DOE/PC/92206--T15

NINTH QUARTERLY TECHNICAL PROGRESS REPORT (JULY, 1996 THROUGH SEPTEMBER, 1996)

BENCH-SCALE TESTING OF THE MICRONIZED MAGNETITE PROCESS

DOE Contract No. DE-AC22-93PC92206 Custom Coals International Project No. 94002

OCTOBER 28, 1996

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NINTH QUARTERLY TECHNICAL PROGRESS REPORT (July, 1996 Through September, 1996)

BENCH-SCALE TESTING OF THE MICRONIZED MAGNETITE PROCESS

DOE Contract No. DE-AC22-93PC92206 Custom Coals, Int. Project No. 94002

This document contains the Quarterly Technical Progress Report for the Micronized Magnetite Testing Project being performed at PETC's Process Research Facility (PRF). This ninth quarterly report covers the period from July, 1996 through September, 1996. No testing was conducted on the Micro-mag Project this quarter since data analysis and the final report are the only items remaining to complete the project.

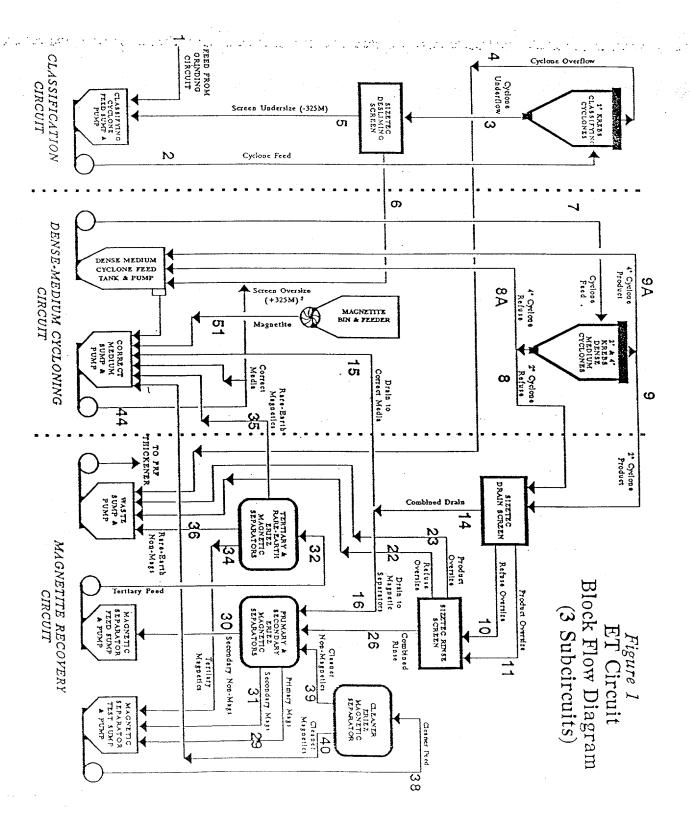
This report contains a short discussion of the project description, objectives, budget, schedule, and teaming arrangement. The final section contains an outline of the specific project goals for the next quarterly reporting period.

SECTION 1 - PROJECT DESCRIPTION

The major focus of the project, which is scheduled to occur through January 1997, is to install and test a 500#/hr. fine-coal cleaning circuit at DOE's Process Research Facility (PRF), located at the Pittsburgh Energy Technology Center (PETC). The circuit will utilize an extremely fine, micron-sized magnetite media and small diameter cyclones to make efficient density separations on minus-28-Mesh coal.

Figure 1 contains a block-flow diagram of the test circuit, which was installed at the PRF. The circuit consists of three subcircuits:

• Classification Circuit - Which consists of a feed sump and pump, a 2" Krebs Classifying Cyclone, and a 2' x 3' Sizetech Inclined Desliming Screen. The Classifying Cyclone is equipped with various orifices to make cuts (i.e., D-50) at 200M to perhaps as fine as 500M. The Desliming Screen has layered screen panels ranging from 100M to 325M. The Classification Circuit is fed 28M x 0 coal slurry from the existing PRF grinding circuit, and will remove the majority of the slimes prior to the heavy-media cycloning circuit.



- Dense-Medium Cycloning Circuit Which consists of a dense-medium cyclone feed, wing tank and feed pump, that overflows into a recirculating correct media sump and pump. Magnetite is added as required via a rotary air-lock feeder from a 0.5 ton magnetite bin. This subcircuit also consists of parallel-mounted Krebs 2" and 4" diameter Dense-Medium Cyclones. The 4" Cyclone products always recirculates back to the feed sump, and the 2" Cyclone products represents the feed to the Magnetite Recovery Circuit.
- Magnetite Recovery Circuit Which consists of a 2' x 3' Sizetec Inclined Desliming Screen (Drain Screen), and a 4' x 9' Sizetec Horizontal Dewatering screen (Rinse Screen). These screens have screen panels Figure 1 MicroMag Circuit Block Flow Diagram ranging from 100M to 325M. The magnetite recovery circuit contains four 36" x 24" Eriez Conventional, Wet-Drum magnetic Separators (CLIMAXX Models), as the Primary, Secondary, Tertiary, and Cleaner Magnetite separators. There is also an Eriez High Gauss, Rare-Earth Magnetic Separator (Concurrent Flow), which is used as a Scavenger Magnetic Separator in the circuit. The final magnetic concentrates return to the Correct Medium Sump, and the final nonmagnetics tailing reports to the Waste Sump and Pump, along with the Classifying Cyclone Overflow and Rinse Screen Oversize (see Figure 1). The Waste Sump discharge is dewatered using the Sharples Centrifuge and Thickener in the existing PRF process water clarification circuit.

The circuit is contained in a new permanent structure, that Custom Coals has installed in the PRF Emerging Technology (ET) Area. In addition to the equipment shown in Figure 1, the ET circuit contains a Clarified Water Head Tank and Pump to provide all water additions to the circuit. A closed-loop system is utilized in the circuit. A Motor Control Center (MCC) in the PRF motor control room, and Control Cabinet (CC) in the field provides the power distribution to the circuit.

The testing scope involved initial closed-loop testing of each subcircuit to optimize the performance of the equipment in each subcircuit (i.e., Component Testing), followed by open-circuit testing of the entire integrated circuit to optimize the process and quantify the process efficiency (i.e., Integrated Testing). All equipment can be run in closed-loop, with the exception of the 2" Krebs Dense-Medium Cyclone and the Drain and Rinse Screens (see Figure 1).

SECTION 2 - PROJECT OBJECTIVES

The overall objectives of the project are to:

• Determine the effects of operating time on the characteristics of the recirculating medium in a continuous integrated processing circuit, and, subsequently, the sensitivity of cyclone separation performance to the quality of the recirculating medium.

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• Determine the technical and economic feasibility of various unit operations and systems in optimizing the separation and recovery of the micronized magnetite from the coal products.

The specific technical objectives of the project are to:

- Establish the classifying circuit's operating conditions to make a separation at, or about 40 microns.
- Determine the effects of the magnetite particle size and medium purity on cyclone separation performance.
- Determine the effects of medium-to-coal ratio, medium density, feed pressure, and cyclone configuration on the separation efficiency of the cyclone. This testing is to verify whether cyclone separation performance equivalent to those produced in earlier research can be achieved and to determine the potential ranges of medium-to-coal ratios and medium densities expected for each cyclone product to help establish recovery circuit feed conditions.
- Quantify the amount and size of the magnetite not recovered by the individual and combined recovery circuit unit operations.
- Assess the technical and economic feasibility of various magnetite recovery circuits. Technically, the focus is on establishing the least complicated, easiest to operate circuit, that will provide the correct recirculating medium properties. Economically, determinations will be made looking at the trade offs between circuit capital and maintenance costs and overall system performance, including expected makeup magnetite requirements and cyclone separation efficiency.
- Determine the characteristics of the recirculating medium (purity and size distribution), and cyclone separation performance over time, during continuous, integrated testing of the entire circuit.

The Test, Sampling, and Analytical Plan was designed with these specific objectives in mind.

SECTION 3 - PROJECT SCHEDULE AND BUDGET

Figure 2 contains the original project schedule, by task series. The schedule in Figure 2 starts when Custom Coals began to actively work on the project (September 1994), and carried for a period of 17 months, until the initial scheduled completion in January 1996. The Major Milestone Tasks on the critical path contain asterisks. The project work scope and labor plan were discussed in detail in the Draft Work Plan, submitted in November, 1994.

Table 1 contains the 1996 Cost Plan estimate for the project. The upper part of the plan shows Custom Coals labor estimate, including markups. The plan incorporates Custom Coals' Project Manager, Ed Torak, working full-time on the project through January 1997. It also includes some time for other Custom Coal's personnel.

The lower part of the Cost Plan, in Table 1, shows the anticipated pass-through costs for subcontractors, as well as travel and equipment and supplies. A detailed description of the project subcontractors responsibilities and the items which have been purchased for the project are discussed in Sections 4 and 5 of this report.

SECTION 4 - PROJECT TEAM ORGANIZATION

Figure 3 contains the project team organization chart, for the project. The project team includes:

- DOE/PETC's project and site management personnel.
- Custom Coals' project and site management personnel.
- Parson's engineers and technicians to operate the existing PRF, during the circuit testing.
- H-Tech Corporation as a subcontractor to Custom Coals to procure all equipment required for the project.
- Dillner Storage as a subcontractor to Custom Coals to provide coal blending and storage services for the project.
- CLI Corporation as a subcontractor to Custom Coals to finalize the circuit design.
- Rizzo & Sons to install the circuit.

Figure 2

MICROMAG PROJECT SCHEDULE BY TASK (DOE Contract No. DE-AC22-93PC92206)

Revision Date: January 04, 1995

1100 *	1000	900 *	800	700 *	б О *	500 *	400	300	2000 *	100	TASK
Final Reporting	Data Evaluation	CircuitiDecommissioning	Analytical	Circuit:Testing	Circuit Commissioning	Circuitinstallation	Magnetite and Coal Procurement	Equipment Procurement & Fabrication	Final Circuit Design	Project Planning and Management	TASK DESCRIPTION
2 Months	11 Months	1 Month	10 Months	5 Months	1 Month	3 Months	7 Months	12 Months	2 Months	16 Months	DURATION MONTHS
15-16	51 - 55	14	5 1 4	9-13	ω	5-7	7-13	Ω 1 3	1 20	1 00	MONTHS
											1994 1995 1995 S O N D J F M A M J J A S O N D

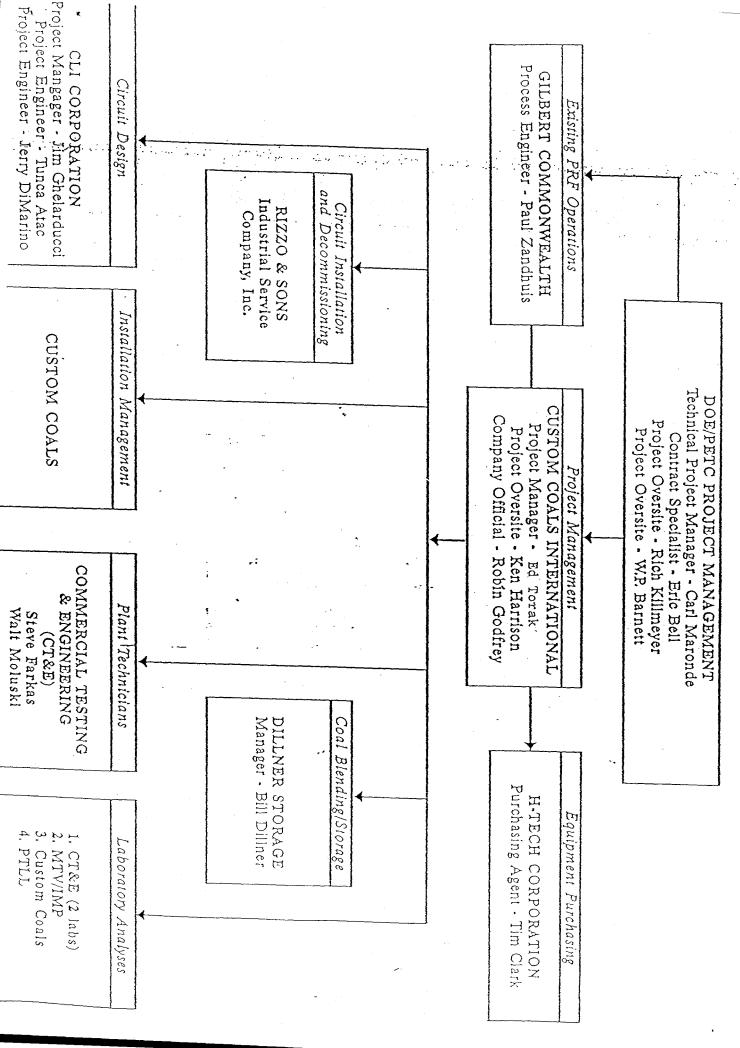
Notes: - * - Major Milestone Tasks on the Critical Path, We scheduled at least a 6-month period for Tasks 600 and 700

Table 1 U.S. DEPARTMENT OF ENERGY COST PLAN

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J.		151.4	8.1		0.0	0.0)	0.0	0.0	0.0		0.0	0.1	0.0	2.8	0.0	0.0	0.0		5.2		2.0	0.8	0.7	1.7		ם ם		_		ω	te Process	
\ /	PARTICIPANTS PROJECT MANAGER AND DATE	159.0 1	7.6		1,1	0.0	0.0	0.2	0.0		0.0	1.1	0.0	0.0	0.0	0.0	0.0		5.2		2.0	0.8	0.7	1.7	+	a a a		Pit	ž	3. PARTICIPANT ADDRESS		
	PROJEC	164.3 1	5.3		1.3	0.0	0.0	0.0	0,0		0.0	0.7	2.5	0.0	0.0	0.0	0.0		0.8		0.3	0.1	0.1	0.3	+	adv		Pittsburgh, PA 15222	First Ave	IPANT AL		
•	T MANAC	164.3 1	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0		0.0	0.0	0.0	0.0	\dashv	YAW	Q	A 15222	100 First Avenue, Suite 500	DRESS		
0//	BER AND	164.9	0.6		0.0	0,0	0.0	0.0	0.0		0,0	0.6	<u>0.</u> 0	0.0	0.0	0.0	0.0		0.0		0.0	0.0	0.0	0.0	+	Z	CURRENT FISCAL YEA		500			
01/10/96			3.1		0.0	0.0	0,0	0.0	0.0		0.0	0.1	3.0	0.0	0.0	0.0	0.0		0.0		0.0	0.0	0.0	0.0	-	-	FISCAL			4		
<u> </u>		1,191.7	23.7		0.0	0.0	0.0	0.0	0,0		0.0	0.0	0,0	0.0	0.0	0.0	0.0		23.7		9.2	2.7	3.3	8.5	100	<u>م</u>	YEAR		Janus	4. COST	-	
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	OF PARTICIPANT'S FINANCIAL REP. AND DATE		1263.5	-	20.5	16.8	ψ.	12.3	259.3		7.5	9.06	133.5	79.9	139.5	0.0	99.8		480.3		199,9	60.7	66.9	152.8	And the state of t	coner.	13. ADD. 14. TOTAL YEARS		October 31,1996	6. COMPLETION DATE	2206	

47

Figure 3 - PROJECT TEAM ORGANIZATION CHART



Custom Coals also performed a number of the more routine sample preparation and analytical procedures at the PRF site (ie., wet screening, coal sample filtering, preparation, pulverizing, and ashing).

