

Selected Tables of Atomic Spectra

A Atomic Energy Levels - Second Edition

B Multiplet Tables

O I

Data Derived from the Analyses of Optical Spectra

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Abstract

The present publication is the seventh Section of a series being prepared in response to the need for a current revision of two sets of the author's tables containing data on atomic spectra as derived from analyses of optical spectra. As in the previous Sections, Part A contains the atomic energy levels and Part B the multiplet tables. Section 7 presents this material for the first spectrum of oxygen, O I. The form of presentation is described in detail in the text to Section 1.

Key words: Atomic energy levels, O I; Atomic spectra, O I; Multiplet Table, O I; Oxygen, first spectrum; Spectrum O I; Wavelengths, O I.

Foreword

The National Standard Reference Data System provides access to the quantitative data of physical science, critically evaluated and compiled for convenience and readily accessible through a variety of distribution channels. The System was established in 1963 by action of the President's Office of Science and Technology and the Federal Council for Science and Technology, and responsibility to administer it was assigned to the National Bureau of Standards.

NSRDS receives advice and planning assistance from a Review Committee of the National Research Council of the National Academy of Sciences-National Academy of Engineering. A number of Advisory Panels, each concerned with a single technical area, meet regularly to examine major portions of the program, assign relative priorities, and identify specific key problems in need of further attention. For selected specific topics, the Advisory Panels sponsor subpanels which make detailed studies of users' needs, the present state of knowledge, and existing data resources as a basis for recommending one or more data compilation activities. This assembly of advisory services contributes greatly to the guidance of NSRDS activities.

The System now includes a complex of data centers and other activities in academic institutions and other laboratories. Components of the NSRDS produce compilations of critically evaluated data, reviews of the state of quantitative knowledge in specialized areas, and computations of useful functions derived from standard reference data. The centers and projects also establish criteria for evaluation and compilation of data and recommend improvements in experimental techniques. They are normally associated with research in the relevant field.

The technical scope of NSRDS is indicated by the categories of projects active or being planned: nuclear properties, atomic and molecular properties, solid state properties, thermodynamic and transport properties, chemical kinetics, and colloid and surface properties.

Reliable data on the properties of matter and materials are a major foundation of scientific and technical progress. Such important activities as basic scientific research, industrial quality control, development of new materials for building and other technologies, measuring and correcting environmental pollution depend on quality reference data. In NSRDS, the Bureau's responsibility to support American science, industry, and commerce is vitally fulfilled.

ERNEST AMBLER, *Acting Director*

Preface

The present publication is the seventh Section of a series that is being prepared in response to the increasing demand for a current revision of two sets of tables containing data on atomic spectra as derived from analyses of optical spectra.

The first set, Atomic Energy Levels, NBS Circular 467, consists of three Volumes published, respectively, in 1949, 1952 and 1958. This Circular has been reprinted as NSRDS-NBS 35, Volumes I, II and III.

The second set consists of two Multiplet Tables; one published in 1945 by the Princeton University Observatory, containing multiplets having wavelengths longer than 3000 Å; the other, An Ultraviolet Multiplet Table, NBS Circular 488, appearing in five Sections, the first in 1950, the second in 1952, and the others in 1962. The Princeton Multiplet Table was reprinted in 1972 as NSRDS-NBS 40.

The present series includes both sets of data, the energy levels and multiplet tables, as parts A and B, respectively, for selected spectra contained in Volume I of "Atomic Energy Levels." The Sections are being published at irregular intervals as revised analyses become available. A flexible paging system permits the arrangement of the various Sections by atomic number, regardless of the order in which the separate spectra are published. Section 1 includes three spectra of silicon, $Z=14$: Si II, Si III, Si IV. Section 2 contains similar data for Si I. Section 3 covers all spectra of carbon, $Z=6$: C I, C II, C III, C IV, C V, C VI. Section 4 includes the last four spectra of nitrogen, $Z=7$: N IV, N V, N VI, N VII. Section 5 completes the spectra of nitrogen, N I, N II, N III. Section 6 contains the spectra of hydrogen, $Z=1$: H I, D, T. The present Section, 7, contains the first spectrum of oxygen, $Z=8$: O I. The form of presentation of the data is described in detail in the text of Section I. All Sections are arranged identically, and the same conversion factor, cm^{-1} to eV, 0.000123981 is used throughout.

The manuscript has been prepared by Charlotte E. Moore, who has published the earlier tables. She appreciates the cordial cooperation of numerous atomic spectroscopists. She is particularly indebted to colleagues in Sweden, B. Edlén and K.B.S. Eriksson for their helpful guidance and for providing valuable data on the analysis. The splendid work of Barbara N. Somerville in typing the press copy of this difficult material is, also, gratefully acknowledged.

Washington, D.C., June 1975.

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NSRDS-NBS 3, SECTION 7

OXYGEN Z = 8

A O I Atomic Energy Levels

B O I Multiplet Table

Atomic Energy Levels

OXYGEN

Part A

O I

8 electrons

Z=8

Ground state $1s^2 2s^2 2p^4$ 3P_2

$2p^4$ 3P_2 109837.02 ± 0.06 cm $^{-1}$, 910.440 Å (Vac)

I P 13.618 eV

The classical paper on O I published in 1943 by B. Edlén has been revised and extended by K. B. S. Eriksson, H. B. S. Isberg and B. Isberg. Their publications in 1963, 1965, 1967, and 1968, have been used for the present compilation. The work of R. E. Huffman, J. C. Larrabee and Y. Tanaka is quoted for the extended absorption series observed from the ground state combinations in the ranges 122 Å to 149 Å and 666 Å to 952 Å. The paper on "Energy Spectra of Auto-Ionizing Electrons in Oxygen," by M. E. Rudd and K. Smith, also includes experimental and theoretical energy levels and transitions in these series, expressed in eV. Their observations are for the most part included by Huffman and his associates.

In 1965 Eriksson pointed out the need for a correction of -0.012 cm $^{-1}$ to selected terms in the 1963 paper by him and Isberg. This correction has been made.

The limits are from the 1968 reference.

Atomic Energy Levels

O I—Continued

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O I

O I

Configuration	Desig.	J	Level	Interval	Configuration	Desig.	J	Level	Interval
$2s^2 2p^4$	$2p^4$ 3P	2	0.000		$2s^2 2p^3(^2D_{1/2})3s$	$3s'$ $^1D^\circ$	2	102662.026	
		1	158.265	-158.265			4d	102865.506	
		0	226.977	-68.712	$2s^2 2p^3(^4S^\circ)4d$	$4d$ $^5D^\circ$	4	102865.547	-0.041
$2s^2 2p^4$	$2p^4$ 1D	2	15867.862				3	102865.606	-0.059
$2s^2 2p^4$	$2p^4$ 1S	0	33792.583				2	102865.655	-0.049
$2s^2 2p^3(^4S^\circ)3s$	$3s$ $^6S^\circ$	2	73768.200		$2s^2 2p^3(^4S^\circ)4d$	$4d$ $^3D^\circ$	3	102908.374	-0.069
$2s^2 2p^3(^4S^\circ)3s$	$3s$ $^3S^\circ$	1	76794.978				2	102908.443	-0.046
$2s^2 2p^3(^4S^\circ)3p$	$3p$ 5P	1	86625.757		$2s^2 2p^3(^4S^\circ)4f$	$4f$ 5F	5 to 1	102968.249	
		2	86627.778	2.021			4f	102968.343	
		3	86631.454	3.676	$2s^2 2p^3(^4S^\circ)4f$	$4f$ 3F	4, 3, 2	102968.343	
$2s^2 2p^3(^4S^\circ)3p$	$3p$ 3P	2	88631.146		$2s^2 2p^3(^4S^\circ)5p$	$5p$ 5P	1	103625.754	0.357
		1	88630.587	0.559			2	103626.111	0.500
		0	88631.303	-0.716			3	103626.611	
$2s^2 2p^3(^4S^\circ)4s$	$4s$ $^6S^\circ$	2	95476.728		$2s^2 2p^3(^4S^\circ)5p$	$5p$ 3P	2	103869.968	-0.060
$2s^2 2p^3(^4S^\circ)4s$	$4s$ $^3S^\circ$	1	96225.049				1	103870.028	-0.224
$2s^2 2p^3(^4S^\circ)3d$	$3d$ $^5D^\circ$	4	97420.630		$2s^2 2p^3(^4S^\circ)6s$	$6s$ $^6S^\circ$	2	105019.307	
		3	97420.716	-0.086			6s	105165.232	
		2	97420.839	-0.123	$2s^2 2p^3(^4S^\circ)6s$	$6s$ $^3S^\circ$	1	105385.354	-0.023
		1	97420.942	-0.103			3	105385.377	-0.032
		0	97420.991	-0.049	$2s^2 2p^3(^4S^\circ)5d$	$5d$ $^5D^\circ$	4	105385.409	-0.027
$2s^2 2p^3(^4S^\circ)3d$	$3d$ $^3D^\circ$	1	97488.378				2	105385.436	-0.013
		2	97488.448	0.070			1	105385.449	
		3	97488.538	0.090			0	105788.431	
$2s^2 2p^3(^4S^\circ)4p$	$4p$ 5P	1	99092.968		$2s^2 2p^3(^4S^\circ)5d$	$5d$ $^3D^\circ$	1, 2, 3	105788.595	0.164
		2	99093.641	0.673			2	105788.856	0.261
		3	99094.837	1.196	$2s^2 2p^3(^4S^\circ)5f$	$5f$ 5F	1 to 5	105788.856	
$2s^2 2p^3(^4S^\circ)4p$	$4p$ 3P	2	99681.049				4, 3, 2	105788.856	
		1	99680.968	-0.081	$2s^2 2p^3(^4S^\circ)5f$	$5f$ 3F	1	105788.856	
		0	99681.309	-0.341	$2s^2 2p^3(^4S^\circ)6p$	$6p$ 5P	1	105788.856	
$2s^2 2p^3(^2D_{1/2})3s$	$3s'$ $^3D^\circ$	3	101135.407				2	105788.856	
		2	101147.526	-12.119			3	105788.856	
		1	101155.422	-7.896	$2s^2 2p^3(^4S^\circ)6p$	$6p$ 3P	2, 1, 0	105912.031	
$2s^2 2p^3(^4S^\circ)5s$	$5s$ $^6S^\circ$	2	102116.698		$2s^2 2p^3(^4S^\circ)7s$	$7s$ $^6S^\circ$	2	106545.354	
$2s^2 2p^3(^4S^\circ)5s$	$5s$ $^3S^\circ$	1	102411.995		$2s^2 2p^3(^4S^\circ)7s$	$7s$ $^3S^\circ$	1	106627.934	

