

# Computer Program Hydraulic Analysis of Culverts

PROGRAM HY-6  
1979



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**Federal Highway  
Administration**

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U.S. DEPARTMENT OF TRANSPORTATION  
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HY-6 - ELECTRONIC COMPUTER PROGRAM FOR  
HYDRAULIC ANALYSIS OF CULVERTS

- BOX CULVERTS
- CIRCULAR CULVERTS

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## PREFACE

This computer program is for the hydraulic analysis of concrete box and circular (concrete, CMP) culverts for any given hydrological data and site condition. This program supersedes the conventional culvert designs provided by the existing Computer Programs HY-1, "Hydraulic Analysis of Circular Culverts," and HY-3, "Hydraulic Analysis of Box Culverts." In addition to designs for conventional culverts, this program includes analysis and designs for improved inlets based on concepts presented in Hydraulic Engineering Circular No. 13, "Hydraulic Design of Improved Inlets for Culverts," dated August 1972. The improved inlet designs include bevel-edged, side-tapered and slope-tapered inlets. The original HY-1 and HY-3 computer programs are based on the concepts presented in Hydraulic Engineering Circular No. 5, "Hydraulic Charts for the Selection of Highway Culverts." Development of improved inlet designs for other geometric configurations (pipe arch, ovals, etc.) are not included in this publication because design criteria are not available.

Terminology used in this publication assumes that the reader is familiar with HEC No. 13 and understands the principles and design approach expressed therein.





STATEMENT OF THE PROBLEM

## STATEMENT OF THE PROBLEM

The Federal Highway Administration's (FHWA) earlier computer programs for the Hydraulic Design of Culverts, HY-1, "Hydraulic Analysis of Circular Culverts," and HY-3, "Hydraulic Analysis of Box Culverts," utilized the principles presented in Hydraulic Engineering Circular (HEC) No. 5 (1)<sup>1/</sup>.

With the advent of HEC No. 13, "Hydraulic Design of Improved Inlets for Culverts," (2) the development of this program was made possible. This program incorporates the principles in HEC No. 5 and HEC No. 13 with significant changes in program data output when compared to the HY-3 and HY-1 data output and a new approach to hydraulic analysis for the design of culverts.

Program output consists of a list of optional culvert sizes, including pertinent performance data for the hydraulic design engineer's use in selecting a culvert which will meet hydraulic requirements at the least cost. This output information is provided in recognition of several facts regarding culvert hydraulic design. (1) There is not a unique solution for any culvert site, i.e., several culvert sizes, shapes, inlet configurations and elevation, materials, etc. can satisfactorily meet the criteria and constraints established by the hydraulic design engineer for the site. (2) Highway agency practices differ regarding the use of materials and the configuration of culverts and practices differ dependent upon environmental conditions at the site and location within a State. (3) The hydraulic performance of any culvert operating with inlet control can be optimized. (4) The so-called "design flood" and the "allowable" headwater at any culvert site can be exceeded and there is a statistical probability that they will be exceeded. In choosing the preferred design alternative or if the contractor is required to bid on design alternatives, the hydraulic design engineer needs to consider the performance of alternative design options for a range of flow rates and the probability of potential damage to the highway and other properties.

The new culvert design approach can be summarized as follows:

1. Introduces the alternative of using external FALL\* at a culvert inlet if the culvert will operate in inlet control and the headwater elevation computed for the culvert performance otherwise exceeds the allowable headwater elevation.

---

\* External Fall refers to the change in the total barrel slope whereas Internal FALL refers to the inlet FALL for a slope-tapered design.

1/ Underlined numbers in parentheses refer to references on page 98.

2. Utilizes elevations with regard to headwater, inlet and outlet inverts, roadway embankment toe elevations. The advantage in using elevations rather than water depths is a unique outlet and inlet control performance curve regardless of inlet invert elevation (figure 2).
3. Ties the roadway cross section (embankment slopes) with the stream profile and the culvert length and height.
4. Use of optimization for design of box and circular culverts (See figures 1 and 2) for three conditions:
  - (a) Minimum fall -- Curve A
  - (b) Maximum discharge -- Curve B
  - (c) Minimum headwater -- Curve C
5. Provides the designer with performance information on all logical culvert sizes, shapes and vertical locations for use in evaluating the cost-effectiveness of available options.

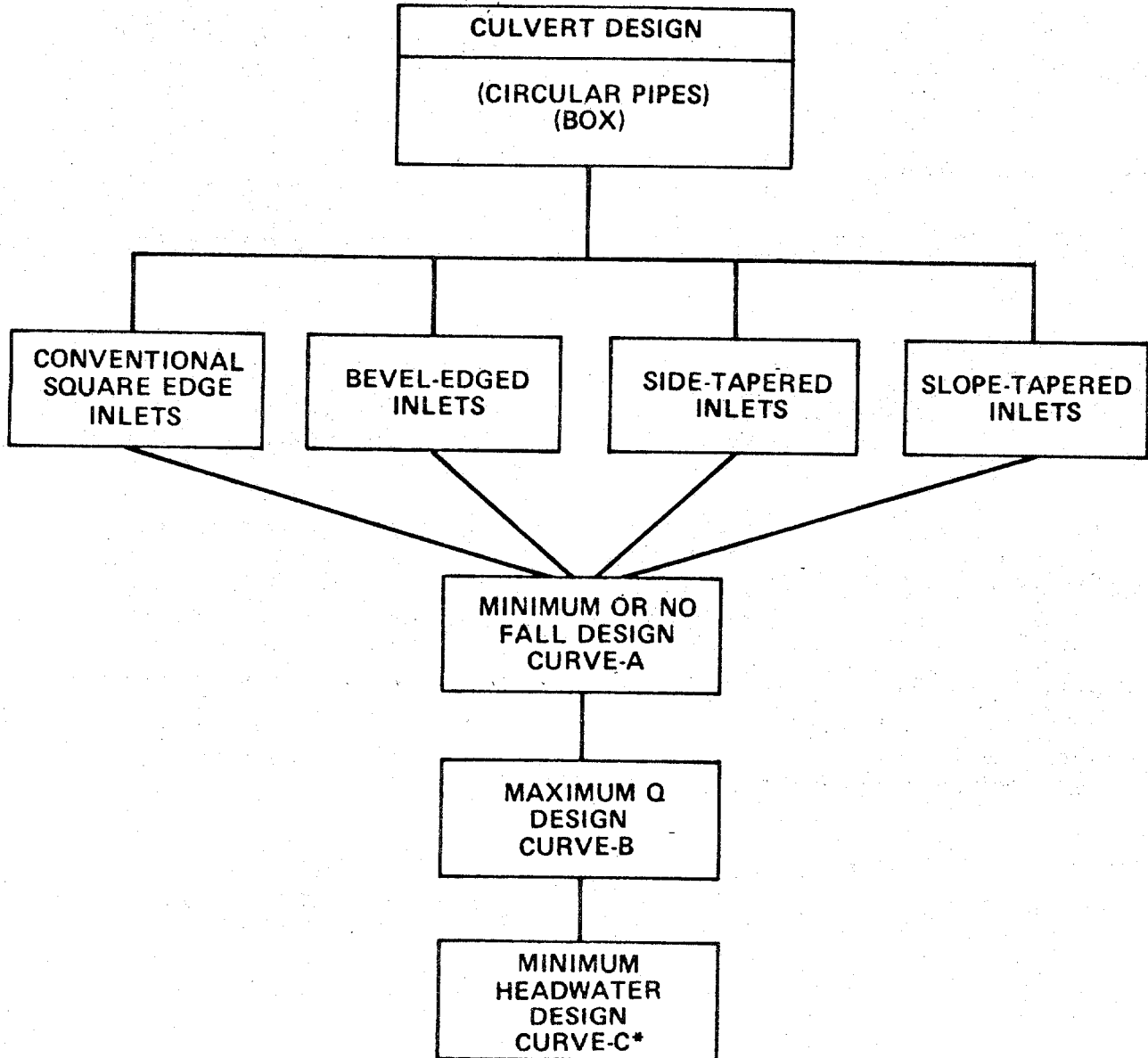
Figure 1 represents an overview of three design conditions provided by the computer program for each of the four inlet configurations. Figure 2 illustrates a typical performance curve relationship for the three design conditions. The dashed curve shows the extent of the computed inlet control headwater elevation above the allowable headwater for a given culvert size and design discharge. Normally for this situation, the culvert would not be accepted for use, but by depressing the culvert inlet, the culvert hydraulic performance is represented by Curve A (figure 2). Curve A represents the minimum design condition required to meet the selected design criteria.

Curve B illustrates the performance of a design which takes full advantage of the potential capacity of the selected culvert and the site to pass the maximum possible flow at the allowable headwater elevation (AHWEL). A safety factor in capacity is thereby incorporated in the design, usually at little cost. This can be accomplished by use of a depression (FALL), by geometry improvements at the inlet or by a combination of the two.

Curve C illustrates the passage of the design flow at the lowest possible headwater elevation. At design discharge, the minimum headwater is a function of outlet control (point 3) or water surface elevation in the stream at the culvert inlet, whichever is higher.

It should be realized that if the invert or throat elevation for a Curve B design is lower than the maximum allowable fall elevation, then the maximum discharge (Q) will not be at Point 2 (figure 2), but will occur where the inlet control curve crosses the allowable headwater elevation. Also, for this situation, Curve C will superimpose Curve B.

# ORGANIZATION CHART FOR CULVERT DESIGN



\*CURVE-C FOR SLOPE-TAPERED DESIGN NOT INCLUDED AT THIS TIME

Figure 1

# TYPICAL PERFORMANCE CURVES FOR OPTIMIZED CULVERT DESIGN

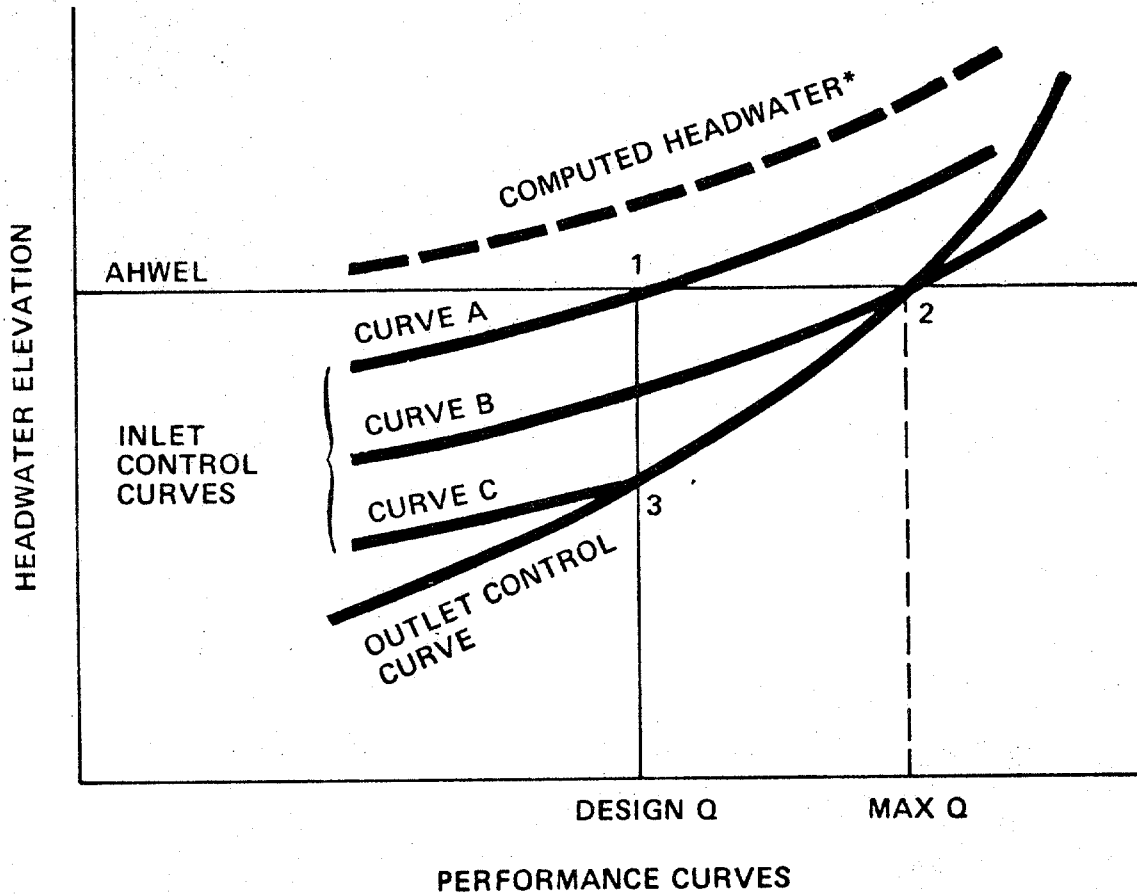


Figure 2

\*This curve shows the computed headwater elevation greater than the "allowable" headwater, therefore necessitating either an external FALL at the inlet or geometry improvements to achieve the minimum design condition imposed by the hydraulic design engineer and illustrated by curve A. When the computed headwater is less than the "allowable" no external FALL is necessary to achieve the minimum design condition.

DESCRIPTION OF PROGRAM

## DESCRIPTION OF PROGRAM

Figure 3 presents an overview of the culvert program which will eventually encompass the various culvert geometric designs within the total program. The program includes the main program (driver) plus the sub-routines associated with the applicable culvert design. The program was developed in modular (subroutine) form for ease in utilization. Figure 4 shows a macroflow diagram of the computer process for this program.

It is beyond the scope of this report to give a full understanding of the concepts presented in Hydraulic Engineering Circulars No. 5 and No. 13. The user of this program should be well acquainted with the two circulars or have them available for reference.

The initial function of the program is to read and store the input data for a particular culvert problem. The program tests the data to determine if the data are valid. If the data are invalid, an invalid message is printed and the problem is bypassed by the program.

As part of the input data, the user identifies the type of conventional inlet he desires by choosing the corresponding culvert code shown in Table 1 for box culverts or Table 6 for circular pipes. In this regard, the program has a built-in feature which will automatically provide the user with an optional bevel-edged inlet design which has a geometry similar to the conventional inlet design. For example, noting Table 1 - BOX CULVERT SECTION, if a wingwall type inlet code 41111 is selected, the program also provides design data for the comparable wingwall type code 41146 which is bevel Option 2. If the user wishes to bypass the conventional designs, he can choose a bevel-edged design and the program will provide data for that design and improved inlets only. The user must enter the program with one of the codes from Table 1 for either box culverts or Table 6 for circular culverts. In addition to the conventional design and/or bevel-edged designs the program provides side- and slope-tapered improved inlet designs for culverts flowing with inlet control.

The first major function of the program is to analyze a series of box culvert sizes or pipe diameters to compute the following:

### Outlet Control Section

1. The required outlet control headwater elevation.
2. The outlet invert elevation for a conventional, bevel-edged and tapered inlet type culvert.

### Inlet Control Section

1. The required inlet control headwater elevation.
2. The amount of external FALL, if the computed inlet control headwater elevation exceeds the "allowable" headwater elevation.
3. The face invert elevation for the conventional and bevel-edged culverts. For the tapered inlet, the throat invert elevation is determined along with the face invert elevation.

The amount of data for all the culvert sizes analyzed is printed on one sheet. This print-out sheet, "INDEX SHEET," allows the hydraulic engineer to make comparisons of inlet and outlet control headwaters and the external FALLS required for any box or circular pipe size. A more detailed description of the INDEX SHEET is found in the output section of this report.

The second major function of the program is to reanalyze the culvert sizes listed on the INDEX SHEET and compute the necessary design data for each culvert size and inlet type. The design data for each individual size is printed on a separate page as indicated by the page reference numbers listed on the INDEX SHEET.



# PROGRAM OVERVIEW

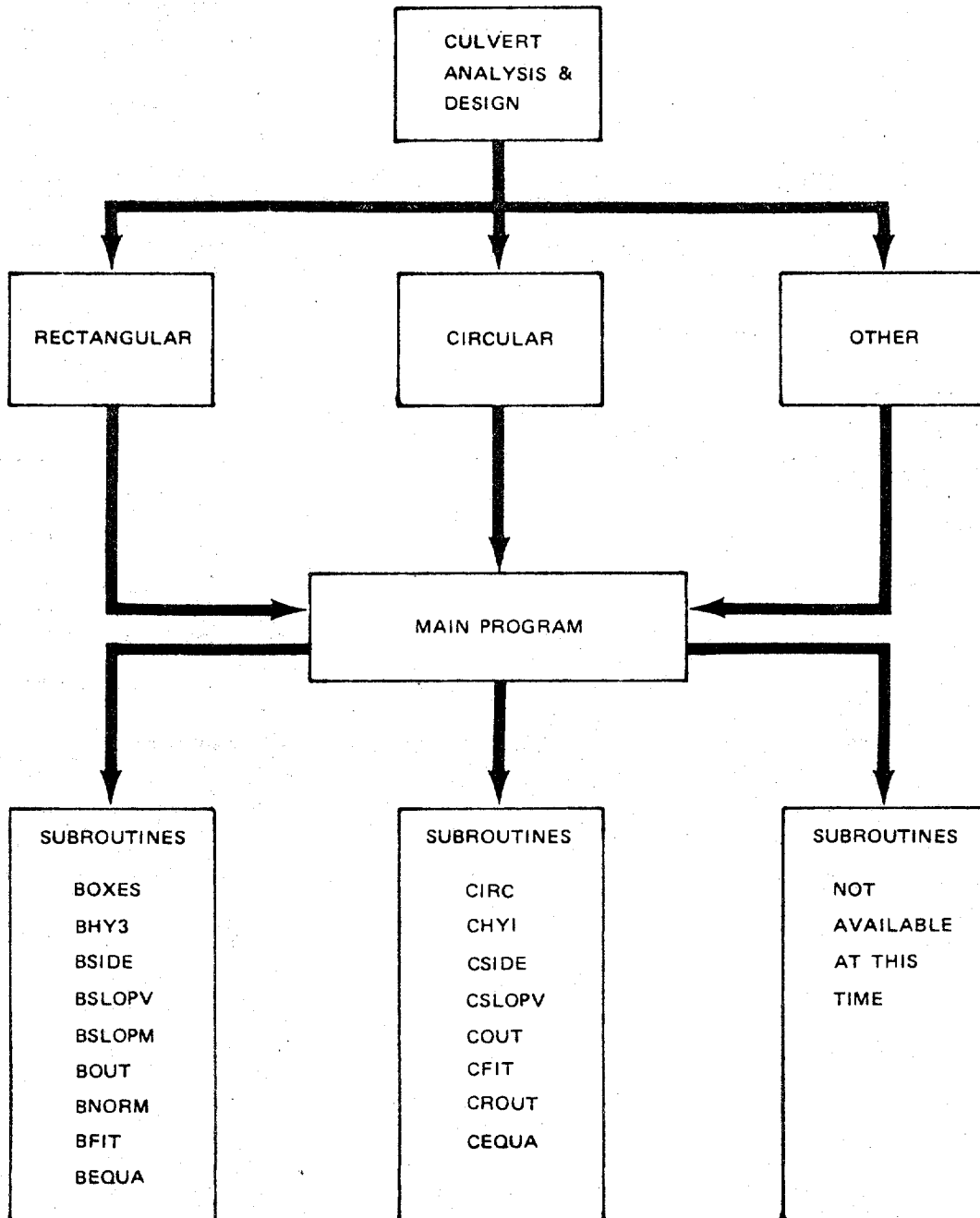


Figure 3

# MACRO FLOW DIAGRAM

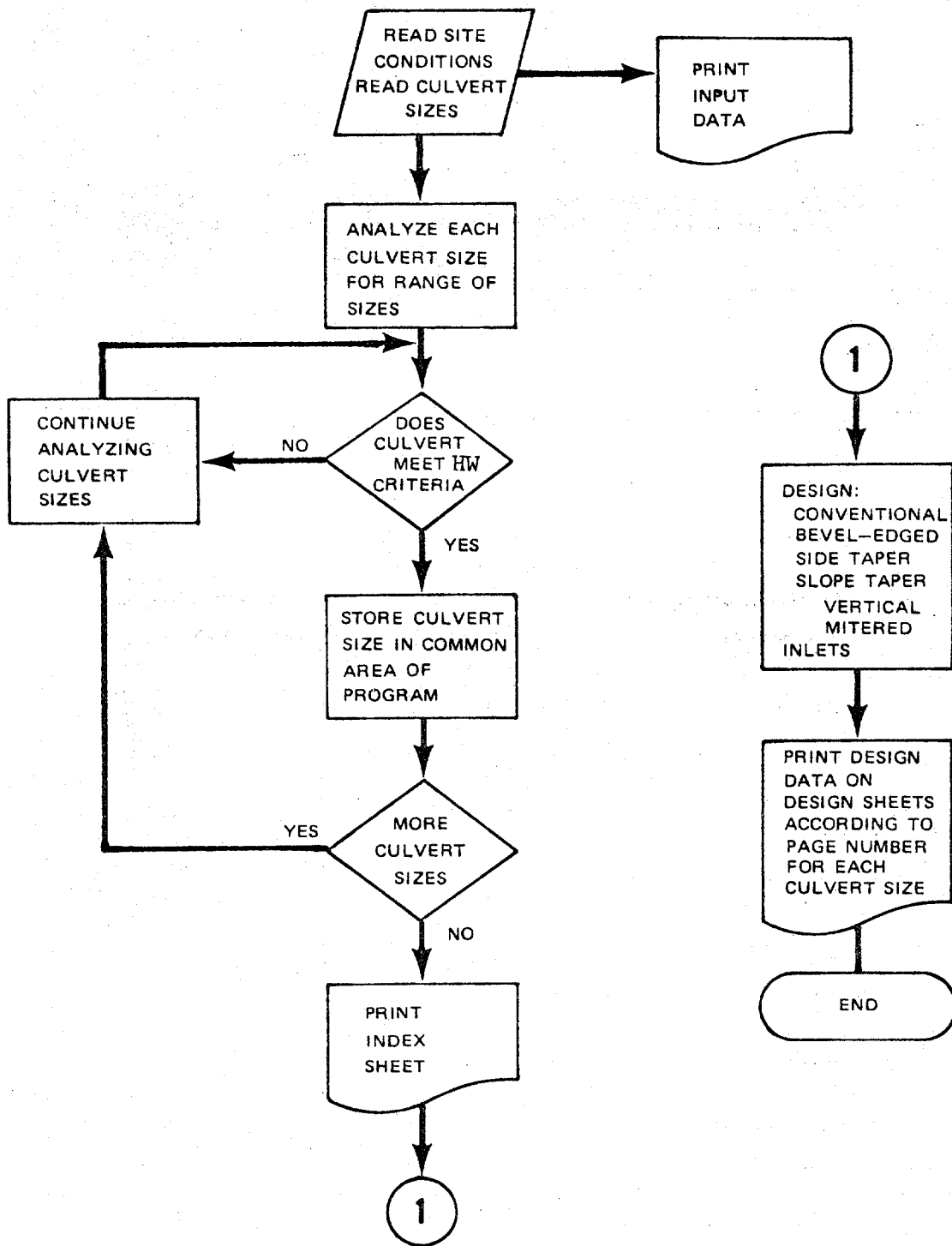


Figure 4

INPUT DATA SECTION

## INPUT DATA SECTION

This section describes the input data card requirements including a detailed description of the input data items, format coding and sample card setup for program processing.

### Card No. 1

Project identification

### Card No. 2

### Field Size

1. Culvert code	XXXXX
2. Stream slope	XX.XXXX
3. Approximate culvert length (identification only)	XXXXX.X
4. Design discharge	XXXXX.X
5. Design tailwater	XXXXX.X
6. Allowable headwater	XXXXX.X
7. Upstream elevation where roadway embankment meets stream profile	XXXXX.X
8. Downstream elevation where roadway embankment meets stream profile	XXXXX.X
9. Upstream roadway embankment slope	XXXXX.X
10. Downstream roadway embankment slope	XXXXX.X
11. Fall slope for slope-tapered inlet	XXXXX.X

### Card No. 3 - For range of box culvert sizes

1. Culvert width, initial value	XX
2. Culvert width, final value	XX
3. Culvert depth, initial value	XX
4. Culvert depth, final value	XX

## INPUT DATA SECTION

### Card No. 3 - For range of circular culvert sizes

- |                                    |       |
|------------------------------------|-------|
| 1. Culvert diameter, initial value | XX.XX |
| 2. Culvert diameter, final value   | XX.XX |

### Card No. 4

Blank card to terminate program execution.

The field size and number of decimals to the right of the units position are shown to the right of each item. A more detailed discussion of the input data follows.

### Culvert Code\*

The Culvert Code is a five-digit number which represents five separate integers that are used by the program to define different culvert and inlet types. Refer to Table 1 for the box culvert codes and Table 6 for circular pipe culverts. These five separate code integers are referred to as I1, I2, I3, I4 and I5. The symbol I1 indicates a type of culvert that the program is to analyze. Thus, for all box culverts, I1 is the integer 4; for CM pipe it is 1; and for concrete pipe, it is 2. Symbols I2 and I3 for box culverts, at the present time, are dummy values which are assigned the integer 1. Symbol I2 for circular pipe indicates whether paved or unpaved and I3 denotes the corrugation type. Symbol I4 defines the type of wingwall and enables the program to select an appropriate value for the entrance loss coefficient. I4 has four values that can be assigned to it, 1, 2, 3 and 4. I5 also refers to a particular entrance condition, namely, square or bevel-edged inlets and is used by the subroutine BEQUA or CEQUA to assign the appropriate mathematical equations for the chosen inlet condition.

An example culvert code that might be used is 41122. This five-digit number indicates to the program that coefficients must be used for a square-edged box culvert with a headwall either normal or skewed up to 45 degrees.

### Stream Slope

Stream slope, SLOPE, is the elevation of the point of intersection of the upstream roadway embankment with the stream profile minus the elevation of the point of intersection of the downstream roadway embankment with the stream profile divided by the horizontal distance between these two points. It is measured in feet per foot. A zero slope can be used.

\* See Tables 1 and 6 on pages 38 and 71

## INPUT DATA SECTION

### Approximate Culvert Length

The approximate culvert length, DIST, represents the distance between the intersection points mentioned in the section Stream Slope and is measured horizontally. Since the program computes true culvert lengths for the three design conditions, this value is printed out with the input data to allow the designer to know the width of the roadway embankment at the stream measured in feet.

### Design Discharge

Design discharge, Q1, is the quantity of water in cubic feet per second to be used in the selection of the barrel dimensions.

### Design Tailwater

Design tailwater, DIW, is the depth of water measured in feet between the water surface elevation and the invert elevation at the outlet end of the culvert.

### Allowable Headwater Elevation

Allowable headwater elevation, AHWEL, is the chosen water surface elevation at the culvert inlet for the design discharge at the culvert site.

### Upstream Elevation for Roadway Embankment Intersecting Stream Profile

This elevation, ELIN, represents the elevation at the point where the upstream embankment slope intersects the stream profile.

### Downstream Elevation for Roadway Embankment Intersecting Stream Profile

This elevation, ELOUT, represents the elevation at the point where the downstream embankment slope intersects the stream profile.

### Upstream Embankment Slope

The embankment slope, SEL, is the embankment slope on the upstream side of the roadway cross section templet measured as 1:1, 2:1, 3.5:1, etc. For a vertical embankment slope SEL=0.0.

### Downstream Embankment Slope

The embankment slope, SER, is the embankment slope on the downstream side of the roadway cross section templet measured as 1:1, 2:1, etc. For a vertical embankment slope SER=0.0.

## INPUT DATA SECTION

### Fall Slope

The fall slope for a slope-tapered inlet. User inputs value between 2:1 to 3:1, inclusive.

### Culvert Sizes (Boxes or Circular Pipes)

Input the range of culvert widths and depths or diameters desired. For example: B(Base) ranges from 4' to 10' and D(Depth) ranges from 4' to 8', or a single box size can be submitted as B ranges from 7' to 7' and D ranges from 6' to 6' for a 7' x 6' box.

#### For Box Culverts - the range of sizes are:

KBAS1 is the initial box width size

KBAS2 is the final box width size

KDEP1 is the initial box depth size

KDEP2 is the final box depth size

#### For Pipe Culverts - the range of diameter sizes are:

DIA1 is the initial diameter size

DIA2 is the final diameter size

Figure 5 represents a typical roadway cross-section depicting several of the variables (symbolic names) used as input data items.

Figure 6 shows a sample input data sheet.

Figure 7 illustrates the source card arrangement including job control cards to process culvert hydraulic analysis.

The following tabulation describes the input data as to the card type, and card columns used, the associated format and the symbolic variable names.

INPUT FORMATS

<u>CARD TYPE</u>	<u>COLUMNS</u>	<u>FORMAT</u>	<u>SYMBOLS</u>	<u>DEFINITION</u>
1	1-78	26A3	IPR0J	Project identification
2	1-5	5I1	I1, I2, I3, I4, I5	Culvert code number (boxes or pipes)
	6-12	F7.4	SLOPE	Slope of the streambed
	13-19	F7.1	DIST	Distance between point of intersection of stream slope and upstream embankment slope and point of intersection of stream slope and downstream embankment of slope measured horizontally
	20-26	F7.1	Q1	Design discharge
	27-33	F7.1	DTW	Design tailwater
	34-40	F7.1	AHWEL	Allowable headwater elevation
	41-47	F7.1	ELIN	Elevation of intersection point of stream slope and upstream embankment slope
	48-54	F7.1	ELOUT	Elevation of intersection point of stream slope and downstream embankment slope
	55-61	F7.1	SEL	Slope of upstream embankment For vertical slopes SEL=0.0



INPUT FORMATS (continued)

<u>CARD TYPE</u>	<u>COLUMNS</u>	<u>FORMAT</u>	<u>SYMBOLS</u>	<u>DEFINITION</u>
	62-68	F7.1	SER	Slope of downstream embankment
	69-75	F7.1	SFACE	Fall slope for slope-tapered inlets
3 (boxes)**	1-2	I2	KBAS1 *	First Base width (B) value for range of culvert sizes
	3-4	I2	KBAS2 *	Last B value for range of culvert sizes
	5-6	I2	KDEP1 *	First Depth (D) value for range of culvert size
	7-8	I2	KDEP2 *	Last D value for range of culvert sizes
3 (pipes)**	1-5	F5.2	DIA1	Initial pipe diameter (ft.)
	6-10	F5.2	DIA2	Final pipe diameter (ft.)

\* To analyze a single box size, for example a 7' x 7' or single pipe size of 7' diameter then

For Boxes      KBAS1 = 7'      KDEP1 = 7'      DIA1 = 7'  
                     KBAS2 = 7'      KDEP2 = 7'      DIA2 = 7'

\*\* Each type of geometric design represents a specific design as indicated by Card No. 3 for boxes or Card No. 3 for pipes. Use only one Card No. 3 per data set.

TYPICAL ROADWAY CROSS SECTION

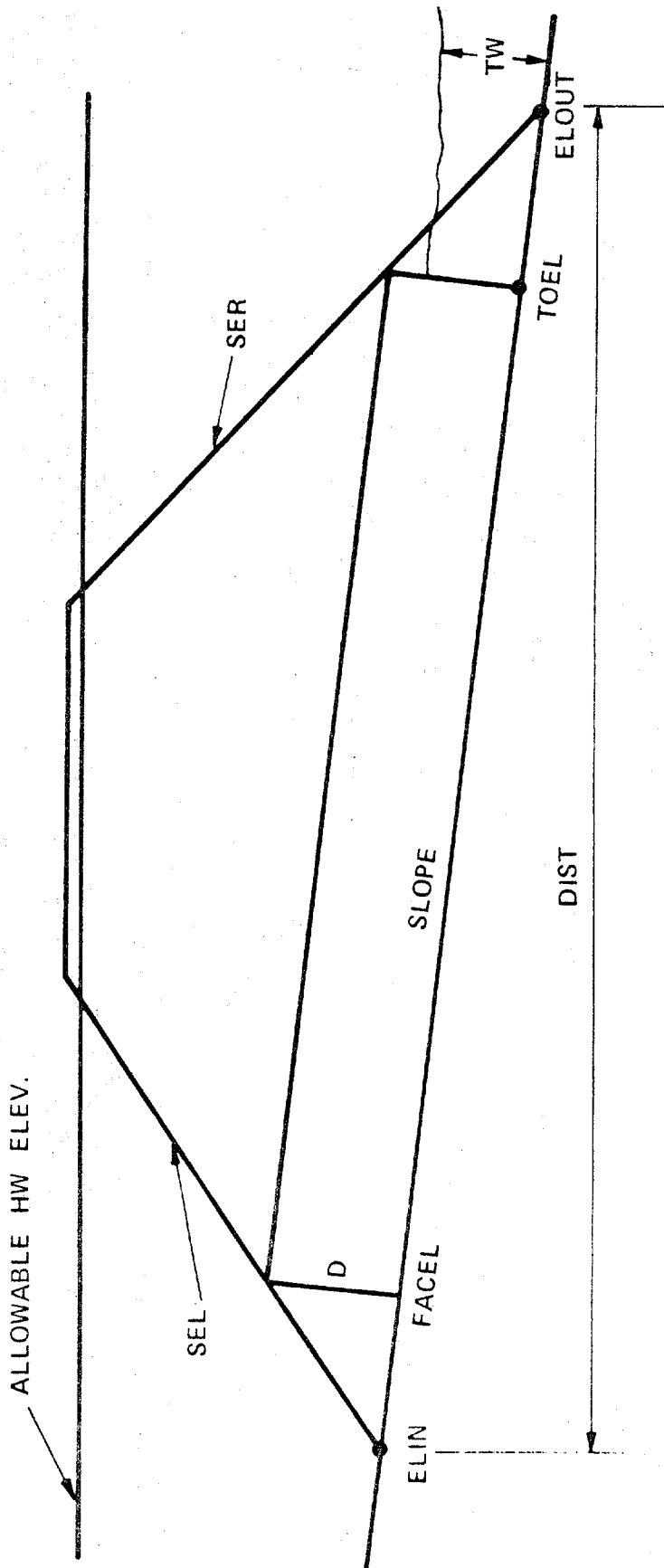


Figure 5



INPUT SECTION

DATA CARD SET-UP

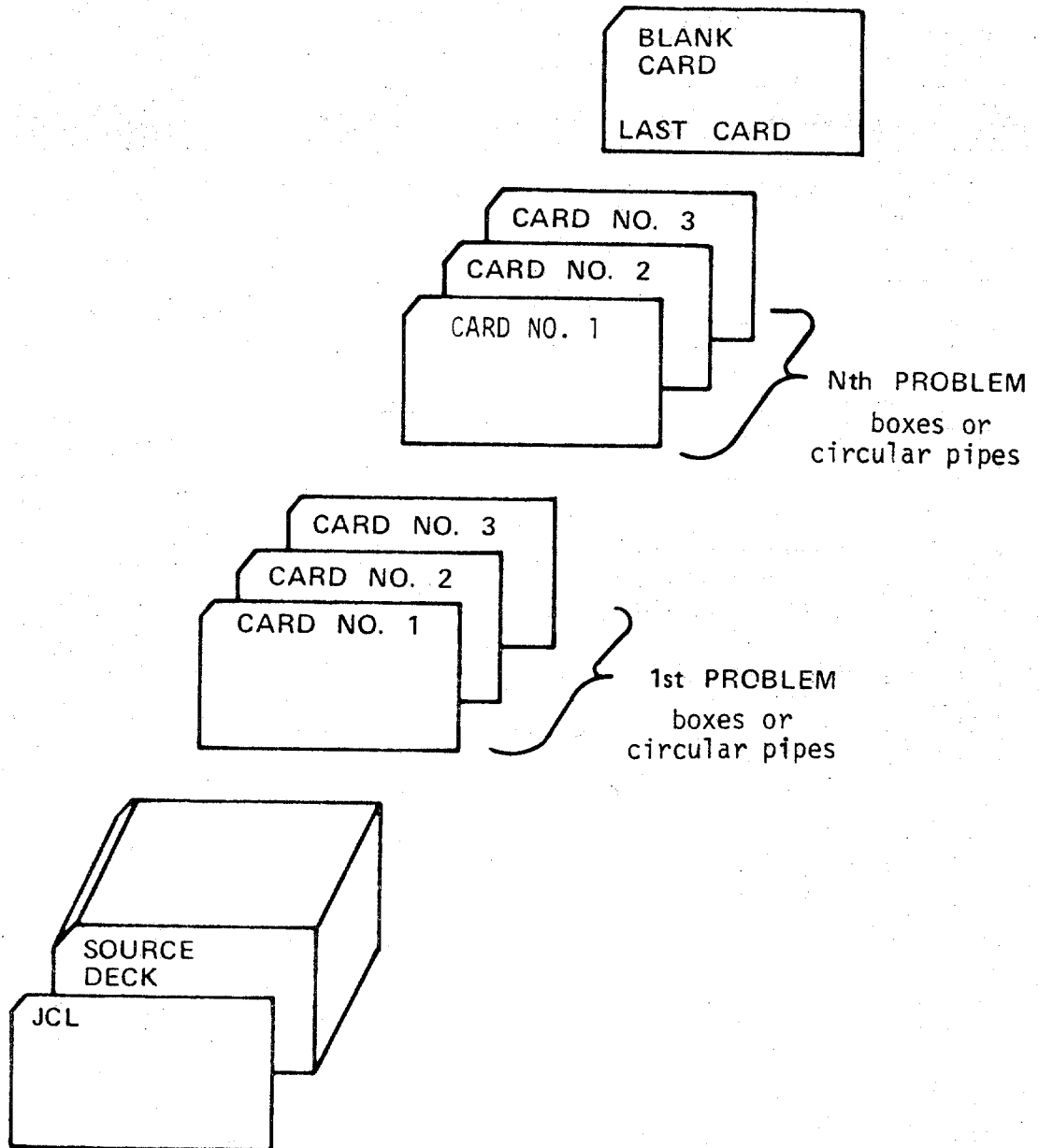


Figure 7

OUTPUT DATA SECTION

## OUTPUT DATA SECTION

The output data for this program is divided into two groups, (1) INDEX SHEET and (2) CULVERT DESIGN DATA SHEETS.

### I. INDEX SHEET

The problem identification, information describing the types of bevel-edged inlets used and the design input data are printed at the top of the INDEX SHEET.

As previously stated, the function of the INDEX SHEET is to show the relationship between the inlet control section (headwater elevation, necessary external FALL and invert elevation) for a conventional inlet, a bevel-edged inlet and a tapered inlet (throat); also the headwater elevation and invert elevation for the outlet control section of a culvert.

The following is a description of the input data items by columns. See example problem No. 1 for output reference.

#### Page Reference

This page number refers to the culvert design data sheet for each culvert size listed on the INDEX SHEET.

#### Number of Barrels

This column is self-explanatory.

#### Barrel Width

The barrel width, in feet.

#### Barrel Depth or Diameter

The barrel depth or diameter, in feet.

#### Outlet Control Headwater Computations

$KE = 0.5$  - this column represents the outlet control headwater elevation for a culvert with a conventional inlet where the entrance loss coefficient is 0.5. Other possible coefficients used in this program are described in Table 2 for box culverts and Table 7 for circular pipes.

## OUTPUT DATA SECTION

KE = 0.2 - This column represents the outlet control headwater elevation for a bevel-edged, side-tapered and slope-tapered culvert inlet, where the entrance loss coefficient is 0.2.

The third column represents the culvert outlet invert elevation.

### Inlet Headwater Computations

Conventional Culvert - The three columns in the group represent the headwater elevation, the external FALL, and the invert elevation for a culvert with a conventional inlet.

Bevel-Edged Culvert - The three columns in this group represent the headwater elevation, the external FALL, and the invert elevation for the optional bevel-edged inlet culvert.

Throat-Improved Inlets - The three columns in this group represent the throat elevation, the throat FALL\*, and the throat invert elevation for side-tapered and slope-tapered vertical face inlets.

Whenever a box or pipe size being analyzed by the computer does not satisfy the design criteria, a set of dashes "—" will be printed as output data on the INDEX SHEET and the culvert design data sheets; also, when the program user wishes to bypass the conventional culvert design and go directly to the bevel and improved inlet design, the computer will print dashes "—" in the column noted by the conventional culvert heading.

For pipe culverts, the INDEX SHEET will show the pipe sizes in groups according to the type of corrugated metal group investigated. For instance, the INDEX SHEET for example problem No. 2A shows three pipe sizes listed under the 2 2/3" by 1/2" corrugated metal and three pipe sizes listed under 3" by 1" corrugated metal. More information on the grouping of pipe sizes by corrugation type is presented under the section for Circular Pipes.

### II.. CULVERT DESIGN DATA SHEET

A culvert design data sheet will be printed for each culvert size listed on the INDEX SHEET with the reference page number printed at the top of the page. This page numbering system will be helpful

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\* This FALL is measured between the face invert elevation at the stream bed and the throat elevation for side-tapered and slope-tapered vertical face designs. FALL for slope-tapered mitered face inlet is measured from crest elevation to throat elevation (not shown on INDEX SHEET, but shown on design sheets).

## OUTPUT DATA SECTION

in locating the design data for any of the culverts listed on the INDEX SHEET. Also printed at the top of the page for easy reference will be the number of barrels, barrel width, barrel depth, design discharge, allowable headwater elevation, stream slope and the FALL slope for a slope-tapered inlet.

The design output data are printed under the following five headings:

1. Conventional inlet design for culvert code: (XXXXX).
2. Beveled inlet design for culvert code: (XXXXX).
3. Side-tapered inlet design.
4. Slope-tapered inlet design - vertical face.
5. Slope-tapered inlet design - mitered face.

A brief discussion of each heading follows:

1. Conventional Inlet Design for Culvert Code: (XXXXX)

If the INDEX SHEET shows dashes for a particular culvert size, no design data is available and the program prints a message, bypasses the conventional design and proceeds to the bevel inlet design (see example problem 1).

If there is data on the INDEX SHEET, then the program computes and prints inlet design data for (1) Minimum Fall -- Curve A, (2) Maximum Q -- Curve B, and (3) Minimum Headwater -- Curve C. This is followed by performance curve data for each of the three mentioned conditions and the outlet control performance curve data for the culvert.

2. Beveled Inlet Design for Culvert Code: (XXXXX)

The output design data for this type inlet consists of (1) Minimum FALL -- Curve A, (2) Maximum Q -- Curve B, and (3) Minimum Headwater -- Curve C, plus the inlet and outlet control performance curve data. If bevel-edged design data is not available (represented by dashes on INDEX SHEET), the data output will consist of a message plus the outlet control performance curve data. This performance curve also applies as the outlet control performance curve for culverts designed with improved inlets (refer to HHC No. 13).



## OUTPUT DATA SECTION

### 3. Side-tapered Inlet Design

The output consists of the Minimum FALL -- Curve A, Maximum Q -- Curve B, Minimum Headwater -- Curve C, and the inlet control performance curve data. The outlet control performance curve data is shown under beveled design.

### 4. Slope-tapered Inlet Design -- Vertical Face

The output data consists of the Minimum FALL -- Curve A, Maximum Q -- Curve B plus the inlet control performance curve data for each design. The outlet control performance curve data is shown under beveled design. The computer algorithm for the Minimum Headwater -- Curve C design has not been developed.

### 5. Slope-tapered Inlet Design -- Mitered Face

Same as 4.

TECHNICAL PROCEDURES

- BOX CULVERT SECTION
- CIRCULAR CULVERT SECTION

## BOX SECTION

This portion of the program presents the equations and the design criteria pertaining to box culvert analysis and design.

### MATHEMATICAL EQUATIONS

#### Inlet Control

Headwater Depth (1)

$$H_F = (D) [(Y) - (S)(SCORR)]$$

Where:  $H_F$  = headwater in feet

$D$  = height of culvert in feet

$$Y = a + bX + cX^2 + dX^3 + eX^4 + fX^5$$

$a, b, c, d, e, f$  = coefficients determined by polynomial curve fitting (see subroutine BEQUA for coefficients)

$S$  = slope of culvert in feet per foot

SCORR = slope correction factor (Table 2, page 39)

$$X = Q/BD^{3/2}$$

$Q$  = discharge in cubic feet per second

$B$  = width in feet

The equations were determined by a computer program which fitted a polynomial curve by the method of least squares to data taken from the nomographs for inlet control in HEC No. 5 and throat control and face control from HEC No. 13.

The equations are located in subroutines called BEQUA, BSIDE, BSLOPV, BSLOPM.

## BOX SECTION

### Outlet Velocity

$$V = Q/A \quad (2)$$

$$A = Q/[(1.486/n)(R^{2/3}S^{1/2})] \quad (3)$$

Where: V = outlet velocity in feet per second

Q = discharge in cubic feet per second

A = Cross-sectional area of water in square feet at any depth of flow

R = hydraulic radius in feet

S = slope of culvert in feet per foot

n = Manning's roughness factor

Normal depth is computed by subroutine BNORM using a polynomial equation developed from OPEN CHANNEL HYDRAULICS (5).

### Outlet Control

#### Head

$$H = (Q/10)^2[(1.555(K_e + 1.0)/A^2) + (45.095n^2L/(A^2R^{4/3}))] \quad (4)$$

Where: H = head in feet for culvert flowing full

Q = discharge in cubic feet per second

$K_e$  = coefficient for entrance loss

A = total cross-sectional area of box

n = Manning's roughness factor

L = length of culvert in feet (actual culvert length)

R = hydraulic radius in feet

## BOX SECTION

### Critical Depth

$$D_c = 0.315(Q/B)^{2/3}$$

Where:  $D_c$  = critical depth in feet  
 $Q$  = discharge in cubic feet per second  
 $B$  = width of box in feet

### Headwater Elevation

$$HWEL = HO + H + \text{Culvert Outlet Invert Elevation} \quad (6)$$

Where:  $HWEL$  = headwater elevation in feet  
 $H$  = head for full flow in feet  
 $HO$  = design tailwater or  $(D_c + D)/2$  whichever is greater  
 $D$  = height of culvert in feet  
 $D_c$  = critical depth in feet

The critical depth cannot exceed the height of the box.

### Test for Full Flow Condition

$$H_f = D + (1 + K_e) V^2/2g \quad (7)$$

Where:  $H_f$  = headwater depth in feet  
 $K_e$  = coefficient for entrance loss  
 $D$  = height of culvert in feet  
 $V$  = mean velocity for full cross section of barrel in feet per second

## BOX SECTION

Backwater (Water surface profile for normal depth greater than or equal to critical depth)

When tailwater is equal to or less than critical depth or normal depth, equations (8) and (9) are used to compute water surface profiles. When tailwater is greater than normal and critical depth, equations (9) and (10) are used to compute water surface profiles.

$$X = [(d_2 + V_2^2/2g) - (d_1 + V_1^2/2g)] / (S - S_0) \quad (\text{M2 Curve}) \quad (8)$$

Where: X = distance in feet between cross sections 1 and 2

$d_1, d_2$  = depths of water in feet at cross sections 1 and 2

$V_1, V_2$  = velocities in feet per second at sections 1 and 2

$S_0$  = slope of the culvert in feet per foot

$g = 32.2 \text{ ft./sec.}^2$

$S = n^2 V^2 / (2.21 R^{4/3})$ , average slope of the water surface between cross sections 1 and 2 in feet per foot (9)

$n$  = Manning's roughness factor

$V$  = average velocity in feet per second of the two cross sections

$R$  = average hydraulic radius in feet of the two cross sections

$$X = [(d_1 + V_1^2/2g) - (d_2 + V_2^2/2g)] / (S_0 - S) \quad (\text{M1 Curve}) \quad (10)$$

$$\text{so that: } HW = d_2 + V_2^2/2g + k_e V_1^2/2g \quad (10A)$$

## BOX SECTION

### Outlet Velocity

$$V=Q/A \quad (11)$$

Where:  $V$  = outlet velocity in feet per second

$Q$  = discharge in cubic feet per second

$A$  = cross-sectional area of water in square feet

Area is determined from the following conditions:

When:  $DTW \geq D$ ,  $A = (B)(D)$

$DSUBC \geq D$ ,  $DSUBC = D$

$DSUBC > DTW$ ,  $A = (B)(DSUBC)$

$DSUBC < DTW$ ,  $A = (B)(DTW)$

Where:  $DTW$  = design tailwater in feet

$D$  = height of culvert in feet

$DSUBC$  = critical depth in feet

## BOX SECTION

### DESIGN CRITERIA

This program is based on the hydraulic design criteria in HEC No. 5 and HEC No. 13 and was developed to provide flexibility in satisfying many different design requirements used by various highway agencies.

To assist users wanting to change design features (within the limits expressed in HEC No. 13), the following is a presentation of the design criteria used in this program. Before modifying the limitations, check HEC No. 13 to ascertain that such modifications are valid.

#### CONVENTIONAL CULVERT DESIGN CRITERIA - Square and Bevel-Edged

1. Inlet and outlet control headwater  $\geq$  (AHWEL - D/4) and  $\leq$  AHWEL
2. D (height) not greater than 1.2B (width)
3. B not greater than 2D
4. Crown elevation not greater than controlling headwater elevation.
5. If inlet headwater elevation  $>$  allowable headwater elevation, use a FALL at inlet invert.
6. FALL not to exceed Max FALL

Where: Max FALL =  $1.5D^*$   
or inlet invert elevation not less than outlet invert elevation

7. Culvert sizes range from  $B = KBAS1^{**}$  to  $B = KBAS2$  and  $D = KDEP1^{**}$  to  $D = KDEP2$  in increments of even feet.
8. Minimum crest length based on Chart 17 in HEC No. 13.

