Chemical Kinetic Data Base for Combustion Chemistry. Part 2. Methanol

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This publication contains evaluated and estimated data on the kinetics of reactions involving methanol and hydroxymethyl radicals and various small inorganic and organic species which are of importance for the proper understanding of methanol combustion and pyrolysis. It is meant to be used in conjunction with the kinetic data given in an earlier publication pertaining to methane pyrolysis and combustion, but which also contains a large volume of data that are applicable to the methanol system. The temperature range covered is 300-2500 K and the density range 1×10^{16} to 1×10^{21} molecules cm⁻³.

Key words: combustion; data base; evaluation; gas kinetics; hydroxymethyl; methanol; rate expressions.

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1. Introduction

1.1. Scope

This is the second of a series of publications presenting evaluated chemical kinetic data important for the detailed understanding of the combustion of organic compounds. Previously¹, we dealt with the reactions of the most likely species present in methane combustion. We now add two new species, CH₃OH and CH₂OH, to this list and include the 41 reactions of these two compounds with the components involved in methane combustion and the reactions with each other. With the appropriate reactions in the earlier data base we are now in a position to give a complete description of the chemistry of methanol combustion. We have selected methanol as the first addition to our data base because of the interest in its use as an alternative fuel. As a result more new kinetic data have been reported². There have also been attempts at modeling methanol decomposition systems³. Finally, because methanol is the simplest of the alcohols, many of the reactions are of use in understanding and modeling the oxidation and pyrolysis of other alcohols.

Our approach has been to be as inclusive as possible. Having decided on the important species, we consider all the

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possible reactions of these species. Where experimental information is not available we give our best estimate. The absence of a recommended number implies that for all purposes the rate constant is sufficiently small that it can be ignored. The reaction grid containing the reactions that we have evaluated in the past and the one presented in this evaluation can be found in Fig. 1. In all cases we have given recommended values that cover the temperature range of $300-2500 \, \mathrm{K}$ and the density range of $1 \times 10^{16}-1 \times 10^{21} \, \mathrm{molecules \, cm^{-3}}$.

1.2. Organization

The data are presented in the same fashion as in the earlier evaluation on methane combustion. The information contained here is meant to be used in conjunction with that in our earlier publication. A more detailed presentation of what is contained in this introduction can be found there. This discussion contains the minimal information necessary for the use of the present data.

The data are presented in three sections. The first contains a summary of the recommended rate expressions, the estimated error factors, and the page where a brief discussion can be found. The second section contains additional information on the individual reactions. It includes a summary of past work and the justification for the recommendations. The third section contains relevant thermodynamic and transport property data.

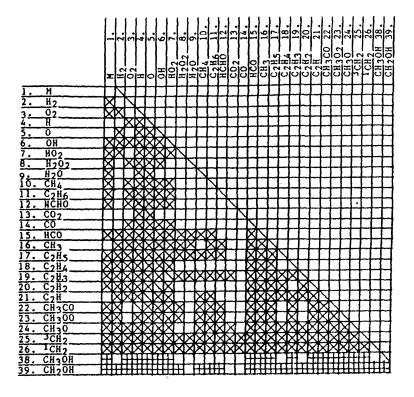


Fig. 1. Reaction grid. X: Reactions covered in Ref. 1. +: Reactions covered in present work.

1.3. Guide to Summary Table

The summary table contains all the recommended rate expressions, the uncertainty factors and the page where a more detailed discussion can be found. For unimolecular processes or their reverse combination we give results in terms of the high pressure or low pressure limit and the departure from this limit in the form of the ratio k/k_{∞} or k/k_0 (where the subscript refers to the limiting high and low pressures) for 1 atm N_2 or Ar.

1.4. Guide to Chemical Kinetic Data Tables

This section contains information on past work, our analysis of the data, rate expression recommendations, and uncertainty factors. We retain the numbering system that we use for the methane combustion system: to the twenty-five species that are labeled from 2 to 26 we now add 38 (methanol) and 39 (hydroxymethyl). The label 1 is reserved for unimolecular reactions. We are also reserving the labels 27-37 for the species of importance to NO_x formation processes. Since pairs of these numbers form a particular reaction, we now consider reactions 38 (methanol) and 39 (hydroxymethyl) with all lower numbered species and of course with themselves. These sequence numbers are at the top left hand corner of all the data tables. This is followed by a statement of the ele-

mentary reaction and, if applicable, the appropriate equilibrium constant.

In the next section is a synopsis of all previous work. It begins with a listing of the author(s) and the year of publication. In the case of a review, a note is made to this effect and in many cases this is used as a starting point for our efforts. This is followed by a synopsis of the reaction conditions, the derived rate expressions and the uncertainty limits. The latter are either given by the author or estimated by the reviewer on the basis of similar experiments. Most of the reactions are bimolecular and the units are cm³ molecule⁻¹ s⁻¹. For unimolecular and termolecular reactions the units are s⁻¹ and cm⁶ molecule⁻² s⁻¹ respectively. As an aid to the user in those cases where there are considerable experimental data we also include a plot in the Arrhenius form of the data and our recommendations.

The next section contains our recommendations and a brief discussion of our rationale. We have discussed our approach in detail in our earlier paper. Here, we simply note that we have used BEBO⁴ transition states to fit hydrogen abstraction data over the 300-2500 K temperature range of interest. This leads in general to a T^2-T^4 temperature dependence for the preexponential factor. Unimolecular reactions and related processes are pressure and species (weak colliders) dependent as well as temperature dependent. We have applied standard RRKM⁵ calculations to model the pressure and weak

collider dependence. Unfortunately, the results could not be expressed in closed form. We have therefore presented the results in the form of a rate expression for either the high pressure or low pressure (strong collision) limit and two tables from which rate constants at reaction conditions can be obtained by interpolation. The choice of the appropriate rate expression was dictated by the closeness of the reaction to these limits under combustion conditions. The first table is the result of RRKM calculations on the basis of the strong collision assumption, with the collision partner being the reactant itself, and leads to values of k/k_{∞} or $k/k_{\rm o}$ as a function of temperature and pressure. These values are essentially correction factors to the limiting high or low pressure rate constants. The second table gives the collision efficiency, $\beta(e)$ (on a per collision basis), as a function of step size down (energy removed per collision). The tabulated results are based on the relation of Troe⁶. At the present time there is controversy regarding the magnitude and temperature dependence of this quantity. We have thus cast it in this form so that users can employ their own step sizes. The values in both tables refer to the reactant itself as the collider. In order to convert these values to those for an arbitrary collider we follow the approach of Troe⁶ and derive a correction factor, B(c), which is based on the ratio of the collisional properties of reactant and collider. Multiplying this factor by the collision efficiency derived earlier leads to a total collision efficiency, $\beta(t) = \beta(e) \times \beta(c)$. $\beta(t)$ is then used to scale the reaction pressure in our table and thus obtain an effective pressure for determining the rate constant ratios.

We illustrate the situation by carrying out fall-off calculations for methanol decomposition in the case of a dilute methanol in argon mixture at 1500 K. As an aid to the user, the calculations are carried out to many more places than justified by the accuracy of the data. This should prevent any ambiguities. We begin by determining $\beta(c)$. This involves the calculation of a number of ratios. In the following, the numerator refers to the properties of the methanol-argon mixture, while the denominator refers to pure methanol itself.

- a) Ratio of reduced masses (R); for methanol and argon this number is 17.78(methanol-argon)/16(methanol-methanol)=1.111.
- b) Ratio of collision diameters (C); for a methanol argon mixture, this ratio is $[3.626(methanol) + 3.542(argon)]/[3.626(methanol) \times 2] = 0.985$.
- c) Ratio of collision integrals (W); where we use the approximation $W=1/(0.697 + 0.5185 \times \log[kT/\epsilon \text{ (argon-methanol)}])^{6.7}$ and ϵ/k (argon-methanol) =($[\epsilon \text{ (argon)/}k][\epsilon \text{(methanol)/}k])^{0.5}$ where ϵ/k is the Lennard Jones well depth. Since ϵ/k is 481.8 K for methanol and 93.3 K for argon, then the ratio of the collision integrals is 0.879/1.049=0.922.

The correction factor is then, $\beta(c) = C^2 W / R^{0.5} = 0.849$.

For the methanol-argon mixture with a 600 cm⁻¹ step size down the collision efficiency on a per collision basis at 1500 K is, $\beta(e) = 0.082$ (see 38,1). The total collision

efficiency is then $\beta(t) = \beta(c) \times \beta(e) = 0.082 \times 0.849$ = 0.07. At 20 atmospheres or 10^{20} molecules/cm³ this is equivalent to a density of 7×10^{18} molecules cm⁻³. From Table A of 38,1 we then find $k/k_{\infty} = 0.38$.

Systems for which the low pressure rate expression is given require the same procedure except that the final bimolecular rate constant is now given by the expression $\beta(t) \times k_o \times (k/k_o)$. For chemical activation processes the rate expressions can be obtained in an analogous manner. In addition to the possible pressure dependence of the total rate, the ratio of decomposition to stabilization is also of importance. Thus, in these cases we include a table giving this ratio as a function of temperature and pressure on the assumption of strong collisions. Note that the procedure for correction for weak collision effects in the chemical activation systems is an untested approximation. Fortunately, for the systems considered here, pressure effects are relatively unimportant.

In the course of carrying out the earlier evaluation¹, we found that the data for unimolecular fall-off can generally be fitted, in the context of weak collisions, by step sizes of $50-100 \text{ cm}^{-1}$ near room temperature and $500-800 \text{ cm}^{-1}$ under higher temperature combustion conditions (>900 K). This was also borne out in the present study for methanol decomposition with argon as the weak collider. For strong colliders the situation is less clear, but the earlier existing data¹ suggest step sizes down in the $1000-2000 \text{ cm}^{-1}$ range. As an additional aid to the user and to eliminate the need to interpolate in the tables for some cases, we also include recommendations for k/k_{∞} or k/k_{0} values at 0.1, 1.0 and 10 atmospheres for N₂ or Ar and the reactant itself (model for strong collider) in the higher temperature region.

Finally, for each reaction we give the references used in the evaluation, the evaluator and the date. Hopefully, all the literature on this reaction previous to this date has been accessed. The author will be grateful to readers who will bring to his attention publications that have been inadvertently omitted.

1.5. Guide to Thermodynamic and Transport Tables

This section contains thermodynamic and transport properties of methanol and the hydroxymethyl radical. For the thermodynamic properties, the temperature range covered is from 300-1500 K. The properties tabulated include heat capacity, entropy, enthalpy of formation and Gibbs free energy of formation. In addition, we give a polynomial fit of the logarithm of the equilibrium constant of formation. The sources for this data can be found in a footnote. The transport properties are of use for evaluation of fall-off behavior. We therefore include the collision cross-section and the Lennard-Jones well depth.

1.6. Acknowledgments

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1.7. References to the Introduction

¹W. Tsang and R. F. Hampson, J. Phys. Chem. Ref. Data 15, 1087 (1986). ²See references in Data Tables.

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- ⁷R. C. Reid, J. M. Prausnitz, and T. K. Sherwood, *The Properties of Gases and Liquids*, 3rd ed. (McGraw-Hill, New York, 1977).