Atomic Energy Levels

O I—Continued

O I—Continued

Configuration	Desig.	<i>J</i>	Level	Interval	Configuration	Desig.	<i>J</i>	Level	Interval	
$^2\ 2p^3(4S^o)6d$	$6d$	$^5D^o$	4 3 2 1 0	106751.447 106751.458 106751.474 106751.487 106751.494	-0.011 -0.016 -0.013 -0.007	$2s^2\ 2p^3(4S^o)15d$ $2s^2\ 2p^3(4S^o)17s$ $2s^2\ 2p^3(4S^o)16d$	$15d$ $17s$ $16d$	$^3D^o$ $^3S^o$ $^3D^o$	3, 2, 1 1 3, 2, 1	109348.9 109402.4 109409.5
$^2\ 2p^3(4S^o)6d$	$6d$	$^3D^o$	3, 2, 1	106765.803		$2s^2\ 2p^3(4S^o)18s$	$18s$	$^3S^o$	1	109454.7
$^2\ 2p^3(4S^o)6f$	$6f$	6F	5 to 1	106785.160		$2s^2\ 2p^3(4S^o)17d$	$17d$	$^3D^o$	3, 2, 1	109457.6
$^2\ 2p^3(4S^o)6f$	$6f$	3F	4, 3, 2	106785.201		$2s^2\ 2p^3(4S^o)18d$	$18d$	$^3D^o$	3, 2, 1	109498.0
$^2\ 2p^3(4S^o)6g$	$6g$	$^5, ^3G^o$	6 to 2	106787.891		$2s^2\ 2p^3(4S^o)19s$	$19s$	$^3S^o$	1	109499.0
$^2\ 2p^3(4S^o)8s$	$8s$	$^6S^o$	2	107446.036		$2s^2\ 2p^3(4S^o)19d$	$19d$	$^3D^o$	3, 2, 1	109533.2
$^2\ 2p^3(4S^o)8s$	$8s$	$^3S^o$	1	107497.224		$2s^2\ 2p^3(4S^o)20s$	$20s$	$^3S^o$	1	109533.3
$^2\ 2p^3(4S^o)7d$	$7d$	$^5D^o$	4 3 2 1 0	107573.476 107573.484 107573.495 107573.504 107573.508	-0.008 -0.011 -0.009 -0.004	$2s^2\ 2p^3(4S^o)20d$ $2s^2\ 2p^3(4S^o)21s$ $2s^2\ 2p^3(4S^o)22s$	$20d$ $21s$ $22s$	$^3D^o$ $^3S^o$ $^3S^o$	3, 2, 1 1 1	109561.5 109562.3 109589.0
$^2\ 2p^3(4S^o)7d$	$7d$	$^3D^o$	3, 2, 1	107582.777		$2s^2\ 2p^3(4S^o)21d$	$21d$	$^3D^o$	3, 2, 1	109589.3
$^2\ 2p^3(4S^o)7f$	$7f$	6F	5 to 1	107595.140		$2s^2\ 2p^3(4S^o)23s$	$23s$	$^3S^o$	1	109610.5
$^2\ 2p^3(4S^o)7f$	$7f$	3F	4, 3, 2	107595.147		$2s^2\ 2p^3(4S^o)22d$	$22d$	$^3D^o$	3, 2, 1	109610.5
$^2\ 2p^3(4S^o)9s$	$9s$	$^3S^o$	1	108056.0		$2s^2\ 2p^3(4S^o)24s$	$24s$	$^3S^o$	1	109630.0
$^2\ 2p^3(4S^o)8d$	$8d$	$^5D^o$	4 3 2 1 0	108106.072 108106.077 108106.085 108106.091 108106.094	-0.005 -0.008 -0.006 -0.003	$2s^2\ 2p^3(4S^o)23d$ $2s^2\ 2p^3(4S^o)25s$ $2s^2\ 2p^3(4S^o)24d$	$23d$ $25s$ $24d$	$^3D^o$ $^3S^o$ $^3D^o$	3, 2, 1 1 3, 2, 1	109630.0 109647.7 109647.7
$^2\ 2p^3(4S^o)8d$	$8d$	$^3D^o$	3, 2, 1	108114.0		$2s^2\ 2p^3(4S^o)26s$	$26s$	$^3S^o$	1	109661.4
$^2\ 2p^3(4S^o)10s$	$10s$	$^3S^o$	1	108436.3		$2s^2\ 2p^3(4S^o)25d$	$25d$	$^3D^o$	3, 2, 1	109661.4
$^2\ 2p^3(4S^o)9d$	$9d$	$^3D^o$	3, 2, 1	108476.7		$2s^2\ 2p^3(4S^o)27s$	$27s$	$^3S^o$	1	109673.5
$^2\ 2p^3(4S^o)11s$	$11s$	$^3S^o$	1	108705.5		$2s^2\ 2p^3(4S^o)26d$	$26d$	$^3D^o$	3, 2, 1	109673.5
$^2\ 2p^3(4S^o)10d$	$10d$	$^3D^o$	3, 2, 1	108736.1		$2s^2\ 2p^3(4S^o)28s$	$28s$	$^3S^o$	1	109686.2
$^2\ 2p^3(4S^o)12s$	$12s$	$^3S^o$	1	108906.1		$2s^2\ 2p^3(4S^o)27d$	$27d$	$^3D^o$	3, 2, 1	109686.2
$^2\ 2p^3(4S^o)11d$	$11d$	$^3D^o$	3, 2, 1	108927.2		$2s^2\ 2p^3(4S^o)29s$	$29s$	$^3S^o$	1	109695.9
$^2\ 2p^3(4S^o)13s$	$13s$	$^3S^o$	1	109056.0		$2s^2\ 2p^3(4S^o)28d$	$28d$	$^3D^o$	3, 2, 1	109695.9
$^2\ 2p^3(4S^o)12d$	$12d$	$^3D^o$	3, 2, 1	109073.3		$2s^2\ 2p^3(4S^o)30s$	$30s$	$^3S^o$	1	109705.4
$^2\ 2p^3(4S^o)14s$	$14s$	$^3S^o$	1	109171.7		$2s^2\ 2p^3(4S^o)29d$	$29d$	$^3D^o$	3, 2, 1	109705.4
$^2\ 2p^3(4S^o)13d$	$13d$	$^3D^o$	3, 2, 1	109186.3		$2s^2\ 2p^3(4S^o)31s$	$31s$	$^3S^o$	1	109713.7
$^2\ 2p^3(4S^o)15s$	$15s$	$^3S^o$	1	109265.9		$2s^2\ 2p^3(4S^o)30d$	$30d$	$^3D^o$	3, 2, 1	109713.7
$^2\ 2p^3(4S^o)14d$	$14d$	$^3D^o$	3, 2, 1	109278.2	O n $2s^2\ 2p^3(4S^o)_{14}$	<i>Limit</i>				109837.02 ± .06
$^2\ 2p^3(4S^o)16s$	$16s$	$^3S^o$	1	109341.0		$2s^2\ 2p^3(^2D^o)3p$	$3p'$	1P	1	113204.445

Atomic Energy Levels

O I—Continued
O I—Continued

Configuration	Desig.	J	Level	Interval	Configuration	Desig.	J	Level	Interval	
$2s^2 2p^3(^2D^{\circ})3p$	$3p'$ 3D	3	113294.816		$2s^2 2p^3(^2P^{\circ})3p$	$3p''$ 1P	1	127667.754		
		2	113294.854	-0.038		$2s^2 2p^3(^2P^{\circ})3p$	$3p''$ 1D	2	128594.916	
		1	113298.320	-3.466		$2s^2 2p^3(^2D^{\circ})5s$	$5s'$ $^3D^{\circ}$	3	128978.8	
$2s^2 2p^3(^2D^{\circ})3p$	$3p'$ 3F	4	113714.444			$5s'$ $^3D^{\circ}$	2	128990.2	-11.4	
		3	113721.413	-6.969		$5s'$ $^3D^{\circ}$	1	128998.2	-8.0	
		2	113727.165	-5.752		$2s^2 2p^3(^2D^{\circ})5s$	$5s'$ $^1D^{\circ}$	2	129132.323	
$2s^2 2p^3(^2P^{\circ})3s$	$3s''$ $^3P^{\circ}$	2	113910.957		$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})5s$	$4d'$ $^3F^{\circ}$	4	129666.907		
		1	113921.391	-10.434		$4d'$ $^3F^{\circ}$	3			
		0	113927.534	-6.143		$4d'$ $^3F^{\circ}$	2			
$2s^2 2p^3(^2D^{\circ})3p$	$3p'$ 1F	3	113996.239		$2s^2 2p^3(^2D^{\circ})4d$	$4d'$ $^3G^{\circ}$	5	129680.522		
$2s^2 2p^3(^2P^{\circ})3s$	$3s''$ $^1P^{\circ}$	1	115918.143			$4d'$ $^3G^{\circ}$	4	129679.841	0.681	
$2s^2 2p^3(^2D^{\circ})3p$	$3p'$ 1D	2	116631.094			$4d'$ $^3G^{\circ}$	3	129693.488	-13.647	
$2s^2 2p^3(^2D^{\circ})4s$	$4s'$ $^3D^{\circ}$	3	122419.7		$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})4d$	$4d'$ $^1S^{\circ}$	0	129682.528		
		2	122433.2	-13.5		$4d'$ $^1S^{\circ}$	1	129683		
		1	122441.0	-7.8	$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})4d$	$4d'$ $^1P^{\circ}$	1			
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})4s$	$4s'$ $^1D^{\circ}$	2	122797.661		$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})4d$	$4d'$ $^3D^{\circ}$	3	129692.3	-5.2	
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})3d$	$3d'$ $^3P^{\circ}$	2	123296.777			$4d'$ $^3D^{\circ}$	2	129697.5	-5.5	
		1	123355.512	-58.735	$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})4d$	$4d'$ $^1G^{\circ}$	4	129703.0		
		0	123387.339	-31.827		$4d'$ $^1G^{\circ}$	3	129699.521		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})3d$	$3d'$ $^3F^{\circ}$	4	124213.607		$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})4d$	$4d'$ $^1D^{\circ}$	2	129731		
		3	124219.025	-5.418		$4d'$ $^1D^{\circ}$	1	129736.6		
		2	124224.118	-5.093	$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})4d$	$4d'$ $^3S^{\circ}$	1			
$2s^2 2p^3(^2D^{\circ})3d$	$3d'$ $^3G^{\circ}$	5	124240.118		$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})4d$	$4d'$ $^1F^{\circ}$	3	129737.052		
		4	124238.650	1.468		$4d'$ $^1F^{\circ}$	2			
		3	124252.926	-14.276	$2s^2 2p^3(^2D^{\circ})4f$	$4f'$ 3G	5	129777.940		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})3d$	$3d'$ $^1S^{\circ}$	0	124242.576			$4f'$ 3G	4			
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})3d$	$3d'$ $^3D^{\circ}$	3	124247.1		$2s^2 2p^3(^2D^{\circ})4f$	$4f'$ 3H	4	129779.919		
		2	124257.7	-10.6		$4f'$ 3H	5	129779.929	0.010	
		1	124264.0	-6.3	$2s^2 2p^3(^2D^{\circ})4f$	$4f'$ 3H	6			
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})3d$	$3d'$ $^1G^{\circ}$	4	124258.780		$2s^2 2p^3(^2D^{\circ})4f$	$4f'$ 1H	5	129799.831		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})3d$	$3d'$ $^1P^{\circ}$	1	124274		$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})4d$	$4d'$ $^3P^{\circ}$	2	129970.000	-9.384	
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})3d$	$3d'$ $^1D^{\circ}$	2	124319.175			$4d'$ $^3P^{\circ}$	1	129979.384	-1.169	
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})3d$	$3d'$ $^1F^{\circ}$	3	124326.779		$2s^2 2p^3(^2P^{\circ})3p$	$3p''$ 1S	0	130942.923		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})3d$	$3d'$ $^3S^{\circ}$	1	124336.3		$2s^2 2p^3(^2D^{\circ})6s$	$6s'$ $^3D^{\circ}$	3	131854.5	-11.0	
$2s^2 2p^3(^2D^{\circ})4p$	$4p'$ 3D	3	125775.493			$6s'$ $^3D^{\circ}$	2	131865.5	-10.6	
		2	125782.889	-7.396	$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})6s$	$6s'$ $^1D^{\circ}$	1	131876.1		
		1	125788.008	-5.119		$6s'$ $^1D^{\circ}$	2	131936		
$2s^2 2p^5$	$2p^5$ $^3P^{\circ}$	2	126266.896		$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})5d$	$5d'$ $^3F^{\circ}$	4	132190.671		
		1	126340.225	-73.329		$5d'$ $^3F^{\circ}$	3			
		0	126383.751	-43.526	$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})5d$	$5d'$ $^3F^{\circ}$	2			
$2s^2 2p^3(^2P^{\circ})3p$	$3p''$ 3D	3	127282.626		$2s^2 2p^3(^2D^{\circ})5d$	$5d'$ $^3G^{\circ}$	3	132198.046		
		2	127288.349	-5.723		$5d'$ $^3G^{\circ}$	4	132198.396	0.350	
		1	127291.638	-3.289		$5d'$ $^3G^{\circ}$	5			