All required subcontracts for the project are in place, and merely need to be managed, modified, and updated as the project testing scope evolves.

SECTION 5 - PROJECT ACCOMPLISHMENTS BY TASK SERIES

Figure 4 contains the work breakdown structure by major task, and minor subtask, for the project. Task 100 "Project Planning and Management" encompasses all the routine reporting requirements, as well as the special plans and reports that must be submitted for the project.

Figure 5 contains the detailed schedule, broken down by the subtasks within the work breakdown structure. The schedule is divided into approximately two week periods (ie., twice monthly), to allow for tighter specifications of document submission and task completion dates. Custom Coals plans to include Figure 5 in each Monthly and Quarterly Technical Progress Report to compare actual accomplishments to this initial schedule. This will be one of the main methods of controlling and monitoring the schedule and success of the project.

Section 5.1 - Task 100: Project Planning and Management (Months 1-16)

Custom Coals anticipates that the project manager, Ed Torak, will work full-time on the project through submission of the draft final report (mid December 1996). He will be responsible for on-site project management, and will also be responsible for all project reporting.

Table 2 shows the major project reporting requirements, with required frequencies and delivery dates for all documents. The table is broken down into 3 categories, which include:

- Routine Financial Reporting Requirements,
- Routine Technical Reporting Requirements, and
- Special Technical Reporting Requirements, submitted only once during the project.

During October, Custom Coals' Project Manager submitted a paper on the Micro-Mag project for publication and presentation at the SME Conference in Phoenix, Arizona.

Figure 4 MICROMAG PROJECT WORK BREAKDOWN STRUCTURE (DOE Contract No. DE-AC22-93PC92206)

TASK	TASK DESCRIPTION
- 100 "."	PROJECT PLANNING AND MANAGEMENT
•••	101 Management Plan
	102 Work Plan (ESH & QA/QC)
	103 Design Report (Two SSA's)
	104. Procurement and Fabrication Plan
	105 Installation and Shakedown Plan
	106 Coal Proc., Handling, & Logistics Plan
	107 Operation and Maintenance Manual (SOP's)
	108 Slurry Commissioning Plan
	109 Test, Sampling, and Analytical Plan (QA/QC)
200	FINAL CIRCUIT DESIGN
200	201 Finalize Flowsheet and P&ID
	202 Finalize Design Drawings
300	EQUIPMENT PROCUREMENT & FABRICATION 301 Process Equipment Procurement
	302 Structural Steel Fab. & Procurement
•	303 Platework Steel Fab. & Procurement
	304. Electrical Equipment Procurement
	305 Ancillary Equipment Procurement
	306 Laboratory Equipment Procurement
	307 Operating Supplies Procurement
400	MAGNETITE AND COAL PROCUREMENT
	401 Magnetite Procurement
	402 Coal Procurement
500	CIRCUIT INSTALLATION
	501 Primary Installation
	502 Piping Installation :
	503 Electrical Installation
600	CIRCUIT COMMISSIONING
600	
	601 Functionality and Leak Testing
	602 Water Commissioning
	603 Slurry Commissioning
700	CIRCUIT TESTING
	701 Component Testing (Coal #1)
	702 Integrated Testing (Coal #1)
	703 Component Testing (Coal #2)
	704 Integrated Testing (Coal #2)
800	ANALYTICAL
500	801 Preliminary Magnetite/Coal Testing .
	802 Circuit Testing Analytical
900	CIRCUIT DECOMMISSIONING
1000	DATA EVALUATION
1100	FINAL REPORTING

Figure 5 MICROMAG PROJECT DETAILED SCHEDULE BY TASK & SUBTASK (DOE Contract No. DE-AC22-93PC92206)

TASK	TASK DESCRIPTION	1994 1995 1995 1995 SEP OCT NOV DEC JAN FEB MAR APRIMAY JUNI JULI AUG SEP OCT NOV DEC 12 12 12 12 12 12 12 12 12 12 12 12 12
100	PROJECT PLANNING AND MANAGEMENT	
	101 Management Plan 102 Work Plan (ESH & QA/QC) 103 Design Report (Two SSA's) 104 Procurement and Fabrication Plan 105 Installation and Shakedown Plan 106 Coal Proc., Handling, & Logistics Plan 107 Operation and Maintenance Manual (SOP 108 Sturry Commissioning Plan 109 Test, Sampling, and Analytical Plan (QA/Q	
200	FINAL CIRCUIT DESIGN	
	201 Finalize Flowsheet and P&fD202 Finalize Design Drawings	
300	EQUIPMENT PROCUREMENT & FABRICATION	
	301 Process Equipment Procurement 302 Structural Steel Fab. & Procurement 303 Platework Steel Fab. & Procurement 304 Electrical Equipment Procurement 305 Ancillary Equipment Procurement 306 Laboratory Equipment Procurement 307 Operating Supplies Procurement	
400	MAGNETITE AND COAL PROCUREMENT	
	401 Magnetite Procurement 402 Coal Procurement	
500	CIRCUIT INSTALLATION	
J	501 Primary Installation502 Piping Installation503 Electrical Installation	
600	CIRCUIT COMMISSIONING	
	601 Functionality and Leak Testing602 Water Commissioning603 Slurry Commissioning	
700	CIRCUIT TESTING	
	701 Component Testing (Coal #1) 702 Integrated Testing (Coal #1) 703 Component Testing (Coal #2) 704 Integrated Testing (Coal #2)	
800	ANALYTICAL	
	801 Preliminary Magnetite/Coal Testing 802 Circuit Testing Analytical	
100	DATA EVALUATION	
110	FINAL REPORTING	

Table 2 PROJECT REPORTING REQUIREMENTS

Routine Financial Reporting Requirements:		M. J
Description	Frequency	Variance
Project Invoice	Monthly	+ 10 Days
Cost Management Report (Form)	Monthly	+10 Days
Summary Report (Form)	Monthly	+10 Days
Financial Summary Report	Monthly	+10 Days
II. Routine Technical Reporting Requirements:		
Description	Frequency	Variance
Schedule/Status Sheet (On-Site Activities)	Weekly	Every Friday
Milestone Schedule/Status Report (Form)	Monthly	+10 Days
Technical Status Report	Monthly	+10 Days
Key Personnel Staffing Report	Quarterly	+30 Days
5. Technical Progress Report	Quarterly	+30 Days
o. Toolinoon Togrood Roport		
6. Property Reports	Yearly & Semi-Annual	+30 Days
Property Reports Reporting Requirements:	Yearly & Semi-Annual	·
Property Reports III. Special Technical Reporting Requirements: Description	Yearly & Semi-Annual Frequency	Variance
Property Reports III. Special Technical Reporting Requirements: Description Management Plan	Yearly & Semi-Annual Frequency October 31, 1994	Variance November 15, 1994
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans)	Yearly & Semi-Annual Frequency October 31, 1994 October 31, 1994	Variance November 15, 1994 November 15, 1995
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans)	Frequency October 31, 1994 October 31, 1994 January 01, 1995	Variance November 15, 1994 November 15, 1995 January 15, 1995
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans) 4. Draft ET Circuit Design Report (two SSA's)	Frequency October 31, 1994 October 31, 1994 January 01, 1995 November 15, 1994	Variance November 15, 1994 November 15, 1995 January 15, 1995 November 30, 1994
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans) 4. Draft ET Circuit Design Report (two SSA's) 5. Final ET Circuit Design Report (two SSA's)	Frequency October 31, 1994 October 31, 1994 January 01, 1995 November 15, 1994 February 15, 1995	Variance November 15, 1994 November 15, 1995 January 15, 1995 November 30, 1994 March 15, 1995
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans) 4. Draft ET Circuit Design Report (two SSA's) 5. Final ET Circuit Design Report (two SSA's) 6. Procurement and Fabrication Plan	Frequency October 31, 1994 October 31, 1994 January 01, 1995 November 15, 1994 February 15, 1995 November 15, 1994	Variance November 15, 1994 November 15, 1995 January 15, 1995 November 30, 1994 March 15, 1995 November 30, 1994
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans) 4. Draft ET Circuit Design Report (two SSA's) 5. Final ET Circuit Design Report (two SSA's) 6. Procurement and Fabrication Plan 7. Installation and Shakedown Plan	Frequency October 31, 1994 October 31, 1994 January 01, 1995 November 15, 1994 February 15, 1995 November 15, 1994 November 30, 1994	Variance November 15, 1994 November 15, 1995 January 15, 1995 November 30, 1994 March 15, 1995 November 30, 1994 December 15, 1994
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans) 4. Draft ET Circuit Design Report (two SSA's) 5. Final ET Circuit Design Report (two SSA's) 6. Procurement and Fabrication Plan 7. Installation and Shakedown Plan 8. Coal Procurement, Handling, and Logistics Plan	Frequency October 31, 1994 October 31, 1994 January 01, 1995 November 15, 1994 February 15, 1995 November 15, 1994 November 30, 1994 January 31, 1995	Variance November 15, 1994 November 15, 1995 January 15, 1995 November 30, 1994 March 15, 1995 November 30, 1994 December 15, 1994 February 15, 1995
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans) 4. Draft ET Circuit Design Report (two SSA's) 5. Final ET Circuit Design Report (two SSA's) 6. Procurement and Fabrication Plan 7. Installation and Shakedown Plan 8. Coal Procurement, Handling, and Logistics Plan 9. Operation and Maintenance Manual (SOP's)	Frequency October 31, 1994 October 31, 1994 January 01, 1995 November 15, 1994 February 15, 1995 November 15, 1994 November 30, 1994 January 31, 1995 February 28, 1995	Variance November 15, 1994 November 15, 1995 January 15, 1995 November 30, 1994 March 15, 1995 November 30, 1994 December 15, 1994 February 15, 1995 March 15, 1995
6. Property Reports III. Special Technical Reporting Requirements: Description 1. Management Plan 2. Draft Work Plan (ESH & QA/QC Plans) 3. Final Work Plan (ESH & QA/QC Plans) 4. Draft ET Circuit Design Report (two SSA's) 5. Final ET Circuit Design Report (two SSA's) 6. Procurement and Fabrication Plan 7. Installation and Shakedown Plan 8. Coal Procurement, Handling, and Logistics Plan 9. Operation and Maintenance Manual (SOP's) 10. Slurry Commissioning Plan	Frequency October 31, 1994 October 31, 1994 January 01, 1995 November 15, 1994 February 15, 1995 November 30, 1994 January 31, 1995 February 28, 1995 March 31, 1995	Variance November 15, 1994 November 15, 1995 January 15, 1995 November 30, 1994 March 15, 1995 November 30, 1994 December 15, 1994 February 15, 1995 March 15, 1995 April 15, 1995
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Section 5.2 - Task 200: Final Circuit Design (Months 1-2)

Custom Coal's subcontracted CLI Corporation to perform the final design of the ET Circuit. During the period from September through November, 1994, CLI completed the design package, and assisted Custom Coals' Project Manager in preparing the bid specification for the circuit installation. In essence, the Circuit Design Task was completed prior to the third quarterly reporting period. CLI's only efforts were to update the P&ID in late March to reflect the actual flowsheet of the as-built circuit.

Figure 6 contains the general flowsheet, including the major equipment and flow streams. Figures 7 and 8 contain the final detailed P&ID and Flowsheet Drawings, respectively. Those drawings specify all equipment and the flow balance, and include all ancillary items (ie., piping, valves, and instrumentation).

Section 5.3 - Task 300: Equipment Procurement and Fabrication (Months 2-13)

For organizational purposes, the equipment and procurement and fabrication task was broken down into a number of subtasks (see Figure 5), which include:

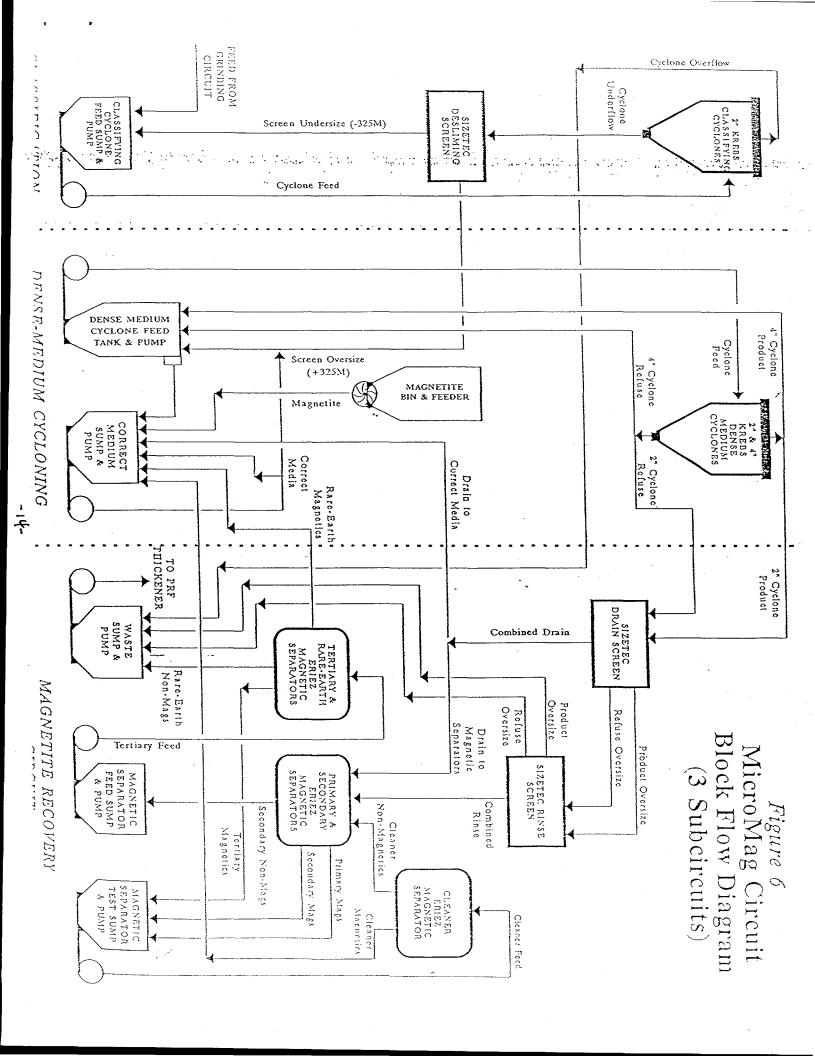
- 301 Process Equipment Procurement
- 302 Structural Steel Fabrication and Procurement
- 303 Platework Steel Fabrication and Procurement
- 304 Electrical Equipment Procurement
- 305 Ancillary Equipment Procurement
- 306 Laboratory Equipment Procurement
- 307 Operating Supplies Procurement

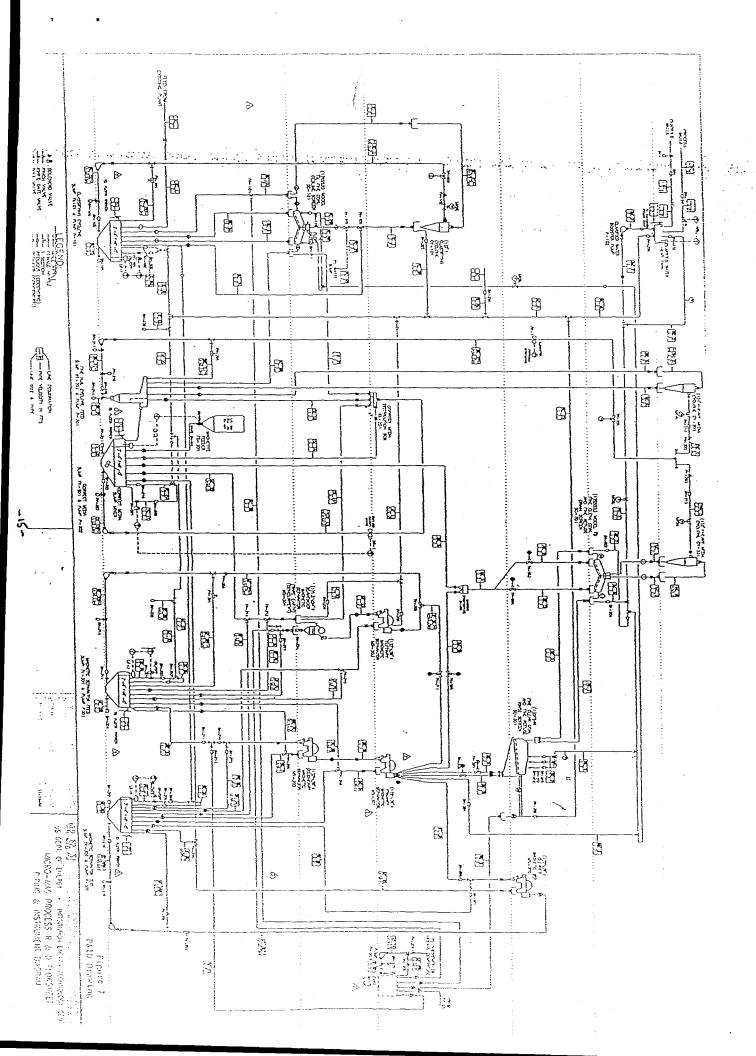
Table 3 contains the equipment list and cost estimate, for all items purchased to date. All of the major equipment was ordered during the second quarterly reporting period. It was delivered to site on the last week of January, 1995. All of the laboratory equipment and project supplies were ordered during the third reporting period.