\* Limitations related to HEC No. 13

\*\* See input data



## BOX SECTION

### SIDE-TAPERED INLET - Design Criteria

1. Design limited to two barrel structure\*
2. Taper = 4:1 to 6:1\*
3.  $FALL \leq \text{Max FALL}$

Where:  $\text{Max FALL} = 1.5D^*$   
or face invert elevation not less than  
outlet invert elevation

4. 45° face bevels:  $b = BF/2$  inches  
if  $BF > 3D$  use  $b = 3D/2$   
 $d = D/2$  inches
5. If  $FALL < D/4$ , there is no minimum crest length

### SLOPE-TAPERED INLET - VERTICAL FACE - Design Criteria

1. Design limited to two barrel structure\*
2. Taper = 4:1 to 6:1\*
3. Fall slope (SF) = input data from 2:1 to 3:1 inclusive\*
4.  $L3 \geq 0.5B^*$
5.  $1.5D \geq FALL \geq D/4^*$
6. Throat elevation > outlet invert elevation
7.  $FALL = \text{Vertical distance between face invert elevation and throat invert elevation}$

\* Limitations related to HEC No. 13

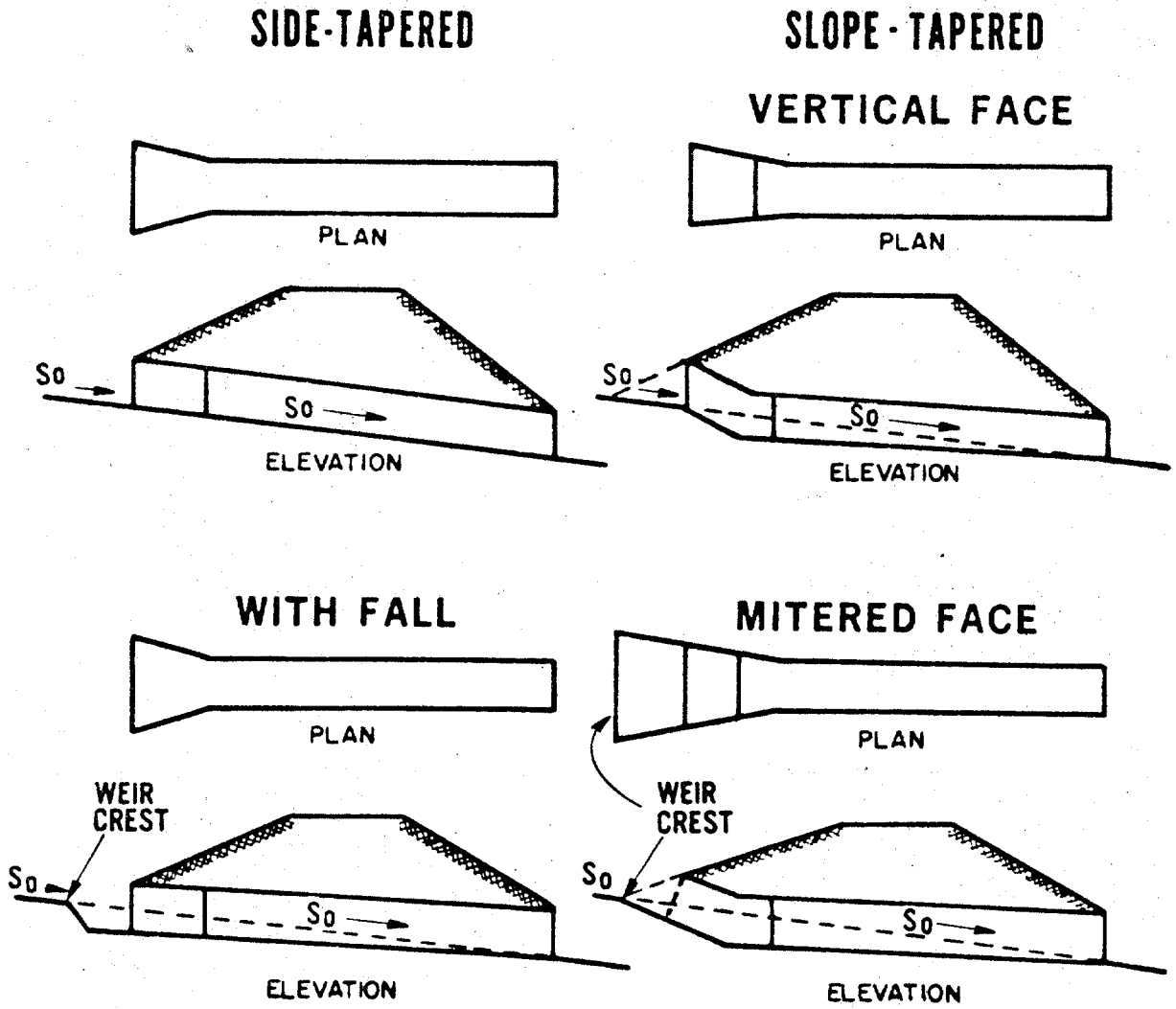
## BOX SECTION

### SLOPE-TAPERED INLET--MITERED-FACE - Design Criteria

1. Design limited to two barrel structure\*
2. Taper = 4:1 to 6:1\*
3. Fall slope (SF) = input data from 2:1 to 3:1 inclusive\*
4.  $L3 \geq 0.5B^*$
5.  $1.5D \geq FALL \geq D/4^*$
6. Throat elevation > outlet invert elevation
7. FALL = Vertical distance between crest invert elevation and throat invert elevation

\* Limitations related to HEC No. 13

BOX SECTION



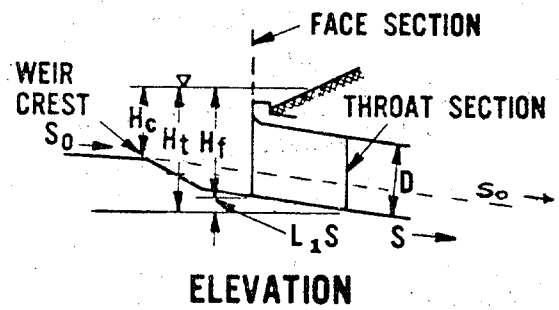
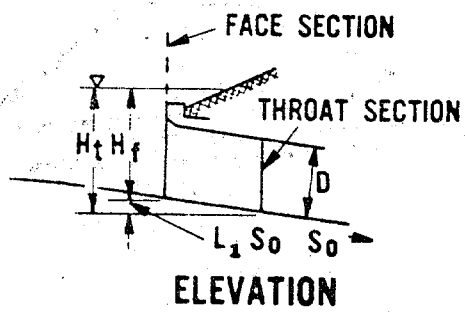
TYPES OF IMPROVED INLETS FOR BOX CULVERTS

Figure 8

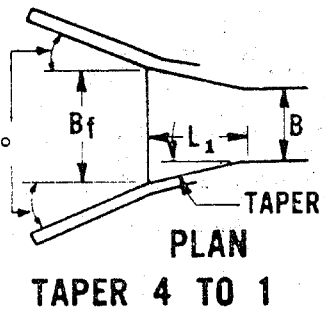
BOX SECTION

No FALL

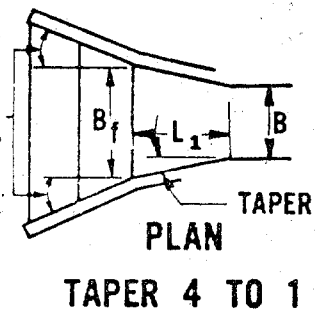
With FALL



SYMMETRICAL  
FLARE ANGLES  
FROM  $15^\circ$  TO  $90^\circ$



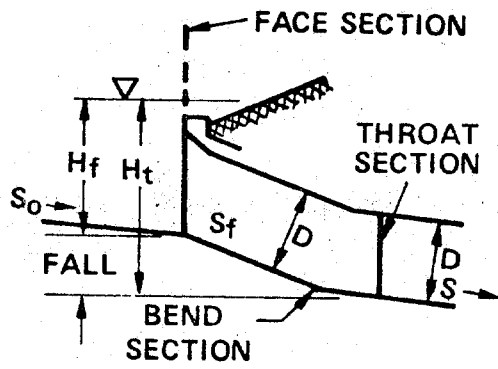
SYMMETRICAL  
FLARE ANGLES  
FROM  $15^\circ$  TO  $90^\circ$



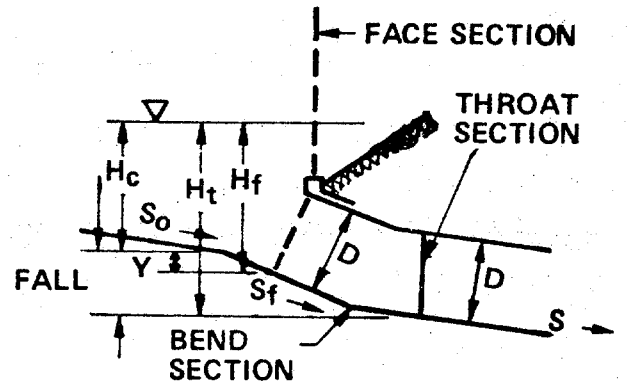
SIDE-TAPERED INLETS

Figure 9

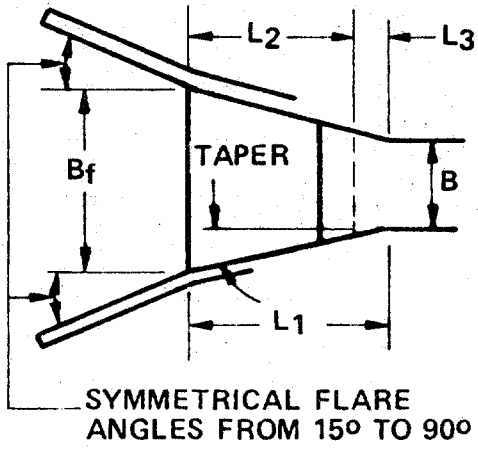
BOX SECTION



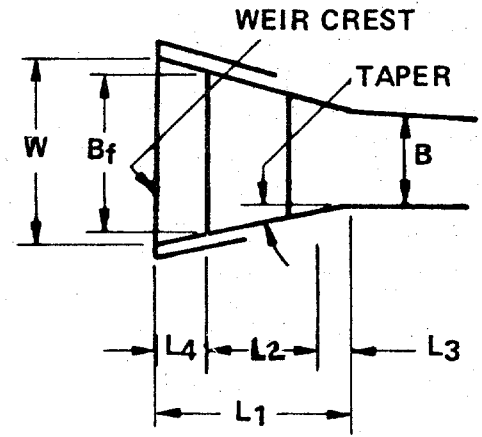
ELEVATION



ELEVATION



PLAN



PLAN

SLOPE-TAPERED VERTICAL FACE and SLOPE-TAPERED MITERED FACE

Figure 10

## BOX SECTION

Table 1 - Box Culvert Codes

Square-Edge and Bevel-Edge Reinforced Concrete Box (RCB)

CODE					INLET TYPE
I1	I2	I3	I4	I5	
4	1	1	1	1	WINGWALLS - 30° - 75° WW Flare Square-top edge HEC 13, Chart 7
4	1	1	2	2	HEADWALLS - Normal (90°) or skewed to 45° - Square edge HEC 13, Chart 7
4	1	1	2	3	WINGWALLS - with 15° WW flare having square edges HEC 13, Chart 7
4	1	1	3	4	WINGWALLS - 0° flare square top edge HEC 13, Chart 7
4	1	1	4	5	HEADWALL - Normal or skewed to 45° with 1:1 bevels (variable bevel on acute angle of skewed HEADWALL, HEC 13 Chart No. 8, 9)
4	1	1	4	6	WINGWALLS - 18° - 33.7° WW flare with 1 1/2:1 top bevel  - with 45° flare with 1:1 top bevel HEC 13 Chart No. 10
4	1	1	4	7	HEADWALL - Normal with 1 1/2:1 bevels on 3 sides HEC 13, Chart 8

BOX SECTION

Table 2 - Hydraulic Constants

Velocity Distribution	Alpha = 1.00
Slope Correction Factor	SCORR = 0.50
Manning's n	cn = 0.012
<u>I4 Entrance Loss Coefficients</u>	
1	30° to 75° WW flare      CKE(1) = 0.40
2	HEADWALL (90° WW) or skewed to 45°      CKE(2) = 0.50
2	15° WW flare      CKE(2) = 0.50
3	0° WW flare (parallel)      CKE(3) = 0.70
4	Bevel-edged inlets      CKE(4) = 0.20

EXAMPLE PROBLEM

- BOX CULVERT



## BOX SECTION

### EXAMPLE PROBLEM No. 1

This problem simulates the site conditions for a box culvert design (problem No. 1) found in HEC No. 13. The following INDEX SHEET illustrates the various culvert sizes (both single and double barrel) which can accommodate the design flow.

At a glance, the hydraulic design engineer can view the headwater relationship for inlet control and outlet control for a conventional, bevel-edged and slide-tapered inlet and determine which control governs. For the range of culvert sizes analyzed, all the single barrel and several double barrel culverts require a certain amount of FALL. The page numbers listed in the left-hand column of the INDEX SHEET refer to the data output page containing the design data for each culvert size. For this example, only the design data referred to by pages 1 and 2 (6 ft. by 7 ft. and 7 ft. by 6 ft. culverts) are included to limit the size of the publication.

A comparison of the design data for the 7 ft. width by 6 ft. depth culvert (page 2 of the output) with example problem No. 1 in HEC No. 13 shows the closeness of the respective values. The differences arise from the methods of calculation. The hand method is based on chart and nomograph readings whereas the computer solution utilizes mathematical equations.

Figure 11 shows the performance curves for the side-tapered design.

PROBLEM IDENTIFICATION

CARD NO. 1																																																					
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54
TEST PROBLEM FOR CODE 41122 SLOPE = 0.05																																																					

SITE DATA

CARD NO. 2																																																					
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54
41122 0.05 386.0 1000.0 3.5 200.0 191.0 171.7																																																					

55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75									
3.0																				3.0									

CARD NO. 3 FOR BOX CULVERTS							
1	2	3	4	5	6	7	8
6	7	6	7				
KBAS1							
				* KDEP2			
				* KDEP1			

CARD NO. 3 FOR PIPE CULVERTS							
1	2	3	4	5	6	7	8
* KD1A2							
* KD1A1							

\*BOX CULVERT AND PIPE CULVERT SIZES—SEE INPUT SECTION

INDEX SHEET

>>>> BOX CULVERT DESIGN FOR PROJECT >>> SAMPLE PROBLEM FOR CODE 41122 SLOPE=.05

>>>> THE PROGRAM PROVIDES A RANGE OF CONVENTIONAL BOX CULVERT SIZES WITH AND WITHOUT BEVELS WHICH SATISFY SITE REQUIREMENTS WHERE: BEVELLED EDGES INCLUDE THE FOLLOWING:

HEADWALLS-NORMAL -CHART NO. 8 IN HEC-13  
 -SKEMED -CHART NO. 9 IN HEC-13

ALLOWABLES -CHART NO. 10 IN HEC-13

>>>> IF INLET CONTROL GOVERNS - IMPROVED INLET DESIGNS ARE PROVIDED FOR SIDE-TAPERED INLETS AND SLOPE-TAPERED INLETS

\*\*\*\*\*  
 DESIGN INPUT DATA  
 \*\*\*\*\*  
 DESIGN INPUT DATA  
 \*\*\*\*\*

CONVENTIONAL CULVERT CODE: 41122 HEADWALL - NORMAL OR SKEMED TO 45 DEGREES - 50 TOP EDGES KE= 0.5  
 BEVELLED-EDGED CULVERT CODE: 41125 HEADWALL - NORMAL OR SKEMED TO 45 DEGREES WITH 1:1 BEVELS KE= 0.2  
 (ADJUSTABLE BEVEL ON ACUTE ANGLE OF SKEMED HEADWALL)

CULVERT CODE	APPROX STREAM SLOPE	ICE-ICE CULVERT LENGTH	DESIGN DISCHARGE	DESIGN TAILWATER	ALLOWABLE HEADWATER ELEVATION	STREAM BED ELEVATION AT INLET	STREAM BED ELEVATION AT OUTLET	LEFT ROADWAY EMBANKMENT SLOPE	RIGHT ROADWAY EMBANKMENT SLOPE
41122	0.0500	356.0	1000.0	3.5	200.0	191.0	171.7	3:0:1	3:0:1

CULVERT SIZES  
 B FROM 6 FT TO 7 FT SLOPE-TAPER  
 D FROM 6 FT TO 7 FT FALL SLOPE 2.0:1  
 COMPUTED STREAM SLOPE = 0.0500

\*\*\*\*\*  
 INDEX SHEET FOR BOX CULVERTS  
 INDEX SHEET FOR BOX CULVERTS  
 \*\*\*\*\*

* SEE PAGE * * NUMBER OF * * BARRELS * (FT) * * * * * *	* --- OUTLET CONTROL --- * *				* --- INLET CONTROL --- * *				
	* BARREL*BARREL* * WIDTH* DEPTH* * (FT) * (FT) * * * * * *	* H* * ELEV * (FT) * * * * * *	* INVERT * * ELEV * * (FT) * * * * * *	* GUTLET * * KE= 0.5 * * * * * *	* H* * ELEV * (FT) * * * * * *	* INVERT * * ELEV * * (FT) * * * * * *	* BEVEL-EDGED CULVERT * * * * * *	* SIDE-TAPERED CULVERT * * * * * *	
* 1 * * * * * *	* 1 * * 6.0 * * 7.0 * * * * * *	* 197.1 * * * * * *	* 172.9 * * * * * *	* 172.9 * * * * * *	* 197.1 * * * * * *	* * * * *	* * * * *	* 200.0 * * * * * *	* 183.2 * * * * * *
* 2 * * * * * *	* 1 * * 7.0 * * 6.0 * * * * * *	* 190.1 * * * * * *	* 172.7 * * * * * *	* 172.7 * * * * * *	* 190.1 * * * * * *	* * * * *	* * * * *	* 200.0 * * * * * *	* 194.1 * * * * * *



DESIGN A-PAGE 1

PAGE= 1 NO. BARRELS= 1 WIDTH= 6.0 FT HEIGHT= 7.0 FT Q(50)= 1000.0 CFS STREAM SLOPE = 0.0500  
 OUTLET INVERT ELEV. = 172.9 FT ANWEL= 200.0 FT

CONVENTIONAL INLET DESIGN FOR CULVERT CODE: 41122  
 \*\*\*\*\*

DESIGN DATA NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE CONVENTIONAL INLET EXCEEDS 1.00 OR L50.

BEVELED INLET DESIGN FOR CULVERT CODE:41145  
 \*\*\*\*\*

DESIGN DATA NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE BEVEL-EDGED INLET EXCEEDS 1.50 OR L50  
 THIS OUTPUT CONSISTS OF THE OUTLET CONTROL PERFORMANCE CURVE DATA FOR KE = 0.2  
 WHICH IS APPLICABLE FOR THE IMPROVED INLETS.

Q	HWD	MAX Q =	1078. CFS
800.0	190.9		
1000.0	197.1		
1200.0	204.7		
1400.0	213.7		
1600.0	224.1		

SIDE TAPERED INLET DESIGN  
 \*\*\*\*\*

FACE EDGE BEVELS = 45 DEG SIDE TAPER = 4:1

MIN FALL DESIGN

MAX Q DESIGN

MAX Q = 1078. CFS

MIN HW DESIGN

CULVERT LENGTH = 364.0 FT  
 FALL = 6.9 FT  
 ELEV THROAT INVERT = 183.2 FT  
 ELEV FACE INVERT = 183.3 FT  
 CULVERT SLOPE = 0.0087  
 VEL AT DESIGN Q = 22.1 FPS  
 FACE WIDTH = 8.52 FT  
 L1 = 5.05 FT  
 MIN CREST LENGTH = 16.7 FT  
 BEVELS = 45 DEGREE  
 B = 4.3 IN D = 3.5 IN

CULVERT LENGTH = 368.9 FT  
 FALL = 8.5 FT  
 ELEV THROAT INVERT = 181.5 FT  
 ELEV FACE INVERT = 181.7 FT  
 CULVERT SLOPE = 0.0238  
 VEL AT MAX Q = 30.3 FPS  
 FACE WIDTH = 8.53 FT  
 L1 = 5.07 FT  
 MIN CREST LENGTH = 19.8 FT  
 BEVELS = 45 DEGREE  
 B = 4.3 IN D = 3.5 IN

CULVERT LENGTH = 372.5 FT  
 FALL = 9.8 FT  
 ELEV THROAT INVERT = 180.3 FT  
 ELEV FACE INVERT = 180.4 FT  
 CULVERT SLOPE = 0.0202  
 VEL AT DESIGN Q = 27.9 FPS  
 FACE WIDTH = 8.5 FT  
 L1 = 5.00 FT  
 MIN CREST LENGTH = 19.9 FT  
 BEVELS = 45 DEGREE  
 B = 4.2 IN D = 3.5 IN

Q	HWT	HWF	Q	HWT	HWF	Q	HWT	HWF
800.0	196.4	196.0	800.0	194.8	194.3	800.0	193.6	193.1
1000.0	200.0	199.8	1000.0	198.4	198.1	1000.0	197.1	196.9
1200.0	204.4	204.6	1200.0	202.8	202.9	1200.0	201.6	201.8
1400.0	209.8	210.3	1400.0	208.2	208.6	1400.0	206.9	207.5
1500.0	215.8	216.4	1600.0	214.2	214.7	1600.0	213.0	213.6

SLOPE TAPERED INLET DESIGN - VERTICAL FACE  
 \*\*\*\*\*

DISTANCE EMBANKMENT-TOE TO FACE = 20.42 FT

MIN FALL DESIGN

CULVERT LENGTH = 341.8 FT  
 FALL = 6.0 FT  
 ELEV THROAT INVERT = 193.2 FT  
 ELEV FACE INVERT = 193.0 FT  
 CULVERT SLOPE = 0.0318  
 VEL AT DESIGN Q = 33.5 FT  
 FACE WIDTH = 12.61 FT  
 L1 = 16.09 FT  
 L2 = 15.4 FT  
 L3 = 3.0 FT  
 SF = 2.00  
 TAPER = 5.54:1

DISTANCE EMBANKMENT-TOP TO FACE = 23.74 FT

MAX Q DESIGN

CULVERT LENGTH = 341.8 FT  
 FALL = 8.4 FT  
 ELEV THROAT INVERT = 191.5 FT  
 ELEV FACE INVERT = 190.0 FT  
 CULVERT SLOPE = 0.0271  
 VEL AT MAX Q = 31.9 FT  
 FACE WIDTH = 13.62 FT  
 L1 = 21.89 FT  
 L2 = 18.7 FT  
 L3 = 3.0 FT  
 SF = 2.00  
 TAPER = 5.69:1

Q	HWT	HWF	Q	HWT	HWF
800.0	196.4	196.0	800.0	194.8	197.6
1000.0	200.0	199.8	1000.0	198.4	199.1
1200.0	204.4	201.8	1200.0	202.8	203.9
1400.0	209.8	204.3	1400.0	208.2	203.0
1500.0	215.8	207.2	1600.0	214.2	205.5

DESIGN DATA-PAGE 1 (CONT'D)

SLOPE TAPERED INLET DESIGN - MITEPED FACE  
 \*\*\*\*\*

MIN FALL DESIGN

CULVERT LENGTH = 362.3 FT  
 FALL = 7.8 FT  
 ELEV THROAT INVERT = 193.2 FT  
 ELEV FACE INVERT = 197.9 FT  
 CULVERT SLOPE = 0.025  
 VEL AT DESIGN Q = 32.0 FPS  
 FACE WIDTH = 10.62 FT  
 L1 = 20.22 FT  
 L2 = 7.8 FT  
 L3 = 3.0 FT  
 L4 = 9.4 FT  
 SF = 2.00  
 TAPER = 1.69:1

Q	HWT	HWF
800.0	196.4	197.2
1000.0	200.0	199.6
1200.0	204.4	202.6
1400.0	209.8	206.2
1600.0	215.8	210.4

MAX Q DESIGN

CULVERT LENGTH = 362.3 FT  
 FALL = 9.8 FT  
 ELEV THROAT INVERT = 191.6 FT  
 ELEV FACE INVERT = 197.9 FT  
 CULVERT SLOPE = 0.025  
 VEL AT MAX Q = 31.1 FPS  
 FACE WIDTH = 11.24 FT  
 L1 = 25.97 FT  
 L2 = 11.2 FT  
 L3 = 3.0 FT  
 L4 = 9.1 FT  
 SF = 2.00  
 TAPER = 5.22:1

Q	HWT	HWF
800.0	194.8	196.6
1000.0	198.4	199.7
1200.0	202.8	201.2
1400.0	208.2	204.3
1600.0	214.2	207.9

DESIGN DATA-PAGE 2

PAGE= 2 NO. BARRELS= 1 WIDTH= 7.0 FT HEIGHT= 6.0 FT Q(50)= 1000.0 CFS AHWEL= 200.0 FT STREAM SLOPE = 0.0500  
 OUTLET INVERT ELEV. = 172.7 FT

CONVENTIONAL INLET DESIGN FOR CULVERT CODE 41122  
 \*\*\*\*\*

DESIGN DATA NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE CONVENTIONAL INLET EXCEEDS 1.50 OR LSO.

BEVELED INLET DESIGN FOR CULVERT CODE:41145  
 \*\*\*\*\*

DESIGN DATA NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE BEVEL-EDGED INLET EXCEEDS 1.50 OR LSO  
 THIS OUTPUT CONSISTS OF THE OUTLET CONTROL PERFORMANCE CURVE DATA FOR KE = 0.2  
 WHICH IS APPLICABLE FOR THE IMPROVED INLETS.

Q	HWC	MAX Q =	1106. CFS
800.0	189.3		
1000.0	196.1		
1200.0	203.7		
1400.0	212.8		
1600.0	223.2		

BOX SECTION

SIDE TAPERED INLET DESIGN  
 \*\*\*\*\*

FACE EDGE BEVELS = 45 DEG SIDE TAPER = 4:1

MIN FALL DESIGN

CULVERT LENGTH = 367.3 FT  
 FALL = 6.1 FT  
 ELEV THROAT INVERT = 184.1 FT  
 ELEV FACE INVERT = 184.3 FT  
 CULVERT SLOPE = 0.0216  
 VEL AT DESIGN Q = 33.9 FPS  
 FACE WIDTH = 9.98 FT  
 L1 = 5.98 FT  
 MIN CREST LENGTH = 16.2 FT  
 BEVELS = 45 DEGREE  
 B = 5.0 IN D = 3.0 IN

MAX Q DESIGN

MAX Q = 1106. CFS

CULVERT LENGTH = 374.2 FT  
 FALL = 8.3 FT  
 ELEV THROAT INVERT = 181.9 FT  
 ELEV FACE INVERT = 182.0 FT  
 CULVERT SLOPE = 0.0249  
 VEL AT MAX Q = 31.6 FPS  
 FACE WIDTH = 10.03 FT  
 L1 = 6.05 FT  
 MIN CREST LENGTH = 20.5 FT  
 BEVELS = 45 DEGREE  
 B = 5.0 IN D = 3.0 IN

MIN HW DESIGN

CULVERT LENGTH = 376.0 FT  
 FALL = 9.0 FT  
 ELEV THROAT INVERT = 181.2 FT  
 ELEV FACE INVERT = 181.4 FT  
 CULVERT SLOPE = 0.0230  
 VEL AT DESIGN Q = 29.9 FPS  
 FACE WIDTH = 10.0 FT  
 L1 = 5.91 FT  
 MIN CREST LENGTH = 19.4 FT  
 BEVELS = 45 DEGREE  
 B = 5.0 IN D = 3.0 IN



BOX SECTION

DESIGN DATA-PAGE 2 (CONT'D)

Q	HWT	HWF	Q	HWT	HWF	Q	HWT	HWF
800.0	196.4	193.1	800.0	194.1	193.7	800.0	193.5	193.1
1000.0	200.0	199.9	1000.0	197.7	197.5	1000.0	197.1	197.0
1200.0	204.5	204.7	1200.0	202.2	202.3	1200.0	201.6	201.8
1400.0	209.8	210.2	1400.0	207.5	207.7	1400.0	206.9	207.3
1600.0	215.6	215.7	1600.0	213.4	213.3	1600.0	212.7	212.9

SLOPE TAPERED INLET DESIGN - VERTICAL FACE  
 \*\*\*\*\*

DISTANCE EMBANKMENT-TOE TO FACE = 17.50 FT

CULVERT OUTLET TO EMBANKMENT-TOE = 20.35 FT

MIN FALL DESIGN

MAX Q DESIGN

CULVERT LENGTH = 348.1 FT  
 FALL = 6.0 FT  
 FLEV THROAT INVERT = 164.1 FT  
 ELEV FACE INVERT = 190.1 FT  
 CULVERT SLOPE = 0.0345  
 VEL AT DESIGN Q = 35.0 FT  
 FACE WIDTH = 13.98 FT  
 L1 = 15.93 FT  
 L2 = 13.3 FT  
 L3 = 3.5 FT  
 SF = 2.00  
 TAPER = 4.82:1

CULVERT LENGTH = 348.1 FT  
 FALL = 8.2 FT  
 ELEV THROAT INVERT = 181.9 FT  
 ELEV FACE INVERT = 190.1 FT  
 CULVERT SLOPE = 0.0280  
 VEL AT MAX Q = 33.1 FT  
 FACE WIDTH = 15.45 FT  
 L1 = 21.46 FT  
 L2 = 18.0 FT  
 L3 = 3.5 FT  
 SF = 2.00  
 TAPER = 5.08:1

BOX SECTION

DESIGN DATA-PAGE 2 (CONT'D)

Q	H&T	H&F	Q	HWT	H&F
800.0	196.4	197.8	800.0	194.1	197.2
1000.0	200.0	199.7	1000.0	197.7	198.8
1200.0	204.5	202.0	1200.0	202.2	200.6
1400.0	209.8	204.8	1400.0	207.5	202.9
1600.0	215.6	208.1	1600.0	213.4	205.6

SLOPE TAPERED INLET DESIGN - MITERED FACE  
 \*\*\*\*\*

MIN FALL DESIGN

MIN FALL DESIGN:

CULVERT LENGTH = 365.6 FT  
 FALL = 6.9 FT  
 ELEV THROAT INVERT = 184.1 FT  
 ELEV FACE INVERT = 186.3 FT  
 CULVERT SLOPE = 0.0329  
 VELOCITY AT DESIGN Q = 34.4 FPS  
 FACE WIDTH = 12.07 FT  
 L1 = 18.40 FT  
 L2 = 6.9 FT  
 L3 = 3.5 FT  
 L4 = 8.0 FT  
 SF = 2.00  
 TAPER = 1.08:1

MAX Q DESIGN

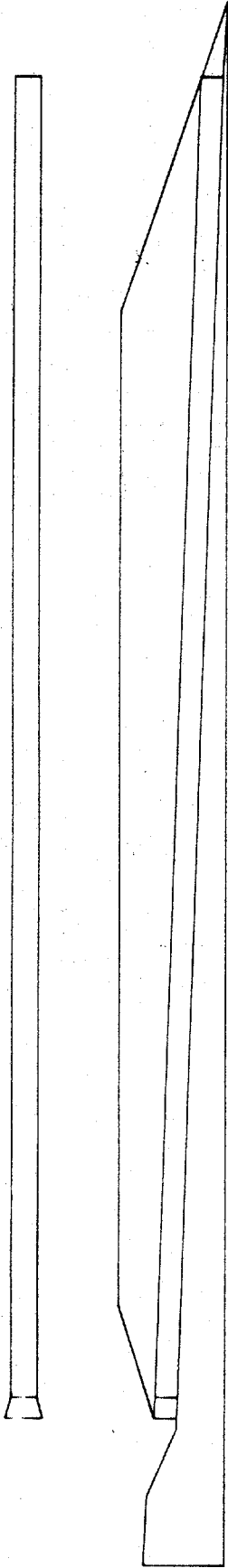
MAX Q DESIGN

---  
 ---  
 ---  
 ---  
 ---  
 ---  
 ---  
 ---  
 ---  
 ---

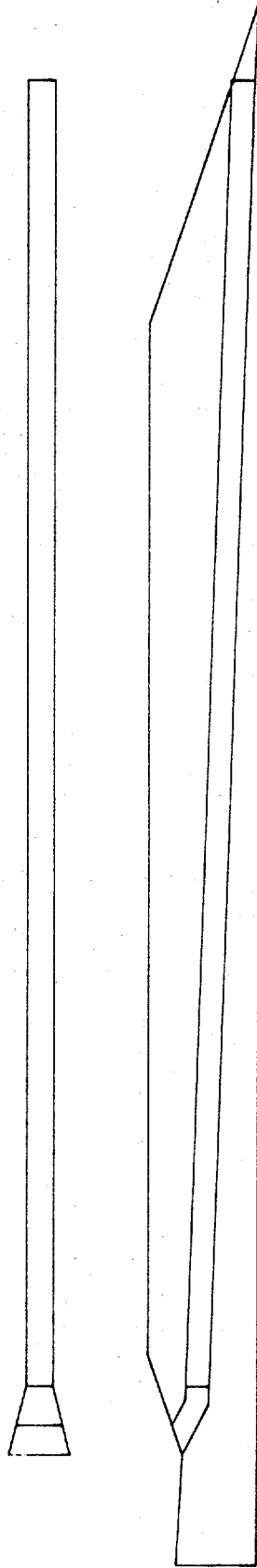
Q	HWT	H&F	Q	HWT	H&F
800.0	196.4	197.2	---	---	---
1000.0	200.0	199.7	---	---	---
1200.0	204.5	202.8	---	---	---
1400.0	209.8	206.7	---	---	---
1600.0	215.6	211.1	---	---	---

PLAN AND PROFILE PLOTS

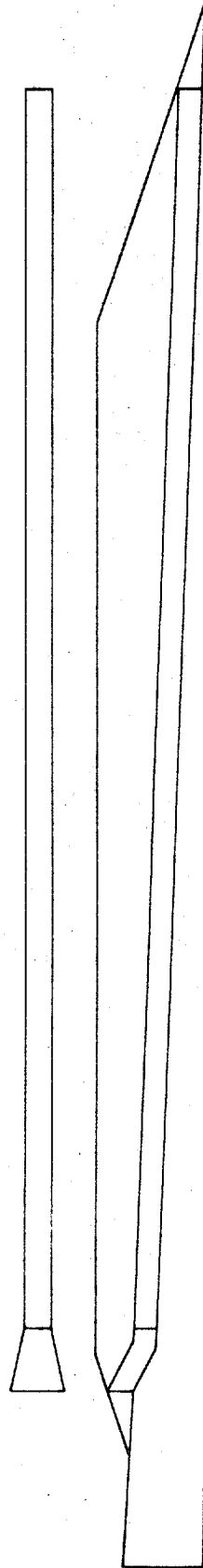
EXAMPLE NO. 1 HEC No. 13 for 7' x 6' Box Culvert



SIDE-TAPERED INLET



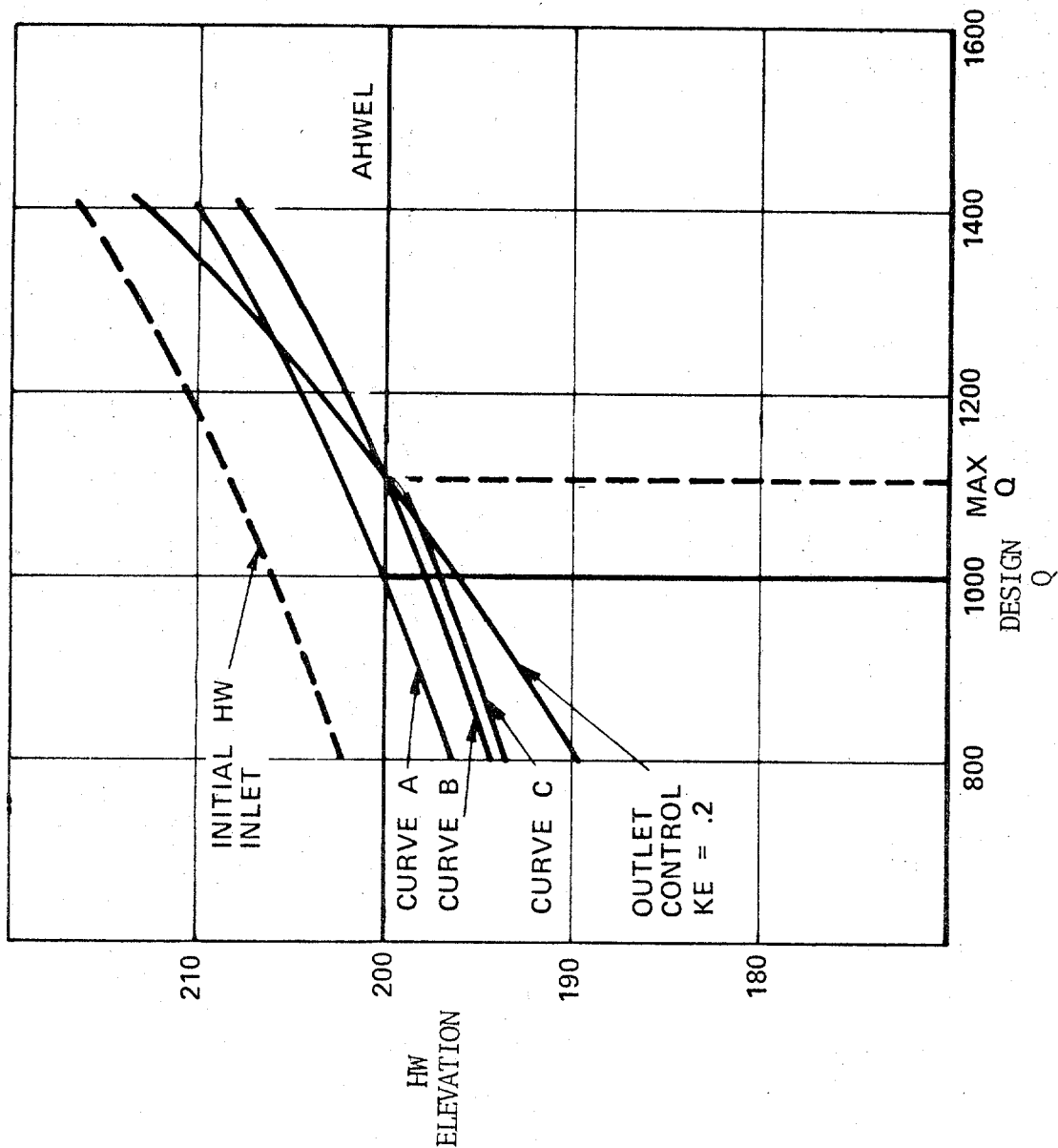
SLOPE-TAPERED INLET - MITERED FACE



SLOPE-TAPERED INLET - VERTICAL FACE

BOX SECTION

EXAMPLE PROBLEM No. 1, PERFORMANCE CURVES  
FOR 1-7'x6' SIDE TAPERED BOX CULVERT



Q cfs

Figure 11

CIRCULAR PIPE SECTION

## CIRCULAR PIPE SECTION

This section of the documentation presents design information for conventional and improved inlets for circular pipes, both corrugated metal and concrete. Included herein are the mathematical equations, design criteria and limitations, code numbers for selecting a pipe type, tables of pipe sizes with associated "n" values for each pipe size, a table of hydraulic constants and example problems.

It should be noted under the section on "Design Criteria and Limitations," that design for side-tapered (flared) metal inlets is based on the standard metal inlet design shown in Figure 12. HEC No. 13 side-tapered designs can be used by initiating the program instructions which are stored in the program as comment cards.

The pipe designs provided by the computer program are divided into three basic categories, i.e., partly paved corrugated metal, unpaved corrugated metal and concrete pipes.

For the metal pipes, Figure 13 shows the three types of metal corrugations that were programmed into the computer process to provide the hydraulic design engineer with sufficient data and still maintain some flexibility in his choice of design options. The choice of design options is controlled by the culvert code indicator, I3, and the options are shown in Table 3.

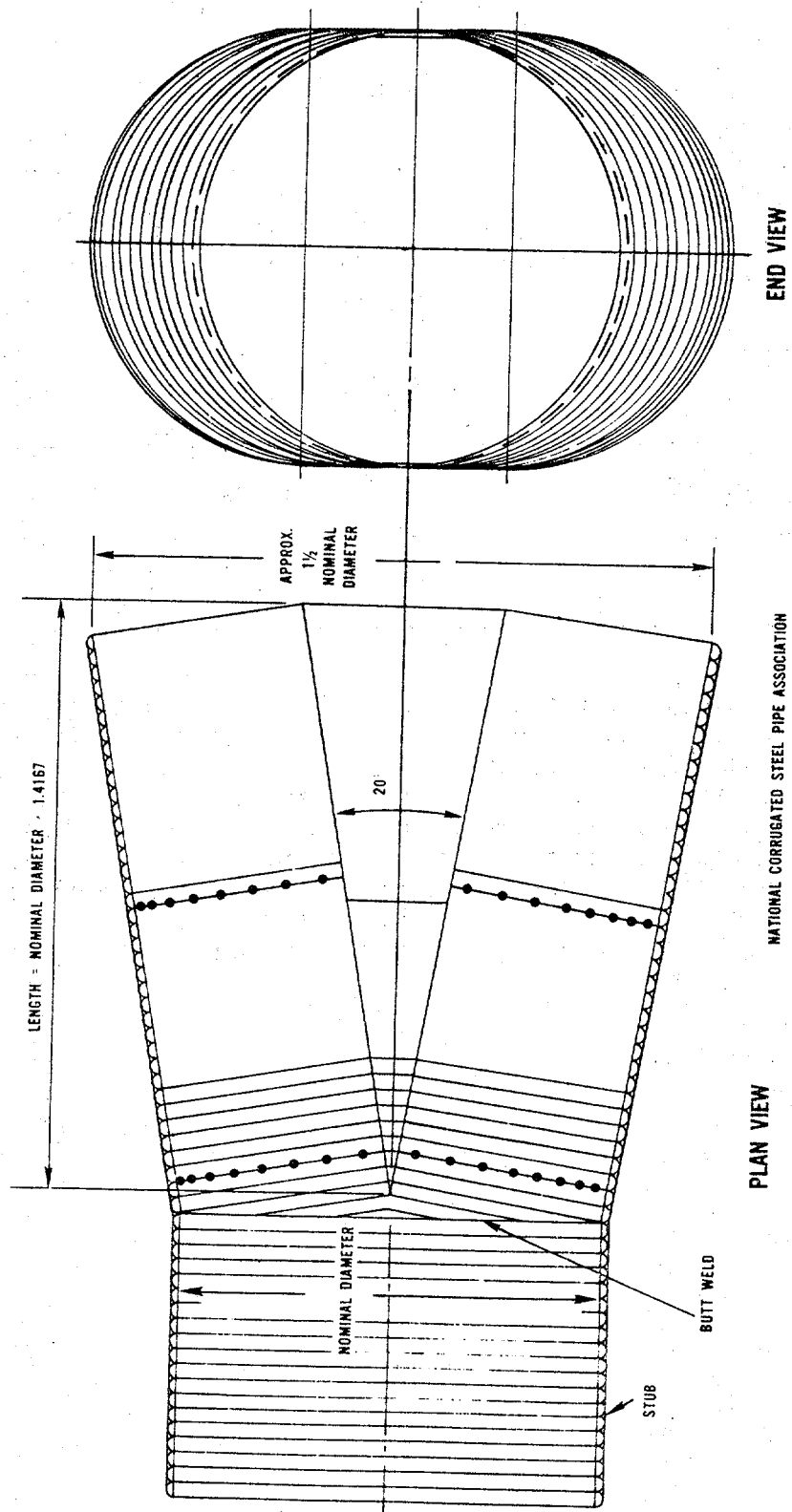
CIRCULAR PIPE SECTION

Table 3

Code Indicator: I3	Options for Corrugated Metal Designs	
	25% Paved Pipe	Unpaved Pipe
When I3 = 1	2-2/3"x1/2", 3"x1", 6"x2"	2-2/3"x1/2", 3"x1", 6"x2"
I3 = 2	3"x1", 6"x2"	3"x1", 6"x2"
I3 = 3	6"x2"	6"x2"

The design options presented in Table 3 are interpreted as follows: If I3 is equal to 1, then the culvert output design data for each of the three corrugated metal types is provided for either the paved or unpaved culverts. If I3 is equal to 2 or 3, then the design data for the corrugated metal types shown is provided for either the paved or unpaved culverts. In example problems 2A and 2B, I3 is equal to 1 and the Index Sheets show the design option as indicated by Table 3 for unpaved CMP. However, in problem 2A, for the range of pipe sizes investigated (4 ft. to 5 ft. diameter) no 6" by 2" corrugated metal pipes satisfied the design criteria.

\* See Table 6 page 71 for the Circular Pipe Culvert Codes.



END VIEW

NATIONAL CORRUGATED STEEL PIPE ASSOCIATION  
DATE = MARCH 1975

PLAN VIEW

**STANDARD FLARED INLET**

Figure 12



CIRCULAR PIPE SECTION

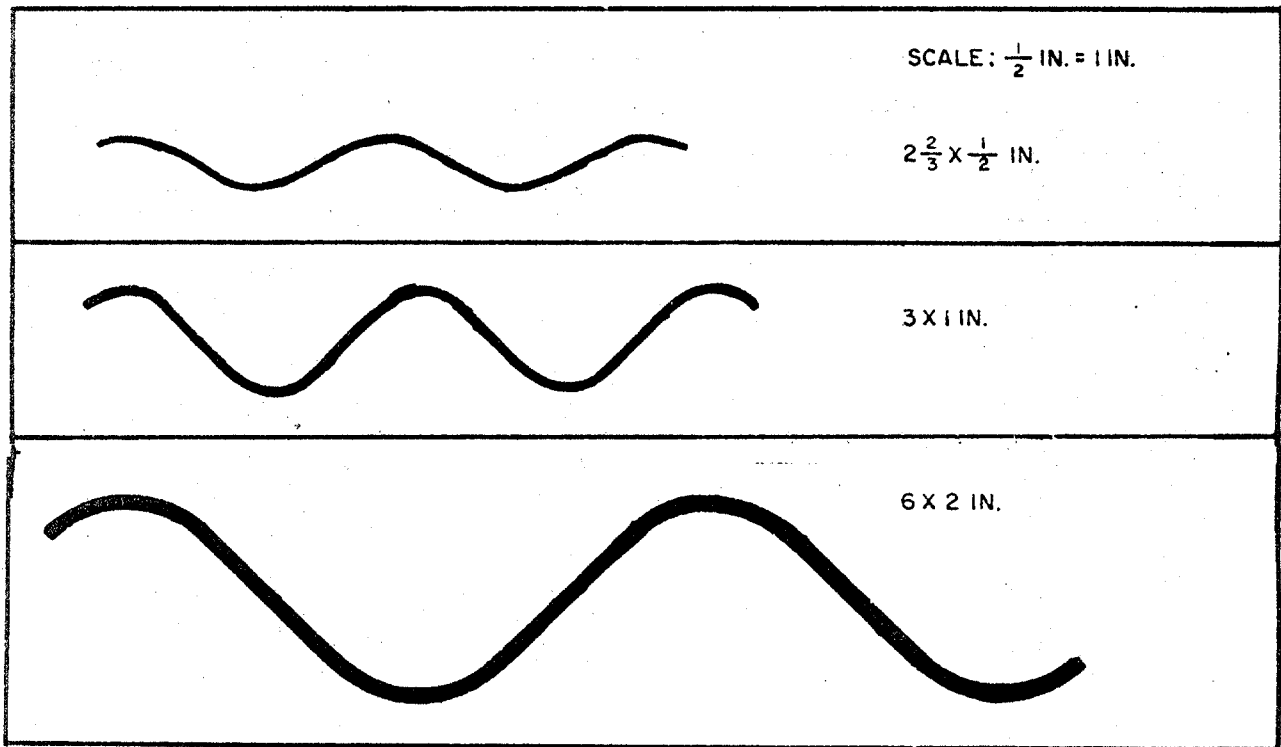


Figure 13. Types of Corrugations Investigated.

The  $2\frac{2}{3}$ " by  $\frac{1}{2}$ " and 3" by 1" corrugated metal pipes are normally riveted and the 6" by 2" structural plate pipes are assembled at the construction site.

CIRCULAR PIPE SECTION

Table 4

Circular Corrugated Metal Pipe Sizes and "n" Values -- Unpaved\*  
for Full Flow

2 2/3" x 1/2" corrugations		3" x 1" corrugations		6" x 2" corrugations	
Dia	n**	Dia	n**	Dia	n**
1.0	.0260	3.0	.0281	5.0	.0332
1.5	.0255	3.5	.0278	5.5	.0330
2.0	.0247	4.0	.0275	6.0	.0327
2.5	.0244	4.5	.0273	6.5	.0325
3.0	.0241	5.0	.0271	7.0	.0323
3.5	.0237	5.5	.0269	7.5	.0321
4.0	.0235	6.0	.0267	8.0	.0320
4.5	.0233	6.5	.0266	8.5	.0318
5.0	.0232	7.0	.0265	9.0	.0317
5.5	.0231	7.5	.0264	9.5	.0315
6.0	.0229	8.0	.0263	10.0	.0314
6.5	.0228	8.5	.0262	10.5	.0313
7.0	.0227	9.0	.0261	11.0	.0312
7.5	.0226	9.5	.0260	11.5	.0311
8.0	.0225	10.0	.0260	12.0	.0310
				12.5	.0309
				13.0	.0308
				13.5	.0307
				14.0	.0307
				14.5	.0306
				15.0	.0305
				15.5	.0305
				16.0	.0304
				16.5	.0304
				17.0	.0303
				17.5	.0303
				18.0	.0302
				18.5	.0302
				19.0	.0301
				19.5	.0301
				20.0	.0300
				20.5	.0300
				21.0	.0300

\* For partly paved CMP, the program uses "n" values based on the equation  $n = .75 \times n + (.25)(.012)$ .

\*\* Based on Research and Development Staff Report "Hydraulic Flow Resistance Factors for Corrugated Metal Conduits," dated September 1970.

