

UNITED STATES DEPARTMENT OF COMMERCE • Maurice H. Stans, *Secretary*

NATIONAL BUREAU OF STANDARDS • Lewis M. Branscomb, *Director*

# Selected Tables of Atomic Spectra

## A Atomic Energy Levels-Second Edition

## B Multiplet Tables

**N IV, N V, N VI, N VII**

**Data Derived From the Analyses of Optical Spectra**

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## **Abstract**

The present publication is the fourth Section of a series being prepared in response to the persistent need for a current revision of two sets of tables containing data on atomic spectra as derived from analyses of optical spectra. As in the previous Sections, Part A contains the atomic energy levels and Part B the multiplet tables. Four spectra of nitrogen, N IV, N V, N VI and N VII, are included. The form of presentation is described in detail in the text to Section 1.

**Key words:** Atomic energy levels, N IV-N VII; Nitrogen spectra, N IV-N VII; Multiplet tables, N IV-N VII; Spectra, N IV-N VII; Wavelengths, nitrogen spectra N IV-N VII.

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## **Foreword**

The National Standard Reference Data System provides effective access to the quantitative data of physical science, critically evaluated and compiled for convenience, and readily accessible through a variety of distribution channels. The System was established in 1963 by action of the President's Office of Science and Technology and the Federal Council for Science and Technology, with responsibility to administer it assigned to the National Bureau of Standards.

The System now comprises a complex of data centers and other activities, carried on in academic institutions and other laboratories both in and out of government. The independent operational status of existing critical data projects is maintained and encouraged. Data centers that are components of the NSRDS produce compilations of critically evaluated data, critical reviews of the state of quantitative knowledge in specialized areas, and computations of useful functions derived from standard reference data. In addition, the centers and projects establish criteria for evaluation and compilation of data and make recommendations on needed improvements in experimental techniques. They are normally closely associated with active research in the relevant field.

The technical scope of the NSRDS is indicated by the principal categories of data compilation projects now active or being planned: nuclear properties, atomic and molecular properties, solid state properties, thermodynamic and transport properties, chemical kinetics, and colloid and surface properties and mechanical properties.

The NSRDS receives advice and planning assistance from the National Research Council of the National Academy of Sciences-National Academy of Engineering. An overall Review Committee considers the program as a whole and makes recommendations on policy, long-term planning, and international collaboration. Advisory Panels, each concerned with a single technical area, meet regularly to examine major portions of the program, assign relative priorities, and identify specific key problems in need of further attention. For selected specific topics, the Advisory Panels sponsor subpanels which make detailed studies of users' needs, the present state of knowledge, and existing data resources, as a basis for recommending one or more data compilation activities. This assembly of advisory services contributes greatly to the guidance of NSRDS activities.

The NSRDS-NBS series of publications is intended primarily to include evaluated reference data and critical reviews of long-term interest to the scientific and technical community.

LEWIS M. BRANSCOMB, *Director*

## Preface

The present publication is the fourth Section of a series that is being prepared in response to the increasing demand for a current revision of two sets of tables containing data on atomic spectra as derived from analyses of optical spectra.

The first set, *Atomic Energy Levels*, NBS Circular 467, consists of three Volumes published, respectively, in 1949, 1952, and 1958, and a fourth one on rare-earth spectra, still in course of preparation. This Circular has been reprinted as NSRDS-NBS 35, Volumes I, II, and III.

The second set consists of two Multiplet Tables; one published in 1945 by the Princeton University Observatory containing multiplets having wavelengths longer than 3000 Å; the other, *An Ultra-Violet Multiplet Table*, NBS Circular 488, appearing in five Sections, the first in 1950, the second in 1952, and the others in 1962. The 1945 Princeton Multiplet Table is being reprinted as NSRDS-NBS 40.