The cost estimate, at the bottom of Table 3, of approximately \$258K, committed thus far, for purchases and shipping is still well below the revised equipment and supplies budget of \$300K, in the revised cost plan (see Table 1).

Section 5.4 - Task 400: Magnetite and Coal Procurement (Months 7-13)

The two major test materials for the project are the magnetite media and the test coals. Custom Coal's is testing 3 grades of magnetites and 2 types of bituminous coals, during the circuit testing. A detailed discussion of the coal and magnetite issues was presented in the Coal and Magnetite Procurement, Handling, and Logistics Plan, submitted in late January.





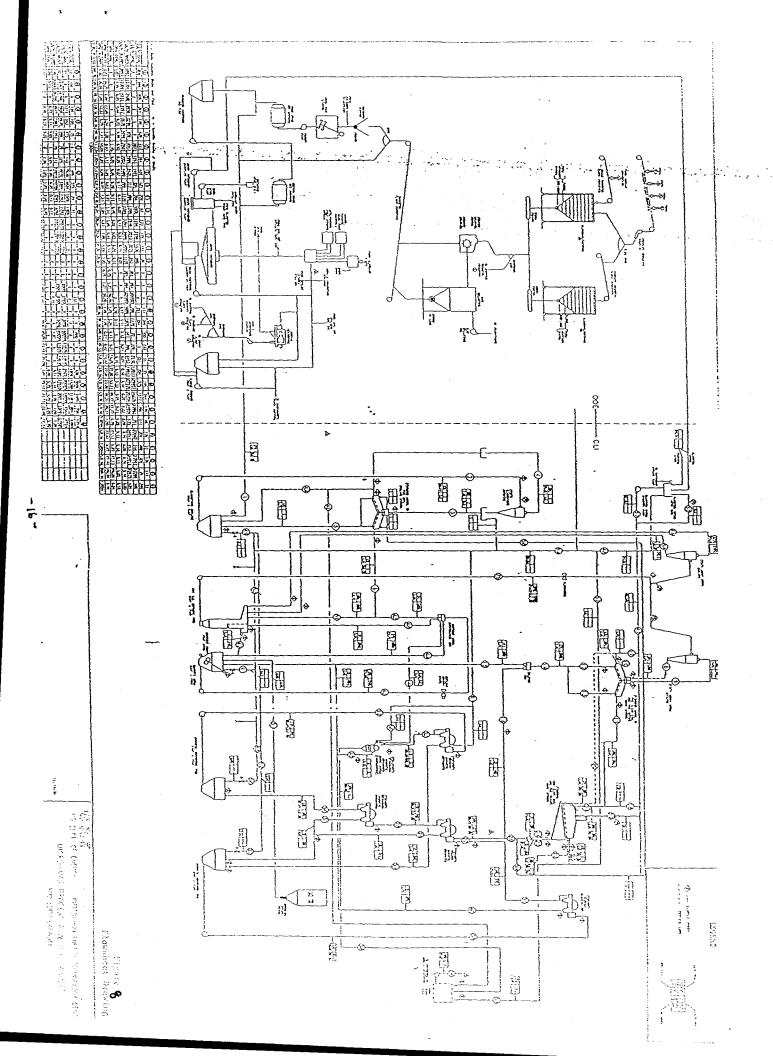


Table 3 CUSTOM COALS CORPORATION MICHOMAG PROJECT EQUIPMENT LIST (DOE CONTRACT NO, DE-AC22-93PC92206)

Revision Date: June 13, 1995

		ć ć	1047	1046	1045	1044	1043	1042	1040	1000	1036	1037	1036	1035	1034	1 033	1032	1031	1030	200	10278	1027A	1026	1025B	1025A	1020	1022	1021	1020	1018	1017	1016	1015	1013	1012	1011	1010	1000	1007	1006	1005	1002	1003	1001	ACHION	Unit	
	sw, 18311	Cestilite and miles scieen spray Nozzies	Wel Sample Splitter and Samplers	Lab. Matrix Separator (HGPM)	Air, Water, and siurry Gauges & Regulators	Steel Flanges and Gaskets	Digital Meter (NEMA 4 & UL Approved)	Solenold Operated Ball Valves (w/ Actuator)	Manual Ball 3-Way and Diantrage Valves	Variable Area proper ricuments:	marcy Equid Density Gauge (Manual)	Deslime and Ringe Screen Spray Nozzies		Handrall	Correct Media Sump Mixer	Spare Level Probas	Clarified Water Head Tank Level Transmitter	Mag. Sep. Test Sump Level Transmitter	Mag. Sec. Feed Sump Level Transmitter	Correct Media Silmo Level Transmitter					Customized Control Cabinet (NEMA 4)				Tertiary Magnetic Separator				2" Classifying Cyclone		100M Layered Screen Panels			Orain Screen	Waste Pump				Correct Media Pump		Ser Chit Description		Revision Date; June 13, 1895
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ī		spiay systelli so spiay Nozzies	Wet Splitter (110 V.) & 2 Samplers	Separator, Cup, and 3 Magnet Sets	Pressure Gauges (6) & Regulators (5)	Flanges (168) & Rubber Gaskets (99)	INFCP-210 Meter & SPC4 Cover	2" Unit (1) & 1" Units (4) W/ Spares	of Steel Valves (41) & OBVO Valves (88)	SIX FOR. CIRES (O RES. & TREC.)	2 Manging Scales With Spare Cups	1-1/2" Beaver Talls (26@\$14.50)	Fabricated Sumps, Chutes, & Frames	Fabricated Structure, Floor, & Rall	Mixer w/ 5' Long Agitator	Spare Probes (12@ 3',3'4",4',&4'4")	16ML1A4-X-03 W/2' & 1'8" Probes	16ML1A4-X-03 W/3' & 3'4" Probes	16M(1A4+X+03 w/2' & 2'4" Probes	18M11441X103W/07 % 0'4" Probes	IMP-20102 Digital Meter W/ Relays(2	LB-389 w/ Nal Detector & Comm.	MST-P Port. Ultrasonic Flowmeter	TMCB & 23 Man. Switches (17 New)	Square D Comp. In Hoffman Box	4 Verical Sections w/o TMOS	Rare Earth Wet Drum 24" x 18"	CLIMAXX Wet Drum 36" x 24"	OCIMAXX Wet Drum 36"x 24"	CLIMAXX Wet Drum 36" x 24"	D48 W/2 F1, 3 VF, & 3 AP	PC2-1424 W/2 FI, 3 VF, & 3 AP	PC2-1424 W/1 Fl. 3 VF. & 3 AP	2'x3'x1" Frame (5@\$286)	2'x3'x1" Frame (6@\$273)	2'x3'x1" Frame (10@\$320)	DSF 49 F 2x2'x9'	SSS 2315TD 2X2'X3'	1.5'X2'X8" W/ VS 1160 HPM	1.5'X2'X6" W/ DC 3500 RPM		1"x1.5"x8" w/ VS 1170 RPM (@ PETC	1'X1.5'X8" W/ VS 1150 BPM (@ PETO)	1"X1.5"X11" W/ VS 1350/1800 RPM	a Edolbusur Describitori		
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Table 4 contains a complete description of the three magnetites that Custom Coals is using for the project, which include:

- PennMag Grade-K Magnetite Ground natural magnetite, with a mean particle size of 9.8 microns.
- PennMag Grade-L Magnetite Finely ground natural magnetite with a mean particle size of 6.6 microns.
- Pea Ridge Grade-M Magnetite Extremely fine magnetite with a mean particle size of 3.0 microns.

Similarly, Custom Coals selected two test coals for the ET circuit testing. The coals are:

- Pittsburgh No.8 Seam bituminous raw coal from Ohio Valley Coal Company in Belmont County, Ohio.
- Lower Kittanning "B" Seam bituminous raw coal from PB&S Coal Company's, Longview Mine in Somerset County, Pennsylvania.

Tables 5 and 6 contain the size and washability analysis for the respective coals. Both coals are obtained from underground mines, and contain dry ash contents of between 20 and 30 Wt%. Over half of the sulfur in both coals is in the pyritic form, so they are good candidates for aggressive cleaning studies. They also both have anticipated yields of 70 to 80 Wt%, when cleaned at about 1.60 SG.

The major differences between the coals is that the Pittsburgh No. 8 Seam raw coal has a much higher organic sulfur content, and is much harder (HGI=60-70) than the Lower Kittanning "B" Seam raw coal (HGI=90-100). Testing of coals with different friabilities is desirable, to allow for comparison of how attrition affects fine coal contamination of the recirculating media, and subsequent media recovery and cyclone performance. The Pittsburgh No. 8 Seam Coal should be the less challenging coal. It was used for the circuit commissioning. The Lower Kittanning "B" Seam raw coal was the second coal tested. It is of major interest to Custom Coals because it will be one of the major feed coals used to make compliance coal at Custom Coals Laurel Cleaning Plant, which became operational in the winter of 1996.

TABLE 4
MICRONIZED MAGNETITE CHARACTERISTICS

Magnetite Head Analysis

Analysis	Grade-K	Grade-L	Grade-M
Moisture (Wt%)	0.1	0.20	
Ash (Wt%)	103*	102*	102
Specific Gravity	5.0	4.9	5.1
Moment (EMU/g)	86	75	81

^{*}Note: Magnetite gains weight during the ashing process.

Magnetite Davis-Tube Recovery Profiles

Davis-Tub	e Settings	Davis-T	ube Recoveries	(Wt%)
Amps	Gauss	Grade-K	Grade-L	Grade-M
0.30	750	84-86	20-22	0
0.50	1,250	96-98	70-72	0
1.70	3,700	98-99	95-97	80-81

Magnetite Size

Microtrac Results	Grade-K	Grade-L	Grade-M
D ₉₀ (90% Passing)	18.0	12.8	5.0
D ₅₀ (50% Passing)	8.9	5.7	2.7
D ₁₀ (10% Passing)	3.5	2.4	1.4
MVD (Mean Volume Dia.)	9.8	6.6	3.0
Moment (EMU/g)	87	77	82

Table 5 GROUND RAW COAL SIZE ANALYSIS AND WASHABILITY Pittsburgh No: 8 Seam Coal (PETC/PRF Dry Grind) Ohio Valley Coal Company (HGI = 60-70)

Top x 0 size analysis representing 100.00 Wt% of total raw coal sample

			Size	Analysis (E	D.B.)	Cumulative Analysis (D.B.)			
Size Fraction		Weight	Ash	Sulfur	Weight	Ash	Sulfur		
<u>Pass</u>		Retain	(Wt%)	_(Wt%)	_(Wt%)	<u>(Wt%)</u>	_(Wt%)	(Wt%)	
Top	X	30M	1.00	28.68	5.19	1.00	28.68	5.19	
30M	Χ	50M	3.30	28.68	5.19	4.30	28.68	5.19	
50M	Χ	70M	3.50	21.50	4.64	7.80	25.46	4.94	
70M	Χ	100M	5.40	18.74	4.74	13.20	22.71	4.86	
100M	Χ	200M	16.00	14.98	5.00	29.20	18.47	4.94	
200M	Χ	400M	22.60	14.08	5.25	51.80	16.56	5.07	
400M	Χ	<u> </u>	48.20	<u>32.43</u>	<u>3.83</u>	100.00	<u>24.21</u>	4.47	
		Total	100.00	24.21	4.47				
	Head		100.00	23.40	4.51				

Top x 0 wasabhility representing 100.00 Wt% of total raw coal sample

			Direc	t Analysis (D.B.)	Cumulative Analysis (D.B.)			
Gravity Fraction		Weight	Ash	Sulfur	Weight	Ash	Sulfur		
Sink		Float	(Wt%)	<u>(Wt%)</u>	(Wt%)	<u>(Wt%)</u>	<u>(Wt%)</u>	_(Wt%)	
Float	Χ	1.30	46.00	2.76	2.35	46.00	2.76	2.35	
1.30	X	1.40	20.20	8.13	2.60	66.20	4.40	2.43	
1.40	X	1.50	6.40	17.32	3.04	72.60	5.54	2.48	
1.50	X	1.60	2.50	33.31	4.67	75.10	6.46	2.55	
1.60	Х	1.80	2.00	34.30	4.94	77.10	7.18	2.62	
1.80	Х	2.20	3.10	52.69	3.23	80.20	8.94	2.64	
2,20	X	_Sink	<u> 19.80</u>	<u>83.19</u>	<u>10.36</u>	100.00	23.64	4.17	
		Total	100.00	23.64	4.17				
Head		100.00	23.83	4.42					

Table 6 CRUSHED RAW COAL SIZE ANALYSIS AND WASHABILITY Longview Mine, Kittanning "B" Seam PB&S Underground Mined Coal (HGI = 90-100)

