



Modeling Alloys under irradiation: *open questions*

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- Limitations of classical approaches
 - “Local” successes
 - Some suggestions



- Engineering alloys =
major components (e.g. Fe Cr Ni Mn C...)
+ *minor elements* (C N S P...)



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- Most ($\approx 90\%$) modeling of
microstructural evolution under irradiation :
book keeping of point defects and of minor elements

\Rightarrow *Defect and solute-defect clusters*
 \Rightarrow *Dislocation climb*

+ *effective medium* approx^{tion} for major components

\Rightarrow swelling, hardening, segregation of minor
elements...

Limitations of the classical approach



- Drawbacks of *effective medium* approx^{ion}
(*concentration dependant properties*):
 - ? Irradiation induced segregations
(e.g. Cr in Austenitic and ferritic steels)?
 - ? Phase separation (e.g. Nb, O in Zalloys...)?
- ? Concentration dependent p^{pties} of dislocation cores
(e.g. sink efficiency as a function of SFE,
stability of Frank loops vs unfaulting...)?
 - e.g. (Austenitic steels)
 - ⇒ Incubation dose for swelling?
 - ⇒ Early dose recovery of the dislocation network?
 - ⇒ ...

Stability criteria for alloy phases under irradiation?

Counterpart to the industrial skill with Calphad, Dictra...??



- Competition ballistic / thermally activated atomic jumps

=> Stationary rather than equilibrium state(s)

- Dienes... 50's : order disorder transitions (*stationary LRO, homogeneous*)

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=> absolute stability of stationary states (*homogeneous, binaries*)

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- Vaks et al 94 : Effective Hamiltonian $V_k^{\text{eff}} / k_B T = V_k f_k(\Gamma_b / \Gamma_{\text{th}}) / k_B T$
(*binaries, interstitial relocation*)

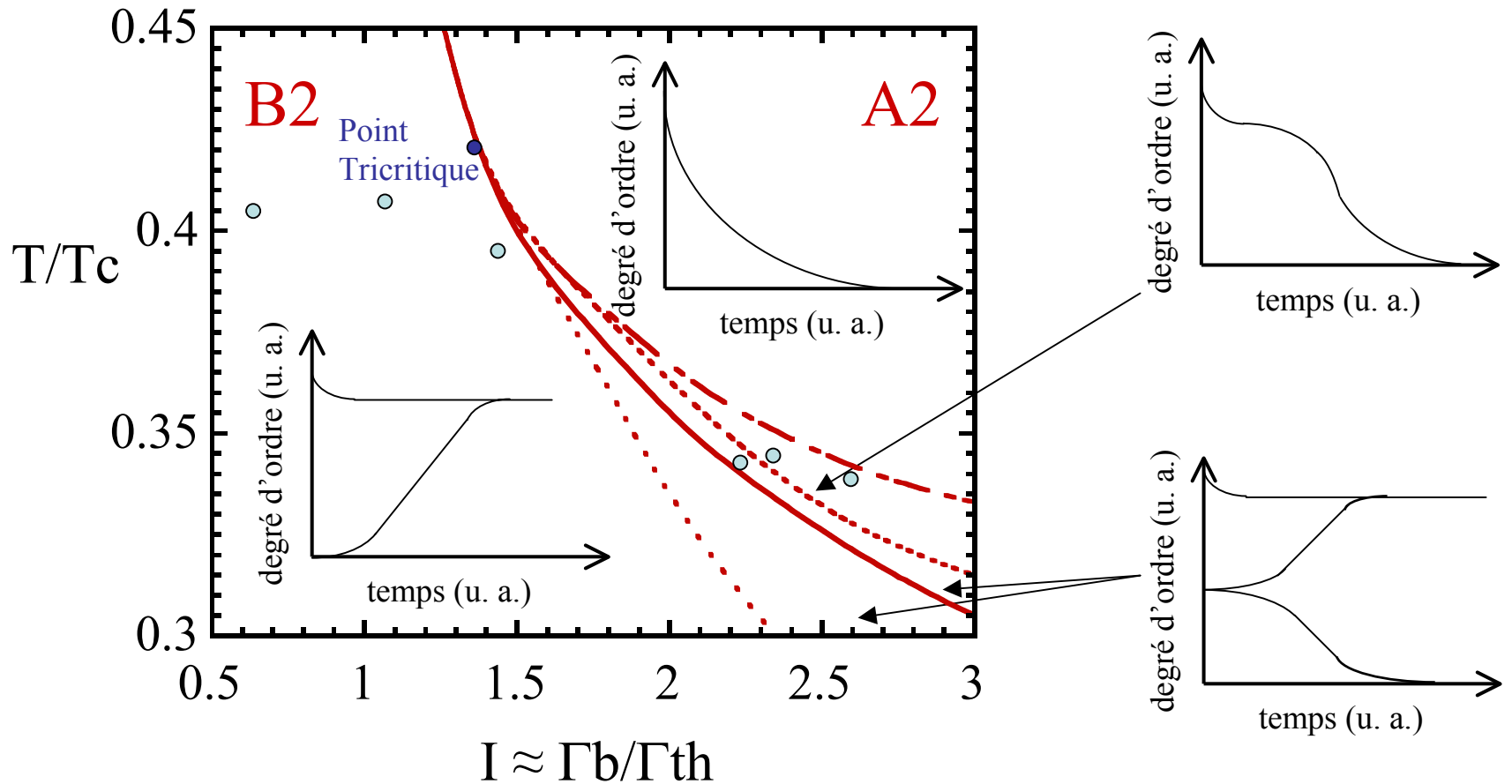
Spectacular successes (inversion of stabilities, effect of cascades size, patterning...) but **limited**.