2. Index of Reactions and Summary of Recommended Rate Expressions

No.	Reaction	Rate Constant k/cm ³ molecule ⁻¹ s ⁻¹	Uncertainty factor	Page
38,1	сн ₃ он → сн ₃ + он	$k^{\infty}=1.9 \times 10^{16} \exp(-46192/T) \text{s}^{-1}$ $k/k^{\infty}=0.312-6.20 \times 10^{-4} \text{T}-2.56 \times 10^{-7} \text{T}^{2}$ (1 atm, N ₂ , >900K)	2	478
38,3	$CH_3OH + O_2 \rightarrow CH_2OH + HO_2$	3.4x10 ⁻¹¹ exp(-22600/T)	10	481
38,4	$CH_3OH + H \rightarrow CH_2OH + H_2$ (a) $\rightarrow CH_3O + H_2$ (b)	$k_{a+b}=3.52 \times 10^{-17} T^{2.1} \exp(-2450/T)$	1.5 to 600K, 3 at 2000K	481
38,5	$CH_3OH + O \rightarrow CH_2OH + OH (a)$ $\rightarrow CH_3O + OH (b)$	$k_a/k_b=4$ $k_{a+b}=6.44 \times 10^{-19} T^{2.5} \exp(-1550/T)$	1.3 to 750K, 2 at 1100K	483
38,6	СН ₃ ОН + ОН → СН ₂ ОН + Н ₂ О (a)	$k_a > k_b$ $k_{a+b} = 1.1 \times 10^{-19} T^{2.5} \exp(483/T)$	1.1 at 300K, 3 at 2000K	485
	\rightarrow CH ₃ O + H ₂ O (b)	k _a /k _b =3.7exp(-1020/T)	1.6 to 500K	
38,7	сн ₃ он + но ₂ → сн ₂ он + н ₂ о ₂	1.6x10 ⁻¹³ exp(-6330/T)	10	487
38,15	сн ₃ он + нсо → сн ₂ он + н ₂ со	$1.6 \times 10^{-20} T^{2.9} \exp(-6596/T)$	10	487
38,16	$CH_3OH + CH_3 \rightarrow CH_2OH + CH_4$ (a) $\rightarrow CH_3O + CH_4$ (b)	$k_a = 5.3 \times 10^{-23} T^3 \cdot {}^{2} exp(-3609/T)$ $k_b = 2.4 \times 10^{-23} T^3 \cdot {}^{1} exp(-3490/T)$	1.4 to 600K, 3 at 2000K	488
38,17	$CH_3OH + C_2H_5 \rightarrow CH_2OH + C_2H_6$ (a) $\rightarrow CH_3O + C_2H_6$ (b)	$k_a = 5.3 \times 10^{-23} T^{3.2} exp(-4610/T)$ $k_b = 2.4 \times 10^{-23} T^{3.1} exp(-4500/T)$	3 3	489
38,19	$CH_3OH + C_2H_3 \rightarrow CH_2OH + C_2H_4$ (a) $\rightarrow CH_3O + C_2H_4$ (b)	$k_a = 5.3 \times 10^{-23} T^{3.2} exp(-3609/T)$ $k_b = 2.4 \times 10^{-23} T^{3.1} exp(-3490/T)$	10 10	489
38,21	$CH_3OH + C_2H \rightarrow CH_2OH + C_2H_2$ (a) $\rightarrow CH_3O + C_2H_2$ (b)	$k_a = 1 \times 10^{-11}$ $k_b = 2 \times 10^{-12}$	5 5	490
38,22	CH ₃ OH + CH ₃ CO → CH ₂ OH + CH ₃ CHO	8.06x10 ⁻²¹ T ³ exp(-6210/T)	3	490
38,23	CH ₃ OH + CH ₃ OO → CH ₂ OH + CH ₃ OOH	3x10 ⁻¹³ exp(-6900/T)	1.3 at 600K, increasing to 2 at 1000K	491
38,24	CH ₃ OH + CH ₃ O → CH ₂ OH + CH ₃ OH	5x10 ⁻¹³ exp(-2050/T)	10	491
38,25	СН ₃ ОН + ¹ СН ₂ → СН ₃ + СН ₂ ОН	2.5x10 ⁻¹²	3	492

2. Index of Reactions and Summary of Recommended Rate Expressions -- Continued

No.	Reaction	Rate Constant k/cm ³ molecule ⁻¹ s ⁻¹	Uncertainty factor	Page
20.26	$CH_3OH + {}^3CH_2 \rightarrow CH_2OH + CH_3$ (a)	k _a =5.3x10 ⁻²³ T ^{3.2} exp(-3609/T)	3	403
30,20	$\rightarrow CH_3O + CH_3 (b)$	$k_a = 3.4 \times 10^{-23} T^{3.1} exp(-3490/T)$	3	493
39,1	CH ₂ OH + M → H + HCHO + M	$k_0 = 75T^{-2.5} \exp(-17205/T)$	4	494
,-		k(N ₂ , >900K)=1.9x10 ¹⁹ T ⁻⁸ exp(-21645/T (strong collider)		
39,2	сн ₂ он + н ₂ → сн ₃ он + н	1.12x10 ⁻¹⁸ T ^{2.0} exp(-6722/T)	4	495
39,3	сн ₂ он + о ₂ → нсно + но ₂	2.0x10 ⁻¹²	2	495
39,4	CH ₂ OH + H → HCHO + H ₂ (a)	k _a =1x10 ⁻¹¹	2	496
	→ CH ₃ + OH (b)	$k_b = 1.6 \times 10^{-10}$	2	
39,5	СН2ОН + О → НСНО + ОН	7x10 ⁻¹¹	2	497
39,6	СН ₂ ОН + ОН → НСНО + Н ₂ О	4x10 ⁻¹¹	2	497
39,7	СН ₂ ОН + НО ₂ → НСНО + Н ₂ О ₂	2x10 ⁻¹¹	2	498
39,8	сн ₂ он + н ₂ о ₂ → сн ₃ он + но ₂	5x10 ⁻¹⁵ exp(-1300/T)	10	498
39,10	сн ₂ он + сн ₄ → сн ₃ он + сн ₃	3.6x10 ⁻²³ T ^{3.1} exp(-8166/T)	3 .	498
39,11	$CH_2OH + C_2H_6 \rightarrow CH_3OH + C_2H_5$	3.3x10 ⁻²² T ³ exp(-7033/T)	5	499
39,12	сн ₂ он + нсно → сн ₃ он + нсо	9.1x10 ⁻²¹ T ^{2.8} exp(-2950/T)	3	499
39,15	CH ₂ OH + HCO → CH ₃ OH + CO (a)	$k_a = 2x10^{-10}$	3	500
	→ 2HCHO (b)	$k_b = 3 \times 10^{-10}$	3	
39,16	$CH_2OH + CH_3 \rightarrow CH_3CH_2OH (a)$	$k_a^{\infty}=2x10^{-11}$ $log(k_a/k_a^{\infty})=0.202+1.755x10^{-4}T-$ $5.61x10^{-7}T^2$ (1 atm N ₂ , >900K)	2	500
	→ CH ₄ + HCHO (b)	$k_b = 4 \times 10^{-12}$	5	
39,17	$CH_2OH + C_2H_5 \rightarrow n-C_3H_7OH$ (a)	k _a =2x10 ⁻¹¹	2	502
	\rightarrow c_2H_6 + HCHO (b)	$k_b = 4 \times 10^{-12}$	5	
	→ C ₂ H ₄ + CH ₃ OH (c)	$k_c = 4 \times 10^{-12}$	5	
39,18	$CH_2OH + C_2H_4 \rightarrow (CH_2)_3OH (a)$	k _a =8x10 ⁻¹⁴ exp(-3500/T) (reversed under combustion conditions)		- 502
	→ C ₂ H ₅ + HCHO (b)	k _b =k _a x(exp(-2000/T)/(1+exp(-2000/T))) 5	

2. Index of Reactions and Summary of Recommended Rate Expressions -- Continued

No.	Reaction	Rate Constant k/cm ³ molecule ⁻¹ s ⁻¹	Uncertainty factor	Page
39,19	$CH_2OH + C_2H_3 \rightarrow C_2H_4 + HCHO (a)$	$k_a = 5 \times 10^{-11}$	2.5	503
	$\rightarrow c_3H_5 + OH (b)$	$k_b = 2x10^{-11}$	2	
39,20	$CH_2OH + C_2H_2 + C_3H_4OH$	1.2x10 ⁻¹² exp(-4531/T)	3	503
39,21	$CH_2OH + C_2H \rightarrow C_2H_2 + HCHO (a)$	$k_a = 6x10^{-11}$	5	504
	$\rightarrow C_3H_3 + OH (b)$	$k_b = 2x10^{-11}$	3	
39,22	сн ₂ он + сн ₃ со → сн ₃ сосн ₂ он	2x10 ⁻¹¹	2	504
39,23	сн ₂ он + сн ₃ оо → сн ₃ о + он + нсно	2x10 ⁻¹¹	3	504
39,24	сн ₂ он + сн ₃ о → сн ₃ он + нсно	4x10 ⁻¹¹	2	505
39,25	$CH_2OH + {}^{1}CH_2 \rightarrow CH_3CHO + H$	3x10 ⁻¹¹	2	505
39,26	$CH_2OH + {}^3CH_2 \rightarrow C_2H_4 + OH (a)$	$k_a = 4x10^{-11}$	3	505
	→ CH ₃ + HCHO (b)	$k_b = 2x10^{-12}$	3	
39,38	сн ₂ он + сн ₃ он + сн ₃ он + сн ₃ о	1.3x10 ⁻¹⁴ exp(-6070/T)	10	506
39,39	CH ₂ OH + CH ₂ OH → HOCH ₂ CH ₂ OH (a)	k _a =1.6x10 ⁻¹¹	2	506
	→ CH ₃ OH + HCHO (b)		2	

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3. Chemical Kinetic Data Tables

38,1 CH₃OH → CH₃ + OH

	Cond	ditions	Reaction rate constant, Ur	certainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor
$\log K_p = 8.04602 - 200$	660.1/T + 67	509.5/T ²		
Cribb, et al. (1984)	1800-2660	1-1.3x10 18 Ar and N ₂ . (Shock tube, laser schlie-	k=8.5x10 ¹⁸ T ^{-7.08} exp(-45317/T)	2
Spindler, Wagner (1982)	1600-2100	ren and mass spec.) 8.0-200.0x10 ¹⁷ Ar. (Shock tube,	$k^{\infty} \simeq 9.4 \times 10^{15} \exp(-45250/T) s^{-1}$	
Tsuboi, et al.	1500-1900	CH ₃ , OH detection) 6.0x10 ¹⁸ Ar.	$k_o(Ar) = 3.3x10^{-7} exp(-34420/T)$ 6.0x10 ¹² exp(-37310/T)s ⁻¹	3
(1981)		3.0x10 ¹⁹ Ar. 6.0x10 ¹⁹ Ar. 0.01 - 1% CH ₂ OH.	3.6x10 ¹³ exp(-37788/T)s ⁻¹ 8.7x10 ¹³ exp(-38270/T)s ⁻¹	3
		(Shock tube, UV absorption and IR emission)		
Westbrook, Dryer (1979)	1000-2200	3.7x10 ¹⁸ N ₂ (Modeling flow reactor, and shock tube results)	5.0x10 ⁻⁶ exp(-40280/T)	
Bowman (1975)	1500-2200	6.0-17.0x10 ¹⁸ Ar, 0.75 to 4% CH ₃ OH. (Shock tube, optical detection of OH, O, H ₂ O)	6.7x10 ⁻⁹ exp(-34200/T)	3
Recommended value	>900	1 atm, N ₂	$k = 1.9 \times 10^{16} \exp(-46192/T) s^{-1}$ $\log k/k = 0.312 - 6.20 \times 10^{-4} T - 2.56 \times 10^{-7} T^2$	2

Comments and Recommendations

The experimental results under almost identical experimental conditions vary by a factor of 30. The results of Westbrook and Dryer and of Spindler and Wagner are in agreement suggesting that the collision efficiencies for N_Z and Argon are similar. The rate constants of Bowman are a factor of 10 lower than those of Spindler and Wagner, while those of Tsuboi are a factor of 3 higher. The results of Cribb et al. occupy an intermediate position between the latter two results. We have fitted the data on the basis of the work of Spindler and Wagner, Cribb et al., Tsuboi, and Westbrook and Dryer, and the measured rate for the reverse process at room temperature (See Rn. 16,6 in Part 1). This leads to a step size down for argon of 500 cm⁻¹ and a high pressure rate expression of $k(CH_3OH \rightarrow CH_3 + OH) = 1.9 \times 10^{16} \exp(-46192/T) s^{-1}$

The results of Bowman lead to a step size down of 160 cm^{-1} and is incompatible with the other measurements. Fall-off behavior on a strong collision basis can be found in Table A. Collision efficiencies as a function of temperature and step size down can be found in Table B. Fall-off behavior at 0.1, 1.0 and 10 atm in argon and CH_3OH over the range of 900-2500 K is as follows:

 $\label{eq:log_k(A, 0.1)/k} \log(k(A, 0.1)/k) = 0.574 - 1.64x10^{-3}T - 3.54x10^{-8}T^2$ $\log(k(A, 1.0)/k) = 0.312 - 6.20x10^{-4}T - 2.56x10^{-7}T^2$ $\log(k(A, 10)/k) = 4.39x10^{-2} + 1.13x10^{-4}T - 3.66x10^{-7}T^2$ $\log(k(CH_3OH, 0.1)/k) = 0.452 - 1.20x10^{-3}T - 1.12x10^{-7}T^2$ $\log(k(CH_3OH, 1.0)/k) = 0.193 - 3.00x10^{-4}T - 2.88x10^{-7}T^2$ $\log(k(CH_3OH, 10)/k) = -2.40x10^{-2} + 2.39x10^{-4}T - 3.35x10^{-7}T^2$ where we have assumed a step size down of 500 cm⁻¹ and 1000 cm⁻¹ respectively. The uncertainty in the rate constant is a factor of 2.