The present series includes both sets of data, the energy levels and multiplet tables as parts A and B, respectively, for selected spectra contained in Volume I of "Atomic Energy Levels." The Sections are being published at irregular intervals as revised analyses become available. A flexible paging system permits the arrangement of the various Sections by atomic number, regardless of the order in which the separate spectra are published. Section 1 includes three spectra of silicon,  $Z=14$ : Si II, Si III, Si IV. Section 2 contains similar data for Si I. Section 3 covers all the spectra of carbon,  $Z=6$ : C I, C II, C III, C IV, C V, C VI. Section 5 is scheduled to include the remaining spectra of nitrogen: N I, N II, N III. The form of presentation of the data is described in detail in the text of Section 1. All Sections are arranged identically and the same conversion factor,  $\text{cm}^{-1}$  to eV, 0.000123981 is used throughout.

The manuscript has been prepared by Charlotte E. Moore of the Office of Standard Reference Data, who published the earlier tables. She appreciates the cordial cooperation of the numerous atomic spectroscopists whose work is quoted here. She is particularly indebted to B. Edlén for his valuable guidance and advice. K. Bockasten and S. G. Tilford have also been most cooperative. The splendid work of Barbara N. Somerville in typing the press copy of this difficult tabular material is gratefully acknowledged.

Washington, D.C., December 18, 1970.

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**NSRDS-NBS 3, SECTION 4**

**NITROGEN. Z = 7**

**A N IV Atomic Energy Levels**

**B N IV Multiplet Table**

## Atomic Energy Levels

### Part A

### NITROGEN

#### N IV

Be I sequence; 4 electrons

$Z=7$

Ground state  $1s^2 2s^2 1S_0$

$2s^2 1S_0 \mathbf{624866 \pm 3}$ , 160.034 Å (Vac)

I P 77.472 eV

The early analysis by Edlén has been revised and extended by R. Hallin, who has observed the spectrum from 300 Å to 8000 Å with a theta-pinch discharge as source. Hallin lists 127 classified lines and derives the ionization limit  $624864.7 \pm 2$  cm<sup>-1</sup> from hydrogen-like terms and by using the polarization formula. A slight revision of this value by A. Ölme in 1970 is quoted above.

The triplet and singlet systems are connected by the two intersystem combination lines at 823 Å and 1486 Å.

D. J. Michels has carried the analysis further by observations in the range 159 Å to 463 Å made with a Hinteregger-type water-cooled quartz capillary discharge tube—a windowless source operated as a pulse discharge. He reports 250 classified lines of which 22 are included by Hallin. Fifty-three of his new terms lie above the first ionization limit.

Michels introduces some revisions to the 1966 analysis. He interchanges the terms  $4s\ ^3S$  and  $3p'\ ^3S$ . This change has been adopted, but Hallin's values have been retained, as they are based on observations in the longer wavelength region. The level  $3d'\ ^1P^o$  has been revised by correcting a transcript error in the earlier work. This change leaves the line of intensity 2 at 2594.34 Å unclassified. Improved values for  $6d\ ^3D$ ,  $4p'\ ^1D$  and  $4,5d'\ ^3D^o$  have resulted from the 1970 observations.

One member in each of three series is missing because of masking:  $5p'\ ^1D$ ,  $5d'\ ^1F^o$  and  $12d'\ ^3D^o$ .