CIRCULAR PIPE SECTION

Table 5

Concrete Pipe Sizes and "n" Values

---

<u>Dia</u>	<u>"n"</u>
2.00	.012
2.25	"
2.50	"
2.75	"
3.00	"
3.50	"
4.00	"
4.50	"
5.00	"
5.50	"
6.00	"
6.50	"
7.00	"
7.50	"
8.00	"
8.50	"
9.00	"
9.50	"
10.00	"
10.50	"
11.00	"
11.50	"
12.00	"
12.50	"
13.00	"
13.50	"
14.00	"
14.50	"
15.00	"

## CIRCULAR PIPE SECTION

### MATHEMATICAL EQUATIONS

The mathematical equations for circular pipes are as follows:

#### INLET CONTROL HEADWATER - Conventional and Bevel-Edged Inlets

$$H_f = (D)[Y-(S)(SCORR)] \quad (1)$$

Where:  $H_f$  = headwater depth in feet

$$Y = A + BX + CX^2 + DX^3 + EX^4 + FX^5$$

D = diameter of pipe in feet

A, B, C, D, E & F are coefficients listed on page 73

SCORR = slope correction factor (table 7, page 73)

S = the slope of the pipe in feet per foot

$$X = Q/D^{5/2}$$

Q = discharge in cfs

#### INLET CONTROL HEADWATER - Side-Tapered Inlets

##### 1. Throat Control - (Chart 18, HEC No. 13)

###### a. Rough Inlets (CMP)

$$H_t/D = -.23339 + .48913X + 1.06864X^2 - 3.074435X^3 + 3.711165X^4 - 1.32836X^5 \quad (2)$$

Where:  $X' = (Q/BAR)/DIA^{5/2}$

$X = \log(X')$

BAR = No. of barrels

###### b. Smooth Inlets - (concrete)

$$H_t/D = -0.23714 + .14679X + 2.18932X^2 - 4.354114X^3 + 4.210539X^4 - 1.347032X^5 \quad (3)$$

Where:  $X' = (Q/BAR)/DIA^{5/2}$

$X = \log(X')$

## CIRCULAR PIPE SECTION

### 2. Face Control - (Chart 19, HEC No. 13)

Face control headwater is computed based on face sizes established by Standard Flared Inlets, where face width is  $1.5D$  and  $L1 = 1.4167D$ . Figure 12 represents a standard flared inlet proposed by the National Corrugated Steel Pipe Association. Equations for face control based on HEC No. 13 are found in Subroutine CSIDE.

### INLET CONTROL HEADWATER - Slope-Tapered Inlets (Chart 16, HEC No. 13)

The inlet designs for slope-tapered inlets are based on Chart 16 (Solid line) in HEC No. 13, face control curves for box culverts. The equation to compute face width is:

$$B_f = Q / (Y \times \text{DIA}^{3/2})$$

$$\text{Where: } Y = 2.26586 + 7.94244X - 4.03503X^2 + 1.61948X^3 - .34582X^4 + .0284677X^5 \quad (4)$$

$$X = H_f / \text{DIA}$$

$H_f$  = allowable Headwater elevation minus face elevation

Throat control equations for slope-tapered inlets same as for side-tapered inlets on page 60.

### Outlet Velocity

$$Q = [1.486/n](AR^{2/3} S^{1/2})$$

Where:  $Q$  = discharge in cfs  
 $A$  = area of water in sq. ft. at any depth of flow defined by equation (13), page 64  
 $WP$  = wetted perimeter in feet at an depth of flow by equation 14, page 64  
 $R$  = hydraulic radius in feet =  $A/WP$   
 $S$  = slope of the pipe in feet per foot  
 $n$  = Manning's roughness value

## CIRCULAR PIPE SECTION

### Outlet Control Equations

$$H = \left[ 1 + K_e + \frac{185.0 n^2 L}{D^{4/3}} \right] \left[ \frac{Q^2}{(39.725)(D)^4} \right] \quad (6)$$

Where: H = the head for circular culverts flowing full, in feet

$K_e$  = the entrance loss coefficient

L = length of pipe in feet

D = diameter of pipe in feet

### Critical Depth

$$\frac{\alpha Q^2}{g} = \frac{A^3}{T} \quad (7)$$

Where: Q = discharge in cfs

$\alpha$  = alpha, coefficient

g = 32.2 ft/sec<sup>2</sup>

A = the area of water in sq. ft. at any depth defined by equation (13), page 64

T = the top surface width of water in feet at any depth of flow defined by equation (15), page 64

### Outlet Control Headwater

HW = TEMP + H + elevation of outlet invert, in feet

Where: TEMP = Distance to the hydraulic gradeline from the culvert outlet invert

HW = the headwater elevation, in feet

$d_c$  = critical depth, in feet

When:  $d_c \geq D$  and  $D > TW$ , then TEMP = D

$d_c < D$  and  $\frac{d_c + D}{2} > TW$ , then TEMP =  $\frac{d_c + D}{2}$

$TW > D$  or  $TW > \frac{d_c + D}{2}$ , then TEMP = TW

Where: TW = tailwater height, in feet

H = head for full flow, in feet

## CIRCULAR PIPE SECTION

Water Surface Profiles for  $d_n \geq d_c$

$$X = \frac{\left( d_1 + \frac{v_1^2}{2g} \right) - \left( d_2 + \frac{v_2^2}{2g} \right)}{S_o - S} \quad (\text{M1 Curve}) \quad (9)$$

$$X = \frac{\left( d_2 + \frac{v_2^2}{2g} \right) - \left( d_1 + \frac{v_1^2}{2g} \right)}{S - S_o} \quad (\text{M2 Curve}) \quad (10)$$

Where:  $X$  = distance in feet between two sections of water  
 $d_1, d_2$  = depths in feet at sections 1 and 2 respectively

$v_1, v_2$  = velocities in feet per second at sections 1 and 2

$S_o$  = slope of the pipe in feet per foot

$$S = \frac{n^2 v^2}{2.21 R^{4/3}}$$

$S$  = the slope of the water surface in feet per foot

$R$  = the average hydraulic radius in feet of the two sections

Based on water surface profiles in the culvert, the headwater is:

$$HW = d_2 + \frac{v_2^2}{2g} + \frac{k_e v_1^2}{2g} \quad (11)$$

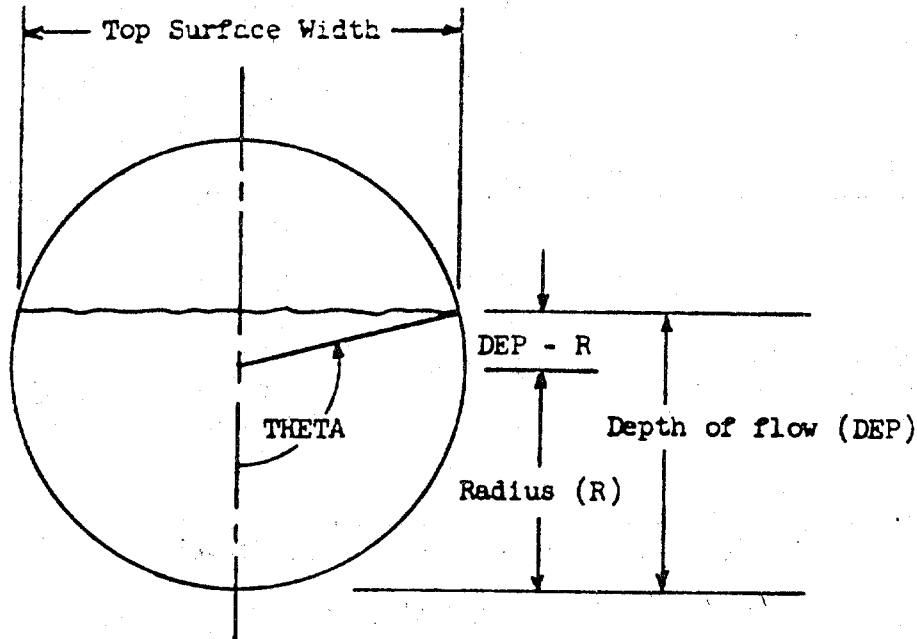
Where:  $d_2$  = either the height of culvert or water depth at inlet depending on the water surface profile in the culvert

$k_e$  = the entrance loss coefficient for the specific inlet type

Outlet Velocity

$$v = \frac{Q}{A}$$

## CIRCULAR PIPE SECTION



$$A = (DEP-R) \sqrt{(2R)(DEP) - DEP^2 + R^2} \left[ \pi/2 + \sin^{-1} \left( \frac{DEP-R}{R} \right) \right] \quad (13)$$

For  $DEP < R$  use  $ABS((DEP-R)/R)$  and use  $(-\sin^{-1})$

Where  $A$  is the area in square feet

$$WP = 2R \left[ \pi/2 + \sin^{-1} \left( \frac{DEP-R}{R} \right) \right] \quad (14)$$

Where  $WP$  is the wetted perimeter in feet

$$T = 2 \sqrt{R^2 - (DEP-R)^2} \quad (15)$$

Where  $T$  is the top surface width in feet

### Side-Tapered and Slope-Tapered Inlets

The equations for throat control and face control for the CMP and concrete pipes (representing charts 18 and 19, HEC No. 13) are located in subroutines CSIDE and CSLOPV. These equations are polynomials developed by a curve fitting technique.



## CIRCULAR PIPE SECTION

### DESIGN CRITERIA AND LIMITATIONS

The design criteria and limitations are basically the same as for box culverts as indicated in HEC No. 13 and are listed below along with additional circular pipe criteria for ease in accessibility.

#### CONVENTIONAL CMP AND CONCRETE PIPE - Culvert Design Criteria

1. Inlet control headwater and outlet control headwater  $\geq (AHWEL - D/4) \leq AHWEL$ . Where AHWEL is the allowable headwater elevation.
2. Pipe sizes limited to diameter sizes listed in tables 4 and 5.
3. Pipe material includes 2 2/3" by 1/2", 3" by 1", 6" by 2" corrugated metal and concrete.
4. Mannings "n" values for partly paved CMP are based on the equation:  
$$n = (0.75) n_1 + .25 (.012)$$
, where  $n_1$  represents the "n" value for the same pipe diameter as "n" but without paving and .012 represents "n" value for concrete.
5. Crown elevation not greater than controlling headwater elevation.
6. Use FALL at inlet invert when inlet headwater is greater than allowable headwater.
7. FALL not to exceed Maximum FALL.  
Where: Max FALL =  $1.5D^*$   
or inlet invert elevation not less than outlet invert elevation.
8. Minimum crest length based on Chart 17 in HEC No. 13.

\*Limitations related to HEC No. 13.

## CIRCULAR PIPE SECTION

### SIDE-TAPERED INLET - Design Criteria

1. E (height) equal to diameter<sup>\*</sup>
2. Face width equal to standard flared inlets (See Figure 12)<sup>\*\*</sup>
3.  $L_1 = 1.4167D$
4. Taper =  $L_1 / (\text{Face width minus DIA}) / 2$
5. FALL = Max FALL<sup>\*</sup>

Where: Max FALL =  $1.5D$ <sup>\*</sup> or inlet invert elevation  
not less than outlet invert elevation.

6. Multiple barrels designed as separate single barrels
7. Throat control represented by curves on Chart 18 of  
HEC No. 13<sup>\*</sup>

<sup>\*</sup> Limitations related to HEC No. 13

<sup>\*\*</sup> National Corrugated Steel Pipe Association

## CIRCULAR PIPE SECTION

### VERTICAL FACE, SLOPE-TAPERED INLET DESIGN

Inlet design same as for box culvert inlet.

1. Multiple barrels designed as single barrels
2. Taper = 4:1 to 6:1\*
3. Fall slope (SF) - Input data from 2:1 to 3:1 inclusive\*
4.  $L_3 = .5B^*$  Minimum
5.  $1.5D \geq \text{FALL} \geq D/4^*$
6. Throat elevation > outlet toe elevation
7. FALL = vertical distance between face invert elevation and throat invert elevation
8. Design for face section limited to solid line curve on Chart 16 of HEC No. 13
9. Rectangular throat section of inlet must be square section with sides equal to diameter of pipe culvert
10. Minimum transition section =  $D/2$

\* Limitations related to HEC No. 13

## CIRCULAR PIPE SECTION

To assist in the use of the pipe culvert code tables, the following definitions will be helpful:

### Type of Pipe

1. Riveted corrugated metal pipe - commonly used riveted metal pipe with 2 2/3" x 1/2" corrugations.
2. Riveted corrugated metal pipe - commonly used riveted metal pipe with 3" x 1 corrugations.
3. Structural plate pipe - sections of structural steel plates with 6" x 2" corrugations. Plates are field assembled.
4. Concrete pipe - any concrete pipe in common use. No distinction is made for length of sections or method of casting.

### Paved Invert

Paved invert relates to a material, asphalt or concrete plated in the bottom portion of the metal culvert barrel.

### Types of Conventional Inlets

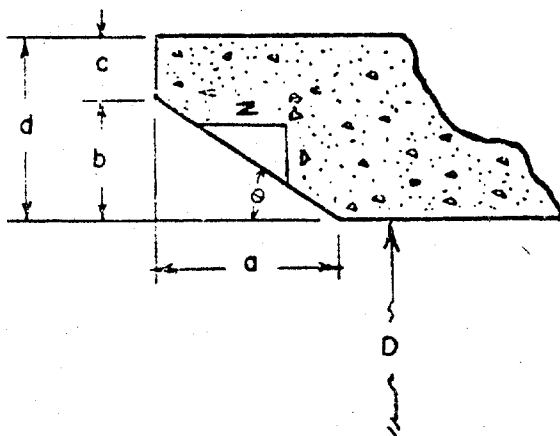
1. Projecting - The culvert barrel extends from the embankment. The transverse section at the inlet is perpendicular to the longitudinal axis of the culvert.
2. Mitered - The end of the culvert barrel is on a miter or bevel to conform with the fill slope. All degrees of miter are treated alike in this program since research data on this type of inlet are limited. Headwater is measured from the culvert invert midway of the mitered section.
3. Headwall - A headwall is a concrete or metal structure placed around the entrance of the culvert. Headwalls considered are those having a flush or square edge with the outside edge of the culvert barrel. No distinction is made for wingwalls or skews.

## CIRCULAR PIPE SECTION

4. End section - This section is the common prefabricated end made of either concrete or metal and placed on the inlet or outlet end of a culvert. The closed portion of the section, if present, is not tapered.
5. Grooved edge - The bell or socket end of a standard concrete pipe is an example of this entrance.
6. Bevel A and Bevel B - These bevels, a type of improved entrance, can be formed of concrete or metal. The shape and dimension for types A and B are shown in the following sketch and table.

### BEVELED RING

The bevel should extend a minimum of 300 degrees around the upper portion of the pipe's circumference.



Bevel can be made of  
Metal or Concrete

BEVEL	$\frac{b}{D}$	$\frac{a}{D}$	$\frac{c}{D}$	$\frac{d}{D}$	Z	$\theta$
A	0.042	0.042	0.042	0.083	1	45°
B	0.063	0.125	0.042	0.125	1 1/2	33.7

## CIRCULAR PIPE SECTION

### Types of Improved Inlets

The improved inlet types are well defined in HEC No. 13. For side-tapered inlets, the face width determined by HEC No. 13 design procedures for any pipe diameter should be compared to the face width for comparable ready-made standardized side-tapered inlet. The computer program utilizes the face dimensions for a standard inlet as shown in Figure 12.

Slope-tapered inlets for circular pipes, are designed the same as for box culverts with the exception of a transition section with minimum length of  $D/2$  between the rectangular and circular sections. The controlling throat section is at the circular section of the throat.

CIRCULAR PIPE SECTION

Table 6

METAL PIPE CULVERT CODE INDICATORS\*\*

Inlet Type	RIVETED With 2 2/3" x 1/2" Corrugation					RIVETED With 3" x 1" Corrugation					STRUCTURAL PLATE With 6"x2" Corrugation				
	I1	I2	I3	I4	I5	I1	I2	I3	I4	I5	I1	I2	I3	I4	I5
Projecting (112)***	1	1	1	1	1*	1	1	2	1	1*	1	1	3	1	1*
Mitered (81)	1	1	1	2	2*	1	1	2	2	2*	1	1	3	2	2*
Headwall (7)	1	1	1	3	3*	1	1	2	3	3*	1	1	3	3	3*
End Section (51)	1	1	1	3	5	1	1	2	3	5	-	-	-	-	-
Bevel (A) (option)	1	1	1	4	6	1	1	2	4	6	1	1	3	4	6
Bevel (B)	1	1	1	4	7	1	1	2	4	7	1	1	3	4	7
	RIVETED & 25% Paved 2 2/3" x 1/2" Corrugation					RIVETED & 25% Paved 3" x 1" Corrugation					STRUCTURAL PLATE & 25% Paved 6" x 2" Corrugation				
	I1	I2	I3	I4	I5	I1	I2	I3	I4	I5	I1	I2	I3	I4	I5
Projecting (112)	1	2	1	1	1*	1	2	2	1	1*	1	2	3	1	1*
Mitered (81)	1	2	1	2	2*	1	2	2	2	2*	1	2	3	2	2*
Headwall (7)	1	2	1	3	3*	1	2	2	3	3*	1	1	3	3	3*
End Section (51)	1	2	1	3	5	1	2	2	3	5	-	-	-	-	-
Bevel (A) (option)	1	2	1	4	6	1	2	2	4	6	1	2	3	4	6
Bevel (B)	1	2	1	4	7	1	2	2	4	7	1	2	3	4	7

\* In the computer, I5 value equals the above value plus 7, giving I5 values of 8, 9, 10

\*\* Used in the computer program and references the subscript of the CONSTANTS and Inlet Control Equation Coefficients.

\*\*\* See note on page 72

CIRCULAR PIPE SECTION

Table 6 (cont'd)

CONCRETE PIPE CODE INDICATORS

	I1	I2	I3	I4	I5
Socket-end Projecting (102)***	2	3	4	4	1
Socket-end Headwall (4)	2	3	4	4	2
Square-edge Projecting (101)	2	3	4	3	3
Square-edge Headwall (1)	2	3	4	3	4
End Section (51)	2	3	4	3	5
<hr style="border-top: 1px dashed black;"/>					
Bevel (A) (option)	2	3	4	4	6
Bevel (B)	2	3	4	4	7

\*\*\* Values in parentheses following the inlet types refer to the hydraulic experimental model number taken from "First Progress Report on Hydraulics of Short Pipes, Hydraulic Characteristics of Commonly Used Pipe Entrances," by John L. French, dated 1955, U.S. Department of Commerce, National Bureau of Standards, pages 48-74.



CIRCULAR PIPE SECTION

Table 7

HYDRAULIC CONSTANTS

I1 - Velocity Distribution Factors				I4 - Entrance Loss Coefficients			
1	CMP	ALPHA <sub>1</sub>	= 1.12**	1	CM projecting	CKE <sub>1</sub>	= 0.90
2	Concrete	ALPHA <sub>2</sub>	= 1.04**	2	CM mitered	CKE <sub>2</sub>	= 0.70
<u>Slope Correction Factor</u>				3	Sq. edge; Concrete or CMP and end section	CKE <sub>3</sub>	= 0.50
Scorr = 0.50				4	Improved inlets	CKE <sub>4</sub>	= 0.20
Scorr = 0.00 (mitered face)				5	Socket-end, concrete headwall or projecting	CKE <sub>5</sub>	= 0.20
Inlet Control Equation Coefficients							
I5	A	B	C	D	E	F	I5
1	0.108786	0.662381	-0.233801	0.0579585	-0.00557890	0.000205052	1
2	0.114099	0.653562	-0.233615	0.0597723	-0.00616338	0.000242832	2
3	0.167287	0.558766	-0.159813	0.0420069	-0.00369252	0.000125169	3
4	0.087483	0.706578	-0.253295	0.0667001	-0.00661651	0.000250619	4
5	0.120659	0.630768	-0.218423	0.0591815	-0.00599169	0.000229287	5
6	0.063343	0.766512	-0.316097	0.0876701	-0.00983695	0.000416760	6
7	0.081730	0.698353	-0.253683	0.0651250	-0.00719750	0.000312451	7
8	0.187321	0.567710	-0.156544	0.0447052	-0.00343602	0.000089661	8
9	0.107137	0.757789	-0.361462	0.1233932	-0.01606422	0.000767390	9
10	0.167433	0.538595	-0.149374	0.0391543	-0.00343974	0.000115882	10

\*\* Values based on Research and Development Staff Report, "Computation of Uniform and Nonuniform Flow in Prismatic Conduits," U.S. Department of Transportation, Federal Highway Administration, November 1972.

## CIRCULAR PIPE SECTION

### EXAMPLE PROBLEM NO. 2A - Corrugated Metal Pipe Design

This design problem, 2A, and the accompanying problem, 2B, simulate corrugated metal and reinforced concrete pipe culvert designs contained in HEC No. 13. The input data for each problem is presented on the attached input data forms. The insignificant difference in values is attributed to the methods of computations, i.e., the computer versus the hand calculation method. Where the hand method uses close approximations in geometric configuration and nomograph interpretation, the computer process is more precise, using geometric and equation oriented computer (algorithms) routines to perform the computations.

As noted previously, the side-tapered (flared) inlet designs produced by the computer program for the Corrugated Metal Pipe follow the standardized inlet dimensions.



## CIRCULAR PIPE SECTION

The INDEX SHEET for problem 2A lists three pipe sizes (4.0, 4.5 and 5.0 ft. diameter) under the 2-2/3 inch by 1/2 inch corrugated metal and the same three pipe sizes for the 3 inch by 1 inch corrugated metal. For the 6 inch by 2 inch multiplate pipe, the INDEX SHEET shows a 5.0 foot diameter pipe. The advantage in providing the INDEX SHEET is self evident, in that the hydraulic design engineer has at his "finger tips" the pipe culvert sizes, number of barrels, the outlet control headwater and the inlet control headwater for the available inlet types. The availability of all this information reduces the amount of time and effort needed by the engineer to make a thorough investigation of the hydraulic problem at hand. Along with the INDEX SHEET, the design data sheets provide the necessary geometric dimensions for the culverts listed on the INDEX SHEET. More importantly, performance curve data is provided for additional culvert analysis.

CIRCULAR PIPE SECTION

INDEX SHEET - PROBLEM 2A

>>>> PIPE CULVERT DESIGN FOR PROJECT >>>> SAMPLE #2A CMP HEC-13 ARHW=100.

>>>> THE PROGRAM PROVIDES A RANGE OF CONVENTIONAL PIPE CULVERT SIZES WITH AND WITHOUT BEVELS WHICH SATISFY SITE REQUIREMENTS

WHERE: REVELED EDGES FOR CMP AND CONCRETE PIPES  
ARE BASED ON CHART 13 IN HEC-13

>>>> IF INLET CONTROL COVERS - IMPROVED INLET DESIGNS ARE PROVIDED FOR SIDE-TAPERED INLETS  
AND SLOPE-TAPERED INLETS

\*\*\*\*\*  
DESIGN INPUT DATA \*\*\*\*\*  
\*\*\*\*\*  
DESIGN INPUT DATA \*\*\*\*\*  
\*\*\*\*\*

CONVENTIONAL CULVERT ----- CM PIPE - HEADWALL - UNPAVED KE= 0.5  
BEVEL-EDGED CULVERT ----- CM PIPE - UNPAVED WITH BEVEL(A) KE= 0.2

CULVERT CODE	APPROX STREAM SLOPE	DESIGN DISCHARGE	DESIGN TAILWATER	ALLOWABLE HEADWATER ELEVATION	STREAM BED ELEVATION AT INLET	STREAM BED ELEVATION AT OUTLET	LEFT ROADWAY EMBANKMENT SLOPE	RIGHT ROADWAY EMBANKMENT SLOPE
11133	0.0500	150.0	2.0	100.0	93.3	75.0	2.0:1	2.0:1

CULVERT SIZES  
DIAMETER FROM 4.00 FT TO 5.00 FT  
SLOPE-TAPER  
FALL SLOPE  
2.0:1  
COMPUTED STREAM  
SLOPE = 0.0500

\*\*\*\*\*  
INDEX SHEET FOR PIPE CULVERTS \*\*\*\*\*  
\*\*\*\*\*  
INDEX SHEET FOR PIPE CULVERTS \*\*\*\*\*  
\*\*\*\*\*

* SEE PAGE #	* NUMBER OF BARRELS*	* DIAMETER (FT)	* -- OUTLET CONTROL -- **			* -- INLET CONTROL -- **					
			* KE= 0.5	* KE=0.2	* OUTLET **	* INVERT **	* HW ELEV **	* INVERT **	* HW ELEV **	* THROAT *HW ELEV	* FALL (FT)
1	1	4.00	85.0	84.4	75.4	100.0	91.9	100.0	92.4	99.3	92.7
2	1	4.50	83.2	87.7	75.5	99.0	92.9	99.0	92.9	98.4	92.6
3	1	5.00	84.8	84.6	75.5	98.4	92.8	98.2	92.8	97.9	92.5

2-2/3 IN X 1/2 IN CORRUGATED-METAL PIPE - UNPAVED

INDEX SHEET - PROBLEM 2A (Cont'd)

Station	Structure	Material	Length	Inlet Elev.	Outlet Elev.	Flow	Velocity	Head Loss	Water Surface Elev.	Bottom Elev.
4	3' x 1' in	CORRUGATED-METAL PIPE	4.00	93.6	93.0	1.0	100.0	0.5	92.4	93.3
5	4	UNPAVED	4.50	90.2	75.5	0.0	100.0	0.3	92.9	98.4
6	5	UNPAVED	5.00	85.9	75.5	0.0	99.3	0.3	92.5	97.9
7	6	3' x 2' in	5.00	93.7	93.4	0.0	98.2	0.3	92.3	97.9

BY DEFINITION OF FALL, WHEN A SIDE-TAPERED INLET LIES ON THE STREAM SLOPE, THE FALL IS THE DIFFERENCE IN ELEVATION OF THE FACE INVERT AND THE THROAT INVERT

WHEN SIDE-TAPERED CULVERT COLUMN (ABOVE) CONTAINS 0.0 0.0 0.0

1. THE THROAT DESIGN EXCEEDED THE DESIGN CRITERIA
- OR 2. IMPROVED INLETS FOR MORE THAN 2 BARRELS NOT AVAILABLE

CIRCULAR PIPE SECTION

CIRCULAR PIPE SECTION

PAGE= 1 NO. BARRELS= 1 DIAMETER = 4.00 FT Q(50)= 150.0 CFS AHWEL= 100.0 FT STREET SLOPE = 0.0300  
 OUTLET INVERT ELEV. = 75.4 FT

CONVENTIONAL INLET DESIGN FOR CULVERT CODE: 11133

OUTLET COMPUTATIONS

KE = 0.5

MIN FALL CURVE

MAX Q CURVE

MAX Q = 170.0 CFS

MIN HW CURVE

Q	HWF	CULVERT LENGTH =	FALL AT FACE =	ELEV FACE INVERT=	CULVERT SLOPE =	VEL AT DESIGN Q =	MIN CREST LENGTH=
120.0	98.1	352.0 FT	1.01 FT	91.9 FT	0.0463	15.4 FPS	3.1 FT
150.0	100.0						
180.0	102.4						
210.0	105.3						
240.0	108.6						
270.0	112.3						
300.0	116.5						

Q	HWF	CULVERT LENGTH =	FALL AT FACE =	ELEV FACE INVERT=	CULVERT SLOPE =	VEL AT DESIGN Q =	MIN CREST LENGTH=
120.0	95.5	355.1 FT	2.57 FT	93.4 FT	0.0420	14.6 FPS	3.8 FT
150.0	98.5						
180.0	100.9						
210.0	103.7						
240.0	107.0						
270.0	110.8						
300.0	115.0						

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BEVELED INLET DESIGN FOR CULVERT CODE: 11146

OUTLET COMPUTATIONS

KE = 0.2

MIN FALL CURVE

MAX Q CURVE

MAX Q = 174.0 CFS

MIN HW CURVE

Q	HWF	CULVERT LENGTH =	FALL AT FACE =	ELEV FACE INVERT=	CULVERT SLOPE =	VEL AT DESIGN Q =	MIN CREST LENGTH=
120.0	98.1	351.1 FT	0.57 FT	92.4 FT	0.0482	15.6 FPS	3.0 FT
150.0	100.0						
180.0	102.4						
210.0	105.3						
240.0	108.6						
270.0	112.3						
300.0	116.5						

Q	HWF	CULVERT LENGTH =	FALL AT FACE =	ELEV FACE INVERT=	CULVERT SLOPE =	VEL AT DESIGN Q =	MIN CREST LENGTH=
120.0	95.5	354.6 FT	2.28 FT	90.7 FT	0.0429	14.7 FPS	3.8 FT
150.0	98.5						
180.0	100.9						
210.0	103.7						
240.0	107.0						
270.0	110.8						
300.0	115.0						

CIRCULAR PIPE SECTION

Q	H&F	Q	H&F	Q	H&F
120.0	86.8	120.0	93.2	120.0	96.5
150.0	94.4	150.0	100.0	150.0	98.3
180.0	101.1	180.0	102.2	180.0	102.5
210.0	104.0	210.0	104.6	210.0	102.9
240.0	118.1	240.0	107.4	240.0	105.7
270.0	128.4	270.0	110.9	270.0	109.2
300.0	139.9	300.0	115.9	300.0	114.2

SIDE TAPERED INLET DESIGN  
 \*\*\*\*\*  
 FACE EDGE BEVELS = 45 DEG      SIDE TAPER = 5.697:1

MIN FALL DESIGN      MAX Q DESIGN

E = D = 4.00 FT      MAX Q = 174. CFS

FACE WIDTH = 1.57 = 6.00 FT  
 L1 = 1.41670 = 5.67 FT

Q	H&F	Q	H&F	Q	H&F
120.0	86.8	120.0	93.2	120.0	96.5
150.0	94.4	150.0	100.0	150.0	98.3
180.0	101.1	180.0	102.2	180.0	102.5
210.0	104.0	210.0	104.6	210.0	102.9
240.0	118.1	240.0	107.4	240.0	105.7
270.0	128.4	270.0	110.9	270.0	109.2
300.0	139.9	300.0	115.9	300.0	114.2

Q	H&F	Q	H&F	Q	H&F
120.0	86.8	120.0	93.2	120.0	96.5
150.0	94.4	150.0	100.0	150.0	98.3
180.0	101.1	180.0	102.2	180.0	102.5
210.0	104.0	210.0	104.6	210.0	102.9
240.0	118.1	240.0	107.4	240.0	105.7
270.0	128.4	270.0	110.9	270.0	109.2
300.0	139.9	300.0	115.9	300.0	114.2

Q	H&F	Q	H&F	Q	H&F
120.0	86.8	120.0	93.2	120.0	96.5
150.0	94.4	150.0	100.0	150.0	98.3
180.0	101.1	180.0	102.2	180.0	102.5
210.0	104.0	210.0	104.6	210.0	102.9
240.0	118.1	240.0	107.4	240.0	105.7
270.0	128.4	270.0	110.9	270.0	109.2
300.0	139.9	300.0	115.9	300.0	114.2

CULVERT LENGTH = 350.5 FT  
 FALL = 0.52 FT  
 ELEV THROAT INVERT = 92.4 FT  
 ELEV FACE INVERT = 92.7 FT  
 CULVERT SLOPE = 0.0492  
 VEL AT MAX Q = 16.1 FPS  
 MIN CREST LENGTH = 3.4 FT  
 BEVELS = 45 DEGREE  
 B = 3.0 IN D = 2.0 IN



DESIGN DATA - Page 1 (cont'd)

SLOPE TAPERED INLET DESIGN - VERTICAL FACE  
\*\*\*\*\*

DISTANCE EMBANKMENT-TO FACE = 8.13 FT      CULVERT OUTLET TO EMBANKMENT-TOE = 8.73 FT

MIN FULL DESIGN      MAX Q DESIGN

TRANSITION SECTION = 3/2  
INLET DESIGNED AS BOX TYPE INLET

NO SLOPE TAPERED INLET - VERTICAL FACE - DESIGN APPLICABLE

DESIGN DATA - Page 2

PAGE= 2 NO. BARRELS= 1 DIAMETER = 4.50 FT Q150)= 150.0 CFS H/WEL= 100.0 FT STREAM SLOPE = 0.0350  
 OUTLET INVERT ELEV. = 75.5 FT

CONVENTIONAL INLET DESIGN FOR CULVERT CODE: 11133

OUTLET COMPUTATIONS

INLET COMPUTATIONS

Q	HWO	HWF	MIN FALL CURVE	MAX Q CURVE	MIN HW CURVE
AE = 0.5					
				MAX Q = 230.0 CFS	
120.0	84.9	99.0	CULVERT LENGTH = 348.0 FT	CULVERT LENGTH = 355.7 FT	CULVERT LENGTH = 351.5 FT
150.0	98.2	99.3	FALL AT FACE = 0.0 FT	FALL AT FACE = 3.86 FT	FALL AT FACE = 8.75 FT
180.0	92.1	100.8	ELEV FACE INVERT = 92.9 FT	ELEV FACE INVERT = 89.0 FT	ELEV FACE INVERT = 86.1 FT
210.0	98.6	102.5	CULVERT SLOPE = 0.0500	CULVERT SLOPE = 0.0361	CULVERT SLOPE = 0.0395
240.0	101.8	104.6	VEL AT DESIGN Q = 16.2 FPS	VEL AT MAX Q = 15.0 FPS	VEL AT DESIGN Q = 13.2 FPS
270.0	107.7	108.9	MIN CREST LENGTH = 0.0 FT	MIN CREST LENGTH = 5.5 FT	MIN CREST LENGTH = 5.4 FT
300.0	114.2	109.5			

CIRCULAR PIPE SECTION

Q	HWO	HWF	MIN FALL CURVE	MAX Q CURVE	MIN HW CURVE
120.0	84.9	94.2	CULVERT LENGTH = 120.0	CULVERT LENGTH = 120.0	CULVERT LENGTH = 120.0
150.0	98.2	95.0	FALL AT FACE = 150.0	FALL AT FACE = 150.0	FALL AT FACE = 150.0
180.0	92.1	95.9	ELEV FACE INVERT = 180.0	ELEV FACE INVERT = 180.0	ELEV FACE INVERT = 180.0
210.0	98.6	96.7	CULVERT SLOPE = 210.0	CULVERT SLOPE = 210.0	CULVERT SLOPE = 210.0
240.0	101.8	100.7	VEL AT DESIGN Q = 240.0	VEL AT MAX Q = 240.0	VEL AT DESIGN Q = 240.0
270.0	107.7	103.1	MIN CREST LENGTH = 270.0	MIN CREST LENGTH = 270.0	MIN CREST LENGTH = 270.0
300.0	114.2	105.7			

BEVELED INLET DESIGN FOR CULVERT CODE: 11146

OUTLET COMPUTATIONS

INLET COMPUTATIONS

Q	HWO	HWF	MIN FALL CURVE	MAX Q CURVE	MIN HW CURVE
KE = 0.2					
				MAX Q = 236. CFS	
120.0	84.9	99.0	CULVERT LENGTH = 349.0 FT	CULVERT LENGTH = 355.1 FT	CULVERT LENGTH = 361.5 FT
150.0	98.2	99.3	FALL AT FACE = 0.0 FT	FALL AT FACE = 3.56 FT	FALL AT FACE = 8.75 FT
180.0	92.1	100.8	ELEV FACE INVERT = 92.9 FT	ELEV FACE INVERT = 89.3 FT	ELEV FACE INVERT = 86.1 FT
210.0	98.6	102.5	CULVERT SLOPE = 0.0500	CULVERT SLOPE = 0.0390	CULVERT SLOPE = 0.0395
240.0	101.8	104.6	VEL AT DESIGN Q = 16.2 FPS	VEL AT MAX Q = 15.1 FPS	VEL AT DESIGN Q = 13.2 FPS
270.0	107.7	108.9	MIN CREST LENGTH = 0.0 FT	MIN CREST LENGTH = 5.5 FT	MIN CREST LENGTH = 6.0 FT
300.0	114.2	109.5			

DESIGN DATA - Page 2 (cont'd)

Q	HWT	HWF	Q	HWF	Q	HWF
120.0	94.6	97.8	120.0	94.3	120.0	91.1
150.0	97.7	99.0	150.0	95.4	150.0	92.2
180.0	91.5	100.3	180.0	96.8	180.0	93.3
210.0	95.8	102.0	210.0	98.4	210.0	95.3
240.0	100.5	103.8	240.0	100.3	240.0	97.1
270.0	103.3	105.6	270.0	102.3	270.0	99.1
300.0	112.6	108.0	300.0	104.5	300.0	101.3

SIDE TAPERED INLET DESIGN

FACE EDGE BEVELS = 45 DEG SIDE TAPER = 5.667:1

MIN FALL DESIGN

B = D = 4.50 FT  
 FACE WIDTH = 1.5D = 6.75 FT  
 S = 1.4187D = 6.36 FT

MAX Q DESIGN

MAX Q = 236. CFS

MIN HW DESIGN

CULVERT LENGTH = 350.0 FT  
 FALL THREAT INVERT = 92.8 FT  
 ELEV FACE INVERT = 92.8 FT  
 CULVERT SLOPE = 0.0500  
 VEL AT DESIGN Q = 16.2 FPS  
 MIN CREST LENGTH = 0.0 FT  
 BEVELS = 45 DEGREE  
 B = 3.4 IN D = 2.3 IN

CULVERT LENGTH = 350.0 FT  
 FALL THREAT INVERT = 91.7 FT  
 ELEV FACE INVERT = 91.7 FT  
 CULVERT SLOPE = 0.0481  
 VEL AT MAX Q = 17.6 FPS  
 MIN CREST LENGTH = 4.3 FT  
 BEVELS = 45 DEGREE  
 B = 3.4 IN D = 2.3 IN

CULVERT LENGTH = 350.0 FT  
 FALL THREAT INVERT = 86.1 FT  
 ELEV FACE INVERT = 86.1 FT  
 CULVERT SLOPE = 0.0300  
 VEL AT DESIGN Q = 13.3 FT  
 MIN CREST LENGTH = 7.3 FT  
 BEVELS = 45 DEGREE  
 B = 3.4 IN D = 2.3 IN

Q	HWT	HWF
120.0	97.6	97.1
150.0	98.4	97.8
180.0	99.3	98.6
210.0	100.3	99.5
240.0	101.4	100.4
270.0	102.7	101.5
300.0	104.0	102.5

Q	HWT	HWF
120.0	96.4	95.9
150.0	97.2	96.6
180.0	98.1	97.4
210.0	99.1	98.3
240.0	100.2	99.2
270.0	101.5	100.2
300.0	102.8	101.3

Q	HWT	HWF
120.0	91.2	90.5
150.0	92.0	91.3
180.0	92.9	92.1
210.0	93.9	92.9
240.0	95.0	93.9
270.0	96.2	94.9
300.0	97.6	96.0

CIRCULAR PIPE SECTION

DESIGN DATA - Page 2 (cont'd)

SLOPE TAPERED INLET DESIGN - VERTICAL FACE  
\*\*\*\*\*

DISTANCE EMBANKMENT-TOE TO FACE = 9.15 FT

MIN FALL DESIGN

TRANSITION SECTION= 3/2  
INLET DESIGNED AS BOX TYPE INLET

CULVERT OUTLET TO EMBANKMENT-TOE = 9.82 FT

MAX Q DESIGN

CULVERT LENGTH = 347.03 FT  
 FALL = 1.43 FT  
 ELEV THROAT INVERT = 91.36 FT  
 ELEV FACE INVERT = 92.84 FT  
 CULVERT SLOPE = 0.0459  
 VELOCITY = 17.05 FPS  
 FACE WIDTH = 6.107 FT  
 L1 = 5.938 FT  
 L2 = 3.74 FT  
 L3 = 2.25 FT  
 SF = 2.00  
 TAPER = 5.426:1

Q	HWT	HWF
120.0	96.4	96.2
150.0	97.2	96.3
180.0	93.1	97.3
210.0	99.1	97.9
240.0	100.2	98.4
270.0	101.5	99.1
300.0	102.8	99.7

Q	HWT	HWF
120.0	96.4	96.2
150.0	97.2	96.3
180.0	93.1	97.3
210.0	99.1	97.9
240.0	100.2	98.4
270.0	101.5	99.1
300.0	102.8	99.7

## CIRCULAR PIPE SECTION

### EXAMPLE PROBLEM NO. 2B - Reinforced Concrete Pipe

The input data for problem 2B is the same as problem 2A. The INDEX SHEET shows an output design for the 4.0, 4.5, and 5.0 foot diameter concrete pipes.



CIRCULAR PIPE SECTION

INDEX SHEET

>>>> PIPE CULVERT DESIGN FOR PROJECT >>> SAMPLE R C PIPE AHW=100.

>>>> THE PROGRAM PROVIDES A RANGE OF CONVENTIONAL PIPE CULVERT SIZES WITH AND WITHOUT BEVELS WHICH SATISFY SITE REQUIREMENTS

WHERE: BEVELED EDGES FOR CMP AND CONCRETE PIPES  
ARE BASED ON CHART 13 IN HEC-13

>>>> IF INLET CONTROL CONDITIONS - IMPROVED INLET DESIGNS ARE PROVIDED FOR SIDE-TAPERED INLETS  
AND SLOPE-TAPERED INLETS

\*\*\*\*\*  
\*\*\*\*\* DESIGN INPUT DATA \*\*\*\*\*  
\*\*\*\*\* DESIGN INPUT DATA \*\*\*\*\*  
\*\*\*\*\*

CONVENTIONAL CULVERT ----- CONCRETE PIPE - SQUARE-EDGE HEADWALL KE= 0.5  
BEVELED-EDGED CULVERT ----- CONCRETE PIPE WITH BEVEL(A) KE= 0.2

CULVERT CODE	APPROX STREAM SLOPE	DESIGN DISCHARGE	DESIGN TAILWATER	ALLOWABLE HEADWATER ELEVATION	STREAM BED ELEVATION AT INLET	STREAM BED ELEVATION AT OUTLET	LEFT ROADWAY EMBANKMENT SLOPE	RIGHT ROADWAY EMBANKMENT SLOPE
23434	0.0500	150.0	2.0	100.0	93.3	75.0	2.0:1	2.0:1

CULVERT SIZES  
DIAMETER FROM 4.00 FT TO 5.00 FT  
SLOPE-TAPER  
FALL SLOPE  
2.0:1  
COMPUTED STREAM  
SLOPE = 0.0500

\*\*\*\*\*  
\*\*\*\*\* INDEX SHEET FOR PIPE CULVERTS \*\*\*\*\*  
\*\*\*\*\* INDEX SHEET FOR PIPE CULVERTS \*\*\*\*\*  
\*\*\*\*\*

* SEE * * PAGE * * * * * * *	* NUMBER * * OF * * BARRELS * * * * *	* -- INLET CONTROL -- *				* -- OUTLET CONTROL -- *				* -- INFLOW CONTROL -- *																		
		* HW * * ELEV * * (FT) *	* KE=0.5 *	* KE=0.2 *	* OUTLET * * INVERT * * ELEV * * (FT) *	* HW * * ELEV * * (FT) *	* KE=0.5 *	* KE=0.2 *	* CONVENTIONAL CULVERT * * FALL * * (FT) *	* INVERT * * ELEV * * (FT) *	* HW * * ELEV * * (FT) *	* KE=0.5 *	* KE=0.2 *	* BEVEL-EDGED CULVERT * * FALL * * (FT) *	* INVERT * * ELEV * * (FT) *	* HW * * ELEV * * (FT) *	* KE=0.5 *	* KE=0.2 *	* SIDE-TAPERED CULVERT * * FALL * * (FT) *	* INVERT * * ELEV * * (FT) *	* HW * * ELEV * * (FT) *	* KE=0.5 *	* KE=0.2 *					
* 1 *	* 1 *	* 85.8 *	* 85.2 *	* 75.4 **	* 100.0 **	* 1.1 *	* 91.8 *	* 100.0 *	* 0.6 *	* 92.4 *	* 99.0 *	* 0.3 *	* 92.7 *	* 92.6 *	* 97.6 *	* 0.4 *	* 92.9 *	* 98.2 *	* 0.3 *	* 92.9 *	* 98.2 *	* 0.3 *	* 92.9 *	* 98.2 *	* 0.3 *	* 92.9 *	* 98.2 *	* 0.3 *
* 2 *	* 1 *	* 63.3 *	* 82.9 *	* 75.5 **	* 99.3 **	* 0.0 *	* 92.9 *	* 99.0 *	* 0.0 *	* 92.9 *	* 99.0 *	* 0.0 *	* 92.9 *	* 98.2 *	* 97.6 *	* 0.4 *	* 92.9 *	* 98.2 *	* 0.0 *	* 92.9 *	* 98.2 *	* 0.0 *	* 92.9 *	* 98.2 *	* 0.0 *	* 92.9 *	* 98.2 *	* 0.0 *
* 3 *	* 1 *	* 82.2 *	* 81.9 *	* 75.5 **	* 99.4 **	* 0.0 *	* 92.8 *	* 98.2 *	* 0.0 *	* 92.8 *	* 98.2 *	* 0.0 *	* 92.8 *	* 97.6 *	* 97.6 *	* 0.4 *	* 92.8 *	* 98.2 *	* 0.0 *	* 92.8 *	* 98.2 *	* 0.0 *	* 92.8 *	* 98.2 *	* 0.0 *	* 92.8 *	* 98.2 *	* 0.0 *

CONCRETE PIPES

INDEX SHEET (cont)

BY DEFINITION OF FALL, WHEN A SIDE-TAPERED INLET LIES ON THE STREAM SLOPE,  
THE FALL IS THE DIFFERENCE IN ELEVATION OF THE FACE INVERT AND THE THROAT INVERT

WHEN SIDE-TAPERED CULVERT COLUMN (ABOVE) CONTAINS 0.0 0.0 0.0

1. THE THROAT DESIGN EXCEEDED THE DESIGN CRITERIA

OR 2. IMPROVED INLETS FOR MORE THAN 2 BARRELS NOT AVAILABLE



CIRCULAR PIPE SECTION

DESIGN DATA FOR PAGE 1

PAGE= 1 NO. BARRELS= 1 DIAMETER = 4.00 FT Q(50)= 150.0 CFS AH\*EL= 100.0 FT STREAM SLOPE = 0.0500  
 OUTLET INVERT ELEV. = 75.4 FT

CONVENTIONAL INLET DESIGN FOR CULVERT CODE: 23434

OUTLET COMPUTATIONS

INLET COMPUTATIONS

KE = 0.5

MIN FALL CURVE

MAX Q CURVE

MIN HW CURVE

MAX Q = 204.0 CFS

CULVERT LENGTH = 352.3 FT  
 FALL AT FACE = 1.14 FT  
 ELEV FACE INVERT = 91.8 FT  
 CULVERT SLOPE = 0.0464  
 VEL AT DESIGN Q = 26.0 FPS  
 MIN CREST LENGTH = 3.1 FT

CULVERT LENGTH = 352.0 FT  
 FALL AT FACE = 5.00 FT  
 ELEV FACE INVERT = 86.9 FT  
 CULVERT SLOPE = 0.0318  
 VEL AT MAX Q = 24.1 FPS  
 MIN CREST LENGTH = 5.6 FT

CULVERT LENGTH = 352.0 FT  
 FALL AT FACE = 5.00 FT  
 ELEV FACE INVERT = 86.9 FT  
 CULVERT SLOPE = 0.0318  
 VEL AT DESIGN Q = 22.5 FPS  
 MIN CREST LENGTH = 4.2 FT

89

Q	HWO	Q	HWF
120.0	83.3	120.0	98.0
150.0	85.8	150.0	100.0
180.0	88.8	180.0	102.5
210.0	92.2	210.0	105.5
240.0	96.7	240.0	108.9
270.0	100.7	270.0	112.8
300.0	105.7	300.0	117.5

Q	HWF
120.0	93.2
150.0	95.2
180.0	97.7
210.0	100.7
240.0	104.0
270.0	107.9
300.0	112.7

Q	HWF
120.0	33.2
150.0	95.2
180.0	97.7
210.0	100.7
240.0	104.0
270.0	107.9
300.0	112.7

BEVELED INLET DESIGN FOR CULVERT CODE: 23446

OUTLET COMPUTATIONS

INLET COMPUTATIONS

KE = 0.2

MIN FALL CURVE

MAX Q CURVE

MIN HW CURVE

MAX Q = 219.0 CFS

CULVERT LENGTH = 351.1 FT  
 FALL AT FACE = 0.57 FT  
 ELEV FACE INVERT = 92.4 FT  
 CULVERT SLOPE = 0.0482  
 VEL AT DESIGN Q = 26.3 FPS  
 MIN CREST LENGTH = 3.0 FT

CULVERT LENGTH = 362.0 FT  
 FALL AT FACE = 6.00 FT  
 ELEV FACE INVERT = 86.9 FT  
 CULVERT SLOPE = 0.0318  
 VEL AT MAX Q = 24.5 FPS  
 MIN CREST LENGTH = 6.0 FT

CULVERT LENGTH = 362.0 FT  
 FALL AT FACE = 6.00 FT  
 ELEV FACE INVERT = 86.9 FT  
 CULVERT SLOPE = 0.0318  
 VEL AT DESIGN Q = 22.5 FPS  
 MIN CREST LENGTH = 4.2 FT

CIRCULAR PIPE SECTION

DESIGN DATA FOR PAGE 1 (cont)

Q	HWO	HWF	Q	HWF	Q	HWF
120.0	82.9	98.2	120.0	92.3	120.0	92.3
150.0	85.2	100.0	150.0	94.5	150.0	94.5
180.0	87.8	102.2	180.0	96.8	180.0	96.8
210.0	90.9	104.6	210.0	99.2	210.0	99.2
240.0	94.5	107.4	240.0	102.0	240.0	102.0
270.0	98.5	110.9	270.0	105.5	270.0	105.5
300.0	103.0	115.9	300.0	110.5	300.0	110.5

SIDE TAPERED INLET DESIGN  
\*\*\*\*\*

FACE EDGE BEVELS = 45 DEG      SIDE TAPER= 5.667:1

MIN FALL DESIGN

E = D = 4.00 FT  
FACE WIDTH= 1.5D= 6.00 FT  
L1= 1.4167D= 5.67 FT

90

MAX Q DESIGN

MAX Q = 276. CFS

MIN HW DESIGN

CULVERT LENGTH = 350.0 FT  
FALL = 0.28 FT  
ELEV THROAT INVERT = 92.7 FT  
ELEV FACE INVERT = 92.9 FT  
CULVERT SLOPE = 0.0500  
VEL AT DESIGN Q = 26.7 FPS  
MIN CREST LENGTH = 0.0 FT  
BEVELS = 45 DEGREE  
B = 3.0 IN D = 2.0 IN

CULVERT LENGTH = 361.4 FT  
FALL = 6.00 FT  
ELEV THROAT INVERT = 86.9 FT  
ELEV FACE INVERT = 87.1 FT  
CULVERT SLOPE = 0.0323  
VEL AT MAX Q = 30.7 FPS  
MIN CREST LENGTH = 7.6 FT  
BEVELS = 45 DEGREE  
B = 3.0 IN D = 2.0 IN

CULVERT LENGTH = 361.4 FT  
FALL = 6.00 FT  
ELEV THROAT INVERT = 86.9 FT  
ELEV FACE INVERT = 87.1 FT  
CULVERT SLOPE = 0.0323  
VEL AT DESIGN Q = 22.6 FT  
MIN CREST LENGTH = 5.6 FT  
BEVELS = 45 DEGREE  
B = 3.0 IN D = 2.0 IN

Q	HWT	HWF
120.0	97.9	97.6
150.0	99.0	98.6
180.0	100.3	99.7
210.0	101.7	100.9
240.0	103.4	102.3
270.0	105.2	103.8
300.0	107.3	105.5

Q	HWT	HWF
120.0	92.2	91.8
150.0	93.3	92.8
180.0	94.6	93.9
210.0	96.0	95.1
240.0	97.7	96.5
270.0	99.5	98.0
300.0	101.6	99.7

Q	HWT	HWF
120.0	92.2	91.8
150.0	93.3	92.8
180.0	94.6	93.9
210.0	96.0	95.1
240.0	97.7	96.5
270.0	99.5	98.0
300.0	101.6	99.7

CIRCULAR PIPE SECTION

DESIGN DATA FOR PAGE 1 (cont)

SLOPE TAPERED INLET DESIGN - VERTICAL FACE  
 \*\*\*\*\*

DISTANCE EMBANKMENT-TOE TO FACE = 8.13 FT

CULVERT OUTLET TO EMBANKMENT-TOE = 8.73 FT

MIN FALL DESIGN

MAX Q DESIGN

TRANSITION SECTION= D/2  
 INLET DESIGNED AS BOX TYPE INLET

CULVERT LENGTH = 349.13 FT  
 FALL = 5.96 FT  
 ELEV THROAT INVERT = 86.94 FT  
 ELEV FACE INVERT = 92.89 FT  
 CULVERT SLOPE = 0.0346  
 VELOCITY = 26.20 FPS  
 FACE WIDTH = 7.517 FT  
 L1 = 15.117 FT  
 L2 = 13.12 FT  
 L3 = 2.00 FT  
 SF = 2.00  
 TAPER = 8.358:1

Q	HWT	HWF	Q	HWT	HWF
120.0	92.2	96.0	120.0	92.2	96.0
150.0	93.3	96.5	150.0	93.3	96.5
180.0	94.6	97.0	180.0	94.6	97.0
210.0	96.0	97.5	210.0	96.0	97.5
240.0	97.7	98.1	240.0	97.7	98.1
270.0	99.5	98.7	270.0	99.5	98.7
300.0	101.6	99.4	300.0	101.6	99.4

CIRCULAR PIPE SECTION

DESIGN DATA FOR PAGE 2

PAGE= 2 NO. BARRELS= 1 DIAMETER = 4.50 FT O(50)= 150.0 CFS ANWEL= 100.0 FT STREAM SLOPE = 0.0500  
 OUTLET INVERT ELEV. = 75.5 FT

CONVENTIONAL INLET DESIGN FOR CULVERT CODE: 23434

\*\*\*\*\*  
 OUTLET COMPUTATIONS  
 \*\*\*\*\*

\*\*\*\*\*  
 INLET COMPUTATIONS  
 \*\*\*\*\*

KE = 0.5

MIN FALL CURVE

MAX Q CURVE

MIN HW CURVE

MAX Q = 264.0 CFS

CULVERT LENGTH = 348.0 FT  
 FALL AT FACE = 0.0 FT  
 ELEV FACE INVERT = 92.9 FT  
 CULVERT SLOPE = 0.0500  
 VEL AT DESIGN Q = 26.5 FPS  
 MIN CREST LENGTH = 0.0 FT

CULVERT LENGTH = 361.5 FT  
 FALL AT FACE = 6.75 FT  
 ELEV FACE INVERT = 86.1 FT  
 CULVERT SLOPE = 0.0295  
 VEL AT MAX Q = 25.0 FPS  
 MIN CREST LENGTH = 7.6 FT

CULVERT LENGTH = 361.5 FT  
 FALL AT FACE = 6.75 FT  
 ELEV FACE INVERT = 86.1 FT  
 CULVERT SLOPE = 0.0295  
 VEL AT DESIGN Q = 21.9 FPS  
 MIN CREST LENGTH = 5.3 FT

H<sub>2</sub>O

Q

Q

HWF

Q

HWF

92

120.0 81.8  
 150.0 83.3  
 180.0 85.2  
 210.0 87.2  
 240.0 89.6  
 270.0 92.2  
 300.0 95.1

120.0 93.1  
 150.0 99.3  
 180.0 100.8  
 210.0 102.7  
 240.0 104.8  
 270.0 107.3  
 300.0 109.9

120.0  
 150.0  
 180.0  
 210.0  
 240.0  
 270.0  
 300.0

91.4  
 92.6  
 94.1  
 96.0  
 98.1  
 100.5  
 103.2

120.0  
 150.0  
 180.0  
 210.0  
 240.0  
 270.0  
 300.0

91.4  
 92.6  
 94.1  
 96.0  
 98.1  
 100.5  
 103.2

BEVELED INLET DESIGN FOR CULVERT CODE: 23446

\*\*\*\*\*  
 OUTLET COMPUTATIONS  
 \*\*\*\*\*

\*\*\*\*\*  
 INLET COMPUTATIONS  
 \*\*\*\*\*

KE = 0.2

MIN FALL CURVE

MAX Q CURVE

MIN HW CURVE

MAX Q = 282.0 CFS

CULVERT LENGTH = 348.0 FT  
 FALL AT FACE = 0.0 FT  
 ELEV FACE INVERT = 92.9 FT  
 CULVERT SLOPE = 0.0500  
 VEL AT DESIGN Q = 26.5 FPS  
 MIN CREST LENGTH = 0.0 FT

CULVERT LENGTH = 361.5 FT  
 FALL AT FACE = 6.75 FT  
 ELEV FACE INVERT = 86.1 FT  
 CULVERT SLOPE = 0.0295  
 VEL AT MAX Q = 25.4 FPS  
 MIN CREST LENGTH = 8.2 FT

CULVERT LENGTH = 361.5 FT  
 FALL AT FACE = 6.75 FT  
 ELEV FACE INVERT = 86.1 FT  
 CULVERT SLOPE = 0.0295  
 VEL AT DESIGN Q = 21.9 FPS  
 MIN CREST LENGTH = 6.0 FT

CIRCULAR PIPE SECTION

DESIGN DATA FOR PAGE 2 (cont.)