Table A. $log(k/k^{\varpi})$ as a function of concentration and temperature for CH_3OH decomposition assuming strong collisions

log[M]	log[M] T/K											
	300	500	700	900	1100	1300	1500	1700	1900	2100	2300	2500
16.0	-0.54	-0.94	-1.3	-1.62	-1.90	-2.12	-2.37	-2.6	-2.81	-3.02	-3.21	-3.39
16.5	-0.32	-0.64	-0.95	-1.24	-1.50	-1.70	-1.94	-2.16	-2.36	-2.56	-2.75	-2.92
17.0	-0.17	-0.40	-0.66	-0.9	-1.13	-1.22	-1.54	-1.75	-1.94	-2.12	-2.31	-2.47
17.5	-0.08	-0.23	-0.42	-0.62	-0.82	-0.98	-1.18	-1.36	-1.54	-1.72	-1.89	-2.04
18.0	-0.03	-0.12	-0.25	-0.39	-0.55	-0.69	-0.86	-1.02	-1.18	-1.34	-1.50	-1.64
18.5	-0.01	-0.05	-0.13	-0.22	-0.33	-0.45	-0.59	-0.72	-0.87	-1.01	-1.14	-1.27
19.0		-0.02	-0.06	-0.11	-0.18	-0.27	-0.37	-0.48	-0.60	-0.72	-0.83	-0.94
19.5		-0.01	-0.02	-0.05	-0.09	-0.15	-0.22	-0.30	-0.38	-0.47	-0.57	-0.66
20.0			-0.01	-0.02	-0.04	-0.07	-0.11	-0.16	-0.22	-0.28	-0.35	-0.42
20.5				-0.01	-0.01	-0.03	-0.05	-0.08	-0.11	-0.15	-0.20	0.24
21.0						-0.01	-0.02	-0.03	-0.05	-0.07	-0.10	-0.12

Table B. Collision efficiency, $\beta_{\rm C},$ as a function of temperature and step size down for CH3OH decomposition

T/K		Step	o-size (cm ⁻¹)		
	150	300	600	1200	2400
300	0.15	0.32	0.52	0.70	0.83
500	0.08	0.17	0.36	0.57	0.74
700	0.043	0.12	0.26	0.46	0.65
900	0.027	0.079	0.19	0.37	0.58
1100	0.018	0.055	0.15	0.30	0.51
1300	0.012	0.038	0.11	0.24	0.43
1500	0.008	0.028	0.082	0.20	0.38
1700	0.006	0.021	0.064	0.16	0.33
1900	0.0045	0.016	0.050	0.13	0.27
2100	0.0034	0.012	0.039	0.11	0.25
2300	0.0026	0.009	0.031	0.09	0.21
2500	0.002	0.007	0.025	0.074	0.18

Arrhenius plots of the rate constants k_r for OH + CH $_3$ combination (in Argon), the reverse of Rn. 38,1, are given in Fig. 2. The values of k_r were obtained from $k_{38,1}$ and the equilibrium constants of Rn. 38,1. The numbers on the curves are the logarithms of the gas concentration in molec/cm 3 .

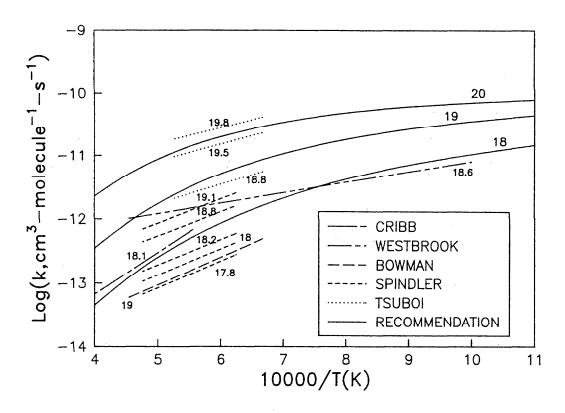


Fig. 2. Arrhenius plots of the rate constants $k_{\rm r}$ for OH + CH $_3$ combination, the reverse of Rn. 38,1.

(W. Tsang, April 1985)

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38,3 $CH_3OH + O_2 \rightarrow CH_2OH + HO_2$

Conditions			Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor
Recommended value			$3.4x10^{-11}exp(-22600/T)$	10

There are no data. We recommend the rate expression 3.4x10⁻¹¹exp(-22600/T), with an uncertainty of a factor of 10, based on Walker's estimates for the rate of O₂ attack on hydrocarbons [R.W. Walker, "A Critical Survey of Rate Constants for Reactions in Gas-phase Hydrocarbon Oxidation", in 'Reaction Kinetics', ed. P.G. Ashmore (Specialist Periodical Report), The Chemical Society, London, 1975, Vol. 1, p. 161]

(W. Tsang, April 1985)

38,4 $CH_3OH + H \rightarrow H_2 + CH_2OH$ (a) $\rightarrow H_2 + CH_3O$ (b)

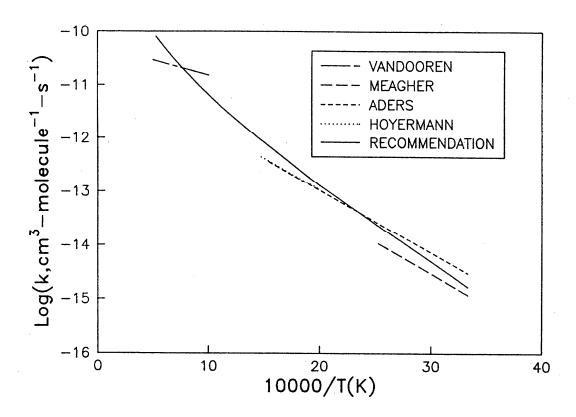
Conc	litions	Reaction rate constant,	Uncertainty	
Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}s^{-1}$	factor	
500-680	0.25-1.0x10 ¹⁷ He	$k_{a+b} = 2.2x10^{-11} exp(-2650/T)$) 1.6	
1000-2000		k = 5 6 × 10 - 11 ov × (-1200 / T) 3	
1000 2000	(Methanol flame,	a+b - 3.0x10 exp(-1309/1	, 3	
	MS-detection)			
298-650		$k_{a+b} = 2.2x10^{-11} exp(-2669/T)$) 2	
	· · · · · · · · · · · · · · · · · · ·	44		
300-404	1.5x10 ¹⁶	$k_{a+b} = 1.1x10^{-11} exp(-2739/T)$) 3	
	(Discharge flow, ESR, MS)			
500-2000		$k_{a+b}=3.52x10^{-17}T^{2.11}x$	1.5 to 600K,	
		exp(-2450/T)	3 at 2000K.	
		$k_a/k_b=4$	3	
	Temp./K 500-680 1000-2000 298-650 300-404	500-680 0.25-1.0x10 ¹⁷ He (Discharge flow - MS) 1000-2000 2-4x10 ¹⁷ (Methanol flame, MS-detection) 298-650 ~ 2.0x10 ¹⁷ (Discharge flow, ESR, MS) 300-404 1.5x10 ¹⁶ (Discharge flow, ESR, MS)	Temp./K [M]/molecule cm ⁻³ k/cm^3 molecule ⁻¹ s ⁻¹ 500-680 0.25-1.0x10 ¹⁷ He $k_{a+b} = 2.2x10^{-11}$ exp(-2650/T (Discharge flow - MS) 1000-2000 2-4x10 ¹⁷ $k_{a+b} = 5.6x10^{-11}$ exp(-1309/T (Methanol flame, MS-detection) 298-650 $\sim 2.0x10^{17}$ $k_{a+b} = 2.2x10^{-11}$ exp(-2669/T (Discharge flow, ESR, MS) 300-404 1.5x10 ¹⁶ $k_{a+b} = 1.1x10^{-11}$ exp(-2739/T (Discharge flow, ESR, MS)	

Comments and Recommendations

Under most combustion conditions it is immaterial whether the reaction goes by path (a) or (b) since the newly formed radicals should decompose to HCHO and H quite rapidly. Reaction (a) is the most exothermic channel. We have fitted all the results on the basis of BEBO transition state calculations, leading to the recommended rate expression listed above. Uncertainty factor in \mathbf{k}_{a+b} is 1.5 up

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to 600 K and 3 at 2000 K. Arrhenius plots of k_{a+b} are given in Fig. 3. From the data on methyl attack on methanol we estimate $k_a/k_b\sim 4$ with an uncertainty factor of 3.



 $\label{eq:Fig. 3. Arrhenius plots of the rate constants k_{a+b}.}$ (W. Tsang, April 1985)

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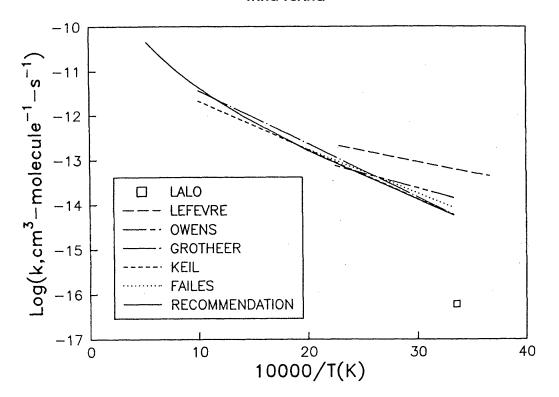
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38,5 $CH_3OH + O \rightarrow OH + CH_2OH$ (a) $\rightarrow OH + CH_3O$ (b)

	Con	ditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Failes, et al. (1982)	297-544	10 ¹⁸ N ₂ O, CH ₃ OH, NO,	k _{a+b} =1.63x10 ⁻¹¹ exp(-2267/T)	1.2	
Keil, et al. (1981)	298-998	(Hg-photosensitized decomp. of N_2O) 3.0-10.0x10 ¹⁶ O_2 , CH_3OH (Discharge flow) 1.0-3.0x10 ¹⁸ Ar, O_2 , CH_3OH	$k_{a+b}=2.7x10^{-11}exp(-2532/T)$	1.1	
Grotheer, Just (1981)	300-1006	(Flash photolysis) 3x10 ¹⁶ CH ₃ OH, O ₂ (Flow reactor,	$k_{a+b} = 5.7x10^{-11} \exp(-2750/T)$	1.3	
Lalo, Vermeil (1981)	298	MS-detection of O atoms) 3.0x10 ¹⁷ Ar	$k_{a+b} = 6.0 \times 10^{-17}$	1.2	
Owens, Roscoe (1975)	301-451	(Flow reactor, Resonance fluorescence detection of O) 3.0x10 ¹⁶ CH ₃ OH, O ₂ (Flow reactor, O-atoms from O+NO emission)	k _{a+b} =2.4x10 ⁻¹² exp(-1540/T)	1.3	
LeFevre, et al. (1972)	273-438	5.0x10 ¹⁶ Ar (Discharge flow, ESR, MS)	$k_{a+b}=2.8x10^{-12}exp(-1140/T)$	2	
Recommended value			$k_{a+b} = 6.44 \times 10^{-19} T^{2.5} x$ exp(-1550/T)	1.3 to 750K, 2 at 1100K	

Three of the most recent measurements on the rate of this reaction are in excellent agreement. We have carried out BEBO calculations and adjusted the activation energy to fit the experimental data in the 300-750 K range. The resulting expression is $k_{a+b} = 6.44 \times 10^{-19} T^{2.5} \exp(-1550/T) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ with an uncertainty factor of 1.3 in the 300-750 K range and increasing to a factor of 2 at 1100 K. Reaction (a) is the exothermic channel and there are three available hydrogens. It is probably the preferred route under most conditions. Arrhenius plots of k_{a+b} are given in Fig.4.