Atomic Energy Levels

O I—Continued

O I—Continued

Configuration	Desig.	J	Level	Interval	Configuration	Desig.	J	Level	Interval
$s^2 2p^3(^2D_{2\frac{1}{2}})5d$	$5d' ^1P^o$	1	132203		$2s^2 2p^3(^2D_{2\frac{1}{2}})8d$	$8d' ^3D^o$	3, 2, 1	134919.2	
$s^2 2p^3(^2D_{2\frac{1}{2}})5d$	$5d' ^3D^o$	3	132203.4		$2s^2 2p^3(^2D_{1\frac{1}{2}})8d$	$8d' ^3S^o$	1	134919.2	
		2	132213.8	-10.4	$2s^2 2p^3(^2D_{2\frac{1}{2}})8d$	$8d' ^1P^o$	1	134921	
		1	132218.1	-4.3	$2s^2 2p^3(^2D_{1\frac{1}{2}})8d$	$8d' ^1D^o$	2	134940	
$s^2 2p^3(^2D_{1\frac{1}{2}})5d$	$5d' ^1G^o$	4	132217.679		$2s^2 2p^3(^2D_{1\frac{1}{2}})8d$	$8d' ^1F^o$	3	134940	
$s^2 2p^3(^2D_{1\frac{1}{2}})5d$	$5d' ^3S^o$	1	132232.6		$2s^2 2p^3(^2D_{1\frac{1}{2}})8d$	$8d' ^3P^o$	2	134943.8	
$s^2 2p^3(^2D_{1\frac{1}{2}})5d$	$5d' ^1D^o$	2	132235		$2s^2 2p^3(^2D_{1\frac{1}{2}})8d$	$8d' ^3P^o$	1	134947.1	-3.3
$s^2 2p^3(^2D_{1\frac{1}{2}})5d$	$5d' ^1F^o$	3	132240				0		
$s^2 2p^3(^2D_{1\frac{1}{2}})5d$	$5d' ^3P^o$	2	132311.1	-5.1	$2s^2 2p^3(^2D^o)10s$	$10s' ^3D^o$	3	135226.7	
		1	132316.2				2		
		0					1		
$s^2 2p^3(^2D^o)7s$	$7s' ^3D^o$	3	133369.8		$2s^2 2p^3(^2D_{1\frac{1}{2}})10s$	$10s' ^1D^o$	2	135252	
		2	133378.8	-9.0	$2s^2 2p^3(^2D_{2\frac{1}{2}})9d$	$9d' ^3D^o$	3, 2, 1	135283.7	
		1	133390.2	-11.4	$2s^2 2p^3(^2D_{2\frac{1}{2}})9d$	$9d' ^3S^o$	1	135283.7	
$s^2 2p^3(^2D_{1\frac{1}{2}})7s$	$7s' ^1D^o$	2	133421		$2s^2 2p^3(^2D_{1\frac{1}{2}})9d$	$9d' ^1P^o$	1	135285	
$s^2 2p^3(^2D_{2\frac{1}{2}})6d$	$6d' ^3D^o$	3, 2, 1	133566.8		$2s^2 2p^3(^2D_{2\frac{1}{2}})9d$	$9d' ^1D^o$	2	135304	
$s^2 2p^3(^2D_{2\frac{1}{2}})6d$	$6d' ^1P^o$	1	133569		$2s^2 2p^3(^2D_{1\frac{1}{2}})9d$	$9d' ^3P^o$	2	135303.5	
$s^2 2p^3(^2D_{1\frac{1}{2}})6d$	$6d' ^3S^o$	1	133577.9				1	135305.0	-1.5
$s^2 2p^3(^2D_{1\frac{1}{2}})6d$	$6d' ^1D^o$	2	133587		$2s^2 2p^3(^2D_{1\frac{1}{2}})9d$	$9d' ^1F^o$	3	135304	
$s^2 2p^3(^2D_{1\frac{1}{2}})6d$	$6d' ^1F^o$	3	133591		$2s^2 2p^3(^2D_{1\frac{1}{2}})9d$	$9d' ^3D^o$	3	135502.3	
$s^2 2p^3(^2D_{1\frac{1}{2}})6d$	$6d' ^3P^o$	2	133622.0	-4.5	$2s^2 2p^3(^2D^o)11s$	$11s' ^3D^o$	3	135541.7	
		1	133626.5				2		
		0					1		
$s^2 2p^3(^2D^o)8s$	$8s' ^3D^o$	3	134265.3		$2s^2 2p^3(^2D_{2\frac{1}{2}})10d$	$10d' ^3D^o$	3, 2, 1	135541.7	
		2	134273.4	-8.1	$2s^2 2p^3(^2D_{2\frac{1}{2}})10d$	$10d' ^3S^o$	1	135541.7	
		1	134285.1	-11.7	$2s^2 2p^3(^2D_{2\frac{1}{2}})10d$	$10d' ^1P^o$	1	135542	
$s^2 2p^3(^2D_{1\frac{1}{2}})8s$	$8s' ^1D^o$	2	134305		$2s^2 2p^3(^2D_{2\frac{1}{2}})10d$	$10d' ^1D^o$	2	135560.3	
$s^2 2p^3(^2D_{2\frac{1}{2}})7d$	$7d' ^3D^o$	3, 2, 1	134385.0		$2s^2 2p^3(^2D_{2\frac{1}{2}})10d$	$10d' ^3P^o$	2	135562.2	-1.9
$s^2 2p^3(^2D_{2\frac{1}{2}})7d$	$7d' ^1P^o$	1	134387				1	135565	
$s^2 2p^3(^2D_{1\frac{1}{2}})7d$	$7d' ^3S^o$	1	134402.5		$2s^2 2p^3(^2D_{1\frac{1}{2}})10d$	$10d' ^1D^o$	3	135565	
$s^2 2p^3(^2D_{1\frac{1}{2}})7d$	$7d' ^1D^o$	2	134409		$2s^2 2p^3(^2D_{1\frac{1}{2}})10d$	$10d' ^1F^o$	3	135565	
$s^2 2p^3(^2D_{1\frac{1}{2}})7d$	$7d' ^1F^o$	3	134409		$2s^2 2p^3(^2P^o)4s$	$4s'' ^3P^o$	2, 1, 0	[135681.7]	
$s^2 2p^3(^2D_{1\frac{1}{2}})7d$	$7d' ^3P^o$	2	134421.4	-5.1	$2s^2 2p^3(^2D^o)12s$	$12s' ^3D^o$	3	135701.8	
		1	134426.5				2		
		0					1		
$s^2 2p^3(^2D^o)9s$	$9s' ^3D^o$	3	134839.0		$2s^2 2p^3(^2D_{1\frac{1}{2}})12s$	$12s' ^1D^o$	2	135723	
		2	134843.7	-4.7	$2s^2 2p^3(^2D_{2\frac{1}{2}})11d$	$11d' ^3D^o$	3, 2, 1	135732.4	
		1			$2s^2 2p^3(^2D_{2\frac{1}{2}})11d$	$11d' ^3S^o$	1	135732.4	
$s^2 2p^3(^2D_{1\frac{1}{2}})9s$	$9s' ^1D^o$	2	134869						

Atomic Energy Levels

Or—Continued

Or—Continued

Configuration	Desig.	J	Level	Interval	Configuration	Desig.	J	Level	Interval	
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})11d$	$11d'$ $^1P^{\circ}$	1	135736		$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})16d$	$16d'$ $^3P^{\circ}$	2	136242.2		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})11d$	$11d'$ $^3P^{\circ}$	2	135752.9				1			
		1	135751.7	1.2			0			
		0			$2s^2 2p^3(^2P^{\circ})4s$	$4s''$ $^1P^{\circ}$	1	136353		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})11d$	$11d'$ $^1D^{\circ}$	2	135755		O II $2s^2 2p^3(^2D^{\circ})$	<i>Limit</i>	$2\frac{1}{2}$	136647.67		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})11d$	$11d'$ $^1F^{\circ}$	3	135755		"	<i>Limit</i>	$1\frac{1}{2}$	136667.46	-19.79	
$2s^2 2p^3(^2D^{\circ})13s$	$13s'$ $^3D^{\circ}$	3	135852.6		$2s^2 2p^3(^2P^{\circ})3d$	$3d''$ $^1D^{\circ}$	2	137928		
		2				$3d''$ $^3P^{\circ}$	2, 1, 0	137946.5		
		1			$2s^2 2p^3(^2P^{\circ})3d$	$3d''$ $^3D^{\circ}$	3, 2, 1	137962.5		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})12d$	$12d'$ $^3D^{\circ}$	3, 2, 1	135876.4		$2s^2 2p^3(^2P^{\circ})3d$	$3d''$ $^1P^{\circ}$	1	137981		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})12d$	$12d'$ $^3S^{\circ}$	1	135876.4		$2s^2 2p^3(^2P^{\circ})5s$	$5s''$ $^3P^{\circ}$	2, 1, 0	142650.5		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})12d$	$12d'$ $^1P^{\circ}$	1	135887		$2s^2 2p^3(^2P^{\circ})5s$	$5s''$ $^1P^{\circ}$	1	142743		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})12d$	$12d'$ $^3P^{\circ}$	2	135899.1		$2s^2 2p^3(^2P^{\circ})4d$	$4d''$ $^1D^{\circ}$	2	143359		
		1	135896.9	2.2		$2s^2 2p^3(^2P^{\circ})4d$	$4d''$ $^3P^{\circ}$	2, 1, 0	143363.4	
		0			$2s^2 2p^3(^2P^{\circ})4d$	$4d''$ $^3D^{\circ}$	3, 2, 1	143363.4		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})12d$	$12d'$ $^1D^{\circ}$	2	135902		$2s^2 2p^3(^2P^{\circ})4d$	$4d''$ $^1P^{\circ}$	1	143384		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})12d$	$12d'$ $^1F^{\circ}$	3	135902		$2s^2 2p^3(^2P^{\circ})4d$	$6s''$ $^3P^{\circ}$	2, 1, 0	145516.5		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})13d$	$13d'$ $^3D^{\circ}$	3, 2, 1	135986.4		$2s^2 2p^3(^2P^{\circ})6s$	$6s''$ $^1P^{\circ}$	1	145620		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})13d$	$13d'$ $^3S^{\circ}$	1	135986.4		$2s^2 2p^3(^2P^{\circ})6s$	$6s''$ $^3P^{\circ}$	2, 1, 0	145868		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})14s$	$14s'$ $^1D^{\circ}$	2	136000		$2s^2 2p^3(^2P^{\circ})5d$	$5d''$ $^1D^{\circ}$	2	145870.5		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})13d$	$13d'$ $^1P^{\circ}$	1	136000		$2s^2 2p^3(^2P^{\circ})5d$	$5d''$ $^3P^{\circ}$	2, 1, 0	145870.5		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})13d$	$13d'$ $^3P^{\circ}$	2	136011.0		$2s^2 2p^3(^2P^{\circ})5d$	$5d''$ $^3D^{\circ}$	3, 2, 1	145870.5		
		1	136011.7	-0.7		$2s^2 2p^3(^2P^{\circ})5d$	$5d''$ $^1P^{\circ}$	1	145887	
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})14d$	$14d'$ $^3D^{\circ}$	3, 2, 1	136071.3		$2s^2 2p^3(^2P^{\circ})7s$	$7s''$ $^3P^{\circ}$	2, 1, 0	147028.7		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})14d$	$14d'$ $^3S^{\circ}$	1	136071.3		$2s^2 2p^3(^2P^{\circ})7s$	$7s''$ $^1P^{\circ}$	1	147057		
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})14d$	$14d'$ $^1P^{\circ}$	1	136085		$2s^2 2p^3(^2P^{\circ})6d$	$6d''$ $^1D^{\circ}$	2	147229		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})14d$	$14d'$ $^3P^{\circ}$	2	136100.1		$2s^2 2p^3(^2P^{\circ})6d$	$6d''$ $^3P^{\circ}$	2, 1, 0	147230.1		
		1				$2s^2 2p^3(^2P^{\circ})6d$	$6d''$ $^3D^{\circ}$	3, 2, 1	147230.1	
		0				$2s^2 2p^3(^2P^{\circ})6d$	$6d''$ $^1P^{\circ}$	1	147240	
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})15d$	$15d'$ $^3D^{\circ}$	3, 2, 1	136138.9		$2s^2 2p^3(^2P^{\circ})6d$	$6d''$ $^1P^{\circ}$	2, 1, 0	147921.1		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})15d$	$15d'$ $^3S^{\circ}$	1	136138.9		$2s^2 2p^3(^2P^{\circ})8s$	$8s''$ $^3P^{\circ}$	2, 1, 0	147942		
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})15d$	$15d'$ $^3P^{\circ}$	2	136171.5		$2s^2 2p^3(^2P^{\circ})8s$	$8s''$ $^1P^{\circ}$	1	148045		
		1				$2s^2 2p^3(^2P^{\circ})7d$	$7d''$ $^1D^{\circ}$	2	148047.7	
		0				$2s^2 2p^3(^2P^{\circ})7d$	$7d''$ $^3P^{\circ}$	2, 1, 0	148047.7	
$2s^2 2p^3(^2D^{\circ}_{2\frac{1}{2}})16d$	$16d'$ $^3D^{\circ}$	3, 2, 1	136194.4			$2s^2 2p^3(^2P^{\circ})7d$	$7d''$ $^3D^{\circ}$	3, 2, 1	148047.7	
$2s^2 2p^3(^2D^{\circ}_{1\frac{1}{2}})16d$	$16d'$ $^3S^{\circ}$	1	136194.4							

Atomic Energy Levels

O I—Continued

O I—Continued

Configuration	Desig.	J	Level	Interval	Configuration	Desig.	J	Level	Interval
² 2P ³ (2P°)7d	7d'' ¹ P°	1	148058		2s ² 2P ³ (3P°)11d	11d'' ³ D°	3, 2, 1	149390.6	
² 2P ³ (2P°)9s	9s'' ³ P°	2, 1, 0	148495.5		2s ² 2P ³ (2P°)11d	11d'' ¹ D°	2	149392	
² 2P ³ (2P°)9s	9s'' ¹ P°	1	148505		2s ² 2P ³ (2P°)13s	13s'' ³ P°	2, 1, 0	149514.4	
² 2P ³ (2P°)8d	8d'' ³ P°	2, 1, 0	148576.9		2s ² 2P ³ (2P°)12d	12d'' ³ P°	2, 1, 0	149539.4	
² 2P ³ (2P°)8d	8d'' ³ D°	3, 2, 1	148576.9		2s ² 2P ³ (2P°)12d	12d'' ³ D°	3, 2, 1	149539.4	
² 2P ³ (2P°)8d	8d'' ¹ D°	2	148578		2s ² 2P ³ (2P°)14s	14s'' ³ P°	2, 1, 0	149631.8	
² 2P ³ (2P°)8d	8d'' ¹ P°	1	148582		2s ² 2P ³ (2P°)13d	13d'' ³ P°	2, 1, 0	149652.2	
² 2P ³ (2P°)10s	10s'' ³ P°	2, 1, 0	148882.9		2s ² 2P ³ (2P°)13d	13d'' ³ D°	3, 2, 1	149652.2	
² 2P ³ (2P°)10s	10s'' ¹ P°	1	148891		2s ² 2P ³ (2P°)14d	14d'' ³ P°	2, 1, 0	149744.9	
² 2P ³ (2P°)9d	9d'' ¹ D°	2	148941		2s ² 2P ³ (2P°)14d	14d'' ³ D°	3, 2, 1	149744.9	
² 2P ³ (2P°)9d	9d'' ³ P°	2, 1, 0	148945.4		2s ² 2P ³ (2P°)15d	15d'' ³ P°	2, 1, 0	149815.6	
² 2P ³ (2P°)9d	9d'' ³ D°	3, 2, 1	148945.4		2s ² 2P ³ (2P°)15d	15d'' ³ D°	3, 2, 1	149815.6	
² 2P ³ (2P°)9d	9d'' ¹ P°	1	148946		2s ² 2P ³ (2P°)17d	17d'' ³ P°	2, 1, 0	149923.7	
² 2P ³ (2P°)11s	11s'' ³ P°	2, 1, 0	149159.1		2s ² 2P ³ (2P°)17d	17d'' ³ D°	3, 2, 1	149923.7	
² 2P ³ (2P°)11s	11s'' ¹ P°	1	149168		2s ² 2P ³ (2P°)18d	18d'' ³ P°	2, 1, 0	149961.5	
² 2P ³ (2P°)10d	10d'' ³ P°	2, 1, 0	149200.6		2s ² 2P ³ (2P°)18d	18d'' ³ D°	3, 2, 1	149961.5	
² 2P ³ (2P°)10d	10d'' ³ D°	3, 2, 1	149200.6		2s ² 2P ³ (2P°)19d	19d'' ³ P°	2, 1, 0	150000.8	
² 2P ³ (2P°)10d	10d'' ¹ D°	2	149203		2s ² 2P ³ (2P°)19d	19d'' ³ D°	3, 2, 1	150000.8	
² 2P ³ (2P°)12s	12s'' ³ P°	2, 1, 0	149359.4		O II 2s ² (2P ³ 2P°)	Limit	150305.6	
² 2P ³ (2P°)11d	11d'' ³ P°	2, 1, 0	149390.6						

April 1975.

