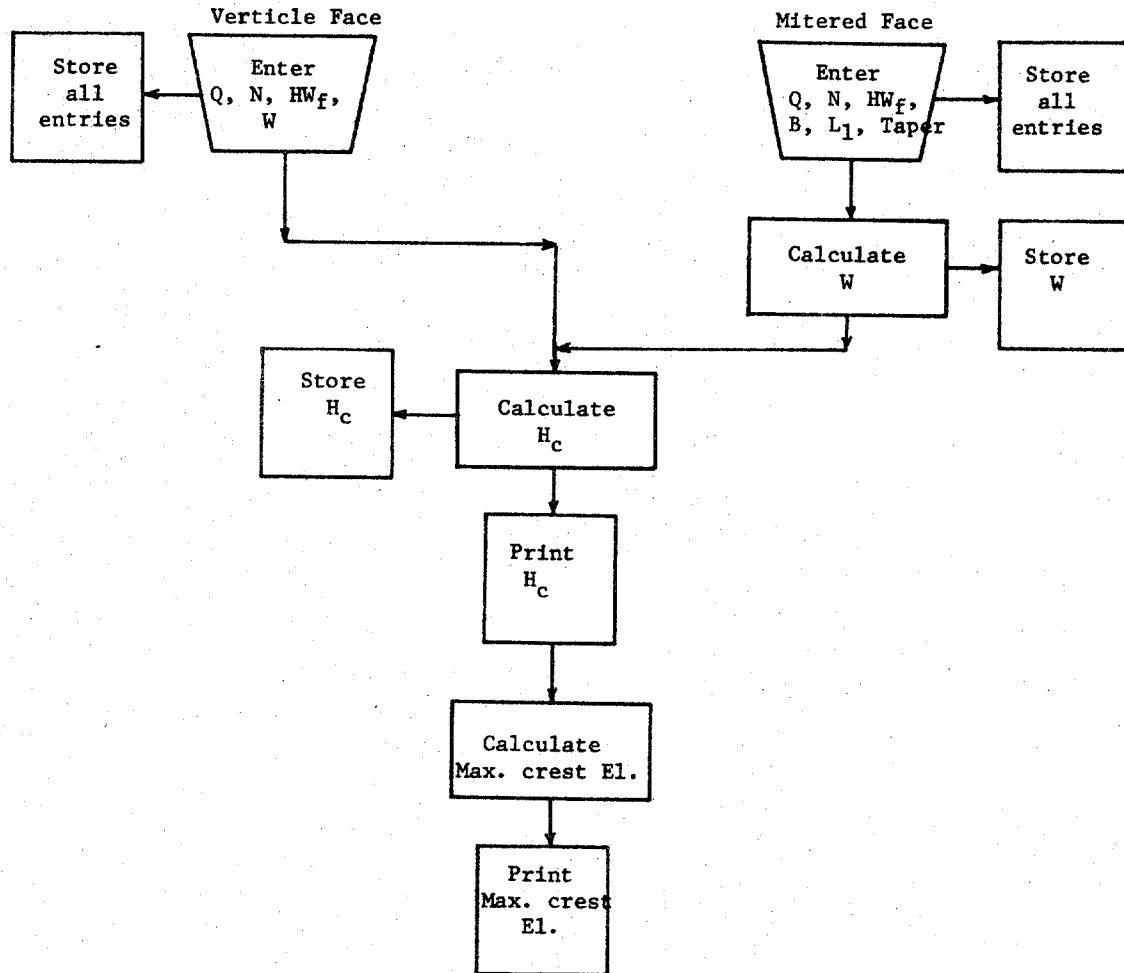
$$\text{Check } L_2 = \frac{[B_f - Nx_B]}{2} \text{ TAPER} - L_3$$

Note: If $\text{check } L_2 > L_2$, adjust $L_3 = \frac{[B_f - Nx_B]}{2} \text{ TAPER} - L_2$

If $L_2 > \text{check } L_2$, adjust TAPER = $(L_2 + L_3) / \frac{[B_f - Nx_B]}{2}$

* Can use a conditional jump: Y = 0 for verticle face
Y is positive for mitered face

Program 1-13



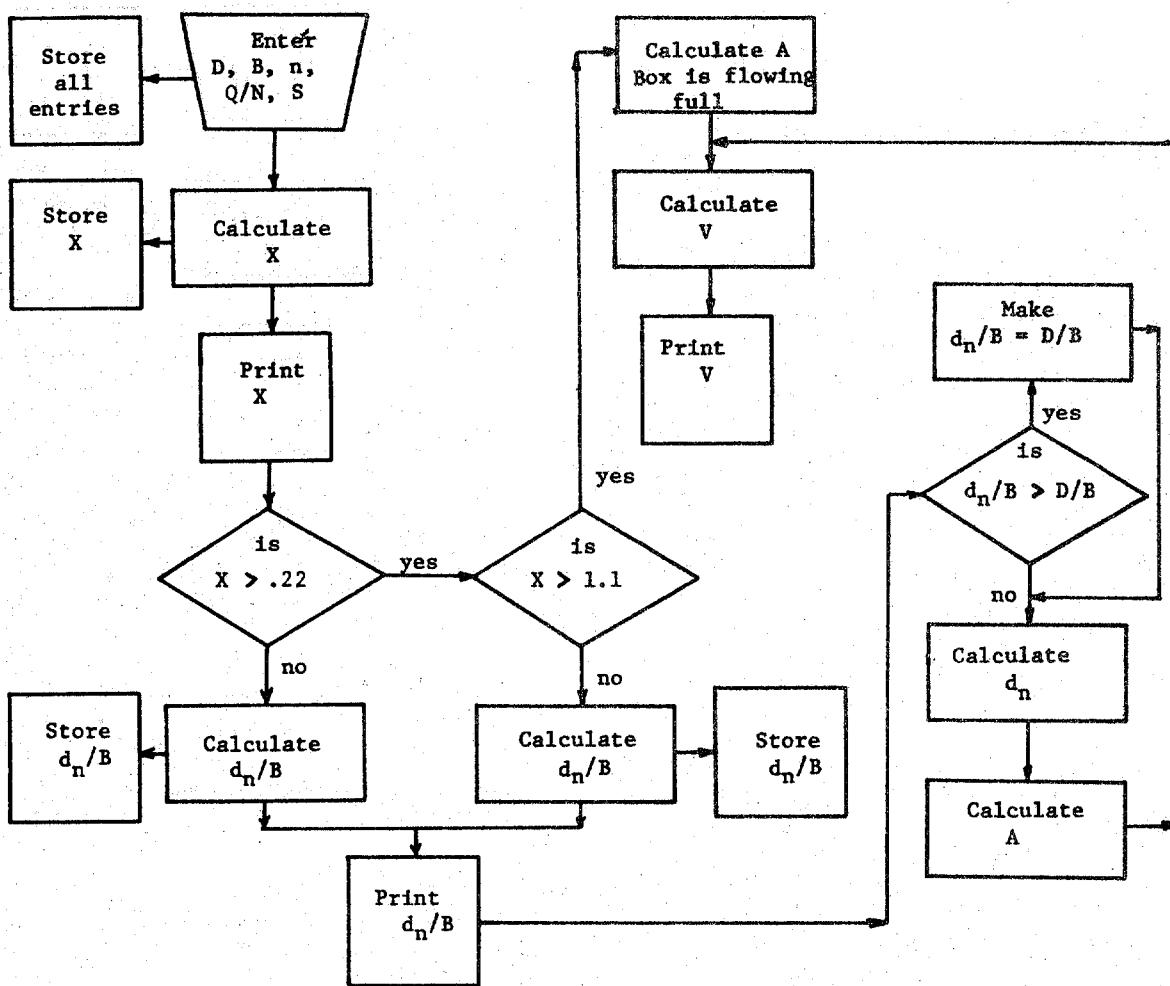
$$H_c = 0.50 \left(\frac{Q}{W} \right)^{2/3} \quad (5)$$

$$\text{Max. Crest Elev.} = HW_f - H_c \quad (5)$$

$W = NB + 2 [L_1/\text{Taper}]$ for mitered face slope-tapered inlet (5)

$W \approx 10 \text{ times FALL}$ for side-tapered inlet

Program 1-14



$$X = \frac{Qn}{\frac{1.486 S^{1/2} N}{B^{2.667}}}$$

(8)

if $X > 1.1$, velocity = $\frac{0}{BxDxN}$

if $.22 < X \leq 1.1$, velocity = $\frac{Q}{Bx_n xN}$

$$\text{and } \frac{d_n}{B} = .084468 + 2.34061X - 1.53643X^2 + 1.636594X^3 - .677621X^4$$

if $X \leq .22$, Velocity = $\frac{Q}{Bx d_n x N}$

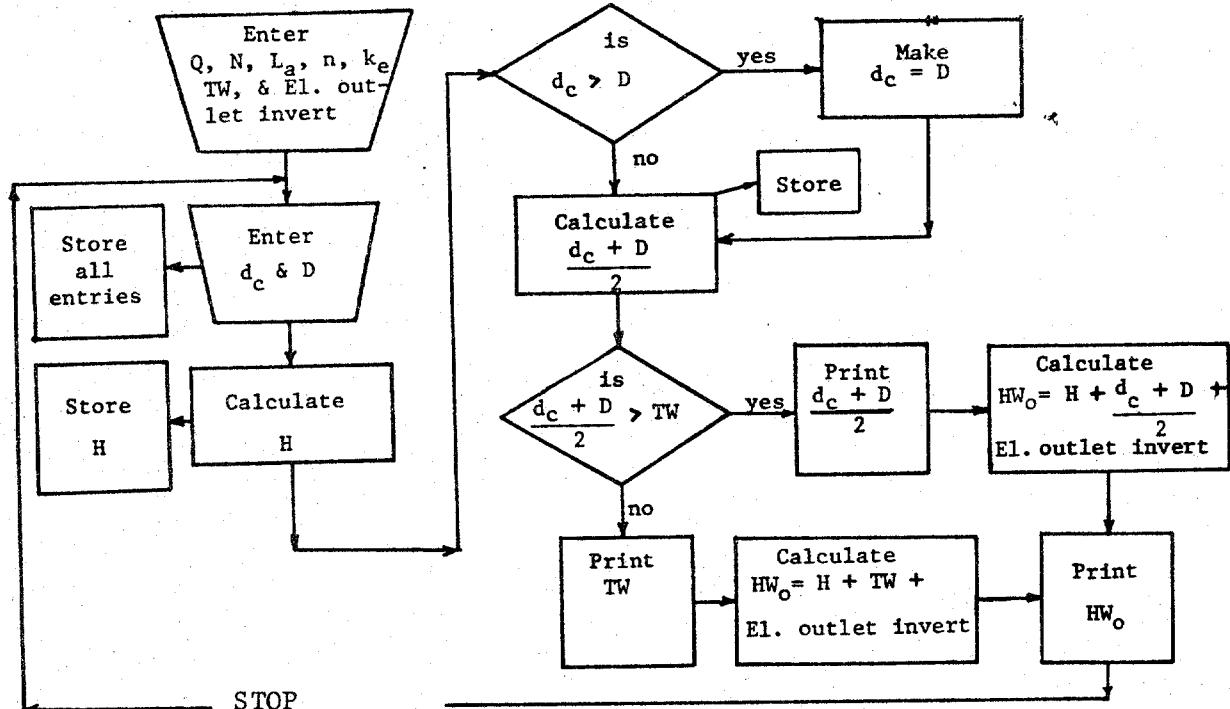
$$\text{and } \frac{d_n}{B} = .036402 + 3.6483784X - 15.152238X^2 + 64.991913X^3 - 110.31635X^4$$

$$d_n = \frac{d_n}{B} \times B$$

$$\frac{d_n}{B} \text{ is limited to } 2 \quad A = Bxd_n \quad V = 0/A$$

Note: d_n cannot exceed D

Program 2-1



$$HW_o = H + h_0 + El. \text{ Outlet Invert} \quad (\text{Basic Equation})$$

$$\text{Where } H = \left[1 + k_e + \frac{29n^2 L_a}{(D/4)1.33} \right] \frac{\left(\frac{Q/N\pi D^2}{4}\right)^2}{64.4} \quad (2)$$

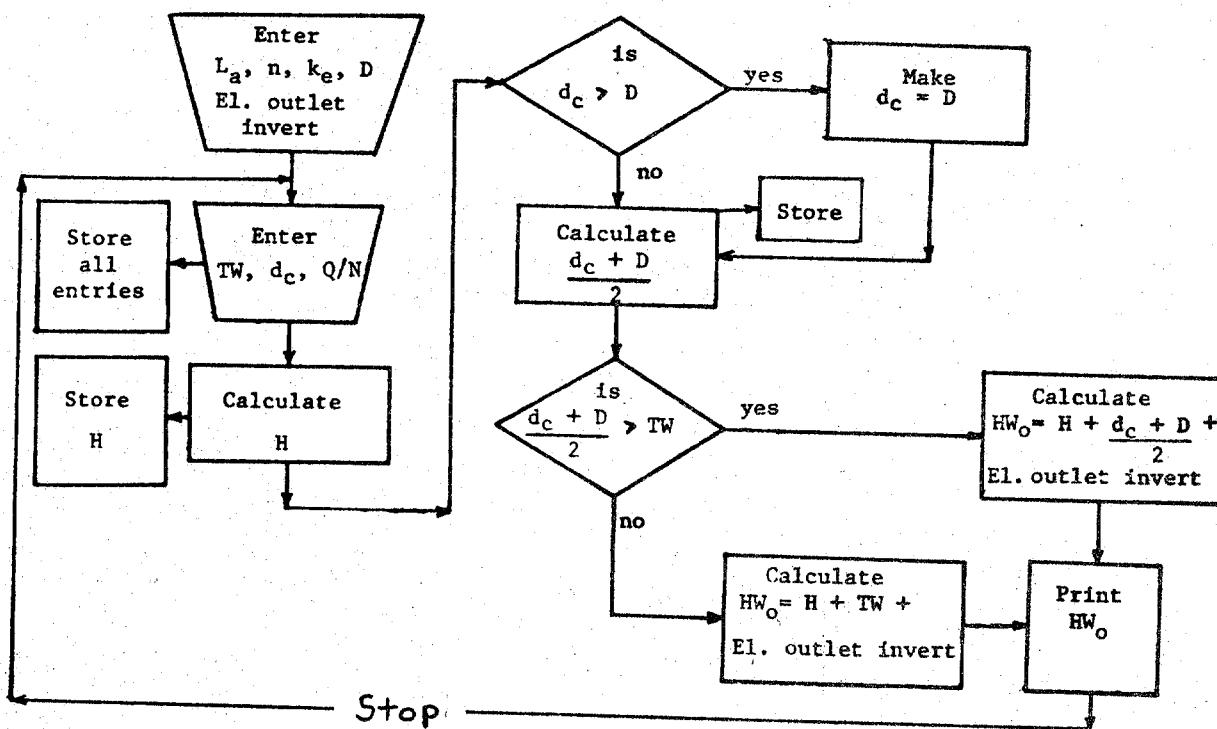
$$h_0 = \frac{d_c + D}{2} \text{ or } TW, \text{ whichever is greater}$$

d_c must be read from charts and entered into calculator.

However, if your calculator is large enough to calculate d_c then calculate it rather than enter it. Program 2-3 calculates d_c .

Note: d_c cannot exceed D

Program 2-2



$$HW_o = H + h_0 + El. Outlet Invert \quad (\text{Basic Equation})$$

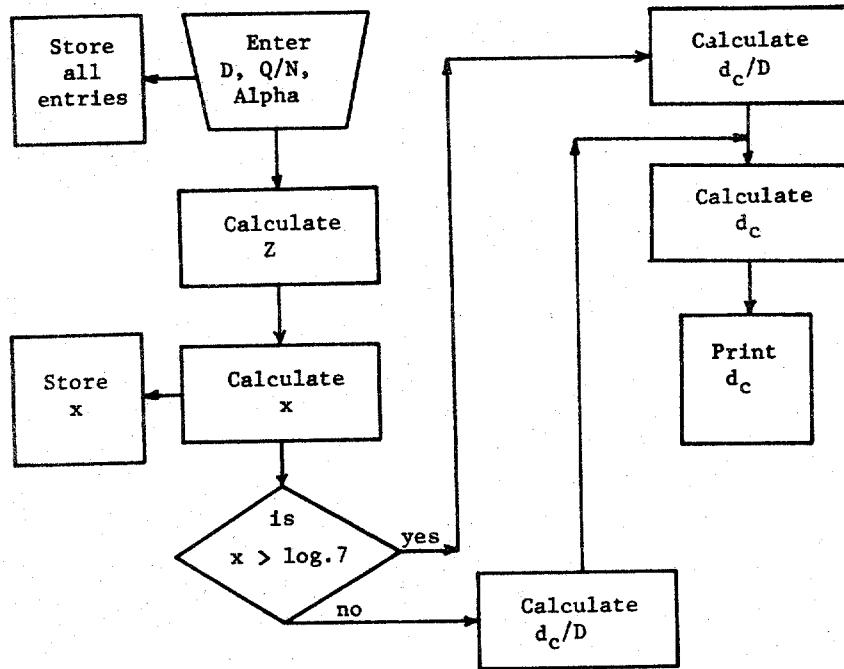
$$\text{Where } H = \left[1 + k_e + \frac{29n^2 L_a}{(D/4)^1.33} \right] \left(\frac{Q/N \pi D^2}{4} \right)^2 \quad (2)$$

$$h_0 = \frac{d_c + D}{2} \text{ or } TW, \text{ whichever is greater}$$

d_c must be read from charts and entered into calculator. However, if your calculator is large enough to calculate d_c then calculate it rather than enter it. Program 2-3 calculates d_c .