Phase diagramme for dynamical equilibrium: FeAl under ball milling



Pochet et al. PRB52 (1995) 4006

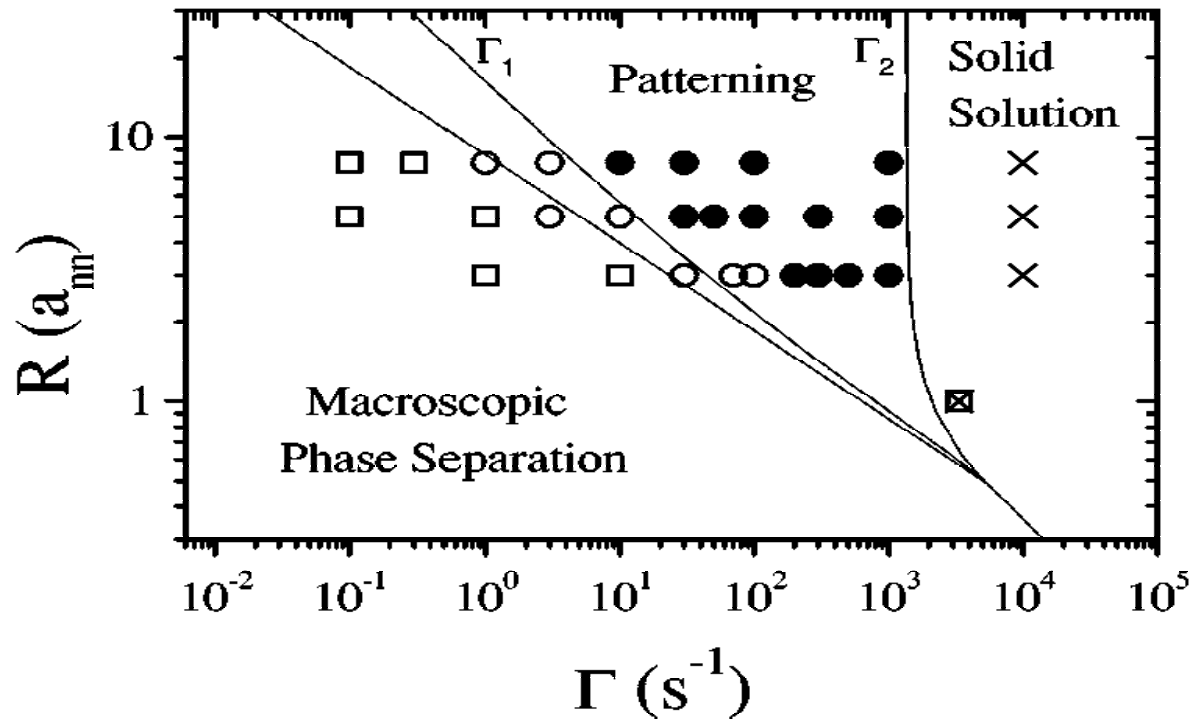
FeAl B2 \longrightarrow A2 sol. sol. (I, T)