Q	HWF	Q	HWF	Q	HWF	Q	HWF
120.0	81.5	120.0	97.8	120.0	91.1	120.0	91.1
150.0	82.9	150.0	99.0	150.0	92.2	150.0	92.2
180.0	84.6	180.0	100.3	180.0	93.6	180.0	93.6
210.0	86.4	210.0	102.0	210.0	95.3	210.0	95.3
240.0	88.5	240.0	103.8	240.0	97.1	240.0	97.1
270.0	90.9	270.0	105.8	270.0	99.1	270.0	99.1
300.0	93.5	300.0	108.0	300.0	101.3	300.0	101.3

SIDE TAPERED INLET DESIGN  
 \*\*\*\*\*

FACE EDGE BEVELS = 45 DEG SIDE TAPER= 5.667:1

MIN FALL DESIGN

E = D = 4.50 FT  
 FACE WIDTH= 1.50= 6.75 FT  
 L1= 1.4:67D= 6.38 FT

MAX Q DESIGN

MAX Q = 356. CFS

MIN HW DESIGN

93

CULVERT LENGTH = 348.0 FT  
 FALL THROAT INVERT = 0.32 FT  
 ELEV THROAT INVERT = 92.6 FT  
 ELEV FACE INVERT = 92.9 FT  
 CULVERT SLOPE = 0.0500  
 VEL AT DESIGN Q = 26.5 FPS  
 MIN CREST LENGTH = 0.0 FT  
 BEVELS = 45 DEGREE  
 B = 3.4 IN D = 2.3 IN

CULVERT LENGTH = 360.9 FT  
 FALL THROAT INVERT = 6.75 FT  
 ELEV THROAT INVERT = 86.1 FT  
 ELEV FACE INVERT = 86.3 FT  
 CULVERT SLOPE = 0.0300  
 VEL AT MAX Q = 32.9 FPS  
 MIN CREST LENGTH = 10.3 FT  
 BEVELS = 45 DEGREE  
 B = 3.4 IN D = 2.3 IN

CULVERT LENGTH = 360.9 FT  
 FALL THROAT INVERT = 6.75 FT  
 ELEV THROAT INVERT = 86.1 FT  
 ELEV FACE INVERT = 86.3 FT  
 CULVERT SLOPE = 0.0300  
 VEL AT DESIGN Q = 22.0 FT  
 MIN CREST LENGTH = 8.2 FT  
 BEVELS = 45 DEGREE  
 B = 3.4 IN D = 2.3 IN

Q	HWT	HWF
120.0	97.3	97.1
150.0	98.2	97.8
180.0	99.1	98.6
210.0	100.0	99.5
240.0	101.1	100.4
270.0	102.3	101.5
300.0	103.6	102.5

Q	HWT	HWF
120.0	90.9	90.5
150.0	91.7	91.3
180.0	92.6	92.1
210.0	93.6	92.9
240.0	94.7	93.9
270.0	95.8	94.9
300.0	97.1	96.0

Q	HWT	HWF
120.0	90.9	90.5
150.0	91.7	91.3
180.0	92.6	92.1
210.0	93.6	92.9
240.0	94.7	93.9
270.0	95.8	94.9
300.0	97.1	96.0

CIRCULAR PIPE SECTION

DESIGN DATA FOR PAGE 2 (cont)

SLOPE TAPERED INLET DESIGN - VERTICAL FACE  
 \*\*\*\*\*

DISTANCE EMBANKMENT-TOE TO FACE = 9.15 FT

CULVERT OUTLET TO EMBANKMENT-TOE = 9.82 FT

MIN FALL DESIGN

MAX Q DESIGN

TRANSITION SECTION= 0/2  
 INLET DESIGNED AS BOX TYPE INLET

CULVERT LENGTH = 347.03 FT  
 FALL = 5.70 FT  
 ELEV THROAT INVERT = 86.14 FT  
 ELEV FACE INVERT = 92.94 FT  
 CULVERT SLOPE = 0.0325  
 VELOCITY = 27.36 FPS  
 FACE WIDTH = 10.624 FT  
 L1 = 16.709 FT  
 L2 = 14.46 FT  
 L3 = 2.25 FT  
 SF = 2.00  
 TAPER = 5.457:1

Q	HWT	HWF	Q	HWT	HWF
120.0	90.9	95.4	120.0	90.9	95.4
150.0	91.7	95.7	150.0	91.7	95.7
180.0	92.6	96.1	180.0	92.6	96.1
210.0	93.6	96.5	210.0	93.6	96.5
240.0	94.7	96.8	240.0	94.7	96.8
270.0	95.8	97.1	270.0	95.8	97.1
300.0	97.1	97.5	300.0	97.1	97.5

PROGRAM IMPLEMENTATION

## JOB CONTROL LANGUAGE

The following job control language for this program is for a typical batch mode processing on an IBM 360/65 computer. More efficient processing can be realized by storing the program in a load mode status on a direct access system.

```
// JOB
// EXEC          FORTGCLG,PARM.FORT=BCD
// FORT.SYSLIN   SPACE=(80,(2000,100),RLSE)
// FORT.SYSIN    DD *
```

```
*
*
```

### SOURCE DECK

```
*
*
```

```
// LKED.SYSLMOD  DD SPACE=(1024,(80,10,1),RLSE)
// LKED.SYSUT1   DD SPACE=(1024,(200,10),RLSE)
// LKED.SYSUDUMP DD SYSOUT=A
// GO.FT09F001  DD SYSOUT=A,DCB=(RECFM=UA,BLKSIZE=133)
// GO.SYSIN      DD *
```

```
Problem No. 1      DATA CARD 1   Header card
                   DATA CARD 2   Hydraulic site data
                   DATA CARD 3   Range of culvert sizes
                   DATA CARD 4   Blank card
```

```
/*
```

## COMPUTER REQUIREMENTS

The computer process described herein is written in FORTRAN IV and was developed on an IBM 360/65 computer with OS operating system. The program is essentially written in EBCDIC but several of the routines contain BCD features which should not pose any problems. This version of the program utilizes about 110K-bytes of storage and the source card deck contains about 3600 cards (1800 for box culvert program and 1800 for circular pipe culvert program).



A P P E N D I X

## REFERENCES

1. "Hydraulic Charts for the Selection of Highway Culverts," HEC No. 5, U.S. Department of Transportation, Federal Highway Administration, December 1965.
2. "Hydraulic Design of Improved Inlets for Culverts," HEC No. 13, U.S. Department of Transportation, Federal Highway Administration, August 1972.
3. Electronic Computer Program, "Hydraulic Analysis of Circular Culverts," U.S. Department of Transportation, Federal Highway Administration, July 1970.
4. Electronic Computer Program, "Hydraulic Analysis of Box Culverts," U.S. Department of Transportation, Federal Highway Administration, April 1969.
5. "Open Channel Hydraulics," McGraw-Hill Book Company, Inc., New York, 1959.

## DEFINITION OF TERMS

The following named variables are used in both the box culvert and circular culvert design subroutines. Subroutine names beginning with a "B" refer to box culverts and subroutines beginning with "C" refer to circular pipes.

### Main Program

Input data items described in INPUT SECTION

CIRC - Subroutine to design improved inlets for CMP and concrete pipes.

BOXES - Subroutine to design improved inlets for box culverts.

ARCH - Proposed subroutine for pipe-arch design.

### Subroutine BOXES

This subroutine initiates the culvert analysis for the range of box culvert sizes requested by the user, computes headwater for inlet and outlet control sections and the throat elevation for improved inlets. Subroutine BOXES also computes the data for Curves A, B, and C which is used by the other subroutines.

ITAB and Tab arrays contain stored information for:

IBAR	- Number of barrels
AK	- Barrel width (b)
AKK	- Barrel depth (d)
HWO(1)	- Outlet control headwater elevation for conventional culverts

HWO(2)	- Outlet control headwater elevation for bevel-edge culverts
TOEL	- Elevation at toe of culvert
HWEL(1) and HWEL(2)	- Inlet headwater elevation for square-edge and bevel-edge inlets
SUMP(1) and SUMP(2)	- Inlet FALL if required or else FALL = 0
FACE(1) and FACE(2)	- Inlet invert elevations for square- and bevel-edge inlets
HWT	- Elevation headwater at throat control section
FALL (external)	- Difference in elevation of throat and stream face elevation
TROEL	- Elevation of invert at throat
NOCA, NOCB, NOCC	- Variables indicating no designs applicable for the three design conditions mentioned in this report
HWOUT	- Headwater for outlet control
FACEL	- Elevation of face invert
ELINCA, ELINCB, ELINCC	- Inlet invert elevation for curves A, B and C
CRESA, CRESB, CRESC	- Minimum crest length necessary at inlets for three curve designs
DISL, DISR	- Distances from toe of embankments to face and outlet of culvert
VELIN	- Velocity at outlet for inlet control
VELOUT	- Velocity at outlet for outlet control
SER, SEL	- Embankment slopes, downstream and upstream respectively
SLOPA, SLOPB, SLOPC	- Culvert slopes for the three curve conditions

### Subroutine BHY3

Subroutine to design conventional and bevel-edge inlets and performance curves for design curves A, B and C.

- |                  |   |
|------------------|---|
| BAR              | - Number of barrels   |
| B, D             | - Culvert width and height  |
| DISL, DISR       | - Variables denoting distances from embankment toe to inlet face and outlet face to toe of culverts |
| DLSTA            | - Culvert length  |
| HDCA, HDCB, HDCC | - Headwater elevations for performance curves for design curves A, B, and C                         |
| HW01, HW02       | - Outlet control headwater elevations for culverts with conventional and bevel-edges, respectively  |
| SA, SB, SC       | - Culvert slopes for design curves A, B, and C  |

### Subroutine BSIDE

Subroutine to design side-tapered inlets for design curves A, B and C.

- |                 |  |
|-----------------|--|
| BAR             | - Number of barrels  |
| B, BB           | - Width of barrel, ft.   |
| BIT, BITB, BITC | - Variables denoting extensions to culvert lengths when the face section is moved toward the toe due to a fall in the culvert design |

BF, BFB, BFC	- Variables denoting face widths
ELFACA	- Elevation of face invert for curve "A"
ELTRCA	- Elevation of throat for curve "A"
ELFACB	- Elevation of face invert for curve "B"
ELTRCB	- Elevation of throat for curve "B"
ELFACC	- Elevation of face invert for curve "C"
ELTRCC	- Elevation of throat for curve "C"
FALLM	- Maximum FALL allowed for inlet
FACEL	- Elevation of face invert
HWFA, HWFB, HWFC	- Face headwater elevations for performance curves A, B and C
HWTB, HWTB, HWTC	- Throat headwater elevations for performance curves A, B and C
L1	- Length of improved inlet
NOCAS, NOCBS, NOCCS	- Variables. No curve A, B and C designs applicable
SCORR	- Slope correction factor
SLO, SA, SB, SC	- Variables for barrel slopes for curves A, B and C
STROEL	- Streambed elevation at the culvert throat
TBFALL	- Inlet FALL for curve "B"
TOEL	- Elevation of culvert outlet invert
WB	- Minimum crest length for curve "B" design

### Subroutine BSLOPV

This subroutine is called to design slope-tapered vertical face box culverts and performance curve data for the two design conditions referred to as curves A and B. The design for curve C is not included at this time.

BAR	- Number of barrels
BF	- Face width, ft.
DIST	- Culvert length from face to outflow, ft.
FACEL	- Face elevation, ft.
FALL	- Vertical distance between crest point elevation and throat elevation, ft.
HWTA	- Headwater at throat for curve A, ft.
HWTB	- Headwater at throat for curve B, ft.
HWFA	- Headwater at face for curve A, ft.
HWFB	- Headwater at face for curve B, ft.
L1, L2, L3, L4	- Variables denoting length of improved culvert entrance design
NOC	- Variable to indicate no design applicable for either curve A and/or B
QUE	- Maximum discharge for curve B design
SF	- Fall slope
S	- Variable for actual culvert barrel slopes
TROE	- Variable used to denote throat elevation for curve A and B

- Y - Vertical distance between crest point and face normal to slope
- VELIN - Inlet control velocity
- VELOUT - Outlet control velocity

Subroutine BSLOPM

Subroutine to design slope-tapered mitered face box culverts and performance curve data for curves "A" and "B" design. Variables are essentially the same for the vertical face design.

Subroutine BOUT

Subroutine to compute outlet control headwaters

- AVEV - Average velocity for backwater calculations
- AVER - Average hydraulic radius for backwater calculations
- CKE - Entrance loss coefficient variable
- DSUBN - Normal depth, in feet
- DSUBC - Critical depth, in feet
- DTW - Design tailwater, in feet
- HEAD - Hydraulic head required for outlet control, in feet
- HO - Variable equal to tailwater or to critical depth plus D divided by 2
- WHW - Outlet control headwater, in feet
- Sl - Friction slope



- SPIH - Specific head for backwater calculations, in feet
- SUMX - Distance between two cross-sections in backwater computations, in feet
- TOEL - Elevation at outlet of culvert
- V - Velocity, fps

Subroutine BNORM

Subroutine to compute normal depth.

- AR23 - Refers to area times hydraulic radius raised to two-thirds power
- AREA - Area based on normal depth
- B & D - Culvert base width and height
- DEP - Normal depth
- WP - Wetted perimeter

Subroutine BFIT

Subroutine to find maximum discharge

- A - Variable used to increment discharge
- AREA - Cross-sectional area of culvert
- AHWEL - Allowable headwater elevation
- B - Width of box culvert, in feet
- CKE - Variable for energy loss coefficients
- CLTH - Culvert length measured on stream slope
- CN - Manning's "n" value
- D - Culvert height, in feet
- DC - Critical depth

- HD - Hydraulic head for given flow in outlet control, in feet
- HO - Variable equal to tailwater or  $\frac{D + d_c}{2}$  whichever is larger
- $Q_{max}$  - Maximum discharge measured at the intersection of outlet control curve and allowable headwater

Subroutine BEQUA

Subroutine to compute inlet control headwater.

- HWOVD - Variable referring to headwater over "D"
- I1, I5 - Variable part of input code number
- DEP - Normal depth

PROGRAM LISTING

Routines containing identification numbers beginning with "B" followed by an integer value refer to box culverts and routines containing identification numbers beginning with "C" plus the integer value refer to circular pipe culverts. Subsequent to the release of the preliminary draft of HY-6, program changes have been incorporated in this version of HY-6.

Changes to the computer program are shown on the program listing with two asterisks following the statement sequence number.



C  
C  
C  
C  
C  
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C

THIS VERSION OF THE PROGRAM WILL ANALYZE BOX CULVERTS  
AND CIRCULAR PIPES (CMP and Concrete)

BY MARIO MARQUES -- FHWA -- 1979

COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),  
TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),  
TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),  
3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),  
4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),  
5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,  
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),  
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),  
8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),  
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,  
ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2  
INTEGER SYSIN, SYSOT  
DATA IBLANK/3H /  
SYSIN=1  
SYSOT=3

C

C-----READ DESIGN DATA

10 READ(SYSIN,901)IPROJ  
IF(IPROJ(1).EQ.'BLANK') GO TO 11  
12 READ(SYSIN,903) I1,I2,I3,I4,I5,SLOPE,DIST,Q1,DTW,AHWEL,ELIN,  
1ELOUT, SEL,SER,SFACE  
50 IF(I1.EQ.1) GO TO 58  
52 IF(I1.EQ.2) GO TO 58  
54 IF(I1.EQ.3) GO TO 58  
56 IF(I1.EQ.4) GO TO 58  
WRITE (SYSOT,2130)  
2130 FORMAT( 22H CULVERT CODE INVALID)  
GO TO 10  
58 SLOPE = SLOPE + 0.000001

C

C-----ROUTINES TO DESIGN PIPES,ARCHES,OR BOXES

15 GO TO (110,110,130,140),I1  
C.....CALL TO CIRCULAR CULVERTS(NOT INCLUDED BUT AVAILABLE)  
110 CALL CIRC(DIST,SLOPE)  
GO TO 10  
C.....CALL TO ARCH PIPES( NOT AVAILABLE AT THIS TIME)  
130 CALL ARCH  
GO TO 10  
C.....CALL BOX CULVERT  
140 CALL BOXES(DIST,SLOPE)  
GO TO 10  
11 WRITE(SYSOT,910)  
STOP  
910 FORMAT(11H END OF JOB)  
901 FORMAT(2SA3)  
903 FFORMAT(SI1,F7.4,9F7.1)  
904 FORMAT(2F4.1)  
END

B 5  
B 10  
B 15  
B 20  
B 25  
B 30  
B 35  
B 40 \*\*  
B 45 \*\*  
B 50 \*\*  
B 55 \*\*  
B 60 \*\*  
B 65 \*\*  
B 70 \*\*  
B 75 \*\*  
B 80 \*\*  
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B 260  
B 265  
B 270  
B 275

C	SUBROUTINE BOXES(DIST,SLOPE)	B	280	**
C		B	285	
C	SUBROUTINE TO DEVELOP INDEX SHEET (INCLUDES OUTLET AND INLET	B	290	
C	CONTROL HEADWATER ,EXTERNAL FALL AND INVERT ELEVATIONS)	B	295	
C		B	300	
	COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),	B	305	**
	1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),	B	310	**
	2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),	B	315	**
	3TQWAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),	B	320	**
	4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),	B	325	**
	5 IPROC(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,	B	330	**
	6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),	B	335	**
	7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),	B	340	**
	8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),	B	345	**
	9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,	B	350	**
	ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2	B	355	**
	DIMENSION HWQ(2),SUMP(2),FACEHW(2),HWEL(2)	B	360	
	DIMENSION CKE(4),FACE(2),KT(7)	B	365	
	INTEGER SYSIN, SYSOT	B	370	
	DATA KT/1111,1122,1123,1134,1145,1146,1147/	B	375	
	DATA ALPHA,SCORR,CN/1.0,.5,.012/	B	380	
	DATA CKE/.4,.5,.7,.2/	B	385	
C		B	390	
C	PRINT CONVENTIONAL CULVERT DESIGN DATA	B	395	
C		B	400	
	READ(SYSIN,2)KBAS1,KBAS2,KDEP1,KDEP2	B	405	
	2 FORMAT(4I2)	B	410	
	WRITE(SYSOT,902) IPROJ	B	415	
902	FORMAT(1H1,'>>>> BOX CULVERT DESIGN FOR PROJECT >>> ',26A3,///	B	420	
	1/ '>>>> THE PROGRAM PROVIDES A RANGE OF CONVENTIONAL BOX CULVERT	B	425	
	2 SIZES WITH AND WITHOUT BEVELS WHICH SATISFY SITE REQUIREMENTS'//	B	430	
	330X,'WHERE: BEVELED EDGES INCLUDE THE FOLLOWING.'//37X,'HEADWALLS	B	435	
	4-NORMAL -CHART NO. 8 IN HEC-13'/37X,' -SKEWED CHART NO. 9	B	440	
	5 INHEC-13'/37X,'WINGWALLS -CHART NO. 10 IN HEC-13'////	B	445	
	6 '>>>> IF INLET CONTROL GOVERNS - IMPROVED INLET DESIGNS ARE PR	B	450	
	7OVIDED FOR SIDE-TAPERED INLETS ' /66X.'AND SLOPE-TAPER	B	455	
	8ED INLETS '///)	B	460	
903	WRITE(SYSOT,904)	B	465	
904	FORMAT(1X,'*****')	B	470	
	1*****')	B	475	
	2*****'/'*****' DESIGN INPUT DATA ***	B	480	
	3*****'/'*****' DESIGN INPUT DATA **	B	485	
	4*****'/'*****' DESIGN INPUT DATA *	B	490	
	5*****'/'*****' DESIGN INPUT DATA	B	495	
	6*****'/'*****' DESIGN INPUT DATA	B	500	
	7*****'/'*****' DESIGN INPUT DATA	B	505	
	8*****'///)	B	510	
	5 GO TO (10,20,30,40,50,60,70),15	B	515	
	10 WRITE(SYSOT,12)I1,I2,I3,I4,I5	B	520	
	12 FORMAT(4X,'CONVENTIONAL CULVERT CODE:',2X,5I1,' WINGWALL - WITH	B	525	
	130-75 DEGREE WW FLARE, SQUARE TOP EDGES KE= 0.4'/)	B	530	
	GO TO 49	B	535	
	20 WRITE(SYSOT,22)I1,I2,I3,I4,I5	B	540	
	22 FORMAT(4X,'CONVENTIONAL CULVERT CODE:',2X,5I1,' HEADWALL - NORMA	B	545	
	1L OR SKEWED TO 45 DEGREES - SQ TOP EDGES KE= 0.5'/)	B	550	

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GO TO 49
30 WRITE(SYSOT,32) I1,I2,I3,I4,I5
32 FORMAT(4X,'CONVENTIONAL CULVERT CODE:',2X,5I1,' WINGWALL - 15 DE
1GREE FLARE - SQ TOP EDGES KE= 0.5'//)
GO TO 49
40 WRITE(SYSOT,42)I1,I2,I3,I4,I5
42 FORMAT(4X,'CONVENTIONAL CULVERT CODE:',2X,5I1,' WINGWALL - NORMA
1L OR SKEWED - ZERO DEGREE WW FLARE KE= 0.7'//)
49 IF(I5.NE.2) GO TO 60
50 WRITE(SYSOT,52)
52 FORMAT(4X,'BEVEL-EDGED CULVERT CODE: 41145 HEADWALL - NORMAL OR
1 SKEWED TO 45 DEGREES WITH 1:1 BEVELS'/40X,'(VARIABLE BEVEL ON ACU
2TE ANGLE OF SKEWED HEADWALL) KE= 0.2'//)
GO TO 80
60 WRITE(SYSOT,62)
62 FORMAT(4X,'BEVEL-EDGED CULVERT CODE: 41146 WINGWALL - 18 TO 33.
17 DEGREE WW FLARE WITH 1.5:1 TOP BEVEL OR'/40X,' 45 DEGREE FLARE W
2ITH 1:1 TOP BEVEL KE= 0.2'//)
GO TO 80
70 WRITE(SYSOT,72)
72 FORMAT(4X,'BEVEL-EDGED CULVERT CODE: 41147 HEADWALL - NORMAL
1WITH 1.5:1 BEVELS ON 3 SIDES KE= 0.2'//)
80 ISEL=SEL
ISER=SER
SLOPP=SLOPE
SLOPE=(ELIN-ELOUT)/DIST +.000001
WRITE(SYSOT,1900)I1,I2,I3,I4,I5,SLOPP,DIST,Q1,DTW,AHWEL,ELIN,
1ELOUT, SEL, SER,KBAS1,KBAS2,KDEP1,KDEP2,SFACE,SLOPE
1900 FORMAT(18X,'APPROX TOE-TOE',27X,
A 'ALLOWABLE STREAM BED STREAM BED LEFT ROADWAY R
1IGHT ROADWAY'/4X,'CULVERT',7X,'STREAM CULVERT DESIGN',6X,'DE
2SIGN',5X,'HEADWATER ELEVATION ELEVATION',5X,'EMBANKMENT',
35X,'EMBANKMENT'/6X,'CODE',8X,'SLOPE',4X,' LENGTH DISCHARGE TAI
4LWATER ELEVATION AT INLET AT OUTLET',7X,'SLOPE',11X,'SLOP
5E'/4X,5I1,8X,F7.4,2X,F8.1,2X,F8.1,4X,F8.1,4X,F8.1,4X,F8.1,5X,
6F8.1,9X,F4.1,':1',10X,F4.1,':1'//4X,'CULVERT SIZES',25X,'SLOPE-TA
7PER'/7X,'B FROM',I4,' FT TO',I4,' FT',12X,'FALL SLOPE',12X,'COMPU
8TED STREAM'/7X,'D FROM',I4,' FT TO',I4,' FT',14X,F4.1,':1',15X,
9'SLOPE =',F7.4//)
WRITE(SYSOT,2100)
2100 FORMAT(130H*****
1*****
2*****/'*****', ' INDEX SHEET FOR BOX
3 CULVERTS *****', '*****'
4*****/'*****', ' INDEX SHEET
5FOR BOX CULVERTS *****
6*****/'*****
7*****
8*****/'/)
459 WRITE(SYSOT 2105) CKE(I4)
2105 FORMAT(30X,'* -- OUTLET CONTROL -- **'.27X,'-- INLET CONTROL --
1'.27X,'*'/
130X,'*',25X,'**',73X,'*/30X,'* KE=',F4.1,' KE=0.2 OUTLET ** CON
2VENTIONAL CULVERT. * BEVEL-EDGED CULVERT * SIDE-TAPERED CULVERT
3 */30X,'-----

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B 670  
B 675  
B 680 \*\*  
B 685  
B 690  
B 695  
B 700  
B 705  
B 710  
B 715  
B 720  
B 725  
B 730  
B 735  
B 740  
B 745  
B 750  
B 755  
B 760  
B 765  
B 770  
B 775  
B 780  
B 785  
B 790  
B 795  
B 800  
B 805  
B 810  
B 815  
B 820  
B 825

```

4-----'/' * SEE *NUMBER
5*BARREL*BARREL* HW HW INVERT ** HW '.11X.'INVERT * HW B 830
6'.13X.'INVERT * THROAT',10X.'INVERT */' * PAGE * OF * WIDTH* D B 835
7EPTH* ELEV ELEV ELEV ** ELEV FALL ELEV * ELEV B 840
8FALL ELEV *HW ELEV FALL ELEV */ B 845
9 ' '.6X.'*BARRELS* (FT) * (FT) * (FT) (FT) B 850
A(FT) ** (FT) (FT) (FT) * (FT) (FT) (FT) B 855
B (FT) (FT) */' *.6X.'*.7X.'*.6X.'*.6X.'*.25X.'**'.23X. B 860
C'*.24X.'*.24X.'*') B 865
DO 457 J=1,100 B 870
ITAB(J)=0 B 875 **
TAB1(J)=0.0 B 880
TAB2(J)=0.0 B 885
TAB3(J)=0.0 B 890
TAB4(J)=0.0 B 895
TAB5(J)=0.0 B 900
TAB6(J)=0.0 B 905
TAB7(J)=0.0 B 910
TAB8(J)=0.0 B 915
TAB9(J)=0.0 B 920
TAB10(J)=0.0 B 925
TAB11(J)=0.0 B 930
TAB12(J)=0.0 B 935
TAB13(J)=0.0 B 940
TAB14(J)=0.0 B 945
TAB15(J)=0.0 B 950
TAB16(J)=0.0 B 955
TQMAX(1,J)=0.0 B 960
TQMAX(2,J)=0.0 B 965
457 CONTINUE B 970
L=1 B 975
458 BAR=1. B 980
I14=14 B 985
I15=15 B 990
IMP=0 B 995
ICOUNT=0 B 1000
53 KODE= I2*1000+I3*100+I4*10+I5 B 1005
DO 63 I=1,7 B 1010
IF(KODE.EQ.KT(I)) GO TO 460 B 1015
63 CONTINUE B 1020
C B 1025
PRINT CULVERT CODE INVALID B 1030
C B 1035
73 PRINT 2130 B 1040
2130 FORMAT(22H CULVERT CODE INVALID) B 1045
RETURN B 1050
C B 1055
START ANALYSIS OF BOX CULVERTS B 1060
460 DO 480 K=KBAS1,KBAS2 B 1065
B=BAR*K B 1070
DO 480 KK=KDEP1,KDEP2 B 1075
D=KK B 1080
NOCA(1,L)=0 B 1085
NOCA(2,L)=0 B 1090
NOCB(1,L)=0 B 1095
NOCB(2,L)=0 B 1100

```



NOCC(1,L)=0	B 1105
NOCC(2,L)=0	B 1110
HWIN=0.0	B 1115
HWO(1)=0.0	B 1120
HWO(2)=0.0	B 1125
SUMP(1)=0.0	B 1130
SUMP(2)=0.0	B 1135
FACEHW(1)=0.0	B 1140
FACEHW(2)=0.0	B 1145
HWOUT=0.0	B 1150
VELIN=0.0	B 1155
VELOUT=0.0	B 1160
IBET=0	B 1165
SMALL=(SLOPE*SEL**2*D)/(1+SLOPE*SEL)	B 1170
SMALR=(SLOPE*SER**2*D)/(1.+SLOPE*SER)	B 1175
DISL=SEL*D-SMALL	B 1180
DISR=SER*D+SMALR	B 1185
ELL=DISL*SLOPE	B 1190
ELR=DISR*SLOPE	B 1195
FACEL=ELIN-ELL	B 1200
FAHC=FACEL	B 1205
CROWN = FACEL+D	B 1210
TOEL=ELOUT+ELR	B 1215
HH=FACEL-TOEL	B 1220
DIST1=DIST-DISL-DISR	B 1225
CLTH=((DIST1*DIST1)+(HH*HH))**.5	B 1230
IF(D.GT.(1.2*(B/BAR))) GO TO 480	B 1235
IF((B/BAR).GT.(2.0*D)) GO TO 480	B 1240
I4=I14	B 1245
I5=I15	B 1250
IBEV=1	B 1255
IF(I5.GT.4) IBEV=2	B 1260
IF(IBEV.EQ.2) NOCA(1,L)=1	B 1265
IF(IBEV.EQ.2) IBET=1	B 1270
Q=Q1/BAR	B 1275
BB=B/BAR	B 1280
461 QMAX=0.0	B 1285
C.....COMPUTE OUTLET CONTROL HEADWATER	B 1290
CALL BOUT(Q,BB,D,HWOUT,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)	B 1295
HWO(IBEV)=HWOUT+TOEL	B 1300
IF(IBEV.EQ.1) GO TO 465	B 1305
462 IF(HWO(2).GT.AHWEL.AND.NOCA(1,L).EQ.1) N^CA(1,L)=0	B 1310
IF(HWO(2).GT.AHWEL) GO TO 480	B 1315
IF(HWO(2).LT.TOEL) GO TO 480	B 1320
C.....COMPUTE MAX Q	B 1325
465 CALL BFIT(Q,BB,D,QMAX,TOEL,SLOPE)	B 1330
Q=Q1/BAR	B 1335
TOMAX(IBEV,L)=QMAX*BAR	B 1340
X=Q1/(B*D**1.5)	B 1345
C.....COMPUTE INLET CONTROL HEADWATER	B 1350
CALL BEQUA(X,HWIN,B,D,SLOPE)	B 1355
124 FACEHW(IBEV)=FACEL+HWIN	B 1360
IF(IBEV.EQ.2) GO TO 132	B 1365
IF(FACEHW(1).LT.(AHWEL-D/3.).AND.HWO(1).LT.(AHWEL-D/3.)) GO TO 480	B 1370 **
GO TO 134	B 1375

132	IF(FACEHW(2).LT.(AHWEL-D/3.).AND.HWO(2).LT.(AHWEL-D/3.)) GO TO 480	B 1380	**
134	FALLM=1.5*D	B 1385	
	FALLT=DIST1*SLOPE	B 1390	
	IF(FALLM.GT.FALLT) FALLM=FALLT	B 1395	
	IF(FACEHW(IBEV).GT.AHWEL) GO TO 140	B 1400	
	GO TO 150	B 1405	
C	COMPUTE THE SUMP	B 1410	
140	SUMP(IBEV)=FACEHW(IBEV)-AHWEL	B 1415	
	IF(SUMP(IBEV).GE.FALLM) NOCA(IBEV,L)=1	B 1420	
	DISTA(IBEV,L)=DIST1	B 1425	
	IF(NOCA(IBEV,L).EQ.1) GO TO 153	B 1430	
	DIS=SUMP(IBEV)*SEL	B 1435	
	DISTA(IBEV,L)=DIS+DIST1	B 1440	
	FACEL=FACEL+SLOPE*DIS	B 1445	
	DIF=FACEL-SUMP(IBEV)-DIS*SLOPE	B 1450	
	IF(DIF.LT.TOEL) DIF=TOEL+.01	B 1455	
	SLOPA(IBEV,L)=(DIF-TOEL)/DISTA(IBEV,L)	B 1460	
	CROWN=DIF+D	B 1465	
	FACE(IBEV)=DIF	B 1470	
	FACEHW(1)=FACE(IBEV)+HWIN	B 1475	
	IF(FACEHW(1).GE.CROWN.OR.HWO(IBEV).GE.CROWN)GO TO 142	B 1480	**
	GO TO 480	B 1485	
142	HWEL(IBEV)=AHWEL	B 1490	
	GO TO 155	B 1495	
C	NO SUMP	B 1500	
150	SUMP(IBEV)=0.0	B 1505	
	SLOPA(IBEV,L)=SLOPE	B 1510	
	DISTA(IBEV,L)=DIST1	B 1515	
	FACE(IBEV)=FACEL	B 1520	
	CROWN=FACEL+D	B 1525	
	HWEL(IBEV)=FACEL+HWIN	B 1530	
	IF(FACEHW(IBEV).GE.CROWN.OR.HWO(IBEV).GE.CROWN)GO TO 155	B 1535	**
	GO TO 480	B 1540	
155	IF(SUMP(IBEV).EQ.0.0) CRESA(IBEV,L)=0.0	B 1545	
C	COMPUTE VELOCITY	B 1550	
	SLO=SLOPA(IBEV,L)	B 1555	
	DA=DISTA(IBEV,L)	B 1560	
	CALL BOUT(Q,BB,D,HWOOUT,VELOUT,DEP,DN,DC,Z,DA, .TOEL,QMAX,SLO)	B 1565	
	CALL BNCRM(Q,CN,SLO,BB,D,DEP,AREA,WP)	B 1570	
C.....	VELOCITY BASED ON EITHER INLET OR OUTLET CONTROL	B 1575	
	VELA(IBEV,L)=Q/AREA	B 1580	
	IF(VELOUT.GT.VELA(IBEV,L)) VELA(IBEV,L)=VELOUT	B 1585	
	IF(DN.GE.DC) GO TO 164	B 1590	
	IF(DTW.LT.DC) GO TO 164	B 1595	
	WHY2=0.247*VELA(IBEV,L)*DN**.5-(.5*DN)	B 1600	
	IF(WHY2.GT.DTW) GO TO 164	B 1605	
	IF(DTW.GE.D) VELA(IBEV,L)=Q/(BB*D)	B 1610	
	IF(DTW.LT.D) VELA(IBEV,L)=Q/(BB*DTW)	B 1615	
164	IF(SUMP(IBEV).EQ.0.0) GO TO 151	B 1620	
	HCA=FAHC+(SUMP(IBEV)*SEL*SLOPE)+(SUMP(IBEV)*3.+D/2.)*SLOPE	B 1625	
	HC=HWEL(IBEV)-HCA	B 1630	
	IF(HC.LT.1.) HC=1.0	B 1635	
	CRES=(.5*Q1**.6667)/HC	B 1640	
	CRESA(IBEV,L)=CRES**.15	B 1645	
C.....	COMPUTE CURVE B	B 1650	

151	ELINCA(IBEV.L)=FACE(IBEV)	B 1655
154	X=TQMAX(IBEV.L)/(B*D**1.5)	B 1660
	CALL BEQUA(X,HWI,B,D,SLOPE)	B 1665
	TEMP=ELINCA(IBEV.L)+HWI	B 1670
	IF(TEMP.LE.AHWEL) GO TO 144	B 1675
	BFALL=TEMP-AHWEL	B 1680
	TBFALL(IBEV.L)=BFALL +SUMP(IBEV)	B 1685
	IF(TBFALL(IBEV.L).GT.FALLM) GO TO 160	B 1690
	ELINCB(IBEV.L)=ELINCA(IBEV.L)-BFALL	B 1695
	IF(ELINCB(IBEV.L).LE.TOEL) ELINCB(IBEV.L)=TOEL+.01	B 1700
	HWCB(IBEV.L)=ELINCB(IBEV.L)+HWI	B 1705
	GO TO 139	B 1710
160	ELINCB(IBEV.L)=ELINCA(IBEV.L)-(FALLM-SUMP(IBEV))	B 1715
	IF(ELINCB(IBEV.L).LE.TOEL) ELINCB(IBEV.L)=TOEL+.01	B 1720
	BFALL=ELINCA(IBEV.L)-ELINCB(IBEV.L)	B 1725
	TBFALL(IBEV.L)=BFALL+SUMP(IBEV)	B 1730
C.....	COMPUTE MAX Q BASED ON INLET CONTROL CURVE	B 1735
	AIN=50.	B 1740
	QUE=Q1	B 1745
162	QUE=QUE-AIN	B 1750
	X=QUE/(B*D**1.5)	B 1755
	CALL BEQUA(X,HIGH,B,D,SLOPE)	B 1760
	HI=HIGH+ELINCB(IBEV.L)	B 1765
	IF(HI.GT.AHWEL) GO TO 170	B 1770
	GO TO 162	B 1775
170	QUE=QUE-AIN	B 1780
	IF(AIN.LT.10.) GO TO 172	B 1785
	AIN=2.0	B 1790
	GO TO 162	B 1795
172	TQMAX(IBEV.L)=QUE	B 1800
	X=QUE/(B*D**1.5)	B 1805
	CALL BEQUA(X,HWI,B,D,SLOPE)	B 1810
	HWCB(IBEV.L)=ELINCB(IBEV.L)+HWI	B 1815
139	DISB=BFALL*SEL	B 1820
	DISTB(IBEV.L)=DISTA(IBEV.L)+DISB	B 1825
	SLOPB(IBEV.L)=(ELINCB(IBEV.L)-TOEL)/DISTB(IBEV.L)	B 1830
C.....	COMPUTE VELOCITY BASED ON MAX Q	B 1835
	SLO=SLOPB(IBEV.L)	B 1840
	QQ=TQMAX(IBEV.L)/BAR	B 1845
	DB=DISTB(IBEV.L)	B 1850
	CALL BOUT(QQ,BB,D,HWOOUT,VELOUT,DEP,DN,DC,Z,DB .TOEL,QMAX,SLO)	B 1855
	CALL BNORM(QQ,CN,SLO,BB,D,DEP,AREA,WP)	B 1860
	VELB(IBEV.L)=QQ/AREA	B 1865
	IF(VELOUT.GT.VELB(IBEV.L)) VELB(IBEV.L)=VELOUT	B 1870
	IF(DN.GE.DC) GO TO 168	B 1875
	IF(DTW.LT.DC) GO TO 168	B 1880
	WHY2=0.247*VELB(IBEV.L)*DN**.5-(.5*DN)	B 1885
	IF(WHY2.GT.DTW) GO TO 168	B 1890
	IF(DTW.GE.D) VELB(IBEV.L)=Q/(BB*D)	B 1895
	IF(DTW.LT.D) VELB(IBEV.L)=Q/(BB*DTW)	B 1900
168	HCB=FAHC+(TBFALL(IBEV.L)*SEL*SLOPE)+(TBFALL(IBEV.L)*3.+D/2.)*SLOPE	B 1905
	HC=AHWEL-HCB	B 1910
	IF(HC.LT.1.) HC=1.0	B 1915
	CRES=(.5*TQMAX(IBEV.L)**.6667)/HC	B 1920
	CRESB(IBEV.L)=CRES**1.5	B 1925

GO TO 145	B 1930
144 TBFALL(IBEVL)=0.0	B 1935
NOCB(IBEVL)=1	B 1940
C.....COMPUTE CURVE C	B 1945
145 TEMP=ELINCA(IBEVL)+HWIN	B 1950
IF(HWO(IBEVL).GE.TEMP) GO TO 143	B 1955
CFALL=TEMP-HWO(IBEVL)	B 1960
TCFALL(IBEVL)=CFALL +SUMP(IBEVL)	B 1965
ELINCC(IBEVL)=ELINCA(IBEVL)-CFALL	B 1970
IF(TCFALL(IBEVL).GT.FALLM) ELINCC(IBEVL)=ELINCA(IBEVL)-(FALLM-	B 1975
1SUMP(IBEVL))	B 1980
IF(ELINCC(IBEVL).LE.TOEL) ELINCC(IBEVL)=TOEL+.01	B 1985
CFALL=ELINCA(IBEVL)-ELINCC(IBEVL)	B 1990
TCFALL(IBEVL)=CFALL+SUMP(IBEVL)	B 1995
HWCC(IBEVL)=ELINCC(IBEVL)+HWIN	B 2000
DISC=CFALL*SEL	B 2005
DISTC(IBEVL)=DISC+DISTA(IBEVL)	B 2010
SLOPC(IBEVL)=(ELINCC(IBEVL)-TOEL)/DISTC(IBEVL)	B 2015
SLO =SLOPC(IBEVL)	B 2020
DCC=DISTC(IBEVL)	B 2025
CALL BOUT(Q,BB,D,HWOOUT,VELOUT,DEP,DN,DC,Z,DCC ,TOEL,QMAX,SLO)	B 2030
CALL BNDRM(Q,CN,SLO,BB,D,DEP,AREA,WP)	B 2035
VELC(IBEVL)=Q /AREA	B 2040
IF(VELOUT.GT.VELC(IBEVL)) VELC(IBEVL)=VELOUT	B 2045
IF(DN.GE.DC) GO TO 169	B 2050
IF(DTW.LT.DC) GO TO 169	B 2055
WHY2=0.247*VELC(IBEVL)*DN**.5-(.5*DN)	B 2060
IF(WHY2.GT.DTW) GO TO 169	B 2065
IF(DTW.GE.D) VELC(IBEVL)=Q/(BB*D)	B 2070
IF(DTW.LT.D) VELC(IBEVL)=Q/(BB*DTW)	B 2075
169 HCC=FAHC+(TCFALL(IBEVL)*SEL*SLOPE)+(TCFALL(IBEVL)*3.+D/2.)*SLOPE	B 2080
HC=TEMP-HCC	B 2085
IF(HC.LT.1.) HC=1.0	B 2090
CRES=(.5*Q1**+.6607)/HC	B 2095
CRESC(IBEVL)=CRES**1.5	B 2100
GO TO 153	B 2105
143 TCFALL(IBEVL)=0.0	B 2110
NOCB(IBEVL)=1	B 2115
153 CONTINUE	B 2120
IF(IBEVL.EQ.2) GO TO 464	B 2125
FACEL=ELIN-ELL	B 2130
IBEVL=IBEVL+1	B 2135
IF(I5.EQ.2) GO TO 463	B 2140
I5=6	B 2145
I4=4	B 2150
GO TO 461	B 2155
463 I5=5	B 2160
I4=4	B 2165
GO TO 461	B 2170
464 I4=I14	B 2175
I5=I15	B 2180
IF(NOCA(1,L).EQ.1) NOCB(1,L)=1	B 2185
IF(NOCA(1,L).EQ.1) NOCC(1,L)=1	B 2190
IF(NOCA(2,L).EQ.1) NOCB(2,L)=1	B 2195
IF(NOCA(2,L).EQ.1) NOCC(2,L)=1	B 2200