Note: d_c cannot exceed D

Program 2-3



$$Z = \frac{Q}{N \left(\frac{32.2}{\alpha} \right) \cdot 5} \cdot \frac{1}{D^{2.5}}$$

$$x = \log Z$$

if $x > \log .7$

$$\frac{d_c}{D} = 10 \left(-.0244603 + .2017057X - .64009815X^2 - .695619X^3 \right)$$

if $x \leq \log .7$

$$\frac{d_c}{D} = 10 \left(-.0051657 + .407362X - .1830236X^2 - .0915565X^3 \right)$$

$$d_c = \frac{d_c}{D} \times D$$

Program 2-4, 2-5, 2-6, 2-9, & 2-10

Use same flow chart as programs #4a, #4b and #5, except enter D for B in addition to entering D at its regular place.

(Thin Edged Projecting)

$$\frac{H_f}{D} = \frac{.187321 + .56771x - .156544^2 + .0447052x^3}{-.00343602x^4 + .000089661x^5} \quad (6)$$

(Headwall - Sq. Edges)

$$\frac{H_f}{D} = \frac{.087483 + .706578x - .253295x^2 + .0667001x^3}{-.00661651x^4 + .000250619x^5} \quad (6)$$

(Beveled edge)

$$\frac{H_f}{D} = \frac{.063343 + .766512x - .316097x^2 + .0876701x^3}{-.00983695x^4 + .00041676x^5} \quad (6)$$

(Tapered inlet throat - Smooth inlet)

$$\frac{H_t}{D} = \frac{.2115 + .3927x - .0414x^2 - .0042x^3 + .0003x^4 - .00003x^5}{.0011x^3 + .0005x^4 - .00003x^5} \quad (7)$$

(Tapered inlet throat - Rough inlet)

$$\frac{H_t}{D} = \frac{.2252 + .3471x - .0252x^2}{.0011x^3 + .0005x^4 - .00003x^5} \quad (7)$$

Where $x = \frac{Q}{ND^{5/2}}$ and

AHW Elev. - H_f = Elev. face invert

(AHW Elev. - H_f) - Elev. Streambed at face = FALL

Elev. face invert + H_f = HW_f

(Same procedure for H_t)

Program 2-7 & 2-8

Use same flow chart as programs 1-5, 1-6 and 1-7 except enter D for B in addition to entering D at its regular place.

(Groove - edged projecting)

$$\frac{H_f}{D} = \frac{.108786 + .662381x - .233801x^2 - .0579585x^3 + .0055789x^4}{-.000205052x^5} \quad (6)$$

(Groove - edged with headwalls)

$$\frac{H_f}{D} = \frac{.114099 + .653562x - .233615x^2 + .0597723x^3 + .006166338x^4}{+.000242832x^5} \quad (6)$$

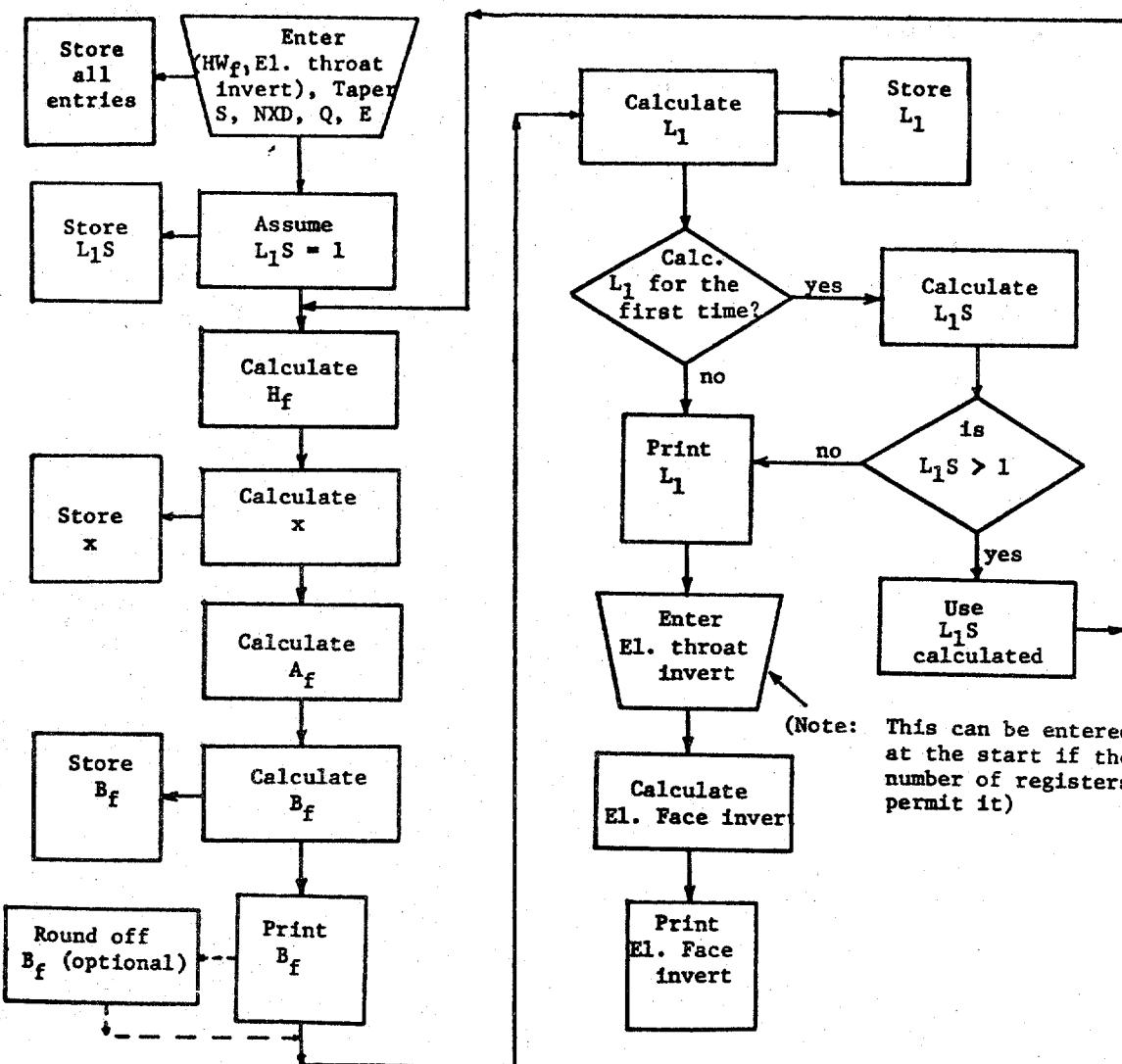
Where $x = \frac{Q}{ND^{5/2}}$ and

AHW Elev. - H_f = Elev. face invert

(AHW Elev. - H_f) - Elev. Streambed at face = FALL

Elev. face invert + H_f = HW_f

(Same procedure for H_t)



(Thin Edged Projecting)

$$A_f = \frac{Q}{E^{1/2}} \div [0.0144 + 1.1505x + 1.8167x^2 - .9642x^3 + .1974x^4 - .0148x^5] \quad (7)$$

(Headwall with Sq. Edges)

$$A_f = \frac{Q}{E^{1/2}} \div [-.0048 + .9426x + 2.9784x^2 - 1.792x^3 + .4228x^4 - .0357x^5] \quad (7)$$

(Beveled edge)

$$A_f = \frac{Q}{E^{1/2}} \div [0.0 + .73932x + 3.2994x^2 - 1.764x^3 + .3744x^4 - .0287x^5] \quad (7)$$

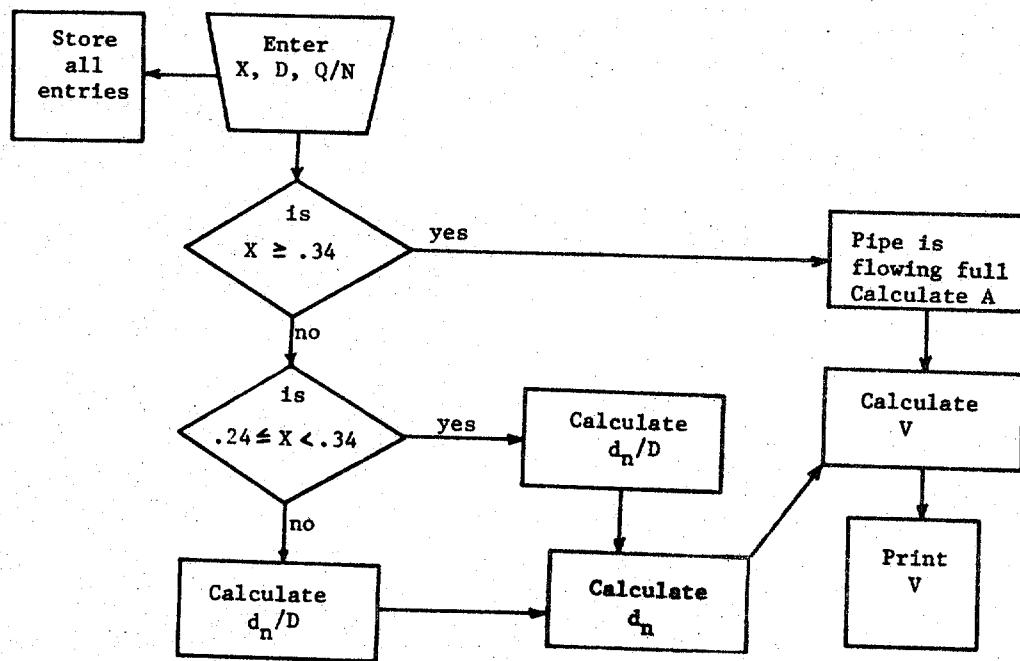
where $x = \frac{H_f}{E}$, $H_f = (HW_f - \text{Elev. Throat Inv.} - L_1S)$

$$B_f = \frac{4A_f}{\pi E} \quad \text{El. face invert} = \text{El. throat invert} + L_1S$$

$$L_1 = \frac{(B_f - NXD)\text{Taper}}{2} \quad S \approx S_0 - \text{FALL/L}_1$$

E is the height of the face of a side-tapered inlet.
It is usually equal to D, however, it can vary between D and 1.1D.

Program 2-14



$$X = \frac{Qn}{1.486 S^{1/2} N} B^{2.667} \quad (\text{computed by program #11a}) \quad (8)$$

$$Z = \log X$$

$$\text{if } .24 \leq .34, \frac{d_n}{D} = 10(.685734 + 2.097532z + 1.125836z^2)$$

$$\text{if } X < .24, \frac{d_n}{D} = 10(.3063639 + .907884z + .192615z^2)$$

For $d_n > R$: ($R = D/2$)

$$A = \pi R^2 - (\pi R^2 \cos^{-1} (r/R)/180) + r(R^2 - r^2) \cdot 5$$

Otherwise:

$$A = (\pi R^2 \cos^{-1} (r/R)/180) + r(R^2 - r^2) \cdot 5$$

$$r = \text{ABS}(R - d_n)$$

REFERENCES

1. "Design Charts for Open Channel Flow" (HDS No. 3), Hydraulics Branch, Bridge Division, FHWA, Washington, D.C.; August 1961.
2. "Hydraulic Charts for the Selection of Highway Culverts" (HEC No. 5), Hydraulics Branch, Bridge Division, FHWA, Washington, D.C.; December 1965.
3. "Electronic Computer Program for Hydraulic Analysis of Box Culverts" (Program HY-3), Office of Development, FHWA, Washington, D.C.; December 1970.
4. Equations Derived by Mario Marques, Hydraulics Branch, Bridge Division, FHWA, Washington, D.C.; November 1972.
5. "Hydraulic Design of Improved Inlets for Culverts" (HEC No. 13), Hydraulics Branch, Bridge Division, FHWA, Washington, D.C.; November 1971.
6. "Electronic Computer Program for Hydraulic Analysis of Circular Culverts" (Program HY-1), Office of Research & Development, FHWA, Washington, D.C.; July 1970.
7. "New York State Improved Inlet Analysis," State of New York, Department of Transportation, Region #1, Albany, New York; January 1973.
8. "Open-Channel Hydraulics," V. T. Chow, McGraw-Hill Book Company, Inc., New York, New York; 1959.

WORKSHEET FOR CULVERT DESIGN

PROJECT: _____

DESIGNER: _____

STATION: _____

DATE: _____

INITIAL DATA

Design Q _____ = cfs Channel Slope, S_o = ft./ft.

AHW Elevation = ft. El. Stream bed at Face ft.

Approx. Culvert length, L_a ft. Barrel Shape _____

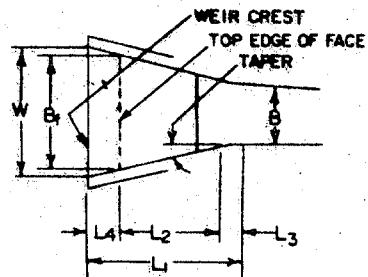
L_a ft. Barrel Material _____

El. Outlet Invert = ft. Barrel Roughness, n _____

(See page 2 for natural stream data)

SUMMARY INFORMATION FOR SELECTED DESIGN

Barrel Shape and Material _____



Face Edge Description _____

Type of Improved Inlet _____

Width of box, B = ft. Inlet length, L_1 = ft.

Depth or Diameter, D = ft. Face to Bend, L_2 = ft.

Width of face, B_f = ft. Bend to Throat, L_3 = ft.

No. of Barrels, N = Crest to Face, L_4 = ft.

Inlet fall, FALL = ft. Side Taper = :1

Barrel Slope, S = ft./ft. Crest Length, W = ft.

Top bevel height, d = in. Side bevel width, b = in.

Outlet velocity, V = ft./sec.

COMMENTS ON DESIGN: _____

STEP 1
CALCULATE TAILWATER

Use file 1, block 1

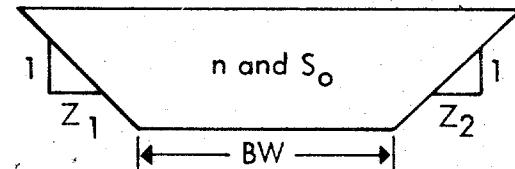
Enter: 1. $n =$ _____ (channel)

2. $S_o =$ _____

3. BW = _____

4. $Z_1 =$ _____

5. $Z_2 =$ _____



(Enter) 6. Q	(Read) TW, Based on d_n	COMMENTS

STEP 2
DETERMINE AN ACCEPTABLE CULVERT SIZE

Use file 1, block 2 if designing a box culvert.

Use file 2, block 1 if designing a circular pipe culvert.

Enter: 1. $Q =$ _____

2. $N =$ _____

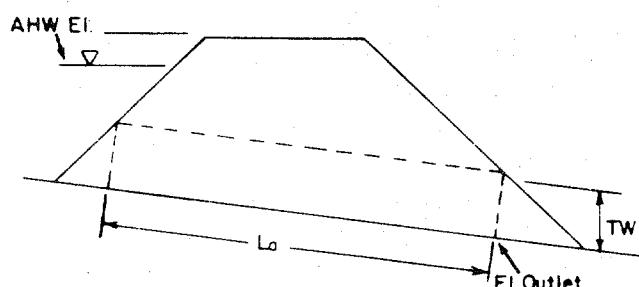
3. $L_a =$ _____

4. $n =$ _____ (Barrel)

5. $k_e =$ _____

6. $TW =$ _____

7. Elev. outlet invert = _____



(Enter) 8. B - If box (1) d_c - If pipe	(Enter) 9. D	(Read) $\frac{d_c + D}{2}$ or TW	(Read) H_w	COMMENTS

(1) d_c values taken from Design Charts For Open-Channel Flow,
Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 3

OUTLET CONTROL PERFORMANCE CURVE DATA

Use file 1, block 3 if designing a box culvert.

Use file 2, block 2 if designing a pipe culvert.

ENTER: 1. L_a = _____
 2. n = _____ (Barrel)
 3. k_e = _____
 4. B = _____ (for box only)
 5. D = _____
 6. Elev. outlet invert = _____

7. (2) (Enter) TW	8. (3) (Enter) d_c - pipe only	9. (Enter) Q/N	(Read) H_w	COMMENTS

Note: Plot outlet control performance curve

(2) Obtain values from Step 1

(3) d_c obtained from Hydraulic Design Series No. 3, HEC #5, or HEC #13

STEP 4

OUTLET VELOCITY WHEN CULVERT IS IN OUTLET CONTROL

If designing a Box Culvert

Use file 1, block 4

Enter: 1. TW = _____
 2. D = _____
 3. B = _____
 4. Q/N = _____

(Read):
Velocity

If designing a pipe culvert

Use file 2, block 3

Enter: 1. D = _____
 2. Q/N = _____
 3. Alpha = _____ (1.04 for RCP, 1.12 for CMP)
 4. TW = _____

(Read):
Velocity

STEP 5

INLET CONTROL CALCULATIONS AND PERFORMANCE CURVE DATA

(BOX CULVERTS)

Use file 1, block 5 if analyzing a square-edge inlet with headwalls.