 $\label{eq:Fig. 4. Arrhenius plots of the rate constants k_{a+b}.}$ (W. Tsang, April 1985)

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Owens, C. M., and Roscoe, J. M., "The Reactions of Atomic Oxygen with Methanol and Ethanol," Can. J. Chem. <u>54</u>, 984 (1976)

38,6 $CH_3OH + OH \rightarrow CH_2OH + H_2O$ (a) $\rightarrow CH_3O + H_2O$ (b)

	Con	ditions	Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor
Meier, et al. (1984,1985)	300-1000	0.5-5x10 ¹⁸ He, trace methanol. (Laser induced fluores- cence, mass. spec.)	k _{a+b} =1.1x10 ⁻¹¹ exp(-718/T)	1.1
Hagele, et al. (1983)	295-420	3.0×10^{17} He, trace of $\mathrm{CH_3OH}$, $\mathrm{HNO_3}$.	$k_a/k_{a+b} = 0.21 \pm 0.1$ $k_{a+b} = 1.2 \times 10^{-11} \exp(-810/T)$ $k_b/k_{a+b} = 0.11 \pm 0.03$ (298K)	1.1
Vandooren,	1100-2000	(OH from HNO ₃ , LPRF) 2.5x10 ¹⁷	$k_b/k_{a+b} = 0.22\pm0.07 (393K)$ $k_{a+b} = 8.0\times10^{-11} \exp(-2266/T)$	3
Van Tiggelen (1981) Ravishankara, Davis (1978)	298	(methanol flame) 1.2x10 ¹⁸ He (Flash photolysis, re-	$k_{a+b} = 1.0 \times 10^{-12}$	1.1
Overend, Paraskevopoulos (1978)	296	sonance fluorescence) 1.6×10^{18} , H_2 , 10% N_2 O; also OH from H_2 O in He (Flash photolysis, Re-	$k_{a+b} = 1.06 \times 10^{-12}$	1.1
Campbell, et al. (1976)	292	sonance absorption) 3.0x10 ¹⁸ , ~ 1% NO ₂ , 0.1% H ₂ O ₂ in CO	$k_{a+b} = 0.95 \times 10^{-12}$	1.1
Osif, et al. (1975)	298	(Static) (8.0-60.0)x10 ¹⁷ , CH ₃ OH, N ₂ O, CO	$k_{a+b} = 9.6x10^{-14}$	1.2
	345	11.30., 11.20, 100	$k_{a+b} = 1.6 \times 10^{-13}$	
Recommended value			4.5	1.1 at 300K
Recommended value			exp(483/T) k _a /k _b =3.7exp(-1020/T)	3 at 2000K.

The room temperature values for this reaction are very well established from direct determinations. Using BEBO calculations, we recommend the rate expression: $k_{a+b} = 1.1 \times 10^{-19} T^2.53 \exp(-483/T) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$

with an uncertainty factor of 1.1 at room temperature and of 2 at 2000 K. Note that this expression goes smoothly through the high temperature results. The Arrhenius plots of k_{a+b} are given in Fig. 5. The work of Hagele et al. leads to $k_b/k_a = 3.7 \exp(-1020/T)$. The results of Meier et al. suggest that the branching ratio is subject to considerable uncertainty.

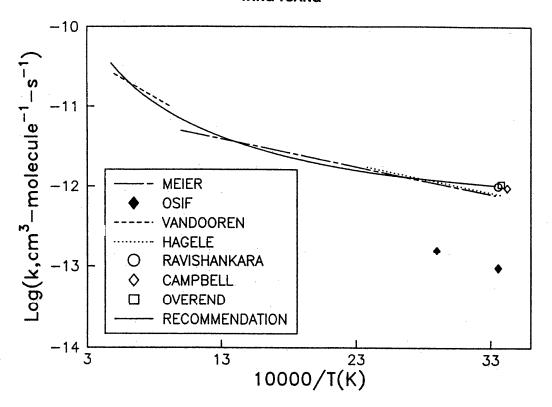


Fig. 5. Arrhenius plots of the rate constants $\mathbf{k}_{\mathbf{a}+\mathbf{b}}$. (W. Tsang, April 1985)

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Vandooren, J., and Van Tiggelen, P. J., "Experimental Investigation of Methanol Oxidation in Flames: Mechanisms and Rate Constants of Elementary Steps," Symp. Combust. <u>18</u> (Combustion Institute, Pittsburgh, 1981) p. 473

38,7
$$CH_3OH + HO_2 \rightarrow H_2O_2 + CH_2OH$$
 (a)
 $\rightarrow H_2O_2 + CH_3O$ (b)

	Conditions		Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor
	·	:		
Recommended value			$k_a=1.6x10^{-13}exp(-6330/T)$	10

Comments and Recommendations

There are no data. We suggest the use for k_a of the same rate expression as recommended by Walker [R.W. Walker, "Rate Constants for Reactions in Gas Phase Hydrocarbon Oxidation", in 'Gas Kinetics and Energy Transfer', ed. P.G. Ashmore and R.J. Donovan (Specialist Periodical Reports), The Chemical Society, London, 1977, Vol. 2, p. 296] for $HO_2 + C_3H_8 \rightarrow i-C_3H_7 + H_2O_2$, i.e. $k_a = 1.6 \times 10^{-13} \exp(-6330/T) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$

The uncertainty is a factor of 10. The exothermicity of the abstraction process will make (a) the favored channel. Reaction (b) is endothermic.

(W. Tsang, April 1985)

38,15
$$CH_3OH + HCO \rightarrow CH_2OH + H_2CO$$
 (a)
 $\rightarrow CH_3O + H_2CO$ (b)

	Cor	nditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
$\log K_{p}(a) = 0.563$	121 - 1639.5/T +	9487/T ² - 364000/T ³		i	
$\log K_{p}(b) = -1.00$	002 - 3456.7/T +	$58603/T^2 - 1.08 \times 10^7/T^3$			
Recommended value			k _a =1.6x10 ⁻²⁰ T ^{2.90} exp(-659	6/T) 10	

Comments and Recommendations

There are no data. We have used the equilibrium constant and the estimated rate expression for the reverse reaction (39,12) to obtain the following value for k_a $k_a = 1.6 \times 10^{-20} T^{2.90} \exp(-6596/T) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ with an uncertainty of a factor of 10. The rate constant of the second channel is estimated to be a factor of 100 or more slower on the basis of the reverse process, $\text{CH}_3\text{O} + \text{HCHO}$ (24,12), and the equilibrium constant. (W. Tsang, May 1985)

38,16
$$CH_3OH + CH_3 \rightarrow CH_4 + CH_2OH$$
 (a)
 $\rightarrow CH_4 + CH_3O$ (b)

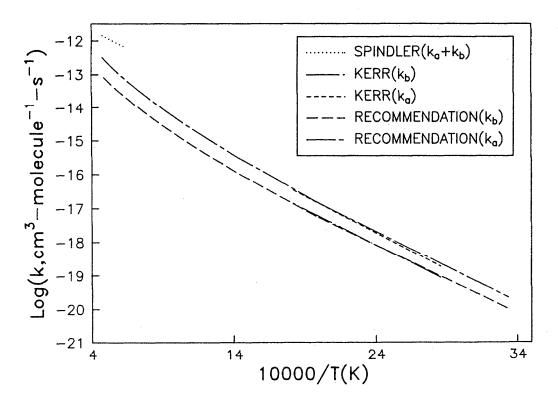
	Conc	ditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Spindler, Wagner (1982)	1600-2100	0.6-33.0x10 ¹⁸ Ar (Shock tube, CH ₃ absorption in CH ₃ OH decomp.)	$k_{a+b} = 1.5x10^{-11} exp(-4940/T)$	2	
Kerr, Parsonage (1976) (review)	350-550		$k_a = 3.24 \times 10^{-13} \exp(-5035/T)$ $k_b = 1.0 \times 10^{-13} \exp(-4884/T)$	1,4	
Recommended value			k _a =5.3x10 ⁻²³ T ^{3.17} x exp(-3609/T)	1.4 to 600K,	
Recommended value			$k_b = 2.4 \times 10^{-23} T^{3.1} \exp(-3490/T)$	-	

Using the results of Kerr and Parsonage and of a BEBO calculation, we suggest:

 $k_b = 2.4 \times 10^{-23} \text{T}^{3.1} \exp(-3490/\text{T}) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$, and

 $k_a = 5.3 \times 10^{-23} T^{3.17} \exp(-3609/T) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$

with an uncertainty factor of 1.4 up to 600 K and increasing to 3 at 2000 K. Arrhenius plots of k_a and k_b are given in Fig. 6.



 $\label{eq:Fig. 6.} \mbox{Fig. 6. Arrhenius plots of the rate constants k_a and k_b.} \mbox{(W. Tsang, April 1985)}$

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38,17
$$CH_3OH + C_2H_5 \rightarrow C_2H_6 + CH_2OH$$
 (a)
 $\rightarrow C_2H_6 + CH_3O$ (b)

	Cor	nditions	Reaction rate constant, U	Uncertainty	
Reference	'Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Recommended value			k _a =5.3x10 ⁻²³ T ^{3.17} exp(-4610/T)) 3	
Recommended value			$k_b = 2.4 \times 10^{-23} T^{3.1} \exp(-4500/T)$ 3		

Comments and Recommendations

There are no data. However, ethyl radicals are known to be considerably less reactive than methyl. We suggest the use of the rate expressions:

$$k_a = 5.3 \times 10^{-23} \text{ T}^3 \cdot 17 \exp(-4610/\text{T}) \text{ cm}^3 \text{ molecule}^{-1} \text{ s}^{-1}$$
 and

 $k_b = 2.4 \times 10^{-23} \text{T}^{3.1} \exp(-4500/\text{T}) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$.

This is based on the reaction of CH_3 with CH_3OH (38,16) and the observed trends in reactivity of methyl and ethyl radicals with hydrocarbons. The uncertainties are a factor of 3.

(W. Tsang, April 1985)

38,19
$$CH_3OH + C_2H_3 \rightarrow C_2H_4 + CH_3O$$
 (a)
 $\rightarrow C_2H_4 + CH_3O$ (b).