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### Atomic Energy Levels

**NIV**

**NIV**

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval	
$2s^2$	$2s^2 \ ^1S$	0	0.0		$2p(^2P^o)3d$	$3d' \ ^3D^o$	1	505554.6		
$2s(^2S)2p$	$2p \ ^3P^o$	0	67209.2				2	505588.2	34.2	
		1	67272.3	63.1			3	505630.6	42.4	
		2	67416.3	144.0	$2p(^2P_{1/2}^o)3d$	$3d' \ ^1F^o$	3	506284.8		
$2s(^2S)2p$	$2p \ ^1P^o$	1	130693.9		$2s(^2S)4p$	$4p \ ^1P^o$	1	507027.9		
$2p^2$	$2p^2 \ ^3P$	0	175535.4		$2s(^2S)4d$	$4d \ ^3D$	1	511440		
		1	175608.1	72.7			2	511446	6	
		2	175732.9	124.8			3	511448.0	2	
$2p^2$	$2p^2 \ ^1D$	2	188882.5		$2p(^2P_{1/2}^o)3d$	$3d' \ ^3P^o$	2	511509.3		
$2p^2$	$2p^2 \ ^1S$	0	235369.3				1	511560.4	-51.1	
							0	511591.2	-30.8	
$2s(^2S)3s$	$3s \ ^3S$	1	377284.8		$2s(^2S)4d$	$4d \ ^1D$	2	514647.7		
$2s(^2S)3s$	$3s \ ^1S$	0	388854.6		$2p(^2P_{1/2}^o)3p$	$3p' \ ^1S$	0	515569.8		
$2s(^2S)3p$	$3p \ ^1P^o$	1	404592.4		$2s(^2S)4f$	$4f \ ^3F^o$	2	516552.6		
$2s(^2S)3p$	$3p \ ^3P^o$	0	405971.6				3	516560.8	8.2	
		1	405987.5	15.9			4	516572.0	11.2	
		2	406022.8	35.3	$2p(^2P_{1/2}^o)3d$	$3d' \ ^1P^o$	1	518610.5		
$2s(^2S)3d$	$3d \ ^3D$	1	420045.8		$2s(^2S)4f$	$4f \ ^1F^o$	3	521862.8		
		2	420049.6	3.8		$2s(^2S)5s$	$5s \ ^3S$	1	544813.4	
		3	420058.0	8.4		$2s(^2S)5s$	$5s \ ^1S$	0	546731.3	
$2s(^2S)3d$	$3d \ ^1D$	2	429159.6		$2s(^2S)5p$	$5p \ ^1P^o$	1	550232.6		
$2p(^2P^o)3s$	$3s' \ ^3P^o$	0	465291.8			$2s(^2S)5d$	$5d \ ^3D$	1, 2		
		1	465371.0	79.2			3	552789.6		
		2	465536.6	165.6	$2s(^2S)5p$	$5d \ ^1D$	2	552790.9	1.3	
$2p(^2P_{1/2}^o)3s$	$3s' \ ^1P^o$	1	473029.3							
$2p(^2P_{0/2}^o)3p$	$3p' \ ^1P$	1	480884.2		$2s(^2S)5d$	$5d \ ^3D$	2	554300.7		
$2p(^2P^o)3p$	$3p' \ ^3D$	1	484498.2		$2s(^2S)5g$	$5g \ ^1G$	4	554339.1		
		2	484594.9	96.7		$2s(^2S)5g$	$5g \ ^3G$	3, 4, 5	554339.7	
		3	484746.2	151.3						
$2s(^2S)4s$	$4s \ ^3S$	1	487607.4		$2s(^2S)5f$	$5f \ ^3F^o$	2, 3, 4	554571.8		
$2p(^2P^o)3p$	$3p' \ ^3P$	0	494253.1		$2s(^2S)5f$	$5f \ ^1F^o$	3	554995.7		
		1	494309.2	56.1	$2s(^2S)6s$	$6s \ ^3S$	1	570381.3		
		2	494402.0	92.8						
$2s(^2S)4s$	$4s \ ^1S$	0	495057.7		$2s(^2S)6s$	$6s \ ^1S$	0	571172.1		
$2p(^2P^o)3d$	$3d' \ ^3F^o$	2	495406.2		$2s(^2S)6p$	$6p \ ^1P^o$	1	572731.1		
		3	495482.6	76.4		$2s(^2S)6d$	$6d \ ^3D$	1, 2, 3	575030.5	
		4	495585.7	103.1						
$2p(^2P_{1/2}^o)3p$	$3p' \ ^3S$	1	498045.5		$2s(^2S)6g$	$6g \ ^1G$	4	575807.9		
$2p(^2P_{0/2}^o)3d$	$3d' \ ^1D^o$	2	498310.3		$2s(^2S)6g$	$6g \ ^3G$	3, 4, 5	575809.4		
$2p(^2P_{1/2}^o)3p$	$3p' \ ^1D$	2	499705.9		$2s(^2S)6d$	$6d \ ^1D$	2	575872.4		
$2s(^2S)4p$	$4p \ ^3P^o$	2	503680.4		$2s(^2S)6f$	$6f \ ^1F^o$	3	575999.3		
		1	503691.9	-11.5						
		0	503699.8	-7.9	$2s(^2S)6h$	$6h \ ^1H^o$	4, 5, 5, 6	576042.9		