Atomic Energy Levels

O I OBSERVED TERMS

Config. $1s^2 +$	Observed Terms		
$2s^2 2p^4$	$2p^4 \ ^3P$ $\left\{ \begin{array}{l} 2p^4 \ ^1S \\ 2p^4 \ ^3S \end{array} \right.$ $2p^4 \ ^1D$		
$2s \ 2p^5$	$2p^5 \ ^3P^o$		
	$ns(n \geq 3)$		
$2s^2 2p^3(^4S^o)nl$	$\left\{ \begin{array}{l} 3-8s \ ^1S^o \\ 3-31s \ ^3S^o \end{array} \right.$	$3-6p \ ^5P$ $3-6p \ ^3P$	
$2s^2 2p^3(^2D^o)nl'$	$\left\{ \begin{array}{l} 3-13s' \ ^3D^o \\ 3-10,12,14s' \ ^1D^o \end{array} \right.$	$3p' \ ^1P$ $3,4p' \ ^3D$ $3p' \ ^1D$ $3p' \ ^3F$	
$2s^2 2p^3(^2P^o)nl''$	$\left\{ \begin{array}{l} 3,5-14s'' \ ^3P^o \\ 3-11s'' \ ^1P^o \end{array} \right.$	$3p'' \ ^1S$ $3p'' \ ^1P$	$3p'' \ ^3D$ $3p'' \ ^1D$
	$nd(n \geq 3)$		
$2s^2 2p^3(^4S^o)nl$	$3-8d \ ^5D^o$ $3-30d \ ^3D^o$		
	$3-16d' \ ^3S^o$ $3-4d' \ ^1S^o$		
$2s^2 2p^3(^2D^o)nl'$	$\left\{ \begin{array}{l} 3-16d' \ ^3S^o \\ 3-14d' \ ^1P^o \end{array} \right.$	$3-16d' \ ^3D^o$ $3-12d' \ ^1D^o$ $3-5d' \ ^3F^o$ $3-12d' \ ^1F^o$ $3-5d' \ ^1G^o$	$4-7f \ ^5F$ $4-7f \ ^3F$
$2s^2 2p^3(^2P^o)nl''$	$\left\{ \begin{array}{l} 3-15,17 \ 19d'' \ ^3P^o \\ 3-9d'' \ ^1P^o \end{array} \right.$	$3-15,17 \ 19d''' \ ^3D^o$ $3-11d''' \ ^1D^o$	$4f' \ ^3G$ $4f' \ ^3H$ $4f' \ ^1H$
	$nf(n \geq 4)$		
	$ng(n \geq 5)$		

Multiplet Table

Part B

OXYGEN

O I (Z=8)

I P 13.618 eV Limit 109837.02 \pm 0.06 cm⁻¹ 910.440 Å (Vac)

Anal A List A April 1975

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- F R. E. Huffman, J. C. Larrabee and Y. Tanaka, J. Chem. Phys. **47**, No. 11, 4462–4471 (1967). T, C L, (I); W L Absorption Series 748 Å–959 Å
B. Edlén, Kungl. Svenska Vetenskapsakad. Handlingar [3] **20**, No. 10, 31 pp. (1943). I P, T, C L; W L 748 Å–1358 Å, 2876 Å–13163 Å
- P Predicted Lines. Four-place wavelengths are quoted from references A and B and are entered with these authors as source.

New Multiplet Numbers, not inserted between older ones, start with UV 6 and 66. The Multiplet Numbers UV 6 through UV 10 in Nat. Bur. Stand. Circ. 488, Section 1, 17 (1950) have been abandoned.

m Masked

‡ Raie Ultima

* Blend

* and § Blend with Ar I

Multiplet Table

O I

O I

I A	Ref.	Int.	E P		J	Multiplet No.	I A	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Vac						
6300.304	D		0.00	1.96	2-2	$2p^4 \ ^3P - 2p^4 \ ^1D$	948.6855	A	(2)	0.00	13.07	2-	$2p^4 \ ^3P - 5d \ ^3D^\circ$
6363.776	D		0.02	1.96	1-2	1F	950.1121	A		0.02	13.07	1-	UV 12
6391.733	P		0.03	1.96	0-2		950.7327	A		0.03	13.07	0-1	
2958.365	P		0.00	4.19	2-0	$2p^4 \ ^3P - 2p^4 \ ^1S$	937.8405	A		0.00	13.22	2-1	$2p^4 \ ^3P - 7s \ ^3S^\circ$
2972.288	D		0.02	4.19	1-0	2F	939.2346	A	(2)	0.02	13.22	1-1	UV 13
Vac							939.8412	A	(2)	0.03	13.22	0-1	
1355.5977	A		0.00	9.15	2-2	$2p^4 \ ^3P - 3s \ ^5S^\circ$	936.6295	A	(3)	0.00	13.24	2-	$2p^4 \ ^3P - 6d \ ^3D^\circ$
1358.5123	A		0.02	9.15	1-2	UV 1	938.0200	A	(2)	0.02	13.24	1-	UV 14
1302.1685‡	A		0.00	9.52	2-1	$2p^4 \ ^3P - 3s \ ^3S^\circ$	930.2566	A	(2)	0.00	13.33	2-1	$2p^4 \ ^3P - 8s \ ^3S^\circ$
1304.8576	A		0.02	9.52	1-1	UV 2	931.6282	A	(2)	0.02	13.33	1-1	UV 15
1306.0286	A		0.03	9.52	0-1		932.2249	A		0.03	13.33	0-1	
1047.376	P		0.00	11.84	2-2	$2p^4 \ ^3P - 4s \ ^5S^\circ$	929.5168	A	(3)	0.00	13.34	2-	$2p^4 \ ^3P - 7d \ ^3D^\circ$
1049.115	P		0.02	11.84	1-2	UV 2.01	930.8862	A	(2)	0.02	13.34	1-	UV 16
1039.2304	A		0.00	11.93	2-1	$2p^4 \ ^3P - 4s \ ^3S^\circ$	925.442	E	(2)	0.00	13.40	2-1	$2p^4 \ ^3P - 9s \ ^3S^\circ$
1040.9425	A		0.02	11.93	1-1	UV 3	926.809	E	(2)	0.02	13.40	1-1	UV 17
1041.6876	A		0.03	11.93	0-1		927.394	P		0.03	13.40	0-1	
1026.476	P		0.00	12.08	2-3	$2p^4 \ ^3P - 3d \ ^5D^\circ$	924.952	E	(2)	0.00	13.40	2-	$2p^4 \ ^3P - 8d \ ^3D^\circ$
1028.145	P		0.02	12.08	1-2	UV 3.01	926.295	E	(3)	0.02	13.40	1-	UV 18
1028.870	P		0.03	12.08	0-1		926.903	E	(2)	0.03	13.40	0-1	
1025.7618	A		0.00	12.09	2-	$2p^4 \ ^3P - 3d \ ^3D^\circ$	922.200	E	(2)	0.00	13.44	2-1	$2p^4 \ ^3P - 10s \ ^3S^\circ$
1027.4307	A		0.02	12.09	1-	UV 4	923.549	P		0.02	13.44	1-1	UV 19
1028.1571	A		0.03	12.09	0-1		924.135	P		0.03	13.44	0-1	
988.7734	A		0.00	12.54	2-3	$2p^4 \ ^3P - 3s' \ ^3D^\circ$	921.860	E	(3)	0.00	13.45	2-	$2p^4 \ ^3P - 9d \ ^3D^\circ$
990.2043	A		0.02	12.54	1-2	UV 5	923.200	E	(3)	0.02	13.45	1-	UV 20
990.8010	A		0.03	12.54	0-1		923.790	P		0.03	13.45	0-1	
988.6549	A		0.00	12.54	2-2		919.908	E	(2)	0.00	13.48	2-1	$2p^4 \ ^3P - 11s \ ^3S^\circ$
990.1269	A		0.02	12.54	1-1		921.247	E	(1)	0.02	13.48	1-1	UV 21
988.5778	A		0.00	12.54	2-1		921.860	E	(3)	0.03	13.48	0-1	
979.272	P		0.00	12.66	2-2	$2p^4 \ ^3P - 5s \ ^5S^\circ$	919.658	E	(3)	0.00	13.48	2-	$2p^4 \ ^3P - 10d \ ^3D^\circ$
980.792	P		0.02	12.66	1-2	UV 6	921.005	E	(3)	0.02	13.48	1-	UV 22
976.4481	A		0.00	12.70	2-1	$2p^4 \ ^3P - 5s \ ^3S^\circ$	921.575	E	(1)	0.03	13.48	0-1	
977.9594	A		0.02	12.70	1-1	UV 7	918.221	E	(2)	0.00	13.50	2-1	$2p^4 \ ^3P - 12s \ ^3S^\circ$
978.6170	A		0.03	12.70	0-1		919.559	E	(2)	0.02	13.50	1-1	UV 23
974.070	P		0.00	12.73	2-2	$2p^4 \ ^3P - 3s' \ ^1D^\circ$	918.039	E	(3)	0.00	13.50	2-	$2p^4 \ ^3P - 11d \ ^3D^\circ$
975.574	P		0.02	12.73	1-2	UV 8	919.376	E	(2)	0.02	13.50	1-	UV 24
972.143	P		0.00	12.75	2-3	$2p^4 \ ^3P - 4d \ ^5D^\circ$	919.971	E	(1)	0.03	13.50	0-1	
973.640	P		0.02	12.75	1-2	UV 9	916.960	E	(2)	0.00	13.52	2-1	$2p^4 \ ^3P - 13s \ ^3S^\circ$
974.292	P		0.03	12.75	0-1		918.293	P		0.02	13.52	1-1	UV 25
971.7381	A		0.00	12.76	2-	$2p^4 \ ^3P - 4d \ ^3D^\circ$	916.816	E	(3)	0.00	13.52	2-	$2p^4 \ ^3P - 12d \ ^3D^\circ$
973.2342	A		0.02	12.76	1-	UV 10	918.149	E	(2)	0.02	13.52	1-	UV 26
973.8852	A		0.03	12.76	0-1		918.724	E	(1)	0.03	13.52	0-1	
950.8846	A	(3)	0.00	13.04	2-1	$2p^4 \ ^3P - 6s \ ^3S^\circ$	915.991	E	(2)	0.00	13.54	2-1	$2p^4 \ ^3P - 14s \ ^3S^\circ$
952.3178	A	(1)	0.02	13.04	1-1	UV 11	917.315	E	(2)	0.02	13.54	1-1	UV 27
952.9413	A	(1)	0.03	13.04	0-1								