	Cor	nditions	Reaction rate constant, U	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Recommended value			k _a =5.3x10 ⁻²³ T ^{3.17} exp(-3609/T)	10	
Recommended value			$k_b = 2.4 \times 10^{-23} T^{3.1} \exp(-3490/T)$	10	

Comments and Recommendations

There are no data. As a very rough estimate we suggest for reaction (a) the use of our estimated rate expressions for methyl attack on methanol (38,16), i.e. $k_a=5.3x10^{-23}T^{3.17}\exp(-3609/T)cm^3molecule^{-1}s^{-1}, \text{ and } k_b=2.4x10^{-23}T^{3.1}\exp(-3490/T)cm^3molecule^{-1}s^{-1}.$ The uncertainties are a factor of 10. (W. Tsang, May 1985)

38,21
$$CH_3OH + C_2H + C_2H_2 + CH_2OH$$
 (a)
+ $CH_3O + C_2H_2$ (b)

	Cor	nditions	Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor
			11	
Recommended value			$k_a = 1 \times 10^{-11}$ $k_b = 2 \times 10^{-12}$	5
Recommended value			k _b =2x10 ⁻¹²	5

There are no data. We suggest for this reaction the following rate expressions:

$$k_a = 1.0 \times 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$$
 and

 $k_b = 2.0 \times 10^{-12} cm^3 molecule^{-1} s^{-1}$

with uncertainties of a factor of 5. Our estimates are based on measurements of C2H attack on CH4 (21,10) and C2H6 (21,11).

(W. Tsang, May 1985)

38,22 $CH_3OH + CH_3CO \rightarrow CH_3CHO + CH_2OH$

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
log K _p = 0.54426	5 - 1463.33/T - 19	9906/T ² + 6.0754x10 ⁶ /T ³			
Recommended value	10		8.06x10 ⁻²¹ T ^{2.99} exp(-6210/T)	3	

Comments and Recommendations

There are no data. Using our estimate for the reverse rate, which should be typical for the attack of alkyl radicals on an aldehydic hydrogen, and the equilibrium constant we find $k(\text{CH}_3\text{OH} + \text{CH}_3\text{CO} \rightarrow \text{CH}_3\text{CHO} + \text{CH}_2\text{OH}) = 8.06\text{x}10^{-21}\text{T}^{2.99}\text{exp}(-6210/\text{T})\text{cm}^3\text{molecule}^{-1}\text{s}^{-1}.$ We estimate an uncertainty of a factor of 3. As expected, the rate constants are very similar to those for HCO attack on methanol. Bydroxy hydrogen abstraction should be much slower and will not be important under combustion conditions. (W. Tsang, May 1985)

38,23 CH₃OH + CH₃O₂ → CH₃OOH + CH₂OH

	Co	nditions	Reaction rate constant,	Uncertainty factor	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$		
Anastasi, Hancock	600	5.0x10 ¹⁸ N ₂ , acetone, oxygen, methanol.	3.2x10 ⁻¹⁸		
Recommended value			3x10 ⁻¹³ exp(-6900/T)	1.3 at 600K, increasing to 2 at 1000K	

Assuming an A-factor of $3.0 \times 10^{-13} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ we obtain the rate expression $\text{k(CH}_3O_2 + \text{CH}_3\text{OH} \rightarrow \text{CH}_3\text{OH} + \text{CH}_2\text{OH}) = } 3.0 \times 10^{-13} \text{exp(-6900/T)cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ We estimate the uncertainty to be a factor of 1.3 at 600 K, increasing to a factor of 2 at 1000 K.

(W. Tsang, May 1985)

References

Anastasi, C., and Hancock, D. U., "Reaction of Methylperoxy Radicals with Methanol and Formaldehyde at 600K," J. Chem. Soc., Faraday Trans. I <u>80</u>, 935 (1984)

38,24 CH₃OH + CH₃O → CH₃OH + CH₂OH

	Cor	ditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K [M]/molecule cm ⁻³		k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
Recommended value			$5x10^{-13}exp(-2050/T)$	10	
			5.12¢ 2.55¢,2,		

Comments and Recommendations

There are no data. We recommend for this reaction the use of the rate expression $5.0 \times 10^{-13} \exp(-2050/T) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$, which is 3 times (1 tertiary hydrogen vs. 3 in HCH_2OH) attack on isobutane (J.A. Kerr and S.J. Moss, Handbook of Bimolecular and Termolecular Gas Reactions, Vol I, CRC Press, Boca Raton, FL, 1981). The uncertainty is a factor of 10. (W. Tsang, May 1985)

38,25
$$CH_3OH + {}^1CH_2 \rightarrow C_2H_5OH (a)$$

 $\rightarrow CH_3 + CH_2OH (b)$

Reference	Conditions Temp./K [M]/molecule cm ⁻³		Reaction rate constant, k/cm3molecule-1s-1	Uncertainty factor	
Recommended value	<u> </u>		2.5x10 ⁻¹²	3	

Although there are no data, there is no doubt that insertion (a) is the main reaction. The hot adduct can dissociate or stabilize. On a strong collision basis the fractional decomposition rates are summarized in Table A. Collision efficiencies can be found in Table B. The absolute rate is estimated to be 2.5×10^{-12} cm³molecule⁻¹s⁻¹, with an uncertainty factor of 3. This is based on the rate of $^{1}\text{CH}_{2}$ insertion into the secondary CH₂ bonds in C₃H₈. Under combustion conditions at 0.1, 1.0 and 10 atm, the predominant reaction is decomposition. There is, however, also the possibility of a direct elimination to form C₂H₄ + H₂O. We are unable to assess the importance of this channel although we suspect that it will not make any larger contribution than a bond dissociation reaction. Note that the abstraction process (b) will yield the same products as decomposition.

Table A. $log(k_b/k_{a+b})$ as a function of density and temperature for the insertion of $^{1}\text{CH}_2$ in methanol assuming strong collisions

log[M	1	T/K										
	300	500	700	900	1100	1300	1500	1700	1900	2100	2300	2500
17.0	-0.02	-0.02	-0.01	-0.01								
17.5	-0.06	-0.04	-0.03	-0.02	-0.01	-0.01						
18.0	-0.16	-0.12	-0.08	-0.06	-0.03	-0.02	-0.01	-0.01	-0.01			
18.5	-0.37	-0.30	-0.20	-0:14	-0.09	-0.06	-0.04	-0.03	-0.02	-0.01	-0.01	-0.01
19.0	-0.71	-0.59	-0.43	-0.31	-0.21	-0.14	-0.10	-0.07	-0.05	-0.03	-0.02	-0.02
19.5	-1.15	-0.98	-0.76	-0.57	-0.42	-0.30	-0.21	-0.15	-0.11	-0.08	-0.06	-0.05
20.0	-1.62	-1.44	-1.18	-0.94	-0.72	-0.55	-0.41	-0.31	-0.24	-0.18	-0.14	-0.11
20.5	-2.11	-1.92	-1.65	-1.36	-1.10	-0.89	-0.70	-0.56	-0.44	-0.37	-0.29	-0.23
21.0	-2.61	-2.41	-2.14	-1.84	-1:55	-1.31	-1.08	-0.90	-0.75	-0.62	-0.52	-0.44

Table B. Collision efficiency, βc , for the decomposition of ${\rm C_2H_5OH}$ as a function of temperature and step size down

T/K		Step	-size (cm ⁻¹)		
	150	300	600	1200	2400
300	0.15	0.31	0.51	0.69	0.83
500	0.07	0.173	0.35	0.55	0.72
700	0.045	0.124	0.27	0.47	0.66
900	0.022	0.066	0.17	0.34	0.54
1100	0.013	0.043	0.12	0.26	0.46
1300	0.008	0.028	0.082	0.20	0.38
1500	0.005	0.018	0.056	0.15	0.31
1700	0.0034	0.012	0.040	0.11	0.25
1900	0.0023	0.0082	0.028	0.081	0.20
2100	0.0015	0.0055	0.019	0.059	0.15
2300	0.001	0.0037	0.013	0.042	0.12
2500	0.0006	0.0024	0.009	0.029	0.09

(W. Tsang, May 1985)

38,26
$$CH_3OH + {}^3CH_2 \rightarrow CH_3 + CH_2OH (a)$$

 $\rightarrow CH_3 + CH_3O (b)$

	<u>Cor</u>	nditions -	Reaction rate constant, U	Jncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
				- 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4	
Recommended value			$k_a = 5.3 \times 10^{-23} T^{3.17} \exp(-3609/T)$) 3	
Recommended value			$k_h=2.4x10^{-23}T^{3.1}exp(-3490/T)$	3	

Comments and Recommendations

There are no data. All existing data on abstraction reactions of ${}^3\mathrm{CH}_2$ are upper limits. For example, see ${}^3\mathrm{CH}_2+\mathrm{H}_2$ (26,2), ${}^3\mathrm{CH}_2+\mathrm{CH}_4$ (26,10), ${}^3\mathrm{CH}_2+\mathrm{C}_2\mathrm{H}$ (26,11). The energetics of the processes is very similar to that for CH_3 abstraction. We therefore suggest the use of our recommended values for CH_3 attack on methanol: $\mathrm{k}(\mathrm{CH}_3\mathrm{OH} + {}^3\mathrm{CH}_2 \to \mathrm{CH}_3 + \mathrm{CH}_2\mathrm{OH}) = 5.28 \times 10^{-23} \mathrm{T}^{3.17} \exp(-3609/\mathrm{T}) \mathrm{cm}^3 \mathrm{molecule}^{-1} \mathrm{s}^{-1} \\ \mathrm{k}(\mathrm{CH}_3\mathrm{OH} + {}^3\mathrm{CH}_2 \to \mathrm{CH}_3 + \mathrm{CH}_3\mathrm{O}) = 2.4 \times 10^{-23} \mathrm{T}^{3.1} \exp(-3490/\mathrm{T}) \mathrm{cm}^3 \mathrm{molecule}^{-1} \mathrm{s}^{-1}$ (W. Tsang, May 1985)

39,1 CH₂OH + M → H + HCHO + M

	Conc	ditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Recommended value			k _o =75T ^{-2.5} exp(-17205/T)	4	
Recommended value	900-2500	N ₂ , 0.1-10 atm.	1.9x10 ¹⁹ T ⁻⁸ exp(-21645/T)	4	

There are no data. The values of the rate constant from the modelling of methanol pyrolysis are subject to large uncertainties. We have derived values of the rate constants using RRKM calculations and assuming a high pressure A-factor of 2.0×10^{13} (characteristic of radical decomposition) at 500 K and an activation energy for the reverse process of 13 kJ. The second order rate expression for hydroxymethyl decomposition is then $75T^{-2.5} \exp(-17205/T) \operatorname{cm}^3 \operatorname{molecule}^{-1} \mathrm{s}^{-1}$. Corrections to take into account pressure effects can be found in Table A. Collision efficiencies can be found in Table B. The rate expression for decomposition at 1 atm N₂ and 900-2500 K and with a step size down of 500 cm⁻¹ is: $1.9 \times 10^{19} \mathrm{T}^{-8} \exp(-21645/T)$ cm³ molecule $^{-1} \mathrm{s}^{-1}$. The uncertainties are factors of 4. Over this temperature range, this expression should also be valid at 0.1 and 10 atm

Table A. $log(k/k_0)$ as a function of concentration and temperature for CH_2OH decomposition

log[M]	l	T/K										
	300	500	700	900	1100	1300	1500	1700	1900	2100	2300	2500
16.5	-0.01								-			
17.0	-0.02	-0.02	-0.02	-0.02	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	
17.5	-0.07	-0.05	-0.04	-0.04	-0.03	-0.03	-0.03	-0.03	-0.02	-0.02	-0.02	-0.02
18.0	-0.18	-0.15	-0.12	-0.11	-0.10	-0.09	-0.08	-0.07	-0.07	-0.05	-0.04	-0.04
18.5	-0.40	-0.34	-0.28	-0.25	-0.21	-0.18	-0.16	-0.14	-0.12	-0.11	-0.09	-0.08
19.0	-0.74	-0.62	-0.52	-0.46	-0.39	-0.34	-0.30	-0.26	-0.23	-0.20	-0.18	-0.15
19.5	-1.16	-1.10	-0.86	-0.74	-0.64	-0.56	-0.49	-0.44	-0.38	-0.33	-0.30	-0.26
20.0	-1.68	-1.43	-1.26	-1.10	-0.97	-0.85	-0.75	-0.67	-0.59	-0.52	-0.46	-0.40
20.5	-2.11	-1.91	-1.70	-1.52	-1.35	-1.20	-1.07	-0.96	-0.86	-0.77	-0.69	-0.61
21.0	-2.60	-2.40	-2.20	-1.98	-1.79	-1.61	-1.46	-1.32	-1.20	-1.08	-0.98	-0.91