Use file 1, block 6 if analyzing a 45° beveled inlet.

Use file 1, block 7 if analyzing a tapered inlet throat.

(PIPE CULVERTS)

Use file 2, block 4 if analyzing a thin-edged projecting inlet.

Use file 2, block 5 if analyzing an inlet with square edges in a headwall.

Use file 2, block 7 if analyzing a groove end projecting inlet.

Use file 2, block 8 if analyzing a groove end inlet and headwalls.

Use file 2, block 6 if analyzing a beveled inlet.

Use file 2, block 9 if analyzing a tapered inlet throat. (Smooth inlet)

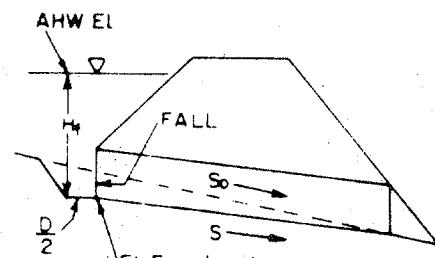
Use file 2, block 10 if analyzing a tapered inlet throat. (Rough inlet)

Enter: 1. AHW Elev. = _____

2. El. Stream bed at face = _____

3. B = _____ (D, if pipe)

4. D = _____



CONVENTIONAL OR BEVELED

Q	5. (Enter) Q/N	(Read) El. Face invert	(Read) FALL	(Read) HW _f	Note: Use Upper headings for Conventional or beveled face; Lower headings for tapered inlet throat. COMMENTS
		El. Throat invert		HW _t	
Program No. _____ , Inlet and Edge Description _____					
Program No. _____ , Inlet and Edge Description _____					

Note: Plot inlet control section performance curve

STEP 6 & 7
SIDE-TAPERED INLET AND CREST CHECK

(BOX CULVERTS)

Use file 1, block 8 if wingwalls have a 26° to 45° flare angle with top edge beveled or 45° to 90° flare angle with bevels on top and sides. (Favorable face edge conditions)
 Use file 1, block 9 if wingwalls have a 15° to 26° flare angle with top edge beveled or 26° to 90° flare angle with no bevels. (Unfavorable face edge conditions)

(PIPE CULVERTS)

Use file 2, block 11 if the face has projecting thin edges.
 Use file 2, block 12 if the face has square edges in a headwall.
 Use file 2, block 13 if the face has bevels or a groove end.

(CREST CHECK)

Use file 1, block 13 for crest check on a conventional, beveled or side-tapered inlet.

Enter: 1. HW_f = _____

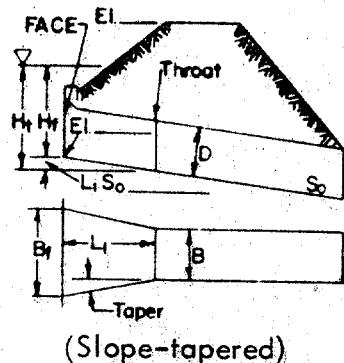
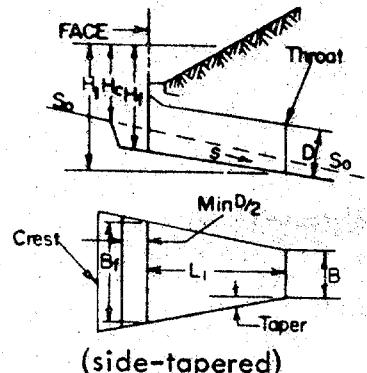
2. EI. Throat Invert = _____

3. (Taper + S) = _____ (Taper is 4:1 to 6:1), ($S \approx S_o - \text{FALL} / L_o$)

4. NxB = _____ (NxD for pipe)

5. Q = _____

6. D = _____ (E for pipe, where $D \leq E \leq 1.1 D$)



(4) (Read) Min. B _f	B _f Used	(Read) L ₁	(Read) EI. face invert	COMMENTS

(4) To use a B_f that is rounded off enter new B_f and press START STOP

Enter: (Crest Check)

1. Q = _____ 2. N = _____ 3. HW_f = _____ 4. W = _____

5. B = _____ 0 6. L₁ = _____ 0 7. Taper = _____ 0

Crest Check: (Read) H_c = _____, (Read) Max. Crest EI. = _____

STEP 8 THROUGH 12
SLOPE-TAPERED INLET AND CREST CHECK

Use file 1, block 10 for B_f if face has favorable edge conditions as in STEP 5.
 Use file 1, block 11 for B_f if face has unfavorable edge conditions as in STEP 5.

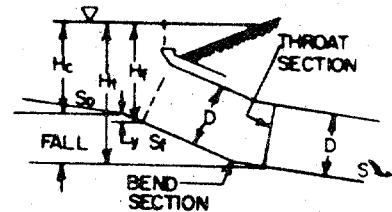
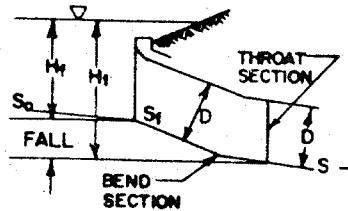
Enter: 1. $Q =$ _____

2. $D =$ _____

3. $HW_f =$ _____

4. E1. Streambed at face = _____ (if vertical face)
 E1. Crest = _____ (if mitered face)

5. $y =$ _____



(Read) Min. B_f , or higher rounded value	Type of Face
	Vertical, $y = 0$
	Mitered, $y = .4D$

Use file 1, block 12 for L dimensions of an inlet with a vertical face.

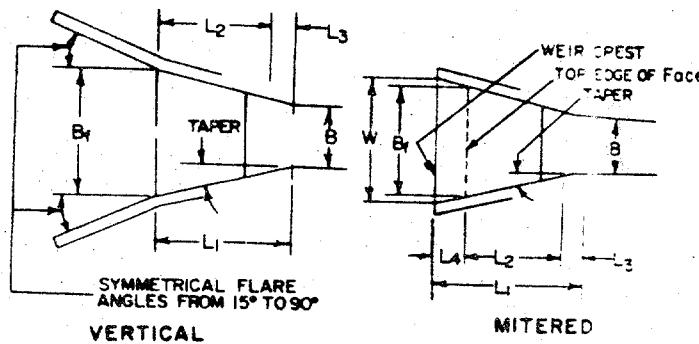
Enter 1. $B =$ _____ 6. Taper = _____ :1

2. $D =$ _____ 7. E1. Crest Inv. = _____

3. $N =$ _____ 8. E1. Throat Inv. = _____

4. $B_f =$ _____ 9. $S_f =$ _____ :1
 (2:1 to 3:1)

5. $y =$ _____



(Read) L_2	(Read) L_3	(Read) L_4	(Read) L_1	(Read) Taper	Type of Face
					Vertical, $y = 0$
					Mitered, $y = .4D$

Use file 1, block 13 for crest check on a slope-tapered inlet with mitered face.

Enter: 1. $Q =$ _____

3. $HW_f =$ _____

6. $L_1 =$ _____

2. $N =$ _____

4. $W =$ _____ 0

7. Taper = _____ : 1

5. $B =$ _____

Crest Check: (Read) $H_c =$ _____, (Read) Max, Crest E1. = _____

STEP 13

OUTLET VELOCITY WHEN CULVERT IS IN INLET CONTROL

Use file 1, block 14 if designing a box culvert

Use file 2, block 14 if designing a pipe culvert

Enter: 1. D = _____

2. B = _____ (Use D if designing a pipe)

3. n = _____

4. Q/N = _____

5. S = _____ = $(S_o - \text{FALL}/L_a)$

(READ) d_n/B	(READ) Velocity

For Box Culvert

(READ) Velocity

For pipe culvert

1 1

Calculates channel tailwater.

• 001	001		1	• 046	021	+		• 091	020	=	
• 002	032	I D		• 047	310	RC	5	• 092	025	d	
• 003	033	S S		• 048	005			• 093	026	(
• 004	034	PT		• 049	023	x		• 094	002)	
• 005	300	ST		• 050	310	RC	0	• 095	024	÷	
• 006	001		2	• 051	000	÷		• 096	003	3	
• 007	002		2	• 052	024	2		• 097	027)	
• 008	032	I D		• 053	002	+		• 098	023	x	
• 009	033	S S		• 054	021	+		• 099	310	RC	
• 010	034	PT		• 055	310	RC	3	• 100	011	s	
• 011	300	ST		• 056	003	3		• 101	023	x	
• 012	002		2	• 057	023	x		• 102	310	RC	
• 013	003		3	• 058	310	RC	9	• 103	002	2	
• 014	032	I D		• 059	000	0		• 104	062	r	
• 015	033	S S		• 060	020	=		• 105	023	x	
• 016	034	PT		• 061	300	ST	9	• 106	001	1	
• 017	300	ST		• 062	011	9		• 107	012	d	
• 018	003		3	• 063	310	RC	4	• 108	004	4	
• 019	004		4	• 064	004	4		• 109	010	s	
• 020	032	I D		• 065	162	SQ		• 110	006	6	
• 021	033	S S		• 066	021	+		• 111	024	+	
• 022	034	PT		• 067	001	1		• 112	310	RC	
• 023	300	ST		• 068	020	=		• 113	001	1	
• 024	004		4	• 069	062	r		• 114	022	-	
• 025	005		5	• 070	021	+		• 115	310	RC	
• 026	032	I D		• 071	026	(• 116	006	6	
• 027	033	S S		• 072	310	RC	5	• 117	020	=	
• 028	034	PT		• 073	005			• 118	110	R	
• 029	300	ST		• 074	162	SQ		• 119	354	JC	
• 030	005		5	• 075	021	+		• 120	002	2	
• 031	203	L 3		• 076	001	1		• 121	320	XC	
• 032	006		5	• 077	020	=		• 122	007	7	
• 033	032	I D		• 078	062	r		• 123	312	RC-	
• 034	033	S S		• 079	027)		• 124	007	7	
• 035	034	PT		• 080	023	x		• 125	354	JC	
• 036	300	ST		• 081	310	RC		• 126	002	2	
• 037	006		6	• 082	000	0		• 127	063	%	
• 038	001		1	• 083	021	+		• 128	023	x	
• 039	300	ST		• 084	310	RC	3	• 129	310	RC	
• 040	000		0	• 085	003	3		• 130	007	7	
• 041	300	ST		• 086	020	=		• 131	023	x	
• 042	010		8	• 087	063	%		• 132	310	RC	
• 043	201	L 1		• 088	023	x		• 133	010	8	
• 044	310	RC		• 089	310	RC	9	• 134	020	=	
• 045	004		4	• 090	011	9		• 135	300	ST	

•136 010 8
•137 302 ST-
•138 000 0
•139 350 J
•140 001 1
•141 202 L 2
•142 310 RC
•143 000 0
•144 035 P A
•145 035 P A
•146 222 DP 2
•147 034 PT
•148 112 D T
•149 224 DP 4
•150 350 J
•151 003 3

1 2 Determines an acceptable box size by calculating HW_o.

•001	001	1	•046	032	I D	•091	001	1
•002	032	I D	•047	033	S S	•092	021	+
•003	033	S S	•048	034	PT	•093	310	RC
•004	034	PT	•049	300	ST	•094	005	5
•005	300	ST	•050	010		•095	023	X
•006	001	1	•051	011		•096	026	(
•007	002	2	•052	032	I D	•097	310	RC
•008	032	I D	•053	033	S S	•098	001	1
•009	033	S S	•054	034	PT	•099	024	÷
•010	034	PT	•055	300	ST	•100	310	RC
•011	300	ST	•056	011		•101	002	2
•012	002	2	•057	310	RC	•102	024	÷
•013	003	3	•058	004		•103	310	RC
•014	032	I D	•059	162	SQ	•104	010	e
•015	033	S S	•060	023	X	•105	024	÷
•016	034	PT	•061	310	RC	•106	310	RC
•017	300	ST	•062	003		•107	011	9
•018	003	3	•063	023	X	•108	027)
•019	004	4	•064	002		•109	162	SO
•020	032	I D	•065	011		•110	024	+
•021	033	S S	•066	024	÷	•111	006	6
•022	034	PT	•067	026	(•112	004	4
•023	300	ST	•068	310	RC	•113	012	d
•024	004	4	•069	010		•114	004	4
•025	005	5	•070	023	X	•115	020	=
•026	032	I D	•071	310	RC	•116	300	ST
•027	033	S S	•072	011		•117	000	0
•028	034	PT	•073	024	÷	•118	310	RC
•029	300	ST	•074	002		•119	001	1
•030	005	5	•075	024	+	•120	024	÷
•031	006	6	•076	026	(•121	310	RC
•032	032	I D	•077	310	RC	•122	002	2
•033	033	S S	•078	010		•123	024	÷
•034	034	PT	•079	021	+	•124	310	RC
•035	300	ST	•080	310	RC	•125	010	e
•036	006	6	•081	011		•126	025	d
•037	007	7	•082	027)	•127	026	(
•038	032	I D	•083	025	d	•128	002	2
•039	033	S S	•084	026	(•129	024	+
•040	034	PT	•085	004		•130	003	3
•041	300	ST	•086	024	÷	•131	027)
•042	007	7	•087	003		•132	023	X
•043	201	L 1	•088	027)	•133	012	d
•044	222	DP 2	•089	027)	•134	003	3
•045	010	8	•090	021	+	•135	001	1

•136	005	5	•187	035	P A
•137	022	-	•188	035	P A
•138	300	ST	•189	034	PT
•139	012	d	•190	112	D T
•140	310	RC	•191	350	J
•141	011	9	•192	001	1
•142	020	=			
•143	356	JC			
•144	002	2			
•145	310	RC			
•146	011	9			
•147	300	ST			
•148	012	d			
•149	202	L 2			
•150	310	RC			
•151	011	9			
•152	021	+			
•153	310	RC			
•154	012	d			
•155	024	+			
•156	002	2			
•157	022	-			
•158	300	ST			
•159	013	S			
•160	310	RC			
•161	006	6			
•162	020	=			
•163	035	P A			
•164	035	P A			
•165	356	JC			
•166	003	3			
•167	310	RC			
•168	013	S			
•169	034	PT			
•170	350	J			
•171	004	4			
•172	203	L 3			
•173	310	RC			
•174	005	5			
•175	034	PT			
•176	310	RC			
•177	006	6			
•178	204	L 4			
•179	112	D T			
•180	021	+			
•181	310	RC			
•182	000	0			
•183	021	+			
•184	310	RC			
•185	007	7			
•186	020	=			

1 3 Calculates outlet control performance curve data for
box culverts.

•001	001	1	•046	032	I D	•091	310	RC
•002	032	I D	•047	033	S S	•092	010	a
•003	033	S S	•048	034	PT	•093	024	÷
•004	034	PT	•049	300	ST	•094	310	RC
•005	300	ST	•050	010		•095	004	4
•006	001	1	•051	310	RC	•096	024	÷
•007	002	2	•052	002		•097	310	RC
•008	032	I D	•053	162	SU	•098	005	5
•009	033	S S	•054	023	x	•099	027)
•010	034	PT	•055	310	RC	•100	162	SU
•011	300	ST	•056	001		•101	024	÷
•012	002	2	•057	023	x	•102	006	6
•013	003	3	•058	002		•103	004	4
•014	032	I D	•059	011		•104	012	d
•015	033	S S	•060	024	÷	•105	004	4
•016	034	PT	•061	026	(•106	020	=
•017	300	ST	•062	310	RC	•107	300	ST
•018	003	3	•063	004		•108	000	0
•019	004	4	•064	023	x	•109	310	RC
•020	032	I D	•065	310	RC	•110	010	a
•021	033	S S	•066	005		•111	024	÷
•022	034	PT	•067	024	÷	•112	310	RC
•023	300	ST	•068	002		•113	004	4
•024	004	4	•069	024	÷	•114	025	d
•025	005	5	•070	026	(•115	026)
•026	032	I D	•071	310	RC	•116	002	2
•027	033	S S	•072	004		•117	024	÷
•028	034	PT	•073	021	+	•118	003	3
•029	300	ST	•074	310	RC	•119	027)
•030	005	5	•075	005	x 5	•120	023	x
•031	006	6	•076	027)	•121	012	d
•032	032	I D	•077	025	d	•122	003	3
•033	033	S S	•078	026	(•123	001	1
•034	034	PT	•079	004		•124	005	5
•035	300	ST	•080	024	÷	•125	022	-
•036	006	6	•081	003		•126	300	ST
•037	201	L 1	•082	027)	•127	012	d
•038	222	DP 2	•083	027)	•128	310	RC
•039	007	7	•084	021	+	•129	005	5
•040	032	I D	•085	001		•130	020	=
•041	033	S S	•086	021	+	•131	356	JC
•042	034	PT	•087	310	RC	•132	002	2
•043	300	ST	•088	003		•133	310	RC
•044	007	7	•089	023	x	•134	005	5
•045	011	9	•090	026	(•135	300	ST

•136 012 d
•137 202 L 2
•138 310 RC
•139 005 s
•140 021 +
•141 310 RC
•142 012 -d
•143 024 ÷
•144 002 2
•145 022 -
•146 300 ST
•147 013 S
•148 310 RC
•149 007 7
•150 020 =
•151 035 P A
•152 035 P A
•153 356 JC
•154 003 3
•155 310 RC
•156 013 S
•157 350 J
•158 004 4
•159 203 L 3
•160 310 RC
•161 007 7
•162 204 L 4
•163 021 +
•164 310 RC
•165 000 0
•166 021 +
•167 310 RC
•168 006 6
•169 020 =
•170 034 PT
•171 112 D T
•172 350 J
•173 001 1

1 4 Calculates outlet velocity for box culverts in outlet control.