1-1/2" x 0 size analysis representing 100.00 Wt% of total raw coal sample

			Size	Analysis (E),B.)	Cumulative Analysis (D.B.)			
Size Fraction		Weight	Ash	Sulfur	Weight	Ash	Sulfur		
Pass		Retain	(Wt%)	<u>(Wt%)</u>	<u>(Wt%)</u>	<u>(Wt%)</u>	(Wt%)	<u>(Wt%)</u>	
1-1/2".	Х	3/8"	21.78	36.77	2.88	21.78	36.77	2.88	
3/8"	Χ	1.0mm	50.44	18.72	2.03	72.22	24.16	2.29	
1.0mm	Χ	150M	21.64	12.74	1.93	93.86	21.53	2.20	
150M	Χ	500M	3.69	11.82	1.88	97.55	21.16	2.19	
500M	Χ	O_	<u>2.45</u>	<u> 18.43</u>	<u>1.21</u>	100.00	21.10	2.17	
		Total	100.00	21.10	2.17				

1-1/2" x 500M washability representing 97.55 Wt% of total raw coal sample

			Direct	t Analysis (D.B.)	_Cumulative Analysis (D.B.)			
Gravity Fraction		Weight	Ash	Sulfur	Weight	Ash	Sulfur		
Sink		Float	<u>(Wt%)</u>	<u>(Wt%)</u>	<u>(Wt%)</u>	(Wt%)	<u>(Wt%)</u>	(Wt%)	
Float	Χ	1.30	19.80	3.02	0.69	19.80	3.02	0.69	
1.30	X	1.40	42.10	7.95	0.83	61.90	6.37	0.79	
1.40	X	1.45	8.43	16.40	1.00	70.33	7.57	0.81	
1.45	X	1.55	5.66	25.22	1.40	75.99	8.89	0.85	
1.55	X	1.65	3.06	32.93	1.87	79.05	9.82	0.89	
1.65	X	1.80	2.87	40.85	2.19	81.92	10.91	0.94	
1.80	Χ	Sink	_18.08	68.43	<u>7.80</u>	100.00	<u>21.31</u>	<u>2.18</u>	
		Total	100.00	21.31	2.18				
Head		100.00	21.16	2.19					

In late February, Custom Coals' procured the 80-ton bulk shipment of Pittsburgh No. 8 Seam Coal, required for the commissioning and testing phases. The coal was delivered to Dillner Storage and blended in fourteen 6-ton lots. These lots were gradually transported to the PRF as feed for the testing. During the blending, Custom Coals' obtained a 100 pound composited sample of the coal and sent it to CT&E for analyses. During July, Custom Coal's Project Manager procured a 46-ton bulk sample of the second coal, Lower Kittanning "B" Seam, and had it delivered to Dillner Storage. It was later blended and split into 6-ton piles for gradual transport to DOE's PRF. A bulk sample was collected, and the individual piles (ie., lots) were covered with poly tarps to avoid any moisture pickup.

Section 5.5 - Task 500: Circuit Installation (Months 5-7)

The major focus of the project work, during the third quarterly reporting period (January through March 1995), was the circuit installation task. Custom Coals subcontracted Rizzo & Sons to perform the circuit installation, based on their experience working at the site and the competitiveness of their bid (\$121K). The installation of the circuit began on January 23rd, and was completed on March 27th, including \$11K of additional work that was not in the work scope. For organizational purposes, Custom Coals broke down the circuit installation into 3 subtasks that Rizzo's performed according to the following schedule:

- Primary Installation: (January 23rd February 10th) Structure, flooring, handrail, equipment, and platework.
- Piping Installation: (February 14th March 27th)
- Electrical Installation: (February 14th March 27th)

From January 23rd through February, Rizzo & Sons had approximately 5-7 men working on-site on the circuit installation task. In March, the work became more detailed and the crew was reduced to 2-4 men. Rizzo's men worked 10-hour shifts (7:00AM through 5:30PM) Monday through Thursday, with Fridays off. Custom Coals' Project Manager was on-site during the entire installation period to ensure that all installations occurred in accordance with the design drawings, the SSA's and DOE's work rules.

The new structure that was installed is permanent and consists of a number of column rows, installed in the PRF's ET circuit area, and fastened to the existing structure. The floor levels match the existing structure on all except the highest floor, and consist of 3/8" checkerplate flooring with removable handrail and toeplate. Design specifications are 150#/sq.ft. live load and 2000# point loading.

The structure and equipment on each floor of the circuit is as follows:

- 1086' Elevation The ground level concrete floor is part of the new structure. The 20'x 20' new equipment area contains the 6 slurry sumps and pumps shown on the bottom of Figure 6, as well as all sample prep equipment setup at the site. All the sumps and pumps, as well as the structural steel are bolted to the concrete floor.
- 1096' Elevation The second floor consists of a new 22'x 13' structure adjacent to the existing circuit. It is enclosed in removable handrail and toeplate. This level contains the primary, secondary, tertiary, and scavenger rare-earth magnetic separators, as well as the magnetite hopper and deslime screen. It also contains the Berthold Density Gauge and the Polysonics Ultrasonic Flowmeter.
- 1106' Elevation The third floor also consists of a new 22'x 13' structure adjacent to the existing circuit, enclosed in removable handrail and toeplate. This level contains the rinse screen, the media distribution and splitter boxes, and the classifying cyclone. It also contains the control cabinet used to operate and monitor the circuit.
- 1116' Elevation The fourth floor consists of a new 10'x 20' structure adjacent to the existing circuit, and enclosed in removable handrail and toeplate. This level contains the clarified water head tank and pump, the two heavy-media cyclones, the drain screen, and the cleaner magnetic separator.

The general arrangement drawings were used to place the structural steel, flooring, handrails, equipment, and platework in the initial part of the installation.

The detailed process piping requirements are shown in the circuit P&ID, (see Figure 9). Figure 9 contains all slurry and water piping lines, including all fittings and valves. Most of the slurry piping was specified as CPVC ("P") to save money and for ease of installation. Steel piping was used for the high-pressure, dense-medium cyclone feed lines.

A detailed piping list for the slurry lines, water lines, and compressed air lines was included in the design package. The piping routes were determined in the field during installation, by Custom Coals and Rizzo staff. All gravity lines were installed first to ensure maximum slope, while maintaining sampling capabilities. Pump discharge lines, water lines, and air lines were installed later, with priorities on maintaining access to the circuit and sampling capabilities.

The final installation subtask, the electrical installation, started in mid-February 1995 was also completed in late-March 1995. Rizzo & Sons were responsible for installing the following units:

- A new 200 Amp. Thermal Magnetic Circuit Breaker (TMCB) in DOE's existing Square D, Model 5 MCC in the PRF MCC room.
- A new, NEMA-12 Allen Bradley MCC in the PRF MCC room (3 Vertical Sections).
- A new customized Control Cabinet in the field to operate and monitor the circuit.
- 23 new disconnects in the field, one next to each new 480 Volt motor.

The electrical work included all conduit runs, wiring, and terminations between these units, and the 23, 480-Volt motors in the circuit. It also included the conduit runs, wiring, and termination between the Control Cabinet and the 11 fixed instruments in the field (1 Berthold nuclear density gauge, 5 Warrick level probe systems, and 5 air solenoids). The circuit also includes a Polysonics portable ultrasonic flowmeter, that does not require any permanent wiring. An illustration of these instrument locations is shown in Figure 9.

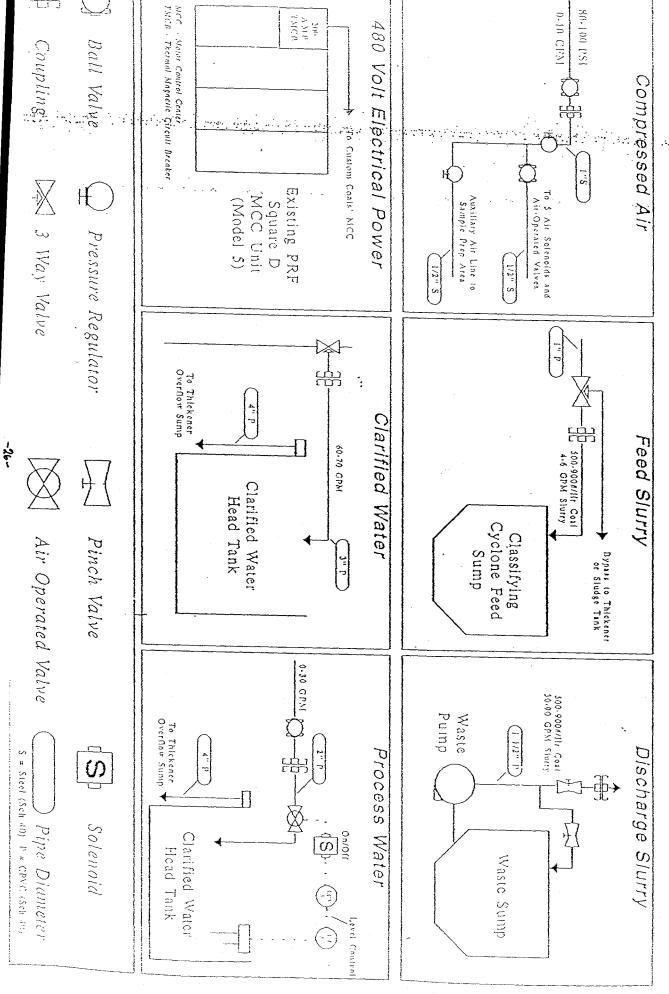
All aspects of the ET Circuit needed to be tied into the existing PRF system. Figure 10 contains the interface drawing for these various tie-ins. The Installation and Shakedown Plan, submitted in late December, included a more detailed discussion of the various installation tasks and work rules.

Section 5.6 - Task 600: Circuit Commissioning (Month 8)

The circuit commissioning task went very smoothly and was completed near the end of April, 1995. The operating staff, at the PRF site, during the commissioning period included:

- Custom Coals' Project Manager.
- One to two men from Rizzo's to assist with required modification and commissioning tasks.
- A part-time Project Engineer (Ed Torak), to assist with the on-site work.
- Two to three full-time Project Technicians (subcontracted from CT&E), to maintain, operate, and sample the circuit.

GC/Existing PRF (black) & Custom Coal's MicroMag Circuit (green) CIRCUIT INTERFACE & TIE-IN DRAWING Figure 10



The commissioning task was broken down into three subtasks:

- Functionality and Leak Testing to test motors and the sump level controls.
- Water Commissioning to balance the circuit flowrates and correct any leaks.
- Slurry Commissioning to balance the circuit with slurry and calibrate the nuclear density gauge and ultrasonic flowmeter.

The screens, cyclones, and magnetic separators were also tested for proper flow patterns and volume splits during the slurry commissioning period. The commissioning plan was discussed in detail in the Installation and Shakedown Plan, submitted late December 1994, and was discussed in even more detail in the Slurry Commissioning Plan, submitted in late March 1995.

Section 5.7 - Task 700: Circuit Testing (Months 9-13)

5.7.1 COMMISSIONING TEST RESULTS

The circuit slurry commissioning task was carried out over the entire month of April, and was broken down by the three subcircuits:

- Classifying Circuit Commissioning Tests
- Heavy-Media Cyclone Commissioning Tests
- Magnetite Recovery Circuit Commissioning Tests

Two men from Rizzo's installation staff stayed on site for the entire commissioning period to assist with required modifications and troubleshooting. The following discussion describes the commissioning results from these three areas of the circuit.

Classifying Circuit Commissioning Results

The goal of the classifying circuit commissioning was to test that subcircuits' ability to remove the majority of the -500M slimes (greater than 90Wt%), while recovering the majority of the +325M particles (greater than 90Wt%), with a high solids content product (greater than 35Wt%). A total of 7 tests were performed and completely analyzed during the testing, using two different circuits. The circuits were:

 Original Circuit - PRF feed to classifying cyclone, followed by north side of deslime screen, with deslime screen undersize recycled. This circuit was used for the first 5 tests. Modified Circuit - PRF feed to north side of deslime screen (desliming), followed by classifying cyclone and south side of deslime screen (dewatering), with south side screen undersize recycled to the classifying cyclone. This circuit was used for the last 2 tests.

Table 7 contains the operating conditions and results for the 7 tests.

As Table 7 illustrates, the initial circuit provided high recoveries, but it was impossible to simultaneously obtain efficient desliming and dewatering. Use of the modified circuit allowed the north side of the screen to focus on desliming and the south side of the screen to focus on dewatering. As a result, CT#6 and CT#7 were the only two tests to achieve the goal of greater than 35 Wt% solids in the final product (ie., 36.5 and 61.5 Wt%, respectively).

Custom Coals used the modified circuit to accomplish the following more aggressive objectives.

- Target over 60 Wt% solids recovery (yield) to obtain 500#/hr of solids product, from 800#/hr of solids feed.
- Target over 60% Wt% solids content in the final product.
- Target over 95 Wt% rejection of -500M particles.
- Target over 95 Wt% recovery of +325M particles.
- Target D-50 separation size of 30-40 microns.

Heavy-Media Cyclone Commissioning Results

The second slurry commissioning subtask involved two tests to access the flow and performance of the parallel 2" and 4" Krebs Heavy-Media Cyclones. Table 8 contains a summary of the test results and conditions.

Table 8 suggests that the 4" Cyclone was separating the +500M particles very efficiently for the feedrate and operating conditions in CMT#1 (ie., 84 Wt% yield, with a 7.5 Wt% Clean Coal Ash Content and 77 Wt% Refuse Ash Content, for a 18.9 Wt% Feed Ash Content), even with the relatively coarse, Lot#1 Grade-K Magnetite. Unfortunately, the 2" Cyclone yield was only 11.2 Wt% for the +500M particles in Test CMT#1. Even with the smallest acceptable apex size of .25 inches, used in CMT#2, the 2" Cyclone yield only increased to about 50 Wt%.

TABLE 7
CLASSIFYING CIRCUIT COMMISSIONING TESTS
(Pittsburgh No. 8 Seam Raw Coal)

တဲ့ သက်လေးသော မေလသေး မေးခဲ့သည် နောက်လျှင် ပေ ကလေးကြောင်းသည် မေးခဲ့ပေသည် ရှည် ပေရမြေးသည်။ မေလ လျှေးနှစ်သည်။

	Initial	Tests	New S	pray Bars	Modified Circuit		
GENERAL DATA	<u>CT#1</u>	<u>CT#2</u>	<u>CT#4</u>	CT#5	<u>CT#6</u>	CT#7	
Date Circuit Type	04/03/95 Original	04/04/95 Original	04/13/95 Original	04/24/95 Original	04/27/95 Modified	05/02/95 Modified	
Feed Rate (#/hr)	644	712	819	783	739	769	
CYCLONE CONDITIONS							
Feed Inlet (sq. in.) Vortex (Inches) Apex (Inches)	0.25 0.625 0.375	0.25 0.625 0.375	0.25 0.625 0.25	0.25 0.625 0.25	0.25 0.625 0.25	0.25 0.80 0.25	
Feed Pressure (PSI) Feed Rate (GPM)	33 17.8	42 20.7	46 18.5	46 18.0	48 17.2	45 22.1	
SCREEN CONDITIONS							
North Side Panel (Mesh) North Side Sprays (GPM)	325 5.0	325 5.8	200 9.8	200 14.5	325 15.0	325 18.5	
South Side Panel (Mesh) South Side Sprays (GPM)			 	 	200 2.4	100 0.0	
PRODUCT QUALITY							
Solids Content (Wt%) Solids Flowrate (#/hr)	26.5 489	16.1 561	31.5 606	18.6 424	36.5 480	61.5 396	
+325 Mesh (Wt%) 325 x 500 Mesh (Wt%) -500 Mesh (Wt%)	 	 	80.8 11.5 7.7	91.1 4.8 4.1	77.6 13.7 8.7	83.4 12.9 3.7	
CIRCUIT PERFORMANCE							
Overall Recovery (Wt%) +325 Mesh Recovery (Wt%) -500 Mesh Rejection (Wt%)	75.9 	78.8 98.5 61.2	74.0 99.1 81.7	54.1 88.0 93.9	65.0 99.7 85.0	51.5 85.9 94.8	
D-50 Size of Sepn. (Microns)			30	60	30	40	

Notes: - Original Circuit - Classifying Cyclone, followed by Deslime Screen (North Side), with Deslime Screen Underflow Recycled.