Cascade size effects

(R : range of ballistic relocation)



Comparison between KMC simulations and a Cahn-Hilliard type model
(P. Bellon and R. Enrique, PRB 2001)



For binaries:

Inverse Kirkendal effect (RIS & RIP)

and

ballistic forcing

⇒ a single common theoretical frame

(G.M. and P. Bellon SSP **50**, 1996, 189)

Higher complexity?

For the time being: brute force atomistic modeling!

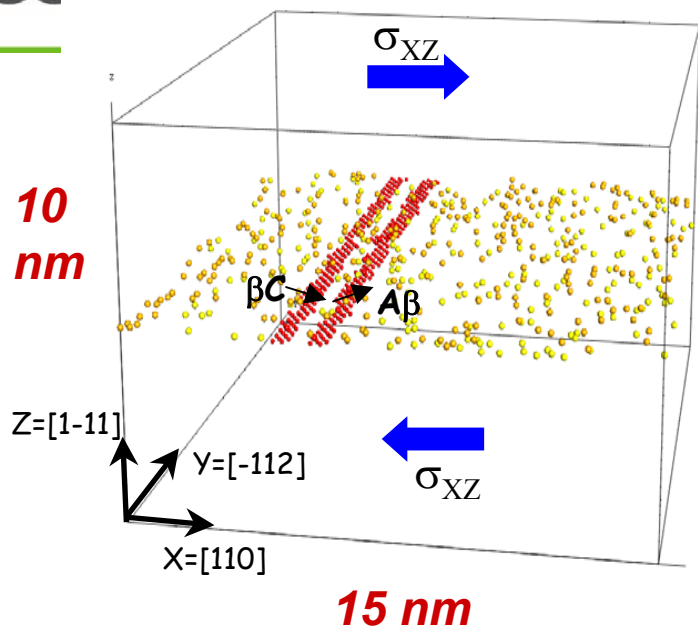
Requires:

- Safe implementation of diffusion mechanisms in KMC(vacancy and self interst^{al}) (Soisson et al.),
- Safer phase field type equations (Nastar et al.),
- Safer alloy models (for cascade simulations, for kinetics...).



- 1 Chemical hardening
 - 2 Fracture in oxides
- 3 Cascades in compounds

Plasticity of alloys: Solid Solution hardening



17.2
nm
≤43.1.

- $2.3 \cdot 10^5$ atoms ;
- $t \leq 700\text{ps}$ ($\delta t = 2 \cdot 10^{-15}$ s)

- EAM optimized for Ni(Al), Ni₃Al
- Boundary conditions :
 $X, Y \Rightarrow$ periodic;
 $Z = \pm Z_{\max} \Rightarrow Z = c^t$ 2D dynamics
 $7,5 \leq \sigma_{XZ} \leq 400\text{MPa}$
 f_{ext} on atoms at $\pm Z_{\max}$
- Temperature : 300K rescaling velocities /100 time steps