### Atomic Energy Levels

#### N IV - Continued

#### N IV - Continued

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval
$\frac{1}{2}p(^2P^{\circ})4s$	$4s' ^3P^{\circ}$	0	577957.8		$2s(^2S)9d$	$9d ^3D$	1, 2, 3	602865.7	
		1	578045.4			$9d ^4D$	2	603107.3	
		2	578210.6	165.2	$2s(^2S)9d$				
$\frac{1}{2}p(^2P_{1/2}^{\circ})4s$	$4s' ^1P^{\circ}$	1	580817.5		$2s(^2S)10s$	$10s ^3S$	1	606142.6	
$\frac{1}{2}p(^2P_{3/2}^{\circ})4p$	$4p' ^1P$	1	584661.6		$2s(^2S)10p$	$10p ^1P^{\circ}$	1	606818.2	
$\frac{1}{2}s(^2S)7s$	$7s ^3S$	1	584977.1		$2s(^2S)10d$	$10d ^3D$	1, 2, 3	607064.2	
$\frac{1}{2}s(^2S)7s$	$7s ^1S$	0	584983.3		$2s(^2S)10d$	$10d ^1D$	2	607242.9 <sup>f</sup>	
$\frac{1}{2}p(^2P^{\circ})4p$	$4p' ^3D$	1	585709.5		$2s(^2S)11s$	$11s ^3S$	1	609465.8	
		2	585798.1			$11p ^1P^{\circ}$	1	609945.8	
		3	585929.8	88.6 131.7	$2s(^2S)11p$				
$\frac{1}{2}s(^2S)7p$	$7p ^1P^{\circ}$	1	587979.4		$2s(^2S)11d$	$11d ^3D$	1, 2, 3	610166.0	
$\frac{1}{2}s(^2S)7d$	$7d ^3D$	1, 2, 3	588382.6		$2s(^2S)11d$	$11d ^1D$	2	610287.2	
$\frac{1}{2}p(^3P_{3/2}^{\circ})4d$	$4d' ^1D^{\circ}$	2	588689.0		$2s(^2S)12p$	$12p ^1P^{\circ}$	1	612329.6	
$\frac{1}{2}p(^2P^{\circ})4p$	$4p' ^3P$	0	588790.1		$2s(^2S)12d$	$12d ^3D$	1, 2, 3	612525.1	
		1	588991.2	201.1 68.1		$12d ^1D$	2	612621.6	
		2	589059.3		$2s(^2S)12d$				
$\frac{1}{2}s(^2S)7d$	$7d ^1D$	2	588884.0		$2s(^2S)13p$	$13p ^1P^{\circ}$	1	614190.3	
$\frac{1}{2}s(^2S)7h$	$7h^{1,3}H^{\circ}$	4, 5, 5, 6	588994.3		$2s(^2S)13d$	$13d ^3D$	1, 2, 3	614380.6	
$\frac{1}{2}s(^2S)7i$	$7i^{1,3}I$	5, 6, 6, 7	589021.4		$2s(^2S)13d$	$13d ^1D$	2	614470.5	