 Modified Circuit - North Side of Deslime Screen (Desliming), followed by Classifying Cyclone and South Side of Deslime Screen (Dewatering), with South Side Screen Undersize Recycled to Cyclone.

TABLE 8
HEAVY-MEDIA CYCLONE SPLITS
Pittsburgh No. 8 Seam Commissioning Tests
(Grade-K Magnetite, Lot #1)

	Conditions		itions	Feed		Overflow			Underflow	
Test #	H.M. <u>Cyclone</u>	Feed Rate (GPM)	Feed Pres. <u>(PSI)</u>	Slurry <u>SG</u>	+500M Ash (Wt%)	Slurry <u>SG</u>	+500M Yield <u>(Wt%)</u>	+500M Ash <u>(Wt%)</u>	Slurry <u>SG</u>	+500M Ash <u>(Wt%)</u>
CMT#1 CMT#1	4" 2"	28 10	81 22	1.34 1.34	18.9 18.9	1.25 1.13	84.0 11.2	7.5 4.6	1.85 1.56	77.1 20.7
CMT#2	2"	10	22	1.32	19.2	1.15	50.0	5.8	1.70	32.6

Notes: - The 4" Cyclone had 0.12 sq. in. inlet, 1.00 inch vortex, and 0.625 inch apex.

- The 2" Cyclone had 0.09 sq. in. inlet, 0.375 inch vortex, and 0.375 inch apex in CMT#1 and 0.25 inch apex in CMT#2.

Magnetite Recovery Circuit Commissioning Test Results

The third and final slurry commissioning subtask involved three tests to assess the magnetite recovery circuit performance (ie., magnetite losses) for the screens and magnetic separators within the MicroMag circuit, once again using the relatively coarse, Lot#1 Grade-K Magnetite. Table 9 contains the total magnetite losses for each test, broken down by the two main sources:

- Rare-Earth Scavenger Magnetic Separator Tailing (Sample 36) Which represents the total losses occurring within the 5 Eriez drum separators (see Figure 1).
- Combined Rinse Screen Products (Samples 22 & 23) Which represents the magnetite trapped in the coarse particles overflowing the refuse and clean coal product screens (also see Figure 1).

The first test listed in Table 9 (MT#2), was a test performed with only magnetite, and no coal slurry. As a result, the magnetics losses were extremely low in the magnetic separator tailings (0.3-0.8 #/ton), and negligible in the Combined Rinse Screen Products (i.e., because there were no products). The magnetics contents and losses are based on two calculations (Davis-Tube based and EMU based), with Davis-Tube based values being an initial approximation, based on Davis-Tube magnetic separations, and EMU based values being a correction due to the slight inefficiency of the Davis Tube. The EMU calculations are based on magnetic moment measurements of the feed, mags, and nonmags from the Davis-Tube tests. The actual losses are probably somewhere in between, but closer to the EMU-based losses.

The last two test results listed in Table 9 are for two tests done with coal and magnetite slurry; the first (CMT#1) done with the finest, 325M drain and rinse screen panels and a deep bed in the rinse screen (-3 degree angle), and the second (CMT#2) done with coarser, 200M drain and rinse panels and a shallow bed on the rinse screen (0 degree angle). The results show that acceptable magnetics losses through the magnetic separators (1.1-3.3 #/ton) were achieved for both tests. However, the magnetics losses in the rinse screen products were unacceptably high (35-88 #/ton), for both tests. The coarser 200M panels and flattening of the rinse screen improved the results but the losses of 35-40 #/ton are still an order of magnetite above acceptable targets (2-5 #/ton). However, these were just some initial scoping tests for each of the units and no attempt was made to optimize the circuits.

TABLE 9
MAGNETITE LOSSES
Pittsburgh No. 8 Seam Commissioning Tests
(Grade-K Magnetic, Lot #1)

				Davis-Tube Based Results		EMU Based Results	
<u>Test</u>	Stream	Stream Solids	m Info. Fl ow	Solids Magnetics (Wt%)	Magnetics Losses (#/Ton)	Solids Magnetics(Wt%)	Magnetics Losses (#/Ton)
MT#2	36 - Scav. Sep. Tails	(#/hr) 5	(GPM)	1.5	0.3	3.9	0.8
CMT#1	36 - Scav. Sep. Tails	100		0.6	2.2	0.9	3.3
CMT#1 CMT#1	22/23 - Rinse Products Total Circuit	400 500		5.0 4.1	80 82.2	5.5 4.6	88 91.3
CMT#1 CMT#2 CMT#2	36 - Scav. Sep. Tails 22/23 - Rinse Products Total Circuit	100 400 500		0.3 2.2 1.8	1.1 35 36.1	0.6 2.5 2.1	2.2 40 42.2

Notes: -

MT#2 had only magnetite being fed and 22 and 23 streams were negligible.

- 36 is Rare-Earth Scavenger Magnetic Separator Tailings (Final Magnetic Separator Nonmags).
- 22 is Rinse Screen Refuse Discharge (Final Refuse Nonmag).
- 23 is Rinse Screen Clean Coal Discharge (Final Clean Coal Nonmags).
- Data Assumes 500#/hr total coal feed, and that pure magnetics are 86 Emug.
- CMT#1 done with 325M panels with -3° angle on rinse screen, and CMT#2 done with 200M panels with 0° angle on rinse screen.

5.7.2 QA\QC RESULTS

The QA/QC required for the plant testing can be broken down into three main areas:

- Sample handing, preparation, and analyses accuracy checks Which requires adopting and adhering to certain set procedures and equipment.
- Instrument accuracy checks Which encompasses flowmeters, pressure gauges, and nuclear density gauges.
- Sample and test, repeatability and reproducibility Which can be affected by procedures and approach, but are more system dependent (ie., stabilization time, system consistency, and feed consistency).

The circuit is set up with a number of manual and redundant systems to routinely check the accuracy of the instruments. When coupled with the planned routine

maintenance of the instruments, Custom Coals did not experience any significant accuracy problems in those areas, at least none that would skew overall test conclusions and results.

The majority of Custom Coals QA/QC focused on the last two areas, particularly obtaining accurate sample analyses and material balances. To date, a number of issues have already been addressed. For example, Table 10 contains the ASTM Standards for within lab repeatability, and between labs reproducibility, of coal laboratory analyses. Since Custom Coals is doing all sample preparation at site, including moisture and ash analyses, a test was done to compare the analyses obtained on samples with PETC's Furnaces (the standard method) to CT&E's commercial laboratory results. Table 11 illustrates, via the duplicate analyses that Custom Coals is well within ASTM repeatability for moisture and ash analyses, using the PETC furnaces. Table 11 also illustrates that Custom Coals analyses match CT&E's for moisture and ash within ASTM reproducibility.

TABLE 10 ASTM STANDARDS FOR COAL ANALYTICAL VARIANCES

ASTM Allowable Differences on Duplicate Samples

<u>Analysis</u>	Coal Type	Repeatability Within Lab	Reproductibility Between Labs
Moisture	Any	0.30 Wt%	0.50 Wt%
Ash	Raw Coal Clean Coal Refuse Coal	0.50 Wt% 0.20 Wt% 1.00 Wt%	1.00 Wt% 0.30 Wt% 2.00 Wt%
Btu/lb.	Any	50	100
Sulfur	<2.0% Sulfur Coal >2.0% Sulfur Coal	0.05 Wt% 0.10 Wt%	0.10 Wt% 0.20 Wt%
Pyritic Sulfur	<2.0% Pyritic Sulfur Coal >2.0% Pyritic Sulfur Coal	0.05 Wt% 0.10 Wt%	0.30 Wt% 0.40 Wt%

TABLE 11
COMPARISON OF COAL ANALYSES
PETC AND CT&E FURNACES
(Test PCT #1, 05/16/95)

Sample	en e	Residual Mois	sture (Wt%)	Dry Ash Conte	ent (Wt%)
No.	Sample Name	PETC	CT&E	PETC	CT&E
1	PRF Feed	1.93/1.93	1.86	27.31/27.48	26.89
2	Class. Cyclone Feed	1.43/1.49	1.50	25.98/25.97	25.41
3	Class. Cyclone Underflow	1.86/1.92	1.92	26.88/26.66	26.02
4	Class. Cyclone Overflow	1.77/1.88	1.70	32.21/32.37	31.73
5	Deslime Screen Unders (South)	1.04/1.04	1.02	56.25/56.00	54.97
5A	Deslime Screen Unders (North)	1.72/1.68	1.59	38.97/39.24	38.44
6	Deslime Screen Disch. (South)	1.47/1.47	1.41	20.91/21.04	20.77
6A	Deslime Screen Disch. (North)	1.77/1.83	1.69	24.19/24.15	23.65

Note: Analyses on PETC Furnace Performed by CT&E Personnel.

Another area of QA/QC testing that has been performed at site is testing of the Carpco Wet-Splitting Unit for accuracy and reproducibility. The testing was done with three types of feed:

- Water-only testing
- Coal/water slurry testing
- Magnetite/water slurry testing

The results from the testing, shown in Table 12 illustrate that the unit makes two consistent 5.5 Wt% splits, that essentially match the composition of the waste stream removed from the bottom (Split #3). The only problem is that a significant portion of the feed is retained within the unit (0.3 to 1.8 Wt%), and the retained portion is higher solids content than the splits, meaning that the splits are slightly lower solids content than the actual feed sample. It appears that the solids retained in the Carpco Unit essentially match the passing portion in composition.

TABLE 12
WET-SPLITTING RESULTS FOR CARPCO UNIT

. Water-Only Testing: (10,000 gram Feed Sample)

	Removed Recovery	Total Recovery
<u>Portion</u>	_(Wt%)	<u>(Wt%)</u>
Split #1	5.4	5.4
Split #2	5.6	5.6
Split #3 (Waste)	89.0	88.7
Retained		0.3
Total	100.0	100.0

II. <u>Coal/Water Slurry Testing</u>: (5,000 gram at 10.0 Wt% Solids)

<u>Portion</u>	Total Slurry Recovery _(Wt%)	Total Solids Recovery _(Wt%)	Solids Content _(Wt%)	Ash Content (Wt%, Dry)
	5.5	5.3		-
Split #1	5.6	5.4	9.6	26.7
Split #2	87.3	84.2	9.7	27.2
Split #3 (Waste)	<u> 1.6</u>	<u>5.1</u>	9.6	26.9
Retained	100.0	100.0	33.2	
Total			10.0	

III. <u>Magnetite/Water Slurry Testing</u>: (Cleaner Mag Separator Concentrate Sample)

	Total Slurry Recovery	Total Solids Recovery _(Wt%)	Solids Content	Solids Analysis MVDMoment Davis-Tube			
Portion	_(Wt%)_		_(Wt%)	(Microns	(Emu/g)	Rec. (Wt%)	
		5.3			•		
Split #1	5.4	5.4	27.3	9.9	87.0	99.8	
Split #2	5.5	85.8	27.3	9.9	87.1	99.6	
Split #3 (Waste)	87.3	3.5	27.3	9.9	87.4	99.7	
Retained	1.8	100.0	<u>53.4</u>	<u>10.1</u>	<u>86.2</u>	99.6	
Total	100.0		27.8	9.9	87.3	99.7	

In May, additional testing was conducted using the Carpco wet-slitting device. Table 13 contains wet splitting results obtained for a Heavy-Media Cyclone Feed Sample (Sample #7), containing a coal/magnetite slurry. Two methods were employed:

- Flushing after removing the splits (Test PHT #21) which should be the best method of obtaining an accurate "wt% solids" split.
- Flushing prior to removing the splits (Test PHT #22) which should be the best method of obtaining an accurate "solids composition" split.

The results in Table 13 verify the theories listed above, and illustrate that the splitting accuracy of the Carpco Unit is more than acceptable, provided the slurry is well mixed as it is poured into the unit.

Throughout the test program, Custom Coals did not need to employ the Carpco wetslitting device, because all samples were filtered in a timely fashion.

Five additional QA/QC issues were also assessed and tested. They included:

- MTU/IMP Laboratory Investigation Results
- Davis-Tube Separation and Magnetic Moment Measurement, Reproducibility Testing done by MTU's IMP.
- Wet Screening Accuracy Testing done by Custom Coals.
- Duplicate Testing and Sample Reproducibility Checks, done by Custom Coals during the Heavy-Media Cyclone Components Tests
- Marcy Balance Sensitivity Testing
- Duplicate EMU Analysis on the Grade-M magnetite.

TABLE 13 CARPCO WET SPLITTER TEST WITH COAL/MAGNETITE SLURRY

(Pittsburgh No. 8 Seam Coal, Grade-K Magnetite)

I. Test PHT#21 - Cyclone Feed (Sample #7) - Flush after removing splits.

	Slur	ry	7	Total Solid	ls		+ 500N	/ Solids		-500M Solid	s Analyses	
Sample	Weight	Direct (Wt%)	Weight	Direct (Wt%)	Ash (Wt%)	Solids Content (Wt%)	Direct (Wt%)	Ash (Wt%)	Ash (Wt%)	Micotrac (MVD)	Moment (Emulg)	D.T. Rec. _(Wt%)
Split #1	965.2	5.8	512.1	5.7	63.11	53.1	23.3	13.44	79.54	12.3	54.37	63.4
Split #2	932.4	5.6	495.6	5.5	62.45	53.2	23.8	13.46	80.07	12.2	54.39	61.5
Split #3 (Waste)	14.665.0	88.6	7.803.0	86.8	66.05	<u>53.2</u>	21.7	<u>14.14</u>	<u>79.47</u>	<u>11.3</u>	<u>56.16</u>	<u>65.0</u>
Rec. Total	16,562.6	100.0	8,810.7	98.0	65.68	53.2	21.9	14.06	79.50	11.4	55.96	64.7
Split #4 (Losses)	397.4	2.3	183.2	2.0	75.96	<u>46.1</u>	33.0	63.56	<u>84.04</u>	<u>11.4</u>	<u>57.90</u>	<u>65.9</u>
Head	16,960.0	102.3	8,993.9	100.0	65.89	53.0	22.1	15.55	79.54	11.4	55.99	64.7

Note: Split #4 represents only portion left in splitter after initial split. It does not include water required to flush it out.