•001	001		1	•046	001		1	•091	003		3
•002	032	1 D		•047	020	=		•092	020	=	
•003	033	S S		•048	351	J C		•093	035	P A	
•004	034	PT		•049	001		1	•094	035	P A	
•005	300	ST		•050	310	R C		•095	034	F T	
•006	001		1	•051	001		1	•096	112	D T	
•007	002		2	•052	022	-		•097	350	J	
•008	032	1 D		•053	310	R C		•098	033	S S	
•009	033	S S		•054	012		2				
•010	034	PT		•055	020	=					
•011	300	ST		•056	356	J C					
•012	002		2	•057	002		2				
•013	003		3	•058	310	R C					
•014	032	1 D		•059	002		2				
•015	033	S S		•060	300	S T					
•016	034	PT		•061	001		1				
•017	300	ST		•062	202	L 2					
•018	003		3	•063	310	R C					
•019	004		4	•064	001		1				
•020	032	1 D		•065	063	X					
•021	033	S S		•066	350	J					
•022	034	PT		•067	003		3				
•023	300	ST		•068	201	L 2					
•024	004		4	•069	310	R C					
•025	222	DP	2	•070	005		5				
•026	310	R C		•071	022	-					
•027	004		4	•072	310	R C					
•028	024	+		•073	002		2				
•029	310	R C		•074	020	=					
•030	003		3	•075	356	J C					
•031	025	4		•076	004		4				
•032	026	(•077	310	R C					
•033	002		2	•078	002		2				
•034	024	+		•079	300	S T					
•035	003		3	•080	005		5				
•036	027)		•081	204	L 4					
•037	023	x		•082	310	R C					
•038	012	a		•083	005		5				
•039	003		3	•084	063	X					
•040	001		1	•085	203	L 3					
•041	005		5	•086	023	X					
•042	022	-		•087	310	R C					
•043	300	ST		•088	004		4				
•044	005		5	•089	024	+					
•045	310	R C		•090	310	R C					

1 5

Calculates the performance of a square-edged inlet
with headwalls on a box culvert.

•001	001		1	•049	300	ST	•097	012	d
•002	032	1 D		•050	006	6	•098	005	s
•003	033	S S		•051	023	x	•099	000	s
•004	034	PT		•052	012	d	•100	005	s
•005	300	ST		•053	000	0	•101	004	d
•006	001		1	•054	000	0	•102	003	s
•007	002		2	•055	000	0	•103	005	s
•008	032	1 D		•056	000	0	•104	023	x
•009	033	S S		•057	003	3	•105	310	RC
•010	034	PT		•058	004	4	•106	006	6
•011	300	ST		•059	005	5	•107	021	+
•012	002		2	•060	006	6	•108	012	d
•013	003		3	•061	022	-	•109	001	s
•014	032	1 D		•062	012	d	•110	002	d
•015	033	S S		•063	000	0	•111	002	s
•016	034	PT		•064	000	0	•112	001	1
•017	300	ST		•065	001	2	•113	001	1
•018	003		3	•066	003	3	•114	007	7
•019	004		4	•067	006	6	•115	023	x
•020	032	1 D		•068	007	7	•116	310	RC
•021	033	S S		•069	005	5	•117	004	4
•022	034	PT		•070	007	7	•118	020	=
•023	300	ST		•071	023	x	•119	300	ST
•024	004		4	•072	310	RC	•120	007	7
•025	001		1	•073	006	6	•121	001	1
•026	300	ST		•074	021	+	•122	302	ST
•027	009		2	•075	012	d	•123	000	0
•028	201	L	1	•076	003	0	•124	310	RC
•029	222	DP	2	•077	002	2	•125	000	0
•030	005		5	•078	000	0	•126	352	JC
•031	032	1 D		•079	007	7	•127	003	3
•032	033	S S		•080	010	8	•128	310	RC
•033	034	PT		•081	000	0	•129	001	1
•034	300	ST		•082	011	9	•130	022	-
•035	005		5	•083	023	x	•131	310	RC
•036	024		+	•084	310	RC	•132	007	7
•037	310	RC		•085	006	6	•133	020	=
•038	003		3	•086	022	-	•134	300	ST
•039	024		+	•087	012	d	•135	010	3
•040	026		4	•088	001	1	•136	022	-
•041	310	RC		•089	000	0	•137	310	RC
•042	004		4	•090	010	8	•138	002	2
•043	025		3	•091	005	5	•139	020	=
•044	001		2	•092	006	6	•140	300	ST
•045	012		d	•093	023	x	•141	012	d
•046	005		5	•094	310	RC	•142	352	JC
•047	027		3	•095	006	6	•143	004	4
•048	020		=	•096	021	+	•144	310	RC

•145 002 2
•146 300 S1
•147 010 8
•148 000 0
•149 •300 ST
•150 012 d
•151 204 L 4
•152 310 RC
•153 010 3
•154 035 P A
•155 035 P A
•156 034 PT
•157 112 L T
•158 310 RC
•159 012 0
•160 035 P A
•161 035 P A
•162 102 F2
•163 034 PT
•164 112 D T
•165 203 L 3
•166 310 RC
•167 010 9
•168 021 4
•169 310 RC
•170 007 7
•171 020 =
•172 035 P A
•173 035 P A
•174 034 PT
•175 112 D T
•176 350 J
•177 001 1

1

6

Calculates the performance of a 45° beveled inlet on
a box culvert.

•001	037	CL	•049	020	=	•097	023	x
•002	001	i	•050	300	ST	•098	310	RC
•003	032	ID	•051	006	s	•099	006	+
•004	033	S S	•052	023	x	•100	021	d
•005	034	PT	•053	012	d	•101	012	3
•006	300	ST	•054	000	o	•102	003	3
•007	001	1	•055	000	o	•103	011	9
•008	002	2	•056	000	o	•104	010	8
•009	032	ID	•057	000	o	•105	011	9
•010	033	S S	•058	001	1	•106	003	3
•011	034	PT	•059	004	4	•107	005	5
•012	300	ST	•060	005	5	•108	003	3
•013	002	2	•061	006	6	•109	023	x
•014	003	3	•062	006	6	•110	310	RC
•015	032	ID	•063	022	-	•111	006	6
•016	033	S S	•064	012	d	•112	021	+
•017	034	PT	•065	000	o	•113	012	d
•018	300	ST	•066	000	o	•114	001	1
•019	003	3	•067	000	o	•115	005	5
•020	004	4	•068	006	6	•116	006	6
•021	032	ID	•069	004	4	•117	006	6
•022	033	S S	•070	004	4	•118	000	+
•023	034	PT	•071	011	9	•119	010	9
•024	300	ST	•072	023	x	•120	J06	6
•025	004	4	•073	310	RC	•121	023	x
•026	001	1	•074	006	s	•122	310	RC
•027	300	ST	•075	021	+	•123	004	4
•028	000	0	•076	012	d	•124	020	=
•029	201	L 1	•077	000	o	•125	300	ST
•030	222	DP 2	•078	001	1	•126	007	7
•031	005	5	•079	001	1	•127	001	1
•032	032	ID	•080	002	2	•128	302	ST =
•033	033	S S	•081	000	o	•129	000	0
•034	034	PT	•082	001	1	•130	310	RC
•035	300	ST	•083	003	3	•131	000	0
•036	005	5	•084	005	s	•132	352	JC
•037	024	+	•085	023	x	•133	003	3
•038	310	RC	•086	310	RC	•134	310	RC
•039	003	3	•087	006	6	•135	001	1
•040	024	÷	•088	022	-	•136	022	-
•041	026	(•089	012	d	•137	310	RC
•042	310	RC	•090	000	o	•138	007	7
•043	004	4	•091	006	s	•139	020	=
•044	025	d	•092	004	4	•140	300	ST
•045	001	1	•093	000	o	•141	010	8
•046	012	d	•094	003	3	•142	022	-
•047	005	5	•095	011	9	•143	310	RC
•048	027)	•096	002	2	•144	002	2
						•145	020	=

•146 300 ST
•147 012 d
•148 356 JC
•149 004 4
•150 310 RC
•151 002 2
•152 300 ST
•153 010 a
•154 000 o
•155 300 ST
•156 012 d
•157 204 L 4
•158 310 RC
•159 310 3
•160 035 P A
•161 035 P A
•162 034 PT
•163 112 D T
•164 310 RC
•165 012 d
•166 035 P A
•167 035 P A
•168 102 F 2
•169 034 PT
•170 112 D T
•171 203 L 3
•172 310 RC
•173 010 9
•174 021 +
•175 310 RC
•176 007 7
•177 020 =
•178 035 P A
•179 035 P A
•180 034 PT
•181 112 D T
•182 350 J
•183 001 1

Calculates the performance of the throat section of a
tapered inlet in a box culvert.

•001	037	CL	•049	020	=	•097	005	S
•002	001	2	•050	300	ST	•096	023	X
•003	032	ID	•051	006	S	•099	310	RC
•004	033	SS	•052	023	X	•100	006	S
•005	034	PT	•053	012	d	•101	021	+
•006	300	ST	•054	000	a	•102	012	d
•007	001	1	•055	000	b	•103	001	2
•008	002	2	•056	000	c	•104	002	2
•009	032	ID	•057	001	x	•105	011	9
•010	033	SS	•058	000	o	•106	005	5
•011	034	PT	•059	006	e	•107	300	0
•012	300	ST	•060	003	3	•108	003	3
•013	002	2	•061	005	5	•109	003	3
•014	003	3	•062	010	a	•110	023	X
•015	032	I U	•063	013	S	•111	310	RC
•016	033	SS	•064	021	+	•112	004	4
•017	034	PT	•065	012	d	•113	020	+
•018	300	ST	•066	000	o	•114	300	ST
•019	003	3	•067	000	o	•115	007	7
•020	004	4	•068	004	4	•116	001	1
•021	032	ID	•069	002	2	•117	302	ST-
•022	033	SS	•070	006	6	•118	000	0
•023	034	PT	•071	003	3	•119	310	RC
•024	300	ST	•072	002	2	•120	000	0
•025	004	4	•073	011	9	•121	352	JC
•026	301	1	•074	023	X	•122	003	3
•027	300	ST	•075	310	RC	•123	310	RC
•028	300	0	•076	006	S	•124	001	1
•029	201	L 1	•077	022	-	•125	022	-
•030	222	DP 2	•078	012	a	•126	310	RC
•031	005	5	•079	000	o	•127	007	7
•032	032	ID	•080	004	4	•128	020	+
•033	033	SS	•081	003	3	•129	300	ST
•034	034	PT	•082	007	7	•130	010	8
•035	300	ST	•083	007	7	•131	022	-
•036	005	5	•084	007	7	•132	310	RC
•037	024	4	•085	010	8	•133	002	2
•038	310	RC	•086	023	X	•134	020	+
•039	003	3	•067	310	RC	•135	300	ST
•040	024	4	•088	006	6	•136	012	d
•041	026	(•089	021	+	•137	352	JC
•042	310	RC	•090	012	d	•138	004	4
•043	004	4	•091	003	3	•139	310	RC
•044	025	d	•092	007	7	•140	302	2
•045	001	1	•093	010	9	•141	300	ST
•046	012	d	•094	011	9	•142	010	8
•047	005	5	•095	004	4	•143	000	0
•048	327)	•096	004	4	•144	300	ST

•145 012 d
•146 204 L 4
•147 310 RC
•148 010 8
•149 035 P A
•150 035 P A
•151 034 PT
•152 112 D T
•153 310 RC
•154 012 d
•155 035 P A
•156 035 P A
•157 102 F2
•158 034 PT
•159 112 D T
•160 203 L 3
•161 310 RC
•162 010 8
•163 021 4
•164 310 RC
•165 007 7
•166 020 =
•167 035 P A
•168 035 P A
•169 J34 PT
•170 112 D T
•171 350 J
•172 001 1

1 1 8

Calculates B_f and L_1 for a side-tapered inlet on a box culvert with favorable face edge conditions. (See Step 7 for definition of favorable conditions).

•001	037	CL	•046	310	RC	•091	002	2
•002	001	1	•047	005	s	•092	001	1
•003	032	ID	•048	020	=	•093	002	2
•004	033	S S	•049	300	ST	•094	010	9
•005	034	FT	•050	007	7	•095	023	x
•006	022	-	•051	001	1	•096	310	RC
•007	002	2	•052	300	ST	•097	010	9
•008	032	ID	•053	013	S	•098	021	+
•009	033	S S	•054	300	ST	•099	003	3
•010	034	PT	•055	012	d	•100	012	o
•011	300	ST	•056	201	L 1	•101	006	6
•012	003	3	•057	310	RC	•102	011	9
•013	J20	=	•058	001	2	•103	010	9
•014	300	ST	•059	022	-	•104	005	5
•015	001	1	•060	310	RC	•105	003	3
•016	003	3	•061	013	S	•106	023	x
•017	032	ID	•062	024	÷	•107	310	RC
•018	033	S S	•063	310	RC	•108	010	8
•019	034	PT	•064	006	6	•109	022	-
•020	300	ST	•065	020	=	•110	001	1
•021	002	2	•066	300	ST	•111	012	d
•022	004	4	•067	010	3	•112	001	1
•023	032	ID	•068	023	x	•113	003	3
•024	033	S S	•069	012	d	•114	006	5
•025	034	PT	•070	000	0	•115	000	0
•026	300	ST	•071	002	2	•116	007	7
•027	004	4	•072	005	5	•117	023	x
•028	005	5	•073	006	5	•118	310	RC
•029	032	ID	•074	011	3	•119	007	7
•030	033	S S	•075	002	2	•120	020	=
•031	034	PT	•076	003	3	•121	063	x
•032	300	ST	•077	022	-	•122	035	F A
•033	005	5	•078	012	d	•123	035	F A
•034	J06	5	•079	012	2	•124	034	PT
•035	032	ID	•080	000	0	•125	112	D T
•036	033	S S	•081	005	5	•126	033	S S
•037	034	PT	•082	003	3	•127	022	-
•038	222	DP	•083	003	3	•128	310	RC
•039	300	SI	•084	011	9	•129	004	4
•040	305	5	•085	023	x	•130	024	÷
•041	025	6	•086	310	RC	•131	002	2
•042	001	1	•087	010	3	•132	023	x
•043	012	d	•088	021	+	•133	310	RC
•044	005	5	•089	012	d	•134	002	2
•045	024	÷	•090	001	1	•135	106	1
						•136	020	=

•137	300	ST	•189	112	D T
•138	000	a	•190	350	J
•139	001	i	•191	033	S S
•140	302	ST-			
•141	012	d			
•142	310	RC			
•143	012	d			
•144	352	JC			
•145	002	2			
•146	310	RC			
•147	000	o			
•148	023	x			
•149	310	RC			
•150	002	2			
•151	105	F5			
•152	020	=			
•153	300	ST			
•154	013	S			
•155	022	-			
•156	001	i			
•157	020	=			
•158	356	JC			
•159	002	2			
•160	310	RC			
•161	000	o			
•162	023	x			
•163	310	RC			
•164	002	2			
•165	105	F5			
•166	020	=			
•167	300	ST			
•168	013	S			
•169	350	J			
•170	001	i			
•171	202	L 2			
•172	035	F A			
•173	035	P A			
•174	310	RC			
•175	000	o			
•176	034	PT			
•177	112	D T			
•178	023	x			
•179	310	RC			
•180	002	2			
•181	105	F5			
•182	021	+			
•183	310	RC			
•184	003	3			
•185	020	=			
•186	035	P A			
•187	035	F A			
•188	034	PT			

1

9

Calculates B_f and L_1 for a side-tapered inlet on a box culvert with unfavorable face edge conditions. (See Step 7 for definition of unfavorable conditions).