Table B. Collision efficiency, βc , as a function of step size down and temperature

T/K		Step-	-size (cm ⁻¹)		
	150	300	600	1200	2400
300	0.15	0.31	0.51	0.70	0.82
500	0.07	0.18	0.35	0.55	0.73
700	0.038	0.11	0.24	0.44	0.63
900	0.023	0.068	0.17	0.34	0.55
1100	0.014	0.045	0.12	0.27	0.47
1300	0.009	0.030	0.088	0.21	0.39
1500	0.006	0.021	0.064	0.16	0.33
1700	0.004	0.015	0.047	0.13	0.28
1900	0.003	0.010	0.034	0.097	0.23
2100	0.002	0.0074	0.025	0.075	0.18
2300	0.0015	0.0053	0.018	0.057	0.15
2500	0.001	0.0038	0.014	0.043	0.12

(W. Tsang, May 1985)

39,2 $CH_2OH + H_2 \rightarrow CH_3OH + H$

the grant of the g	Cor	nditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³ .	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
$\log K_{\rm p} = -1.8034 - 1$	741.76/T + 12	2769/T ² - 0.3547x10 ⁷ /T ³			
Recommended value	500-2500		1.12x10 ⁻¹⁸ T ^{2.02} exp(-6722/T)	4	

Comments and Recommendations

There are no data. From k values for reverse reaction (38,4) and equilibrium constant we obtain the recommended expression. Estimated uncertainty factor is 4. (W. Tsang, May 1985)

39,3 $CH_2OH + O_2 \rightarrow HCHO + HO_2$

	Cor	nditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Radford (1980)	300	1.6x10 ¹⁶ He, (1.0-4.0)x10 ¹⁴ CH ₃ OH, O ₂ .	2.0x10 ⁻¹²	2	
Recommended value			2.0x10 ⁻¹²	. 2	

Comments and Recommendations

We recommend use of the reported value over all temperatures. (W. Tsang, May 1985)

References

Radford, H. E., "The Fast Reaction of CH_2OH with O_2 ," Chem. Phys. Lett. 71, 195 (1980)

39,4 H +
$$CH_2OH \rightarrow BCHO + H_2$$
 (a)
 $\rightarrow CH_3 + OH$ (b)
 $\rightarrow CH_3OH$ (c)

	Cor	ditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
Recommended value			k _a =1x10 ⁻¹¹ k _b =1.6x10 ⁻¹⁰	3 2	

Comments and Recommendations

There are no data. We estimate that the disproportionation reaction (a) will be somewhat faster than that for C_2H_5+H (17,3), i.e., $k_a-1.0x10^{-11} cm^3 molecule^{-1} s^{-1}$ with an uncertainty of a factor of 3. The addition process (b) is the main reaction. We estimate its rate constant to be $1.6x10^{-10} cm^3 molecule^{-1} s^{-1}$ with an uncertainty of a factor of 2. Calculations show that, because of the existence of an exothermic decomposition channel, the rate constant is virtually independent of pressure. The branching ratio on the basis of strong collisions can be found in Table A. Collision efficiencies, as a function of step size down and temperature, can be found in Table B. In the pressure range of 0.1, 1 and 10 atms under higher temperature conditions decomposition is the predominant process. Here we assume 500 cm⁻¹ for step size down for N_2 and 1000 cm⁻¹ as the step size down for CH_3OH . This is based on the general trends established in our analysis in the Introduction.

Table A. $\log (k_b/k_{b+c})$ as a result of hydrogen addition to hydroxymethyl radical under strong collision conditions

						T/K					
300	50,0	700	900	1100	1300	1500	1700	1900	2100	2300	2500
-0.01											
-0.03	-0.01	-0.01									
-0.07	-0.04	-0.02	-0,02	-0.01							
-0.20	-0.11	-0.07	-0.04	-0.03	-0.02	-0.01	-0.01				
-0.43	-0.27	-0.15	-0.10	-0.07	-0.04	-0.02	-0.02	-0.01	-0.01	-0.01	
-0.76	-0.52	-0.35	-0.23	-0.15	-0.10	-0.07	-0.05	-0.03	-0.02	-0.02	-0.01
-1.20	-0.86	-0.60	-0.43	-0.29	-0.20	-0.14	-0.12	-0.07	-0.05	-0.04	-0.03
-1.66	-1.29	-0.95	-0.69	-0.50	-0.38	-0.27	-0.21	-0.16	-0.12	-0.10	-0.07
-2.16	-1.75	-1.36	-1.04	-0.80	-0.62	-0.48	-0.39	-0.31	-0.24	-0.20	-0.16
-2.67	-2.24	-1.82	-1.45	-1.17	-0.95	-0.77	-0.63	-0.52	-0.44	-0.36	-0.31
-3.18	-2.74	-2.30	-1.92	-1.60	-1.34	-1.17	-0.96	-0.81	-0.70	-0.61	-0.52
	-0.01 -0.03 -0.07 -0.20 -0.43 -0.76 -1.20 -1.66 -2.16	-0.01 -0.03 -0.01 -0.07 -0.04 -0.20 -0.11 -0.43 -0.27 -0.76 -0.52 -1.20 -0.86 -1.66 -1.29 -2.16 -1.75 -2.67 -2.24	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.20 -0.11 -0.07 -0.43 -0.27 -0.15 -0.76 -0.52 -0.35 -1.20 -0.86 -0.60 -1.66 -1.29 -0.95 -2.16 -1.75 -1.36 -2.67 -2.24 -1.82	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.20 -0.11 -0.07 -0.04 -0.43 -0.27 -0.15 -0.10 -0.76 -0.52 -0.35 -0.23 -1.20 -0.86 -0.60 -0.43 -1.66 -1.29 -0.95 -0.69 -2.16 -1.75 -1.36 -1.04 -2.67 -2.24 -1.82 -1.45	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.01 -0.20 -0.11 -0.07 -0.04 -0.03 -0.43 -0.27 -0.15 -0.10 -0.07 -0.76 -0.52 -0.35 -0.23 -0.15 -1.20 -0.86 -0.60 -0.43 -0.29 -1.66 -1.29 -0.95 -0.69 -0.50 -2.16 -1.75 -1.36 -1.04 -0.80 -2.67 -2.24 -1.82 -1.45 -1.17	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.01 -0.20 -0.11 -0.07 -0.04 -0.03 -0.02 -0.43 -0.27 -0.15 -0.10 -0.07 -0.04 -0.76 -0.52 -0.35 -0.23 -0.15 -0.10 -1.20 -0.86 -0.60 -0.43 -0.29 -0.20 -1.66 -1.29 -0.95 -0.69 -0.50 -0.38 -2.16 -1.75 -1.36 -1.04 -0.80 -0.62 -2.67 -2.24 -1.82 -1.45 -1.17 -0.95	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.01 -0.20 -0.11 -0.07 -0.04 -0.03 -0.02 -0.01 -0.43 -0.27 -0.15 -0.10 -0.07 -0.04 -0.02 -0.76 -0.52 -0.35 -0.23 -0.15 -0.10 -0.07 -1.20 -0.86 -0.60 -0.43 -0.29 -0.20 -0.14 -1.66 -1.29 -0.95 -0.69 -0.50 -0.38 -0.27 -2.16 -1.75 -1.36 -1.04 -0.80 -0.62 -0.48 -2.67 -2.24 -1.82 -1.45 -1.17 -0.95 -0.77	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.01 -0.20 -0.11 -0.07 -0.04 -0.03 -0.02 -0.01 -0.01 -0.43 -0.27 -0.15 -0.10 -0.07 -0.04 -0.02 -0.02 -0.76 -0.52 -0.35 -0.23 -0.15 -0.10 -0.07 -0.05 -1.20 -0.86 -0.60 -0.43 -0.29 -0.20 -0.14 -0.12 -1.66 -1.29 -0.95 -0.69 -0.50 -0.38 -0.27 -0.21 -2.16 -1.75 -1.36 -1.04 -0.80 -0.62 -0.48 -0.39 -2.67 -2.24 -1.82 -1.45 -1.17 -0.95 -0.77 -0.63	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.01 -0.20 -0.11 -0.07 -0.04 -0.03 -0.02 -0.01 -0.01 -0.43 -0.27 -0.15 -0.10 -0.07 -0.04 -0.02 -0.02 -0.01 -0.76 -0.52 -0.35 -0.23 -0.15 -0.10 -0.07 -0.05 -0.03 -1.20 -0.86 -0.60 -0.43 -0.29 -0.20 -0.14 -0.12 -0.07 -1.66 -1.29 -0.95 -0.69 -0.50 -0.38 -0.27 -0.21 -0.16 -2.16 -1.75 -1.36 -1.04 -0.80 -0.62 -0.48 -0.39 -0.31 -2.67 -2.24 -1.82 -1.45 -1.17 -0.95 -0.77 -0.63 -0.52	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.01 -0.20 -0.11 -0.07 -0.04 -0.03 -0.02 -0.01 -0.01 -0.43 -0.27 -0.15 -0.10 -0.07 -0.04 -0.02 -0.02 -0.01 -0.01 -0.76 -0.52 -0.35 -0.23 -0.15 -0.10 -0.07 -0.05 -0.03 -0.02 -1.20 -0.86 -0.60 -0.43 -0.29 -0.20 -0.14 -0.12 -0.07 -0.05 -1.66 -1.29 -0.95 -0.69 -0.50 -0.38 -0.27 -0.21 -0.16 -0.12 -2.16 -1.75 -1.36 -1.04 -0.80 -0.62 -0.48 -0.39 -0.31 -0.24 -2.67 -2.24 -1.82 -1.45 -1.17 -0.95 -0.77 -0.63 -0.52 -0.44	-0.01 -0.03 -0.01 -0.01 -0.07 -0.04 -0.02 -0.02 -0.01 -0.20 -0.11 -0.07 -0.04 -0.03 -0.02 -0.01 -0.01 -0.43 -0.27 -0.15 -0.10 -0.07 -0.04 -0.02 -0.02 -0.01 -0.01 -0.01 -0.76 -0.52 -0.35 -0.23 -0.15 -0.10 -0.07 -0.05 -0.03 -0.02 -0.02 -1.20 -0.86 -0.60 -0.43 -0.29 -0.20 -0.14 -0.12 -0.07 -0.05 -0.04 -1.66 -1.29 -0.95 -0.69 -0.50 -0.38 -0.27 -0.21 -0.16 -0.12 -0.10 -2.16 -1.75 -1.36 -1.04 -0.80 -0.62 -0.48 -0.39 -0.31 -0.24 -0.20 -2.67 -2.24 -1.82 -1.45 -1.17 -0.95 -0.77 -0.63 -0.52 -0.44 -0.36

Table B. Collision efficency, βc , as a function of temperature and step size down

T/K		Step	-size (cm ⁻¹)		
	150	300	600	1200	2400
300	0.15	0.32	0.52	0.70	0.83
500	0.08	0.17	0.36	0.57	0.74
700	0.043	0.12	0.26	0.46	0.65
900	0.027	0.079	0.19	0.37	0.58
1100	0.018	0.055	0.15	0.30	0.51
1300	0.012	0.038	0.11	0.24	0.43
1500	0.008	0.028	0.082	0.20	0.38
1700	0.006	0.021	0.064	0.16	0.33
1900	0.0045	0.016	0.050	0.13	0.27
2100	0.0034	0.012	0.039	0.11	0.25
2300	0.0026	0.009	0.031	0.09	0.21
2500	0.002	0.007	0.025	0.074	0.18

⁽W. Tsang, May 1985)

39,5 CH₂OH + O → HCHO + OH

	Con	ditions	Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}s^{-1}$	factor
Recommended value			7x10 ⁻¹¹	2

Comments and Recommendations

There are no data. We estimate a rate constant of $7.0 \times 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ with an uncertainty of a factor of 2.