Multiplet Table

O I—Continued

O I—Continued

IA	Ref.	Int.	EP		J	Multiplet No.	IA	Ref.	Int.	EP		J	Multiplet No.
			Low	High						Low	High		
Vac							Vac						
915.877	E	(3)	0.00	13.54	2-	2p ⁴ ³P -13d ³D°	*912.318	E	(3)	0.00	13.59	2-	2p ⁴ ³P -22d ³D°
917.185	E	(2)	0.02	13.54	1-	UV 28	913.644	E	(3)	0.02	13.59	1-	UV 46
915.199	E	(1)	0.00	13.55	2-1	2p ⁴ ³P -15s ³S°	*912.155	E	(3)	0.00	13.59	2-1	2p ⁴ ³P -24s ³S°
916.526	P		0.02	13.55	1-1	UV 29	913.483	E	(3)	0.02	13.59	1-	UV 47
915.100	E	(2)	0.00	13.55	2-	2p ⁴ ³P -14d ³D°	*912.155	E	(3)	0.00	13.59	2-	2p ⁴ ³P -23d ³D°
916.420	E	(3)	0.02	13.55	1-	UV 30	913.483	E	(3)	0.02	13.59	1-	UV 48
916.960	E	(2)	0.03	13.55	0-1		*912.012	E	(3)	0.00	13.59	2-1	2p ⁴ ³P -25s ³S°
914.588	E	(3)	0.00	13.56	2-1	2p ⁴ ³P -16s ³S°	*912.012	E	(3)	0.00	13.59	2-	2p ⁴ ³P -24d ³D°
915.877	E	(3)	0.02	13.56	1-1	UV 31	*911.898	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -26s ³S°
914.513	E	(3)	0.00	13.56	2-	2p ⁴ ³P -15d ³D°	*911.898	E	(2)	0.00	13.60	2-	2p ⁴ ³P -26s ³S°
915.821	E	(3)	0.02	13.56	1-	UV 32	*911.898	E	(2)	0.00	13.60	2-	2p ⁴ ³P -25d ³D°
914.057	E	(1)	0.00	13.56	2-1	2p ⁴ ³P -17s ³S°	*911.898	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -25d ³D°
915.381	P		0.02	13.56	1-1	UV 33	*911.786	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -27s ³S°
913.997	E	(4)	0.00	13.56	2-	2p ⁴ ³P -16d ³D°	*911.786	E	(2)	0.00	13.60	2-	2p ⁴ ³P -26d ³D°
915.321	E	(2)	0.02	13.56	1-	UV 34	*911.786	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -27s ³S°
913.644	E	(3)	0.00	13.57	2-1	2p ⁴ ³P -18s ³S°	*911.786	E	(2)	0.00	13.60	2-	2p ⁴ ³P -26d ³D°
*914.918	E	(2)	0.02	13.57	1-1	UV 35	*911.786	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -28s ³S°
913.590	E	(3)	0.00	13.57	2-	2p ⁴ ³P -17d ³D°	913.127	E	(2)	0.02	13.60	1-	UV 54
*914.918	E	(2)	0.02	13.57	1-	UV 36	*911.692	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -28s ³S°
915.499	E	(1)	0.03	13.57	0-1		*911.692	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -28s ³S°
*913.250	E	(4)	0.00	13.58	2-	2p ⁴ ³P -18d ³D°	*911.692	E	(2)	0.00	13.60	2-	2p ⁴ ³P -27d ³D°
914.588	E	(3)	0.02	13.58	1-	UV 37	*911.692	E	(2)	0.00	13.60	2-	2p ⁴ ³P -28d ³D°
915.199	E	(1)	0.03	13.58	0-1		*911.692	E	(2)	0.00	13.60	2-	2p ⁴ ³P -28d ³D°
*913.250	E	(4)	0.00	13.58	2-1	2p ⁴ ³P -19s ³S°	*911.611	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -29s ³S°
*912.964	E	(4)	0.00	13.58	2-	2p ⁴ ³P -19d ³D°	*911.611	E	(2)	0.00	13.60	2-	2p ⁴ ³P -28d ³D°
914.293	E	(2)	0.02	13.58	1-	UV 39	*911.611	E	(2)	0.00	13.60	2-	2p ⁴ ³P -28d ³D°
914.854	E	(1)	0.03	13.58	0-1		*911.538	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -30s ³S°
*912.964	E	(4)	0.00	13.58	2-1	2p ⁴ ³P -20s ³S°	*911.538	E	(2)	0.00	13.60	2-1	2p ⁴ ³P -29d ³D°
*912.723	E	(4)	0.00	13.58	2-	2p ⁴ ³P -20d ³D°	912.843	E	(3)	0.02	13.60	1-	UV 60
914.057	E	(3)	0.02	13.58	1-	UV 41	*911.463	E	(1)	0.00	13.60	2-1	2p ⁴ ³P -31s ³S°
*912.723	E	(4)	0.00	13.58	2-1	2p ⁴ ³P -21s ³S°	*911.463	E	(1)	0.00	13.60	2-	2p ⁴ ³P -30d ³D°
*912.500	E	(3)	0.00	13.59	2-1	2p ⁴ ³P -22s ³S°	877.8787	A	(7)	0.00	14.12	2-2	2p ⁴ ³P -3s'' ³P°
*912.500	E	(3)	0.00	13.59	2-	2p ⁴ ³P -21d ³D°	879.0194	A	(4)	0.02	14.12	1-1	UV 63
913.815	E	(3)	0.02	13.59	1-	UV 44	877.7983	A	(8)	0.00	14.12	2-1	
*912.318	E	(3)	0.00	13.59	2-1	2p ⁴ ³P -23s ³S°	878.9720	A	(4)	0.02	14.12	1-0	
						UV 45	879.1001	A	(4)	0.02	14.12	1-2	
							879.5507	A	(5)	0.03	14.12	0-1	

Multiplet Table

O I—Continued

O I—Continued

IA	Ref.	Int.	E P		J	Multiplet No.	IA	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Vac							Vac						
862.678	P		0.00	14.37	2-1	$2p^4 \ ^3P - 3s'' \ ^1P^\circ$	756.410	E	(6)	0.00	16.39	2-3	$2p^4 \ ^3P - 5d' \ ^3D^\circ$
863.857	P		0.02	14.37	1-1	UV 64	757.254	E	(4)	0.02	16.39	1-2	UV 75
864.370	P		0.03	14.37	0-1		757.627	E	(3)	0.03	16.39	0-1	
							756.354	E	(5)	0.00	16.39	2-2	
816.862	E	(9)	0.00	15.18	2-3	$2p^4 \ ^3P - 4s' \ ^3D^\circ$							
817.835	E	(7)	0.02	15.18	1-2	UV 65	756.243	E	(6)	0.00	16.39	2-1	$2p^4 \ ^3P - 5d' \ ^3S^\circ$
818.236	E	(7)	0.03	15.18	0-1		*757.149	E	(3)	0.02	16.39	1-1	UV 76
816.766	E	(9)	0.00	15.18	2-2								
817.777	E	(7)	0.02	15.18	1-1		755.790	E	(6)	0.00	16.40	2-2	$2p^4 \ ^3P - 5d' \ ^3P^\circ$
							756.676	E	(4)	0.02	16.40	1-	UV 77
811.0512	A		0.00	15.29	2-2	$2p^4 \ ^3P - 3d' \ ^3P^\circ$	756.704	E	(3)	0.02	16.40	1-2	
811.7064	A		0.02	15.29	1-1	UV 66	757.059	E	(3)	0.03	16.40	0-1	
810.6650	A		0.00	15.29	2-1								
811.4968	A		0.02	15.30	1-0		749.795	E	(3)	0.00	16.54	2-3	$2p^4 \ ^3P - 7s' \ ^3D^\circ$
812.0936	A		0.02	15.29	1-2		750.637	E	(3)	0.02	16.54	1-2	UV 78
812.1594	A		0.03	15.29	0-1		750.956	E	(3)	0.03	16.54	0-1	
							749.742	E	(3)	0.00	16.54	2-2	
804.848	E	(7)	0.00	15.40	2-3	$2p^4 \ ^3P - 3d' \ ^3D^\circ$	750.573	E	(2)	0.02	16.54	1-1	
805.810	E	(8)	0.02	15.41	1-2	UV 67							
806.231	E	(4)	0.03	15.41	0-1		748.680	E	(5)	0.00	16.56	2-3	$2p^4 \ ^3P - 6d' \ ^3D^\circ$
804.775	E	(6)	0.00	15.41	2-2		749.586	E	(3)	0.02	16.56	1-2	UV 79
805.745	E	(3)	0.02	15.41	1-1								
							748.632	E	(5)	0.00	16.56	2-1	$2p^4 \ ^3P - 6d' \ ^3S^\circ$
804.267	E	(9)	0.00	15.42	2-1	$2p^4 \ ^3P - 3d' \ ^3S^\circ$	749.517	E	(3)	0.02	16.56	1-1	UV 80
805.295	E	(7)	0.02	15.42	1-1	UV 68	749.894	E	(2)	0.03	16.56	0-1	
805.745	E	(3)	0.03	15.42	0-1								
							748.380	E	(6)	0.00	16.57	2-2	$2p^4 \ ^3P - 6d' \ ^3P^\circ$
791.9732	A	(7)	0.00	15.65	2-2	$2p^4 \ ^3P - 2p^5 \ ^3P^\circ$	749.253	E	(6)	0.02	16.57	1-	UV 81
792.5063	A	(4)	0.02	15.66	1-1	UV 69	749.628	E	(3)	0.03	16.57	0-1	
791.5136	A	(5)	0.00	15.66	2-1								
792.2330	A	(4)	0.02	15.67	1-0		*744.794	E	(7)	0.00	16.65	2-3	$2p^4 \ ^3P - 8s' \ ^3D^\circ$
792.9671	A	(6)	0.02	15.65	1-2		745.628	E	(2)	0.02	16.65	1-2	UV 82
792.9381	A	(6)	0.03	15.66	0-1		745.945	E	(2)	0.03	16.65	0-1	
775.321	E	(7)	0.00	15.99	2-3	$2p^4 \ ^3P - 5s' \ ^3D^\circ$	744.128	E	(5)	0.00	16.66	2-	$2p^4 \ ^3P - 7d' \ ^3D^\circ$
776.206	E	(5)	0.02	15.99	1-2	UV 70	745.011	E	(3)	0.02	16.66	1-	UV 83
776.569	E	(4)	0.03	15.99	0-1								
775.252	E	(6)	0.00	15.99	2-2		744.051	E	(6)	0.00	16.66	2-1	$2p^4 \ ^3P - 7d' \ ^3S^\circ$
776.159	E	(5)	0.02	15.99	1-1		744.899	E	(3)	0.02	16.66	1-1	UV 84
							745.287	E	(2)	0.03	16.66	0-1	
771.056	E	(9)	0.00	16.08	2-3	$2p^4 \ ^3P - 4d' \ ^3D^\circ$							
771.967	E	(6)	0.02	16.08	1-2	UV 71	743.929	E	(5)	0.00	16.67	2-2	$2p^4 \ ^3P - 7d' \ ^3P^\circ$
772.344	E	(4)	0.03	16.08	0-1		*744.794	E	(7)	0.02	16.67	1-	UV 85
							745.159	E	(3)	0.03	16.67	0-1	
770.793	E	(7)	0.00	16.08	2-1	$2p^4 \ ^3P - 4d' \ ^3S^\circ$							
771.729	E	(5)	0.02	16.08	1-1	UV 72	741.625	E	(4)	0.00	16.72	2-3	$2p^4 \ ^3P - 9s' \ ^3D^\circ$
772.147	E	(2)	0.03	16.08	0-1		742.471	E	(2)	0.02	16.72	1-2	UV 86
769.4083	A		0.00	16.11	2-2	$2p^4 \ ^3P - 4d' \ ^3P^\circ$	*741.177	E	(6)	0.00	16.73	2-	$2p^4 \ ^3P - 8d' \ ^3D^\circ$
770.2907	A		0.02	16.11	1-1	UV 73	*742.062	E	(3)	0.02	16.73	1-	UV 87
769.3528	A		0.00	16.11	2-1								
770.2600	A		0.02	16.12	1-0		*741.177	E	(6)	0.00	16.73	2-1	$2p^4 \ ^3P - 8d' \ ^3S^\circ$
770.3464	A		0.02	16.11	1-2		*742.062	E	(3)	0.02	16.73	1-1	UV 88
*770.6986	A		0.03	16.11	0-1								
							741.055	E	(5)	0.00	16.73	2-2	$2p^4 \ ^3P - 8d' \ ^3P^\circ$
758.412	E	(5)	0.00	16.35	2-3	$2p^4 \ ^3P - 6s' \ ^3D^\circ$	741.914	E	(4)	0.02	16.73	1-	UV 89
759.262	E	(4)	0.02	16.35	1-2	UV 74	742.280	E	(3)	0.03	16.73	0-1	
759.593	E	(3)	0.03	16.35	0-1								
758.347	E	(4)	0.00	16.35	2-2		739.499	E	(3)	0.00	16.77	2-3	$2p^4 \ ^3P - 10s' \ ^3D^\circ$
759.200	E	(3)	0.02	16.35	1-1								UV 90