$\frac{1}{2}p(^3P_{1/2}^{\circ})4d$	$4d' ^1F^{\circ}$	3	591047.8		$2s(^2S)14d$	$14d ^3D$	1, 2, 3	615894.4	
$\frac{1}{2}p(^2P_{1/2}^{\circ})4p$	$4p' ^1D$	2	591060.9		$2s(^2S)15d$	$15d ^3D$	1, 2, 3	617038.7	
$\frac{1}{2}p(^2P^{\circ})4d$	$4d' ^3D^{\circ}$	1	593690.0		$N\pi(^2S_{1/2})$	<b>Limit</b>		<b>624866 ± 3</b>	
		2	593713.7	23.7					
		3	593772.1	58.4	$2p(^2P^{\circ})5s$	$5s' ^3P^{\circ}$	0	626355.0	
$\frac{1}{2}p(^2P_{1/2}^{\circ})4p$	$4p' ^1S$	0	594182.6				1	626445.3	90.3
							2	626611.9	166.6
$\frac{1}{2}p(^2P^{\circ})4d$	$4d' ^3P^{\circ}$	2	594489.9		$2p(^2P_{1/2}^{\circ})5s$	$5s' ^1P^{\circ}$	1	628546.9	
		1	594547.7	-57.8					
		0	594573.8	-26.1	$2p(^2P_{1/2}^{\circ})5s$				
$\frac{1}{2}p(^2P_{1/2}^{\circ})4p$	$4p' ^3S$	1	595296.3		$2p(^2P_{3/2}^{\circ})5p$	$5p' ^1P$	1	629845.3	
$\frac{1}{2}s(^2S)8s$	$8s ^1S$	0	596150.1		$2p(^2P^{\circ})5p$	$5p' ^3D$	1	630268.8	
$\frac{1}{2}s(^2S)8p$	$8p ^1P^{\circ}$	1	596270.9			$5p' ^3D$	2	630333.6	64.8
$\frac{1}{2}s(^2S)8d$	$8d ^3D$	1, 2, 3	597026.8		$2p(^2P^{\circ})5p$	$5p' ^3P$	0	631807.7	
$\frac{1}{2}s(^2S)8d$	$8d ^1D$	2	597349.1				1	631868.2	60.5
$\frac{1}{2}s(^2S)8s$	$8s ^3S$	1	597481.6		$2p(^2P^{\circ})5d$	$5d' ^3D^{\circ}$	1	634158.4	
$\frac{1}{2}p(^3P_{1/2}^{\circ})4d$	$4d' ^1P^{\circ}$	1	598538.2				2	634182.8	24.4
$\frac{1}{2}s(^2S)9s$	$9s ^3S$	1	601621.5		$2p(^2P^{\circ})5d$	$5d' ^3P^{\circ}$	0, 1, 2	634669.5	
$\frac{1}{2}s(^2S)9p$	$9p ^1P^{\circ}$	1	602609.3		$2p(^2P_{1/2}^{\circ})5d$	$5d' ^1P^{\circ}$	1	636467	