(W. Tsang, May 1985)

39,6 $CH_2OH + OH \rightarrow H_2O + HCHO$

	Cor	nditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
Recommended value			4x10 ⁻¹¹	2	

Comments and Recommendations

There are no data. The estimated rate constant is $4.0 \times 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ with an uncertainty of a factor of 2. (W. Tsang, May 1985)

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39,7 $CH_2OH + HO_2 \rightarrow H_2O_2 + HCHO$

	Cor	nditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
Recommended value			2x10 ⁻¹¹	2	

Comments and Recommendations

There are no data. We recommend the rate constant $2.0 \times 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ with an uncertainty of a factor of 2. (W. Tsang, May 1985)

39,8 $CH_2OH + H_2O_2 \rightarrow CH_3OH + HO_2$

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
log K _p = -1.5963	+ 2322.74/T - 90	$424.6/T^2 + 5.947 \times 10^6/T^3$			
Recommended valu	l e	•	5x10 ⁻¹⁵ exp(-1300/T)	· 10	

Comments and Recommendations

There are no data. We have used our estimated rate expression for the reverse process (38,7) and the equilibrium constant to derive the following $k_{39,8}$ value $5.0 \times 10^{-15} \exp(-1300/T) \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$. The estimated uncertainty factor is 10. (W. Tsang, May 1985)

39,10 сп20п + сп4 → сп30п + сп3

	Conditions		Reaction rate constant,	Uncertainty factor	
Reference	Temp./K	Temp./K [M]/molecule cm ⁻³ k/cm^3 molecule ⁻¹ s ⁻¹			
Log K _n = -0.2933	3 - 1935.86/T - 20	$0872/T^2 + 3.6024 \times 10^6/T^3$			
Recommended valu	1 0 ·		$3.6 \times 10^{-23} \text{T}^{3.14} \exp(-8166/\text{T})$	3	

Comments and Recommendations

There are no data. We have used the rate expression for the reverse process, $CH_3OH + CH_3 \rightarrow CH_4 + CH_2OH$ (38,16), and the equilibrium constant to derive the rate expression

 $k(CH_2OH + CH_4 + CH_3OH + CH_3) = 3.6x10^{-23}T^{3.14}exp(-8166/T)cm^3molecule^{-1}s^{-1}$

The uncertainties are due mostly to possible errors in the heat of formation of CH_2OH , which we estimate, will lead to an uncertainty factor of 3 from 700 K up. (W. Tsang, May 1985)

39,11 $CH_2OH + C_2H_6 \rightarrow C_2H_5 + CH_3OH$

	Conditions		Reaction rate constant,	Uncertainty factor
Reference	Temp./K [M]/molecule cm ⁻³ k/cm ³ m		k/cm^3 molecule $^{-1}$ s $^{-1}$	
log K _p = 0.02297	/-913.89/T-25937/I	r ² +1.4066x10 ⁶ /T ³		•
Recommended value	ıe	·	$3.3 \times 10^{-22} \text{T}^{2.95} \exp(-7033/\text{T})$	5

Comments and Recommendations

There are no data. We have used our estimated rate expression for the reverse reaction and the equilibrium constant to derive

 $k(CH_2OH + C_2H_6 \rightarrow CH_3OH + C_2H_5) = 3.3x10^{-22}T^{2.95}exp(-7033/T)cm^3molecule^{-1}s^{-1}$ The uncertainty is a factor of 5. (W. Tsang, May 1985)

39,12 CH₂OH + HCHO → CH₃OH + HCO

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
Recommended value			$9.1x10^{-21}T^{2.81}exp(-2950/T)$	3	

Comments and Recommendations

There are no data. In view of the constancy of the rate of alkyl radical attack on the aldehydic H at 182 C (J. A. Kerr and A. F. Trotman-Dickenson, "The Reactions of Alkyl Radicals," in 'Progress in Reaction Kinetics, Vol I,' G. Porter ed., Pergamon Press, NY, 1961, p. 107), we suggest use of our recommended rate expression for $CH_3 + H_2CO$ (12,10) leading to:

 $k(CH_2OH + HCHO \rightarrow CH_3OH + CHO) = 9.1x10^{-21}T^{2.81}exp(-2950/T)cm^3molecule^{-1}s^{-1}$ with an uncertainty of a factor of 3. (W. Tsang, May 1985)

39,15 CH₂OH + HCO → CH₃OH + CO (a) → 2HCHO (b)

	<u>Conditions</u>		Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Recommended value			k _a =2x10 ⁻¹⁰	3	
Recommended value			k _a =2x10 ⁻¹⁰ k _b =3x10 ⁻¹⁰	3 '	

There are no data. We believe that disproportionation will be the predominant process and that it will favor the most exothermic channel. We estimate rate constants of $2.0 \text{x} 10^{-10} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ for (a) and $3.0 \text{x} 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ for (b). The uncertainties are a factor of 3 for each process. (W. Tsang, May 1985)

39,16 $CH_2OH + CH_3 \rightarrow CH_3CH_2OH$ (a) $\rightarrow CH_4 + CH_2O$ (b)

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K [M]/molecule cm ⁻³		k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Recommended value			k _a o=2x10 ⁻¹¹	2	
Recommended value	>900 K	1 atm N ₂	$\log k_a/k_a^{\infty=0.202+1.755 \times 10^{-4} T}$ $5.61 \times 10^{-7} T^2$	-	
Recommended value			$k_b = 4 \times 10^{-12}$	5	

Comments and Recommendations

There are no data. The high pressure rate constant for combination should be $2.0 \text{x} 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ with an uncertainty of a factor of 2. Fall-off behavior on a strong collision basis can be found in Table A. Collision efficiencies as a function of temperature and step size down are given in Table B. Departure from strong collision behavior at 0.1, 1.0 and 10.0 atms for (Ar) and $\text{C}_2\text{H}_5\text{OH}$ are as follows:

$$\log(k(Ar, 0.1)/k\omega) = 0.794 - 8.69x10^{-4}T - 3.794x10^{-7}T^{2}$$

$$\log(k(Ar, 1.0)/k\omega) = 0.202 + 1.755x10^{-4}T - 5.614x10^{-7}T^{2}$$

$$\log(k(Ar, 10)/k\omega) = -0.29 + 8.827x10^{-4}T - 6.307x10^{-7}T^{2}$$

 $\log(k(C_2H_5OH, 0.1)/k\omega) = 0.488 - 3.630 \times 10^{-4} \text{T} - 4.395 \times 10^{-7} \text{T}^2$ $\log(k(C_2H_5OH, 1.0)/k\omega) = -0.070 + 5.603 \times 10^{-4} \text{T} - 5.893 \times 10^{-7} \text{T}^2$ $\log(k(C_2H_5OH, 10)/k\omega) = -0.405 + 9.694 \times 10^{-4} \text{T} - 5.666 \times 10^{-7} \text{T}^2$

where we have assumed step sizes down of $500~{\rm cm}^{-1}$ and $1000~{\rm cm}^{-1}$, respectively. The results for argon should also be applicable for nitrogen.

For the disproportionation process, we estimate $k_{\rm b}/k_{\rm a}\sim 0.2$ with an uncertainty of a factor of 5.

Table A. Fall off behavior log(k/km) for the combination of methyl and hydroxymethyl radicals assuming strong collisions

log[M]						T/K					
	500	700	900	1100	1300	1500	1700	1900	2100	2300	2500
16.0	-0.16	-0.36	-0.59	-0.87	-1.16	-1.50	-1.81	-2.11	-2.4	-2.08	-2.95
16.5	-0.08	-0.Z1	-0.39	-0.62	-0.87	-1.19	-1.46	-1.74	-2.01	-2.27	-2.52
17.0	-0.04	-0.11	-0.24	-0.42	-0.63	-0.90	-1.15	-1.40	-1.64	-1.88	-2.11
17.5	-0.01	-0.05	-0.13	-0.26	-0.43	-0.65	-0.86	-1.08	-1.29	-1.52	-1.73
18.0		-0.02	-0.07	-0.15	-0.27	-0.44	-0.61	-0.80	-0.99	-1.18	-1.37
18.5		-0.01	-0.03	-0.08	-0.16	-0.28	-0.41	-0.56	-0.72	-0.88	-1.05
19.0			-0.02	-0.04	-0.08	-0.16	-0.26	-0.37	-0.49	-0.62	-0.76
19.5				-0.02	-0.04	-0.08	-0.14	-0.22	-0.31	-0.41	-0.59
20.0				-0.01	-0.01	-0.04	-0.07	-0.12	-0.18	-0.24	-0.32
20.5						-0.02	-0.03	-0.06	-0.09	-0.13	-0.18
21.0							-0.01	-0.02	-0.04	-0.06	-0.09

Table B. Collision efficiency, β c, for the combination of methyl and hydroxymethyl radicals as a function of temperature and step size down

T/K		Step-size (cm ⁻¹)					
	150	300	600	1200	2400		
300	0.15	0.31	0.51	0.69	0.83		
500	0.07	0.173	0.35	0.55	0.72		
700	0.045	0.124	0.27	0.47	0.66		
900	0.022	0.066	0.17	0.34	0.54		
1100	0.013	0.043	0.12	0.26	0.46		
1300	0.008	0.028	0.082	0.20	0.38		
1500	0.005	0.018	0.056	0.15	0.31		
1700	0.0034	0.012	0.040	0.11	0.25		
1900	0.0023	0.0082	0.028	0.081	0.20		
2100	0.0015	0.0055	0.019	0.059	0.15		
2300	0.001	0.0037	0.013	0.042	0.12		
2500	0.0006	0.0024	0.009	0.029	0.09		

(W. Tsang, May 1985)

39,17
$$C_2H_5 + CH_2OH \rightarrow n-C_3H_7OH$$
 (a)
 $\rightarrow C_2H_6 + HCHO$ (b)
 $\rightarrow C_2H_4 + CH_3OH$ (c)

	<u>Cor</u>	nditions	Reaction rate constant,	Uncertainty	
Reference	Temp./K [M]/molecule cm ⁻³		k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Recommended value			k _a =2x10 ⁻¹¹	2	
Recommended value			$k_a = 2x10^{-11}$ $k_b = 4x10^{-12}$ $k_c = 4x10^{-12}$	5	
Recommended value			k ₀ =4x10 ⁻¹²	5	

There are no data. The combination rate must be very close to 2x10⁻¹¹cm³molecule-1s-1 with an uncertainty of a factor of 2. Fall off behavior does not become important until temperatures are in excess of 1000 K. In view of the instability of ethyl and hydroxymethyl, their lifetimes at 1000 K will be short and combination cannot be an important process. We estimate the rate constants of reactions (b) and (c) to be $4x10^{-12}$ cm³ molecule⁻¹ s⁻¹ with an uncertainty of a factor of 5. (W. Tsang, May 1985)

39,18
$$CH_2OH + C_2H_4 \rightarrow CH_2CH_2CH_2OH$$
 (a)
 $\rightarrow C_2H_5 + HCHO$ (b)

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K [M]/molecule cm ⁻³		k/cm ³ molecule ⁻¹ s ⁻¹	factor	
Recommended value			k _a =8x10 ⁻¹⁴ exp(-3500/T)	5	
			(reversed under combustion		
			conditions)		
Recommended value			$k_b = k_a x(exp(-2000/T)/$		
			(1+exp(-2000/T)))	5	

Comments and Recommendations

There are no data. The rate constant for the addition process, as for n-propyl addition to ethylene (41,18), is estimated to be 8.0x10⁻¹⁴exp(-3500/T)cm³molecule-1s-1 since the rates of alkyl radical addition to ethylene are remarkably si-(J. A. Kerr and A. F. Trotman-Dickenson, "The Reactions of Alkyl Radicals," in 'Progress in Reaction Kinetics' Vol. I (G. Porter, ed) Pergamon Press, New York, 1961, p. 105). However, under most combustion conditions the reaction is reversible. For reaction (b), which involves a 1-4 hydrogen shift, we suggest multiplying this rate expression by the factor $\exp(-2000/T)(1+\exp(-2000/T)$. The uncertainty is a factor of 5. (W. Tsang, May 1985)

39,19
$$CH_2OH + C_2H_3 \rightarrow C_2H_4 + HCHO$$
 (a)
 $\rightarrow C_3H_5 + OH$ (b)

Conditions		Reaction rate constant,	Uncertainty
Temp./K	mp./K [M]/molecule cm ⁻³ k/cm ³ molecule ⁻¹ s ⁻¹		factor
		$k_a = 5 \times 10^{-11}$	2.5
•		$k_b = 2x10^{-11}$	2

There are no data. The large reaction exothermicity will lead to disproportionation products with a rate constant near collisional $5.0 \times 10^{-11} \mathrm{cm}^3 \mathrm{molecule}^{-1} \mathrm{s}^{-1}$, with an uncertainty of a factor of 2.5. The combination process (b) will lead to a hot adduct, which will decompose under combustion conditions to give C_3H_5 and OH. The rate expression is $2.0 \times 10^{-11} \mathrm{cm}^3 \mathrm{molecule}^{-1} \mathrm{s}^{-1}$ with an uncertainty of a factor of 2.