Multiplet Table

O I—Continued

O I—Continued

I A	Ref.	Int.	E P		J	Multiplet No.	I A	Ref.	Int.	E P		J	Multiplet No.	
			Low	High						Low	High			
Vac							Vac							
*739.188	E	(5)	0.00	16.77	2-	$2p^4 \ ^3P - 9d'' \ ^3D^\circ$	*734.913	E	(4)	0.00	16.87	2-	$2p^4 \ ^3P - 14d'' \ ^3D^\circ$	
*740.053	E	(3)	0.02	16.77	1-	UV 91	*735.760	E	(2)	0.02	16.87	1-	UV 110	
*739.188	E	(5)	0.00	16.77	2-1	$2p^4 \ ^3P - 9d'' \ ^3S^\circ$	*734.913	E	(4)	0.00	16.87	2-1	$2p^4 \ ^3P - 14d'' \ ^3S^\circ$	
*740.053	E	(3)	0.02	16.77	1-1	UV 92	*735.760	E	(2)	0.02	16.87	1-1	UV 111	
739.085	E	(4)	0.00	16.78	2-2	$2p^4 \ ^3P - 9d'' \ ^3P^\circ$	734.746	E	(2)	0.00	16.87	2-	$2p^4 \ ^3P - 14d'' \ ^3P^\circ$	
739.940	E	(4)	0.02	16.78	1-	UV 93	735.616	E	(3)	0.02	16.87	1-	UV 112	
740.313	E	(0)	0.03	16.78	0-1		*734.544	E	(3)	0.00	16.88	2-	$2p^4 \ ^3P - 15d'' \ ^3D^\circ$	
737.995	E	(3)	0.00	16.80	2-3	$2p^4 \ ^3P - 11s' \ ^3D^\circ$	UV 94	*734.544	E	(3)	0.00	16.88	2-1	$2p^4 \ ^3P - 15d'' \ ^3S^\circ$
*737.779	E	(5)	0.00	16.80	2-	$2p^4 \ ^3P - 10d'' \ ^3D^\circ$	UV 95	734.368	E	(2)	0.00	16.88	2-2	$2p^4 \ ^3P - 15d'' \ ^3P^\circ$
*738.644	E	(3)	0.02	16.80	1-			*734.251	E	(3)	0.00	16.89	2-	$2p^4 \ ^3P - 16d'' \ ^3D^\circ$
*737.779	E	(5)	0.00	16.80	2-1	$2p^4 \ ^3P - 10d'' \ ^3S^\circ$	UV 96	*735.092	E	(2)	0.02	16.89	1-	UV 116
*738.644	E	(3)	0.02	16.80	1-1			*734.251	E	(3)	0.00	16.89	2-1	$2p^4 \ ^3P - 16d'' \ ^3S^\circ$
737.683	E	(3)	0.00	16.81	2-2	$2p^4 \ ^3P - 10d'' \ ^3P^\circ$	UV 97	*735.092	E	(2)	0.02	16.89	1-1	UV 117
738.537	E	(4)	0.02	16.81	1-			733.987	E	(2)	0.00	16.89	2-2	$2p^4 \ ^3P - 16d'' \ ^3P^\circ$
738.906	E	(2)	0.03	16.81	0-1			724.932	E	(5)	0.00	17.10	2-	$2p^4 \ ^3P - 3d'' \ ^3P^\circ$
737.019	E	(2)	0.00	16.82	2-	$2p^4 \ ^3P - 4s'' \ ^3P^\circ$	UV 98	725.748	E	(4)	0.02	17.10	1-	UV 119
736.910	E	(3)	0.00	16.82	2-3	$2p^4 \ ^3P - 12s' \ ^3D^\circ$	UV 99	726.104	E	(3)	0.03	17.10	0-1	
*736.734	E	(5)	0.00	16.83	2-	$2p^4 \ ^3P - 11d'' \ ^3D^\circ$	UV 100	724.830	E	(6)	0.00	17.10	2-	$2p^4 \ ^3P - 3d'' \ ^3D^\circ$
*737.614	E	(3)	0.02	16.83	1-			725.665	E	(5)	0.02	17.10	1-	UV 120
*736.734	E	(5)	0.00	16.83	2-1	$2p^4 \ ^3P - 11d'' \ ^3S^\circ$	UV 101	726.035	E	(3)	0.03	17.10	0-1	
736.629	E	(3)	0.00	16.83	2-	$2p^4 \ ^3P - 11d'' \ ^3P^\circ$	UV 102	701.014	E	(2)	0.00	17.69	2-	$2p^4 \ ^3P - 5s'' \ ^3P^\circ$
737.495	E	(4)	0.02	16.83	1-			697.532	E	(6)	0.00	17.77	2-	$2p^4 \ ^3P - 4d'' \ ^3P^\circ$
737.873	E	(3)	0.03	16.83	0-1			698.297	E	(4)	0.02	17.77	1-	UV 121
736.092	E	(3)	0.00	16.84	2-3	$2p^4 \ ^3P - 13s' \ ^3D^\circ$	UV 103	698.631	E	(3)	0.03	17.77	0-1	
*735.960	E	(4)	0.00	16.85	2-	$2p^4 \ ^3P - 12d'' \ ^3D^\circ$	UV 104	687.202	E	(4)	0.00	18.04	2-	$2p^4 \ ^3P - 6s'' \ ^3P^\circ$
*736.824	E	(3)	0.02	16.85	1-			687.997	E	(2)	0.02	18.04	1-	UV 123
*735.960	E	(4)	0.00	16.85	2-1	$2p^4 \ ^3P - 12d'' \ ^3S^\circ$	UV 105	688.245	E	(2)	0.03	18.04	0-	
*736.824	E	(3)	0.02	16.85	1-1			685.544	E	(7)	0.00	18.09	2-	$2p^4 \ ^3P - 5d'' \ ^3P^\circ$
735.840	E	(2)	0.00	16.85	2-	$2p^4 \ ^3P - 12d'' \ ^3P^\circ$	UV 106	686.284	E	(5)	0.02	18.09	1-	UV 124
737.083	E	(3)	0.03	16.85	0-1			686.603	E	(3)	0.03	18.09	0-1	
*735.367	E	(4)	0.00	16.86	2-	$2p^4 \ ^3P - 13d'' \ ^3D^\circ$	UV 107	680.146	E	(2)	0.00	18.23	2-	$2p^4 \ ^3P - 7s'' \ ^3P^\circ$
*736.225	E	(3)	0.02	16.86	1-			680.866	E	(2)	0.02	18.23	1-	UV 125
*735.367	E	(4)	0.00	16.86	2-1	$2p^4 \ ^3P - 13d'' \ ^3S^\circ$	UV 108	679.202	E	(4)	0.00	18.25	2-	$2p^4 \ ^3P - 6d'' \ ^3P^\circ$
*736.225	E	(3)	0.02	16.86	1-1			679.948	E	(4)	0.02	18.25	1-	UV 126
735.234	E	(3)	0.00	16.86	2-	$2p^4 \ ^3P - 13d'' \ ^3P^\circ$	UV 109	680.256	E	(2)	0.03	18.25	0-1	
736.092	E	(3)	0.02	16.86	1-			676.033	E	(2)	0.00	18.34	2-	$2p^4 \ ^3P - 8s'' \ ^3P^\circ$
736.460	E	(2)	0.03	16.86	0-1			676.763	E	(1)	0.02	18.34	1-	UV 127

Multiplet Table

O I—Continued

O I—Continued

IA	Ref.	Int.	E P		J	Multiplet No.	IA	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Vac													
675.463	E	(5)	0.00	18.36	2-	$2p^4 \ ^3P - 7d'' \ ^3P^\circ$	1641.305	P		1.96	9.52	2-1	$2p^4 \ ^1D - 3s \ ^3S^\circ$ UV 146
676.183	E	(3)	0.02	18.36	1-	UV 128 $\ ^3D^\circ$							
676.487	E	(2)	0.03	18.36	0-1		1240.377	P		1.96	12.09	2-3	$2p^4 \ ^1D - 3d \ ^3D^\circ$ UV 147
673.421	E	(2)	0.00	18.41	2-	$2p^4 \ ^3P - 9s'' \ ^3P^\circ$ UV 129	1240.378	P		1.96	12.09	2-2	
673.052	E	(5)	0.00	18.42	2-	$2p^4 \ ^3P - 8d'' \ ^3P^\circ$ UV 130 $\ ^3D^\circ$	1152.1512	A		1.96	12.73	2-2	$2p^4 \ ^1D - 3s' \ ^1D^\circ$ UV 148
671.669	E	(2)	0.00	18.46	2-	$2p^4 \ ^3P - 10s'' \ ^3P^\circ$ UV 131	999.4974	A		1.96	14.37	2-1	$2p^4 \ ^1D - 3s'' \ ^1P^\circ$ UV 149
671.406	E	(5)	0.00	18.47	2-	$2p^4 \ ^3P - 9d'' \ ^3P^\circ$	935.1930	A	(9)	1.96	15.22	2-2	$2p^4 \ ^1D - 4s' \ ^1D^\circ$ UV 150
672.090	E	(3)	0.02	18.47	1-	UV 132 $\ ^3D^\circ$							
672.404	E	(2)	0.03	18.47	0-1		922.46	F	(2)	1.96	15.41	2-1	$2p^4 \ ^1D - 3d' \ ^1P^\circ$ UV 151
*670.425	E	(2)	0.00	18.49	2-	$2p^4 \ ^3P - 11s'' \ ^3P^\circ$ UV 133	922.0727	A	(4)	1.96	15.41	2-2	$2p^4 \ ^1D - 3d' \ ^1D^\circ$ UV 152
670.237	E	(4)	0.00	18.50	2-	$2p^4 \ ^3P - 10d'' \ ^3P^\circ$	922.0081	A	(8)	1.96	15.41	2-3	$2p^4 \ ^1D - 3d' \ ^1F^\circ$ UV 153
670.952	E	(3)	0.02	18.50	1-	UV 134 $\ ^3D^\circ$	882.8895	A	(6)	1.96	16.01	2-2	$2p^4 \ ^1D - 5s' \ ^1D^\circ$ UV 154
669.526	E	(2)	0.00	18.52	2-	$2p^4 \ ^3P - 12s'' \ ^3P^\circ$ UV 135	878.62	F	(0)	1.96	16.08	2-1	$2p^4 \ ^1D - 4d' \ ^1P^\circ$ UV 155
669.371	E	(4)	0.00	18.52	2-	$2p^4 \ ^3P - 11d'' \ ^3P^\circ$	878.25	F	(3)	1.96	16.08	2-2	$2p^4 \ ^1D - 4d' \ ^1D^\circ$ UV 156
670.091	E	(2)	0.02	18.52	1-	UV 136 $\ ^3D^\circ$	878.2007	A	(4)	1.96	16.08	2-3	$2p^4 \ ^1D - 4d' \ ^1F^\circ$ UV 157
*670.425	E	(2)	0.03	18.52	0-1		861.56	F	(6)	1.96	16.36	2-2	$2p^4 \ ^1D - 6s' \ ^1D^\circ$ UV 158
668.832	E	(1)	0.00	18.54	2-	$2p^4 \ ^3P - 13s'' \ ^3P^\circ$ UV 137	859.59	F	(1)	1.96	16.39	2-1	$2p^4 \ ^1D - 5d' \ ^1P^\circ$ UV 159
668.720	E	(4)	0.00	18.54	2-	$2p^4 \ ^3P - 12d'' \ ^3P^\circ$	859.35	F	(3)	1.96	16.39	2-2	$2p^4 \ ^1D - 5d' \ ^1D^\circ$ UV 160
668.307	E	(1)	0.00	18.55	2-	$2p^4 \ ^3P - 14s'' \ ^3P^\circ$ UV 139	859.31	F	(4)	1.96	16.40	2-3	$2p^4 \ ^1D - 5d' \ ^1F^\circ$ UV 161
668.211	E	(3)	0.00	18.55	2-	$2p^4 \ ^3P - 13d'' \ ^3P^\circ$	850.68	F	(2)	1.96	16.54	2-2	$2p^4 \ ^1D - 7s' \ ^1D^\circ$ UV 162
668.928	F	(1)	0.02	18.55	1-	UV 140 $\ ^3D^\circ$	849.61	F	(2)	1.96	16.56	2-1	$2p^4 \ ^1D - 6d' \ ^1P^\circ$ UV 163
668.509	E	(2)	0.02	18.57	1-	$2p^4 \ ^3P - 14d'' \ ^3P^\circ$ UV 141 $\ ^3D^\circ$	849.48	F	(1)	1.96	16.56	2-2	$2p^4 \ ^1D - 6d' \ ^1D^\circ$ UV 164
667.487	E	(3)	0.00	18.57	2-	$2p^4 \ ^3P - 15d'' \ ^3P^\circ$ UV 142 $\ ^3D^\circ$							
667.006	E	(3)	0.00	18.59	2-	$2p^4 \ ^3P - 17d'' \ ^3P^\circ$ UV 143 $\ ^3D^\circ$							
666.838	E	(2)	0.00	18.59	2-	$2p^4 \ ^3P - 18d'' \ ^3P^\circ$ UV 144 $\ ^3D^\circ$							
666.663	E	(1)	0.00	18.60	2-	$2p^4 \ ^3P - 19d'' \ ^3P^\circ$ UV 145 $\ ^3D^\circ$							
Air	D		1.96	4.19	2-0	$2p^4 \ ^1D - 2p^4 \ ^1S$ $3F$	849.48	F	(1)	1.96	16.56	2-2	$2p^4 \ ^1D - 6d' \ ^1D^\circ$ UV 164
5577.339													