## Atomic Energy Levels

## N IV - Continued

## N IV - Continued

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval
$2p(^2P^{\circ})6s$	$6s' ^3P^{\circ}$	0 1 2	651590.1 651671.8 651859.9	81.7 188.1	$2p(^2P^{\circ})8d$	$8d' ^3P^{\circ}$	0, 1, 2	678025.9	
$2p(^2P_{0\downarrow\downarrow}^{\circ})6p$	$6p' ^1P$	1	653629.9		$2p(^2P_{1\downarrow\downarrow}^{\circ})8d$	$8d' ^1P^{\circ}$	1	678355	
$2p(^2P^{\circ})6p$	$6p' ^3D$	1 2 3	653909.4 654053.9	144.5	$2p(^2P^{\circ})9s$	$9s' ^3P^{\circ}$	0 1 2	682464.8	
$2p(^2P^{\circ})6p$	$6p' ^3P$	0, 1, 2	654791.3		$2p(^2P^{\circ})9p$	$9p' ^3D$	1 2 3	683092.7	
$2p(^2P_{1\downarrow\downarrow}^{\circ})6d$	$6d' ^1F^{\circ}$	3	655270.0		$2p(^2P^{\circ})9p$	$9p' ^3P$	0, 1, 2	683278.4	
$2p(^2P_{1\downarrow\downarrow}^{\circ})6p$	$6p' ^1D$	2	655284.1		$2p(^2P_{1\downarrow\downarrow}^{\circ})9p$	$9p' ^1D$	2	683399.9	
$2p(^2P^{\circ})6d$	$6d' ^3D^{\circ}$	1 2 3	656043.6 656074.7 656155.7	31.1 81.0	$2p(^2P^{\circ})9d$	$9d' ^3D^{\circ}$	1, 2, 3	683692.6	
$2p(^2P^{\circ})6d$	$6d' ^3P^{\circ}$	0, 1, 2	656349.6		$2p(^2P_{1\downarrow\downarrow}^{\circ})9d$	$9d' ^1P^{\circ}$	1	684015	
$2p(^2P_{1\downarrow\downarrow}^{\circ})6d$	$6d' ^1P^{\circ}$	1	657392		$2p(^2P^{\circ})10s$	$10s' ^3P^{\circ}$	0 1 2		
$2p(^2P^{\circ})7s$	$7s' ^3P^{\circ}$	0 1 2	666458.2 666665.4	207.2	$2p(^2P^{\circ})10p$	$10p' ^3D$	1 2 3	686954.2	
$2p(^2P_{0\downarrow\downarrow}^{\circ})7p$	$7p' ^1P$	1	667698.9		$2p(^2P^{\circ})10p$	$10p' ^3P$	0, 1, 2	687432.9	
$2p(^2P^{\circ})7p$	$7p' ^3D$	1 2 3	667872.6 668031.3	158.7	$2p(^2P_{1\downarrow\downarrow}^{\circ})10p$	$10p' ^1D$	2	687548.3	
$2p(^2P^{\circ})7p$	$7p' ^3P$	0, 1, 2	668460.9		$2p(^2P^{\circ})10d$	$10d' ^3D^{\circ}$	1, 2, 3	687875.8	
$2p(^2P_{1\downarrow\downarrow}^{\circ})7p$	$7p' ^1D$	2	668753.5		$2p(^2P^{\circ})10d$	$10d' ^3P^{\circ}$	0, 1, 2	688022.7	
$2p(^2P^{\circ})7d$	$7d' ^3D^{\circ}$	1, 2, 3	669328.5		$2p(^2P_{1\downarrow\downarrow}^{\circ})10d$	$10d' ^1P^{\circ}$	1	688094	
$2p(^2P^{\circ})7d$	$7d' ^3P^{\circ}$	0, 1, 2	669596.6		$2p(^2P^{\circ})11p$	$11p' ^3P$	0, 1, 2	690659.5	
$2p(^2P_{1\downarrow\downarrow}^{\circ})7d$	$7d' ^1P^{\circ}$	1	670086		$2p(^2P_{1\downarrow\downarrow}^{\circ})11p$	$11p' ^1D$	2	690770.5	
$2p(^2P^{\circ})8s$	$8s' ^3P^{\circ}$	0 1 2			$2p(^2P^{\circ})11d$	$11d' ^3D^{\circ}$	1, 2, 3	690976.4	
$2p(^2P_{0\downarrow\downarrow}^{\circ})8p$	$8p' ^1P$	1	676706.4		$2p(^2P^{\circ})12p$	$12p' ^3P$	0, 1, 2	693069.3	
$2p(^2P^{\circ})8p$	$8p' ^3D$	1 2 3			$2p(^2P^{\circ})13p$	$13p' ^3P$	0, 1, 2	694902.7	
$2p(^2P^{\circ})8p$	$8p' ^3P$	0, 1, 2	677276.5		$2p(^2P^{\circ})13d$	$13d' ^3D^{\circ}$	1, 2, 3	695124.4	
$2p(^2P_{1\downarrow\downarrow}^{\circ})8p$	$8p' ^1D$	2	677458.7		$N v(2p ^2P_{0\downarrow\downarrow}^{\circ})$	<i>Limit</i>		705327.9	259.7
$2p(^2P^{\circ})8d$	$8d' ^3D^{\circ}$	1, 2, 3	677844.3		$N v(2p ^2P_{1\downarrow\downarrow}^{\circ})$	<i>Limit</i>		705586.6	