(W. Tsang, May 1985)

39,20
$$CH_2OH + C_2H_2 \rightarrow C_3H_4OH$$
 (a) $\rightarrow C_2H_3 + BCHO$ (b)

	Conditions		Reaction rate constant,	Uncertainty
Reference	Temp./K [M]/molecule cm ⁻³		k/cm^3 molecule $^{-1}$ s $^{-1}$	factor
				
Recommended value			$k_b = 1.2 \times 10^{-12} \exp(-4531/T)$	3

Comments and Recommendations

There are no data. The rates of addition should be close to those for the addition of alkyl radicals to acetylene. The major uncertainty is the relative importance of the reverse reaction as compared to 1-4 hydrogen shift reaction (b). In view of the exothermicity of the latter, we believe it will be the major process and recommend

 $k(C_2H_2+CH_2OH \rightarrow C_2H_3 + HCHO) = 1.2x10^{-12}exp(-4531/T)cm^3molecule^{-1}s^{-1}$. This is similar to that for alkyl radical addition to acetylene. The unceratinty is a factor of 3.

(W. Tsang, May 1985)

39,21
$$CH_2OH + C_2H \rightarrow C_2H_2 + HCHO$$
 (a)
 $\rightarrow C_3H_3 + OH$ (b)

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
Recommended value			k_=6x10 ⁻¹¹	5	
Recommended value			$k_a = 6 \times 10^{-11}$ $k_b = 2 \times 10^{-11}$	3	

There are no data. Taking into account the very exothermic nature of reaction (a), we estimate $k_a(CH_2OH + C_2H \rightarrow C_2H_2 + HCHO) = 6.0x10^{-11} cm^3 molecule^{-1} s^{-1}$. The second decompositions channel involves combination followed by decomposition of the hot adduct. We estimate $k_b(CH_2OH + C_2H \rightarrow C_3H_3 + OH) = 2.0x10^{-11} cm^3 molecule^{-1} s^{-1}$. The uncertainties are a factor of 5 and 3 respectively. (W. Tsang, May 1985)

39,22 $CH_2OH + CH_3CO \rightarrow CH_3COCH_2OH$

	<u>Conditions</u>		Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor
<u> </u>				
Recommended value			2x10 ⁻¹¹	2

Comments and Recommendations

There are no data. Combination is the main process. The rate constant is estimated to be $2.0 \text{x} 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$, with an uncertainty of a factor of 2. (W. Tsang, May 1985)

39,23 СП20П + СП302 → СП30 + ОП + ПСПО

	Conditions		Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor
Recommended value			2x10 ⁻¹¹	3

Comments and Recommendations

There are no data. Under combustion conditions combination followed by rapid decomposition of the peroxide and 'OCH₂OH will lead to the production of CH₃O, OH and HCHO. We estimate the rate constant to be $2.0 \times 10^{-11} \mathrm{cm}^3 \mathrm{molecule}^{-1} \mathrm{s}^{-1}$ with an uncertainty of a factor of 3.

(W. Tsang, May 1985)

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39,24 CH₂OH + CH₃O → CH₃OH + HCHO

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	M]/molecule cm ⁻³ k/cm ³ molecule ⁻¹ s ⁻¹		
	· · · · · · · · · · · · · · · · · · ·			· · · · · · · · · · · · · · · · · · ·	
Recommended value			$4x10^{-11}$	2	

Comments and Recommendations

There are no data. We estimate the rate constant to be $4.0 \times 10^{-11} \text{cm}^3 \text{molecule}^{-1} \text{s}^{-1}$ with an uncertainty of a factor of 2. (W. Tsang, May 1985)

39,25 $CH_2OH + {}^{1}CH_2 \rightarrow CH_3CHO + H$

	Conditions		Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm ³ molecule ⁻¹ s ⁻¹	factor
Recommended value			3x10 ⁻¹¹	2

Comments and Recommendations

There are no data. However, since ${}^{1}\text{CH}_{2}$ is known to insert extremely rapidly into C-H bonds, there can be no doubt that the product is an extremely hot adduct, which decomposes to acetaldehyde and a hydrogen atom. We suggest the use of a rate constant of $3.0 \times 10^{-11} \text{cm}^{3} \text{molecule}^{-1} \text{s}^{-1}$, with an uncertainty factor of 2. (W. Tsang, May 1985)

39,26
$$CH_2OH + {}^3CH_2 \rightarrow C_2H_4 + OH (a)$$

 $\rightarrow CH_3 + HCHO (b)$

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K [M]/molecule cm ⁻³		k/cm^3 molecule $^{-1}s^{-1}$	factor	
Recommended value			k =/v10 ⁻ 11	3	
Recommended value			$k_a = 4 \times 10^{-11}$ $k_b = 2.0 \times 10^{-12}$	3	

Comments and Recommendations

There are no data. One expects a fast combination, with a rate constant of $\sim 4.0 \times 10^{-11} \mathrm{cm}^3 \mathrm{molecule}^{-1} \mathrm{s}^{-1}$, followed by decomposition of the adduct, since the reaction is highly exothermic. The uncertainty is a factor of 3. The disproportionation reaction may be considerably slower. We estimate a rate constant of $2.0 \times 10^{-12} \mathrm{cm}^3 \mathrm{molecule}^{-1} \mathrm{s}^{-1}$ with an uncertainty of a factor of 3. (W. Tsang, May 1985)

39,38 $CH_2OH + CH_3OH \rightarrow CH_3O + CH_3OH$

	Conditions		Reaction rate constant,	Uncertainty	
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor	
log K _p = -1.561 -	1817.2/T + 4911	167/T ² - 1.044x10 ⁷ /T ³			
Recommended value			1.3x10 ⁻¹⁴ exp(-6070/T)	10	

There are no data. We have calculated the following recommended rate expression $k(CH_2OH + CH_3OH \rightarrow CH_3O + CH_3OH) = 1.3x10^{-14}exp(-6070/T)cm^3molecule^{-1}s^{-1}$, using the estimated reverse rate (38,14) and the equilibrium constant. The estimated uncertainty is a factor of 10.

(W. Tsang, May 1985)

39,39 $CH_2OH + CH_2OH \rightarrow HOCH_2CH_2OH$ (a) $\rightarrow CH_3OH + HCHO$ (b)

	Conditions		Reaction rate constant,	Uncertainty
Reference	Temp./K	[M]/molecule cm ⁻³	k/cm^3 molecule $^{-1}$ s $^{-1}$	factor
Meier, et al. (1985)		k _{a+b} =1.5x10 ⁻¹¹	. 2	
Recommended value			k _a =1.0x10 ⁻¹¹	. 2
Recommended value			$k_a = 1.0 \times 10^{-11}$ $k_b = 5 \times 10^{-12}$	2

Comments and Recommendations

The results of Meier et al. are in the expected range. One would expect that the greater exothermicity of the disproportionation process (b) than that for alkyl radicals would lead to a higher disproportionation to combination ratio. Therefore, we assign the value $k_{\rm b}/k_{\rm a}=0.5$, with an uncertainty of a factor of 2. (W. Tsang, May 1985)

References

Meier, V., Grotheer, H. H., Riekert, G., and Just, T., "Study of Hydroxyl Reactions with Methanol and Ethanol by Laser Induced Fluorescence," Ber. Bunsenges. Phys. Chem. <u>80</u>, 325 (1985)

CHEMICAL KINETIC DATA BASE FOR COMBUSTION CHEMISTRY

4. Thermodynamic Data Tables

Thermodynamic properties of CH3OH (Species No. 38)

Thermodynamic properties of CH_2OH (Species No. 39)

	J mol ⁻¹ K ⁻¹		kJ mol ⁻¹			J mo	1 ⁻¹ K ⁻¹	1 _K -1 kJ mol ⁻¹	
T/K	c_p	s	$\Delta H_{ ilde{\mathbf{f}}}$	$\Delta \mathtt{G}_{\mathtt{f}}$	T/K	c _p	S	$^{\Delta H}$ f	ΔGf
300	44,14	239.96	-201.17	-162.17	300	43.01	255.55	-17.53	-2.87
500	59.71	266.06	-207.86	-134.22	500	54.82	280.28	-21.91	8.16
700	73.85	288.49	-212.71	-103.85	700	64.79	300.38	-25.27	20.81
900	84.98	308.44	-215,98	-103.85	900	72.61	317.64	-27.72	34.32
1100	93.60	326.45	-217.94	-40.17	1100	78.75	332.83	-29.41	48.29
1300	100.25	342.54	-219.07	-7.70	1300	83.53	346.39	-30,56	62.51
1500	108.41	357.27	-219.57	24.89	1500	87.22	358.62	-31.39	76.90

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 $\log K_D = -8.7463 + 12055.9/T - 402680/T^2 + 3.47379x107/T^3$

 $log Kp = -3.89504 + 2016.76/T - 305220/T^2 + 2.87909x107/T^3$

September 1985

Chen, S.S., Wilhoit, R. C., and Zwolinski, B. J.; "Thermodynamic Properties of Normal and Deuterated Methanols," J. Phys. Chem. Ref. Data, 6, 105 (1977).

Frequencies are: 3300 (1), 2950 (2), 1400 (3), 1030 (1), 800 (1). 1 Free Rotor; Moment of Inertia = 1.67×10^{-40} gm cm² and symmetry = 1. $IxIyIz = 4.45x10^{-117} \text{ gm}^3 \text{ cm}^6$. Symmetry No. = 1. Heat of Formation at 300 K = -17.53kJ mol⁻¹ from W. Tsang, Int. J. Chem. Kin. 7, 173 (1976)

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5. Transport Properties

Parameters in the Lennard-Jones Potential used to calculate transport properties pertinent to unimolecular reactions.

Substance	σ (Angstroms)	€/k (K)	
Argon	3.542	93.3	
Helium	2.551	10.22	
Krypton	3.655	178.9	
Neon	2.82	32.8	
Air	3.711	78.6	
Methane	3.758	148.6	
Carbon Monoxide	3.690	91.7	
Carbon Dioxide	3.941	195.2	
Acetylene	4.033	231.8	
Ethylene	4.163	224.7	
Ethane	4.443	215.7	
Hydrogen(H2)	2.827	59.7	
Nitrogen(N2)	3.798	71.1	
Oxygen(O2)	3.467	106.7	
Sulfur Hexafluoride	5.128	222.1	
Water	2.641	804.1	
Methanol	3.626	481.8	
Hydroxymethyl	we used same values a	s for methanol	

From: Reid, R. C., Prausnitz, J. M. and Sherwood, T. K., "The
Properties of Gases and Liquids" (3rd. ed.), McGraw-Hill
Book Company, New York, (1977).