•001	037	CL	•047	005		•093	004	4	
•002	001		•048	020	=	•094	012	d	
•003	032	ID	•049	300	ST	•095	003	3	
•004	033	SS	•050	007		•096	023	x	
•005	034	PT	•051	001		•097	310	RC	
•006	022	-	•052	300	ST	•098	010	9	
•007	002		•053	013	S	•099	022	-	
•008	032	ID	•054	300	ST	•100	001	1	
•009	033	SS	•055	012	L	•101	012	d	
•010	034	PT	•056	201	1	•102	002	2	
•011	300	ST	•057	310	RC	•103	001	1	
•012	003		•058	001	1	•104	011	9	
•013	020	=	•059	022	-	•105	023	x	
•014	300	ST	•060	310	RC	•106	310	RC	
•015	001		•061	013	S	•107	007	7	
•016	003		•062	024	÷	•108	020	=	
•017	032	ID	•063	310	RC	•109	063	b	
•018	033	SS	•064	006	6	•110	035	PA	
•019	034	PT	•065	020	=	•111	035	PA	
•020	300	ST	•066	300	ST	•112	034	PT	
•021	002		•067	010	8	•113	112	D T	
•022	004		•068	023	x	•114	033	SS	
•023	032	ID	•069	012	8	•115	022	-	
•024	033	SS	•070	000	0	•116	310	RC	
•025	034	PT	•071	000	0	•117	004	4	
•026	300	ST	•072	002	2	•118	024	÷	
•027	004		•073	007	7	•119	002	2	
•028	005		•074	021	+	•120	023	x	
•029	032	ID	•075	012	d	•121	310	RC	
•030	033	SS	•076	000	0	•122	002	2	
•031	034	PT	•077	002	2	•123	106	I	
•032	300	ST	•078	007	7	•124	020	=	
•033	005		•079	003	3	•125	300	ST	
•034	006		•080	023	x	•126	000	0	
•035	032	ID	•081	310	RC	•127	001	1	
•036	033	SS	•082	010	8	•128	302	ST-	
•037	034	PT	•083	022	-	•129	012	d	
•038	222	DP	2	•084	012	d	•130	310	RC
•039	300	ST		•085	006	6	•131	012	d
•040	3L6		5	•086	001	1	•132	352	JC
•041	025	c		•087	005	5	•133	002	2
•042	001		1	•088	003	3	•134	310	RC
•043	012	d		•089	023	x	•135	000	0
•044	005		5	•090	310	RC	•136	023	x
•045	024	÷		•091	010	8	•137	310	RC
•046	310	RC		•092	021 _{OR}	+	•138	002	2

•139	105	Fs
•140	020	=
•141	300	ST
•142	013	S
•143	022	-
•144	001	2
•145	020	=
•146	356	JC
•147	002	2
•148	310	RC
•149	000	0
•150	023	X
•151	310	RC
•152	002	2
•153	105	Fs
•154	020	=
•155	300	ST
•156	013	S
•157	350	J
•158	001	1
•159	202	L 2
•160	035	PA
•161	035	PA
•162	310	RC
•163	000	J
•164	034	PT
•165	112	DT
•166	023	X
•167	310	RC
•168	002	2
•169	105	Fs
•170	021	+
•171	310	RC
•172	003	3
•173	020	=
•174	035	PA
•175	035	PA
•176	034	PT
•177	112	DT
•178	350	J
•179	033	S S

1 10

Calculates B_f for slope-tapered inlets on culverts with favorable face edge conditions and either a vertical or mitered face.

•001	037	CL	•046	005	5	•092	310	RC	s
•002	001	2	•047	023	x	•093	005		
•003	032	I D	•048	012	d	•094	021	+	7
•004	033	S S	•049	000	0	•095	007		d
•005	034	PT	•050	002	2	•096	012		3
•006	300	ST	•051	010	8	•097	011		4
•007	001	1	•052	004	4	•098	004		2
•008	002	2	•053	006	6	•099	002		4
•009	032	I D	•054	007	7	•100	004		4
•010	033	S S	•055	006	6	•101	004		4
•011	034	PT	•056	007	7	•102	001		i
•012	300	ST	•057	022	-	•103	023	x	
•013	002	2	•058	012	d	•104	310	RC	
•014	003	3	•059	003	3	•105	005		s
•015	032	I D	•060	004	4	•106	022		-
•016	033	S S	•061	005	5	•107	002		2
•017	034	PT	•062	010	8	•108	012		d
•018	300	ST	•063	002	2	•109	002		2
•019	003	3	•064	001	1	•110	006		6
•020	004	4	•065	004	4	•111	005		5
•021	032	I D	•066	023	x	•112	010		s
•022	033	S S	•067	310	RC	•113	006		5
•023	034	PT	•068	005	5	•114	003		3
•024	300	ST	•069	021	+	•115	023	x	
•025	004	4	•070	001	1	•116	026		(
•026	005	5	•071	012	d	•117	310	RC)
•027	032	I D	•072	006	5	•118	002		2
•028	033	S S	•073	001	1	•119	025		d
•029	034	PT	•074	311	9	•120	001		i
•030	300	ST	•075	054	4	•121	012		d
•031	007	7	•076	010	8	•122	005		s
•032	222	DP	•077	001	1	•123	027		
•033	310	RC	•078	023	x	•124	020	=	
•034	003	3	•079	310	RC	•125	063	x	
•035	022	-	•080	005	5	•126	023	x	
•036	310	RC	•081	022	-	•127	310	RC	
•037	004	4	•082	004	4	•128	001		i
•038	021	+	•083	012	d	•129	020	=	
•039	310	RC	•084	000	2	•130	035	P A	
•040	007	7	•085	003	3	•131	035	P A	
•041	024	+	•086	005	5	•132	034	PT	
•042	310	RC	•087	002	2	•133	112	D T	
•043	002	2	•088	000	0	•134	350	J	
•044	020	=	•089	C11	9	•135	033	S S	
•045	300	ST	•090	004	4				
			•091	023	x				

Calculates B_f for slope-tapered inlets on culverts with unfavorable face edge conditions and either a vertical or mitered face.

•001	037	CL	•046	005	5	•091	003	3
•002	001	1	•047	023	x	•092	005	5
•003	032	ID	•048	012	d	•093	003	3
•004	033	S S	•049	000	o	•094	023	x
•005	334	PT	•050	000	o	•095	026	(
•006	300	ST	•051	001	1	•096	310	RC
•007	001	1	•052	001	1	•097	002	2
•008	002	2	•053	022	-	•098	025	x
•009	032	ID	•054	012	d	•099	001	1
•010	033	S S	•055	000	o	•100	012	d
•011	034	PT	•056	001	1	•101	005	5
•012	300	ST	•057	004	4	•102	027)
•013	002	2	•058	004	4	•103	020	=
•014	003	3	•059	023	x	•104	063	x
•015	032	ID	•060	310	RC	•105	023	x
•016	033	S S	•061	005	5	•106	310	RC
•017	034	PT	•062	021	+	•107	001	1
•018	300	ST	•063	012	d	•108	020	=
•019	003	3	•064	001	1	•109	035	PA
•020	004	4	•065	005	5	•110	035	PA
•021	032	ID	•066	007	7	•111	034	PT
•022	033	S S	•067	010	9	•112	112	DT
•023	034	PT	•068	023	x	•113	350	J
•024	300	ST	•069	310	RC	•114	033	S S
•025	004	4	•070	005	5			
•026	005	5	•071	022	-			
•027	032	ID	•072	001	1			
•028	033	S S	•073	012	d			
•029	034	PT	•074	001	1			
•030	300	ST	•075	003	3			
•031	007	7	•076	001	1			
•032	222	DP	•077	023	x			
•033	310	RC	•078	310	RC			
•034	003	3	•079	005	5			
•035	022	-	•080	021	+			
•036	310	RC	•081	005	5			
•037	004	4	•082	012	d			
•038	021	+	•083	001	1			
•039	310	RC	•084	005	5			
•040	007	7	•085	023	x			
•041	024	+	•086	310	RC			
•042	310	RC	•087	005	5			
•043	002	2	•088	022	-			
•044	020	=	•089	001	1			
•045	300	ST	•090	012	d			

1 12 Calculates L₁, L₂, L₃, L₄ and Taper for a slope-tapered inlet on culverts with either a vertical or mitered face.

•001	222	DP	2	•046	010	8	•091	310	RC	
•002	037	CL		•047	032	ID	•092	011		9
•003	137	CA		•048	033	SS	•093	022	-	
•004	001		1	•049	034	PT	•094	310	RC	0
•005	032	ID		•050	300	ST	•095	000		
•006	033	SS		•051	010	9	•096	020	=	
•007	034	PT		•052	011	9	•097	300	ST	
•008	300	ST		•053	032	ID	•098	012	d	
•009	001		1	•054	033	SS	•099	310	RC	
•010	002		2	•055	034	PT	•100	001		1
•011	032	ID		•056	300	ST	•101	023	x	
•012	033	SS		•057	011	9	•102	310	RC	
•013	034	PT		•058	310	RC	•103	003		3
•014	300	ST		•059	005	5	•104	024	÷	
•015	002		2	•060	354	JC	•105	002		2
•016	003		3	•061	001	1	•106	020	=	
•017	032	ID		•062	310	RC	•107	300	ST	
•018	033	SS		•063	011	9	•108	013	S	
•019	034	PT		•064	023	x	•109	360	B	
•020	300	ST		•065	310	RC	•110	005		5
•021	003		3	•066	005	5	•111	023	x	
•022	004		4	•067	021	+	•112	310	RC	
•023	032	ID		•068	026	(•113	006		6
•024	033	SS		•069	310	RC	•114	022	-	
•025	034	PT		•070	002	2	•115	310	RC	
•026	300	ST		•071	024	÷	•116	013	S	
•027	004		4	•072	310	RC	•117	022	-	
•028	005		5	•073	011	9	•118	310	RC	
•029	032	ID		•074	027)	•119	012	d	
•030	033	SS		•075	020	=	•120	020	=	
•031	034	PT		•076	300	ST	•121	351	JC	
•032	300	ST		•077	000	0	•122	003		3
•033	005		s	•078	350	J	•123	310	RC	
•034	006		s	•079	002	2	•124	012	d	
•035	032	ID		•080	201	L 1	•125	021	+	
•036	033	SS		•081	003	0	•126	310	RC	
•037	034	PT		•082	300	ST	•127	013	S	
•038	300	ST		•083	000	0	•128	024	÷	
•039	006		6	•084	202	L 2	•129	026	(
•040	007		7	•085	310	RC	•130	360	B	
•041	032	ID		•086	007	7	•131	005		5
•042	033	SS		•087	022	-	•132	027)	
•043	034	PT		•088	310	RC	•133	J20	=	
•044	300	ST		•089	010	9	•134	300	ST	
•045	007		7	•090	023	x	•135	006		6

•136	350	J	•188	025	(
•137	004	4	•189	310	RC
•138	203	L 3	•190	001	1
•139	360	B	•191	023	x
•140	005	5	•192	310	RC
•141	023	x	•193	003	3
•142	310	RC	•194	027)
•143	006	6	•195	024	÷
•144	022	-	•196	002	2
•145	310	RC	•197	030	RT
•146	012	d			
•147	020	=			
•148	300	ST			
•149	013	S			
•150	204	L 4			
•151	035	P A			
•152	035	P A			
•153	310	RC			
•154	012	d			
•155	034	PT			
•156	021	+			
•157	112	D T			
•158	035	P A			
•159	035	P A			
•160	310	RC			
•161	013	S			
•162	034	PT			
•163	021	+			
•164	112	D T			
•165	035	P A			
•166	035	P A			
•167	310	RC			
•168	000	2			
•169	034	PT			
•170	020	=			
•171	112	D T			
•172	035	P A			
•173	035	P A			
•174	034	PT			
•175	112	D T			
•176	035	P A			
•177	035	P A			
•178	310	RC			
•179	006	6			
•180	034	PT			
•181	112	U T			
•182	350	J			
•183	033	S S			
•184	205	L S			
•185	310	RC			
•186	004	4			
•187	022	-			

1 13 Checks crest control for either a side- or slope-tapered inlet.

•001	222	DP	2	•046	005	5	•091	035	P A
•002	037	CL		•047	354	J C	•092	035	P A
•003	001		1	•048	001		•093	034	P T
•004	032	I D		•049	310	R C	•094	112	D T
•005	033	S S		•050	002		•095	350	J
•006	034	PT		•051	023	X	•096	033	S S
•007	300	ST		•052	310	R C			
•008	001		1	•053	005		5		
•009	002		2	•054	021	+			
•010	032	I D		•055	026	(
•011	033	S S		•056	002		2		
•012	034	PT		•057	023	X			
•013	300	ST		•058	310	R C			
•014	002		2	•059	006		6		
•015	003		3	•060	024	÷			
•016	032	I D		•061	310	R C			
•017	033	S S		•062	007		7		
•018	034	PT		•063	027)			
•019	300	ST		•064	020	=			
•020	003		3	•065	300	ST			
•021	004		4	•066	004		4		
•022	032	I D		•067	201	L 1			
•023	033	S S		•068	310	R C			
•024	034	PT		•069	001		1		
•025	300	ST		•070	024	÷			
•026	004		4	•071	310	R C			
•027	005		5	•072	004		4		
•028	032	I D		•073	025	÷			
•029	033	S S		•074	026	(
•030	034	PT		•075	302		2		
•031	300	ST		•076	024	÷			
•032	005		5	•077	003		3		
•033	006		6	•078	027)			
•034	032	I D		•079	024	÷			
•035	033	S S		•080	002		2		
•036	034	PT		•081	020	=			
•037	300	ST		•082	035	P A			
•038	006		6	•083	035	P A			
•039	007		7	•084	034	P T			
•040	032	I D		•085	112	D T			
•041	033	S S		•086	022	-			
•042	034	PT		•087	310	R C			
•043	300	ST		•088	003		3		
•044	007		7	•089	020	=			
•045	310	RC		•090	013	S			

1 14

Calculates outlet velocity for box culverts in inlet control.

•001	037	CL	•047	024	÷	•093	006	6
•002	001	1	•048	026	(•094	022	-
•003	032	I D	•049	310	RC	•095	001	1
•004	033	S S	•050	002	2	•096	005	5
•005	034	PT	•051	025	÷	•097	012	d
•006	300	ST	•052	026	(•098	001	1
•007	001	1	•053	010	÷	•099	005	5
•008	002	2	•054	024	÷	•100	002	2
•009	032	I D	•055	003)	•101	002	2
•010	033	S S	•056	027)	•102	003	3
•011	034	PT	•057	027	=	•103	010	8
•012	300	ST	•058	320	ST	•104	023	x
•013	002	2	•059	300	ST	•105	310	RC
•014	003	3	•060	006	6	•106	006	6
•015	032	I D	•061	022	-	•107	021	+
•016	033	S S	•062	012	d	•108	003	3
•017	034	PT	•063	002	2	•109	012	d
•018	300	ST	•064	002	2	•110	006	6
•019	003	3	•065	028	=	•111	004	4
•020	004	4	•066	351	J C	•112	010	8
•021	032	I D	•067	001	1	•113	003	3
•022	033	S S	•068	061	1	•114	007	7
•023	034	PT	•069	001	1	•115	010	3
•024	300	ST	•070	000	0	•116	004	4
•025	004	4	•071	012	d	•117	023	x
•026	005	5	•072	003	3	•118	310	RC
•027	032	I D	•073	001	1	•119	006	6
•028	033	S S	•074	006	6	•120	021	+
•029	034	PT	•075	003	3	•121	012	d
•030	300	ST	•076	005	5	•122	000	0
•031	005	5	•077	013	S	•123	003	3
•032	222	DF	•078	023	x	•124	006	6
•033	062	7	•079	310	RC	•125	004	4
•034	063	8	•080	006	6	•126	000	0
•035	024	÷	•081	021	+	•127	002	2
•036	001	1	•082	000	6	•128	360	8
•037	012	9	•083	004	4	•129	005	5
•038	004	4	•084	012	d	•130	350	J
•039	010	8	•085	011	9	•131	033	S S
•040	006	6	•086	011	9	•132	201	L 1
•041	023	x	•087	001	1	•133	310	RC
•042	310	RC	•088	011	9	•134	006	6
•043	004	4	•089	001	1	•135	022	-
•044	023	x	•090	003	3	•136	001	1
•045	310	RC	•091	023	x	•137	012	d
•046	003	3	•092	310	RC	•138	001	1