II. Test PHT#22 - Cyclone Feed (Sample #7) - Flush Prior to Removing Splits.

	Slur	ry	7	otal Solid	S		+ 500	VI Solids		-500M Solid	is Analyses	
<u>Sample</u>	Weight	Direct (Wt%)	Weight	Direct (Wt%)	Ash (Wt%)	Solids Content (Wt%)	Direct (Wt%)	Ash (Wt%)	Ash (Wt%)	Micotrac (MVD)	Moment (Emu/g)	D.T. Rec. _(Wt%)
Split #1	1,081.1	5.8	544.9	5.8	64.70	50.4	22.6	17.14	78.71	12.2	55.01	63.6
Split #2	1,064.3	5.7	526.1	5.7	67.59	49.4	23.2	16.34	81.15	12.0	56.22	63.3
Split #3 (Waste)	<u>16.535.0</u>	_88.5	8.260.0	88.5	65.32	50.0	20.8	<u>17.41</u>	82.44	<u>11.5</u>	<u>56.05</u>	66.6
Rec. Total	18,680.4	100.0	9,331.0	100.0	65.41	50.0	21.0	17.36	82.11	11.6	56.00	66.2
Losses (+)	166.2	0.9	0.0	-	-	0.0	-	· -	· -	-	-	-
Total Flush (-)	1.406.6	<u>-7.5</u>	0.0			_0.0						
Head	17,440.0	93.4	9,331.0	100.0	65.41	53.5	21.0	17.36	82.11	11.6	56.00	66.2

MTU/IMP LABORATORY INVESTIGATION RESULTS

In February 1995, Custom Coals subcontracted MTU's IMP to perform a laboratory investigation to determine required laboratory procedures for the fine-coal and magnetite slurry and solid samples that will be generated during the project testing. The main analytical concerns were obtaining accurate and reproducible:

- density, viscosity, and agglomeration measurements
- magnetics/nonmagnetics separations
- magnetics analyses (ie., magnetic moments and compositions)
- magnetics and nonmagnetics size analyses, down to submicron sizes.

The goal was have MTU's IMP to continue to provide laboratory analyses services, for the project test samples, using the equipment and procedures they developed during this investigation.

Mictotrac Size Analyses

One of the first areas of concern was developing sample pretreatment methods to obtain accurate particle size analysis of solids and slurry samples, using the IMP's Leeds and Northrup Microtrac Particle Size Analyzer. During the testing, the IMP staff found that three pretreatment steps were necessary to obtain accurate and reproducible size analyses with the unit. It was included that:

- The samples had to be wetted in the presence of a surfactant, if they were dry, to enhance both wetting and dispersion.
- The samples had to be demagnetized to ensure that any magnetite agglomerates were broken up.
- The samples had to be treated with an ultrasonic probe, for 5-10 minutes to ensure that all coal agglomerates were broken up.

The samples had to also be well agitated during these steps, as well as during removal of the small portion for analyses, to ensure good dispersion and a representative sample.

Once these procedures were followed, the IMP staff found that they could obtain essentially identical analyses for parallel splits, even when one split had been filtered and dried and the other had not. They also found that the Microtrac analyses for feed, magnetics, and nonmagnetics balanced around their magnetics separations, which was also an important QA/QC test.

As a check of their Microtrac analyses for bias, the IMP also sent samples of the feed magnetite to another laboratory (PTLL) for testing in a similar machine (a Malvern Unit), and also did an elaborate particle counting analysis in there SEM to determine the particle size populations. The size distribution proved to be very similar with the following reported results:

MTU's IMP Mitrotrac
 PTLL's Malvern
 MTU's IMP SEM
 5.7 micron mean volume diameter (MVD).
 5.8 micron mean volume diameter (MVD).
 6.2 micron mean volume diameter (MVD).

For the remainder of the project the -500M particle size analyses will be done with the IMP's Microtrac.

Solids Density Measurements

Table 14 shows some solids density measurements that the IMP has performed as part of their investigation. Once they switched to kerosene as the measuring media, the accuracy and reproducibility of their measurements greatly improved (to \pm 0.02 SG units) over those obtained with water, due to improved wetting. All required solids density measurements will be done by the IMP.

Davis-Tube Separation Testing (Magnetite Only)

The first step in MTU's IMP Davis-Tube separation testing was to determine a profile of Amps vs. Gauss for their Davis Tube and see if the separations matched earlier work during this project by Eriez Magnetics. The results provided essentially identical, except that MTU recovered all nonmags, so they could reconstitute yields from weights of both products, as well as from feed and mags weights. The IMP also determined that once magnetics saturations were reached on the Davis-Tube (ie., at about 0.7 amps), the recoveries remained constant, up to the maximum setting of 1.7 amps. This indicated that any amp level could be used between 0.7 and 1.7 amps to lead to similar results. However, they later found that when the highest 1.7 amp level was used the Davis-Tube had much higher capacity (ie., up to 6 grams of magnetics). This proved to be desirable to allow bigger samples, and subsequently more nonmagnetics to analyze, and better overall particle recovery (ie., approaching 99 Wt%). It was therefore decided that all Davis Tube measurements would be made at 1.7 amps.

TABLE 14 SOLIDS DENSITIES (Measured with Kerosene)

SAMPLE	SG
PennMag Grade-K "Old" Magnetite	4.73
DOE 90-X Magnetite	4.86
Hi-Temp. Magnetite	4.57
	And the second of the second o
Pittsburgh No. 8 (-325 M)	1.68
Lower Kittanning (-325 M)	1.42

Davis-Tube Separations & Magn. Moment Measurements (Coal & Magn.)

In combination with the Davis-Tube separations, the MTU's IMP has also made magnetic moment measurements of the feed, mags, and nonmags to compliment the measurements. Table 15 shows the results for separations with the initial PennMag Grade-K magnetite (old magnetite), which has a pure magnetics moment of about 84 Emu/g, and the coarser Lot #1, PennMag Grade-K Magnetite from PeaRidge (new magnetite) which has a pure magnetics moment of about 87 Emu/g. The results indicate the occasional and unexplained inefficiency of magnetics separation with the Davis-Tube, for coal and magnetite mixtures, as shown by the drop in Emu/g of the magnetics product (see DT-33, S-15, and S-16) and the higher than expected Emu/g of the nonmagnetics (see DT-33).

The inefficiencies, illustrated in Table 15, are not understood. As a result, the product team plans to compliment the Davis-Tube separation results, with magnetics moment measurements, so that magnetics contents and magnetics losses can be calculated two ways:

- From Davis-Tube magnetics at 1.70 amps.
- From magnetics moment of all samples (feeds, mags, and nonmags).

Another advantage of the magnetic moment measurements is that they allow a quick and inexpensive estimate of magnetics content of a sample. For instance, for the new magnetite testing the magnetics content can be estimated by measuring the sample Emu/g and dividing it by 87 Emu/g (the magnetic moment of pure magnetics). This has proven to be a valuable tool in the project testing.

TABLE 15
DAVIS-TUBE AND MOMENT BALANCES
(Old and New PennMag Grade-K Magnetite)

I. OLD MAGNETITE:

Test <u>Number</u>	Feed Description	<u>Sample</u>	Weight (Grams)	Weight (Wt%)	Moment (Emu/g)	Dist.
DT-24	Magnetite Only	Mags <u>Non Mags</u> Total	5.64 <u>0.27</u> 5.91	95.5 <u>4.5</u> 100.0	84.30 _1.00 80.55	99.9 <u>0.0</u> 100.0
DT-37	Pitts. No. 8 Coal Only	Mags <u>Non Mags</u> Total	0.00 <u>5.87</u> 5.87	0.0 <u>100.0</u> 100.0	0.00 <u>0.21</u> 0.21	0.0 <u>100.0</u> 100.0
DT-33	Sim. Cyclone Feed (1.0/4.7g. Coal/Mag.)	Mags <u>Non Mags</u> Total	4.32 <u>1.30</u> 5.62	76.9 <u>23.1</u> 100.0	80.40 _ <u>1.67</u> 62.21	99.3 <u>0.6</u> 100.0

II. <u>NEW MAGNETITE</u>:

Test <u>Number</u>	Feed Description	Sample	Weight (Grams)	Weight (Wt%)	Moment (Emu/g)	Mome Dist. <u>(Wt%</u>
DT-54	Magnetite Only	Mags <u>Non Mags</u> Total	4.92 <u>0.04</u> 4.96	99.2 <u>0.8</u> 100.0	86.74 <u>7.35</u> 86.10	99.9 <u>0.0</u> 100.0
S-13	Cyclone Feed	Mags <u>Non Mags</u> Total	4.00 	68.7 _31.3 100.0	87.07 <u>0.53</u> 59.98	99.7 <u>0.2</u> 100.0
S-15	Final Coal Product	Mags <u>Non Mags</u> Total	0.05 <u>15.76</u> 15.81	0.3 <u>99.7</u> 100.0	83.71 <u>0.12</u> 0.37	67.8 <u>32.1</u> 100.0
S-16	Scav. Mag. Sep. Tailings	Mags <u>Non Mags</u> Total	0.05 <u>8.40</u> 8.45	0.6 <u>99.4</u> 100.0	70.67 <u>0.36</u> 0.78	54.2 _45.7 100.0

DAVIS-TUBE AND MAGNETIC MOMENT REPRODUCIBILITY TESTING

During May, MTU's IMP performed a number of duplicate analyses to observe the reproducibility and closure of the Davis-Tube magnetics separations and magnetic moment measurements they perform, as part of their routine analyses for the project. Table 16 illustrates duplicate Davis-Tube separations for two methods they have tested during the project. All four separations were performed with identical dried splits of a Combined Drain Screen Underflow Sample (Sample #16) from the commissioning tests. The two methods tested included:

- Complete water evaporation of the Davis-Tube products to ensure complete, particle recovery, followed by magnetics moment analyses (Lab. No. S-8-1A & S-8-1B).
- Partial settling of Davis-Tube products followed by decanting and micropore filtering (Lab. No. S-8-2A & S-8-2B).

The second method was the standard method MTU's IMP normally employs.

The results in Table 16, and in other duplicate tests, illustrates that either method leads to very good reproducibility of separations (ie., magnetics yields, moment measurements, and moment distributions). The major difference is that the water evaporation method causes a significant weight gain due to precipitation of solids from the vast amount of water used in the Davis-Tube Procedure; whereas, the normal method leads to a slight weight loss due to decanting and filtering losses. Custom Coals has decided that the normal method (ie., decanting and filtering) is preferred, and has setup procedures to maximize sample size so that the slight losses of colloidal and/or soluble particles do not skew results.

Similarly, Table 17 contain a number of duplicate magnetic moment measurements for samples with vastly differing magnetics contents. The results illustrate that the moment measurements are reproducible to within 0.3 to 0.7 EMU/g. This does not create a problem for high EMU content samples, but can cause significant percentage-basis errors for samples containing minute amounts of magnetite (ie., see R.E. Magnetic Separator Tailings in Table 17). Custom Coals plans to duplicate and tripulate the magnetic moment samples, and also plans to combine the moment measurements with Davis-Tube separations, to reduce the likelihood of errors and ensure that accurate determinations of magnetics losses are obtained during integrated testing.

TABLE 16
DAVIS-TUBE SEPARATION
ACCURACY AND REPEATABILITY TESTING
(Pittsburgh No. 8 Seam Coal, Grade-K Magnetite)

	•					
MTU/IMP	Particle Recovery	Davis Tube	Weight	Weight	Moment	Moment
Lab. No.	Method/Approach	Product	(g)	(Wt%)	(Emu/g)	Dist. (%)
5-8-1A	Water Evaporation	Mags	6.444	82.46	85.099	99.85
		<u>NonMags</u>	<u>1.371</u>	<u> 17.54</u>	<u> 0.601</u>	<u> </u>
		Recon. Feed	7.815	100.00	70.275	100.00
		Head	7.537	-	74.084	
5-8-1B	Motor Evoporation	Maga	6.893	82.09	86.007	99.83
3-0-1D	Water Evaporation	Mags				
		NonMags .	<u>1.504</u>	<u> 17.91</u>	<u>0.652</u>	0.17
		Recon. Feed	8.397	100.00	70.719	100.00
		Head	8.064	-	74.084	_
5-8-2A	Settle, Decant, & Filter	Mags	6.424	85.61	85.285	99.84
	•	<u>NonMags</u>	1,080	_14.39	0.595	0.16
•		Recon. Feed	7.504	100.00	73.096	100.00
		Head	7.527		74.084	-
5-8-2B	Settle, Decant, & Filter	Mags	5.301	85.96	87.052	99.84
3-0-25	Settle, Decant, & Filter	-				
		<u>NonMags</u>	<u>0.866</u>	<u>_14.04</u>	<u>0.855</u>	0.16
		Recon. Feed	6.167	100.00	74.948	100.00
		Head	6.254	-	73.986	-

Notes: All four separations done with identical splits of Test CMT#1, Sample #16 (Combined Drain Screen Underflow), from Commissioning Tests.

TABLE 17
MAGNETIC MOMENT
MEASUREMENT REPRODUCIBILITY
(Pittsburgh No. 8 Seam Coal, Grade-K Magnetite)

					Ma	gnetic Mom	ent
MTU/IMP <u>Lab No.</u>	Test <u>Number</u>	Sample Number	Sample Description	Davis Tube <u>Product</u>	Dup. #1 (Emu/g)	Dup. #2 (<u>Emu/g)</u>	Avg. (Emu/g)
S-2	MT #2	#40	Cleaner Magnetic Separator Conc.	Head Mags	86.995 87.324	86.800 86.989	86.897 87.156
S-8	CMT #1	#16	Combined Drain Screen Effluent	Head Mags NonMags	74.886 85.577 0.636	74.783 84.993 0.554	74.834 85.285 0.595
S-14	CMT #1	#22	Rinse Screen Refuse Discharge	Head NonMags	8.746 0.297	9.441 0.316	9.093 0.307
S-16	CMT #1	#36	R.E. Magnetic Separator Tails	Head NonMags	0.922 0.723	0.940 0.437	0.931 0.580

Note: All measurements done with 0.03 to 0.15 gram sample dependent on bulk density of sample.

WET SCREENING ACCURACY TESTING

Custom Coals performed QA/QC testing to assess the completeness of the 500M wet screening being done with the homemade, vibrating-vacuum unit being used at site (see results in Table 18). In the testing, samples of heavy-media cyclone overflow (Sample #9A), underflow (Sample #8A), and feed (Sample #7) were subjected to normal screening and washing, where the sample is assumed complete once the lab screen effluent becomes clear (PHT#1). The washing amounts were also doubled in a similar test to access any improvement (PHT#2). Since all the magnetite is slightly finer than 500M the distribution of magnetics offers the best possible quantification of screening efficiency. The results in Table 18 illustrate, that in all cases, over 99.95 Wt% of the sample magnetics were screened into the 500Mx0 fraction, where they belong. This is extremely efficient, and illustrates that the normal washing approach is more than adequate for our test samples.

DUPLICATE TESTING AND SAMPLE REPRODUCIBILITY

The final set of QA/QC-related tests, performed in May were duplicate testing and sampling done as part of the Heavy-Media Cyclone Component Testing. These tests were performed during the second batch of Heavy-Media Cyclone Component Tests (PHT#11-#20), at 10:1 media-to-coal ratio, after the inadequate mixing occurring during batch #1 had been principally corrected. Table 19 contains the results from two identical, back-to-back tests and illustrates the good performance reproducibility that can occur when the mixing stays steady.

By contrast, Table 20 shows the variability of a number of "actual" and "reconstituted" feed samples that were taken over a slightly longer period. The results indicate that the mixing is not yet perfect, and there are random and biased variations that occur as the sump volume is dropping that need to be considered when drawing conclusions from the data.