INDEX=0	B 2205
IF (BAR.GT.2.) GO TO 120	B 2210
IBAR=BAR	B 2215
CALL CBSIDE(B,D,FALL,HWT,TRDEL,IBAR,DIST1,INDEX,SLOPE)	B 2220
IF (FALL.GT.900.) GO TO 120	B 2225
IF (FALL.GE.FALLM) GO TO 480	B 2230
GO TO 122	B 2235
120 FALL=0.0	B 2240
TRDEL=0.0	B 2245
HWT=0.0	B 2250
IF (NOCA(1,L).EQ.1.AND.NOCA(2,L).EQ.1) GO TO 480	B 2255
122 IBAR=BAR	B 2260
AK=K	B 2265
AKK=KK	B 2270
ITAB(L)=IBAR	B 2275
TAB1(L)=AK	B 2280
TAB2(L)=AKK	B 2285
TAB3(L)=HWO(1)	B 2290
TAB4(L)=HWO(2)	B 2295
TAB5(L)=TOEL	B 2300
TAB6(L)=HWEL(1)	B 2305
TAB7(L)=SUMP(1)	B 2310
TAB8(L)=FACE(1)	B 2315
TAB9(L)=HWEL(2)	B 2320
TAB10(L)=SUMP(2)	B 2325
TAB11(L)=FACE(2)	B 2330
TAB12(L)=HWT	B 2335
TAB13(L)=FALL	B 2340
TAB14(L)=TRDEL	B 2345
TAB15(L)=DIST2	B 2350
TAB16(L)=QMAX*IBAR	B 2355
IF (NOCA(1,L).EQ.1.AND.NOCA(2,L).EQ.1.AND.TAB4(L).GT.TAB12(L))	B 2360
GO TO 480	B 2365
IF (NOCA(1,L).EQ.0.AND.NOCA(2,L).EQ.0) GO TO 126	B 2370
IF (NOCA(2,L).EQ.0) GO TO 130	B 2375
GO TO 125	B 2380
130 TAB3(L)=0.0	B 2385
TAB6(L)=0.0	B 2390
TAB7(L)=0.0	B 2395
TAB8(L)=0.0	B 2400
C.....PRINT DATA FOR INDEX SHEET	B 2405
WRITE (SYSOT,127) L,IBAR,AK,AKK,HWO(2),TOEL,HWEL(2),SUMP(2),	B 2410
1 FACE(2),HWT,FALL,TRDEL	B 2415
127 FORMAT (' *',I3,3X,'*',I4,3X,'*',F5.1,'*',F5.1,'* --',F9.1,	B 2420
1 F10.1,'** --',5X,'--',7X,'-- *',2(F6.1,4X,F4.1,3X,F6.1,'*'))	B 2425
GO TO 123	B 2430
126 WRITE (SYSOT,123) L,IBAR,AK,AKK,HWO(1),HWO(2),TOEL,HWEL(1),	B 2435
1 SUMP(1),FACE(1),HWEL(2),SUMP(2),FACE(2),HWT,FALL,TRDEL	B 2440
123 FORMAT (' *',I3,3X,'*',I4,3X,'*',F5.1,'*',F5.1,'*'.2F7.1,F10.1,	B 2445
1' *',F6.1,3X,F4.1,3X,F6.1,'*'.2(F6.1,4X,F4.1,3X,F6.1,'*'))	B 2450
GO TO 128	B 2455
125 WRITE (SYSOT,129) L,IBAR,AK,AKK,HWO(2),TOEL,HWT,FALL,TRDEL	B 2460
129 FORMAT (' *',I3,3X,'*',I4,3X,'*',F5.1,'*',F5.1,'* --',F9.1,	B 2465
1 F10.1,'** --',5X,'--',7X,'-- *',3X,'--',6X,'--',7X,'-- *',	B 2470
2F6.1,4X,F4.1,3X,F6.1,'*')	B 2475

128	L=L+1	B	2480
479	ICOUNT=IBAR	B	2485
480	CONTINUE	B	2490
481	BAR=BAR+1.	B	2495
	IF(BAR.GT.5) L=L-1	B	2500
	IF(BAR.GT.5.) GO TO 482	B	2505
	GO TO 460	B	2510
482	IF(ICOUNT.EQ.0)WRITE(SYSOT,483)	B	2515 **
483	FORMAT(///5X,'RANGE OF CULVERT SIZES EXCEED DESIGN CRITERIA')	B	2520 **
	IF(ICOUNT.EQ.0)RETURN	B	2525 **
	WRITE(SYSOT,484)	B	2530
484	FORMAT(///25X,'BY DEFINITION OF FALL, WHEN A SIDE-TAPERED INLET LI	B	2535
	1ES ON THE STREAM SLOPE, '/25X,'THE FALL IS THE DIFFERENCE IN ELEVAT	B	2540
	2ION OF THE FACE INVERT AND THE THROAT INVERT'//25X,'WHEN SIDE-TAPE	B	2545
	3RED CULVERT COLUMN (ABOVE) CONTAINS 0.0 0.0 0.0'/30X.'1. THROAT DE	B	2550
	4SIGN EXCEEDS DESIGN LIMITS'/27X,'OR 2. IMPROVED INLETS FOR MORE TH	B	2555
	5AN 2 BARRELS NOT AVAILABLE')	B	2560
C.....	CALL TO BHY3 FOR CONVENTIONAL AND BEVEL DESIGN	B	2565
	CALL BHY3(DIST,SLOPE)	B	2570
	RETURN	B	2575
	END	B	2580

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SUBROUTINE BHY3(DIST,SLOPE)
C
C.....DESIGN CULVERTS LISTED ON INDEX SHEET
COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),
3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),
4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),
5      IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,
6NDCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),
8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,
ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2
DIMENSION HWO(2),SUMP(2),FACEHW(2),HWEL(2)
DIMENSION CKE(4),FACE(2)
REAL L1,L2,L3,L4
INTEGER SYSIN,SYSOT
DATA CKE/.4,.5,.7,.2/
II4=I4
II5=I5
90 LL=I
100 IBAR=ITAB(LL),
B=TAB1(LL)*IBAR
D=TAB2(LL)
SMALL=(SLOPE*SEL**2*D)/(1.+SLOPE*SEL)
SMALR=(SLOPE*SER**2*D)/(1.+SLOPE*SER)
DISL=SEL*D-SMALL
DISR=SER*D+SMALR
ELL=DISL*SLOPE
ELR=DISR*SLOPE
DIST1=DIS1-DISL-DISR
PAGE HEADINGS
94 WRITE(SYSOT,80) LL,ITAB(LL),TAB1(LL),TAB2(LL),Q1,AHWEL,SLOPE
1,TAB5(LL)
80 FORMAT(1H1,' PAGE=' ,I3,5X,'NO. BARRELS=' ,I2,4X,'WIDTH=' ,F5.1,' FT
1',4X,'HEIGHT=' ,F5.1,' FT',4X,'Q(50)' ,F7.1,' CFS AHWEL=' ,
2F7.1,' FT',4X,'STREAM SLOPE =' ,F7.4/50X,'OUTLET INVERT ELEV. =' ,
3F7.1,' FT'////)
IF(I5.GT.4)WRITE(SYSOT,8)
8 FORMAT(1X,'CONVENTIONAL INLET DESIGN'//1X,'*****')
1*///;20X,'CONVENTIONAL CULVERT DESIGN NOT REQUESTED'///)
IF(I5.GT.4) GO TO 212
IF(NOCA(1,LL).EQ.0) GO TO 89
WRITE(SYSOT,91)I1,I2,I3,I4,I5
91 FORMAT(1X,'CONVENTIONAL INLET DESIGN FOR CULVERT CODE ',5I1/
11X,'*****'//20X,
2'DESIGN DATA NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE CONV
3ENTIONAL INLET EXCEEDS 1.50 OR L50. ')
GO TO 206
C
C.....CONVENTIONAL INLET DESIGN + PERFORMANCE CURVE DATA
89 WRITE(SYSOT,81)I1,I2,I3,I4,I5,CKE(I4),TOMAX(1,LL)
81 FORMAT(1X,'CONVENTIONAL INLET DESIGN FOR CULVERT CODE: ',5I1/
11X,'*****'//4X,'OUT

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B 2585
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B 2605 **
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B 2855

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2LET COMPUTATIONS',34X,'INLET COMPUTATIONS'/3X.'*****
3*'.8X.'*****
4*****
5URVE'.17X,'MAX Q CURVE',21X,'MIN HW CURVE'//67X.'MAX Q '='.F7.1.
6' CFS'//)
DA=DISTA(1,LL)
SA=SLOPA(1,LL)
SB=SLOPB(1,LL)
SC=SLOPC(1,LL)
IF(NOCB(1,LL).EQ.1.AND.NOCC(1,LL).EQ.1) GO TO 14
IF(NOCB(1,LL).EQ.1) GO TO 32
IF(NOCC(1,LL).EQ.1) GO TO 18
10 WRITE(SYSOT,12)DISTA(1,LL),DISTB(1,LL),DISTC(1,LL),TAB7(LL),
1TB FALL(1,LL),TCFALL(1,LL),ELINCA(1,LL),ELINCB(1,LL),ELINCC(1,LL),
2SLOPA(1,LL),SLOPB(1,LL),SLOPC(1,LL),VELA(1,LL),VELB(1,LL),VELC(1,
3LL),CRESA(1,LL),CRESB(1,LL),CRESC(1,LL)
12 FORMAT(30X,'CULVERT LENGTH '='.F7.1,' FT'.6X,'CULVERT LENGTH '='.
1F7.1,' FT'.6X,'CULVERT LENGTH '='.F7.1,' FT'/30X,'FALL AT FACE
2='.F7.1,' FT'.6X,'FALL AT FACE '='.F7.1,' FT'.6X,'FALL AT FACE
3 '='.F7.1,' FT'/30X,'ELEV FACE INVERT='.F7.1,' FT'.6X,'ELEV FACE I
4NVERT='.F7.1,' FT'.6X,'ELEV FACE INVERT='.F7.1,' FT'/30X,'CULVERT
5SLOPE '='.F9.4.7X,'CULVERT SLOPE '='.F9.4.7X,'CULVERT SLOPE '='
6.F9.4/30X,'VEL AT DESIGN Q '='.F7.1,' FPS'.5X,'VEL AT MAX Q '='.
7F7.1,' FPS'.5X,'VEL AT DESIGN Q '='.F7.1,' FPS'/30X,'MIN CREST LENG
8TH='.F7.1,' FT'.6X,'MIN CREST LENGTH='.F7.1,' FT'.6X,'MIN CREST LE
9NGTH='.F7.1,' FT'//8X,'Q'.8X,'HWO'.20X,'Q'.8X,'HWF'.20X,'Q'.8X,'HW
AF'.20X,'Q'.8X,'HWF'//)
QD=Q1-(Q1*.2)
63 Q=QD/IBAR
BB=B/IBAR
CALL BOUT(Q,BB,D,HWO,VELOUT,DEP,ON,DC,Z,DIST1,TOEL,QMAX,SLOPE)
HWO1=HWO+TAB5(LL)
X=QD/(B*D**1.5)
CALL BEQUA(X,HWN,B,D,SA)
HDCA=ELINCA(1,LL)+HWN
CALL BEQUA(X,HWN,B,D,SB)
HDCB=ELINCB(1,LL)+HWN
CALL BEQUA(X,HWN,B,D,SC)
HDCC=ELINCC(1,LL)+HWN
WRITE(SYSOT,85)QD,HWO1,QD,HDCA,QD,HDCB,QD,HDCC
85 FORMAT(3X,F9.0,F9.1,3(13X,F9.0,1X,F9.1))
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 206
QD=QD+(Q1*.2)
GO TO 63
14 WRITE(SYSOT,15)DISTA(1,LL),TAB7(LL),ELINCA(1,LL),SLOPA(1,LL),
1VELA(1,LL),CRESA(1,LL)
16 FORMAT(30X,'CULVERT LENGTH '='.F7.1,' FT'.19X,'--',26X,'--'/30X,
1'FALL AT FACE '='.F7.1,' FT'.19X,'--',26X,'--'/30X,'ELEV FACE I
2NVERT='.F7.1,' FT'.19X,'--',26X,'--'/30X,'CULVERT SLOPE '='.F9.4.
320X,'--',26X,'--'/30X,'VEL AT DESIGN Q '='.F7.1,' FPS'.18X,'--',
426X,'--'/30X,'MIN CREST LENGTH='.F7.1,' FT'.19X,'--',26X,'--'/8X,
5'Q'.8X,'HWO'.20X,'Q'.8X,'HWF'.20X,'Q'.8X,'HWF'//)
QD=Q1-(Q1*.2)
60 Q=QD/IBAR
BB=B/IBAR

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B 2860
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B 3120
B 3125
B 3130

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CALL BOUT(Q,BB,D,HWOOUT,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)
HWO1=HWOOUT+TAB5(LL)
X=QD/(B*D*1.5)
CALL BEQUA(X,HWN,B,D,SA)
HDCA=ELINCA(1,LL)+HWN
WRITE(SYSOT,186)QD,HWO1,QD,HDCA
186 FORMAT(3X,F9.0,F9.1,14X,F9.0,F9.1,20X,'---',8X,'---',18X,'---',8X,'---
1')
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 205
QD=QD+(Q1*.2)
GO TO 60
18 WRITE(SYSOT,20)DISTA(1,LL),DISTB(1,LL),TAB7(LL),TBFALL(1,LL),
1ELINCA(1,LL),ELINCB(1,LL),SLOPA(1,LL),SL^PB(1,LL),VELA(1,LL),
2VELB(1,LL),CRESA(1,LL),CRESB(1,LL)
20 FORMAT(30X,'CULVERT LENGTH =',F7.1,' FT',6X,'CULVERT LENGTH =',
1F7.1,' FT',14X,'---'/30X,'FALL AT FACE =',F7.1,' FT',6X,'FALL AT
2FACE =',F7.1,' FT',14X,'---'/30X,'ELEV FACE INVERT=',F7.1,' FT'
4,6X,'ELEV FACE INVERT=',F7.1,' FT',14X,'---'/30X,'CULVERT SLOPE =
5',F9.4,7X,'CULVERT SLOPE =',F9.4,15X,'---'/30X,'VEL AT DESIGN Q =
6',F7.1,' FPS',5X,'VEL AT MAX Q =',F7.1,' FPS',13X,'---'/30X,'MIN
7CREST LENGTH=',F7.1,' FT',6X,'MIN CREST LENGTH=',F7.1,' FT',14X,
8'---'/8X,'Q',8X,'HWO',20X,'Q',8X,'HWF',20X,'Q',8X,'HWF',18X,'Q',
98X,'HWF'/)
QD=Q1-(Q1*.2)
64 Q=QD/IBAR
BB=B/IBAR
CALL BOUT(Q,BB,D,HWOOUT,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)
HWO1=HWOOUT+TAB5(LL)
X=QD/(B*D*1.5)
CALL BEQUA(X,HWN,B,D,SA)
HDCA=ELINCA(1,LL)+HWN
CALL BEQUA(X,HWN,B,D,SB)
HDCB=ELINCB(1,LL)+HWN
WRITE(SYSOT,183)QD,HWO1,QD,HDCA,QD,HDCB
183 FORMAT(3X,F9.0,F9.1,14X,F9.0,F9.1,14X,F9.0,F9.1,15X,'---',8X,'---')
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 206
QD=QD+(Q1*.2)
GO TO 64
32 WRITE(SYSOT,24)DISTA(1,LL),DISTC(1,LL),TAB7(LL),TCFALL(1,LL),
1ELINCA(1,LL),ELINCC(1,LL),SLOPA(1,LL),SL^PC(1,LL),VELA(1,LL),
2VELC(1,LL),CRESA(1,LL),CRESB(1,LL)
24 FORMAT(30X,'CULVERT LENGTH =',F7.1,' FT',19X,'---',15X,'CULVERT LE
1NGTH =',F7.1,' FT'/30X,'FALL AT FACE =',
2F7.1,' FT',19X,'---',15X,'FALL AT FACE =',
3F7.1,' FT'/30X,'ELEV FACE INVERT=',F7.1,' FT',19X,'---'
4,15X,'ELEV FACE INVERT=',F7.1,' FT'/30X,'CULVERT SLOPE =',F9.4,
520X,'---',15X,'CULVERT SLOPE =',F9.4,30X,'VEL AT DESIGN Q =',F7.1,
6'FPS',19X,'---',15X,'VEL AT DESIGN Q =',F7.1,' FPS'/30X,'MIN CREST
7LENGTH=',F7.1,' FT',19X,'---',15X,'MIN CREST LENGTH=',F7.1,' FT'//
88X,'Q',8X,'HWO',20X,'Q',8X,'HWF',20X,'Q',8X,'HWF',18X,'Q',8X,
9'HWF'/)
QD=Q1-(Q1*.2)
86 Q=QD/IBAR
BB=B/IBAR
CALL BOUT(Q,BB,D,HWOOUT,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)

```

B 3135  
B 3140  
B 3145  
B 3150  
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B 3265  
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B 3295  
B 3300  
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B 3345  
B 3350  
B 3355  
B 3360  
B 3365  
B 3370  
B 3375  
B 3380  
B 3385  
B 3390  
B 3395  
B 3400  
B 3405

\*\*

```

HWO1=HWOUT+TAB5(LL)
X=QD/(B+D**1.5)
CALL BEQUA(X,HWN ,B.D,SA)
HDCA=ELINCA(1,LL)+HWN
CALL BEQUA(X,HWN ,B.D,SC)
HDCC=ELINCC(1,LL)+HWN
WRITE(SYSOT,180)QD,HWO1,QD,HDCA,QD,HDCC
180 FORMAT(3X,F9.0,F9.1,14X,F9.0,F9.1,19X,'--'.8X,'--'.13X,F9.0,F9.1)
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 206
QD=QD+(Q1*.2)
GO TO 86
206 IF(I5.EQ.2) GO TO 210
I5=6
I4=4
GO TO 212
210 I5=5
I4=4
C
C.....BEVELED INLETS
C
212 DA=DISTA(2,LL)
SA=SLOPA(2,LL)
SB=SLOPB(2,LL)
SC=SLOPC(2,LL)
IF(NOCA(2,LL).EQ.0) GO TO 208
WRITE(SYSOT,211) I1,I2,I3,I4,I5,TQMAX(2,LL)
211 FORMAT(///1X,'BEVELED INLET DESIGN FOR CULVERT CODE:'.5I1/1X.'****
1*****'///20X,'DESIGN DATA
2 NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE BEVEL-EDGED INLE
3T EXCEEDS 1.50 OR L50'/20X,'THIS OUTPUT CONSISTS OF THE OUTLET CON
4TROL PERFORMANCE CURVE DATA FOR KE = 0.2'/20X,'WHICH IS APPLICABLE
5 FOR THE IMPROVED INLETS.'//30X,'Q',10X,'HWO',15X,'MAX Q = ',
6F7.0,' CFS'//)
240 QD=Q1-(Q1*.2)
214 Q=QD/IBAR
BB=B/IBAR
CALL GOBT(Q,BB,D,HWOUT,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)
HWO1=HWOUT+TAB5(LL)
241 WRITE(SYSOT,243)QD,HWO1
243 FORMAT(26X,F7.1,6X,F6.1)
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 330
QD=QD+(Q1*.2)
GO TO 214
208 WRITE(SYSOT,213) I1,I2,I3,I4,I5,CKE(I4),TQMAX(2,LL)
213 FORMAT(///1X,'BEVELED INLET DESIGN FOR CULVERT CODE:'.5I1/
A1X.'*****'//
1 4X,'OUTLET COMPUTATIONS',34X,'INLET COMPUTATIONS'/ 3X.'*****'
2*****'.8X.'*****'//
2*****'//10X,'KE ='.
3F4.1,18X,'MIN FALL CURVE',17X,'MAX Q CURVE',21X,'MIN HW CURVE'/
4 /67X,'MAX Q =',F7.0,' CFS'//)
IF(NOCC(2,LL).EQ.1.AND.NOCC(2,LL).EQ.1) GO TO 25
IF(NUCB(2,LL).EQ.1) GO TO 22
IF(NOCC(2,LL).EQ.1) GO TO 28
21 WRITE(SYSOT,12)DISTA(2,LL),DISTB(2,LL),DISTC(2,LL),TAB10(LL).

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B 3410
B 3415
B 3420
B 3425
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B 3455
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B 3595
B 3600
B 3605
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B 3630
B 3635
B 3640
B 3645
B 3650
B 3655
B 3660
B 3665
B 3670
B 3675
B 3680

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1	TBFALL(2,LL),TCFALL(2,LL),ELINCA(2,LL),ELINCB(2,LL),ELINCC(2,LL),	B 3685
2	SLOPA(2,LL),SLOPB(2,LL),SLOPC(2,LL),VELA(2,LL),VELB(2,LL),VELC(2,	B 3690
3	3LL),CRESA(2,LL),CRESB(2,LL),CRESC(2,LL)	B 3695
	QD=Q1-(Q1*.2)	B 3700
88	Q=QD/IBAR	B 3705
	BB=B/IBAR	B 3710
	CALL BOUT(Q,BB,D,HWO2,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)	B 3715
	HWO2=HWO2+TAB5(LL)	B 3720
	X=QD/(B*D**1.5)	B 3725
	CALL BEQUA(X,HWN,B,D,SA)	B 3730
	HDCA=ELINCA(2,LL)+HWN	B 3735
	CALL BEQUA(X,HWN,B,D,SB)	B 3740
	HDCB=ELINCB(2,LL)+HWN	B 3745
	CALL BEQUA(X,HWN,B,D,SC)	B 3750
	HDCC=ELINCC(2,LL)+HWN	B 3755
	WRITE(SYSOT,85)QD,HWO2,QD,HDCA,QD,HDCB,QD,HDCC	B 3760
	IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 330	B 3765
	QD=QD+(Q1*.2)	B 3770
	GO TO 88	B 3775
25	WRITE(SYSOT,16)DISTA(2,LL),TAB10(LL),ELINCA(2,LL),SLOPA(2,LL),	B 3780
	1VELA(2,LL),CRESA(2,LL)	B 3785
	QD=Q1-(Q1*.2)	B 3790
62	Q=QD/IBAR	B 3795
	BB=B/IBAR	B 3800
	CALL BOUT(Q,BB,D,HWO2,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)	B 3805
	HWO2=HWO2+TAB5(LL)	B 3810
	X=QD/(B*D**1.5)	B 3815
	CALL BEQUA(X,HWN,B,D,SA)	B 3820
	HDCA=ELINCA(2,LL)+HWN	B 3825
	WRITE(SYSOT,186)QD,HWO2,QD,HDCA	B 3830
	IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 330	B 3835
	QD=QD+(Q1*.2)	B 3840
	GO TO 62	B 3845
28	WRITE(SYSOT,20)DISTA(2,LL),DISTB(2,LL),TAB10(LL),TBFALL(2,LL),	B 3850
	1ELINCA(2,LL),ELINCB(2,LL),SLOPA(2,LL),SLOPB(2,LL),VELA(2,LL),	B 3855
	2VELB(2,LL),CRESA(2,LL),CRESB(2,LL)	B 3860
	QD=Q1-(Q1*.2)	B 3865
66	Q=QD/IBAR	B 3870
	BB=B/IBAR	B 3875
	CALL BOUT(Q,BB,D,HWO2,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)	B 3880
	HWO2=HWO2+TAB5(LL)	B 3885
	X=QD/(B*D**1.5)	B 3890
	CALL BEQUA(X,HWN,B,D,SA)	B 3895
	HDCA=ELINCA(2,LL)+HWN	B 3900
	HDCB=ELINCB(2,LL)+HWN	B 3905
	WRITE(SYSOT,183)QD,HWO2,QD,HDCA,QD,HDCB	B 3910
	IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 330	B 3915
	QD=QD+(Q1*.2)	B 3920
	GO TO 66	B 3925
22	WRITE(SYSOT,24)DISTA(2,LL),DISTC(2,LL),TAB10(LL),TCFALL(2,LL),	B 3930
	1ELINCA(2,LL),ELINCC(2,LL),SLOPA(2,LL),SLOPC(2,LL),VELA(2,LL),	B 3935
	2VELC(2,LL),CRESA(2,LL),CRESC(2,LL)	B 3940
	QD=Q1-(Q1*.2)	B 3945
87	Q=QD/IBAR	B 3950
	BB=B/IBAR	B 3955

CALL BOUT(Q,BB,D,HWO2,VELOUT,DEP,DN,DC,Z,DIST1,TOEL,QMAX,SLOPE)	B 3960
HWO2=HWO2+TAB5(LL)	B 3965
X=QD/(B*D*1.5)	B 3970
CALL BEQUA(X,HWN ,B,D,SA)	B 3975
HDCA=ELINCA(2,LL)+HWN	B 3980
CALL BEQUA(X,HWN ,B,D,SC)	B 3985
HDCC=ELINCC(2,LL)+HWN	B 3990
WRITE(SYSOT,180)QD,HWO2,QD,HDCA,QD,HDCC	B 3995
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 330	B 4000
QD=QD+(Q1*.2)	B 4005
GO TO 87	B 4010
C	B 4015
C SIDE TAPERED INLETS	B 4020
330 IF(ITAB(LL).GT.2) WRITE(SYSOT,250)	B 4025
250 FORMAT(//' IMPROVED-INLET DESIGN'/5X,'*****'/////	B 4030
135X,'NO IMPROVED-INLET DESIGNS AVAILABLE FOR CULVERTS HAVING MORE	B 4035
1THAN " 2 " BARRELS')	B 4040
IF(ITAB(LL).GT.2) GO TO 362	B 4045
INDEX=2	B 4050
C.....DESIGN SIDE-TAPERED INLETS	B 4055
CALL BSIDE(B,D,FALL,HWT,TROEL,IBAR,DIST1,INDEX,SLOPE)	B 4060
C	B 4065
C.....DESIGN SLOPE-TAPERED INLETS(VERTICAL AND MITERED	B 4070
CALL BSLOPV(B,D,SLOPE)	B 4075
CALL BSLOPM(B,D,SLOPE)	B 4080
362 LL=LL+1	B 4085
IF(LL.GT.L) RETURN	B 4090
I4=I14	B 4095
I5=I15	B 4100
GO TO 100	B 4105
END	B 4110

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SUBROUTINE BSIDE(B,D,FALL,HWT,TROEL,IBAR,DIST1,INDEX,SLOPE)
  DESIGN SIDE TAPERED INLETS
C
COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),
3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),
4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),
5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),
BSLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,
ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2
REAL L1,L1B,L1C
INTEGER SYSIN, SYSOT
DATA ALPHA,SCORR,CN/1.0,.5,.012/
TAPER=4.
IF(IBAR.GT.2) GO TO 480
460 HWOUT=0.0
HW=0.
NOCAS=0
NOCBS=0
NOCCS=0
FACEL=ELIN-ELL
TOEL=ELOUT+ELR
C.....THROAT EQUATION - CHART 14 - HEC-13
X=Q1/(B*D**1.5)
Y16 =.1295033+.3789445*X-.0437776*X*X+.00426329*X*X*X
1-.000106358*X*X*X*X
IF(Y16.LT.1.0) FALL=999.
IF(Y16.LT.1.0.AND.INDEX.GT.1) WRITE(SYSOT,18)
18 FORMAT(////1X,'SIDE-TAPER DESIGN'/1X,'*****'////20X,
1'THIS SIDE-TAPERED INLET EXCEEDS DESIGN CRITERIA')
IF(Y16.LT.1)RETURN
HT=Y16*D
52 X=(HT-1.)/D
C.....FACE EQUATION - CHART 15 - HEC 13
20 Y15 =-1.13607+3.698525*X+.1212797*X*X-.20533949*X*X*X
1+.0256923*X*X*X*X
TROEL=AHWEL-HT
BF=Q1/(Y15*D**1.5)+.1
42 L1=((BF-D)/2.)*TAPER
DLEFT=DISL+L1
DROP=DLEFT+SLOPE
SUET=DIST1-L1
STROEL=ELIN-DROP
DIF=STROEL-TROEL
IF(DIF.LE.0.0) GO TO 10
C
COMPUTE FALL
FALL=DIF+L1*SLOPE
HWT=AHWEL
3 IF(INDEX.EQ.1) RETURN
IF(INDEX.EQ.2) GO TO 5
IF(INDEX.EQ.3) GO TO 5
B 4115
B 4120
B 4125
B 4130 **
B 4135 **
B 4140 **
B 4145 **
B 4150 **
B 4155 **
B 4160 **
B 4165 **
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B 4375
B 4380
B 4385

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	INDEX=INDEX+1	B 4390
	X=(HT-L1*SLOPE)/D	B 4395
	GO TO 20	B 4400
5	BIT=SEL-DIF	B 4405
	SUBT=SUBT+BIT	B 4410
	TOTA=SUBT+L1	B 4415
	SA=(TROEL-TOEL)/SUBT	B 4420
	STFACE=STROEL+SLOPE*L1+BIT*SLOPE	B 4425
	ELFACA=TROEL+SA*L1	B 4430
	ELTRCA=TROEL	B 4435
	IF(FALL.LT.D/4.) WA=0.0	B 4440
	IF(FALL.LT.D/4.)GO TO 100	B 4445
	HCA=FACEL+(FALL*SEL*SLOPE)+(FALL*3.+D/2.)*SLOPE	B 4450
	HC=AHWEL-HCA	B 4455
	IF(HC.LT.1.) HC=1.0	B 4460
	W23A=(.5*Q1**2.6667)/HC	B 4465
	WA=W23A**1.5	B 4470
	GO TO 100	B 4475
C	NO FALL	B 4480
10	WA=0.0	B 4485
	FALL=FACEL-STROEL	B 4490
	TROEL=STROEL	B 4495
	HWT=TROEL+HT	B 4500
	IF(INDEX.EQ.1)RETURN	B 4505
	IF(INDEX.EQ.0) GO TO 3	B 4510
	ELFACA=TROEL+SLOPE*L1	B 4515
	TOTA=SUBT+L1	B 4520
	ELTRCA=TROEL	B 4525
	SA=SLOPE	B 4530
	STFACE=ELFACA	B 4535
100	SLO=SA	B 4540
	BAR=IBAR	B 4545
	Q=Q1/BAR	B 4550
	BB=B/BAR	B 4555
	CALL BOUT(Q, BB, D, HWOUT, VELOUT, DEP, DN, DC, Z, SUBT ,TOEL, QMAX, SLO)	B 4560
	CALL BNORM(Q ,CN, SLO ,BB, D, DEP, AREA, WP)	B 4565
	VELAA=Q /AREA	B 4570
	IF(VELOUT.GT.VELAA) VELAA=VELOUT	B 4575
	IF(DN.GE.DC) GO TO 12	B 4580
	IF(DTW.LT.DC) GO TO 12	B 4585
	WHY2=0.247*VELAA*DN**2.5-(.5*DN)	B 4590
	IF(WHY2.GT.DTW) GO TO 12	B 4595
	IF(DTW.GE.D) VELAA=Q/(BB*D)	B 4600
	IF(DTW.LT.D) VELAA=Q/(BB*DTW)	B 4605
12	BEA=BF*.5	B 4610
	DEA=D*.5	B 4615
101	INDEX=INDEX+1	B 4620
	IF(INDEX.EQ.4) GO TO 102	B 4625
	X=(HT-L1*SA)/D	B 4630
	GO TO 20	B 4635
C	COMPUTE CURVE B - SIDE TAPER	B 4640
102	INDEX=2	B 4645
	HWTMP=HWT	B 4650
	FALLM=1.5*D	B 4655
	FALLT=SUBT*SLOPE	B 4660

IF(FALLM.GT.FALLT) FALLM=FALLT	B 4665
QUE= TAB16(LL)	B 4670
X=QUE/(B*D**1.5)	B 4675
Y16 =.1295033+.3789445*X-.0437778*X*X+.00426329*X*X*X	B 4680
1-.000106358*X*X*X	B 4685
HWATER=Y16*D	B 4690
TEMP=ELTRCA+HWATER	B 4695
IF(TEMP.LE.AHWEL)GO TO 466	B 4700
BFALL=TEMP-AHWEL	B 4705
TBFAL =BFALL+FALL	B 4710
ELTRCB=ELTRCA-BFALL	B 4715
IF(ELTRCB.LT.TOEL) ELTRCB=TOEL+.01	B 4720
IF(TBFAL.GT.FALLM) ELTRCB=ELTRCA-(FALLM-FALL)	B 4725
BFALL=ELTRCA-ELTRCB	B 4730
TBFAL=BFALL+FALL	B 4735
BITB=SEL*BFALL	B 4740
SB=(ELTRCB-TOEL)/(SUBT+BITB)	B 4745
AIN= 50.	B 4750
QUE=Q1	B 4755
470 QUE=QUE+AIN	B 4760
X=QUE/(B*D**1.5)	B 4765
Y16 =.1295033+.3789445*X-.0437778*X*X+.00426329*X*X*X	B 4770
1-.000106358*X*X*X	B 4775
HIGH=Y16*D	B 4780
HI=HIGH+ELTRCB	B 4785
IF(HI.GT.AHWEL) GO TO 474	B 4790
H=HIGH	B 4795
GO TO 470	B 4800
474 QUE=QUE-AIN	B 4805
IF(AIN.LT.10.) GO TO 475	B 4810
AIN=2.0	B 4815
GO TO 470	B 4820
475 IF(QUE.GT.TAB16(LL)) QUE=TAB16(LL)	B 4825
X=(AHWEL-ELTRCB-L1*SB)/D	B 4830
Y15 =-1.13807+3.698525*X+.1212797*X*X-.20533949*X*X*X	B 4835
1+.0256923*X*X*X	B 4840
BFB=QUE/(Y15*D**1.5)+.1	B 4845
L1B=((BFB-B)/2.)*TAPER	B 4850
TOTR=SUBT+L1B+BITB	B 4855
ELFACB=ELTRCB+L1B*SB	B 4860
QQ=QUE/DAR	B 4865
TB=SUBT+BITB	B 4870
CALL BOUT(QQ,BB,D,HWOUT,VELOUT,DEP,DN,DC,Z,TB ,TOEL,QMAX,SLO)	B 4875
CALL BNORM(QQ,CN,SB,BB,D,DEP,AREA,WP)	B 4880
VELBB=QQ /AREA	B 4885
IF(VELOUT.GT.VELBB) VELBB=VELOUT	B 4890
IF(DN.GE.DC) GO TO 14	B 4895
IF(DTW.LT.DC) GO TO 14	B 4900
WHY2=0.247-VELBB*DN*.5-(.5*DN)	B 4905
IF(WHY2.GT.DTW) GO TO 14	B 4910
IF(DTW.GE.D) VELBB=Q/(BB*D)	B 4915
IF(DTW.LT.D) VELBB=Q/(BB*DTW)	B 4920
14 HCB=FACEL+(TBFAL*SEL*SLOPE)+(TBFAL*3.+D/2.)*SLOPE	B 4925
HC=AHWEL-HCB	B 4930
IF(HC.LT.1.) HC=1.0	B 4935

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W23B=(.5*QUE**1.6667)/HC
WB=W23B**1.5
BEB=BFB+.5
DEB=D*.5
GO TO 490
466 TBFAL =0.0
NOCBS=1
C COMPUTE CURVE C - SIDE TAPER
490 TEMP=ELTRCA+4T
IF(TAB4(LL).GE.TEMP) GO TO 482
CFAL=TEMP-TAB4(LL)
TCFAL=CFAL+FALL
ELTRCC=ELTRCA-CFAL
IF(TCFAL.GT.FALLM) ELTRCC=ELTRCA-(FALLM-FALL)
IF(ELTRCC.LT.TOEL) ELTRCC=TOEL+.01
CFAL=ELTRCA-ELTRCC
TCFAL=CFAL+FALL
BITC=SEL*CFAL
SC=(ELTRCC-TOEL)/(SUBT+BITC)
X=(TEMP -CFAL-ELTRCC-L1*SC)/D
Y15 =-1.13607+3.698525*X+.1212797*X*X-.20533949*X*X*X
1+.0256923*X*X*X*X
BFC=Q1/(Y15-D**1.5)+.1
L1C=((BFC-B)/2.)*TAPER
TOTC=SUBT+L1C+BITC
ELFACC=ELTRCC+L1C*SC
HCC=FACEL+(TCFAL*SEL*SLOPE)+(TCFAL*3.+D/2.)*SLOPE
HC=TEMP-HCC
IF(HC.LT.1.) HC=1.0
W23C=(.5*Q1**1.6667)/HC
WC=W23C**1.5
SLO=SC
TC=SUBT+BITC
CALL BOUT(Q,BB,D,HWO,VELOUT,DEP,DN,DC,Z,TC ,TOEL,QMAX,SLO)
CALL SNORM(Q ,CN,SC,BS,D,DEP,AREA,WP)
VELCC=Q /AREA
IF(VELOUT.GT.VELOC) VELOC=VELOUT
IF(DN.GE.DC) GO TO 16
IF(DTW.LT.DC) GO TO 16
WHY2=0.247*VELOC*DN*.5-(.5*DN)
IF(WHY2.GT.DTW) GO TO 16
IF(DTW.GE.D) VELOC=Q/(BB*D)
IF(DTW.LT.D) VELOC=Q/(BB*DTW)
16 BEC=BFC+.5
DEC=D*.5
GO TO 483
482 TCFAL=0.0
NOCBS=1
C.....DESIGN PRINTOUT + PERFORMANCE CURVE DATA
483 WRITE(SYSOT,104)QUE
104 FORMAT(///1X,'SIDE TAPERED INLET DESIGN'/'*****'
1**',10X,'FACE EDGE BEVELS = 45 DEG',5X,'SIDE TAPER = 4:1'//
2 10X,'MIN FALL DESIGN',30X,'MAX Q DESIGN',30X,'MIN HW DESIG
3N'//55X,'MAX Q =',F7.0,' CFS'//)
IF(NOCBS.EQ.0.AND.NOCBS.EQ.0) GO TO 30

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B 4940
B 4945
B 4950
B 4955
B 4960
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B 4990
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B 5010
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B 5195
B 5200
B 5205
B 5210

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IF(NCCDS.EQ.0) GO TO 32
IF(NCCDS.EQ.0) GO TO 34
WRITE(SYSOT,28)TOTA,TAB13(LL),TAB14(LL),ELFACA,SA,VELAA,BF,L1,WA,
1BEA,DEA
28 FORMAT(5X,'CULVERT LENGTH      =',F7.1,' FT',26X,'--',44X,'--'/5X,
1'FALL',14X,'=',F7.1,' FT',26X,'--',44X,'--'/5X,'ELEV THROAT INVERT
2=',F7.1,' FT',26X,'--',44X,'--'/5X,'ELEV FACE INVERT  =',F7.1,' FT
3',26X,'--',44X,'--'/5X,'CULVERT SLOPE',5X,'=',F7.4,29X,'--',44X,'-
4-'/5X,'VEL AT DESIGN Q  =',F6.1,' FPS',26X,'--',44X,'--'/5X,'FACE
5 WIDTH'.8X,'=',F7.2,' FT',26X,'--',44X,'--'/5X,'L1',16X,'=',F7.2,
6' FT',26X,'--',44X,'--'/5X,'MIN CREST LENGTH  =',F7.1,' FT',26X,'-
7-',44X,'--'/5X,'BEVELS = 45 DEGREE',36X,'--',44X,'--'/9X,'B =',
8F5.1,' IN  D =',F5.1,' IN',27X,'--',44X,'--'/5X,'Q'.8X,'HWT'.8X,
9'HWF'.32X,'--',44X,'--'/)
QD=Q1-Q1*.2
29 X=QD/(B*D**1.5)
Y16 =.1295033+.3789445*X-.0437778*X*X+.00426329*X*X*X
1-.000106358*X*X*X*X
HWTA=ELTRCA+Y16*D
X=QD/(BF*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFA=ELFACA+Y13*D
WRITE(SYSOT,27)QD,HWTA,HWFA
27 FORMAT(3X,F7.1,2X,F7.1,3X,F7.1,31X,'--',44X,'--')
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 29
30 WRITE(SYSOT,332)TOTA,TOTB,TOTC,TAB13(LL),TBFAL,TCFAL,TAB14(LL),
1ELTRCB,ELTRCC,
2ELFACA,ELFACB,ELFACC,SA,SB,SC,VELAA,VELBB,VELCC,BF,BFB,BFC
332 FORMAT( 5X,'CULVERT LENGTH      =',F7.1,' FT',20X,'CULVERT LENGTH
1 =',F7.1,' FT',15X,'CULVERT LENGTH      =',F7.1,' FT'/
2 5X,'FALL',14X,'=',F7.1,' FT',20X,'FALL',14X,'=',F7.1,' FT',
3 15X,'FALL',14X,'=',F7.1,' FT',5X,'ELEV THROAT INVERT=',F7.1,
4 ' FT',20X,'ELEV THROAT INVERT=',F7.1,' FT',15X,'ELEV THROAT INVER
5T=',F7.1,' FT',5X,'ELEV FACE INVERT  =',F7.1,' FT',20X,'ELEV FACE
6INVERT  =',F7.1,' FT',15X,'ELEV FACE INVERT  =',F7.1,' FT'/ 5X,
7 'CULVERT SLOPE      =',F7.4,23X,'CULVERT SLOPE      =',F7.4,18X,
8 'CULVERT SLOPE      =',F7.4/ 5X,'VEL AT DESIGN Q  =',F6.1,' FPS',
920X,'VEL AT MAX Q      =',F6.1,' FPS',15X,'VEL AT DESIGN Q  =',
AF6.1,' FPS'/ 5X,'FACE WIDTH'.8X,'=',F7.2,' FT',20X,'FACE WIDTH',
B8X,'=',F7.2,' FT',15X,'FACE WIDTH'.8X,'=',F7.1,' FT')
WRITE(SYSOT,504)L1,L1B,L1C,WA,WB,WC,BEA,DEA,BEB,DEB,BEC,DEC
504 FORMAT(
1F7.2,' FT',20X,'L1',16X,'=',F7.2,' FT',15X,'L1',16X,'=',
2/5X,'MIN CREST LENGTH  =',F7.1,' FT',20X,'MIN CREST LENGTH  =',
3F7.1,' FT',15X,'MIN CREST LENGTH  =',F7.1,' FT'/5X,'BEVELS = 45 D
4EGREE',30X,'BEVELS = 45 DEGREE',25X,'BEVELS = 45 DEGREE'/9X,'B =
5',F5.1,' IN  D =',F5.1,' IN',24X,'B =',F5.1,' IN  D =',F5.1,' IN',
622X,'B =',F5.1,' IN  D =',F5.1,' IN',5X,'Q'.8X,'HWT'.8X,'HWF',
729X,'Q'.8X,'HWT'.8X,'HWF',20X,'Q'.8X,'HWT'.8X,'HWF',
QD=Q1-(Q1*.2)
31 X=QD/(B*D**1.5)
Y16 =.1295033+.3789445*X-.0437778*X*X+.00426329*X*X*X

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B 5215  
B 5220  
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B 5445  
B 5450  
B 5455  
B 5460  
B 5465  
B 5470  
B 5475  
B 5480  
B 5485

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1-.000100358*X*X*X*X
HWTB=ELTRCA+(Y16*D)
HWTB=ELTRCB+(Y16*D)
HWTB=ELTRCC+(Y16*D)
X=QD/(BF*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFA=ELFACA+(Y13*D)
X=QD/(BFB*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFB=ELFACB+(Y13*D)
X=QD/(BFC*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFC=ELFACC+Y13*D
WRITE(SYSOT,36)QD,HWTB,HWFA,QD,HWTB,HWFB,QD,HWTB,HWFC
36 FORMAT(3X,F7.1,2X,F7.1,2X,F7.1,22X,F9.1,1X,F9.1,3X,F9.1,13X,
12F9.1,2X,F9.1)
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 31
32 WRITE(SYSOT,110)TOTA,TOTB,TAB13(LL),TBFAL,TAB14(LL),ELTRCB,ELFACA,
1ELFACB,SA,SB,VELAA,VELBB,BF,BFB
110 FORMAT(5X,'CULVERT LENGTH =',F7.1,' FT',20X,'CULVERT LENGTH
1=',F7.1,' FT',2X,'--'/5X,'FALL',14X,'=',F7.1,' FT',20X,'FALL',14X
2=',F7.1,' FT',21X,'--'/5X,'ELEV THROAT INVERT=',F7.1,' FT',20X,
3'ELEV THROAT INVERT=',F7.1,' FT',21X,'--'/ 5X,'ELEV FACE INVERT
4=',F7.1,' FT',20X,'ELEV FACE INVERT =',F7.1,' FT',21X,'--'/ 5X,
5'CULVERT SLOPE',5X,'=',F7.4,23X,'CULVERT SLOPE',5X,'=',F7.4,24X,'-
6-'/ 5X,'VEL AT DESIGN Q =',F6.1,' FPS',20X,'VEL AT MAX Q =
7',F6.1,' FPS',21X,'--'/ 5X,'FACE WIDTH',8X,'=',F7.2,' FT',20X,'
8FACE WIDTH',8X,'=',F7.2,' FT',21X,'--')
WRITE(SYSOT,112)L1,L1B,WA ,WB,BEA,DEA,BEB,DEB
112 FORMAT(5X,'L1',16X,'=',F7.2,' FT',20X,'L1',16X,'=',F7.2,' FT',21X,
1'--'/ 5X,'MIN CREST LENGTH =',F7.1,' FT',20X,'MIN CREST LENGTH
2=',F7.1,' FT',21X,'--'/5X,'BEVELS = 45 DEGREE',31X,'BEVELS = 45
3DEGREE',30X,'--'/9X,'B =',F5.1,' IN D =',F5.1,' IN',25X,'B =',
4F5.1,' IN D =',F5.1,' IN',22X,'--'/5X,'Q',8X,'HWT',8X,'HWF',
529X,'Q',8X,'HWT',8X,'HWF',24X,'--'/)
QD=Q1-Q1*.2
33 X=QD/(B*D**1.5)
Y16 =.1295033+.3789445*X-.0437778*X*X+.00426329*X*X*X
1-.000100358*X*X*X*X
HWTB=ELTRCA+Y16*D
HWTB=ELTRCB+Y16*D
X=QD/(BF*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFA=ELFACA+Y13*D
X=QD/(BFB*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFB=ELFACB+Y13*D
WRITE(SYSOT,38)QD,HWTB,HWFA,QD,HWTB,HWFB

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B 5490
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B 5750
B 5755
B 5760

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38 FORMAT(3X,F7.1,2X,F7.1,3X,F7.1,22X,F9.1,1X,F9.1,3X,F9.1,
122X,'--')
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 33
34 WRITE(SYSOT,106)TOTA,TOTC,TAB13(LL),TCFAL,TAB14(LL),ELTRCC,ELFACA
1,ELFACC,SA,SC,VELAA,VELCC,BF,BFC,L1,L1C,WA,WC,BEA,DEA,BEC,DEC
106 FORMAT(5X,'CULVERT LENGTH'='F7.1,'FT',.26X,'--',.36X,'CULVERT L
LENGTH'='F7.1,'FT'/5X,'FALL',.14X,'='F7.1,'FT',.26X,'--',.36X,
2'FALL',.14X,'='F7.1,'FT'/5X,'ELEV THROAT INVERT='F7.1,'FT',.26X,
3'--',.36X,'ELEV THROAT INVERT='F7.1,'FT'/5X,'ELEV FACE INVERT'='
5,F7.1,'FT',.26X,'--',.36X,'ELEV FACE INVERT'='F7.1,'FT'/5X,'CUL
6VERT SLOPE',5X,'='F7.4,29X,'--',.36X,'CULVERT SLOPE',5X,'='F7.4/
75X,'VEL AT DESIGN Q'='F7.1,'FPS',.26X,'--',.36X,'VEL AT DESIGN Q
8'='F7.1,'FPS'/5X,'FACE WIDTH',8X,'='F7.2,'FT',.26X,'--',.36X,'FA
9CE WIDTH',8X,'='F7.2,'FT'/5X,'L1',.16X,'='F7.2,'FT',.26X,'--',
A36X,'L1',.16X,'='F7.2,'FT'/5X,'MIN CREST LENGTH'='F7.1,'FT',
B26X,'--',.36X,'MIN CREST LENGTH'='F7.1,'FT'/5X,'BEVELS = 45 DEGR
CEE',37X,'--',.36X,'BEVELS = 45 DEGREE'/9X,'B'='F5.1,'IN' D ='
DF5.1,'IN',.27X,'--',.41X,'B'='F5.1,'IN' D ='F5.1,'IN'//5X,'Q',
E8X,'HWT',8X,'HWF',32X,'--',.38X,'Q',8X,'HWT',8X,'HWF'/)
QD=Q1-(Q1*.2)
35 X=QD/(B*D**1.5)
Y16 =.1295033+.3789445*X-.0437778*X*X+.00426329*X*X*X
1-.000106358*X*X*X*X
HWTA=ELTRCA+Y16*D
HWTC=ELTRCC+Y16*D
X=QD/(3F*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFA=ELFACA+Y13*D
X=QD/(BFC*D**1.5)
Y13=.11111164+.53786558*X-.10516936*X*X+.016074687*X*X*X
1-.0006418302*X*X*X*X
HWFC=ELFACC+Y13*D
WRITE(SYSOT,37)QD,HWTA,HWFA,QD,HWTC,HWFC
37 FORMAT(3X,F7.1,2X,F7.1,3X,F7.1,31X,'--',.33X,2F9.1,2X,F9.1)
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 33
480 RETURN
END

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B 5765
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B 5960
B 5965
B 5970