•139	020	=	•191	004	4	•243	320	=
•140	351	JC	•192	004	4	•244	300	ST
•141	002	2	•193	005	6	•245	007	7
•142	012	d	•194	010	8	•246	204	L 4
•143	006	6	•195	360	B	•247	310	RC
•144	007	7	•196	005	5	•248	007	7
•145	007	7	•197	350	J	•249	035	PA
•146	006	6	•198	033	S S	•250	035	PA
•147	002	2	•199	202	L 2	•251	034	PT
•148	001	1	•200	310	RC	•252	045	PA
•149	013	S	•201	001	2	•253	023	X
•150	023	X	•202	024	4	•254	310	RC
•151	310	RC	•203	310	RC	•255	002	2
•152	006	6	•204	002	2	•256	162	SO
•153	021	+	•205	020	=	•257	024	+
•154	001	1	•206	035	PA	•258	310	RC
•155	012	d	•207	035	PA	•259	004	4
•156	006	6	•208	034	PT	•260	020	=
•157	003	3	•209	035	PA	•261	063	b
•158	006	6	•210	310	RC	•262	034	PT
•159	005	5	•211	004	4	•263	112	D T
•160	011	9	•212	024	4	•264	030	RT
•161	004	4	•213	310	RC			
•162	023	X	•214	002	2			
•163	310	RC	•215	024	4			
•164	006	6	•216	310	RC			
•165	022	-	•217	001	1			
•166	001	1	•218	020	=			
•167	012	d	•219	034	PT			
•168	005	5	•220	112	D T			
•169	003	3	•221	350	J			
•170	006	6	•222	033	S S			
•171	004	4	•223	205	L S			
•172	003	3	•224	020	=			
•173	023	X	•225	300	ST			
•174	310	RC	•226	007	7			
•175	006	6	•227	022	-			
•176	021	+	•228	026	(
•177	002	2	•229	310	RC			
•178	012	d	•230	001	1			
•179	003	3	•231	024	4			
•180	004	4	•232	310	RC			
•181	000	0	•233	002	2			
•182	006	6	•234	027)			
•183	001	1	•235	020	=			
•184	023	X	•236	356	JC			
•185	310	RC	•237	004	4			
•186	006	6	•238	310	RC			
•187	021	+	•239	001	1			
•188	012	d	•240	024	4			
•189	000	0	•241	310	RC			
•190	010	9	•242	002	2			

2

1 Determines an acceptable pipe size by computing HW_o.

•001	037	CL	•047	032	I D	•093	024	÷
•002	031	1	•048	033	S S	•094	310	RC
•003	032	I D	•049	034	PT	•095	002	2
•004	033	S S	•050	306	ST	•096	024	÷
•005	034	PT	•051	012	d	•097	310	RC
•006	306	ST	•052	311	s	•098	011	9
•007	301	2	•053	032	I D	•099	162	SU
•008	032	2	•054	033	S S	•100	024	÷
•009	032	I D	•055	034	PT	•101	107	π
•010	033	S S	•056	306	ST	•102	027	1
•011	034	PT	•057	011	s	•103	162	SU
•012	305	ST	•058	310	RC	•104	024	÷
•013	002	2	•059	004	4	•105	006	5
•014	003	3	•060	162	SU	•106	004	4
•015	032	I D	•061	023	x	•107	012	d
•016	033	S S	•062	310	RC	•108	004	4
•017	034	PT	•063	003	3	•109	026	=
•018	305	ST	•064	023	x	•110	300	ST
•019	003	3	•065	002	2	•111	300	0
•020	004	4	•066	011	s	•112	310	RC
•021	032	I D	•067	024	÷	•113	012	d
•022	033	S S	•068	026	(•114	022	-
•023	034	PT	•069	026	(•115	310	RC
•024	305	ST	•070	310	RC	•116	011	9
•025	004	4	•071	011	9	•117	020	=
•026	005	5	•072	024	÷	•118	356	JC
•027	032	I D	•073	004	4	•119	002	2
•028	033	S S	•074	027)	•120	310	RC
•029	034	PT	•075	025	d	•121	011	9
•030	305	ST	•076	026	(•122	300	ST
•031	005	5	•077	004	4	•123	012	d
•032	006	5	•078	024	÷	•124	202	L 2
•033	032	I D	•079	003	9	•125	310	RC
•034	033	S S	•080	027)	•126	011	9
•035	034	PT	•081	027)	•127	021	+
•036	305	ST	•082	021	+	•128	310	RC
•037	006	5	•083	001	1	•129	012	d
•038	007	7	•084	021	+	•130	024	÷
•039	032	I D	•085	310	RC	•131	002	2
•040	033	S S	•086	005	5	•132	020	=
•041	034	PT	•087	023	x	•133	300	ST
•042	305	ST	•088	026	(•134	013	S
•043	307	7	•089	310	RC	•135	022	-
•044	201	L 1	•090	001	1	•136	310	RC
•045	222	DP 2	•091	023	x	•137	006	5
•046	010	8	•092	004	4	•138	020	=

•139 035 P A
•140 035 P A
•141 356 JC
•142 003 3
•143 310 FC
•144 013 S
•145 034 PT
•146 350 J
•147 004 4
•148 203 L 3
•149 310 RC
•150 005 5
•151 034 PT
•152 310 RC
•153 006 6
•154 204 L 4
•155 112 D T
•156 021 +
•157 310 RC
•158 003 0
•159 021 +
•160 310 RC
•161 007 7
•162 020 =
•163 035 P A
•164 035 P A
•165 034 PT
•166 112 J T
•167 350 J
•168 001 1

2

**Calculates outlet control performance curve data for
pipe culverts.**

•001	037	CL	•047	032	I D	•093	027	
•002	001		•048	033	S S	•094	162	SC
•003	032	I D	•049	034	PT	•095	024	
•004	033	S S	•050	300	ST	•096	006	5
•005	034	PT	•051	010		•097	004	4
•006	300	ST	•052	310	RC	•098	012	3
•007	001		•053	002		•099	004	4
•008	002		•054	162	SC	•100	020	=
•009	032	I D	•055	023	X	•101	300	ST
•010	033	S S	•056	310	RC	•102	000	0
•011	034	PT	•057	001		•103	310	RC
•012	300	ST	•058	023	X	•104	004	4
•013	002		•059	002		•105	022	-
•014	003		•060	011		•106	310	RC
•015	032	I D	•061	024		•107	005	5
•016	033	S S	•062	025	(•108	020	=
•017	034	PT	•063	026	(•109	356	JC
•018	300	ST	•064	310	RC	•110	002	2
•019	003		•065	005	5	•111	310	RC
•020	005	S	•066	024	÷	•112	005	5
•021	032	I D	•067	004	4	•113	300	ST
•022	033	S S	•068	027)	•114	004	4
•023	034	PT	•069	025	2	•115	202	L 2
•024	300	ST	•070	026	(•116	310	RC
•025	005		•071	004	4	•117	005	5
•026	006		•072	024	÷	•118	021	+
•027	032	I D	•073	003	3	•119	310	RC
•028	033	S S	•074	027)	•120	004	4
•029	034	PT	•075	027)	•121	024	÷ 2
•030	300	ST	•076	021	+	•122	002	2
•031	006	S	•077	001	1	•123	020	=
•032	201	L 1	•078	021	+	•124	300	ST
•033	222	DP 2	•079	310	RC	•125	013	S
•034	007		•080	003	3	•126	022	-
•035	032	I D	•081	023	X	•127	310	RC
•036	033	S S	•082	026	(•128	007	7
•037	034	PT	•083	310	RC	•129	020	=
•038	300	ST	•084	010	4	•130	356	JC
•039	007		•085	023	X	•131	003	3
•040	010		•086	004	4	•132	310	RC
•041	032	I D	•087	024	÷	•133	013	S
•042	033	S S	•088	310	RC	•134	350	
•043	034	PT	•089	005	5	•135	004	4
•044	300	ST	•090	162	S)	•136	203	L 3
•045	004		•091	024	÷	•137	310	RC
•046	011		•092	107	R	•138	007	7

• 139 204 L 4
• 140 821 +
• 141 310 RC
• 142 033 0
• 143 021 +
• 144 310 RC
• 145 006 6
• 146 020 =
• 147 035 P A
• 148 035 P A
• 149 034 PT
• 150 112 D T
• 151 350 J
• 152 001 2

2 3

**Calculates outlet velocity for pipe culverts in
outlet control.**

•001	037	CC	•047	005	5	•093	310	RC
•002	222	DF	•048	027	0	•094	005	5
•003	001	1	•049	020	=	•095	022	-
•004	032	I D	•050	001	LC	•096	012	5
•005	033	S S	•051	300	ST	•097	000	0
•006	034	PT	•052	003	5	•098	000	0
•007	300	ST	•053	022	-	•099	005	5
•008	001	1	•054	012	0	•100	001	1
•009	002	2	•055	007	7	•101	006	6
•010	032	I D	•056	001	LC	•102	005	5
•011	033	S S	•057	020	=	•103	007	7
•012	034	PT	•058	351	J C	•104	350	J
•013	300	ST	•059	001	2	•105	002	2
•014	002	2	•060	012	0	•106	201	1
•015	003	3	•061	000	0	•107	012	d
•016	032	I D	•062	011	5	•108	006	5
•017	033	S S	•063	001	1	•109	011	9
•018	034	PT	•064	005	5	•110	005	5
•019	300	ST	•065	305	5	•111	006	5
•020	003	3	•066	006	6	•112	001	1
•021	004	4	•067	305	5	•113	011	9
•022	032	I D	•068	013	8	•114	023	x
•023	033	S S	•069	023	x	•115	310	RC
•024	034	PT	•070	310	PC	•116	005	5
•025	310	ST	•071	005	5	•117	022	-
•026	004	4	•072	022	-	•118	012	d
•027	310	RC	•073	012	0	•119	006	6
•028	002	2	•074	001	1	•120	004	4
•029	024	4	•075	010	9	•121	000	0
•030	026	6	•076	003	3	•122	000	0
•031	003	3	•077	000	0	•123	011	9
•032	002	2	•078	002	2	•124	010	9
•033	012	6	•079	303	3	•125	001	1
•034	002	2	•080	006	6	•126	005	5
•035	024	4	•081	323	x	•127	023	x
•036	310	RC	•082	310	PC	•128	310	RC
•037	003	3	•083	315	5	•129	005	5
•038	027	7	•084	021	4	•130	021	+
•039	002	7	•085	312	0	•131	012	d
•040	024	4	•086	004	4	•132	002	2
•041	026	6	•087	305	5	•133	000	0
•042	310	I D	•088	007	7	•134	001	1
•043	001	1	•089	003	3	•135	007	7
•044	025	8	•090	006	6	•136	000	0
•045	012	2	•091	002	2	•137	005	5
•046	312	0	•092	023	x	•138	007	7

•139	023	X	•191	310			•243	325	
•140	310	RC	•192	301			•244	310	
•141	005	5	•193	324			•245	310	
•142	022	-	•194	302			•246	324	
•143	012	4	•195	327			•247	310	
•144	003	0	•196	310			•248	312	
•145	302	2	•197	312			•249	323	
•146	004	4	•198	320			•250	171	CA
•147	304	4	•199	313			•251	324	
•148	006	5	•200	301	S1		•252	301	
•149	305	3	•201	313			•253	310	
•150	003	3	•202	162	ST		•254	305	
•151	202	L 2	•203	310	ST		•255	323	
•152	020	=	•204	303			•256	167	
•153	161	L-1	•205	310	ST		•257	323	
•154	023	X	•206	313			•258	310	RC
•155	310	RC	•207	351	JC		•259	312	
•156	001	1	•208	310			•260	152	SC
•157	020	=	•209	167	A		•261	327	
•158	300	ST	•210	323			•262	300	RT
•159	006	1	•211	310	HC		•263	314	L
•160	022	-	•212	312			•264	326	C
•161	310	RC	•213	162	ST		•265	310	RC
•162	004	4	•214	342			•266	312	C
•163	020	=	•215	360			•267	162	SC
•164	351	JC	•216	011			•268	322	-
•165	003	3	•217	021			•269	310	AC
•166	310	AC	•218	360			•270	310	
•167	004	4	•219	312			•271	162	SC
•168	350	J	•220	320			•272	313	=
•169	004	4	•221	330	J		•273	002	C
•170	203	L 3	•222	313			•274	023	X
•171	310	RC	•223	210	L		•275	310	RC
•172	000		•224	360			•276	000	
•173	264	L 4	•225	011			•277	327	
•174	300	ST	•226	322			•278	033	RT
•175	007	7	•227	300					
•176	022	-	•228	312					
•177	310	RC	•229	020					
•178	002	1	•230	213	L				
•179	020	=	•231	005					
•180	352	JC	•232	023					
•181	005	3	•233	310	RC				
•182	310	RC	•234	002					
•183	001	1	•235	020					
•184	310	ST	•236	035	PA				
•185	007	7	•237	035	PA				
•186	200	L 5	•238	034	PT				
•187	310	RC	•239	112	AT				
•188	307		•240	351	J				
•189	002	-	•241	300	S				
•190	020	C	•242	211	L				

Calculates performance of a thin-edged projecting inlet
on a pipe culvert.

•001	037	CL	•049	020	=	•097	310	RC	
•002	001	1	•050	000	ST	•098	006		6
•003	032	I D	•051	006	6	•099	021	+	
•004	033	S S	•052	023	X	•100	012	a	
•005	034	PT	•053	012	d	•101	005	5	
•006	300	ST	•054	000	0	•102	006	6	
•007	001	1	•055	000	0	•103	007	7	
•008	002	2	•056	000	0	•104	007	7	
•009	032	I D	•057	000	0	•105	001	1	
•010	033	S S	•058	010	9	•106	023	X	
•011	034	PT	•059	011	3	•107	310	RC	
•012	300	ST	•060	006	6	•108	006	6	
•013	002	2	•061	006	6	•109	021	+	
•014	303	3	•062	001	1	•110	012	d	
•015	032	I D	•063	022	-	•111	001	1	
•016	033	S S	•064	012	d	•112	010	5	
•017	034	PT	•065	000	0	•113	007	7	
•018	300	ST	•066	000	0	•114	003	3	
•019	003	3	•067	003	3	•115	002	2	
•020	004	4	•068	004	4	•116	001	1	
•021	032	I D	•069	003	3	•117	023	X	
•022	033	S S	•070	006	6	•118	310	RC	
•023	034	PT	•071	000	0	•119	004	4	
•024	300	ST	•072	002	2	•120	020	=	
•025	004	4	•073	023	X	•121	300	ST	
•026	001	1	•074	310	RC	•122	007	7	
•027	300	ST	•075	006	5	•123	001	1	
•028	000	0	•076	021	+	•124	302	ST-	
•029	201	L 1	•077	012	d	•125	000	0	
•030	222	DP 2	•078	000	0	•126	310	RC	
•031	005	5	•079	004	4	•127	000	0	
•032	032	I D	•080	004	4	•128	352	JC	
•033	033	S S	•081	007	7	•129	003	3	
•034	034	PT	•082	000	0	•130	310	RC	
•035	300	ST	•083	005	5	•131	001	1	
•036	005	5	•084	002	2	•132	022	-	
•037	024	4	•085	023	X	•133	310	RC	
•038	310	RC	•086	310	RC	•134	007	7	
•039	003	3	•087	006	6	•135	020	=	
•040	024	4	•088	022	-	•136	300	ST	
•041	026	6	•089	012	d	•137	010	3	
•042	310	RC	•090	001	1	•138	022	-	
•043	004	4	•091	005	5	•139	310	RC	
•044	025	d	•092	006	6	•140	002	2	
•045	001	1	•093	003	5	•141	020	=	
•046	012	0	•094	004	4	•142	300	ST	
•047	005	5	•095	004	4	•143	012	d	
•048	027	7	•096	023	X	•144	352	JC	

•145 004 4
•146 310 RC 2
•147 002 2
•148 300 ST 3
•149 010 0
•150 000 0
•151 300 ST 4
•152 012 d
•153 204 L 4
•154 310 RC 8
•155 010 8
•156 035 P A
•157 035 P A
•158 034 PT
•159 112 D T
•160 310 RC
•161 012 d
•162 035 P A
•163 035 P A
•164 102 F 2
•165 034 PT
•166 112 D T
•167 203 L 3
•168 310 RC
•169 010 8
•170 021 +
•171 310 RC
•172 007 7
•173 020 =
•174 035 P A
•175 035 P A
•176 024 PT
•177 112 D T
•178 350 J
•179 001 2

2 5 Calculates performance of an inlet with square edges on
a pipe culvert.