$$(N, V, T, \sigma_{\text{appl}}) = c^t$$

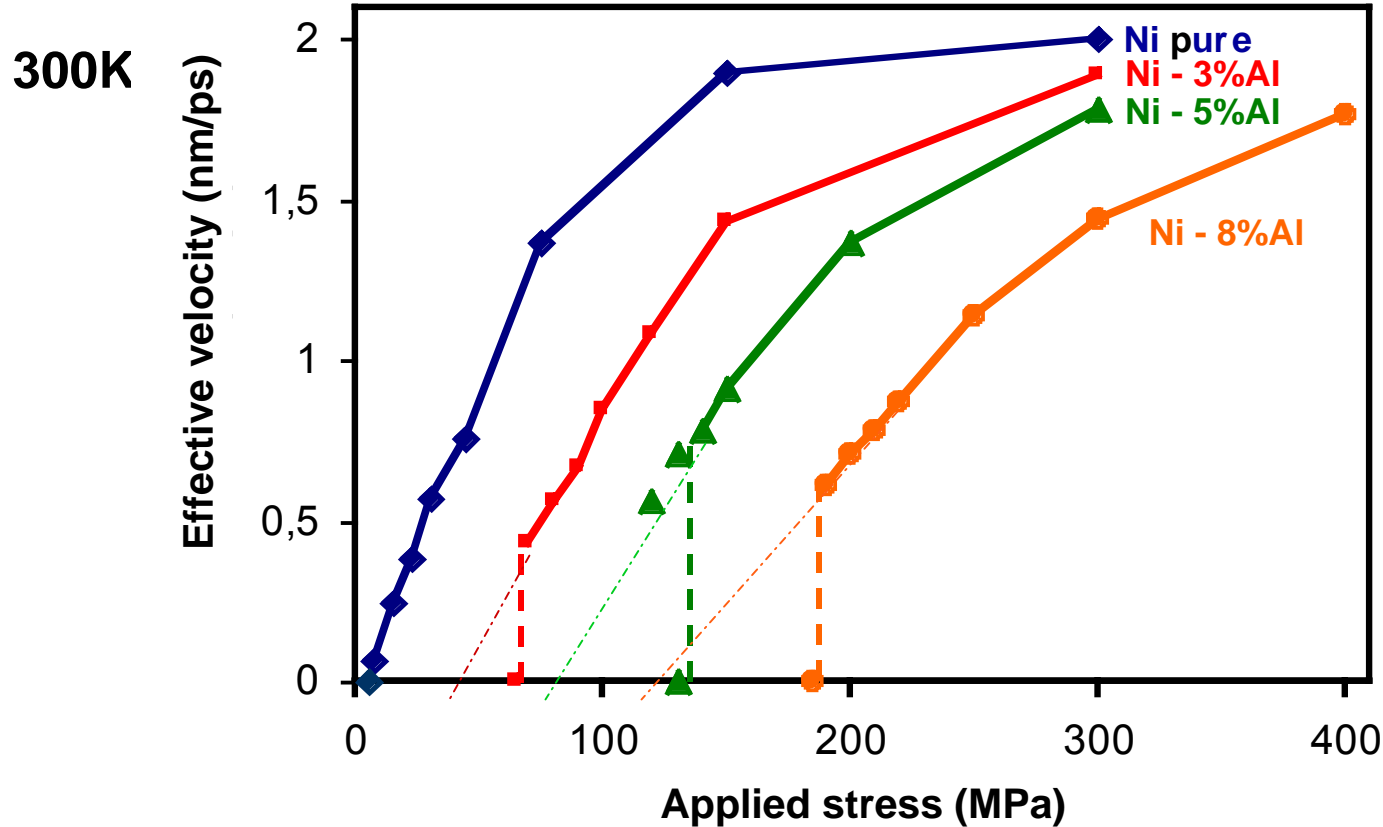
(Rodary et al. 2004)

Glide of an edge dislocation : *random* solid solution 3 at% Al, 70MPa (300K)



QuickTime™ and a Cinepak decompressor are needed to see this picture.

Effective dislocation velocity = f(applied stress)



$$\text{static } and V \quad C_{sound} \quad then V \quad \frac{b}{B(c)} \quad \text{dynamical } (c)$$

From glide velocity $v(\sigma;c) \rightarrow$ to stress strain curves $\sigma(\varepsilon)$



$$\text{static } \text{and } V \ll C_{\text{sound}} \text{ then } V = \frac{b \text{ dynamical}(c)}{B(c)}$$

Can be implemented in models of :

- DDD,

with appropriate mobility law;