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	SUBROUTINE BSLOPV(B,D,SLOPE)	B 5975
	DESIGN SLOPE-TAPERED INLETS	B 5980
C		B 5985
C		B 5990
	COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),	B 5995 **
	1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),	B 6000 **
	2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),	B 6005 **
	3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),	B 6010 **
	4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),	B 6015 **
	5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,	B 6020 **
	6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),	B 6025 **
	7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),	B 6030 **
	8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),	B 6035 **
	9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,	B 6040 **
	ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2	B 6045
	DIMENSION FALL(2),S(2),L1(2),L2(2),L3(2),VEL(2),BF(2),	B 6050
	1TAPER(2),NOC(2),DA(2)	B 6055
	INTEGER SYSIN, SYSOT	B 6060
	RFAL L1,L2,L3,L4,L150	B 6065
	DATA ALPHA,SCORR,CN/1.0,.5,.012/	B 6070
460	ISLOPE=0	B 6075
	HW=0.0	B 6080
	QS=Q1	B 6085
	BAR=ITAB(LL)	B 6090
	NOC(1)=0	B 6095
	NOC(2)=0	B 6100
	I=1	B 6105
	TAPER(1)=4.0	B 6110
	TAPER(2)=4.0	B 6115
	Y1=(D**2/(SFACE**2+1.))**.5	B 6120
	Y2=Y1/SFACE	B 6125
	DY=SFACE*Y1+Y2	B 6130
	SMAL3=(SLOPE*SEL**2+DY)/(1.+SLOPE*SEL)	B 6135
	DIL3=SEL*DY-SMAL3	B 6140
	EL3=DIL3*SLOPE	B 6145
	FACEL=ELIN-EL3	B 6150
	TOEL=ELOUT+ELR	B 6155
	DIST=(FACEL-TOEL)/SLOPE	B 6160
C		B 6165
C		B 6170
	CURVE A	B 6175
	IF (TAB14(LL).EQ.0.0)NOC(2)=1	B 6180
	IF (TRDE.LE.TDEL) NOC(1)=1	B 6185
14	FALL(I)=FACEL+TRDE	B 6200
	IF (FALL(I).LT.(D*.4.).OR.FALL(I).GT.(1.5*D))NOC(1)=1	B 6205
	IF (NOC(1).EQ.1) GO TO 48!	B 6210
24	HW=HWTEMP-FACEL	B 6215
	X=HW/D	B 6220
C.....	FACE EQUATION - CHART 16 - HEC 13	B 6225
	Y21=-2.2658.3+7.942441*X-4.0350294*X*X+1.619481*X*X*X-.3458214*X	B 6230
	1*X*X*X+.02846767*X*X*X*X*X	B 6235
	BF(I)=QS/(Y21*D**1.5)+.1	B 6240
	L1(I)=((BF(I)-B)/2.)*TAPER(I)	B 6245
26	S(I)=(TRDE-TOEL)/(DIST-L1(I))	B 6250
	DIF=FACEL+DY-(TRDE+(D**2+(D*S(I))**2)**.5)	B 6255

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L3(I)=.5*B
28 L2(I)=L1(I)-L3(I)
SF=L2(I)/((DIF-S(I)*L1(I)+L2(I)*S(I))
IF(SF.EQ.SFACE) GO TO 450
IF(SF.LT.SFACE) GO TO 30
SF=SFACE
L2(I)=SFACE*(DIF-S(I)*L1(I))/(1.-S(I)*SFACE)
L3(I)=L1(I)-L2(I)
IF(L3(I).LT.(.5*B)) L3(I)=.5*B
L2(I)=L1(I)-L3(I)
GO TO 450
30 SF=SFACE
L2(I)=SFACE*(DIF-S(I)*L1(I))/(1.-S(I)*SFACE)
L1(I)=L2(I)+L3(I)
TAPER(I)=2.*L1(I)/(BF(I)-B)
450 S(I)=(TROE-TOEL)/(DIST-L1(I))
SLO=S(I)
DA(I)=DIST-L1(I)
DD=DA(I)
Q=QS/BB
BB=B/BB
CALL BCUT(Q, BB, D, HWOUT, VELOUT, DEP, DN, DC, Z, DIST, TOEL, QMAX, SLO)
CALL BNORM(Q, CN, SLO, BB, D, DEP, AREA, WP)
VELIN=Q/AREA
VEL(I)=VELIN
IF(VELOUT.GT.VELIN) VEL(I)=VELOUT
IF(DN.GE.DC) GO TO 122
IF(DTW.LT.DC) GO TO 122
IF(WHY2.GT.DTW) GO TO 122
WHY2=0.247*VELIN*DN*.5-(.5*DN)
IF(DTW.GE.D) VEL(I)=Q/(BB*D)
IF(DTW.LT.D) VEL(I)=Q/(BB*DTW)
122 I=I+1
481 Q=Q-QUE
TROE=ELTRCB
I=I+1
IF(I.EQ.3) GO TO 483
GO TO 14
483 WRITE(SYSOT,478) DIL3,DISR
478 FORMAT(///1X, 'SLOPE TAPERED INLET DESIGN - VERTICAL FACE', '*****
1*****'//5X, 'DISTANCE EMBANKMENT-TO
2E TO FACE =', F7.2, ' FT', '10X, 'CULVERT OUTLET TO EMBANKMENT-TOE =',
3 F7.2, ' FT'//10X, 'MIN FALL DESIGN', 35X, 'MAX Q DESIGN')
IF(NOC(1).EQ.1.AND.NOC(2).EQ.1) GO TO 484
IF(NOC(1).EQ.1.AND.NOC(2).EQ.0) GO TO 486
IF(NOC(1).EQ.0.AND.NOC(2).EQ.1) GO TO 488
340 WRITE(SYSOT,342)DIST, DIST, FALL(1), FALL(2), TROEL, ELTRCB, FACEL,
9'HWF', 34X, 'Q', 8X, 'HWT', 8X, 'HWF'//
QD=Q1-Q1*.2
1FACEL, S(1), S(2), VEL(1), VEL(2), BF(1), BF(2), L1(1), L1(2), L2(1), L2(2),
2L3(1), L3(2), SFACE, SFACE, TAPER(1), TAPER(2)
342 FORMAT(///5X, 'CULVERT LENGTH =', F7.1, ' FT', 25X, 'CULVERT LENGTH
1 =', F7.1, ' FT'//5X, 'FALL', 14X, '=', F7.1, ' FT', 25X, 'FALL', 14X, '=',
2F7.1, ' FT'//5X, 'ELEV THROAT INVERT =', F7.1, ' FT', 25X, 'ELEV THROAT IN
3VERT =', F7.1, ' FT'//5X, 'ELEV FACE INVERT =', F7.1, ' FT', 25X, 'ELEV FA

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B 6480
B 6485
B 6490
B 6495
B 6500
B 6505
B 6510
B 6515
B 6520

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4CE INVERT =',F7.1,' FT'/ 5X,'CULVERT SLOPE      =',F7.4.28X,'CULVE B 6525
5RT SLOPE  =',F7.4/5X,'VEL AT DESIGN Q    =',F6.1,' FT',.26X,'VEL B 6530 **
6AT MAX Q   =',F6.1,' FT'/5X,'FACE WIDTH'.8X,'=',F7.2,' FT', B 6535
725X,'FACE WIDTH'.8X,'=',F7.2,' FT'/5X,'L1',.15X,'=', B 6540
8F7.2,' FT',.25X,'L1',.16X,'=',F7.2,' FT' B 6545
9/5X,'L2',.16X,'=',F7.1,' FT',.25X,'L2',.16X,'=',F7.1,' FT' B 6550
A           /5X,'L3',.16X,'=',F7.1,' FT',.25X,'L3',.16X,'=', B 6555
BF7.1,' FT'/5X, B 6560
C 'SF',.16X,'=',F7.2.28X,'SF',.16X,'=',F7.2/ B 6565
D 5X,'TAPER'.3X,'=',F5.2,' :1',.28X,'TAPER',.13X,'=',F5.2,' :1'//8X, B 6570
E'Q'.8X,'HWT'.8X,'HWF'.34X,'Q'.8X,'HWT'.8X,'HWF'/) B 6575
QD=Q1-Q1*.2 B 6580
31 X=QD/(B*D**1.5) B 6585
Y16=.12950325+.37894446*X-.04377779*X*X+.00426329*X*X*X B 6590
1-.00010635862*X*X*X+X B 6595
HWTA=TRDEL+Y16*D B 6600
HWTB=ELTRCB+Y16*D B 6605
X=QD/(BF(1)*D**1.5) B 6610
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X B 6615
1-.000496383*X*X*X+X B 6620
HWFA=FACEL+Y18*D B 6625
X=QD/(BF(2)*D**1.5) B 6630
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X B 6635
1-.000496383*X*X*X+X B 6640
HWFB=FACEL+Y18*D B 6645
WRITE(SYSOT,32)QD,HWTA,HWFA,QD,HWTB,HWFB B 6650
32 FORMAT(1X,3F10.1,30X,3F10.1) B 6655 **
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480 B 6660
QD=QD+Q1*.2 B 6665
GO TO 31 B 6670
484 WRITE(SYSOT,485) B 6675
485 FORMAT(///20X,'NO SLOPE TAPERED INLET - VERTICAL FACE - DESIGN APP B 6680
'CALCABLE') B 6685
GO TO 480 B 6690
486 WRITE(SYSOT,487)DIST, FALL(2),ELTRCB,FACEL,S(2),VEL(2),BF(2), B 6695
2L1(2),L2(2),L3(2),SPACE,TAPER(2) B 6700
487 FORMAT(//16X,'- -',.40X,'CULVERT LENGTH      =',F7.1,' FT' /16X,'- -' B 6705
1,.40X, B 6710
2',.15X,'=',F7.1,' FT'/16X,'- -',.40X,'ELEV THROAT INVERT=' F7.1 B 6715
3,' FT'/16X,'- -',.40X,'ELEV FACE INVERT =',F7.1,' FT'/16X,'- -',.40 B 6720
4X,'CULVERT SLOPE      =',F9.4/16X,'- -',.40X,'VEL AT MAX Q      =', B 6725
5F6.1,' FPS'/16X,'- -',.40X,'FACE WIDTH'.8X,'=',F7.2,' FT'/16X,'- -' B 6730
6,.40X,'L1',.16X,'=',F7.2,' FT'/16X,'- -',.40X,'L2',.16X,F7.1,' FT' B 6735
7/16X,'- -',.40X,'L3',.16X,'=',F7.1,' FT'/16X,'- -',.40X,'SF',.16X,'=' B 6740
8F9.2/16X,'- -',.40X,'TAPER',.13X,'=',F5.2,' :1'//8X,'Q'.8X,'HWT'.8X, B 6745
9 B 6750
33 X=QD/(B*D**1.5) B 6755
Y16=.12950325+.37894446*X-.04377779*X*X+.00426329*X*X*X B 6760
1-.00010635862*X*X*X+X B 6765
HWTB=ELTRCB+Y16*D B 6770
X=QD/(BF(2)*D**1.5) B 6775
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X B 6780
1-.000496383*X*X*X+X B 6785
HWFB=FACEL+Y18*D B 6790
WRITE(SYSOT,34)QD,HWTB,HWFB B 6795
34 FORMAT(16X,'- -',.40X,3F10.1)

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IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 33
488 WRITE(SYSOT,489)DIST, FALL(1),TROEL,FACEL,S(1),VEL(1),BF(1),L1(1),
1L2(1),L3(1),SPACE,TAPER(1)
489 FORMAT(/5X,'CULVERT LENGTH' =',F7.1,' FT',30X,'--'/5X,'FALL',14
1X,'=',F7.1,' FT',30X,'--'/5X,'ELEV THROAT INVERT=',F7.1,' FT',30X
3,'--'/5X,'ELEV FACE INVERT' =',F7.1,' FT',30X,'--'/5X,'CULVERT S
4LOPE' =',F9.4,33X,'--'/5X,'VEL AT DESIGN Q' =',F6.1,' FPS',
530X,'--'/5X,'FACE WIDTH',8X,'=',F7.2,' FT',30X,'--'/5X,'L1',16X,
6=' ',F7.2,' FT',30X,'--'/5X,'L2',16X,'=',F7.1,' FT',30X,'--'/5X,
7'L3',16X,'=',F7.1,' FT',30X,'--'/5X,'SF',16X,'=',F9.2,33X,'--'/
85X,'TAPER',13X,'=',F5.2,' :1'//8X,'Q',8X,'HWT',8X,'HWF',34X,'Q',8X,
9'HWT',8X,'HWF'/)
QD=Q1-Q1*.2
35 X=QD/(B*D*.1.5)
Y16=.12950325+.37894446*X-.04377779*X*X+.00426329*X*X*X
1-.00010635862*X*X*X*X
HWTA=TROEL+Y16*D
X=QD/(BF(1)*D*.1.5)
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X
1-.000496383*X*X*X*X
HWFA=FACEL+Y18*D
WRITE(SYSOT,36)QD,HWTA,HWFA
36 FORMAT(1X,3F10.1,40X,'--')
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 35
460 RETURN
END

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B 6800  
B 6805  
B 6810  
B 6815  
B 6820  
B 6825  
B 6830  
B 6835  
B 6840  
B 6845  
B 6850  
B 6855  
B 6860  
B 6865  
B 6870  
B 6875  
B 6880  
B 6885  
B 6890  
B 6895  
B 6900  
B 6905  
B 6910  
B 6915  
B 6920  
B 6925  
B 6930  
B 6935  
B 6940  
B 6945

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SUBROUTINE BSLOPM(B,D,SLOPE)
DESIGN SLOPE-TAPERED INLETS - MITERED FACE

COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),
3TOMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),
4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),
5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),
8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,
ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2
DIMENSION FALL(2),S(2),L1(2),L2(2),L3(2),VEL(2),BF(2),L4(2),
1TAPER(2),NOC(2),CL(2)
INTEGER SYSIN, SYSOT
REAL L1,L2,L3,L4,L150,L2L3
DATA ALPHA,SCORR,CN/1.0,.5,.012/
HW=0.0
SF=SFACE
QS=Q1
BAR=ITAB(LL)
NOC(1)=0
NOC(2)=0
I=1
TAPER(1)=4.0
TAPER(2)=4.0
TOEL=ELOUT+ELR
FACE=ELIN-E
DIST=(ELIN-TOEL)/SLOPE
TROEL=TAB14(LL)
TROE=TROEL
Y=(D*(SF*SEL-1))/((SF+SEL)*(1+SF**2)**.5)
FACEL=ELIN-Y
14 FALL(I)=ELIN-TROE
IF(TAB14(LL).EQ.0.0)NOC(2)=1
IF(FACEL.LT.TROE) NOC(I)=1
IF(TROE.LE.TOEL) NOC(I)=1
IF(FALL(I).LT.(D/4.+Y).OR.FALL(I).GT.(1.5*D))NOC(I)=1
IF(NOC(I).EQ.1) GO TO 481
24 HW=HWTEMP-FACEL
X=HW/D
Y21=-2.265863+7.942141*X-4.0350294*X*X+1.619481*X*X*X-.3458214*X
1+X*X*X+.02846737*X*X*X-X*X
L4(I)=D*SEL*(1+SF**2)**.5/(SEL+SF)
BF(I)=QS/(Y21+D**1.5)+.1
XL4=(D**2/(1.+SF**2))**.5
SFX=SF*XL4
L2L3=((BF(I)-B)/2.)*TAPER(I)
L1(I)=L2L3+L4(I)
26 S(I)=(TROE-TOEL)/(DIST-L1(I))
DIFF=TROE+(D**2+(D*S(I))**2)**.5
DIF=FACEL+SFX-DIFF
L3(I)=.5*B

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B 6950
B 6955
B 6960
B 6965 **
B 6970 **
B 6975 **
B 6980 **
B 6985 **
B 6990 **
B 6995 **
B 7000 **
B 7005 **
B 7010 **
B 7015 **
B 7020
B 7025
B 7030
B 7035
B 7040
B 7045
B 7050
B 7055
B 7060
B 7065
B 7070
B 7075
B 7080
B 7085
B 7090
B 7095
B 7100
B 7105
B 7110
B 7115
B 7120
B 7125
B 7130 **
B 7135
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B 7145
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B 7180
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B 7195
B 7200
B 7205
B 7210
B 7215
B 7220

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28 L2(I)=L1(I)-L3(I)-L4(I)
SF=L2(I)/(DIF-S(I)*(L1(I)-L4(I)-L2(I)))
IF(SF.EQ.SFACE) GO TO 450
IF(SF.LT.SFACE) GO TO 30
SF=SFACE
L2(I)=(SF*(DIF-S(I)*L1(I)+S(I)*L4(I)))/(1.-SF*S(I))
L3(I)=L1(I)-L2(I)-L4(I)
GO TO 450
30 SF=SFACE
L2(I)=(SF*(DIF-S(I)*L1(I)+S(I)*L4(I)))/(1.-SF*S(I))
L1(I)=L2(I)+L3(I)+L4(I)
TAPER(I)=2.*(L2(I)+L3(I))/(BF(I)-B)
450 S(I)=(TROE-TOEL)/(DIST-L1(I))
SLO=S(I)
CL(I)=DIST-L1(I)
Q=QS/BAR
BB=B/BAR
DA=CL(I)
CALL BOUT(Q, BB, D, HWOUT, VELOUT, DEP, DN, DC, Z, DIST, TOEL, QMAX, SLO)
CALL BNORM(Q, CN, SLO, BB, D, DEP, AREA, WP)
VELIN=Q/AREA
VEL(I)=VELIN
IF(VELOUT.GT.VELIN) VEL(I)=VELOUT
IF(DN.GE.DC) GO TO 122
IF(DTW.LT.DC) GO TO 122
WHY2=0.247*VELIN*DN**.5-(.5*DN)
IF(WHY2.GT.DTW) GO TO 122
IF(DTW.GE.D) VEL(I)=Q/(BB*D)
IF(DTW.LT.D) VEL(I)=Q/(BB*DTW)
122 IBAR=BAR
481 QS=QUE
TROE=ELTRCB
I=I+1
IF(I.EQ.3) GO TO 483
GO TO 14
483 WRITE(SYSOT,478)
478 FORMAT(///1X,'SLOPE TAPERED INLET DESIGN - MITERED FACE'/'*****
1*****'//10X,'MIN FALL DESIGN'.35X,
2'MAX Q DESIGN')
IF(NOC(1).EQ.1.AND.NOC(2).EQ.1) GO TO 484
IF(NOC(1).EQ.1.AND.NOC(2).EQ.0) GO TO 486
IF(NOC(1).EQ.0.AND.NOC(2).EQ.1) GO TO 488
340 WRITE(SYST,342)DIST,DIST, FALL(1),FALL(2),TROEL,ELTRCB,FACEL,
1FACEL,S(1),S(2),VEL(1),VEL(2),BF(1),BF(2),L1(1),L1(2),L2(1),L2(2),
2L3(1),L3(2)
342 FORMAT(/5X,'CULVERT LENGTH =',F7.1,' FT',25X,'CULVERT LENGTH
1 =',F7.1,' FT',5X,'FALL',14X,'=',F7.1,' FT',25X,'FALL',14X,'=',F7
2.1,' FT',5X,'ELEV THROAT INVERT=',F7.1,' FT',25X,'ELEV THROAT INV
3ERT=',F7.1,' FT',5X,'ELEV FACE INVERT =',F7.1,' FT',25X,'ELEV F
4ACE INVERT =',F7.1,' FT',5X,'CULVERT SLOPE =',F7.4,28X,'CULVE
5RT SLOPE =',F7.4/5X,'VEL AT DESIGN Q =',F6.1,' FPS',25X,'VEL
6 AT MAX Q =',F6.1,' FPS',5X,'FACE WIDTH',8X,'=',F7.2,' FT',25
7X,'FACE WIDTH',8X,'=',F7.2,' FT',5X,'L1',16X,'=',F7.2,' FT',25X,'L
81',16X,'=',F7.2,' FT',5X,'L2',16X,'=',F7.1,' FT',25X,'L2',16X,'='
9F7.1,' FT',5X,'L3',16X,'=',F7.1,' FT',25X,'L3',16X,'=',F7.1,' FT')

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B 7225
B 7230
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B 7485
B 7490
B 7495

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WRITE(SYSOT,346)L4(1),L4(2),SFACE,SFACE,TAPER(1),TAPER(2)
346 FORMAT(5X,'L4',16X,'=',F7.1,' FT',25X,'L4',16X,'=',F7.1,' FT'/5X,
1'SF',16X,'=',F7.2,28X,'SF',16X,'=',F7.2/5X,'TAPER',13X,'=',F5.2,
2':1',28X,'TAPER',13X,'=',F5.2,' :1'//8X,'Q',8X,'HWT',8X,'HWF',34X,
3'Q',8X,'HWT',8X,'HWF'/)
QD=Q1-Q1*.2
31 X=QD/(B*D**1.5)
Y16=.12950325+.37894446*X-.04377779 *X*X+.00426329*X*X*X
1-.0001063586*X*X*X*X
HWTA=TROEL+Y16*D
HWTB=ELTRCB+Y16*D
X=QD/(BF(1)*D**1.5)
Y18=.1379509+.42974097*X-.07646745 *X*X+.012651097*X*X*X
1-.000496383*X*X*X*X
HWFA=FACEL+Y18*D
X=QD/(BF(2)*D**1.5)
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X
1-.000496383*X*X*X*X
HWFB=FACEL+Y18*D
WRITE(SYSOT,32)QD,HWTA,HWFA,QD,HWTB,HWFB
32 FORMAT(1X,3F10.1,24X,3F10.1)
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 31
484 WRITE(SYSOT,485)
485 FORMAT(//20X,'NO SLOPE TAPERED MITERED INLET DESIGN APPLICABLE')
GO TO 480
486 WRITE(SYSOT,487)DIST, FALL(2),ELTRCB,FACEL,S(2),VEL(2),BF(2),L1(2)
2,L2(2),L3(2),L4(2),SFACE,TAPER(2)
487 FORMAT(//10X,'MIN FALL DESIGN',35X,'MAX Q DESIGN'//16X,'- -.40X,
1'CULVERT LENGTH =',F7.1,' FT'/16X,'- -.40X,
2'FALL',15X,'=',F7.1,' FT'/16X,'- -.40X,'ELEV THROAT INVERT=',F7.1
3,' FT'/16X,'- -.40X,'ELEV FACE INVERT =',F7.1,' FT'/16X,'- -.40
4X,'CULVERT SLOPE =',F9.4/16X,'- -.40X,'VEL AT MAX Q =',
5F6.1,' FPS'/16X,'- -.40X,'FACE WIDTH',8X,'=',F7.2,' FT'/16X,'- -.
6,40X,'L1',16X,'=',F7.2,' FT'/16X,'- -.40X,'L2',16X,'=',F7.1,
7,' FT'/16X,'- -.40X,'L3',16X,'=',F7.1,' FT'/16X,'- -.40X,'L4',
816X,'=',F7.1,' FT'/
16X,'- -.40X,'SF',16X,'=',
9F9.2,16X,'- -.40X,'TAPER',13X,'=',F5.2,' :1'//8X,'Q',8X,'HWT',8X,
A'HWF',34X,'Q',8X,'HWT',8X,'HWF'/)
QD=Q1-Q1*.2
33 X=QD/(B*D**1.5)
Y16=.12950325+.37894446*X-.04377779*X*X+.00426329*X*X*X
1-.0001063586*X*X*X*X
HWTB=ELTRCB+Y16*D
X=QD/(BF(2)*D**1.5)
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X
1-.000496383*X*X*X*X
HWFB=FACEL+Y18*D
WRITE(SYSOT,34)QD,HWTB,HWFB
34 FORMAT(16X,'- -.40X,3F10.1)
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 33
488 WRITE(SYSOT,489)DIST, FALL(1),TROEL,FACEL,S(1),VEL(1),BF(1),L1(1),

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B 7500  
B 7505  
B 7510  
B 7515  
B 7520  
B 7525  
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B 7545  
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B 7555  
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B 7725  
B 7730  
B 7735  
B 7740  
B 7745  
B 7750  
B 7755  
B 7760  
B 7765  
B 7770

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1L2(1),L3(1),L4(1),SFACE,TAPER(1)
489 FORMAT( //10X,'MIN FALL DESIGN',35X,'MAX Q DESIGN'//5X,'CULVERT LE
1NGTH' =',F7.1,' FT',30X,'- -'/
2',F7.1,' FT',30X,'- -'/5X,'ELEV THROAT INVERT=',F7.1,' FT',30X,'- -'/
35X,'ELEV FACE INVERT' =',F7.1,' FT',30X,'- -'/5X,'CULVERT SLOPE
4' =',F9.4,31X,'- -'/5X,'VEL AT DESIGN Q' =',F6.1,' FPS',29X,
5'- -'/5X,'FACE WIDTH',8X,'=',F7.2,' FT',30X,'- -'/5X,'L1',16X,'=',
6F7.2,' FT',30X,'- -'/5X,'L2',16X,'=',F7.1,' FT',30X,'- -'/5X,'L3',
716X,'=',F7.1,' FT',30X,'- -'/5X,'L4',16X,'=',F7.1,' FT',30X,'- -'/
85X,'SF',16X,'=',F9.2,31X,'- -'/5X,'TAPER',13X,'=',F5.2,' :1',25X,
9'--'//8X,'Q',8X,'HWT',8X,'HWF',34X,'Q',8X,'HWT',8X,'HWF'/)
QD=Q1-Q1*.2
35 X=QD/(B*D*.1.5)
Y16=.12950325+.37894446*X-.04377779*X*X+.00426329*X*X*X
1-.00010635862*X*X*X*X
HWTA=TRDEL+Y16*D
X=QD/(BF(1)*D*.1.5)
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X
1-.000496383*X*X*X*X
HWFA=FACEL+Y18*D
WRITE(SYSOT,36)QD,HWTA,HWFA
36 FORMAT(1X,3F10.1,40X,'--')
IF(QD.GT.(Q1+2*(Q1*.2)+5.)) GO TO 480
QD=QD+Q1*.2
GO TO 35
480 RETURN
END

```

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B 7775
B 7780
B 7785
B 7790 **
B 7795
B 7800 **
B 7805
B 7810
B 7815
B 7820 **
B 7825 **
B 7830
B 7835
B 7840
B 7845
B 7850
B 7855
B 7860
B 7865
B 7870
B 7875
B 7880
B 7885
B 7890
B 7895
B 7900
B 7905

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	SUBROUTINE BOUT(QADJ,B,D,WHW,VEL,DEP,DSUBN,DSUBC,Z,DIST,TOEL,	B 7910
	1QMAX,SLOPE)	B 7915
	COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),	B 7920
	1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),	B 7925 **
	2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),	B 7930 **
	3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),	B 7935 **
	4L,LL,K,SYIN,SYST,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),	B 7940 **
	5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,	B 7945 **
	6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),	B 7950 **
	7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),	B 7955 **
	8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),	B 7960 **
	9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,	B 7965 **
	ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2	B 7970 **
	DIMENSION CKE(4),V(2),R(2),SPH(2)	B 7975
	DATA CKE/.4,.5,.7,.2/,ALPHA,SCORR,CN/1.0,.5,.012/	B 7980
C		B 7985
C	OUTLET CONTROL COMPUTATIONS	B 7990
	410 CALL BNORM%QADJ,CN,SLOPE,B,D,DEP,AREA,WP<	B 7995
	585 DSUBN # DEP	B 8000
	AREA # B*D	B 8005
	HR # AREA*.2.*D&B<<	B 8010
	HEAD # QADJ/10.<.*QADJ/10.<.*%1.555*%1.&CKE%I4<<</%AREA*	B 8015
	1AREA<8.45.095*CN*CH*DIST/%AREA*AREA*HR**1.333333<<<	B 8020
	DSUBC # .315*%QADJ/B<*.666667	B 8025
	IF %DSUBC-D< 630,630,620	B 8030
	620 DSUBC # D	B 8035
	630 TEMP # %DSUBC&D</2.	B 8040
	IF %DTW-TEMP< 640,640,650	B 8045
	640 HO # TEMP	B 8050
	GO TO 655	B 8055
	650 HO # DTW	B 8060
	655 WHW # HO&HEAD	B 8065
	656 IF(WHW.LE.0) GO TO 710	B 8070
	690 TEMP # D&%1.&CKE%I4<<.*%QADJ*QADJ</%64.4*AREA*AREA<<	B 8075
	IF %WHW-TEMP< 710,700,700	B 8080
	700 GO TO 900	B 8085
	710 K22 # 0	B 8090
C		B 8095
C	TEST FOR INLET CONTROL GOVERNS	B 8100
C		B 8105
	IF %DSUBN-DSUBC< 900,720,720	B 8110
	720 IF %DTW-DSUBC< 730,730,725	B 8115
	725 IF %DTW-DSUBC< 740,740,735	B 8120
	730 DEP # DSUBC	B 8125
	GO TO 750	B 8130
	735 K22 # 1	B 8135
	740 DEP # DTW	B 8140
	750 I # 1	B 8145
	SUMX # 0.	B 8150
	IF %DEP-D<700,751,752	B 8155
	751 IF %K22<752,700,752	B 8160
	752 DEP # DTW - SLOPE * DIST	B 8165
	IF %DEP-D<SUBN<753,753,754	B 8170
	753 DEP # DSUBN	B 8175
	754 K22 # -1	B 8180

	I # 1	B 8185
C		B 8190
C	BACKWATER COMPUTATIONS	B 8195
C		B 8200
	760 AREA # DEP*9	B 8205
	V%I< # QADJ/AREA	B 8210
	SPH%I< # DEP&ALPHA+V%I<*V%I</64.4	B 8215
	R%I< # AREA/%2.*DEP<B<	B 8220
	770 IF %I-2< 780,790,790	B 8225
	780 I # 2	B 8230
	IF %K22< 800,781,782	B 8235
	781 DEP # DEP&.2	B 8240
	IF %DEP-D<760,700,700	B 8245
	782 DEP # DEP-.2	B 8250
	GO TO 760	B 8255
	790 AVEV # %V%1<&V%2<</2.	B 8260
	AVER # %R%1<&R%2<</2.	B 8265
	S. # CN+CN-AVEV-AVEV/%2.21*AVER**1.33333<	B 8270
	IF %K22< 795,795,790	B 8275
	795 IF %S1-SLOPE<753,753,810	B 8280
	796 IF %SLOPE-S1<753,753,811	B 8285
	800 SPH%2< # SPH%1<	B 8290
	WHV # SPH%2<&CKE%I4<+V%1<+V%1</64.4	B 8295
	GO TO 700	B 8300
	810 DX1 # %SPH%2<-SPH%1<</%S1-SLOPE<	B 8305
	GO TO 812	B 8310
	811 DX1 # %SPH%1<-SPH%2<</%SLOPE - S1<	B 8315
	8.2 SUMX # SUMX&DX1	B 8320
	IF %SUMX-CLTH< 800,813,813	B 8325
	813 IF %K22<815,814,815	B 8330
	814 DEP # DEP-%SUMX-CLTH</DX1*.2	B 8335
	GO TO 754	B 8340
	815 DEP # DEP&%SUMX-CLTH</DX1*.2	B 8345
	GO TO 754	B 8350
	820 V%1< # V%2<	B 8355
	SPH%1< # SPH%2<	B 8360
	R%1< # R%2<	B 8365
	GO TO 780	B 8370
	900 IF (D.LT.DSUBC) GO TO 1020	B 8375
	1010 IF %DTW-D< 1030,1020,1020	B 8380
	1020 AREA # B*D	B 8385
	GO TO 1060	B 8390
	1030 IF %DSUBC-DTW< 1050,1050,1040	B 8395
	1040 AREA # B*DSUBC	B 8400
	GO TO 1060	B 8405
	1050 AREA # B*DTW	B 8410
	1060 VEL # QADJ/AREA	B 8415
	RETURN	B 8420
	END	B 8425

SUBROUTINE BFIT(Q,B,D,QMAX,TOEL,SLOPE)	B 8430
COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),	B 8435 **
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),	B 8440 **
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),	B 8445 **
3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),	B 8450 **
4L,LL,K,SYISIN,SYISOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),	B 8455 **
5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,	B 8460 **
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),	B 8465 **
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),	B 8470 **
8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),	B 8475 **
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,	B 8480 **
ADIA1,ADIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2	B 8485 **
DIMENSION CKE(4)	B 8490
DATA CKE/.4,.5,.7,.2/,CN/.012/	B 8495
DIST=CLTH	B 8500
A=50:	B 8505
10 Q=Q+A	B 8510
AREA=B*D	B 8515
HR=AREA/(2.*(B+D))	B 8520
HD=(Q/10.)*(Q/10.)*((1.555*(1.+CKE(I4)))/(AREA*AREA)+(45.095*CN*	B 8525
1CN+DIST/(AREA*AREA*HR**1.333333)))	B 8530
DC=.315*(Q/B)**.666667	B 8535
IF(DC.LE.D) GO TO 30	B 8540
20 DC=D	B 8545
30 T=(DC+D)/2.	B 8550
IF(DTW.GT.T) GO TO 50	B 8555
40 HO=T	B 8560
GO TO 55	B 8565
50 HO=DTW	B 8570
55 WHW=HO+HD	B 8575
HWD=WHW+TOEL	B 8580
IF(HWD.GT.AHWEL)GO TO 60	B 8585
GO TO 10	B 8590
60 Q=Q-A	B 8595
IF(A.LT.5.) GO TO 70	B 8600
A=2.0	B 8605
GO TO 10	B 8610
70 QMAX=Q	B 8615
RETURN	B 8620
END	B 8625

C  
C  
C

```
SUBROUTINE BNORM%QADJ,CN,SLOPE,B,D,DEP,AREA,WP<
COMPUTE NORMAL DEPTH
DEP#D
AR23#QADJ*CN/%1.486*SLOPE** .5<
XX#AR23,B*2.6667
IF XX.GT.2.0< GO TO 440
IF XX.GT.0.22< GO TO 420
YOB=.030402 J.6483784*XX-15.152238*XX*XX&64.991913*XX*XX*XX
1-110.31635*XX*XX*XX*XX
GO TO 430
420 YOB=.031468&2.34061*XX-1.53643*XX*XX&1.636594*XX*XX*XX
1-.677621*XX*XX*XX*XX
430 DEP # YOB*B
IF DEP.GT.D<DEP#D
440 AREA # B*DEP
WP # 2.*DEP&3
RETURN
END
```

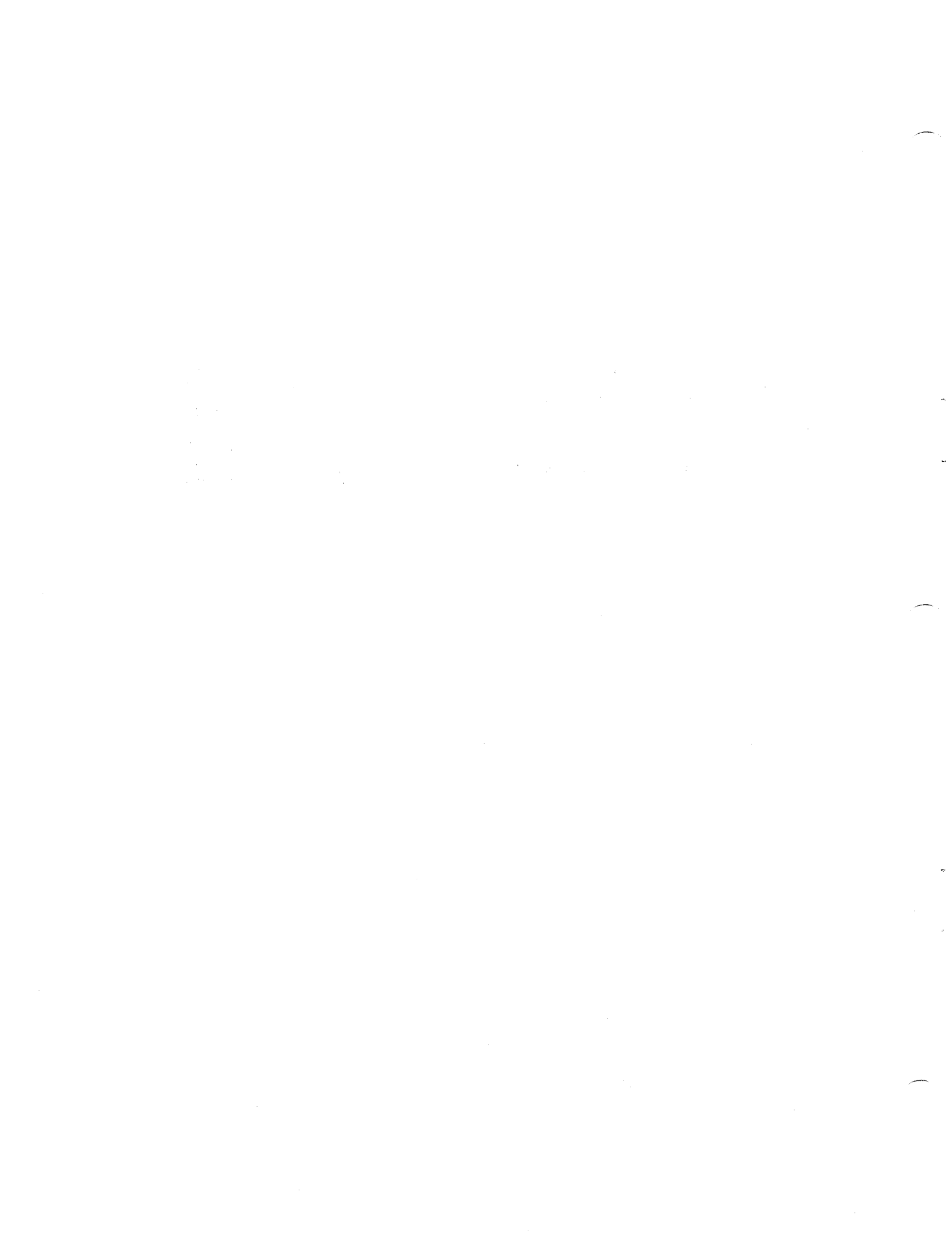
B 8630  
B 8635  
B 8640  
B 8645  
B 8650  
B 8655  
B 8660  
B 8665  
B 8670  
B 8675  
B 8680  
B 8685  
B 8690  
B 8695  
B 8700  
B 8705  
B 8710  
B 8715  
B 8720  
B 8725

	SUBROUTINE BEQUA(X, HW,B,D,SLOPE)	B 8730
C		B 8735
C	SUBROUTINE CONTAINING CULVERT EQUATIONS	B 8740
	COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),	B 8745 **
	1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),	B 8750 **
	2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),	B 8755 **
	3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),	B 8760 **
	4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),	B 8765 **
	5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,	B 8770 **
	6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),	B 8775 **
	7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),	B 8780 **
	8SLOPB(2,100),CRESE(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),	B 8785 **
	9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,	B 8790 **
	ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2	B 8795 **
	INTEGER SYSIN, SYSOT	B 8800
	DATA SCORR/.5/	B 8805
	SYSIN=1	B 8810
	SYSOT=3	B 8815
	GO TO (100,100,200,310),I1	B 8820
C	CIRCULAR PIPES -- METAL AND CONCRETE	B 8825
	100 WRITE(SYSOT,10)	B 8830
	10 FORMAT(27H CIRCULAR NOT AVAILABLE YET)	B 8835
C	PIPE-ARCH EQUATIONS	B 8840
	200 WRITE(SYSOT,20)	B 8845
	20 FORMAT(29H PIPE-ARCH NOT AVAILABLE YET)	B 8850
C		B 8855
C	BOX CULVERT EQUATIONS	B 8860
C	WINGWALLS - SQUARE EDGES - HEC NO. 5	B 8865
	310 GO TO (312,314,314,316,330,331,332),I5	B 8870
	312 HWOVD=.0724927+.507087*X-.117474*X*X+.0221702*X*X*X-.00148958*X*X	B 8875
	1*X*X+.0000380*X*X*X*X-X -SCORR*SLOPE	B 8880
	GO TO 318	B 8885
	314 HWOVD=.122117+.505435*X-.10856*X*X+.0207809*X*X*X-.00136757*X*X*X	B 8890
	1*X+.00003456*X*X*X*X-X -SCORR*SLOPE	B 8895
	GO TO 318	B 8900
	316 HWOVD=.144133+.461383*X-.0921507*X*X+.0200028*X*X*X-.00136449*X*X	B 8905
	1*X*X+.0000358*X*X*X*X-X -SCORR*SLOPE	B 8910
	318 HW=HWOVD*D	B 8915
	RETURN	B 8920
C	... BEVEL EDGES - WINGWALLS, SKEWS HEC NO. 13 CHARTS 8.9,10	B 8925
	320 HWOVD=.1566086+.3980353*X-.0640392*X*X+.01120135*X*X*X-.0006449*X	B 8930
	1*X*X*X+.000014566*X*X*X*X-X	B 8935
	GO TO 312	B 8940
	331 HWOVD=.0895633+.4412465*X-.0743498*X*X+.01273183*X*X*X	B 8945
	1-.0007988*X*X-X*X+.00001774*X*X*X *X*X -.02	B 8950
	GO TO 312	B 8955
	332 HWOVD=.0967588+.4551575*X-.0812895*X*X+.01215577*X*X*X-.00067794*X	B 8960
	1*X*X*X+.0000148*X*X*X*X-X	B 8965
	342 HW=HWOVD*D	B 8970
	RETURN	B 8975
	END	B 8980



```
SUBROUTINE CIRC(DIST,SLOPE)
WRITE(3,10)
10 FORMAT(20X,'CIRCULAR PIPE PROGRAM AVAILABLE')
RETURN
END
SUBROUTINE ARCH
WRITE(3,10)
10 FORMAT(20X,'PIPE ARCH PROGRAM NOT AVAILABLE AT THIS TIME')
RETURN
END
```

B	8985
B	8990
B	8995
B	9000
B	9005
B	9010
B	9015
B	9020
B	9025
B	9030



C		C	5
C	ROUTINES TO DESIGN AND ANALYZE PIPE CULVERTS	C	10
C		C	15
C	BY MARIO MARQUES -- FHWA	C	20
	COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),	C	25
	1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),	C	30
	2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),	C	35
	3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),	C	40
	4L,LL,K,SYSLN,SYSLT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),	C	45
	5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,ISS,	C	50
	6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),	C	55
	7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),	C	60
	8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),	C	65
	9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,	C	70
	ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2	C	75
	INTEGER SYSLN, SYSLT	C	80
	DATA IBLANK/3H /	C	85
	SYSLN=1	C	90
	SYSLT=3	C	95
C		C	100
C	-----READ DESIGN DATA	C	105
	10 READ(SYSLN,901)IPROJ	C	110
	IF(IPROJ(1).EQ.IBLANK) GO TO 11	C	115
	12 READ(SYSLN,903) I1,I2,I3,I4,I5,SLOPE,DIST,Q1,DTW,AHWEL,ELIN,	C	120
	1 ELOUT,SEL,SER,SFACE	C	125
	50 IF(I1.EQ.1) GO TO 58	C	130
	52 IF(I1.EQ.2) GO TO 58	C	135
	54 IF(I1.EQ.3) GO TO 58	C	140
	56 IF(I1.EQ.4) GO TO 58	C	145
	WRITE (SYSLT,2130)	C	150
	2130 FORMAT( 22H CULVERT CODE INVALID)	C	155
	GO TO 10	C	160
	58 SLOPE = SLOPE + 0.000001	C	165
C		C	170
C		C	175
C	-----ROUTINES TO DESIGN PIPES,ARCHES,OR BOXES	C	180
C	15 GO TO (110,110,130,140),I1	C	185
	110 CALL CIRC(DIST,SLOPE)	C	190
	GO TO 10	C	195
C	130 CALL ARCH	C	200
	GO TO 10	C	205
C	140 CALL BOXES(DIST,SLOPE)	C	210
	GO TO 10	C	215
C	11 WRITE(SYSLT,910)	C	220
	STOP	C	225
	910 FORMAT(11H END OF JOB)	C	230
	901 FORMAT(26A3)	C	235
	903 FORMAT(5I1,F7.4,9F7.1)	C	240
	904 FORMAT(2F4.1)	C	245
	END	C	250

C  
C  
C

SUBROUTINE CIRC(DIST,SLOPE)

SUBROUTINE FOR HYDRAULIC DESIGN OF PIPE CULVERTS

```

COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),
3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),
4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),
5 IPRON(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,155,
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),
8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUF,DISL,DISR,SFACE,
ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2
DIMENSION HWO(2),SUMP(2),FACEHW(2),HWEL(2)
DIMENSION CKE(5),FACE(2),CMP(90),CN(90)
INTEGER SYSIN, SYSOT
DATA CN/.0247,.0244,.0241,.0237,.0235,.0233,.0232,.0231,.0229,
1.0228,.0227,.0226,.0225,.0281,.0278,.0275,.0273,.0271,.0269,.0267,
2.0266,.0265,.0263,.0262,.0261,.026,.026,.0332,.033,.0327,
3.0325,.0323,.0321,.032,.0318,.0317,.0315,.0314,.0313,.0312,.0311,
4.031,.0309,.0308,.0307,.0307,.0306,.0305,.0305,.0304,.0304,.0303,
5.0303,.0302,.0302,.0301,.0301,.03,.03,.03,29*.012/
DATA
CCKE/.9,.7,.5,.2,.2/
DATA CMP/2,.2,3,3,3,4,4,4,5,5,5,5,6,6,6,5,7,7,7,5,8,3,3,3,5,4,4,4,
15,5,5,5,6,6,6,5,7,7,7,5,8,8,8,5,9,9,9,5,10,5,5,5,6,6,6,5,7,7,7,5,8,
28,5,9,9,5,10,10,5,11,11,5,12,12,5,13,13,5,14,14,5,15,15,5,
316,16,5,17,17,5,18,18,5,19,19,5,20,20,5,21,2,2,2,25,2,5,
42,75,3,3,3,5,4,4,4,5,5,5,5,6,6,6,5,7,7,7,5,8,8,8,5,9,9,9,5,10,10,5,
511,11,5,12,12,5,13,13,5,14,14,5,15,15,5/