TABLE 18
QA/QC TEST FOR ON-SITE WET SCREENING
(Pittsburgh No. 8 Seam Coal, Grade-K Magnetite)

Michigan Company and American State of Special Company	PHT#1 (Nor	mal Washing)	PH	T#2 (Double Was	shing)
	Sample #9A Cyclone Overflow	Sample #8A Cyclone Underflow	Sample #9A Cyclone _Overflow	Sample #8A Cyclone Underflow	Sample #7 Actual Feed
Top x 325M Size Fraction					
Weight Distribution (Wt%)	44.9	7.3	47.4	4.2	22.9
Magnetics (Wt%)	0.01	0.44	0.01	0.41	0.07
Magnetics Distribution (Wt%)	0.01	0.04	0.01	0.02	0.02
325 x 500M Size Fraction					
Weight Distribution (Wt%)	5.7	2.4	7.9	1.5	4.2
Magnetics (Wt%)	0.03	0.40	0.04	0.47	0.17
Magnetics Distribution (Wt%)	0.00	0.01	0.01	0.01	0.01
500M x 0 Size Fraction					
Weight Distribution (Wt%)	49.4	90.3	44.7	94.3	72.9
Magnetics (Wt%)	93.78	96.97	85.33	94.96	94.22
Magnetics Distribution (Wt%)	99.99	99.95	99.98	99.97	99.97
Combined Size Fractions					
Weight Distribution (Wt%)	100.0	100.0	100.0	100.0	100.0
Magnetics (Wt%)	46.33	87.61	38.15	89.57	68.71
Magnetics Distribution (Wt%)	100.00	100.00	100.00	100.00	100.00

Note: Magnetics (Wt%) determined from Davis-Tube Separations on all size fractions.

TABLE 19
DUPLICATE TEST RESULTS
HEAVY-MEDIA CYCLONE COMPONENT TESTS
(Pittsburgh No. 8 Seam Coal, Grade-K Magnetite)

	Te:	st PHT #18 Resul	ts	Tes	st PHT #19 Resul	ts
	Sample 9A Cyclone Overflow	Sample 8A Cyclone <u>Underflow</u>	Recon. <u>Feed</u>	Sample 9A Cyclone <u>Overflow</u>	Sample 8A Cyclone <u>Underflow</u>	Recon. <u>Feed</u>
SLURRY COMPOSITION						
Slurry Feedrate (GPM)	-	-	36.2	. **	-	36.2
Slurry SG	1.31	1.80	1.48	1.32	1.80	1.50
Solids Content (Wt%)	48.3	59.3	53.1	48.6	59.5	53.4
OVERALL SOLIDS PERFORMANCE						
Yield (Wt%)	51.6	48.4	100.0	50.9	49.1	100.0
Proportion (Wt%)	100.0	100.0	100.0	100.0	100.0	100.0
Ash Content (Wt%)	42.49	87.15	64.11	45.17	89.32	66.81
TOP X 325M PERFORMANCE						
Yield (Wt%)	79.4	20.6	100.0	78.8	21.2	100.0
Proportion (Wt%)	25.3	7.0	16.5	23.7	6.6	15.3
Ash Content (Wt%)	6.19	58.38	16.94	6.32	59.82	17.66
325 X 500M PERFORMANCE						
Yield (Wt%)	76.3	23.7	100.0	75.0	25.0	100.0
Proportion (Wt%)	12.1	4.0	8.2	11.3	3.9	7.7
Ash Content (Wt%)	4.83	24.00	9.37	4.96	26.24	10.28
500M x 0 PERFORMANCE						
Yield (Wt%)	42.8	57.2	100.0	43.0	57.0	100.0
Proportion (Wt%)	62.5	88.9	75.3	65.0	89.5	77.0
Ash Content (Wt%)	64.46	92.35	80:41	66.32	94.24	82.23

Note: Both tests performed at 10:1 media-to-coal ratio, at 90 PSI feed pressure, with 0.12 square inch inlet 1.0 inch vortex, and 0.875 inch apex in 4" Heavy-Media Cyclone.

TABLE 20
DUPLICATE FEED SAMPLE RESULTS
HEAVY-MEDIA CYCLONE COMPONENT TESTS
(Pittsburgh No. 8 Seam Coal, Grade-K Magnetite)

	Test PHT #	#18 Results	Test PHT #19 <u>Results</u>	Test PHT #	[£] 20 Results
	Actual	Recon.	Recon.	Recon.	Actual
	<u>Feed</u>	<u>Feed</u>	<u>Feed</u>	<u>Feed</u>	<u>Feed</u>
SLURRY COMPOSITION					
Slurry SG	-	1.48	1.50	1.50	-
Solids Content (Wt%)	53.4	53.1	53.4	53.4	53.4
OVERALL SOLIDS ANALYSIS					
Proportion (Wt%) Ash Content (Wt%)	100.0	100.0	100.0	100.0	100.0
	69.82	64.11	66.81	67.01	64.84
TOP X 325M ANALYSIS					
Proportion (Wt%) Ash Content (Wt%)	13.4	16.5	15.3	15.1	16.7
	19.36	16.94	17.66	17.64	16.56
325 X 500M ANALYSIS					
Proportion (Wt%) Ash Content (Wt%)	7.2	8.2	7.7	7.5	8.1
	11.33	9.37	10.28	9.35	9.09
500M X 0 ANALYSIS					
Proportion (Wt%) Ash Content (Wt%)	79.4	75.3	77.0	77.4	75.2
	83.64	80.41	82.23	82.23	81.57

Note: All Tests performed with same feed batch at 40.0 Wt% Media Contamination.

MARCY BALANCE SENSITIVITY TESTING

During June CCI conducted a sensitivity test on the Marcy Balance to assure that accurate specific gravity measurements were being obtained. CCI decided to conduct this sensitivity test since in many cases the measured specific gravities of the 4" heavy media cyclone overflow and underflow did not agree with the calculated specific gravities of the overflow and underflow. Before conducting the sensitivity test the Marcy Gauge was calibrated with water and known specific gravity test The results of the calibration indicated that the Marcy Balance was samples. producing accurate results. Next, researchers developed four means to determine the sensitivity of the Marcy Balance. First the Marcy cup was allowed to overfill the entire cup before removing it from the correct media stream. Any material that was deposited on the sides of the cup were not removed and the cup was then placed on the Marcy Balance (column #1-Table 21) and a reading was obtained. Second, the cup was then removed and the sides cleaned to remove any material that was deposited on the cup sides before another reading was obtained (column #2 - Table 21). Next the media in the cup was removed and the cup was cleaned. The cup was then filled only to the overflow holes allowing any material that was deposited on the sides of the cup to remain and another reading was taken (column #3 - Table 9). Lastly, the cup was removed and the sides cleaned to remove any material that was deposited on the cup sides before another reading was obtained (column #4 -Table 9).

As can be seen from Table 21 the small amount of material deposited on the sides of the cup had almost no influence in the specific gravity reading. However, overfilling the Marcy cup had a significant influence on the specific gravity reading. This is most likely do to the solids setting in the cup during the time the sample is taken until the cup is placed on the Marcy Balance. By the time the cup is placed on the Marcy Balance most of the solids have settled below the overflow holes concentrating the solids in the Marcy cup which falsely increases the specific gravity reading of the Marcy Balance. During future test work, efforts will be made not to overfill the Marcy cup, and calculated specific gravities will be used instead of measured specific gravities if the measured vs. the calculated specific gravities differ by a large percentage.

TABLE 21: Marcy Balance Sensitivity Test Results

verfilling Marcy and Not Cleaning	Overfilling Marcy and Then Cleaning	Not Overfilling Marcy and Not Cleaning	Not Overfilling Marcy and Then Cleaning	Nuclear Density Gauge
S.G.	S.G.	S.G.	S,G,	S.G.
1.440	1.430	1.410	1.410	1.42
1.435	1.430	1.400	1.400	1.43
1.435	1.430	1.400	1.400	1.43
1.435	1.425	1.405	1.405	1.43
1.430	1.430	1.410	1.410	1.43
1.430	1.430	1.410	1.405	1.42
1.430	1.430	1.410	1.405	1.43
1.433	1.429	1.406	1.405	1.427

During this quarterly technical progress report two additional QA/QC issues were assessed. They included:

- Reconstituting the Grade-L magnetite magnetics and non-magnetics size fractions to assure that their reconstituted head agreed with the "as received" magnetite size consist.
- Assuring that the Grade-L magnetite size analysis did not change after numerous hours of integrated testing.

RECONSTITUTION OF GRADE-L MAGNETITE

During August concerns arose, regarding the Microtrac results of the "as received" magnetite vs. the 1.7 Amp Davis Tube magnetics of the magnetite in that the magnetics fraction of the magnetite was approximately 1 MVD finer than that of the "as received" magnetite. As a result, MTU's IMP performed Microtrac analysis on:

- The Grade-L "as received" magnetite.
- The 1.7 Amp Davis Tube magnetics from the Grade-L magnetite, and
- The 1.7 Amp Davis Tube non-magnetics from the Grade-L magnetite.

MTU's IMP then reconstituted the magnetics and non-magnetics fractions to obtain a reconstituted "as received" sample. The results are contained in Table 22.

Table 22: Reconstituted Grade-L Magnetite Comparison

Size(μ)	Cumulative As Received (Wt%)	Cumulative Magnetics (Wt%)	Cumulative Non-Magnetics (Wt%)	Cumulative Reconstituted Head
+88	0.0	0.0	0.0	0.0
88 x 62	0.0	0.0	0.0	0.0
62 x 44	0.0	0.0	0.0	0.0
44 x 31	0.0	0.0	0.0	0.0
31 x 22	0.0	0.0	0.0	0.0
22 x 16	1.1	0.8	3.5	0.9
16 x 11	8.6	7.9	13.7	8.2
11 x 7.8	24.5	23.2	27.0	23.4
7.8 x 5.5	43.7	42.6	40.3	42.5
5.5 x 3.9	58.9	57.9	50.5	57.6
3.9 x 2.8	75.9	76.8	65.1	76.3
2.8 x 1.9	91.0	92.1	82.6	91.7
1.9 x 1.4	96.3	96.6	91.3	96.4
1.4 x 0.9	99.3	99.2	97.3	99.1
-0.9	100.1	100.1	99.8	100.1

As can be seen from Table 22, the reconstituted head results agree extremely well with the "as received" results. Table No. 22 also indicates that the non-magnetics fraction is coarser than the magnetics fraction which explains the 1 MVD size difference between the "as received" magnetite and the 1.7 Amp Davis Tube magnetics.

GRADE-L MAGNETITE COMPARISONS

When removing the Grade-L magnetite from the Micro-Mag circuit a sample of the circulating media was obtained and analyzed for size and magnetic moment. This was done to assure that the magnetite quality did not change after numerous hours of processing during the primary integrated testing. Table 23 compares the results for the Grade-L magnetics before processing and after processing.

Table 23: Grade-L Magnetite Magnetics Comparison

Size (μ)	As Re	ceived	After Pi	rocessing
	Vol.	Cum.	Vol.	Cum.
+22 22 x 16 16 x 11 11 x 7.8 7.8 x 5.5 5.5 x 3.9 3.9 x 2.8 2.8 x 1.9 1.9 x 1.4	3.1 10.7 17.6 20.1 18.3 15.8 10.0 2.7 1.5	100.0 96.9 86.2 68.6 48.5 30.2 14.5 4.5	3.4 10.1 16.4 19.2 18.0 17.3 11.1 2.7 1.5	100.0 96.6 86.5 70.2 50.9 32.9 15.6 4.5
-0.9	0.3	0.3	0.3	0.3
MVD D ₉₀ D ₅₀ D ₁₀ EMU/gm	12 5. 2.	64 .78 67 40 .24	12 5 2	.51 2.72 .42 .34 7.02

As can be seen from Table 23, the magnetics fraction of the Grade-L magnetite quality after processing in the Micro-Mag circuit is identical to that of the as received.

GRADE-M DUPLICATE EMU ANALYSIS

During November while performing Davis-Tube magnetic analysis on the two Grade-M primary integrated tests (PIT #9 and #10) it became obvious from the high ash contents in the Davis Tube tailings that the Davis Tube was unable to provide accurate magnetic analysis on the Grade-M magnetite. As a result, researchers were unable to compare the Davis Tube magnetics to those of the EMU magnetics to assure accurate magnetic analysis was being obtained. With no second method to verify magnetic content of samples, researchers decided to run duplicate EMU analysis on numerous samples to assure that the EMU magnetic analysis was

repeatable and could by itself be relied upon for magnetic analysis. The results from these duplicate samples are contained in Table 24.

Table 24: Comparison of Duplicate EMU Analysis

Sample No.	Original EMU Measurement	Duplicate EMU Measurement
84	76.629	76.025
85	74.479	74.411
87	44.545	44.544
88	21.862	22.037
90	64.929	65.227
92	79.201	80.005
99	59.337	60.091
100	23.539	23.007
102	51.289	51.298

As can be seen from Table No. 24, the duplicate EMU measurements compare extremely well to the original EMU measurements. With such excellent duplication results, EMU measurements will be used to determine magnetic content on all Grade-M magnetite test runs.

5.7.3 CIRCUIT TESTING RESULTS

During September data analysis was completed on the Grade-M primary integrated tests. One test was conducted using the Micro-Mag circuits drain and rinse screens (PIT #9) and one test was conducted by-passing the drain and rinse screens (PIT #10) which allowed the 2-inch H.M. cyclone products to report directly to the magnetic separator circuits. As can be seen from the results contained in Appendix A, 486 lbs/ton of the Grade-M magnetite was lost when using the drain and rinse screen configuration and 94 lbs/ton of the Grade-M magnetite was lost when by-passing the drain and rinse screens. These results are not surprising since large losses of magnetite were seen using other grades of magnetite when incorporating the drain and rinse screens in the Micro-Mag circuit. Additionally, the 94 lbs/ton magnetite loss seen when by-passing the drain and rinse screens is also not surprising since the Davis Tube profile of the Grade-M magnetite indicated that its recovery would be extremely difficult. Another significant finding from PIT #10 is the ash valves of the 4-inch H.M. cyclone products. Fairly low ash valves were obtained on the +200M (39.62% Ash) and the 200M x 500M (54.23 % Ash) cyclone underflow, indicating poor cyclone performance. This corresponds to the poor performance of the cyclone that was seen during the "closed-looped" cyclone tests using the Grade-M magnetite.

Section 5.8 - Task 80-: Analytical (Month 5-14)

As discussed in previous Quarterly Reports the analytical requirements have been determined. They are:

- Custom Coals on site laboratory performed % solids, ashing, wet screening, and sample preparation
- MTU's IMP performed density, magnetics/nonmagnetics separations, ashing on 500M x 0 nonmagnetics and microtrac analysis.
- CTE's Kentucky laboratory performed all fine washability analysis.
- CTE's Pennsylvania laboratory performed sulfur, sulfur forms, and Btu analysis.

Section 5.9 - Task 900: Circuit Decommissioning (Month 14)

The circuit decommissioning task has been deleted from Custom Coals' Contract as DOE has elected to leave to Micro-Mag circuit in place for possible future testing. As a result, the 20K that was budgeted for decommissioning the circuit will be used for additional testing. However, all equipment will be transferred to DOE possession prior to Custom Coals leaving site.

Section 5.10 - Task 1000: Data Evaluation (Months 5-15)

The data evaluation task began in January 1995 with the Laboratory Procedure Investigation and will run through December 1996. It will include evaluation of the preliminary laboratory procedure studios done prior to the circuit commissioning, as well as evaluation of all the circuit commissioning and testing results. Custom Coals' Project Manager will keep up on all data evaluation and present it in a timely fashion, within the Monthly Technical Status Reports and Quarterly Technical Progress Reports.