- crystalline plasticity,

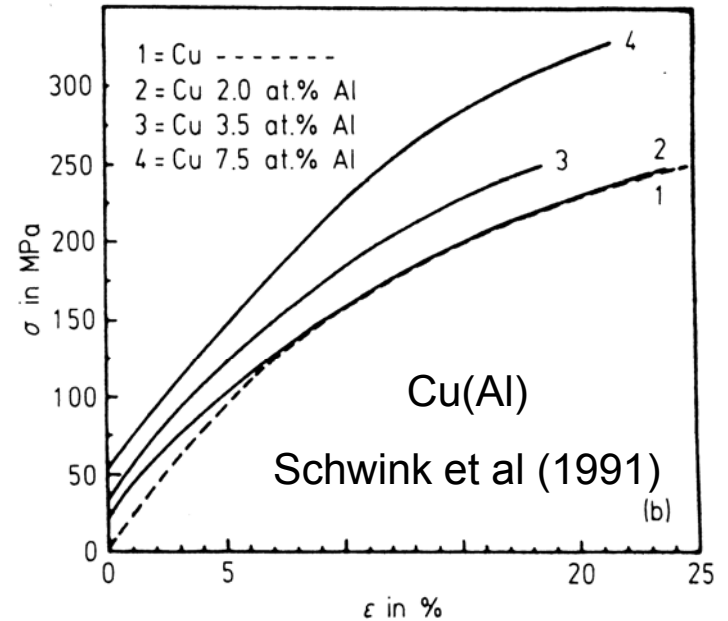
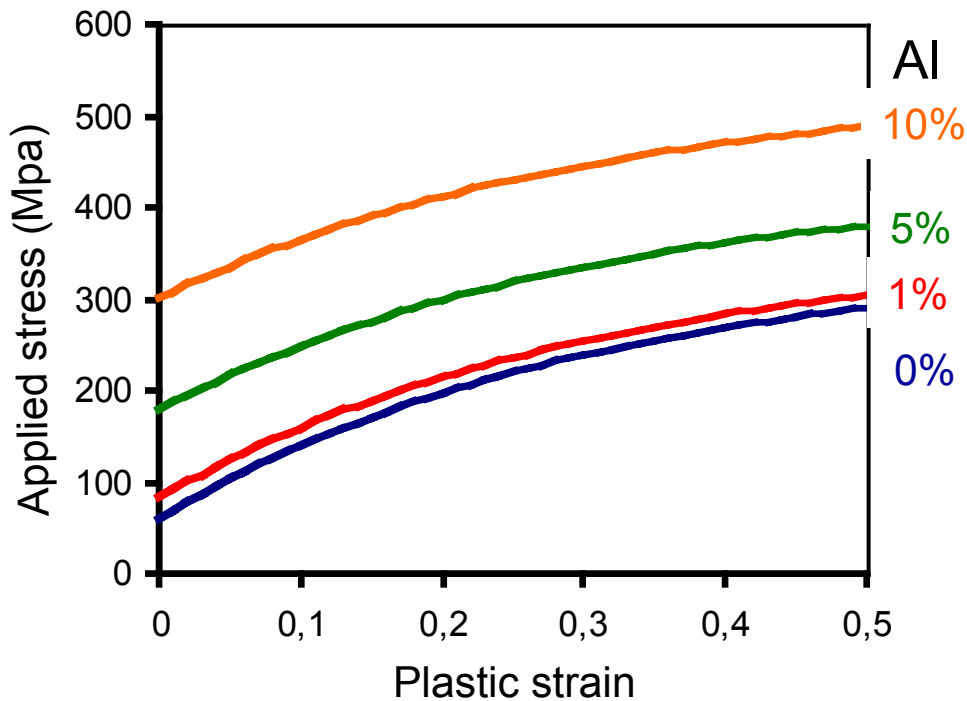
with $\sigma > \sigma_{\text{yield}}$ instead of $\sigma > \sigma_{\text{static}}$:

$$\text{yield} \quad \text{static} \quad b \sqrt{\quad}$$

From nano to macro scale?

$$\sigma_{\text{yield}} \text{ and } \nu \quad C_{\text{sound}} \text{ then } V \quad \frac{b}{B(c)} \text{ dynamical } (c)$$

$$Y_p \quad b V \quad \dot{Y} \quad \dot{Y}_p \quad A \sqrt{\quad} \quad D$$



¥ $\sigma_{\text{flow}} / c = 25$ (MPa/at%) (vs 10 exp.) ; missing strain hardening (c%) : A(c), D(c)



-1 Chemical *hardening*

results from solute-solute interaction,

(rather than from solute-dislocation interaction)