Multiplet Table

O I—Continued

O I—Continued

I A	Ref.	Int.	E P		J	Multiplet No.	I A	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 849.45	F	(0)	1.96	16.56	2-3	$2p^4 \ ^1D - 6d' \ ^1F^\circ$ UV 165	Vac *832.42	F	(0)	1.96	16.86	2-1	$2p^4 \ ^1D - 13d' \ ^1P^\circ$ UV 186
844.53	F	(0)	1.96	16.65	2-2	$2p^4 \ ^1D - 8s' \ ^3D^\circ$ UV 166	831.83	F	(0)	1.96	16.87	2-1	$2p^4 \ ^1D - 14d' \ ^1P^\circ$ UV 187
844.33	F	(0)	1.96	16.65	2-2	$2p^4 \ ^1D - 8s' \ ^1D^\circ$ UV 167	829.98	F	(1)	1.96	16.91	2-1	$2p^4 \ ^1D - 4s'' \ ^1P^\circ$ UV 188
843.75	F	(1)	1.96	16.66	2-1	$2p^4 \ ^1D - 7d' \ ^1P^\circ$ UV 168	819.27	F	(3)	1.96	17.10	2-2	$2p^4 \ ^1D - 3d'' \ ^1D^\circ$ UV 189
843.59	F	(1)	1.96	16.66	2-2	$2p^4 \ ^1D - 7d' \ ^1D^\circ$ -3 UV 169	788.18	F	(1)	1.96	17.70	2-1	$2p^4 \ ^1D - 5s'' \ ^1P^\circ$ UV 190
840.49	F	(0)	1.96	16.72	2-2	$2p^4 \ ^1D - 9s' \ ^3D^\circ$ UV 170	784.37	F	(2)	1.96	17.77	2-2	$2p^4 \ ^1D - 4d'' \ ^1D^\circ$ UV 191
840.33	F	(0)	1.96	16.72	2-2	$2p^4 \ ^1D - 9s' \ ^1D^\circ$ UV 171	*770.70	F	(2)	1.96	18.05	2-1	$2p^4 \ ^1D - 6s'' \ ^1P^\circ$ UV 192
839.96	F	(1)	1.96	16.73	2-1	$2p^4 \ ^1D - 8d' \ ^1P^\circ$ UV 172	769.23	F	(2)	1.96	18.08	2-2	$2p^4 \ ^1D - 5d'' \ ^1D^\circ$ UV 193
839.83	F	(1)	1.96	16.73	2-2	$2p^4 \ ^1D - 8d' \ ^1D^\circ$ -3 UV 173	762.26	F	(1)	1.96	18.23	2-1	$2p^4 \ ^1D - 7s'' \ ^1P^\circ$ UV 194
837.76	F	(0)	1.96	16.77	2-2	$2p^4 \ ^1D - 10s' \ ^3D^\circ$ UV 174	761.26	F	(1)	1.96	18.25	2-2	$2p^4 \ ^1D - 6d'' \ ^1D^\circ$ UV 195
837.63	F	(0)	1.96	16.77	2-2	$2p^4 \ ^1D - 10s' \ ^1D^\circ$ UV 175	757.15	F	(1)	1.96	18.34	2-1	$2p^4 \ ^1D - 8s'' \ ^1P^\circ$ UV 196
837.40	F	(1)	1.96	16.77	2-1	$2p^4 \ ^1D - 9d' \ ^1P^\circ$ UV 176	756.56	F	(0)	1.96	18.35	2-2	$2p^4 \ ^1D - 7d'' \ ^1D^\circ$ UV 197
837.27	F	(1)	1.96	16.78	2-2	$2p^4 \ ^1D - 9d' \ ^1D^\circ$ -3 UV 177	753.94	F	(0)	1.96	18.41	2-1	$2p^4 \ ^1D - 9s'' \ ^1P^\circ$ UV 198
835.60	F	(1)	1.96	16.80	2-1	$2p^4 \ ^1D - 10d' \ ^1P^\circ$ UV 178	753.52	F	(1)	1.92	18.42	2-2	$2p^4 \ ^1D - 8d'' \ ^1D^\circ$ UV 199
835.44	F	(1)	1.96	16.81	2-2	$2p^4 \ ^1D - 10d' \ ^1D^\circ$ -3 UV 179	751.75	F	(0)	1.96	18.46	2-1	$2p^4 \ ^1D - 10s'' \ ^1P^\circ$ UV 200
834.34	F	(0)	1.96	16.83	2-2	$2p^4 \ ^1D - 12s' \ ^1D^\circ?$ UV 180	751.47	F	(1)	1.96	18.47	2-2	$2p^4 \ ^1D - 9d'' \ ^1D^\circ$ UV 201
834.25	F	(0)	1.96	16.83	2-1	$2p^4 \ ^1D - 11d' \ ^1P^\circ$ UV 181	750.19	F	(1)	1.96	18.49	2-1	$2p^4 \ ^1D - 11s'' \ ^1P^\circ$ UV 202
834.12	F	(0)	1.96	16.83	2-2	$2p^4 \ ^1D - 11d' \ ^1D^\circ$ -3 UV 182	749.99	F	(0)	1.96	18.50	2-2	$2p^4 \ ^1D - 10d'' \ ^1D^\circ$ UV 203
833.20	F	(0)	1.96	16.85	2-1	$2p^4 \ ^1D - 12d' \ ^1P^\circ$ UV 183	748.93	F	(0)	1.96	18.52	2-2	$2p^4 \ ^1D - 11d'' \ ^1D^\circ$ UV 204
833.10	F	(0)	1.96	16.85	2-2	$2p^4 \ ^1D - 12d' \ ^1D^\circ$ -3 UV 184							
*832.42	F	(0)	1.96	16.86	2-2	$2p^4 \ ^1D - 14s' \ ^1D^\circ$ UV 185							

Multiplet Table

O I—Continued

O I—Continued

IA	Ref.	Int.	E P		J	Multiplet No.	IA	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Air 2324.738	P		4.19	9.52	0-1	$2p^4 \ ^1S - 3s \ ^3S^o$ UV 205	3348.1776 3348.2336 3348.2737	C C C	8 7 6	9.15 9.15 9.15	12.85 12.85 12.85	2-3 2-2 2-1	$3s \ ^5S^o - 5p \ ^5P$ 3.01
Vac 1601.731	P		4.19	11.93	0-1	$2p^4 \ ^1S - 4s \ ^3S^o$ UV 206	10167.252 10169.347	B P	10	9.52 9.52	10.74 10.74	1-2 1-1	$3s \ ^3S^o - 3p \ ^3P$ 3.02
1217.6477	A		4.19	14.37	0-1	$2p^4 \ ^1S - 3s' \ ^1P^o$ UV 207	8446.3596 8446.7581 8446.250	B B B	30 29 27	9.52 9.52 9.52	10.99 10.99 10.99	1-2 1-1 1-0	$3s \ ^3S^o - 3p \ ^3P$ 4
1105.20	P		4.19	15.41	0-1	$2p^4 \ ^1S - 3d' \ ^1P^o$ UV 208	4368.2467 4368.1933	C C	11 8	9.52 9.52	12.36 12.36	1- 1-0	$3s \ ^3S^o - 4p \ ^3P$ 5
1042.86	P		4.19	16.08	0-1	$2p^4 \ ^1S - 4d' \ ^1P^o$ UV 209	3692.3945 3692.3863 3692.3558	A A A		9.52 9.52 9.52	12.88 12.88 12.88	1-2 1-1 1-0	$3s \ ^3S^o - 5p \ ^3P$ 6
975.04	P		4.19	16.91	0-1	$2p^4 \ ^1S - 4s'' \ ^1P^o$ UV 210	11302.376 11297.682 11295.104	B B B	23 22 21	10.74 10.74 10.74	11.84 11.84 11.84	3-2 2-2 1-2	$3p \ ^5P - 4s \ ^5S^o$ 7
959.80	F	(0)	4.19	17.11	0-1	$2p^4 \ ^1S - 3d'' \ ^1P^o$ UV 211	9266.006 9262.774 9260.935 9265.938 9262.671 9260.845 9265.827 9262.584 9260.806	B B B B B B P B B	24 23 20 21 21 19 22 19 20	10.74 10.74 10.74 10.74 10.74 10.74 10.74 10.74 10.74	12.08 12.08 12.08 12.08 12.08 12.08 12.08 12.08 12.08	3-4 2-3 1-2 3-3 2-2 1-1 3-2 2-1 1-0	$3p \ ^5P - 3d \ ^5D^o$ 8
912.48	F	(0)	4.19	17.78	0-1	$2p^4 \ ^1S - 4d'' \ ^1P^o$ UV 212	6455.9756 6454.4451 6453.6023	B B B	19 18 17	10.74 10.74 10.74	12.66 12.66 12.66	3-2 2-2 1-2	$3p \ ^5P - 5s \ ^5S^o$ 9
892.11	F	(1)	4.19	18.09	0-1	$2p^4 \ ^1S - 5d'' \ ^1P^o$ UV 213	6158.1835 6156.7658 6155.9756	B B B	21 20 19	10.74 10.74 10.74	12.75 12.75 12.75	3- 2- 1-	$3p \ ^5P - 4d \ ^5D^o$ 10
881.47	F	(0)	4.19	18.25	0-1	$2p^4 \ ^1S - 6d'' \ ^1P^o$ UV 214	5330.7396 5329.6855 5329.1012	B B B	13 12 11	10.74 10.74 10.74	13.07 13.07 13.07	3- 2- 1-	$3p \ ^5P - 5d \ ^5D^o$ 12
875.16	F	(1)	4.19	18.36	0-1	$2p^4 \ ^1S - 7d'' \ ^1P^o$ UV 215	5020.2179 5019.2910 5018.7832	B B B	7 6 5	10.74 10.74 10.74	13.21 13.21 13.21	3-2 2-2 1-2	$3p \ ^5P - 7s \ ^5S^o$ 13
871.16	F	(0)	4.19	18.42	0-1	$2p^4 \ ^1S - 8d'' \ ^1P^o$ UV 216	5436.8616 5435.7756 5435.1767	B B B	11 10 9	10.74 10.74 10.74	13.02 13.02 13.02	3-2 2-2 1-2	$3p \ ^5P - 6s \ ^5S^o$ 11
868.41	F	(0)	4.19	18.47	0-1	$2p^4 \ ^1S - 9d'' \ ^1P^o$ UV 217	5330.7396 5329.6855 5329.1012	B B B	19 18 17	10.74 10.74 10.74	13.07 13.07 13.07	3-2 2-2 1-2	$3p \ ^5P - 5d \ ^5D^o$ 12
Air 7771.9436	B	28	9.15	10.74	2-3	$3s \ ^5S^o - 3p \ ^3P$ 1	5020.2179 5019.2910 5018.7832	B B B	7 6 5	10.74 10.74 10.74	13.21 13.21 13.21	3-2 2-2 1-2	$3p \ ^5P - 7s \ ^5S^o$ 13
7774.1665	B	27	9.15	10.74	2-2								
7775.3884	B	26	9.15	10.74	2-1								
6726.2833	B	9	9.15	10.99	2-2	$3s \ ^5S^o - 3p \ ^3P$ 2							
6726.5389	B	6	9.15	10.99	2-1								
3947.2948	C	15	9.15	12.29	2-3	$3s \ ^5S^o - 4p \ ^3P$ 3							
3947.4812	C	14	9.15	12.29	2-2								
3947.5862	C	13	9.15	12.29	2-1								

Multiplet Table

O I—Continued

O I—Continued

I A	Ref.	Int.	E P		J	Multiplet No.	I A	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
4968.7931	B	8	10.74	13.24	3-	3p ³ P - 6d ³ D°	3954.6073	A	11	10.99	14.12	2-2	3p ³ P - 3s'' ³ P°
4967.8821	B	7	10.74	13.24	2-	14	3952.8870	A	5	10.99	14.12	1-1	30
4967.3783	B	6	10.74	13.24	1-		*3952.9834	A	7	10.99	14.12	2-1	
4802.9816	B	4	10.74	13.32	3-2	3p ³ P - 8s ³ S°	3951.9271	A	8	10.99	14.12	1-0	
4802.132	B	3	10.74	13.32	2-2	15	*3952.9834	A	9	10.99	14.12	1-2	
4773.7522	B	5	10.74	13.34	3-	3p ³ P - 7d ³ D°	2883.8557	A		10.99	15.29	2-2	3p ³ P - 3d' ³ P°
4772.9133	B	4	10.74	13.34	2-	16	2878.9312	A		10.99	15.29	1-1	30.01
4772.4489	B	3	10.74	13.34	1-		2878.9776	A		10.99	15.29	2-1	
4655.359	B	3	10.74	13.40	3-	3p ³ P - 8d ³ D°	2883.8092	A		10.99	15.30	1-0	
4654.5584	B	2	10.74	13.40	2-	18	2878.9906	A		10.99	15.29	1-2	
4654.1183	B	1	10.74	13.40	1-					10.99	15.29	0-1	
13164.85	B	26	10.99	11.93	2-1	3p ³ P - 4s ³ S°	9694.661	C	10	11.84	13.12	2-3	4s ³ S° - 6p ³ P
13163.89	B	25	10.99	11.93	1-1	18.01	9694.906	C	9	11.84	13.12	2-2	30.02
13165.11	B	24	10.99	11.93	0-1		9695.060	C	8	11.84	13.12	2-1	
11286.914	B	24	10.99	12.09	2-3	3p ³ P - 3d ³ D°							
11286.344	B	23	10.99	12.09	1-	18.02	13076.91	C	14	11.93	12.88	1-	4s ³ S° - 5p ³ P
11287.318	B	21	10.99	12.09	0-1								30.03
11287.022	B	21	10.99	12.09	2-		10320.304	C	9	11.93	13.13	1-	4s ³ S° - 6p ³ P
7995.0742	B	15	10.99	12.54	2-3	3p ³ P - 3s' ³ D°							30.04
7986.9777	B	13	10.99	12.54	1-2	19							
7982.3986	B	11	10.99	12.54	0-1								
7987.3330	B	11	10.99	12.54	2-2								
7981.9414	B	10	10.99	12.54	1-1								
7254.4475	B	20	10.99	12.70	2-1	3p ³ P - 5s ³ S°	18021.21	B	23	12.08	12.77	3d ³ D°- 4f ³ F	
7254.1544	B	19	10.99	12.70	1-1	20							30.05
7254.529	B	17	10.99	12.70	0-1		12464.02	B	21	12.08	13.07	3d ³ D°- 5f ³ F	
7002.2282	B	20	10.99	12.76	2-	3p ³ P - 4d ³ D°							30.06
7001.9157	B	18	10.99	12.76	1-	21	10675.725	B	17	12.08	13.24	3d ³ D°- 6f ³ F	
6046.4381	B	13	10.99	13.04	2-1	3p ³ P - 6s ³ S°	10675.940	B	16	12.08	13.24	3d ³ D°- 7f ³ F	
6046.2329	B	12	10.99	13.04	1-1	22							30.07
6046.494	B	10	10.99	13.04	0-1		9825.847	B	13	12.08	13.34		
5958.5830	B	13	10.99	13.07	2-	3p ³ P - 5d ³ D°	9826.002	B	12	12.08	13.34	3d ³ D°- 7f ³ F	
5958.3868	B	12	10.99	13.07	1-	23							30.08
5555.0036	B	9	10.99	13.22	2-1	3p ³ P - 7s ³ S°	18243.63	B	22	12.09	12.77	3d ³ D°- 4f ³ F	
5554.8322	B	8	10.99	13.22	1-1	24							30.09
5512.7709	B	8	10.99	13.24	2-	3p ³ P - 6d ³ D°	12570.04	B	20	12.09	13.07	3d ³ D°- 5f ³ F	
5512.6030	B	7	10.99	13.24	1-	25							30.10
5299.0441	B	5	10.99	13.33	2-1	3p ³ P - 8s ³ S°	10753.530	B	17	12.09	13.24	3d ³ D°- 6f ³ F	
5298.8876	B	4	10.99	13.33	1-1	26							30.11
5275.121	B	4	10.99	13.34	2-	3p ³ P - 7d ³ D°	9891.743	B	13	12.09	13.34	3d ³ D°- 7f ³ F	
5274.9680	B	2	10.99	13.34	1-	27							30.12