Section 5.11 - task 1100: Final Reporting (Months 15-16)

Custom Coals anticipates submitting a Draft Final Report in December 1996. The report will contain:

- A chronology of the project events by task series.
- A summary of all testing results, sample analyses, and data calculations.
- A list of the major project conclusions with specific emphasis on the project objectives.
- A discussion of the project successes and failures with specific emphasis on methods of eliminating problems in future projects.

 An economic evaluation of the micronized magnetite project, including case studies for scale-up of the as-tested circuit.

After review by DOE's Technical Project Management Team, the Draft Final Report will be revised and resubmitted.

SECTION 6 - GOALS FOR NEXT QUARTERLY REPORTING PERIOD

The goals for the next quarterly reporting period include completing:

- Data analysis on the Grade-M Long Duration Tests
- Data analysis on the Grade-L Long Duration Tests
- Partion curves on the Grade-L and Grade-M Long duration tests
- Draft final report for DOE Comments

APPENDIX A

GRADE-M PRIMARY INTEGRATED TEST RESULTS

MEDIA RECOVERY CIRCUIT TESTS

CONDITIONS AND MAGNETICS RESULTS Total Circuit Losses = 38,00+39,80+9,62 = . DATE

4100+69.20+146.48

COAL

Pittsbotsh No. 8 Seam

Test Sam MAGNETITE: Par Bay - Gride-M 30 .6 33 77 B 39 40 BE çı Çı Q 9 A.A. Coxxxt Madia Scal Mag. Adams 143 May Sep Feat Recoll. Pri Clean. Mas. C.C. Discharge Ringe School Cyclone Fred Heavy Madia Sep. CONC Cyclove Under Clean. May, Sup Tails RECOM Sample Fread 2420 ·· CONC なる Discharge Touls Screen configuration Riuso School Angle ON Correct Media No Draw to Slight Mag. (cuty) | meas | Cale. | meas | Colc. | Cuty) (#/hd) SES SES · SIDIN SG 1.38 1.36 486,41651pH 1:37 1:32 1.33 1.39 55.8 1.31 1.38 ı 1 1 į 1 1.22 42.5 1,02 1,0% 1,02 101 <u>ئ</u> ئ 70,7 1.31 8 Ħ . 1 ı ı ŧ ı Flowrate (GAM) ı ŧ l 8.4 3.5 3.57 3.9 30.30744 1951 1990 80 رق 194,3 | 5.51 | 781 31.5 0.23 73 55 31.701.114 1.6 34.95 370 14.1 25.57 659 4.7 30.46 943 36.2 5.38 1,016 1 30.93 33.24 4.03 120 122 Solids 199 64 • 1 (また) (まな) ried Warght 1 1 ١ soomxo magnetics 1 ţ 1 ţ 1 1 1 1 ١ 1 1 1 1 I. 66.14 33.86 94.86 (Teld | County Keld | County 100.00 93.48 100,00 94.57 100.00 95.91 ľ, 9666 97.05 95,91196.77 1 3.34 54.32 1 1 4.09 79.36 ٦, COMMENTS: Primary Internited Tast (No Recite 87.78 87.90 90.80 26.77 93.88 97,08 1 i ١ Total Magnetics ١ I ١ 1 1 1 ١ ١ 1 ١ 1 1 l 1 1 1 1 1 14 i ŧ 96.66 96.66 32.9 100.00 18.78 14.3 33.86 80.29 18.5 66.14 1803 12.8 100.00 184.38 17.4 95.91 96.77 30.0 100.00 93.66 409 53.11 3.8 3.34 18.03 35.91 74,00 8.9 6.16 84.36 30.10 33,2 23.4 13.7 100/ -500m 707A Coal Rate 0.4 9.9 <u>-</u> ġ 28.9 0.4 2010g 30.0 9.0 3.6 5.4 0 5,4 3.7 4.1. 14.8 ە:0 -ZA 79/# N.A. 1,120 ONH N.A. N.A. Z <u>₹</u> 131 N.A. N.A 198 N.A. N.A

MEOIA RECOVERY CIRCUIT TESTS

1	٤)	* *			·				*	# 7		1			>0. Test		3	C	
	ИН	36	30	29	27	39	40	38	25	ಶಿಶಿ	١	80	0	7	\$ 3		300	COAL	
	Correct Media	Scav. Mag. Sap. Tails	Sep. Tails			Sep. Tails	Sep. Conc.	Clean May. Sap Faced	Rinse School C.C. Discharge	Rinse Schann Ref. Discharge	Recon Faced). Under	P	Hoavy Modia Cyclone Food	NAME!C		MAGNETITE: B	: P.Hsbursh	
	1	J	95.03	4.97	100.00	100.00 14.6	0.00	100.0	-	. 1	100.00	39.61	60139	1	(4th)		Pen-Ridge-Grade	h 16.8	
	7.0/	35.8	21.48	0,2	3.47	14.6	0.0	0.40	54.2	8.23	7.3	8.7	6.6	9.2	(m4 42)	200m	- Grad	Seam	
	13.62	10.00	10.41	17.82	10.78	13.31		16.79	5.19	27.23	14.80	26.06	7.42	17.07	(mage)	7	B	13	
	}	ì	97.64	a.36	00.00	100.00 18.1	000	100.0	1	1	100.00	26.35	13165	ł	rield (usz)	20		••	
	6.1	51.2	97.64 45.7	0.2	7.31	18.1	0.0	0.21	12.7	5.6	4.8	6.7	9.3	8.5	(m+m)	200x Spom			3
	15.30	11.18	11.85	22.15	12.09	14.00	1	21.37	5.26	17,22	11.79	31.23	4.83	14.17	(was)	3			Nonmacs
	1		5,81	94.19	100.00	4.94	95.06	100.0	١		100.00	33.36	66.64 84.1	<u></u>	Tipld (what)	4 .		·	35/2E
	96.9	23.0	5,81 33.2	94.19 99.6 >100.00	89.2	67.3	95,56 100.0	97.17	33.1	38.6	84.3	84.6	84.1	823	curun)	axwoos	·	•	
	00.00	64.72	79.39	>/00.00	08:8P¢	94.80	>/00.00	>/00.00	97.34	14.86	>98.73	>/00.00	98.10	7/00.00	(ware)	9			ERBCHONS.
	Ī	1	48.85 45.60	51,15	100.00	25.00 20.64	7500	100.0	1	1	100.00	36.17	73.83		Yield Curns		CON	DATE	SAG
	2,98	79,23	45.60	2.95	15,43	20.64	3.23	4.09	9.20	6.92	5.50	5.12	7.32	8.30	(n+70) (n+70)	DXO No	COMMENTS	M	
	1	1	1	ł	¥	1	1		1	1		1	ħ;	[(0.44%)	Nonmags	•••	10-	
	. 1	1	81.94 81.97	18.06	100.00 15.62	52.7	47.3	0,00		ì	100.00 21.22	30.86 19.71	69.14	J	(2 \$ 2) X & & & & & & & & & & & & & & & & & &		Primary	10-16-95	
	15.64	93.94	81.97	3.34	15.62	46.59	3.43	6.34	69.90	64.09	a1.aa	19.71	21.97	26.00	Casal	Total Nonmas	Tuteur	19	
	1	1	•	1	1	•	1	J		,	(.1	Ži.	•	Ash (wth)	n.tmags	ted Tac		
	1	1	15.62	84.38	00.00	7.17	92.83	100.00	¥	j	100.00 >85.30	29.63	70.37		(m+%)	1 -	Total Test CM Recirc.		
	90.77	19.28	18.86	>/00.0	>89.39	69.91	0.001	100.00>100.0	38.68	50.14	>8530	88.62	83.43	84.55	Cutro Cutro	10	Recirc)		

								7											
949	0.1	0.4	4.82	1			28.38	ı		I	394	3 1.50	SB.3	ŏ	- 1,00			Sent 1003	36
3,157	1.7	11.5	68.38	77.97	1	١	72.82	72.97	ı	I	1,063	2.98	15.8	1	80.1			11	30
N.A	9.3	14.3	99.9%	82.03	P	1	93.48	24.03	1	١	308	7 11.13	3.7	19	- 1.09			1 1	2 22
N.A.	0.E	12.0	14.39	0.001	1)	92 ,32	100,0	.1	1	1,271	5 12.07	19,5	100	- 1.08			L 18 ' '	3 1
											П		H	H		-		•	T
A.S	3.9	13.5	74.67		1	1	93.10	- Veri	- 1	1		34.16	79 -	7 57.9	1.33 1.27			Media	HH
												H	H	H		· ·	SEPARATORS	11	
N.A.	1.4	14.0	57.51	2.29	١	1	જ્વ.કર	2.29	. 1	١	34	6 O.H3	13.6	5	- 1.00	3.	RAN All 5	Cleanor Mag. Sep. 791/5	39
NA	30.8°	25.8	34.38	17.79	l	1	7637	97.71	1.	ŀ	870	16.3K	н.8	280	3-		Correct media	Cleaner Mag. Sep. Conc.	40
N.A.	15.6	25.3	9399	100.0	١	1	96,30	100.0	1	1	404	11.5	18.4	37	- 1.07	;	No omin to	Sep. Fand	38
												H	H	H				1 1	Á
N.A.	2.0	12.0	67.19	100.00 67.19	١	1	92.39	100.00	1	1	1,237	33,60	5.9	5	- 1.25		1 mpc10	Recon. Feed	11
N.A.	a.o	II.a	66/15	31,99	١	1	91,79	31,99	١	1	400	38.38	1.7	1	1:39 1.26		No DtR	Cyclone Under	80
N.A.	<i>a.i</i>	12.4	67.53	69.01	1		92.53	1089	1	ì	937	31.75	4,2	15	1.27 1.25		•	Cyclone Overs	9
												H	Ħ			7	to 21 Cyclone	•	T
N.A.	1.7	1.8	63.40	100.00	١	}	1068	100.00	1] -	8,115	3608	36.6	1.	- 1.39	Min,	PSI	Recon Feed	
N.A.	1.2	90	53.66	16.54	İ		81.18	16.54	ŀ	1	1,586	145.33	5,2	5	1.50 1.35	<i>(</i> =	to H"Cydom	8A Gyclone Under	8A
N.A.	1.9	1.9	65.76	83,46	J	1	98.99	83.46		1	6,529	32,73	91.4	7	1.30 1.87		#54 a8	Cyclone Overs	9,4
7 11 7 1									-			IT	H	H.	\prod	1 4			
XA	20	10.8			1	1		1		l.	k	34.05	1	7 12.5	1.27			Cyclone Feed	7
	2	7 3 1			3 2 E	12.5 12.5			2 C C C C C C C C C C C C C C C C C C C	3 2 P	(wat) (#/h)	- Carr	s. Ook.	e, Mens.	max Cale.	(mother man	Configuration	Name	· t sam
		Coal Ret		Canetics	71 000	70m/	î	ragner	N N N	Soom	solids	_	2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	6 GH	storm SG				
6/kc)	CHO R.	1 Test	Intervation		Rimary	72	36	200	· · · · · · · · · · · · · · · · · · ·	•							Ridge - Gmda-M	AGNETITE: Pen-F	AGNE:
· -			-	-95	-16	0	DATE:	DA.	= 94 165 / Am	4/165	···	Losses	1	dirent	76/4/	、 1	No.8 Seam	-Pittsburnh	JAL:
					-		प	RESUL	ics 's	WET	ma.	ANO		700	COMOITIONS			•	Ή. (υ)

	3 4							-		,		7					\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\			3	6/ Ø/	4
36	30	29	1	144	39	40	38	_	1		. 6	1	1 .	8,8	9,9	7	i Se	SAm.		SQL SQL	con L	V
Scav. Mag; Sup Tails		Primary Mag. Sep. Conc.		Madia	Cleanet Mrg. Sep. Tails	Cleanet Mag. Sep. Conc.	Clannet Mag. Sep. Feed	_		2" Hrm Cyclone Unders	N X			choise nyers	Chelous Dans	Cyclone Feed	_	Sample		177E : _£	Pitsburst	
4	97.43	2.57	00.001		67.91	32.09	000		00.00	35.17	64.83		00.00	30.71	69.39	,	("L PM)	PI 3'A	+	es Aidre	No. :	
41.0	17.0	23	14,62	10.0	38.3	0.7	a-17		14.0	15.a	13.4		14.3	22.7	12.3	14.a	(24 tm)		200m	e-Gride-M	10	•
11.05	11.91	16.75	16.43	15.02	9.23	14.75	12.03		16.95	38,82	5.08			39.63	5.28	15.11	(mm)	Ash		e-M	Seem	
•	19.61	1,39	100.00	1	3.87	96 13	100.0		00.00	30.36	69.64		100.00	ga. ao	77.80	1	(may)	rield	20		, , , , , , , , , , , , , , , , , , ,	•
42.0	15.2	1.1	12.87	9.8	0.2	0,2	0.2		13.2	12.4	13.6		14.3	16.4	13.8	13.0	(W.J.)	46.00	modexor		-	\$; \$;
14.69	15.19	28.71	15.86	17.52	15.01	32.47	18.87		15.86	35.98	7.09		17,09	54.33	6.50	16.71	(Katric)	2,2	3	`	3 e	Nownmas
ì	79.35	21.75	00.00	i,	2:36	97.64	0.001		100.00	32.17	67.93		00.00	16.52	83.48	- 1	(my	R)ay	(4	· 	<u>-</u>	2215 5
17.0	67.8	96.6	72.51	80,2	61.6	99.1	97.7	_1_	72.8	72.4	73.0		71.17	60.9	73.9	72.8	(East	467	xmoos			
67.34	89.28	>100.00	99.3/	00.00	16:88	7/00,00	>/00.00		>99.55	2/00.00	99.34		99.22	99.34	99.20	99.26	(mage)	Ash	Ö		.4	FRAGTIONS
)	81.55	18.45	00.001	440	4.17	95.83	100.0		/00.00	34.27	65.73		100.00	16.35	83.65	1	Tara?	Yeld	5000	Con	DATE	28
71.62	108	6.52	7.68	6.90	37.45	9.73	08.8		7.71	8.21	7.47		10.99	10.87	10.11	8.47	(m)	=	on oxe	Commen	m	' i
	- Andrews Andrews	1	j.			1,	1		1		ł			1	1	1	(24h)	NIB	sour non	• •	10-	
	95,31	14.79	00.001		26.41	73.59	0.001		100.00	33,08	16.33		00,00	BRNE	75.73	1	(Krtzz)	1901	76	Biomaty -	16-95	۵ ۳ ۳
95.18	37.62	10.04	33.06	35.33	42.49	4.60	6.01		32,81	33.55	32.45		36.60	46.34	3424	33.37	_	3	7010/10	Internited 7	17	
		•	t			١			1	1	1		1	1	1	1	(With)		Shumar	ted Tes		
. 1	83.67	16.33	100.00	1	3.74	96.26	100.00		100.00	34.35	67.65		100.00	19.54	80.16)	(****)		10+01	Test (No		,
80.1	36.72	99.5	76.4	83.5	39.4.	7,0016	99.21		0.00/	31.47	74.81		75.5.	78.36	73.8	76.5:	cmaq.	Ash	Solids	Recito	-	7