- 2 Fracture of oxides

- 3 Cascades in compounds



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Fracture of complex compounds; SiO₂ cristobalite vs glass



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Van Brutzel et al
2002

Fracture of complex compounds; SiO_2 cristobalite vs glass



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-1 Chemical hardening

- 2 Fracture in oxides:

*Fracture of SiO₂ glass proceeds by cavitation;
can be tuned by adjusting % of network modifiers.*

- 3 Cascades in compounds



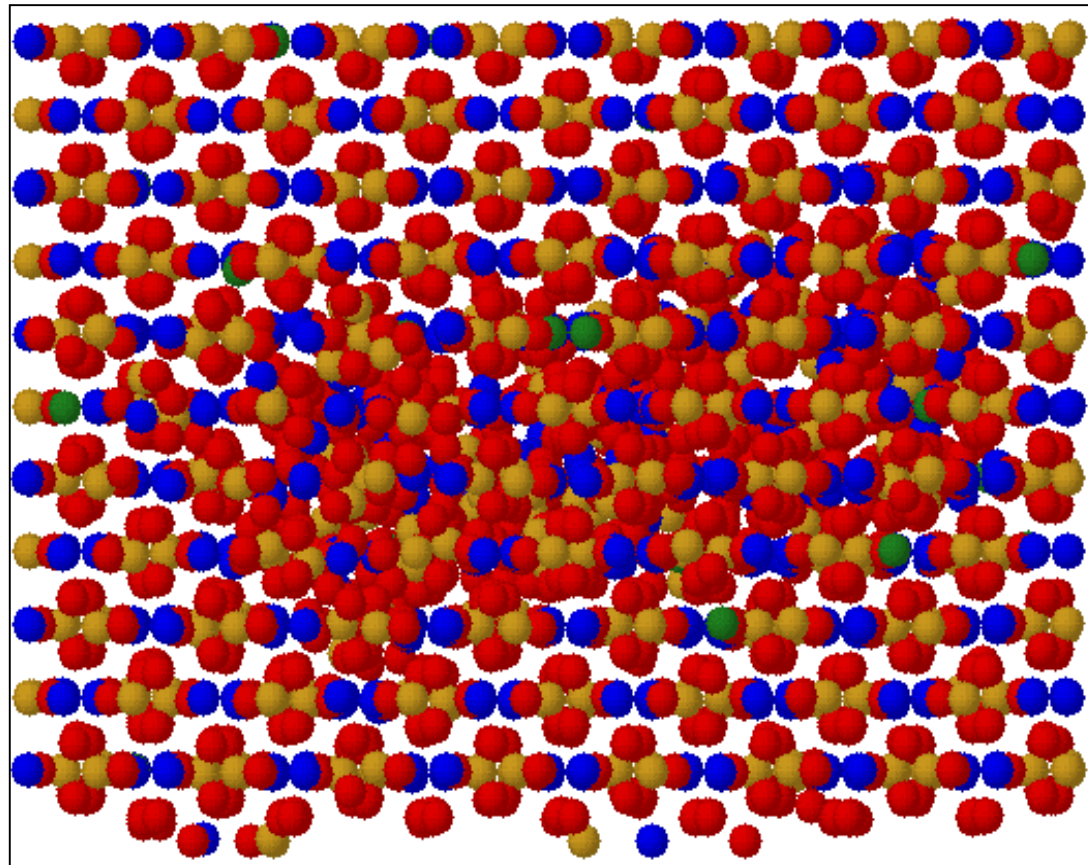
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Zircon (ZrSiO_4)

Crocombette et al. 2002

➤ Direct amorphization

Zr Si O U





- 1 Chemical hardening
- 2 Fracture in oxides:
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Systematic: the more covalent the easier to amorphize



For the time being:

Nothing as versatile as Calphad, Dictra...

*Calphad, Dictra can be taken advantage of (e.g. for RIS),
provided*

the appropriate Mobility matrix is implemented;

Need for basic developments:

theory + experimental

(wishful thinking? combining appropriate skill and support!)

Atomistic simulations +

integration in multiscale m^{dlg} schemes

~~do teach a lot + several successful “niche applications”.~~