### Atomic Energy Levels

#### N IV Observed Terms

Config. $1s^2+$	Observed Terms			
$2s^2$	$2s^2 \ ^1S$			
$2s(^2S)2p$	$2p \ ^3P^o$ $2p \ ^1P^o$			
$2p^2$	$2p^2 \ ^3P$ $2p^2 \ ^1S$ $2p^2 \ ^1D$			
	$ns(n \geq 3)$	$np(n \geq 3)$	$nd(n \geq 3)$	
$2s(^2S)nl$	$3-11s \ ^3S$ $3-8s \ ^1S$	$3, 4p \ ^3P^o$ $3-13p \ ^1P^o$	$3-15d \ ^3D$ $3-13d \ ^1D$	
$2p(^2P^o)nl'$	$3-10s' \ ^3P^o$ $3-5s' \ ^1P^o$	$3, 4p' \ ^3S$ $3-13p' \ ^3P$ $3, 4p' \ ^1S$ $3-8p' \ ^1P$	$3-10p' \ ^3D$ $3, 4, 6-11p' \ ^1D$	$3-10d' \ ^3P^o$ $3-11, 13d' \ ^3D^o$ $3-10d' \ ^1P^o$ $3, 4d' \ ^1D^o$ $3, 4, 6d' \ ^1F^o$
	$nf(n \geq 4)$	$ng(n \geq 5)$	$nh(n \geq 6)$	$ni(n \geq 7)$
$2s(^2S)nl$	$4, 5f \ ^3F^o$ $4-6f \ ^1F^o$	$5, 6g \ ^3G$ $5, 6g \ ^1G$	$6, 7h \ ^3, ^1H^o$	$7i \ ^3, ^1I$

### Multiplet Table

#### Part B

#### NITROGEN

#### N IV ( $Z = 7$ )

I P 77.472 eV      Limit  $628466 \pm 3$  cm<sup>-1</sup>      160.034 Å (Vac)

Anal A      List A      October 1970

#### REFERENCES

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- A R. Hallin, Ark. Fys. (Stockholm) **32**, No. 11, 201–210 (1966). I P, T, C L, I; W L, 300 Å–7702 Å
- B D. J. Michels, J. Opt. Soc. Am. **61**, No. 5, 625–631 (1971), and private communication regarding intensity estimates. T, CL, G D, Theory(I); W L, 159Å–463Å
- C B. Edlén, Nova Acta Reg. Soc. Sci. Uppsala [IV] **9**, No. 6, 62–65 (1934). T, C L, I; W L, 181 Å–7127 Å
- P Predicted Lines

In column 3 parentheses indicate that the estimated intensities are from a different reference and on a different scale than the entries without parentheses.

New Multiplet Numbers, not inserted between older ones, start with UV 20 and 18.

\*Blend

‡Raiet ultime

#### N IV

#### N IV

I A	Ref	Int	E P				J	Multiplet No.	I A	Ref	Int	E P				J	Multiplet No.
			Low	High								Low	High				
Vac 1486.496	A	2	0.00	8.34	0-1	$2s^2 \ ^1S - 2p \ ^3P^o$ UV 0.01			Vac 211.405	B	(400)	0.00	58.65	0-1	$2s^2 \ ^1S - 3s' \ ^1P^o$ UV 2.03		
765.148‡	A	15	0.00	16.20	0-1	$2s^2 \ ^1S - 2p \ ^1P^o$ UV 1			197.230	C	(500)	0.00	62.86	0-1	$2s^2 \ ^1S - 4p \ ^1P^o$ UV 2.04		
569.450	P		0.00	21.77	0-1	$2s^2 \ ^1S - 2p^2 \ ^3P$ UV 1.01F			192.823	P		0.00	64.30	0-1	$2s^2 \ ^1S - 3d' \ ^1P^o$ UV 2.05		
529.430	P		0.00	23.42	0-2	$2s^2 \ ^1S - 2p^2 \ ^1D$ UV 1.02F			181.746	C	(400)	0.00	68.22	0-1	$2s^2 \ ^1S - 5p \ ^1P^o$ UV 2.06		
424.864	P		0.00	29.18	0-0	$2s^2 \ ^1S - 2p^2 \ ^1S$ UV 1.03F			174.602	B	(200)	0.00	71.01	0-1	$2s^2 \ ^1S - 6p \ ^1P^o$ UV 2.07		
247.205	C	(900)	0.00	50.15	0-1	$2s^2 \ ^1S - 3p \ ^1P^o$ UV 2			172.171	P		0.00	72.01	0-1	$2s^2 \ ^1S - 4s' \ ^1P^o$ UV 2.08		
246.313	P		0.00	50.33	0-1	$2s^2 \ ^1S - 3p \ ^3P^o$ UV 2.01			170.074	B	(200)	0.00	72.90	0-1	$2s^2 \ ^1S - 7p \ ^1P^o$ UV 2.09		
214.882	P		0.00	57.70	0-1	$2s^2 \ ^1S - 3s' \ ^3P^o$ UV 2.02			167.709	B	(150)	0.00	73.93	0-1	$2s^2 \ ^1S - 8p \ ^1P^o$ UV 2.10		