Multiplet Table

O I—Continued

O I—Continued

I A	Ref.	Int.	E P		J	Multiplet No.	I A	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
6324.842	A	7	12.09	14.05	-1	3d ³ D° - 3p' ³ D 31	8820.426	A	20	12.73	14.13	2-3	3s' ¹ D° - 3p' ¹ F 37
6323.388	A	5	12.09	14.05			7156.701	A	16	12.73	14.46	2-2	3s' ¹ D° - 3p' ¹ D 38
3534.1883	A		12.09	15.59	3-3	3d ³ D° - 4p' ³ D 31.01	3997.9528	A	4	12.73	15.83	2-1	3s' ¹ D° - 3p'' ¹ P 38.01
3533.2532	A		12.09	15.59	2-2		3855.0141	A	6	12.73	15.94	2-2	3s' ¹ D° - 3p'' ¹ D 38.02
3532.6054	A		12.09	15.60	1-1								
3533.2645	A		12.09	15.59	3-2								
3532.6141	A		12.09	15.60	2-1								
3534.1771	A		12.09	15.59	2-3								
3533.2445	A		12.09	15.59	1-2								
18229.23	C	13	12.36	13.04	-1	4p ³ P - 6s ³ S° 31.02	*9625.290	A	12	12.76	14.05	3-3	4d ³ D° - 3p' ³ D 38.03
*7025.509	A	5	12.36	14.12	2-2	4p ³ P - 3s'' ³ P° 32	*9625.290	A	12	12.76	14.05	2-2	
*7020.357	A	2	12.36	14.12	1-1		*9622.127	A	11	12.76	14.05	1-1	
*7020.357	A	2	12.36	14.12	2-1		*9625.290	A	12	12.76	14.05	3-2	
*7025.509	A	5	12.36	14.12	1-2		*9622.127	A	11	12.76	14.05	2-1	
4233.2680	A	10	12.36	15.29	-2	4p ³ P - 3d' ³ P° 33	*9625.290	A	12	12.76	14.05	2-3	
4222.7651	A	8	12.36	15.29	-1		*26173.56	C	13	12.77	13.24		4f ⁵ F - 6g ⁶ G° 38.04
4217.0875	A	7	12.36	15.30	1-0								
4222.8182	A	7	12.36	15.29	0-1								
8221.823	A	22	12.54	14.05	3-	3s' ³ D° - 3p' ³ D 34	*26173.56	C	13	12.77	13.24		4f ³ F - 6g ³ G° 38.05
8230.020	A	18	12.54	14.05	2-								
8233.005	A	20	12.54	14.05	1-1								
8227.652	A	18	12.54	14.05	2-1								
8235.351	A	12	12.54	14.05	1-2								
7947.548	A	17	12.54	14.10	3-4	3s' ³ D° - 3p' ³ F 35	5146.096	A	7	12.88	15.29	-2	5p ³ P - 3d' ³ P° 39
7950.804	A	16	12.54	14.10	2-3		5130.586	A	5	12.88	15.29	-1	
7952.160	A	15	12.54	14.10	1-2		5122.229	A	4	12.88	15.30	1-0	
7943.153	A	11	12.54	14.10	3-3		5130.655	A	5	12.88	15.29	0-1	
7947.169	A	11	12.54	14.10	2-2		3830.3261	P		12.88	16.11	2-2	5p ³ P - 4d' ³ P° 39.01
7939.514	A	6	12.54	14.10	3-2		3830.3349	P		12.88	16.11	1-2	
3823.4123	A	12	12.54	15.78	3-3	3s' ³ D° - 3p'' ³ D 36							
3824.3509	A	7	12.54	15.78	2-2								
3825.0221	A	7	12.54	15.78	1-1								
3822.5740	A	5	12.54	15.78	3-2								
3823.8686	A	6	12.54	15.78	2-1								
3825.1873	A	8	12.54	15.78	2-3								
3825.498	A		12.54	15.78	1-2								
							10421.177	A	12d	14.04	15.22	1-2	3p' ⁴ P - 4s' ⁴ D° 40.01
9482.884	A	12d	12.73	14.04	2-1	3s' ¹ D° - 3p' ¹ P 36.01	9057.014	A	14d	14.04	15.40	1-0	3p' ¹ P - 3d' ¹ S° 40.02
9402.290	P		12.73	14.05	2-3	3s' ¹ D° - 3p' ³ D 36.02	8994.604	A	9d	14.04	15.41	1-2	3p' ¹ P - 3d' ¹ D° 40.03
9402.256	P		12.73	14.05	2-2								
9399.192	A	15	12.73	14.05	2-1								
9039.607	A	8	12.73	14.10	2-3	3s' ¹ D° - 3p' ³ F 36.03	6276.563	A	7d	14.04	16.01	1-2	3p' ¹ P - 5s' ¹ D° 40.04
9034.912	P		12.73	14.10	2-2								

Multiplet Table

O I—Continued

O I—Continued

IA	Ref.	Int.	EP		J	Multiplet No.	IA	Ref.	Int.	EP		J	Multiplet No.
			Low	High						Low	High		
Air 6066.986	A	7d	14.04	16.08	1-0	$3p' \ ^1P - 4d' \ ^1S^o$ 40.05	Air 9521.956 9523.364 9523.965 9528.282	A	16	14.10	15.40	4-4	$3p' \ ^3F - 3d' \ ^3F^o$ 45
*9995.310	A	14	14.05	15.29	3-2	$3p' \ ^3D - 3d' \ ^3P^o$ 40.06	9497.974	A	18	14.10	15.40	4-5	$3p' \ ^3F - 3d' \ ^3G^o$ 47
9936.983	A	13	14.05	15.29	2-1		9505.594	A	17	14.10	15.40	3-4	
9909.050	A	12	14.05	15.30	1-0		9497.895	P	m O I	14.10	15.41	2-3	
*9995.310	A	14	14.05	15.29	2-2		9499.300	A	14	14.10	15.40	4-4	
9940.408	A	12	14.05	15.29	1-1		9492.708	A	13	14.10	15.41	3-3	
9998.802	A	8	14.05	15.29	1-2								
9156.011	A	17	14.05	15.40	3-4	$3p' \ ^3D - 3d' \ ^3F^o$ 41	9481.165	A	12	14.10	15.41	4-4	$3p' \ ^3F - 3d' \ ^1G^o$ 47.01
*9151.481	A	10	14.05	15.40	2-3		9487.434	A	17	14.10	15.41	3-4	
9150.135	A	10	14.05	15.40	1-2		9431.715	A	8	14.10	15.41	2-3	$3p' \ ^3F - 3d' \ ^1F^o$ 47.02
*9151.481	A	10	14.05	15.40	3-3								
*9147.230	A	9	14.05	15.40	2-2		6266.890	A	9	14.10	16.08	4-4	$3p' \ ^3F - 4d' \ ^3F^o$ 48
*9147.230	A	9	14.05	15.40	3-2								
9135.055	A	9	14.05	15.40	3-4	$3p' \ ^3D - 3d' \ ^3G^o$ 41.01	6261.547	A	11	14.10	16.08	4-5	$3p' \ ^3F - 4d' \ ^3G^o$ 50
9134.711	A	10	14.05	15.40	1-0	$3p' \ ^3D - 3d' \ ^1S^o$ 41.02	6264.549	A	9	14.10	16.08	3-4	
							6261.451	P	m O I	14.10	16.08	2-3	
							6261.814	A	6	14.10	16.08	4-4	
9118.288	A	12	14.05	15.41	3-4	$3p' \ ^3D - 3d' \ ^1G^o$ 41.03	6259.196	A	6	14.10	16.08	3-3	
9071.209	A	8	14.05	15.41	1-2	$3p' \ ^3D - 3d' \ ^1D^o$ 41.04	6254.102	A	4	14.10	16.08	4-4	$3p' \ ^3F - 4d' \ ^1G^o$ 50.01
9062.098	A	7	14.05	15.41	-3	$3p' \ ^3D - 3d' \ ^1F^o$ 41.05	6256.832	A	10	14.10	16.08	3-4	
							5410.856	A	4	14.10	16.39	4-4	$3p' \ ^3F - 5d' \ ^3F^o$ 51
*7706.751	A	11	14.05	15.65	3-2	$3p' \ ^3D - 2p^5 \ ^3P^o$ 42	5408.595	A	6	14.10	16.39	4-5	$3p' \ ^3F - 5d' \ ^3G^o$ 53
7663.443	A	9	14.05	15.66	2-1		5410.739	A	4	14.10	16.39	3-4	
7639.984	A	7	14.05	15.67	1-0								
*7706.751	A	11	14.05	15.65	2-2		5404.993	A	5	14.10	16.39	3-4	$3p' \ ^3F - 5d' \ ^1G^o$ 53.01
7665.483	A	7	14.05	15.66	1-1								
7708.825	A	3	14.05	15.65	1-2								
6106.266	A	11	14.05	16.08	3-4	$3p' \ ^3D - 4d' \ ^3F^o$ 43	8426.164	A	12	14.12	15.59	2-3	$3s'' \ ^3P^o - 4p' \ ^3D$ 54
							8428.319	A	8	14.12	15.59	1-2	
6101.750	A	3	14.05	16.08	1-0	$3p' \ ^3D - 4d' \ ^1S^o$ 43.01	8429.050	A	8	14.12	15.60	0-1	
							8420.918	A	6	14.12	15.59	2-2	
							8424.687	P	m Ar I	14.12	15.60	1-1	
6094.126	A	6	14.05	16.08	3-4	$3p' \ ^3D - 4d' \ ^1G^o$ 43.02							
*5995.277	A	10	14.05	16.11	3-2	$3p' \ ^3D - 4d' \ ^3P^o$ 44	7476.440	A	16	14.12	15.78	2-3	$3s'' \ ^3P^o - 3p'' \ ^3D$ 55
5991.915	A	7	14.05	16.11	2-1		7479.075	A	12	14.12	15.78	1-2	
5991.305	A	7	14.05	16.12	1-0		7480.670	A	12	14.12	15.78	0-1	
*5995.277	A	10	14.05	16.11	2-2		7473.241	A	9	14.12	15.78	2-2	
5993.163	A	6	14.05	16.11	1-1		7477.236	A	11	14.12	15.78	1-1	
5290.693	A	6	14.05	16.39	3-4	$3p' \ ^3D - 5d' \ ^3F^o$ 44.01	7471.404	A	6	14.12	15.78	2-1	
							11358.692	A	18	14.13	15.22	3-2	$3p' \ ^1F - 4s' \ ^1D^o$ 55.01

Multiplet Table

O I—Continued

O I—Continued

I A	Ref.	Int.	E P		J	Multiplet No.	I A	Ref.	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
*9784.55§	A		14.13	15.40	3-4	$3p' \ ^1F - 3d' \ ^3F^o$ 55.02	8508.583	A	7	14.37	15.83	1-1	$3s'' \ ^1P^o - 3p'' \ ^1P$ 61.03
9760.653	A	17	14.13	15.40	3-4	$3p' \ ^1F - 3d' \ ^3G^o$ 55.03	7886.273	A	10	14.37	15.94	1-2	$3s'' \ ^1P^o - 3p'' \ ^1D$ 64
9741.503	A	17	14.13	15.41	3-4	$3p' \ ^1F - 3d' \ ^1G^o$ 55.04	6653.834	A	11	14.37	16.23	1-0	$3s'' \ ^1P^o - 3p'' \ ^1S$ 65
9684.513	A	8	14.13	15.41	3-2	$3p' \ ^1F - 3d' \ ^1D^o$ 55.05	16212.06	A	14	14.46	15.22	2-2	$3p' \ ^1D - 4s' \ ^1D^o$ 66
9677.384	A	14	14.13	15.41	3-3	$3p' \ ^1F - 3d' \ ^1F^o$ 58	12990.77	A	12	14.46	15.41	2-3	$3p' \ ^1D - 3d' \ ^1F^o$ 67
6604.906	A	10	14.13	16.01	3-2	$3p' \ ^1F - 5s' \ ^1D^o$ 58.01	7997.013	A	8	14.46	16.01	2-2	$3p' \ ^1D - 5s' \ ^1D^o$ 68
6374.324	A	11	14.13	16.08	3-4	$3p' \ ^1F - 4d' \ ^3G^o$ 59							
6366.335	A	11	14.13	16.08	3-4	$3p' \ ^1F - 4d' \ ^1G^o$ 59.01	17966.70	A	12	15.40	16.09	4-5	$3d' \ ^3F^o - 4f' \ ^3G$ 69
6351.156	A	8	14.13	16.08	3-3	$3p' \ ^1F - 4d' \ ^1F^o$ 61							
5492.432	A	5	14.13	16.39	3-4	$3p' \ ^1F - 5d' \ ^3G^o$ 61.01	18046.23 18041.48	A A	12 12	15.40 15.40	16.09 16.09	5-6 4-5	$3d' \ ^3G^o - 4f' \ ^3H$ 70
5486.517	A	5	14.13	16.39	3-4	$3p' \ ^1F - 5d' \ ^1G^o$ 61.02	18042.19	A	12	15.41	16.09	4-5	$3d' \ ^1G^o - 4f' \ ^1H$ 71