PRINT CONVENTIONAL CULVERT DESIGN DATA

READ(SYSIN,20) DIA1, DIA2
20 FORMAT(2F5.2)
WRITE(SYSOT,902) IPRON
902 FORMAT(1H1,' >>>> PIPE CULVERT DESIGN FOR PROJECT >>> ',26A3,///
1/' >>>> THE PROGRAM PROVIDES A RANGE OF CONVENTIONAL PIPE CULVERT
2 SIZES WITH AND WITHOUT BEVELS WHICH SATISFY SITE REQUIREMENTS'//
330X,'WHERE: BEVELED EDGES FOR CMP AND CONCRETE PIPES'/37X,'ARE BA
4SED ON CHART 13 IN HEC-13'////
A ' >>>> IF INLET CONTROL GOVERNS - IMPROVED INLET DESIGNS ARE PR
BOVIDED FOR SIDE-TAPERED INLETS ' /66X,'AND SLOPE-TAPER
CED INLETS '////)
903 WRITE(SYSOT,904)
904 FORMAT(1X,
1..... DESIGN INPUT DATA ***
2.....
3..... DESIGN INPUT DATA **
4.....
5.....
6.....
7.....
8...../ )

```

C 255  
C 260  
C 265  
C 270  
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C 285  
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C 430 \*\*  
C 435  
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C 445  
C 450  
C 455  
C 460  
C 465  
C 470  
C 475  
C 480  
C 485  
C 490  
C 495  
C 500  
C 505  
C 510  
C 515  
C 520  
C 525

C  
C  
C

GO TO (12,14),11		C	530
12 GO TO (42,44),12		C	535
42 GO TO (48,50,52,52,56,58,58),15		C	540
48 WRITE(SYSOT,41)		C	545
41 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - PROJECT	C	550
1ING - UNPAVED	KE= 0.9'//)	C	555
GO TO 58		C	560
50 WRITE(SYSOT,43)		C	565
43 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - MITERED	C	570
1 - UNPAVED	KE= 0.7'//)	C	575
GO TO 58		C	580
52 WRITE(SYSOT,45)		C	585
45 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - HEADWAL	C	590
1L - UNPAVED	KE= 0.5'//)	C	595
GO TO 58		C	600
56 WRITE(SYSOT,47)		C	605
47 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - END-SEC	C	610
1TION - UNPAVED	KE= 0.5'//)	C	615
58 IF(15.EQ.7) GO TO 60		C	620
WRITE(SYSOT,49)		C	625
49 FORMAT(4X,'BEVEL-EDGED CULVERT -----	CM PIPE - UNPAVED	C	630
1WITH BEVEL(A)	KE= 0.2'//)	C	635
GO TO 80		C	640
60 WRITE(SYSOT,61)		C	645
61 FORMAT(4X,'BEVEL-EDGED CULVERT -----	CM PIPE - UNPAVED	C	650
1WITH BEVEL(B)	KE= 0.2'//)	C	655
GO TO 80		C	660
44 GO TO (64,66,68,68,70,72,72),15		C	665
64 WRITE(SYSOT,65)		C	670
65 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - PROJECTING -	C	675
1 PAVED	KE= 0.9'//)	C	680
GO TO 72		C	685
66 WRITE(SYSOT,67)		C	690
67 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - MITERED	C	695
1 - PAVED	KE= 0.7'//)	C	700
GO TO 72		C	705
68 WRITE(SYSOT,69)		C	710
69 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - HEADWAL	C	715
1L - PAVED	KE= 0.5'//)	C	720
GO TO 72		C	725
70 WRITE(SYSOT,71)		C	730
71 FORMAT(4X,'CONVENTIONAL CULVERT -----	CM PIPE - END-SEC	C	735
1TION - PAVED	KE= 0.5'//)	C	740
72 IF(15.EQ.7) GO TO 74		C	745
WRITE(SYSOT,73)		C	750
73 FORMAT(4X,'BEVEL-EDGED CULVERT -----	CM PIPE - PAVED WI	C	755
1TH BEVEL(A)	KE= 0.2'//)	C	760
GO TO 80		C	765
74 WRITE(SYSOT,75)		C	770
75 FORMAT(4X,'BEVEL-EDGED CULVERT -----	CM PIPE - PAVED WI	C	775
1TH BEVEL(B)	KE= 0.2'//)	C	780
GO TO 80		C	785
14 IF(15.GT.5) GO TO 12		C	790
GO TO (21,23,25,27,29),15		C	795
21 WRITE(SYSOT,22)		C	800

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22 FORMAT(4X,'CONVENTIONAL CULVERT ----- CONCRETE PIPE - S C 808
   SOCKET-END - PROJECTING KE= 0.2'//) C 810
   GO TO 19 C 815
23 WRITE(SYSOT,24) C 820
24 FORMAT(4X,'CONVENTIONAL CULVERT ----- CONCRETE PIPE - S C 825
   SOCKET-END HEADWALL KE= 0.2'//) C 830
   GO TO 19 C 835
25 WRITE(SYSOT,26) C 840
26 FORMAT(4X,'CONVENTIONAL CULVERT ----- CONCRETE PIPE - S C 845
   SQUARE-EDGE PROJECTING KE= 0.5'//) C 850
   GO TO 19 C 855
27 WRITE(SYSOT,28) C 860
28 FORMAT(4X,'CONVENTIONAL CULVERT ----- CONCRETE PIPE - S C 865
   SQUARE-EDGE HEADWALL KE= 0.5'//) C 870
   GO TO 19 C 875
29 WRITE(SYSOT,16) C 880
30 FORMAT(4X,'CONVENTIONAL CULVERT ----- CONCRETE PIPE - E C 885
   1ND SECTION KE= 0.5'//) C 890
   IF(.I5.EQ.7) GO TO 15 C 895
18 WRITE(SYSOT,13) C 900
13 FORMAT(4X,'BEVEL-EDGED CULVERT ----- CONCRETE PIPE WITH C 905
   1 BEVEL(A) KE= 0.2'//) C 910
   GO TO 80 C 915
15 WRITE(SYSOT,17) C 920
17 FORMAT(4X,'BEVEL-EDGED CULVERT ----- CONCRETE PIPE WITH C 925
   1 BEVEL(B) KE= 0.2'//) C 930
80 ISEL=SEL C 935
   ISER=SER C 940
   SLOPP=SLOPE C 945
   SLOPE = (EL I-ELOUT)/DIST + .000001 C 950 **
   WRITE(SYSOT,1900)I1,I2,I3,I4,I5,SLOPP,DIST,Q1,DTW,AHWEL,ELIN, C 955
   1ELOT, SEL, SER, DIA1, DIA2, SFACE,SLOPE C 960
1900 FORMAT(18X,'APPROX TOE-TOE',27X, C 965
   A 'ALLOWABLE STREAM BED STREAM BED US ROADWAY/ C 970 **
   1DS ROADWAY',4X,'CULVERT',7X,'STREAM CULVERT DESIGN',5X,'DE C 975 **
   2SIGN',5X,'HEADWATER ELEVATION ELEVATION',5X,'EMBANKMENT', C 980
   35X,'EMBANKMENT',5X,'CODE',8X,'SLOPE',4X,'LENGTH DISCHARGE TAI C 985
   4LWATER ELEVATION AT INLET AT OUTLET',7X,'SLOPE',11X,'SLOP C 990
   5E',4X,F4.1,F4.1,F7.4,2X,F8.1,2X,F8.1,4X,F9.1,4X,F8.1,4X,F8.1,5X, C 995
   6F9.1,9X,F4.1,'1',10X,F4.1,'1'//4X,'CULVERT SIZES',33X,'SLOPE-TA C 1000
   7PER',7X,'DIAMETER FROM',F6.2,' FT TO',F6.2,' FT',9X,'FALL SLOP C 1005
   8E',10X,'COMPUTED STREAM',52X,F4.1,'1',15X,'SLOPE =',F7.4//) C 1010
   WRITE(SYSOT,2100) C 1015
2100 FORMAT(130H'***** C 1020
   1***** C 1025
   2*****/*****' INDEX SHEET FOR PIPE C 1030
   3 CULVERTS *****' ***** C 1035
   4*****//*****' INDEX SHEET C 1040
   5FOR PIPE CULVERTS ***** C 1045
   6*****//***** C 1050
   7***** C 1055
   8*****//) C 1060
459 WRITE(SYSOT,2105) 'E(I4) C 1065
2105 FORMAT(30X,'* --- O TLET CONTROL -- **',27X,'--- INLET CONTROL -- C 1070
   1',27X,'*'/ C 1075

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130X, '0.25X, '0.73X, '1/30X, ' KE='0.4, ' KE=0.2 OUTLET ** CON C 1080
2VENTIONAL CULVERT * BEVEL-EDGED CULVERT * SIDE-TAPERED CULVERT C 1085
3 '1/30X, '-----* C 1090
4-----* C 1095
5* BARREL * HW HW INVERT ** HW '0.11X, 'INVERT * HW C 1100
6'.13X, 'INVERT * THROAT', '10X, 'INVERT * C PAGE * OF * DIAMETE C 1105
7R * ELEV ELEV ELEV ** ELEV FALL ELEV * ELEV C 1110
8FALL ELEV HW ELEV FALL ELEV * C 1115
9 '0.6X, 'BARRELS* (FT) * (FT) (FT) C 1120
A(FT) ** (FT) (FT) * (FT) (FT) * (FT) C 1125
B (FT) (FT) '0.6X, '0.7X, '0.6X, '0.6X, '0.25X, '0.23X. C 1130
C'0.24X, '0.24X, '0.24X) C 1135
I55=15 C 1140
30 IF(I1.EQ.1.AND.I5.LE.3) I5=I5+7 C 1145
DO 457 J=1,100 C 1150 **
ITAB(J)=0 C 1155
TAB1(J)=0.0 C 1160
TAB2(J)=0.0 C 1165
TAB3(J)=0.0 C 1170
TAB4(J)=0.0 C 1175
TAB5(J)=0.0 C 1180
TAB6(J)=0.0 C 1185
TAB7(J)=0.0 C 1190
TAB8(J)=0.0 C 1195
TAB9(J)=0.0 C 1200
TAB10(J)=0.0 C 1205
TAB11(J)=0.0 C 1210
TAB12(J)=0.0 C 1215
TAB13(J)=0.0 C 1220
TAB14(J)=0.0 C 1225
TAB15(J)=0.0 C 1230
TAB16(J)=0.0 C 1235
TAB17(J)=0.0 C 1240
TAB18(J)=0.0 C 1245
457 CONTINUE C 1250
L=1 C 1255
I14=14 C 1260
I15=15 C 1265
I16=13 C 1270
IF(I3.EQ.4) I13=3 C 1275
KD1=1 C 1280
KD2=13 C 1285
JL2=0 C 1290
C TO ANALYZE SEPERATE CORRUGATED METAL PIPES REPLACE THE NEXT CARD WITH C 1295 **
C ' DO 480 K1 = I13, I15 ' C 1300 **
DO 480 K1=I13,3 C 1305
JL=0 C 1310
IF(I1.EQ.2) GO TO 10 C 1315
IF(K1.EQ.2) KD1=14 C 1320
IF(K1.EQ.2) KD2=28 C 1325
IF(K1.EQ.3) KD1=29 C 1330
IF(K1.EQ.3) KD2=61 C 1335
10 IF(I1.EQ.2) KD1=62 C 1340
IF(I1.EQ.2) KD2=90 C 1345
DO 480 IBAR=1,5 C 1350

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ICOUNT=0
460 HWIN=0.0
HWJ(1)=0.0
HWJ(2)=0.0
SUMP(1)=0.0
SUMP(2)=0.0
FACEHW(1)=0.0
FACEHW(2)=0.0
HWOUT=0.0
VELIN=0.0
VELOUT=0.0

C
C START DESIGN OF PIPE CULVERTS
DO 480 K=KD1,KD2
NOCA(1,L)=0
NOCA(2,L)=0
NOCB(1,L)=0
NOCB(2,L)=0
NOCC(1,L)=0
NOCC(2,L)=0
D=CMP(K)
DIA=D
BAR=IBAR
I4=I14
I5=I15
IBEV=1
IF(I5.EQ.6.OR.I5.EQ.7)IBEV=2
IF(IBEV.EQ.2) NOCA(1,L)=1
Q=Q1/BAR
IF(K.EQ.29.AND.I5.EQ.5) GO TO 462
IF(D.GE.DIA1.AND.D.LE.DIA2) GO TO 461
GO TO 480
461 SMALL=(SLOPE*SEL**2*D)/(1+SLOPE*SEL)
SMALR=(SLOPE*SER**2*D)/(1.+SLOPE*SER)
DISL=SEL*D-SMALR
DISR=SER*D+SMALR
IF(I5.EQ.1.OR.I5.EQ.3.OR.I5.EQ.8) DISL=0.0
IF(I5.EQ.1.OR.I5.EQ.3.OR.I5.EQ.8) DISR=0.0
ELL=DISL*SLOPE
ELR=DISR*SLOPE
FACEL=ELIN-ELL
FAHC=FACEL
CROWN = FACEL+D
TOEL=FLOUT+ELR
HH=FACEL-TOEL
DIST1=DIST-DISL-DISR
CLTH=((DIST1+DIST1)-(HH*HH))**.5
39 QMAX=0.0
AN=CN(K)
IF(I2.EQ.2) AN=.75*CN(K)+.25*.012
CALL CDUT(Q,D,HWOUT,VELOUT,DEP,CN,DC,DIST1,SLOPE,AN)
HWJ(IBEV)=HWOUT+TOEL
IF(IBEV.EQ.1) GO TO 465
IF(HWJ(2).GT.AHWEL.AND.NOCA(1,L).EQ.1) NOCA(1,L)=0
IF(HWJ(2).GT.AHWEL.AND.NOCB(1,L).EQ.1) NOCB(1,L)=0

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C 1355
C 1360
C 1365
C 1370
C 1375
C 1380
C 1385
C 1390
C 1395
C 1400
C 1405
C 1410
C 1415
C 1420
C 1425
C 1430
C 1435
C 1440
C 1445
C 1450
C 1455
C 1460
C 1465
C 1470
C 1475
C 1480
C 1485
C 1490
C 1495
C 1500
C 1505
C 1510
C 1515
C 1520
C 1525
C 1530
C 1535
C 1540 **
C 1545
C 1550
C 1555
C 1560
C 1565
C 1570
C 1575
C 1580
C 1585
C 1590
C 1595
C 1600
C 1605
C 1610
C 1615
C 1620
C 1625

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IF(HWO(2).GT.AHWEL.AND.NOCC(1,L).EQ.1) *C 1630
IF(HWO(2).GT.AHWEL) GO TO 480 C 1635
IF(HWO(2).LT.TOEL) GO TO 480 C 1640
465 CALL CFIT(Q,AN,D,QMAX,TOEL,SLOPE,I4,I1,CLTH,DTW,AHWEL) C 1645
Q=Q1/BAR C 1650
TQVAX(IBEV,L)=QMAX*BAR C 1655
X=Q/D*.2.5 C 1660
CALL CEQUA(X,HWIN,D,SLOPE,I5) C 1665
124 FACEHW(IBEV)=FACEL+HWIN C 1670
IF(FACEHW(IBEV).LT.(AHWEL-D).AND.HWO(IBEV).LT.(AHWEL-D)) C 1675 **
GO TO 480 C 1680
134 FALLM=1.5*D C 1685
FALLT=CLTH+SLOPE C 1690
IF(FALLM.GT.FALLT) FALLM=FALLT C 1695
IF(FACEHW(IBEV).GT.AHWEL) GO TO 140 C 1700
GO TO 150 C 1705
C COMPUTE THE SUMP C 1710
140 SUMP(IBEV)=FACEHW(IBEV)-AHWEL C 1715
IF(SUMP(IBEV).GE.FALLM) NOCA(IBEV,L)=1 C 1720
DISTA(IBEV,L)=DIST1 C 1725
IF(NOCA(IBEV,L).EQ.1) GO TO 153 C 1730
DIS=SUMP(IBEV)*SEL C 1735
DISTA(IBEV,L)=DIS+DIST1 C 1740
FACEL=FACEL+SLOPE*DIS C 1745
DIF=FACEL-SUMP(IBEV)-DIS*SLOPE C 1750
IF(DIF.LT.TOEL) DIF=TOEL+.01 C 1755
SLOPA(IBEV,L)=(DIF-TOEL)/DISTA(IBEV,L) C 1760
CROWN=DIF+D C 1765
FACE(IBEV)=DIF C 1770
FACEHW(1)=FACE(IBEV)+HWIN C 1775
IF(FACEHW(1).GE.CROWN.OR.HWO(IBEV).GE.CROWN) GO TO 142 C 1780 **
GO TO 140 C 1785
142 HWEL(IBEV)=AHWEL C 1790
GO TO 155 C 1795
C NO SUMP C 1800
150 SUMP(IBEV)=0.0 C 1805
SLOPA(IBEV,L)=SLOPE C 1810
DISTA(IBEV,L)=DIST1 C 1815
FACE(IBEV)=FACEL C 1820
CROWN=FACEL+D C 1825
HWEL(IBEV)=FACEL+HWIN C 1830
IF(FACEHW(1).GE.CROWN.OR.HWO(IBEV).GE.CROWN) GO TO 155 C 1835 **
GO TO 480 C 1840
155 IF(SUMP(IBEV).EQ.0.0) CRESA(IBEV,L)=0.0 C 1845
C COMPUTE VELOCITY C 1850
SLT=SLOPA(IBEV,L) C 1855
DA=DISTA(IBEV,L) C 1860
CALL COUT(Q,D,HWO,VELOUT,DEP,DN,DC,DA,SLO,AN) C 1865
CALL CROUT(DN,AREA,F,WP,DIA,R) C 1870
VELA(IBEV,L)=Q/AREA C 1875
IF(VELOUT.GT.VELA(IBEV,L)) VELA(IBEV,L)=VELOUT C 1880
IF(SUMP(IBEV).EQ.0.0) GO TO 151 C 1885
C..... COMPUTE MINIMUM CREST LENGTH C 1890
HCA=F*HC+(SUMP(IBEV)*SEL*SLOPE)+(SUMP(IBEV)+3.+D/2.)*SLOPE C 1895
HC=HWEL(IBEV)-HCA C 1900

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	IF(HC.LT.1.) HC=1.0	C 1905
	CRES=(.5*Q1**(.6667))/HC	C 1910
	CRESA(IBEV,L)=CRES**1.5	C 1915
C	CCMPUTE CURVE B	C 1920
151	ELINCA(IBEV,L)=FACE(IBEV)	C 1925
154	X=(TOMAX(IBEV,L)/BAR)/(D**2.5)	C 1930
	CALL CEQUA(X,HWI,DIA,SLOPE,I5)	C 1935
	TEMP=ELINCA(IBEV,L)+HWI	C 1940
	IF(TEMP.LE.AHWEL) GO TO 144	C 1945
	BFALL=TEMP-AHWEL	C 1950
	TBFALL(IBEV,L)=BFALL +SUMP(IBEV)	C 1955
	IF(TBFALL(IBEV,L).GT.FALLM) GO TO 160	C 1960
	ELINCB(IBEV,L)=ELINCA(IBEV,L)-BFALL	C 1965
	IF(ELINCB(IBEV,L).LT.TOEL) ELINCB(IBEV,L)=TOEL+.01	C 1970
	HWCB(IBEV,L)=ELINCB(IBEV,L)+HWI	C 1975
	GO TO 139	C 1980
160	ELINCB(IBEV,L)=ELINCA(IBEV,L)-(FALLM-SUMP(IBEV))	C 1985
	IF(ELINCB(IBEV,L).LT.(TOEL+.01)) ELINCB(IBEV,L)=TOEL+.01	C 1990
	BFALL=ELINCA(IBEV,L)-ELINCB(IBEV,L)	C 1995
	TBFALL(IBEV,L)=BFALL+SUMP(IBEV)	C 2000
C	COMPUTE MAX Q BASED ON INLET CURVE	C 2005
	AIN=50.	C 2010
	QUE=Q1/BAR	C 2015
162	QUE=QUE+AIN	C 2020
	X=QUE/D**2.5	C 2025
	CALL CEQUA(X,HIGH,DIA,SLOPE,I5)	C 2030
	HI=HIGH+ELINCB(IBEV,L)	C 2035
	IF(HI.GT.AHWEL) GO TO 170	C 2040
	GO TO 162	C 2045
170	QUE=QUE-AIN	C 2050
	IF(AIN.LT.10.) GO TO 172	C 2055
	AIN=2.0	C 2060
	GO TO 162	C 2065
172	TOMAX(IBEV,L)=QUE+BAR	C 2070
	X=QUE/D**2.5	C 2075
	CALL CEQUA(X,HWI,DIA,SLOPE,I5)	C 2080
	HWCB(IBEV,L)=ELINCB(IBEV,L)+HWI	C 2085
139	DISB=BFALL*SEL	C 2090
	DI=TB(IBEV,L)=DISTA(IBEV,L)+DISB	C 2095
	SLOB(IBEV,L)=(ELINCB(IBEV,L)-TOEL)/DISTB(IBEV,L)	C 2100
C	COMPUTE VELOCITY	C 2105
	SLO=SLOB(IBEV,L)	C 2110
	QQ=TOMAX(IBEV,L)/BAR	C 2115
	DB=DISTB(IBEV,L)	C 2120
	CALL CROUT(QQ,D,HXOUT,VELOUT,DEP.DN,DC,DB,SLO,AN)	C 2125
	CALL CROUT(DN,AREA,T,WP,DIA,R)	C 2130
	VELB(IBEV,L)=QQ/AREA	C 2135
	IF(VELOUT.GT.VELB(IBEV,L)) VELB(IBEV,L)=VELOUT	C 2140
	HCB=FARC+(TBFALL(IBEV,L)*SEL*SLOPE)+(TBFALL(IBEV,L)*3.+D/2.)*SLOPE	C 2145
	HC-AHWEL-HCB	C 2150
	IF(HC.LT.1.) HC=1.0	C 2155
	CRES=(.5*TOMAX(IBEV,L)**.6667)/HC	C 2160
	CRESB(IBEV,L)=CRES**1.5	C 2165
	GO TO 145	C 2170
144	TBFALL(IBEV,L)=0.0	C 2175

	NOCB(IBEV,L)=1	C 2180
C	COMPUTE CURVE C	C 2185
145	TEMP=ELINCA(IBEV,L)+HWIN	C 2190
	IF(HWO(IBEV).GE.TEMP) GO TO 143	C 2195
	CFALL=TEMP-HWO(IBEV)	C 2200
	TCFALL(IBEV,L)=CFALL +SUMP(IBEV)	C 2205
	ELINCC(IBEV,L)=ELINCA(IBEV,L)-CFALL	C 2210
	IF(TCFALL(IBEV,L).GT.FALLM) ELINCC(IBEV,L)=ELINCA(IBEV,L)-(FALLM-	C 2215
	1SUMP(IBEV))	C 2220
	IF(ELINCC(IBEV,L).LT.(TOEL+.01))ELINCC(IBEV,L)=TOEL+.01	C 2225
	CFALL=ELINCA(IBEV,L)-ELINCC(IBEV,L)	C 2230
	TCFALL(IBEV,L)=CFALL+SUMP(IBEV)	C 2235
	HWCC(IBEV,L)=ELINCC(IBEV,L)+HWIN	C 2240
	DISC=CFALL*SEL	C 2245
	DISTC(IBEV,L)=DISC+DISTA(IBEV,L)	C 2250
	SLOPC(IBEV,L)=(ELINCC(IBEV,L)-TOEL)/DISTC(IBEV,L)	C 2255
	SLO =SLOPC(IBEV,L)	C 2260
	DCC=DISTC(IBEV,L)	C 2265
	CALL CDUT(Q,D,HWOOUT,VELOUT,DEP,DN,DC,DCC,SLO,AN)	C 2270
	CALL CROUT(DN,AREA,T,WP,DIA,R)	C 2275
	VELC(IBEV,L)=Q /AREA	C 2280
	IF(VELOUT.GT.VELC(IBEV,L)) VELC(IBEV,L)=VELOUT	C 2285
	HCC=FAHC+(TCFALL(IBEV,L)*SEL*SLOPE)+(TCFALL(IBEV,L)*3.+D/2.)*SLOPE	C 2290
	HC=TEMP-HCC	C 2295
	IF(HC.LT.1.) HC=1.0	C 2300
	CRES=(.5*Q1**(.6667))/HC	C 2305
	CRESC(IBEV,L)=CRES**1.5	C 2310
	GO TO 153	C 2315
143	TCFALL(IBEV,L)=0.0	C 2320
	NOCB(IBEV,L)=1	C 2325
153	CONTINUE	C 2330
	IF(IBEV.EQ.2) GO TO 464	C 2335
	IBEV=IBEV+1	C 2340
	FACEL=ELIN-ELL	C 2345
	I4=4	C 2350
	I5=6	C 2355
	GO TO 461	C 2360
464	IF(NOCA(1,L).EQ.1) NOCB(1,L)=1	C 2365
	IF(NOCA(1,L).EQ.1) NOCC(1,L)=1	C 2370
	IF(NOCA(2,L).EQ.1) NOCB(2,L)=1	C 2375
	IF(NOCA(2,L).EQ.1) NOCC(2,L)=1	C 2380
	INDEX=0	C 2385
C	IF(BAR.GT.2.) GO TO 120	C 2390
	IBAR=BAR	C 2395
	CALL CSIDE( D,FALL,HWT,TROEL,IBAR,DIST1,INDEX,SLOPE,AN)	C 2400
	IF(FALL.GT.900.) GO TO 120	C 2405 **
	IF(FALL.GE.FALLM) GO TO 480	C 2410
	GO TO 121	C 2415
120	FALL=0.0	C 2420
	TRDEL=0.0	C 2425
	HWT=0.0	C 2430
	IF(NOCA(1,L).EQ.1.AND.NOCA(2,L).EQ.1) GO TO 480	C 2435
121	IF(I2.EQ.2) GO TO 32	C 2440
	IF(I2.EQ.1) GO TO 31	C 2445
	IF(JL2.EQ.0.AND.K.LI.90) GO TO 186	C 2450

IF(JL2.EQ.1.AND.K.LE.90) GO TO 122	C 2455
31 IF(L.EQ.1.AND.K.LE.13) GO TO 180	C 2460
IF(K.LE.13) GO TO 122	C 2465
IF(JL.EQ.0.AND.K.LE.28) GO TO 182	C 2470
IF(JL.EQ.1.AND.K.LE.28) GO TO 122	C 2475
IF(JL.EQ.0.AND.K.LE.61) GO TO 184	C 2480
IF(JL.EQ.1.AND.K.LE.61) GO TO 122	C 2485
32 IF(L.EQ.1.AND.K.LE.13) GO TO 34	C 2490
IF(K.LE.13) GO TO 122	C 2495
IF(JL.EQ.0.AND.K.LE.28) GO TO 36	C 2500
IF(JL.EQ.1.AND.K.LE.28) GO TO 122	C 2505
IF(JL.EQ.0.AND.K.LE.61) GO TO 38	C 2510
IF(JL.EQ.0.AND.K.LE.61) GO TO 122	C 2515
34 WRITE(SYSOT,35)	C 2520
35 FORMAT(/10X,'2-2/3 IN X 1/2 IN CORRUGATED-METAL PIPE - PAVED')	C 2525
JL=1	C 2530
GO TO 122	C 2535
36 WRITE(SYSOT,37)	C 2540
37 FORMAT(/10X,'3 IN X 1 IN CORRUGATED-METAL PIPE -----PAVED')	C 2545
JL=1	C 2550
GO TO 122	C 2555
38 WRITE(SYSOT,40)	C 2560
40 FORMAT(/10X,'6 IN X 2 IN MULTIPLATE PIPE -----PAVED')	C 2565
JL=1	C 2570
GO TO 122	C 2575 **
180 WRITE(SYSOT,181)	C 2580
181 FORMAT(/10X,'2-2/3 IN X 1/2 IN CORRUGATED-METAL PIPE - UNPAVED')	C 2585
JL=1	C 2590 **
GO TO 122	C 2595
182 WRITE(SYSOT,183)	C 2600
183 FORMAT(/10X,'3 IN X 1 IN CORRUGATED-METAL PIPE -----UNPAVED')	C 2605
JL=1	C 2610
GO TO 122	C 2615
184 WRITE(SYSOT,185)	C 2620
185 FORMAT(/10X,'6 IN X 2 IN MULTIPLATE PIPE -----UNPAVED')	C 2625
JL=1	C 2630
GO TO 122	C 2635
186 WRITE(SYSOT,187)	C 2640
187 FORMAT(/10X,'CONCRETE PIPES')	C 2645
JL2=1	C 2650
122 ISAR=BAR	C 2655
ITAB(L)=IBAR	C 2660
TAB1(L)=D	C 2665
TAB2(L)=AN	C 2670
TAB3(L)=HWD(1)	C 2675
TAB4(L)=HWD(2)	C 2680
TAB5(L)=TOEL	C 2685
TAB6(L)=HWEL(1)	C 2690
TAB7(L)=SUMP(1)	C 2695
TAB8(L)=FACE(1)	C 2700
TAB9(L)=HWEL(2)	C 2705
TAB10(L)=SUMP(2)	C 2710
TAB11(L)=FACE(2)	C 2715
TAB12(L)=HWT	C 2720
TAB13(L)=FALL	C 2725

TAB14(L)=TRGEL	C 2730
TAB15(L)=DIST2	C 2735
TAB16(L)=QMAX*IBAR	C 2740
IF(NOCA(1,L).EQ.0.AND.NOCA(2,L).EQ.0) GO TO 126	C 2745
IF(NOCA(2,L).EQ.0) GO TO 130	C 2750
GO TO 125	C 2755
130 TAB3(L)=0.0	C 2760
TAB5(L)=0.0	C 2765
TAB7(L)=0.0	C 2770
TAB8(L)=0.0	C 2775
WRITE(SYSOT,127)L,IBAR,D, HWO(2),TOEL,HWEL(2),SUMP(2),	C 2780
1 FACE(2),HWT,FALL,TRDEL	C 2785
127 FORMAT(' ',I3,3X,' ',I4,3X,' ',F9.2,3X, ' ',F9.1,	C 2790
1 F10.1,' ** ',5X,' ',7X,' ',2(F6.1,4X,F4.1,3X,F6.1,' '))	C 2795
GO TO 128	C 2800
126 WRITE(SYSOT,123)L,IBAR,D, HWO(1),HWO(2),TOEL,HWEL(1),	C 2805
1 SUMP(1),FACE(1),HWEL(2),SUMP(2),FACE(2),HWT,FALL,TRDEL	C 2810
123 FORMAT(' ',I3,3X,' ',I4,3X,' ',F9.2,3X, ' ',2F7.1,F10.1,	C 2815
1 ' ',F3.1,3X,F4.1,3X,F6.1,' ',2(F6.1,4X,F4.1,3X,F6.1,' '))	C 2820
GO TO 128	C 2825
125 WRITE(SYSOT,129)L,IBAR,D, HWO(2),TOEL,HWT,FALL,TRDEL	C 2830
129 FORMAT(' ',I3,3X,' ',I4,3X,' ',F9.2,3X, ' ',F9.1,	C 2835
1 F10.1,' ** ',5X,' ',7X,' ',3X,' ',6X,' ',7X,' ',	C 2840
2F6.1,4X,F4.1,3X,F6.1,' ')	C 2845
128 L=L+1	C 2850
479 ICOUNT=IBAR	C 2855
480 CONTINUE	C 2860
482 L=L-1	C 2865
IF(L.EQ.0) WRITE(SYSOT,483)	C 2870
483 FORMAT(' ',5X,' THE RANGE OF CULVERT SIZES ANALYZED EXCEED THE DESIG	C 2875
IN CRITERIA'')	C 2880
IF(L.EQ.0) RETURN	C 2885
WRITE(SYSOT,484)	C 2890
484 FORMAT(' ',25X,' BY DEFINITION OF FALL, WHEN A SIDE-TAPERED INLET LI	C 2895
1ES ON THE STREAM SLOPE, ' ',25X,' THE FALL IS THE DIFFERENCE IN ELEVAT	C 2900
2ION OF THE FACE INVERT AND THE THROAT INVERT' ',25X,' WHEN SIDE-TAPE	C 2905 **
3RED CULVERT COLUMN: (ABOVE) CONTAINS 0.0 0.0 0.0 ' ',30X,' 1. THE TH	C 2910 **
4ROAT DESIGN EXCEEDED THE DESIGN CRITERIA' ',27X,' OR 2. IMPROVED INLE	C 2915 **
5T FOR MORE THAN 2 BARRELS NOT AVAILABLE'')	C 2920 **
C.....CALL TO CHY1 FOR CONVENTIONAL AND BEVEL PIPE DESIGN	C 2925
CALL CHY1(DIST,SLOPE)	C 2930
RETURN	C 2935 **
END	C 2940

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SUBROUTINE CHY1(DIST,SLOPE)
COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),
3TQMAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),
4L,LL,K,SYSD,SYSDT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),
5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),
8SLOPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,
ADIA1,DAI2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2
DIMENSION HWO(2),SUMP(2),FACEHW(2),HWEL(2)
DIMENSION CKE(5),FACE(2)
REAL L1,L2,L3,L4
INTEGER SYSD,SYSDT
DATA CKE/.9,.7,.5,.2,.2/
II1=I1
I1=I2
II3=I3
II4=I4
II5=I5
90 LL=1
100 IBAR=1TAB(LL)
BAR=IBAR
CN=TAB2(LL)
D=TAB1(LL)
SMALL=(SLOPE*SEL**2+D)/(1.+SLOPE*SEL)
SMALR=(SLOPE*SER**2+D)/(1.+SLOPE*SER)
DISL=SEL*D-SMALL
DISR=SER*D+SMALR
ELL=DISL*SLOPE
ELR=DISR*SLOPE
DIST1=DIST-DISL-DISR
PAGE HEADINGS
94 WRITE(SYSDT,90) LL,ITAB(LL), TAB1(LL),Q1,AHWEL,SLOPE
1,TAB5(LL)
80 FORMAT(1H1,'PAGE=',I3,5X,'NO. BARRELS=',I2,5X,
1'DIAMETER=',F5.2,' FT',5X,'Q(50)=',F7.1,' CFS AHWEL=',F7.1,
2' FT',4X,'STREAM SLOPE=',F7.4/50X,'OUTLET INVERT ELEV.=',F7.1,
3' FT'///)
IF(I5.EQ.6.OR.I5.EQ.7) GO TO 212
IF(NOCA(1,LL).EQ.0) GO TO 89
WRITE(SYSDT,91)I1,I2,I3,I4,I55
91 FORMAT(1X,'CONVENTIONAL INLET DESIGN FOR CULVERT CODE ',5I1/
11X,'*****'//20X,
2'DESIGN DATA NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE CONV
SENTIONAL INLET EXCEEDS 1.50 OR 150.')
GO TO 206
C
C.....CONVENTIONAL PIPE CULVERTS + PERFORMANCE CURVE DATA
C
89 WRITE(SYSDT,81)I1,I2,I3,I4,I55,CKE(I4),TQMAX(1,LL)
81 FORMAT(1X,'CONVENTIONAL INLET DESIGN FOR CULVERT CODE: ',5I1/
11X,'*****'//4X,'OUT

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C 2945
C 2950
C 2955
C 2960
C 2965
C 2970
C 2975
C 2980
C 2985
C 2990
C 2995
C 3000
C 3005
C 3010
C 3015
C 3020
C 3025
C 3030
C 3035
C 3040
C 3045
C 3050
C 3055
C 3060
C 3065
C 3070
C 3075 **
C 3080 **
C 3085 **
C 3090 **
C 3095
C 3100
C 3105
C 3110
C 3115
C 3120
C 3125
C 3130
C 3135 **
C 3140
C 3145
C 3150
C 3155
C 3160
C 3165
C 3170
C 3175
C 3180
C 3185
C 3190
C 3195
C 3200
C 3205
C 3210
C 3215

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2LET COMPUTATIONS',34X,'INLET COMPUTATIONS'/3X,'*****' C 3220
3',8X,'*****' C 3225
4*****'//10X,'KE='F7.1,18X,'MIN FALL C C 3230
5URVE'.17X,'MAX Q CURVE',21X,'MIN HW CURVE'//67X,'MAX Q ='F7.1. C 3235
6' CFS'//) C 3240
DA=DISTA(1,LL) C 3245
SA=SLOPA(1,LL) C 3250
SB=SLOPB(1,LL) C 3255
SC=SLOPC(1,LL) C 3260
IF(NOCB(1,LL).EQ.1.AND.NOCC(1,LL).EQ.1) GO TO 14 C 3265
IF(NOCB(1,LL).EQ.1) GO TO 32 C 3270
IF(NOCC(1,LL).EQ.1) GO TO 18 C 3275
10 WRITE(SYSOT,12)DISTA(1,LL),DISTB(1,LL),DISTC(1,LL),TAB7(LL). C 3280
11BFALL(1,LL),TCFALL(1,LL),ELINCA(1,LL),ELINCB(1,LL),ELINCC(1,LL). C 3285
2SLOPA(1,LL),SLOPB(1,LL),SLOPC(1,LL),VELA(1,LL),VELB(1,LL),VELC(1. C 3290
3LL),CRESA(1,LL),CRESB(1,LL),CRESA(1,LL) C 3295
12 FORMAT(30X,'CULVERT LENGTH ='F7.1,' FT'.6X,'CULVERT LENGTH =' C 3300
1F7.1,' FT'.6X,'CULVERT LENGTH ='F7.1,' FT'/30X,'FALL AT FACE C 3305
2='F7.2,' FT'.6X,'FALL AT FACE ='F7.2,' FT'.6X,'FALL AT FACE C 3310
3 ='F7.2,' FT'/30X,'ELEV FACE INVERT='F7.1,' FT'.6X,'ELEV FACE I C 3315
4NVERT='F7.1,' FT'.6X,'ELEV FACE INVERT='F7.1,' FT'/30X,'CULVERT C 3320
5SLOPE ='F9.4,7X,'CULVERT SLOPE ='F9.4,7X,'CULVERT SLOPE =' C 3325
6,F9.4/30X,'VEL AT DESIGN Q ='F7.1,' FPS'.5X,'VEL AT MAX Q =' C 3330
7F7.1,' FPS'.5X,'VEL AT DESIGN Q ='F7.1,' FPS'/30X,'MIN CREST LENG C 3335
8TH='F7.1,' FT'.6X,'MIN CREST LENGTH='F7.1,' FT'.6X,'MIN CREST LE C 3340
9NGTH='F7.1,' FT'//8X,'Q'.8X,'HWD'.20X,'Q'.8X,'HWF'.20X,'Q'.8X,'HW C 3345
AF'.20X,'Q'.8X,'HWF'//) C 3350
QD=Q1/BAR-(Q1/BAR*.2) C 3355
63 Q=QD C 3360
CALL COUT(Q,D,HWDOUT,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN) C 3365
HWD1=HWDOUT+1AB5(LL) C 3370
X=Q /D+.2.5 C 3375
CALL CEQUA(X,HWN,D,SA,I5) C 3380
HDCA=ELINCA(1,LL)+HWN C 3385
CALL CEQUA(X,HWN,D,SB,I5) C 3390
HDCB=ELINCB(1,LL)+HWN C 3395
CALL CEQUA(X,HWN,D,SC,I5) C 3400
HDCC=ELINCC(1,LL)+HWN C 3405
QU=QD*BAR C 3410
WRITE(SYSOT,85)QU,HWD1,QU,HDCA,QU,HDCB,QU,HDCC C 3415
85 FORMAT(3X,2F9.1,3(13X,F9.1,1X,F9.1)) C 3420
IF(QD.G1.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 206 C 3425
QD=QD+(Q1/BAR)*.2 C 3430
GO TO 63 C 3435
14 WRITE(SYSOT,16)DISTA(1,LL),TAB7(LL),ELINCA(1,LL),SLOPA(1,LL), C 3440
1VELA(1,LL),CRESA(1,LL) C 3445
16 FORMAT(30X,'CULVERT LENGTH ='F7.1,' FT'.19X,'---',26X,'---'/30X. C 3450
1'FALL AT FACE ='F7.2,' FT'.19X,'---',26X,'---'/30X,'ELEV FACE I C 3455
2NVERT='F7.1,' FT'.19X,'---',26X,'---'/30X,'CULVERT SLOPE ='F9.4. C 3460
320X,'---',26X,'---'/30X,'VEL AT DESIGN Q ='F7.1,' FPS'.18X,'---'. C 3465
426X,'---'/30X,'MIN CREST LENGTH='F7.1,' FT'.19X,'---',26X,'---'//8X. C 3470
5'Q'.8X,'HWD'.20X,'Q'.8X,'HWF'.20X,'Q'.8X,'HWF',18X,'Q'.8X,'HWF'//) C 3475
QD=Q1/BAR-(Q1/BAR*.2) C 3480
60 Q=QD C 3485
CALL COUT(Q,D,HWDOUT,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN) C 3490

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HWD1=HWOUT+TAB5(LL) C 3495
X=Q/D+.2.5 C 3500
CALL CEQUA(X,HWN,D,SA,I5) C 3505
HDCA=ELINCA(1,LL)+HWN C 3510
QU=QD+BAR C 3515
WRITE(SYSOT,186)QU,HWD1,QU,HDCA C 3520
186 FORMAT(3X,2F9.1,14X,2F9.1,20X,'---',8X,'---',18X,'---',8X,'---') C 3525
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 206 C 3530
QD=QD+(Q1/BAR)*.2 C 3535
GO TO 60 C 3540
18 WRITE(SYSOT,20)DISTA(1,LL),DISTB(1,LL),TAB7(LL),TBFALL(1,LL). C 3545
1ELINCA(1,LL),ELINCB(1,LL),SLOPA(1,LL),SLPB(1,LL),VELA(1,LL). C 3550
2VELB(1,LL),CRESA(1,LL),CRESB(1,LL) C 3555
20 FORMAT(30X,'CULVERT LENGTH =',F7.1,' FT',6X,'CULVERT LENGTH =', C 3560
1F7.1,' FT',14X,'--'/30X,'FALL AT FACE =',F7.2,' FT',6X,'FALL AT C 3565
2FACE =',F7.2,' FT',14X,'--'/30X,'ELEV FACE INVERT=',F7.1,' FT' C 3570
4,6X,'ELEV FACE INVERT=',F7.1,' FT',14X,'--'/30X,'CULVERT SLOPE = C 3575
5',F9.4,7X,'CULVERT SLOPE =',F9.4,15X,'--'/30X,'VEL AT DESIGN Q = C 3580
6',F7.1,' FPS',5X,'VEL AT MAX Q =',F7.1,' FPS',13X,'--'/30X,'MIN C 3585
7CREST LENGTH=',F7.1,' FT',6X,'MIN CREST LENGTH=',F7.1,' FT',14X, C 3590
8'--'/8X,'Q',8X,'HWO',20X,'Q',8X,'HWF',20X,'Q',8X,'HWF',18X,'Q', C 3595
98X,'HWF /) C 3600
QD=Q1/BAR-(Q1/BAR*.2) C 3605
64 Q=QD C 3610
CALL COUT(Q,D,HWOUT,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN) C 3615
HWD1=HWOUT+TAB5(LL) C 3620
X=Q/D+.2.5 C 3625
CALL CEQUA(X,HWN,D,SA,I5) C 3630
HDCA=ELINCA(1,LL)+HWN C 3635
CALL CEQUA(X,HWN,D,SB,I5) C 3640
HDCA=ELINCB(1,LL)+HWN C 3645
QU=QD+BAR C 3650
WRITE(SYSOT,183)QU,HWD1,QU,HDCA,QU,HDCA C 3655
183 FORMAT(3X,2F9.1,14X,2F9.1,14X,2F9.1,17X,'---',8X,'---') C 3660
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 206 C 3665
QD=QD+(Q1/BAR)*.2 C 3670
GO TO 64 C 3675
32 WRITE(SYSOT,24)DISTA(1,LL),DISTC(1,LL),TAB7(LL),TCFALL(1,LL). C 3680
1ELINCA(1,LL),ELINCC(1,LL),SLOPA(1,LL),SLPC(1,LL),VELA(1,LL). C 3685
2VELC(1,LL),CRESA(1,LL),CRESC(1,LL) C 3690
24 FORMAT(30X,'CULVERT LENGTH =',F7.1,' FT',19X,'---',15X,'CULVERT LE C 3695
1NGTH =',F7.1,' FT',30X,'FALL AT FACE =', C 3700
2F7.2,' FT',19X,'---',15X,'FALL AT FACE =', C 3705
3 F7.2,' FT',30X,'ELEV FACE INVERT=',F7.1,' FT',19X,'---' C 3710
4,15X,'ELEV FACE INVERT=',F7.1,' FT',30X,'CULVERT SLOPE =',F9.4, C 3715
520X,'--',15X,'CULVERT SLOPE =',F9.4/30X,'VEL AT DESIGN Q=',F7.1, C 3720
6' FPS',19X,'--',15X,'VEL AT DESIGN Q =',F7.1,' FPS',30X,'MIN CREST C 3725
7LENGTH=',F7.1,' FT',19X,'---',15X,'MIN CREST LENGTH=',F7.1,' FT'// C 3730
88X,'Q',8X,'HWO',20X,'Q',8X,'HWF',20X,'Q',8X,'HWF',18X,'Q',8X, C 3735
9'HWF /) C 3740
QD=Q1/BAR-(Q1/BAR*.2) C 3745
66 Q=QD C 3750
CALL COUT(Q,D,HWOUT,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN) C 3755
HWD1=HWOUT+TAB5(LL) C 3760
X=Q/D+.2.5 C 3765

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CALL CEQUA(X,HWN,D,SA,I5)	C 3770
HDCA=ELINCA(1,LL)+HWN	C 3775
CALL CEQUA(X,HWN,D,SC,I5)	C 3780
HDCC=ELINCC(1,LL)+HWN	C 3785
QU=QD+BAR	C 3790
WRITE(SYSOT,180)QU,HWO1,QU,HDCA,QU,HDCC	C 3795
180 FORMAT(JX,2F9.1,14X,2F9.1,19X,'--',8X,'--',13X,2F9.1)	C 3800
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 206	C 3805
QD=QD+(Q1/BAR)*.2	C 3810
GO TO EG	C 3815
206 I4=4	C 3820
I5=6	C 3825
C	C 3830
C.....BEVELED INLETS	C 3835
C	C 3840
212 DA=DISTA(2,LL)	C 3845
SA=SLOPA(2,LL)	C 3850
SB=SLOPB(2,LL)	C 3855
SC=SLOPC(2,LL)	C 3860
IF(NDCA(2,LL).EQ.0) GO TO 208	C 3865
WRITE(SYSOT,211) I1,I2,I3,I4,I5,TQMAX(2,LL)	C 3870
211 FORMAT(//1X,'BEVELED INLET DESIGN FOR CULVERT CODE: ',5I1/1X,'***	C 3875
1*****'///20X,'DESIGN DATA	C 3880
2 NOT APPLICABLE BECAUSE THE REQUIRED FALL FOR THE BEVEL-EDGED INLE	C 3885
3T EXCEEDS 1.5D OR L50'/20X,'THIS OUTPUT CONSISTS OF THE OUTLET CON	C 3890
4TROL PERFORMANCE CURVE DATA FOR KE = 0.2'/20X,'WHICH IS APPLICABLE	C 3895
5 FOR THE IMPROVED INLETS.'//30X,'Q',10X,'HWO',15X,'MAX Q = ',	C 3900
6F7.0,' CFS'//)	C 3905
2-0 QD=Q1/BAR-(Q1/BAR*.2)	C 3910
214 Q=QD	C 3915
CALL COUT(Q,D,HWO1,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN)	C 3920
HWO1=HWO1+TAB5(LL)	C 3925
QU=QD+BAR	C 3930
241 WRITE(SYSOT,243)QU,HWO1	C 3935
243 FORMAT(26X,F7.1,6X,F6.1)	C 3940
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 330	C 3945
QD=QD+(Q1/BAR)*.2	C 3950
GO TO 214	C 3955
208 WRITE(SYSOT,213) I1,I2,I3,I4,I5,CKE(I4),TQMAX(2,LL)	C 3960
213 FORMAT(//1X,'BEVELED INLET DESIGN FOR CULVERT CODE: ',5I1/	C 3965
14X,'.....'//	C 3970
2*****'//	C 3975
3F4.1,16X,'MIN FALL CURVE',17X,'MAX Q CURVE',21X,'MIN HW CURVE'//	C 3980
4/67X,'MAX Q = ',F7.0,' CFS'//)	C 3985
IF(NDCB(2,LL).EQ.1.AND.NDCC(2,LL).EQ.1) GO TO 25	C 3990
IF(NDCB(2,LL).EQ.1) GO TO 22	C 4000
IF(NDCC(2,LL).EQ.1) GO TO 28	C 4005
21 WRITE(SYSOT,2)DISTA(2,LL),DISTB(2,LL),DISTC(2,LL),TAB10(LL),	C 4010
1TBFA(2,LL),TCFA(2,LL),ELINCA(2,LL),ELINCB(2,LL),ELINCC(2,LL),	C 4015
2SLOPA(2,LL),SLOPB(2,LL),SLOPC(2,LL),VELA(2,LL),VELB(2,LL),VELC(2,	C 4020
3LL),CRESA(2,LL),CRESB(2,LL),CRESC(2,LL)	C 4025
QD=Q1/BAR-(Q1/BAR*.2)	C 4030
38 Q=QD	C 4035
	C 4040

CALL COUT(Q,D,HWO2,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN)	C 4045
HWO2=HWO2+TAB5(LL)	C 4050
X= Q/D*.25	C 4055
CALL CEQUA(X,HWN,D,SA,I5)	C 4060
HDCA=ELINCA(2,LL)+HWN	C 4065
CALL CEQUA(X,HWN,D,SB,I5)	C 4070
HDCB=ELINCB(2,LL)+HWN	C 4080
CALL CEQUA(X,HWN,D,SC,I5)	C 4085
HDCC=ELINCC(2,LL)+HWN	C 4090
QU=QD*BAR	C 4095
WRITE(SYSOT,85)QU,HWO2,QU,HDCA,QU,HDCB,QU,HDCC	C 4100
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 330	C 4105
QD=QD+(Q1/BAR)*.2	C 4110
GO TO 88	C 4115
25 WRITE(SYSOT,16)DISTA(2,LL),TAB10(LL),ELINCA(2,LL),SLOPA(2,LL),	C 4120
1VELA(2,LL),CRESA(2,LL)	C 4125
QD=Q1/BAR-(Q1/BAR*.2)	C 4130
62 Q=QD	C 4135
CALL COUT(Q,D,HWO2,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN)	C 4140
HWO2=HWO2+TAB5(LL)	C 4145
X= Q/D*.25	C 4150
CALL CEQUA(X,HWN,D,SA,I5)	C 4155
HDCA=ELINCA(2,LL)+HWN	C 4160
QU=QD*BAR	C 4165
WRITE(SYSOT,186)QU,HWO2,QU,HDCA	C 4170
IF(QD.GT.(Q1/BAR+6*((Q1/BAR)*.2)+5.)) GO TO 330	C 4175
QD=QD+(Q1/BAR)*.2	C 4180
GO TO 62	C 4185
28 WRITE(SYSOT,20)DISTA(2,LL),DISTB(2,LL),TAB10(LL),TBFALL(2,LL),	C 4190
1ELINCA(2,LL),ELINCB(2,LL),SLOPA(2,LL),SLCPB(2,LL),VELA(2,LL),	C 4195
2VELB(2,LL),CRESA(2,LL),CRESB(2,LL)	C 4200
QD=Q1/BAR-(Q1/BAR*.2)	C 4205
66 Q=QD	C 4210
CALL COUT(Q,D,HWO2,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN)	C 4215
HWO2=HWO2+TAB5(LL)	C 4220
X= Q/D*.25	C 4225
CALL CEQUA(X,HWN,D,SA,I5)	C 4230
HDCA=ELINCA(2,LL)+HWN	C 4235
HDCB=ELINCB(2,LL)+HWN	C 4240
QU=QD*BAR	C 4245
WRITE(SYSOT,183)QU,HWO2,QU,HDCA,QU,HDCB	C 4250
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 330	C 4255
QD=QD+(Q1/BAR)*.2	C 4260
GO TO 66	C 4265
22 WRITE(SYSOT,24)DISTA(2,LL),DISTC(2,LL),TAB10(LL),TCFALL(2,LL),	C 4270
1ELINCA(2,LL),ELINCC(2,LL),SLOPA(2,LL),SLCPC(2,LL),VELA(2,LL),	C 4275
2VELC(2,LL),CRESA(2,LL),CRESC(2,LL)	C 4280
QD=Q1/BAR-(Q1/BAR*.2)	C 4285
87 Q=QD	C 4290
CALL COUT(Q,D,HWO2,VELOUT,DEP,DN,DC,DIST1,SLOPE,CN)	C 4295
HWO2=HWO2+TAB5(LL)	C 4300
X= Q/D*.25	C 4305
CALL CEQUA(X,HWN,D,SA,I5)	C 4310
HDCA=ELINCA(2,LL)+HWN	C 4315
CALL CEQUA(X,HWN,D,SC,I5)	C 4320

	HDCC=ELINCC(2,LL)+HWN	C 4320
	QU=QD+BAR	C 4325
	WRITE(SYSOT,180)QU,HWO2,QU,HDCA,QU,HDCC	C 4330
	IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 330	C 4335
	QD=QD+(Q1/BAR)*.2	C 4340
	GO TO 87	C 4345
C		C 4350
C	SIDE TAPERED INLETS	C 4355
C	330 IF(ITAB(LL).GT.2) WRITE(SYSOT,250)	C 4360
C	250 FORMAT(// ' IMPROVED-INLET DESIGN'/5X,'*****'/////	C 4365
C	135X,'NO IMPROVED-INLET DESIGNS AVAILABLE FOR CULVERTS HAVING MORE	C 4370
C	1THAN " 2 " BARRELS ')	C 4375
C	IF(ITAB(LL).GT.2) GO TO 362	C 4380
C	330 INDEX=2	C 4385
C	CALL CSIDE( D,FALL,HWT,TRDEL,IBAR,DIST ,INDEX,SLOPE,CN)	C 4390
C		C 4395
C	SLOPE TAPERED INLETS	C 4400
C	CALL CSLDPV( D,SLOPE)	C 4405
C	CALL CSLDPM(B,D,SLOPE)	C 4410
C	362 LL=LL+1	C 4415
	IF(LL.GT.L) RETURN	C 4420
	I4=II4	C 4425
	I5=II5	C 4430
	GO TO 100	C 4435
	END	C 4440



C	STANDARD SIDE-TAPERED INLET DESIGN EQUATIONS FOR BF AND L1	C 4720 **
	BF=1.5*D	C 4725
42	L1=1.4167*D	C 4730
C	HEC-13 SIDE-TAPERED INLET DESIGN EQUATIONS FOR BF AND L1	C 4735 **
C	BF=(Q1/BAR)/(YC19*(3.1416/4.)*E**1.5)	C 4740
C	42 L1=((BF-D)/2.)*TAPER	C 4745
	TAPER=L1/((BF-D)/2.)	C 4750
	DLEFT=DIL +L1	C 4755
	DROP= DLEFT*SLOPE	C 4760
	SUBT=DIST1-L1	C 4765
	STROEL=ELIN -DROP	C 4770
	FAHC=STROEL+SLOPE*L1	C 4775
	DIF=STROEL-TROEL	C 4780
	IF(DIF.LE.0.0) GO TO 10	C 4785
C	COMPUTE FALL	C 4790
	FALL=DIF+L1*SLOPE	C 4795
	HWT=AHWEL	C 4800
3	IF(INDEX.EQ.1) RETURN	C 4805
	IF(INDEX.EQ.2) GO TO 5	C 4810
	IF(INDEX.EQ.3) GO TO 5	C 4815
	INDEX=INDEX+1	C 4820
	X=(HT-L1*SLOPE)/D	C 4825
	GO TO 20	C 4830
5	BIT=SEL*DIF	C 4835
	SUBT=SUBT+BIT	C 4840
	TOTA=SUBT+L1	C 4845
	SA=(TROEL-TCOEL)/SUBT	C 4850
	STFACE=STROEL+SLOPE*L1+BIT*SLOPE	C 4855
	ELFACA=TROEL+SA*L1	C 4860
	ELTRCA=TROEL	C 4865
	IF(FALL.LT.D/4.) WA=0.0	C 4870
	IF(FALL.LT.D/4.)GO TO 100	C 4875
C.....	MINIMUM CREST LENGTH - CHART 17 - HEC 13	C 4880
	HCA=FAHC+(FALL*SEL*SLOPE)+(FALL*3.+D/2.)*SLOPE	C 4885
	HC=AHWEL-HCA	C 4890
	IF(HC.LT.1.) HC=1.0	C 4895
	W23A=(.5*Q1**1.6667)/HC	C 4900
	WA=W23A**1.5	C 4905
	GO TO 100	C 4910
C	NO FALL	C 4915
10	WA=0.0	C 4920
	FALL=FACE1-STROEL	C 4925
	TROEL=STROEL	C 4930
	HWT=TROEL-HT	C 4935
	IF(INDEX.EQ.1)RETURN	C 4940
	IF(INDEX.EQ.0) GO TO 3	C 4945
	ELFACA=TROEL+SLOPE*L1	C 4950
	TOTA=SUBT+L1	C 4955
	ELTRCA=TROEL	C 4960
	SA=SLOPE	C 4965
	STFACE=ELFACA	C 4970
100	SLO=SA	C 4975
	BAR=IBAR	C 4980
	O=Q1/BAR	C 4985
	CALL COUT(Q, D,HWOUT,VELOUT,DEP,DN,DC, SUBT,SLO,AN)	C 4990

CALL CROUT(DN,AREA,T,WP,D ,R)	C 4995
VELAA=C /AREA	C 5000
IF(VELOUT.GT.VELAA) VELAA=VELOUT	C 5005
BEA=BF*.5	C 5010
DEA=D*.5	C 5015
101 INDEX=INDEX+1	C 5020
IF(INDEX.EQ.4) GO TO 102	C 5025
X=(HT-L1*SA)/D	C 5030
GO TO 20	C 5035
C COMPUTE CURVE B - SIDE TAPER	C 5040
102 INDEX=2	C 5045
HWTEMP=HWT	C 5050
FALLM=1.5*D	C 5055
FALLT=SUBT*SLOPE	C 5060
IF(FALLM.GT.FALLT) FALLM=FALLT	C 5065
QUE= TAB16(LL)/BAR	C 5070
GO TO (12,14),I1	C 5075
12 HTOVD=.0341*(QUE/D**2.5)**2+.89	C 5080
GO TO 15	C 5085
14 HTOVD=.0318*(QUE/D**2.5)**2+.89	C 5090
15 HWATER=HTOVD*D	C 5095
TEMP=ELTRCA+HWATER	C 5100
IF(TEMP.LE.AHWEL)GO TO 466	C 5105
BFALL=TEMP-AHWEL	C 5110
TBFAL =BFALL+FALL	C 5115
ELTRCB=ELTRCA-BFALL	C 5120
IF(TBFAL.GT.FALLM) ELTRCB=ELTRCA-(FALLM-FALL)	C 5125
IF(ELTRCB.LT.TOEL) ELTRCB=TOEL+.01	C 5130
BFALL=ELTRCA-ELTRCB	C 5135
TBFAL=BFALL+FALL	C 5140
BITB=SEL+BFALL	C 5145
SB=(ELTRCB-TOEL)/(SUBT+BITB)	C 5150
AIN= 50.	C 5155
QUE=Q1/BAR	C 5160
470 QUE=QUE+AIN	C 5165
GO TO (17,18),I1	C 5170
17 HTOVD=.0341*(QUE/D**2.5)**2+.89	C 5175
GO TO 19	C 5180
18 H OVD=.0318*(QUE/D**2.5)**2+.89	C 5185
19 HIGH=HTOVD*D	C 5190
HI=HIGH+ELTRCB	C 5195
IF(HI.GT.AHWEL) GO TO 474	C 5200
H=HIGH	C 5205
GO TO 470	C 5210
474 QUE=QUE-AIN	C 5215
IF(AIN.LT.10.) GO TO 475	C 5220
AIN=2.0	C 5225
GO TO 470	C 5230
4 5 IF(QUE.GT.TAB16(LL)/BAR) QUE=TAB16(LL)/BAR	C 5235
X=(AHWEL-ELTRCB-L1*SB)/D	C 5240
X=ALOG10(X)	C 5245
YC19=.4140027+1.327566*X-.722612*X*X+.155368*X*X*X	C 5250
1-.4421735*X-X*X*X+.5065368*X*X*X*X	C 5255
YC19=10**YC19	C 5260
C BFB=QUE/(YC19*.7854-E**1.5)	C 5265

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C      L1B=((BFB-D)/2.)*TAPER
      BFB=1.5*D
      L1B=1.4167*D
      TOTB=SUBT+L1B+BITB
      ELFACB=ELTRCB+L1B*SB
      QQ=QUE/BAR
      TB=SUBT+BITB
      CALL COUT(QQ, D,HWOUT,VELOUT,DEP,DN,DC, SUBT,SLO,AN)
      CALL CROUT(DN,AREA,T,WP,D ,R)
      VELBB=QQ/AREA
      IF(VELOUT.GT.VELBB) VELBB=VELOUT
C.....MINIMUM CREST LENGTH - CHART 17 - HEC 13
      HCB=FAHC+(TBFAL*SEL*SLOPE)+(TBFAL*3.+D/2.)*SLOPE
      HC=AHWEL-HCB
      IF(HC.LT.1.) HC=1.0
      W23B=(.3*QQ**1.6667)/HC
      WB=W23B**1.5
      BFB=BFB*.5
      DEB=D*.5
      GO TO 490
466  TBFAL =0.0
      NOCBS=1
C      COMPUTE CURVE C - SIDE TAPER
490  TEMP=ELTRCA+HT
      IF(TAB4(LL).GE.TEMP) GO TO 482
      CFAL=TEMP-TAB4(LL)
      TCFAL=CFAL+FALL
      ELTRCC=ELTRCA-CFAL
      IF(TCFAL.GT.FALLM) ELTRCC=ELTRCA-(FALLM-FALL)
      IF(ELTRCC.LT.TOEL) ELTRCC=TOEL+.01
      CFAL=ELTRCA-ELTRCC
      TCFAL=CFAL+FALL
      BITC=SEL*CFAL
      SC=(ELTRCC-TOEL)/(SUBT+BITC)
      X=(TEMP -CFAL-ELTRCC-L1*SC)/D
      X=ALOG10(X)
      YC19=.4140027+1.327566*X-.722612*X*X+.155368*X*X*X
      1-.4421735*X*X*X*X+.5065368*X*X*X*X*X
      YC19=10**YC19
      BFC=1.5*D
      L1C=1.4167*D
C      BFC=(Q1/BAR)/(YC19*.7854*E**1.5)
C      L1C=((BFC-D)/2.)*TAPER
      TOTC=SUBT+L1C+BITC
      ELFACC=ELTRCC+L1C*SC
C.....MINIMUM CREST LENGTH - CHART 17 - HEC 13
      HCC=FAHC+(TCFAL*SEL*SLOPE)+(TCFAL*3.+D/2.)*SLOPE
      HC=TEMP-HCC
      IF(HC.LT.1.) HC=1.0
      W23C=(.5*Q1**1.6667)/HC
      WC=W23C**1.5
      SLO=SC
      TC=SUBT+BITC
      CALL COUT(Q, D,HWOUT,VELOUT,DEP,DN,DC, SUBT,SLO,AN)
      CALL CROUT(DN,AREA,T,WP,D ,R)

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C 5270
C 5275
C 5280
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C 5495
C 5500
C 5505
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C 5515
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C 5525
C 5530
C 5535
C 5540

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VELCC=(Q1/342)/AREA
IF(VELOUT.GT.VELCC) VELCC=VELOUT
BEC=BFC*.5
DEC=D*.5
GO TO 483
482 TCFAL=0.0
NOCCS=1
483 QUE=QUE*BAR
WRITE(SYSOT,104) TAPER,E,QUE,BF,L1
104 FORMAT(///1X,'SIDE TAPERED INLET DESIGN'/'*****
1***',10X,'FACE EDGE BEVELS = 45 DEG',5X,'SIDE TAPER=',F6.3,'/'//
2 10X,'MIN FALL DESIGN',30X,'MAX Q DESIGN',30X,'MIN HW DESIG
3N',10X,'E = D =',F6.2,' FT',29X,'MAX Q =',F7.0,' CFS'/10X,'FACE
4WIDTH= 1.5D=',F6.2,' FT'/10X,'L1= 1.4167D=',F6.2,' FT'//)
IF(NOCCS.EQ.0.AND.NOCCS.EQ.0) GO TO 30
IF(NOCCS.EQ.0) GO TO 32
IF(NOCCS.EQ.0) GO TO 34
WRITE(SYSOT,28)TOTA,TAB13(LL),TAB14(LL),ELFACA,SA,VELAA, WA.
1BEA,DEA
28 FORMAT(5X,'CULVERT LENGTH =',F7.1,' FT',26X,'--',44X,'--'/5X,
1'FALL',14X,'=',F7.1,' FT',26X,'--',44X,'--'/5X,'ELEV THROAT INVERT
2=',F7.1,' FT',26X,'--',44X,'--'/5X,'ELEV FACE INVERT =',F7.1,' FT,
3',26X,'--',44X,'--'/5X,'CULVERT SLOPE',5X,'=',F7.4,29X,'--',44X,'-
4-'/5X,'VEL AT DESIGN Q =',F6.1,' FPS',26X,'--',44X,'--'/
6 5X,'MIN CREST LENGTH =',F7.1,' FT',26X,'-
7-',44X,'--'/5X,'BEVELS = 45 DEGREE',36X,'--',44X,'--'/9X,'B =',
8F5.1,' IN D =',F5.1,' IN',27X,'--',44X,'--'/5X,'Q',8X,'HWT',8X,
9'HWF',32X,'--',44X,'--'/)
C-----PERFORMANCE CURVE DATA
QD=Q1-Q1*.2
QD=QD*BAR
29 X=QD/D*.25
X=ALOG10(X)
GO TO (40,41),I1
40 HTOVD=-.233392+.489125*X+1.068638*X*X-3.074435*X*X*X
1+3.711165*X*X*X*X-1.32836*X*X*X*X*X
GO TO 43
41 HTOVD=-.237139+.146792*X+2.189321*X*X-4.354114*X*X*X
1+4.210539*X*X*X*X-1.347032*X*X*X*X*X
43 HT=10.*HTOVD
HWTA=ELFRCA+HT
X=QD*(3F*.7854+E*.1.5)
X=ALOG10(X)
Y=-.2676+.01765*X-.11698*X*X+.41498*X*X*X
HFOVE=10.*Y
HWFA=ELFACA+HFOVE+E
QU=QD*BAR
WRITE(SYSOT,27)QU,HWTA,HWFA
27 FORMAT(3X,F7.1,2X,F7.1,3X,F7.1,31X,'--',44X,'--')
IF(QD.GT.(Q1/342+(Q1/342*.2)+5.)) GO TO 480
QD=QD+(Q1*.2)/342
GO TO 29
30 WRITE(SYSOT,332)TOTA,TOTB,TOTC,TAB13(LL),TBFAL,TCFAL,TAB14(LL),
1ELTRCB,ELTRCC,
2ELFACA,ELFACB,ELFACC,SA,SB,SC,VELAA,VELBB,VELCC

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C 5545  
C 5550  
C 5555  
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C 5775  
C 5780  
C 5785  
C 5790  
C 5795  
C 5800  
C 5805  
C 5810  
C 5815



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332 FORMAT( 5X,'CULVERT LENGTH      ',F7.1,' FT',20X,'CULVERT LENGTH      ' C 5820
1  =',F7.1,' FT',15X,'CULVERT LENGTH      ',F7.1,' FT'/ C 5825
2  5X,'FALL',14X,'=',F7.2,' FT',20X,'FALL',14X,'=',F7.2,' FT', C 5830
3  15X,'FALL',14X,'=',F7.2,' FT'/5X,'ELEV THROAT INVERT=',F7.1, C 5835
4  ' FT',20X,'ELEV THROAT INVERT=',F7.1,' FT',15X,'ELEV THROAT INVER C 5840
5T=',F7.1,' FT'/5X,'ELEV FACE INVERT      ',F7.1,' FT',20X,'ELEV FACE C 5845
6INVERT      ',F7.1,' FT',15X,'ELEV FACE INVERT      ',F7.1,' FT'/ 5X, C 5850
7 'CULVERT SLOPE      ',F7.4,23X,'CULVERT SLOPE      ',F7.4,18X, C 5855
8 'CULVERT SLOPE      ',F7.4/ 5X,'VEL AT DESIGN Q      ',F6.1,' FPS', C 5860
920X,'VEL AT MAX Q      ',F6.1,' FPS',15X,'VEL AT DESIGN Q      ', C 5865
AF6.1,' FT') C 5870
WRITE(SYSQT,504) WA,WB,WC,BEA,DEA,BEB,DEB,BEC,DEC C 5875
504 FORMAT( C 5880
2 5X,'MIN CREST LENGTH      ',F7.1,' FT',20X,'MIN CREST LENGTH      ', C 5885
3F7.1,' FT',15X,'MIN CREST LENGTH      ',F7.1,' FT'/5X,'BEVELS = 45 D C 5890
4EGREE',30X,'BEVELS = 45 DEGREE',25X,'BEVELS = 45 DEGREE'/9X,'B = C 5895
5',F5.1,' IN D =',F5.1,' IN',24X,'B =',F5.1,' IN D =',F5.1,' IN', C 5900
622X,'B =',F5.1,' IN D =',F5.1,' IN'//5X,'Q',8X,'HWT',8X,'HWF', C 5905
729X,'Q',8X,'HWT',8X,'HWF',20X,'Q',8X,'HWT',8X,'HWF'/) C 5910
QD=Q1-(Q1*.2) C 5915
QD=QD/BAR C 5920
31 X=QD/D*.25 C 5925
X=ALOG10(X) C 5930
GO TO (46,44),I1 C 5935
46 HTOVD=-.233392+.489125*X+.068638*X*X-3.074435*X*X*X C 5940
1+3.711165*X*X*X*X-1.32836*X*X*X*X*X C 5945
GO TO 45 C 5950
44 HTOVD=-.237139+.146792*X+.2.189321*X*X-4.354114*X*X*X C 5955
1+4.210539*X*X*X*X-1.347032*X*X*X*X*X C 5960
45 HT=10.**HTOVD*D C 5965
HWTA=ELTRCA+HT C 5970
HWTB=ELTRCB+HT C 5975
HWTC=ELTRCC+HT C 5980
X=QD/(BF*.7854*E**1.5) C 5985
X=ALOG10(X) C 5990
Y=-.2676+.61766*X-.11698*X*X+.41498*X*X*X C 5995
HFOVE=10.**Y C 6000
HWFA=ELFACA+HFOVE*E C 6005
X=QD/(BF*.7854*E**1.5) C 6010
X=ALOG10(X) C 6015
Y=-.2676+.61766*X-.11698*X*X+.41498*X*X*X C 6020
HFOVE=10.**Y C 6025
HWFB=ELFACB+HFOVE*E C 6030
X=QD/(BFC*.7854*E**1.5) C 6035
X=ALOG10(X) C 6040
Y=-.2676+.61766*X-.11698*X*X+.41498*X*X*X C 6045
HFOVE=10.**Y C 6050
HWFC=ELFACC+HFOVE*E C 6055
QU=QD*BAR C 6060
WRITE(SYSQT,36)QU,HWTA,HWFA,QU,HWTB,HWFB,QU,HWTC,HWFC C 6065
36 FORMAT(3X,F7.1,2X,F7.1,3X,F7.1,22X,F9.1,1X,F9.1,3X,F9.1,13X, C 6070
12F9.1,2X,F9.1) C 6075
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 480 C 6080
QD=QD+(Q1/BAR)*.2 C 6085
GO TO 31 C 6090

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32 WRITE(SYSOT,110)TOTA,TOTB,TAB13(LL),TBFAL,TAB14(LL),ELTRCB,ELFACA. C 6095
1ELFACB,SA,SB,VELAA,VELBB C 6100
110 FORMAT(5X,'CULVERT LENGTH =',F7.1,' FT',20X,'CULVERT LENGTH C 6105
1=',F7.1,' FT',21X,'--'/5X,'FALL',14X,'=',F7.1,' FT',20X,'FALL',14X C 6110
2=',F7.1,' FT',21X,'--'/5X,'ELEV THROAT INVERT=',F7.1,' FT',20X. C 6115
3'ELEV THROAT INVERT=',F7.1,' FT',21X,'--'/ 5X,'ELEV FACE INVERT C 6120
4=',F7.1,' FT',20X,'ELEV FACE INVERT =',F7.1,' FT',21X,'--'/ 5X. C 6125
5'CULVERT SLOPE',5X,'=',F7.4,23X,'CULVERT SLOPE',5X,'=',F7.4,24X,'- C 6130
6-'/ 5X,'VEL AT DESIGN Q =',F6.1,' FPS',20X,'VEL AT MAX Q = C 6135
7',F6.1,' FPS',21X,'--') C 6140
WRITE(SYSOT,112) WA ,WB,BEA,DEA,BEB,DEB C 6145
112 FORMAT(5X,'MIN CREST LENGTH =',F7.1,' FT',20X,'MIN CREST LENGTH C 6150
2=',F7.1,' FT',21X,'--'/5X,'BEVELS = 45 DEGREE',31X,'BEVELS = 45 C 6155
3DEGREE',27X,'--'/9X,'B =',F5.1,' IN D =',F5.1,' IN',25X,'B =', C 6160
4'F5.1,' IN D =',F5.1,' IN',27X,'--'/5X,'Q',8X,'HWT',8X,'HWF', C 6165
529X,'Q',8X,'HWT',8X,'HWF',26X,'--'/) C 6170
QD=Q1-(Q1*.2) C 6175
QD=QD/BAR C 6180
33 X=.D'D*.2.5 C 6185
X=ALOG10(X) C 6190
GO TO (56,57),I1 C 6195
56 HTOVD=-.233392+.489125*X+1.068638*X*X-3.074435*X*X*X C 6200
1+3.711165*X*X*X*X-1.32836*X*X*X*X*X C 6205
GO TO 58 C 6210
57 HTOVD=-.237139+.146792*X+2.189321*X*X-4.354114*X*X*X C 6215
1+4.210539*X*X*X*X-1.347032*X*X*X*X*X C 6220
58 HT=10.**HTOVD*D C 6225
HWTB=ELTRCA+HT C 6230
HWTB=ELTRCB+HT C 6235
X=QD/(BF*.7854*E**1.5) C 6240
X=ALOG10(X) C 6245
Y=-.2676+.61766*X-.11698*X*X+.41498*X*X*X C 6250
HFOVE=10.**Y C 6255
HWFA=ELFACA+HFOVE*E C 6260
X=QD/(BFB*.7854 *E**1.5) C 6265
X=ALOG10(X) C 6270
Y=-.2676+.61766*X-.11698*X*X+.41498*X*X*X C 6275
HFOVE=10.**Y C 6280
HWFB=ELFACB+HFOVE*E C 6285
QU=QD*BAR C 6290
WRITE(SYSOT,38)QU,HWTB,HWFA,QU,HWTB,HWFB C 6295
38 FORMAT(3X,F7.1,2X,F7.1,3X,F7.1,22X,F9.1,1X,F9.1,3X,F9.1. C 6300
130X,'--') C 6305
IF(QD.GT.(Q1/BAR+6*((Q1/BAR)*.2)+5.)) GO TO 480 C 6310
QD=QD+(Q1/BAR)*.2 C 6315
GO TO 33 C 6320
34 WRITE(SYSOT,106)TOTA,TOTC,TAB13(LL),TCFAL,TAB14(LL),ELTRCC,ELFACA C 6325
1,ELFACC,SA,SC,VELAA,VELCC, WA,WC,BEA,BEA,DEC C 6330
106 FORMAT(5X,'CULVERT LENGTH =',F7.1,' FT',26X,'--',.36X,'CULVERT L C 6335
1LENGTH =',F7.1,' FT',5X,'FALL',14X,'=',F7.1,' FT',26X,'--',.36X. C 6340
2'FALL',14X,'=',F7.1,' FT',5X,'ELEV THROAT INVERT=',F7.1,' FT',26X. C 6345
3'--',.36X,'ELEV THROAT INVERT=',F7.1,' FT',5X,'ELEV FACE INVERT =', C 6350
5,F7.1,' FT',26X,'--',.36X,'ELEV FACE INVERT =',F7.1,' FT',5X,'CUL C 6355
6VERT SLOPE',5X,'=',F7.4,29X,'--',.36X,'CULVERT SLOPE',5X,'=',F7.4/ C 6360
75X,'VEL AT DESIGN Q =',F7.1,' FPS',26X,'--',.36X,'VEL AT DESIGN Q C 6365

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SUBROUTINE CSLOPV( D,SLOPE)
DESIGN SLOPE-TAPERED INLETS                - VERTICAL FACE

COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),
3TQVAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),
4L,LL,K,SYSIN,SYSOT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),
5      IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),
8SLDPR(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,DISR,SFACE,
ADIA1, DIA2, ELLE, ELRR, NOCBS, HWTEMP, KBA51, KBA52, KDEP1, KDEP2
DIMENSION FALL(2),S(2),L1(2),L2(2),L3(2),VEL(2),BF(2),
1TAPER(2),NOC(2),DA(2)
INTEGER SYSIN, SYSOT
REAL L1, L2, L3, L4, L150
460 ISLOPE=0
HW=0.0
BAR=ITAB(LL)
QS=Q1/BAR
CN=TAB2(LL)
NOC(1)=0
NOC(2)=0
B=D
I=1
TAPER(1)=4.0
TAPER(2)=4.0
Y1=(D + .2/(SFACE**2+1.))**.5
Y2=Y1/SFACE
DY=SFACE*Y1+Y2
SMAL3=(SLOPE*SEL**2*DY)/(1.+SLOPE*SEL)
DIL3=SEL*DY-SMAL3
EL3=DIL3+SLOPE
FACEL=ELIN-EL3
TOEL=ELOUT+ELR
DIST=(FACEL-TOEL)/SLOPE

DO 14 I=1,2
TRDEL=TAB14(LL)
TRDEL=TRDEL
14 FALL(I)=FACEL-TRDEL
IF(TAB14(LL).EQ.0.0) NOC(2)=1
IF(TRDEL.LE.TOEL) NOC(I)=1
IF(FALL(I).LT.(D/4.).OR.FALL(I).GT.(1.5*D))NOC(I)=1
IF(NOC(I).EQ.1) GO TO 481
24 HW=HWTEMP-FACEL
X=HW/D
Y21=-2.265863+7.942441*X-4.0350294*X*X+1.619481*X*X*X-.3458214*X
1*X*X*X+.02846767*X*X*X*X*X
C.....COMPUTE FACE WIDTH FROM CHART 16 - HEC-13
BF(1)=QS/(Y21-D**1.5)+.1
L1(I)=(BF(I)-B)/2.*TAPER(I)
26 S(I)=(DIST*SLOPE-FALL(I))/(DIST-L1(I)-D/2.)

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C 6550
C 6555
C 6560
C 6565
C 6570
C 6575
C 6580
C 6585
C 6590
C 6595
C 6600
C 6605
C 6610
C 6615
C 6620
C 6625
C 6630
C 6635
C 6640
C 6645
C 6650
C 6655
C 6660
C 6665
C 6670
C 6675
C 6680
C 6685
C 6690
C 6695
C 6700
C 6705
C 6710
C 6715
C 6720
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C 6730
C 6735
C 6740
C 6745
C 6750
C 6755
C 6760 **
C 6765
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C 6775
C 6780
C 6785
C 6790
C 6795
C 6800
C 6805
C 6810
C 6815
C 6820

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DIF=FACEL+DY-(TROE+(D**2+(D*S(I))**2)**.5)
L3(I)=.5*B
28 L2(I)=L1(I)-L3(I)
SF=L2(I)/(DIF-S(I)*L1(I)-S(I)*(D/2.))+L2(I)*S(I)
IF(SF.EQ.SFACE) GO TO 450
IF(SF.LT.SFACE) GO TO 30
SF=SFACE
L2(I)=(SF*(DIF-S(I)*L1(I)-S(I)*(D/2.)))/(1.-S(I)*SF)
L3(I)=L1(I)-L2(I)
GO TO 450
30 SF=SFACE
L2(I)=(SF*(DIF-S(I)*L1(I)-S(I)*(D/2.)))/(1.-S(I)*SF)
L1(I)=L2(I)+L3(I)
TAPER(I)=2.*L1(I)/(BF(I)-B)
450 S(I)=(DIST*SLOPE-FALL(I))/(DIST-L1(I)-D/2.)
SLO=S(I)
DA(I)=DIST
DD=DA(I)-L1(I)
CALL COUT(QS, D,HWOUT,VELOUT,DEP,DN,DC,DD,SLO,CN)
CALL CROUT(DN,AREA,T,WP,D ,R)
VELIN=QS/AREA
IF(VELIN.GT.VELOUT) GO TO 152
VEL(I)=VELOUT
GO TO 122
152 VEL(I)=VELIN
122 IBAR=BAR
481 QS=QOE /BAR
IF(NOCBS.EQ.1) NOC(2)=1
IF(NOCBS.EQ.1) GO TO 483
TRDE=ELTRCB
I=I+1
IF(I.EQ.3) GO TO 483
GO TO 14
483 WRITE(SYSOT,479) DIL3,DISR
478 FORMAT(///1X,'SLOPE TAPERED INLET DESIGN - VERTICAL FACE'/'*****
1*****'//5X,'DISTANCE EMBANKMENT-TO
2E TO FACE =' ,F7.2,' FT',10X,'CULVERT OUTLET TO EMBANKMENT-TOE =' ,
3F7.2,' FT'//
4'MAX Q DESIGN'//10X,'TRANSITION SECTION= D/2'/10X,'INLET DESIGNE
5D AS BOX TYPE INLET'//)
IF(NOC(1).EQ.1.AND.NOC(2).EQ.1) GO TO 484
IF(NOC(1).EQ.1.AND.NOC(2).EQ.0) GO TO 486
IF(NOC(1).EQ.0.AND.NOC(2).EQ.1) GO TO 488
340 WRITE(SYSOT,342)DA(1),DA(2),FALL(1),FALL(2),TROEL,ELTRCB,FACEL,
1FACEL,S(1),S(2),VEL(1),VEL(2),BF(1),BF(2),L1(1),L1(2),L2(1),L2(2),
2L3(1),L3(2),SFACE,SFACE,TAPER(1),TAPER(2)
342 FORMAT(//5X,'CULVERT LENGTH =' ,F8.2,' FT',24X,'CULVERT LENGTH
1 =' ,F8.2,' FT',5X,'FALL',14X,'=' ,F8.2,' FT',24X,'FALL',14X,'=' ,F8
2.2,' FT',5X,'ELEV THROAT INVERT=' ,F8.2,' FT',24X,'ELEV THROAT INV
3ERT=' ,F8.2,' FT',5X,'ELEV FACE INVERT =' ,F8.2,' FT',24X,'ELEV FAC
4E INVERT =' ,F8.2,' FT',5X,'CULVERT SLOPE =' ,F8.4,27X,'CULVERT
5 SLOPE =' ,F8.2/5X,'VELOCITY',10X,'=' ,F8.2,' FPS',
6 23X,'VELOCITY',10X,'=' ,F8.2,' FPS'
7 / 5X,'FACE WIDTH',8X,'=' ,F8.3,' FT',24X,'FACE WIDTH',8X,
8'=' ,F8.3,' FT' /5X,'L1',16X,'=' ,

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C 6825
C 6830
C 6835
C 6840
C 6845
C 6850
C 6855
C 6860
C 6865
C 6870
C 6875
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C 6955
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C 6975
C 6980
C 6985
C 6990
C 6995
C 7000
C 7005
C 7010
C 7015
C 7020
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C 7055
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C 7065
C 7070
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C 7080
C 7085
C 7090
C 7095

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9FB.3.' FT',24X,'L1',16X,'=',FB.3,' FT' C 7100
A/5X,'L2',16X,'=',FB.2,' FT',24X,'L2',16X,'=',FB.2,' FT' C 7105
B /5X,'L3',16X,'=',FB.2,' FT', 24X,'L3',16X,'=', C 7110
CFB.2.' FT'/5X,'SF',16X,'=',FB.2,27X,'SF',16X,'=',FB.2/ C 7115
D 5X,'TAPER',13X,'=',FB.3,' :1',25X,'TAPER',13X,'=',FB.3,' :1'//8X. C 7120
E'Q',8X,'HWT',8X,'HWF',34X,'Q',8X,'HWT',8X,'HWF'// C 7125
QD=Q1-Q1*.2 C 7130
QD=QD/BAR C 7135
31 X=QD/D*.2.5 C 7140
X=ALOG10(X) C 7145
GO TO (4,6),I1 C 7150
4 HTCVD=-.233392+.489125*X+1.068638*X*X-3.074435*X*X*X C 7155
1+3.711165*X*X*X*X-1.32836*X*X*X*X*X C 7160
GO TO 8 C 7165
6 HTCVD=-.237139+.146792*X+2.189321*X*X-4.354114*X*X*X C 7170
1+4.210539*X*X*X*X-1.347032*X*X*X*X*X C 7175
8 Y16=10.*HTCVD C 7180
HWA=TRDEL+Y16*D C 7185
HWTB=ELTRCB+Y16*D C 7190
X=QD/(BF(1)*D*.1.5) C 7195
Y16=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X C 7200
1-.000496383*X*X*X*X C 7205
HWFA=FACEL+Y18*D C 7210
X=QD/(BF(2)*D*.1.5) C 7215
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X C 7220
1-.000496383*X*X*X*X C 7225
HWF8=FACEL+Y18*D C 7230
QU=QD*BAR C 7235
WRITE(SYSOT,32)QU,HWA,HWFA,QU,HWTB,HWF8 C 7240
32 FORMAT(1X,3.10.1,24X,3F10.1) C 7245
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 480 C 7250
QD=QD+(Q1/BAR)*.2 C 7255
GO TO 31 C 7260
484 WRITE(SYSOT,485) C 7265
405 FORMAT(///20X,'NO SLOPE TAPERED INLET - VERTICAL FACE - DESIGN APP C 7270
1LICABLE') C 7275
GO TO 480 C 7280
486 WRITE(SYSOT,487)DA(2),FALL(2),ELTRCB,FACEL,S(2),VEL(2),BF(2). C 7285
2L1(2),L2(2),L3(2),SFACE,TAPER(2) C 7290
487 FORMAT(//16X,'- -',40X,'CULVERT LENGTH =',FB.2,' FT' /16X,'- -' C 7295
1,40X, C 7300
2'FALL',15X,'=',FB.2,' FT'/16X,'- -',40X,'ELEV THROAT INVERT=',FB.2 C 7305
3,' FT'/16X,'- -',40X,'ELEV FACE INVERT =',FB.2,' FT'/16X,'- -',40 C 7310
4X,'CULVERT SLOPE =',FB.4/16X,'- -',40X,'VELOCITY',10X,'=' C 7315
5FB.2,' FPS',16X,'- -',40X,'FACE WIDTH',8X,'=',FB.3,' FT'/16X,'- -' C 7320
6,40X,'L1',16X,'=',FB.3,' FT'/16X,'- -',40X,'L2',16X,FB.2,' FT'/ C 7325
716X,'- -',40X,'L3',16X,'=',FB.2,' FT'/16X,'- -',40X,'SF',16X,'=' C 7330
8FB.2/16X,'- -',40X,'TAPER',13X,'=',FB.3,' :1'//8X,'Q',8X,'HWT',8X. C 7335
9'HWT',34X,'Q',8X,'HWT',8X,'HWF'// C 7340
QD=Q1-Q1*.2 C 7345
QD=QD/BAR C 7350
33 X=QD/D*.2.5 C 7355
X=ALOG10(X) C 7360
GO TO (1,2),I1 C 7365
1 HTCVD=-.233392+.489125*X+1.068638*X*X-3.074435*X*X*X C 7370

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1+3.711165*X*X*X*X-1.32836*X*X*X*X*X
GO TO 3
2 HTOVD=-.237139+.146792*X+2.189321*X*X-4.354114*X*X*X
1+4.210539*X*X*X*X-1.347032*X*X*X*X*X
3 Y16=10.**HTOVD
HWTB=ELTRCB+Y16*D
X=QD/(BF(2)*D**1.5)
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X
1-.000496383*X*X*X*X
HWF8=FACE1+.8*D
QU=QD*BAR
WRITE(SYSOT,34)QU,HWTB,HWF8
34 FORMAT(16X,'--',40X,3F10.1)
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 480
QD=QD+(Q1/BAR)*.2
GO TO 33
488 WRITE(SYSOT,489)DA(1),FALL(1),TRDEL,FACEL,S(1),VEL(1),BF(1),L1(1),
1L2(1),L3(1),SPACE,TAPER(1)
489 FORMAT(/,5X,'CULVERT LENGTH',F8.2,' FT',30X,'- -',5X,'FALL',1
14X,'=',F8.2,' FT',30X,'- -',5X,'ELEV THROT INVERT=',F8.2,' FT',30
3X,'- -',5X,'ELEV FACE INVERT',F8.2,' FT',30X,'- -',5X,'CULVERT
4SLOPE',F8.4,34X,'- -',5X,'VELOCITY',10X,'=',F8.2,' FPS',28X,
5'- -',5X,'FACE WIDTH',8X,'=',F8.3,' FT',30X,'- -',5X,'L1',16X,'=',
6F8.3,' FT',30X,'- -',5X,'L2',16X,'=',F8.2,' FT',30X,'- -',5X,'L3',
716X,'=',F8.2,' FT',30X,'- -',5X,'SF',16X,'=',F8.2,34X,'- -',5X,
85X,'TAPER',13X,'=',F8.3,' :1'//8X,'Q',8X,'HWT',8X,'HWF',34X,'Q',8X,
9'HWT',8X,'HWF'/)
QD=Q1-Q1*.2
QD=QD/BAR
35 X=QD/D**2.5
X=ALOG10(X)
GO TO (5,7),I1
5 HTOVD=-.233392+.489125*X+1.068638*X*X-3.074435*X*X*X
1+3.711165*X*X*X*X-1.32836*X*X*X*X*X
GO TO 9
7 HTOVD=-.237139+.146792*X+2.189321*X*X-4.354114*X*X*X
1+4.210539*X*X*X*X-1.347032*X*X*X*X*X
9 Y16=10.**HTOVD
H. A=TRDEL+Y16*D
X=QD/(BF(1)*D**1.5)
Y18=.1379509+.42974097*X-.07646745*X*X+.012651097*X*X*X
1-.000496383*X*X*X*X
QU=QD*BAR
HWF8=FACE1+Y18*D
WRITE(SYSOT,36)QU,HWTB,HWF8
36 FORMAT(1X,3F10.1,40X,'--')
IF(QD.GT.(Q1/BAR+4*((Q1/BAR)*.2)+5.)) GO TO 480
QD=QD+(Q1/BAR)*.2
GO TO 35
480 RETURN
END