•001	037	CL	•049	026	=	•097	310	RC
•002	001	i	•050	303	ST	•098	006	s
•003	032	I D	•051	006	6	•099	321	+
•004	033	S S	•052	023	x	•100	312	d
•005	034	PT	•053	012	o	•101	007	7
•006	300	ST	•054	000	o	•102	000	0
•007	001	2	•055	000	o	•103	006	6
•008	002	2	•056	000	o	•104	005	5
•009	032	I D	•057	002	2	•105	007	7
•010	033	S S	•058	005	5	•106	010	8
•011	034	PT	•059	000	o	•107	023	x
•012	300	ST	•060	006	6	•108	310	RC
•013	002	2	•061	001	1	•109	006	6
•014	003	3	•062	011	9	•110	021	+
•015	032	I D	•063	022	-	•111	012	d
•016	033	S S	•064	012	d	•112	000	0
•017	034	PT	•065	000	o	•113	010	9
•018	300	ST	•066	000	o	•114	007	7
•019	003	3	•067	006	6	•115	004	4
•020	004	4	•068	306	6	•116	010	8
•021	032	I D	•069	001	1	•117	003	3
•022	033	S S	•070	006	6	•118	023	x
•023	034	PT	•071	005	5	•119	310	RC
•024	300	ST	•072	001	1	•120	004	4
•025	004	4	•073	023	x	•121	020	=
•026	001	2	•074	310	RC	•122	300	ST
•027	300	ST	•075	006	6	•123	017	7
•028	000	0	•076	021	+	•124	001	1
•029	201	L 2	•077	012	d	•125	302	ST-
•030	222	DP	•078	000	o	•126	000	0
•031	005	5	•079	006	6	•127	310	RC
•032	032	I D	•080	006	6	•128	000	0
•033	033	S S	•081	307	7	•129	352	JC
•034	034	PT	•082	000	o	•130	003	3
•035	300	ST	•083	040	o	•131	310	KC
•036	005	5	•084	001	1	•132	001	1
•037	024	÷	•085	023	x	•133	022	-
•038	310	RC	•086	310	RC	•134	310	RC
•039	003	3	•087	006	6	•135	007	7
•040	324	÷	•088	022	-	•136	020	=
•041	026	(•089	012	d	•137	300	ST
•042	310	RL	•090	002	2	•138	010	8
•043	004	4	•091	005	5	•139	022	-
•044	025	4	•092	003	3	•140	310	RC
•045	001	2	•093	002	2	•141	002	2
•046	012	d	•094	011	9	•142	020	=
•047	005	5	•095	005	5	•143	300	ST
•048	027)	•096	023	x	•144	012	d

•145 352 JC
•146 004 4
•147 310 RC
•148 002 2
•149 300 ST
•150 010 8
•151 000 0
•152 300 ST
•153 012 6
•154 204 L 4
•155 310 RC
•156 010 9
•157 035 P A
•158 035 P A
•159 034 FT
•160 112 D T
•161 310 RC
•162 012 6
•163 035 P A
•164 035 P A
•165 102 F 2
•166 034 PT
•167 112 D T
•168 203 L 8
•169 310 RC
•170 013 9
•171 021 +
•172 310 RC
•173 007 7
•174 020 =
•175 035 P A
•176 035 P A
•177 034 PT
•178 112 D T
•179 350 J
•180 001 1

Calculates performance of an inlet with 45° bevels on a pipe culvert.

•001	037	CL	•048	027)	•096	310	RC
•002	•031	1	•049	020	=	•097	006	6
•003	032	ID	•050	300	ST	•098	021	+
•004	033	S S	•051	006	6	•099	012	d
•005	034	PT	•052	023	x	•100	007	7
•006	300	ST	•053	012	d	•101	006	6
•007	001	1	•054	000	o	•102	006	6
•008	002	2	•055	000	o	•103	005	5
•009	032	ID	•056	000	o	•104	001	1
•010	033	S S	•057	004	4	•105	002	2
•011	034	PT	•058	001	1	•106	023	x
•012	300	ST	•059	006	6	•107	310	RC
•013	002	2	•060	007	7	•108	006	6
•014	003	3	•061	006	6	•109	021	+
•015	032	ID	•062	022	-	•110	012	d
•016	033	S S	•063	012	d	•111	000	0
•017	034	PT	•064	000	o	•112	006	6
•018	300	ST	•065	000	o	•113	003	3
•019	003	3	•066	011	9	•114	003	3
•020	004	4	•067	010	8	•115	004	4
•021	032	ID	•068	003	3	•116	003	3
•022	033	S S	•069	006	5	•117	023	x
•023	034	PT	•070	011	9	•118	310	RC
•024	300	ST	•071	005	5	•119	004	4
•025	004	4	•072	023	x	•120	020	=
•026	001	1	•073	310	RC	•121	300	ST
•027	300	ST	•074	006	6	•122	007	7
•028	000	3	•075	021	+	•123	001	1
•029	201	L 1	•076	012	d	•124	302	ST-
•030	222	DP 2	•077	000	o	•125	000	0
•031	005	5	•078	010	8	•126	310	RC
•032	032	ID	•079	007	7	•127	000	0
•033	033	S S	•080	006	6	•128	352	JC
•034	034	PT	•081	007	7	•129	003	3
•035	300	ST	•082	000	o	•130	310	RC
•036	005	5	•083	001	1	•131	001	1
•037	024	4	•084	023	x	•132	022	-
•038	310	RC	•085	310	RC	•133	310	RC
•039	003	3	•086	006	6	•134	007	7
•040	024	4	•087	022	-	•135	020	=
•041	026	6	•088	012	d	•136	300	ST
•042	310	RC	•089	003	3	•137	010	8
•043	004	4	•090	001	1	•138	022	-
•044	025	d	•091	006	6	•139	310	RC
•045	001	1	•092	000	o	•140	002	2
•046	012	d	•093	011	9	•141	020	=
•047	005	5	•094	007	7	•142	300	ST
			•095	023	x	•143	012	d

•144 352 JC
•145 004 4
•146 310 RC
•147 002 2
•148 300 ST
•149 010 3
•150 063 0
•151 300 ST
•152 012 6
•153 204 L 4
•154 310 RC
•155 010 8
•156 035 P A
•157 035 P A
•158 034 PT
•159 112 D T
•160 310 RC
•161 012 d
•162 035 P A
•163 035 F A
•164 102 F 2
•165 034 PT
•166 112 D T
•167 203 L 3
•168 310 RC
•169 010 B
•170 021 +
•171 310 RC
•172 007 7
•173 020 =
•174 035 P A
•175 035 P A
•176 034 PT
•177 112 D T
•178 350 J
•179 001 1

2 7 Calculates the performance of a groove end projecting inlet on a pipe culvert.

•001	037	CL	•050	300	ST	•099	012	d
•002	001	1	•051	006	6	•100	006	6
•003	032	I D	•052	023	x	•101	006	6
•004	033	S S	•053	012	c	•102	002	2
•005	034	PT	•054	000	0	•103	003	3
•006	300	ST	•055	000	0	•104	010	8
•007	001	1	•056	000	0	•105	001	1
•008	002	2	•057	002	2	•106	023	x
•009	032	I D	•058	000	0	•107	310	RC
•010	033	S S	•059	005	5	•108	036	6
•011	034	PT	•060	000	0	•109	021	+
•012	300	ST	•061	005	5	•110	012	d
•013	002	2	•062	002	2	•111	001	1
•014	003	3	•063	022	-	•112	000	0
•015	032	I D	•064	012	a	•113	010	3
•016	033	S S	•065	000	0	•114	007	7
•017	034	PT	•066	000	0	•115	010	8
•018	300	ST	•067	005	5	•116	006	6
•019	003	3	•068	005	5	•117	023	x
•020	004	4	•069	007	7	•118	310	RC
•021	032	I D	•070	010	9	•119	004	4
•022	033	S S	•071	011	9	•120	020	=
•023	034	PT	•072	023	x	•121	300	ST
•024	300	ST	•073	310	RC	•122	007	7
•025	004	4	•074	006	6	•123	001	1
•026	001	2	•075	021	+	•124	302	ST-
•027	300	ST	•076	012	d	•125	000	0
•028	000	0	•077	000	0	•126	310	RC
•029	201	L 1	•078	005	5	•127	000	0
•030	222	DP	•079	007	7	•128	352	JC
•031	005	5	•080	011	9	•129	003	3
•032	032	I D	•081	005	5	•130	310	RC
•033	033	S S	•082	010	8	•131	001	1
•034	034	PT	•083	005	5	•132	022	-
•035	300	ST	•084	023	x	•133	310	RC
•036	005	5	•085	310	RC	•134	007	7
•037	024	÷	•086	006	6	•135	020	=
•038	310	RC	•087	022	-	•136	300	ST
•039	003	3	•088	012	d	•137	010	3
•040	024	÷	•089	002	2	•138	022	-
•041	026	(•090	003	3	•139	310	RC
•042	310	RC	•091	003	3	•140	002	2
•043	004	4	•092	010	8	•141	020	=
•044	025	d	•093	000	0	•142	300	ST
•045	001	1	•094	001	1	•143	012	d
•046	012	d	•095	023	x	•144	352	JC
•047	005	s	•096	310	RC	•145	004	4
•048	027)	•097	006	6	•146	310	RC
•049	020	=	•098	021	+	•147	002	2

•148	300	ST
•149	310	3
•150	600	0
•151	300	ST
•152	012	d
•153	204	L 4
•154	310	RC
•155	010	3
•156	035	P A
•157	035	P A
•158	034	PT
•159	112	D T
•160	310	RC
•161	012	d
•162	035	P A
•163	035	P A
•164	102	F2
•165	034	PT
•166	112	D T
•167	203	L 3
•168	310	RC
•169	010	3
•170	021	+
•171	310	RC
•172	007	?
•173	020	=
•174	035	P A
•175	035	P A
•176	034	PT
•177	112	D T
•178	350	J
•179	001	1.

Calculates the performance of a groove end inlet with
headwalls on a pipe culvert.

•001	037	CL	•050	300	ST	•098	006	6
•002	001	1	•051	006	6	•099	021	+
•003	032	I D	•052	023	x	•100	012	d
•004	033	S S	•053	J12	d	•101	006	5
•005	034	PT	•054	000	0	•102	005	5
•006	300	ST	•055	000	0	•103	003	3
•007	001	1	•056	000	0	•104	005	5
•008	002	2	•057	002	2	•105	006	5
•009	032	I D	•058	004	4	•106	002	2
•010	033	S S	•059	002	2	•107	023	x
•011	034	PT	•060	010	E	•108	310	RC
•012	300	ST	•061	003	3	•109	006	6
•013	002	2	•062	002	2	•110	021	+
•014	003	3	•063	022	-	•111	012	d
•015	032	I D	•064	012	d	•112	001	1
•016	033	S S	•065	000	0	•113	001	1
•017	034	PT	•066	000	0	•114	004	4
•018	300	ST	•067	006	6	•115	000	0
•019	003	3	•068	001	1	•116	011	9
•020	004	4	•069	006	6	•117	011	9
•021	032	I D	•070	003	3	•118	023	x
•022	033	S S	•071	003	3	•119	310	RC
•023	034	PT	•072	010	9	•120	004	4
•024	300	ST	•073	023	x	•121	020	=
•025	004	4	•074	310	RC	•122	300	ST
•026	001	1	•075	006	6	•123	007	7
•027	300	ST	•076	J21	+	•124	001	1
•028	000	0	•077	012	d	•125	302	ST-
•029	201	L 1	•078	000	0	•126	000	0
•030	222	DP	•079	005	5	•127	310	RC
•031	005	5	•080	011	9	•128	000	0
•032	032	I D	•081	007	7	•129	352	JC
•033	033	S S	•082	007	7	•130	003	3
•034	034	PT	•083	002	2	•131	310	RC
•035	300	ST	•084	003	3	•132	001	1
•036	005	5	•085	023	x	•133	022	=
•037	024	+	•086	310	RC	•134	310	RC
•038	310	RC	•087	006	6	•135	007	7
•039	003	3	•088	022	-	•136	020	=
•040	024	+	•089	012	d	•137	300	ST
•041	026	(•090	002	2	•138	010	8
•042	310	RC	•091	003	3	•139	022	=
•043	004	4	•092	J03	3	•140	310	RC
•044	025	d	•093	006	6	•141	002	2
•045	001	1	•094	001	1	•142	020	=
•046	012	d	•095	J05	5	•143	300	ST
•047	005	5	•096	023	x	•144	012	d
•048	027)	•097	310	RC	•145	352	JC
•049	020	=						

•146 004 4
•147 310 RC 2
•148 002 2
•149 300 ST
•150 010 8
•151 000 0
•152 300 ST
•153 012 d
•154 204 L 4
•155 310 RC
•156 010 8
•157 035 P A
•158 035 P A
•159 034 PT
•160 112 D T
•161 310 RC
•162 012 d
•163 035 P A
•164 035 P A
•165 102 F2
•166 034 PT
•167 112 D T
•168 203 L 3
•169 310 RC
•170 010 8
•171 021 +
•172 310 RC
•173 007 7
•174 020 =
•175 035 P A
•176 035 P A
•177 034 PT
•178 112 D T
•179 350 J
•180 001 1

Calculates performance of a tapered inlet throat in a smooth pipe culvert.

•001	037	CL	•049	020	=	•097	012	d
•002	001	1	•050	300	ST	•098	002	2
•003	032	ID	•051	006	x	•099	001	1
•004	033	S S	•052	023	x	•100	001	1
•005	034	PT	•053	012	d	•101	005	5
•006	306	ST	•054	000	o	•102	023	x
•007	061	1	•055	000	o	•103	310	RC
•008	062	2	•056	000	o	•104	004	=
•009	032	ID	•057	000	o	•105	020	4
•010	033	S S	•058	003	3	•106	300	ST
•011	034	PT	•059	013	s	•107	007	7
•012	306	ST	•060	021	+	•108	001	1
•013	002	2	•061	012	o	•109	302	ST-
•014	003	3	•062	000	o	•110	300	0
•015	032	ID	•063	000	o	•111	310	RC
•016	033	S S	•064	000	o	•112	000	0
•017	034	PT	•065	003	3	•113	352	JC
•018	306	ST	•066	023	x	•114	003	3
•019	002	3	•067	310	RC	•115	310	RC
•020	004	4	•068	006	6	•116	001	1
•021	032	ID	•069	021	+	•117	022	-
•022	033	S S	•070	012	d	•118	310	RC
•023	034	PT	•071	000	3	•119	007	7
•024	306	ST	•072	000	o	•120	020	=
•025	004	4	•073	004	4	•121	300	ST
•026	001	1	•074	002	2	•122	010	8
•027	306	ST	•075	023	x	•123	022	-
•028	000	0	•076	310	RC	•124	310	RC
•029	201	L 2	•077	006	s	•125	002	2
•030	222	DP	•078	022	-	•126	020	=
•031	005	5	•079	012	o	•127	300	ST
•032	032	ID	•080	000	o	•128	012	a
•033	033	S S	•081	004	4	•129	352	JC
•034	034	PT	•082	001	1	•130	304	4
•035	306	ST	•083	004	4	•131	310	RC
•036	005	5	•084	023	x	•132	002	2
•037	024	+	•085	310	RC	•133	300	ST
•038	310	RC	•086	006	6	•134	010	8
•039	003	3	•087	021	+	•135	000	0
•040	024	+	•088	012	d	•136	300	ST
•041	026	6	•089	003	3	•137	012	d
•042	310	PC	•090	011	3	•138	204	L 4
•043	004	4	•091	002	2	•139	310	RC
•044	025	a	•092	007	7	•140	010	b
•045	011	2	•093	023	x	•141	035	F A
•046	012	3	•094	310	RC	•142	035	F A
•047	005	5	•095	006	6	•143	034	PT
•048	027	7	•096	021	+	•144	112	U T

•145	310	HC
•146	012	C
•147	035	P A
•148	035	P A
•149	102	F ₂
•150	034	PT
•151	112	D T
•152	203	L 3
•153	310	RC
•154	040	9
•155	021	+
•156	310	RC
•157	007	7
•158	020	=
•159	035	P A
•160	035	P A
•161	034	PT
•162	112	U T
•163	350	J
•164	001	1

Calculates the performance of a tapered inlet throat
in a rough pipe culvert.

•001	037	CL	•049	020	=	•097	012	d
•002	001	1	•050	300	ST	•098	002	2
•003	032	ID	•051	006	x	•099	002	2
•004	033	S S	•052	023	x	•100	005	5
•005	034	PT	•053	012	d	•101	002	2
•006	300	ST	•054	000	x	•102	023	x
•007	001	1	•055	000	x	•103	310	RC
•008	002	2	•056	000	x	•104	004	=
•009	032	ID	•057	000	x	•105	020	ST
•010	033	S S	•058	003	x	•106	300	7
•011	034	PT	•059	013	s	•107	007	1
•012	300	ST	•060	021	+ s	•108	001	ST
•013	002	2	•061	012	+ s	•109	302	0
•014	003	3	•062	000	+ s	•110	000	RC
•015	032	ID	•063	000	+ s	•111	310	JC
•016	033	S S	•064	000	+ s	•112	000	3
•017	034	PT	•065	005	+ s	•113	352	RC
•018	300	ST	•066	023	x	•114	003	=
•019	003	3	•067	310	RC	•115	310	RC
•020	004	4	•068	006	x	•116	001	1
•021	032	ID	•069	021	+ s	•117	022	RC
•022	033	S S	•070	012	+ d	•118	310	7
•023	034	PT	•071	000	+ s	•119	007	=
•024	300	ST	•072	000	+ s	•120	020	ST
•025	004	4	•073	001	+ s	•121	300	8
•026	001	1	•074	001	+ s	•122	010	-
•027	300	ST	•075	023	x	•123	022	-
•028	000	5	•076	310	RC	•124	310	RC
•029	201	L	•077	006	x	•125	002	2
•030	222	DF	•078	022	-	•126	020	=
•031	065	5	•079	012	+ d	•127	300	ST
•032	032	ID	•080	000	+ d	•128	012	0
•033	033	S S	•081	002	+ s	•129	352	JC
•034	034	PT	•082	005	+ s	•130	004	+
•035	300	ST	•083	002	+ s	•131	310	RC
•036	005	5	•084	023	x	•132	002	2
•037	024	÷	•085	310	RC	•133	300	ST
•038	310	RL	•086	006	x	•134	010	8
•039	003	3	•087	021	+ s	•135	000	0
•040	024	÷	•088	012	+ s	•136	300	ST
•041	026	(•089	003	+ s	•137	012	0
•042	310	RC	•090	004	+ s	•138	204	L
•043	004	4	•091	007	+ s	•139	310	RC
•044	025	d	•092	001	+ s	•140	010	3
•045	001	1	•093	023	x	•141	035	P A
•046	012	d	•094	310	RC	•142	035	P A
•047	005	5	•095	006	x	•143	034	FT
•048	027)	•096	021	+ s	•144	112	D T

• 145 310 RC
• 146 012 d
• 147 035 P A
• 148 035 P A
• 149 102 F2
• 150 034 PT
• 151 112 U T
• 152 203 L 3
• 153 310 RC
• 154 010
• 155 021 +
• 156 310 RC
• 157 037
• 158 020 =
• 159 035 P A
• 160 035 P A
• 161 034 PT
• 162 112 U T
• 163 350
• 164 061

2 11

Calculates B_f and L_1 for a side-tapered inlet on a pipe culvert if the face has projecting thin edges.