```

C 7375  
C 7380  
C 7385  
C 7390  
C 7395  
C 7400  
C 7405  
C 7410  
C 7415  
C 7420  
C 7425  
C 7430  
C 7435  
C 7440  
C 7445  
C 7450  
C 7455  
C 7460  
C 7465  
C 7470  
C 7475  
C 7480  
C 7485  
C 7490  
C 7495  
C 7500  
C 7505  
C 7510  
C 7515  
C 7520  
C 7525  
C 7530  
C 7535  
C 7540  
C 7545  
C 7550  
C 7555  
C 7560  
C 7565  
C 7570  
C 7575  
C 7580  
C 7585  
C 7590  
C 7595  
C 7600  
C 7605  
C 7610  
C 7615  
C 7620  
C 7625

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SUBROUTINE COUT(QADJ,DIA,WHW,VEL1,DEP,DSUBN,DSUBC,DIST,SLOPE,CN)
COMMON ITAB(100),TAB1(100),TAB2(100),TAB3(100),TAB4(100),
1TAB5(100),TAB6(100),TAB7(100),TAB8(100),TAB9(100),TAB10(100),
2TAB11(100),TAB12(100),TAB13(100),TAB14(100),TAB15(100),TAB16(100),
3TQVAX(2,100),ELINCB(2,100),ELINCC(2,100),HWCB(2,100),HWCC(2,100),
4L,LL,K,SYSLN,SYSDT,ELIN,ELOUT,AHWEL,SEL,SER,ELINCA(2,100),
5 IPROJ(26),I1,I2,I3,I4,I5,ELL,ELR,Q1,AHW,DTW,CLTH,I55,
6NOCA(2,100),NOCB(2,100),NOCC(2,100),TBFALL(2,100),TCFALL(2,100),
7DISTA(2,100),SLOPA(2,100),CRESA(2,100),VELA(2,100),DISTB(2,100),
8SLJPB(2,100),CRESB(2,100),VELB(2,100),DISTC(2,100),SLOPC(2,100),
9CRESC(2,100),VELC(2,100),ELTRCB,ELTRCC,QUE,DISL,D'SR,SFACE,
ADIA1,DIA2,ELLE,ELRR,NOCBS,HWTEMP,KBAS1,KBAS2,KDEP1,KDEP2
DIMENSION V(2),SPH(2),HYDR(2),CKE(5)
DATA
DATA CKE/.9,.7,.5,.2,.2/
C
101 HEAD = (1. + CKE(I4) + ( 185.0*CN *CN *DIST/DIA**1.33333 ))
1* (QADJ*QADJ/39.725/DIA**4 )
ALPHA=1.12
IF(I1.EQ.2) ALPHA=1.04
C
C CRITICAL DEPTH CALCULATIONS
Z=QADJ/(32.2/ALPHA)**.5
X=ALOG10(Z/DIA**2.5)
IF(X.GT.ALOG10(.7)) GO TO 80
YOD=-.0051657+.407362*X-.1830236*X*X-.0915565*X*X*X
GO TO 85
80 YOD=-.0244603+.2017057*X-.64009815*X*X+.695619*X*X*X
85 YOD=10.**YOD
120 DSUBC=YOD*DIA
C
C NORMAL DEPTH CALCULATIONS
Z=CN *QADJ/(1.486*SLOPE**.5)
X=ALOG10(Z/DIA**2.6667)
IF(X.LE.ALOG10(.24)) GO TO 60
IF(X.LE.ALOG10(.315)) GO TO 62
YOD=1.0581646+2.32063*X+1.089492*X*X
GO TO 64
60 YOD=.3003639+.907884*X+.192615*X*X
GO TO 64
62 YOD=.685734+2.097532*X+1.125936*X*X
64 IF(X.GT.ALOG10(.335)) YOD=0.0
YOD=10.**YOD
130 DSUBN=YOD*DIA
WTW=DTW
TEVP=(DSUBC+DIA)*0.5
160 IF ( TEMP - WTW )161,161,170
161 TEMP = WTW
170 WHW = TEMP + HEAD
180 IF(WHW - (DIA+(1.+CKE(I4))*(QADJ*QADJ/39.725/DIA**4))) )200,450,450
200 IF(DSUBN-DSUBC)450,205,205
205 NSW4 = 0
IF ( WTW - DSUBC )225,225,210
210 IF (WTW - DSUBN )220,220,215
215 NSW4 = 1
220 DEP = WTW
C 7630
C 7635
C 7640
C 7645
C 7650
C 7655
C 7660
C 7665
C 7670
C 7675
C 7680
C 7685
C 7690
C 7695
C 7700
C 7705
C 7710
C 7715
C 7720
C 7725
C 7730
C 7735
C 7740
C 7745
C 7750
C 7755
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C 7805
C 7810
C 7815
C 7820
C 7825
C 7830
C 7835
C 7840
C 7845
C 7850
C 7855
C 7860
C 7865
C 7870 **
C 7875 **
C 7880
C 7885
C 7890
C 7895
C 7900

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	GO TO 320	C 7905
225	DEP = DSUBC	C 7910
	GO TO 320	C 7915
C		C 7920
320	SUMX = 0.0	C 7925
	I = 1	C 7930
	NSW10 = 0	C 7935
	IF ( DEP - DIA ) 700,325,330	C 7940
325	IF ( NSW4 ) 700,390,700	C 7945
330	DEP = WTW - SLOPE * DIST	C 7950
	IF ( DEP - DSUBN ) 335,335,376	C 7955
335	SUMX = ( WTW-DIA / ( 1.0+SLOPE*SLOPE ) ** 0.5 ) * ( 1.0+1.0/SLOPE/SLOPE ) ** 0.5	C 7960
	DEP = DIA	C 7965
700	CALL CROUT( DEP, AREA, T, WP, DIA, R )	C 7970
C		C 7975
C	COMPUTE THE VELOCITY, SPECIFIC HEAD + HYDRAULIC RADIUS	C 7980
C	FOR TWO CROSS-SECTIONS	C 7985
C		C 7990
340	V(I) = QADJ / AREA	C 7995
	SPH(I) = DEP + ALPHA * V(I)*V(I) / 64.4	C 8000
	HYDR(I) = AREA / WP	C 8005
	IF ( I - 2 ) 350,360,360	C 8010
350	I = I + 1	C 8015
351	IF ( NSW4 ) 380,355,356	C 8020
355	DEP = DEP + 0.2	C 8025
	IF ( DEP - DIA ) 700,390,390	C 8030
356	DEP = DEP - 0.2	C 8035
	GO TO 700	C 8040
C		C 8045
C	COMPUTE AVERAGE VELOCITY AND AVERAGE HYDRAULIC RADIUS	C 8050
C	FOR THE CROSS-SECTIONS	C 8055
C		C 8060
360	AVEV = ( V(1) + V(2) ) * 0.5	C 8065
	AVEHR = ( HYDR(1) + HYDR(2) ) * 0.5	C 8070
	S1 = CN * CN * AVEV * AVEV / 2.21 / AVEHR ** 1.33333	C 8075
	IF ( NSW4 ) 362,361,362	C 8080
361	IF ( S1 - SLOPE ) 375,375,366	C 8085
362	IF ( SLOPE - S1 ) 375,375,367	C 8090
C		C 8095
C	COMPUTE DISTANCE X1	C 8100
C		C 8105
366	DX1 = ( SPH(2) - SPH(1) ) / ( S1 - SLOPE )	C 8110
	GO TO 368	C 8115
367	DX1 = ( SPH(1) - SPH(2) ) / ( SLOPE - S1 )	C 8120
C		C 8125
C	COMPUTE ACCUMULATED DISTANCE FROM THE OUTLET	C 8130
C		C 8135
368	SUMX = SUMX + DX1	C 8140
	IF ( SUMX - CLTH ) 370,371,371	C 8145
370	V(1) = V(2)	C 8150
	SPH(1) = SPH(2)	C 8155
	HYDR(1) = HYDR(2)	C 8160
	GO TO 351	C 8165
371	IF ( NSW4 ) 373,372,373	C 8170
372	DEP = DEP - ( SUMX-CLTH ) / DX1 * 0.2	C 8175

	GO TO 376	
373	DEP = DEP + (SUMX-CLTH)/DX1*0.2	C 8180
	GO TO 375	C 8185
375	DEP = DSUBN	C 8190
376	NSW4 = -1	C 8195
	I = 1	C 8200
	CALL CROUT(DEP,AREA,T,WP,DIA,R)	C 8205
380	WHW = SPH(1) + CKE(I4) * V(1) * V(1) / 64.4	C 8210
390	GO TO 450	C 8215
C		C 8220
C	VELOCITY CALCULATIONS FOR INLET AND OUTLET CONTROL	C 8225
C		C 8230
C		C 8235
C	OUTLET CONTROL CALCULATIONS	C 8240
C		C 8245
450	IF ( WTW - DIA )451,470,470	C 8250
451	IF(DSUBC - DIA)452,470,470	C 8255
452	IF(DSUBC - WTW)453,454,454	C 8260
453	DEP = WTW	C 8265
	GO TO 460	C 8270
454	DEP=DSUBC	C 8275
460	R = 0.5*DIA	C 8280
	CALL CROUT(DEP,AREA,T,WP,DIA,R)	C 8285
	GO TO 480	C 8290
C		C 8295
C	AREA CALCULATION FOR PIPE FLOWING FULL	C 8300
C		C 8305
470	AREA = 0.785398 * DIA * DIA	C 8310
480	VEL1 = QADJ / AREA	C 8315
	RETURN	C 8320
	END	C 8325
		C 8330

SUBROUTINE CFIT(Q,CN,D,QMAX,TOEL,SLOPE,I4,I1,CLTH,DTW,AHWEL)	
DIMENSION CKE(5)	C 8335
DATA CKE/.9,.7,.5,.2,.2/	C 8340
DIST=CLTH	C 8345
ALPHA=1.12	C 8350
IF(I1.EQ.2) ALPHA=1.04	C 8355
QF=Q	C 8360
AREA=.785398*D*D	C 8365
WP=3.14159*D	C 8370
A=50.	C 8375
10 QF=QF+A	C 8380
HR=AREA*WP	C 8385
HD=(QF/10.)*(QF/10.)*((1.555*(1.+CKE(I4)))/(AREA*AREA)+(45.095*CN*	C 8390
1CN*DIST/(AREA*AREA*HR**1.33333)))	C 8395
Z= QF/(32.2/ALPHA)**.5	C 8400
X=ALOG10(Z/D**2.5)	C 8405
IF(X.GT.ALOG10(.7)) GO TO 80	C 8410
YCD=-.0051657+.407362*X-.1830236*X*X-.0915565*X*X*X	C 8415
GO TO 85	C 8420
80 YCD=-.0244603+.2017057*X-.64009815*X*X+.695619*X*X*X	C 8425
85 YOD=10.**YCD	C 8430
DC=YOD*D	C 8435
IF(DC.LE.D) GO TO 30	C 8440
20 DC=D	C 8445
30 T = (DC+D)/2.	C 8450
IF(DTW.GT.T) GO TO 50	C 8455
40 HO= T	C 8460
GO TO 55	C 8465
50 HO=DTW	C 8470
55 WHW=HO+HD	C 8475
HWO=WHW+TOEL	C 8480
IF(HWO.GT.AHWEL)GO TO 60	C 8485
GO TO 10	C 8490
60 QF=QF-A	C 8495
IF(A.LT.5.) GO TO 70	C 8500
A=2.	C 8505
GO TO 10	C 8510
70 QMAX=QF	C 8515
RETURN	C 8520
END	C 8525
	C 8530

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SUBROUTINE CEQUA(X,HW,DIA,SLOPE,I5)
DIMENSION      A(10),B(10),C(10),D(10),E(10),F(10)
DATA A/.108786,.114099,.167287,.087483,.120659,.063343,.081730,
1      .187321,.107137,.167433/
DATA B/.662381,.653562,.558766,.706578,.630768,.766512,.698353,
1      .567710,.757789,.538595/
DATA C/-.233801,-.233615,-.159813,-.253295,-.218423,-.316097,
1-.253683,      -.156544,-.361462,-.149374/
DATA D/.0579565,.0597723,.0420069,.0667001,.0591815,.0876701,
1.0651250,      .0447052,.1233932,.0391543/
DATA E/-.0055789,-.00616338,-.00369252,-.0066165,-.0059917,
1-.00983695,-.0071975,      -.00343602,-.0160642,-.00343974/
DATA F/.000205052,.000242832,.000125169,.000250619,.000229287,
1.00041676,.00031245,      .00008966,.00076739,.000115882/
C
C-----CONVENTIONAL PIPES
SCJRR=.5
IF(I5.EQ.9) SCCRR=0.0
HWQVD = A(I5) + ( B(I5) + ( C(I5) + ( D(I5) + ( E(I5) + F(I5)*X )
1 * X ) * X ) * X ) * X - SCJRR      * SLOPE
HW = HWQVD * DIA
RETURN
END
C 8535
C 8540
C 8545
C 8550
C 8555
C 8560
C 8565
C 8570
C 8575
C 8580
C 8585
C 8590
C 8595
C 8600
C 8605
C 8610
C 8615
C 8620
C 8625
C 8630
C 8635
C 8640
C 8645

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C      SUBROUTINE GROUT(DEP,AREA,T,WP,DIA,R)
C      CALCULATIONS FOR PIPE CHARACTERISTICS FOR ANY DEPTH OF FLOW
C      ANSWERS ARE 1. AREA OF PIPE 2. WETTED PERIMETER 3. TOP WIDTH
C      R=0.5*DIA
700   DAB = DEP - R
      Y = DAS / R
      Y1 = ABS( Y )
C
C      ARCSIN APPROXIMATION
C
      PHIY = 1.570796 + (-0.214512 + ( 0.0878763 + (-0.0449589 + (
10.0193499 - 0.00433777 * Y1) * Y1) * Y1) * Y1) * Y1
      ANGLE = 1.570796 - ( 1.0 - Y1) ** 0.5 * PHIY
      IF( Y )705,710,710
705   ANGLE = - ANGLE
710   DAC = ANGLE + 1.570796
      AREA = ( DAB * ( DIA*DEP - DEP*DEP )**0.5 ) + (R*R*DAB)
712   T = 2.0 * ( R*R - DAB*DAB ) ** 0.5
713   WP = DIA * DAC
      RETURN
      END
C 8650
C 8655
C 8660
C 8665
C 8670
C 8675
C 8680
C 8685
C 8690
C 8695
C 8700
C 8705
C 8710
C 8715
C 8720
C 8725
C 8730
C 8735
C 8740
C 8745
C 8750
C 8755

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