•001	037	CL	•046	300	ST	•091	001	1
•002	001	1	•047	007	7	•092	012	d
•003	032	I D	•048	001	1	•093	010	s
•004	033	S S	•049	300	ST	•094	001	1
•005	034	PT	•050	013	S	•095	006	5
•006	022	-	•051	300	ST	•096	007	7
•007	002	2	•052	012	d	•097	023	x
•008	032	I D	•053	201	L 1	•098	310	RC
•009	033	S S	•054	310	RC	•099	010	s
•010	034	PT	•055	001	1	•100	021	+
•011	300	ST	•056	022	-	•101	001	1
•012	003	3	•057	310	RC	•102	012	d
•013	020	=	•058	013	S	•103	001	1
•014	300	ST	•059	024	÷	•104	005	5
•015	001	1	•060	310	RC	•105	005	05
•016	003	3	•061	006	6	•106	005	5
•017	032	I D	•062	020	=	•107	023	x
•018	033	S S	•063	300	ST	•108	310	RC
•019	034	PT	•064	010	9	•109	010	s
•020	300	ST	•065	023	x	•110	021	+
•021	002	2	•066	012	d	•111	012	d
•022	004	4	•067	000	0	•112	000	0
•023	032	I D	•068	001	1	•113	001	1
•024	033	S S	•069	004	4	•114	004	4
•025	034	PT	•070	010	9	•115	004	4
•026	300	ST	•071	013	S	•116	023	x
•027	004	4	•072	021	+	•117	310	RC
•028	005	5	•073	012	d	•118	007	7
•029	032	I D	•074	001	1	•119	020	=
•030	033	S S	•075	011	9	•120	063	x
•031	034	PT	•076	007	7	•121	023	x
•032	300	ST	•077	004	4	•122	004	4
•033	005	5	•078	023	x	•123	024	÷
•034	006	6	•079	310	RC	•124	107	n
•035	032	I D	•080	010	9	•125	024	+
•036	033	S S	•081	022	-	•126	310	RC
•037	034	PT	•082	012	d	•127	006	6
•038	300	ST	•083	011	9	•128	020	=
•039	006	6	•084	006	6	•129	035	P A
•040	222	DP 2	•085	004	4	•130	035	P A
•041	062	r	•086	002	2	•131	034	PT
•042	024	+	•087	023	x	•132	112	D T
•043	310	RC	•088	310	RC	•133	033	S S
•044	005	s	•089	010	9	•134	022	-
•045	020	=	•090	021	+	•135	310	RC

•136	004	4	•186	105	Fs
•137	024	÷	•189	021	+
•138	002	2	•190	310	RC
•139	023	×	•191	033	
•140	310	RC	•192	020	=
•141	002	2	•193	035	FA
•142	106	I	•194	035	FA
•143	020	=	•195	034	PT
•144	300	ST	•196	112	LT
•145	000	0	•197	350	J
•146	001	1	•198	033	S S
•147	302	ST-			
•148	012	d			
•149	310	RC			
•150	012	d			
•151	352	JC			
•152	002	2			
•153	310	RC			
•154	000	0			
•155	023	×			
•156	310	RC			
•157	002	2			
•158	105	Fs			
•159	020	=			
•160	300	ST			
•161	013	S			
•162	022	-			
•163	001	1			
•164	020	=			
•165	356	JC			
•166	002	2			
•167	310	RC			
•168	000	0			
•169	023	×			
•170	310	RC			
•171	002	2			
•172	105	Fs			
•173	020	=			
•174	300	ST			
•175	013	S			
•176	350	J			
•177	001	1			
•178	202	L 2			
•179	035	FA			
•180	035	FA			
•181	310	RC			
•182	000	J			
•183	034	PT			
•184	112	LT			
•185	023	Y			
•186	310	RC			
•187	002	2			

2 12

Calculates B_f and L_1 for a side-tapered inlet on a pipe culvert if the face has square edges in a headwall.

•001	037	CL	•047	007	7	•093	011	9
•002	001	2	•048	001	1	•094	007	7
•003	032	I D	•049	300	ST	•095	010	3
•004	033	S S	•050	013	S	•096	004	4
•005	034	PT	•051	300	ST	•097	023	x
•006	022	-	•052	012	d	•098	310	RC
•007	002	?	•053	201	L 1	•099	010	9
•008	032	I D	•054	310	RC	•100	021	+
•009	033	S S	•055	001	1	•101	012	d
•010	034	PT	•056	022	-	•102	011	9
•011	300	ST	•057	310	RC	•103	004	4
•012	033	3	•058	013	S	•104	002	2
•013	020	=	•059	024	÷	•105	006	5
•014	300	ST	•060	310	RC	•106	023	x
•015	001	1	•061	006	6	•107	310	RC
•016	003	3	•062	020	=	•108	010	8
•017	032	I D	•063	300	ST	•109	022	-
•018	033	S S	•064	010	9	•110	012	d
•019	034	PT	•065	023	x	•111	000	0
•020	300	ST	•066	012	d	•112	000	0
•021	002	2	•067	003	0	•113	004	4
•022	004	4	•068	003	3	•114	010	8
•023	032	I D	•069	005	5	•115	023	x
•024	033	S S	•070	007	7	•116	310	RC
•025	034	PT	•071	013	S	•117	007	7
•026	300	ST	•072	021	+	•118	020	=
•027	004	4	•073	012	d	•119	063	x
•028	005	5	•074	004	4	•120	023	x
•029	032	I D	•075	002	2	•121	004	4
•030	033	S S	•076	002	2	•122	024	÷
•031	034	PT	•077	010	8	•123	107	π
•032	300	ST	•078	023	x	•124	024	÷
•033	005	5	•079	310	RC	•125	310	RC
•034	006	6	•080	010	9	•126	006	6
•035	032	I D	•081	022	-	•127	020	=
•036	033	S S	•082	001	1	•128	035	P A
•037	034	PT	•083	012	d	•129	035	P A
•038	300	ST	•084	007	7	•130	034	PT
•039	006	6	•085	011	9	•131	112	D T
•040	222	DP 2	•086	002	2	•132	033	S S
•041	052	r	•087	023	x	•133	022	-
•042	024	+	•088	310	RC	•134	310	RC
•043	310	RC	•089	010	8	•135	004	4
•044	005	5	•090	021	+	•136	024	÷
•045	020	=	•091	002	2	•137	002	2
•046	300	ST	•092	012	d	•138	023	x

•139	310	RC		•191	020		
•140	002	I	2	•192	033	P	A
•141	106	I		•193	035	P	A
•142	020	=		•194	034	F	T
•143	360	ST		•195	112	E	T
•144	000	O		•196	350	J	
•145	001	I		•197	033	S	S
•146	302	ST					
•147	012	d					
•148	310	RC					
•149	012	a					
•150	352	JC					
•151	002	I	2				
•152	310	RC					
•153	000	O					
•154	023	x					
•155	310	RC					
•156	002	I	2				
•157	105	Fs					
•158	320	=					
•159	300	ST					
•160	013	S					
•161	022	-					
•162	001	I	2				
•163	020	=					
•164	356	JC					
•165	002	I	2				
•166	310	RC					
•167	000	O					
•168	023	x					
•169	310	RC					
•170	002	I	2				
•171	105	Fs					
•172	020	=					
•173	300	ST					
•174	013	S					
•175	350	J					
•176	001	I	2				
•177	202	L	2				
•178	035	F A					
•179	035	F A					
•180	310	RC					
•181	000	O					
•182	034	PT					
•183	112	D T					
•184	023	x					
•185	310	RC					
•186	002	I	2				
•187	105	Fs					
•188	021	+					
•189	310	RC					
•190	003	I	3				

Calculates B_f and L_1 for a side-tapered inlet on a pipe culvert if the face has 45° bevels or a grooved end.

•001	037	CL	•047	007	7	•093	002	2
•002	JJ1	1	•048	001	1	•094	011	9
•003	032	ID	•049	300	ST	•095	011	3
•004	033	S S	•050	013	S	•096	004	4
•005	034	PT	•051	300	ST	•097	023	x
•006	022	-	•052	012	d	•098	310	RC
•007	002	2	•053	201	L	•099	010	+
•008	032	ID	•054	310	RC	•100	021	d
•009	033	S S	•055	001	1	•101	012	7
•010	034	PT	•056	022	-	•102	007	3
•011	300	ST	•057	310	RC	•103	003	9
•012	003	3	•058	013	S	•104	011	3
•013	020	=	•059	024	÷	•105	003	2
•014	300	ST	•060	310	RC	•106	002	x
•015	001	1	•061	006	s	•107	023	RC
•016	003	3	•062	020	=	•108	310	9
•017	032	ID	•063	300	ST	•109	010	3
•018	033	S S	•064	010	s	•110	023	x
•019	034	PT	•065	023	x	•111	310	RC
•020	300	ST	•066	012	d	•112	007	7
•021	002	2	•067	000	3	•113	020	=
•022	004	4	•068	002	2	•114	063	x
•023	032	ID	•069	010	3	•115	023	x
•024	033	S S	•070	007	7	•116	004	4
•025	034	PT	•071	013	s	•117	024	÷
•026	300	ST	•072	021	+	•118	107	π
•027	004	4	•073	012	o	•119	024	+
•028	005	5	•074	003	3	•120	310	RC
•029	032	ID	•075	007	7	•121	006	6
•030	033	S S	•076	004	4	•122	020	=
•031	034	PT	•077	004	4	•123	035	PA
•032	300	ST	•078	023	x	•124	035	PA
•033	005	5	•079	310	RC	•125	034	PT
•034	006	5	•080	010	s	•126	112	DT
•035	032	ID	•081	022	-	•127	033	S S
•036	033	S S	•082	001	1	•128	022	-
•037	034	PT	•083	012	d	•129	310	RC
•038	300	ST	•084	007	7	•130	004	4
•039	006	6	•085	006	6	•131	024	÷
•040	222	DP	•086	004	4	•132	002	2
•041	002	r	•087	023	x	•133	023	x
•042	024	÷	•088	310	RC	•134	310	RC
•043	310	RC	•089	010	s	•135	002	2
•044	005	s	•090	021	+	•136	106	I
•045	020	=	•091	003	3	•137	020	=
•046	300	ST	•092	012	d	•138	300	ST

•139	000	0	•191	350	J
•140	001	1	•192	033	S S
•141	302	ST-			
•142	012	d			
•143	310	RC			
•144	012	o			
•145	352	JC			
•146	002	2			
•147	310	RC			
•148	000	o			
•149	023	x			
•150	310	RC			
•151	002	2			
•152	105	Fs			
•153	020	=			
•154	300	ST			
•155	013	S			
•156	022	-			
•157	001	1			
•158	020	=			
•159	356	JC			
•160	002	2			
•161	310	RC			
•162	000	o			
•163	023	x			
•164	310	RC			
•165	002	2			
•166	105	Fs			
•167	020	=			
•168	300	ST			
•169	013	S			
•170	350	J			
•171	001	1			
•172	202	L 2			
•173	035	P A			
•174	035	P A			
•175	310	RC			
•176	000	o			
•177	034	PT			
•178	112	o 1			
•179	023	x			
•180	310	RC			
•181	002	2			
•182	105	Fs			
•183	021	+			
•184	310	RC			
•185	003	o			
•186	020	=			
•187	035	P A			
•188	035	P A			
•189	034	PT			
•190	112	L T			

Calculates outlet velocity for circular pipes in inlet control.

•001	037	CL	•047	024	÷	•093	021	+
•002	031	1	•048	026	(•094	012	8
•003	032	ID	•049	310	RC	•095	003	3
•004	033	SS	•050	302	2	•096	000	0
•005	034	PT	•051	025	3	•097	006	5
•006	300	ST	•052	026	4	•098	003	3
•007	001	1	•053	010	5	•099	006	6
•008	002	2	•054	024	6	•100	003	3
•009	032	ID	•055	003	7	•101	011	9
•010	033	SS	•056	027)	•102	350	J
•011	034	PT	•057	027)	•103	003	3
•012	300	ST	•058	020	=	•104	201	L 1
•013	002	2	•059	300	ST	•105	310	RC
•014	003	3	•060	306	s	•106	006	6
•015	032	ID	•061	061	LG	•107	022	-
•016	033	SS	•062	300	ST	•108	012	d
•017	034	PT	•063	007	7	•109	003	3
•018	300	ST	•064	161	L-1	•110	004	a
•019	003	3	•065	022	-	•111	020	=
•020	004	4	•066	012	o	•112	355	JC
•021	032	ID	•067	002	2	•113	002	2
•022	033	SS	•068	004	4	•114	001	1
•023	034	PT	•069	020	=	•115	012	o
•024	300	ST	•070	355	JC	•116	001	1
•025	004	4	•071	001	1	•117	002	2
•026	005	5	•072	012	3	•118	005	5
•027	032	ID	•073	001	1	•119	010	9
•028	033	SS	•074	011	9	•120	003	3
•029	034	PT	•075	002	2	•121	006	6
•030	300	ST	•076	006	5	•122	023	x
•031	005	5	•077	001	1	•123	310	RC
•032	222	DP	•078	005	5	•124	007	7
•033	062	7	•079	023	x	•125	021	+
•034	003	3	•080	310	RC	•126	002	2
•035	024	÷	•081	007	7	•127	012	d
•036	001	1	•082	021	+	•128	000	0
•037	012	c	•083	012	d	•129	011	9
•038	004	4	•084	011	9	•130	007	7
•039	010	8	•085	300	o	•131	005	5
•040	006	6	•086	007	7	•132	003	3
•041	023	x	•087	010	3	•133	002	2
•042	310	RC	•088	010	8	•134	023	x
•043	004	4	•089	004	4	•135	310	RC
•044	023	x	•090	023	x	•136	007	7
•045	310	RC	•091	310	RC	•137	021	+
•046	003	3	•092	007	7	•138	012	d



Publications listed below are not available from the Government Printing Office. These publications are available in limited numbers to State highway agencies and other public agencies from the Federal Highway Administration. Requests for these documents and suggestions on the contents of any publications should be addressed to the Federal Highway Administration, Office of Engineering, Bridge Division, HNG-31, Washington, D.C. 20590

Hydraulic Design Series

- HDS No. 2 Discontinued
HDS No. 3 DESIGN CHARTS FOR OPEN-CHANNEL FLOW - 1961, Reprinted 1973
HDS No. 4 DESIGN OF ROADSIDE DRAINAGE CHANNELS - 1965

Hydraulic Engineering Circulars

- HEC No. 1 SELECTED BIBLIOGRAPHY OF HYDRAULIC AND HYDROLOGIC SUBJECTS - December 1979
HEC No. 2, 4, 6, 7 and 8 Discontinued
HEC No. 3 HYDROLOGY OF A HIGHWAY STREAM CROSSING - January 1961
HEC No. 9 DEBRIS-CONTROL STRUCTURES - March 1971
HEC No. 10 CAPACITY CHARTS FOR THE HYDRAULIC DESIGN OF HIGHWAY CULVERTS - November 1972
HEC No. 11 USE OF RIPRAP FOR BANK PROTECTION - June 1967
HEC No. 13 HYDRAULIC DESIGN OF IMPROVED INLETS FOR CULVERTS - August 1972
HEC No. 17 THE DESIGN OF ENCROACHMENTS ON FLOOD PLAINS USING RISK ANALYSIS - October 1980

Electronic Computer Programs

- HY-1, 3 and 5 Discontinued
HY-2 HYDRAULIC ANALYSIS OF PIPE-ARCH CULVERTS
HY-4 HYDRAULICS OF BRIDGE WATERWAYS
HY-6 HYDRAULIC ANALYSIS OF CULVERTS (Box and Circular)

Calculator Design Series

- CDS No. 1 HYDRAULIC DESIGN OF IMPROVED INLETS FOR CULVERTS USING PROGRAMMABLE CALCULATORS, (COMPUCORP 325) - October 1980
CDS No. 2 HYDRAULIC DESIGN OF IMPROVED INLETS FOR CULVERTS USING PROGRAMMABLE CALCULATORS, (HP-65) - October 1980
CDS No. 3 HYDRAULIC DESIGN OF IMPROVED INLETS FOR CULVERTS USING PROGRAMMABLE CALCULATORS, (TI-59) - October 1980