Multiplet Table

## N IV—Continued

## N IV—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 167.074	P		0.00	74.21	0-1	2s <sup>2</sup> 1S — 4d' 1P° UV 2.11	234.195	C	(600w)*	8.36	61.30	2-2	2p 3P°— 3p' 3P UV 5.05
165.945	B	(50)	0.00	74.71	0-1	2s <sup>2</sup> 1S — 9p' 1P° UV 2.12	234.172	P		8.34	61.28	1-1	
164.794	B	(30)	0.00	75.23	0-1	2s <sup>2</sup> 1S — 10p' 1P° UV 2.13	234.249	C	(600w)*	8.36	61.28	2-1	
163.949	B	(10d)	0.00	75.62	0-1	2s <sup>2</sup> 1S — 11p' 1P° UV 2.14	232.223	B	(200)	8.36	61.75	2-1	2p 3P°— 3p' 3S UV 5.07
163.311	B	(1d)	0.00	75.92	0-1	2s <sup>2</sup> 1S — 12p' 1P° UV 2.15	232.145	B	(150)	8.34	61.75	1-1	
162.816	B	(1d)	0.00	76.15	0-1	2s <sup>2</sup> 1S — 13p' 1P° UV 2.16	232.112	B	(100)	8.33	61.75	0-1	
							231.326	P		8.36	61.95	2-2	2p 3P°— 3p' 1D UV 5.08
							231.249	P		8.34	61.95	1-2	
							225.212	B	(800)	8.36	63.41	2-3	2p 3P°— 4d' 3D UV 6
							225.142	B	(800w)*	8.34	63.41	1-2	
							225.110	B		8.33	63.41	0-1	
923.220	A	16	8.36	21.79	2-2	2p 3P°— 2p <sup>2</sup> 3P UV 3	223.598	P		8.36	63.81	2-2	2p 3P°— 4d' 1D UV 6.01
923.057	A	14-	8.34	21.77	1-1		223.526	P		8.34	63.81	1-2	
924.283	A	14+	8.36	21.77	2-1		223.066	P		8.34	63.92	1-0	2p 3P°— 3p' 1S UV 6.02
923.675	A	14	8.34	21.76	1-0								
921.992	A	14+	8.34	21.79	1-2								
922.519	A	14	8.33	21.77	0-1								
823.273	A	2	8.36	23.42	2-2	2p 3P°— 2p <sup>2</sup> 1D UV 3.01	209.471	B	(400w)*	8.36	67.55	2-1	2p 3P°— 5s' 3S UV 6.03
822.299	P		8.34	23.42	1-2		209.407	B		8.34	67.55	1-1	
							209.378	B		8.33	67.55	0-1	
594.895	P		8.34	29.18	1-0	2p 3P°— 2p <sup>2</sup> 1S UV 3.02	206.028	B	(500)	8.36	68.54	2-3	2p 3P°— 5d' 3D UV 6.04
							205.968	B	(500w)*	8.34	68.54	1-2	
							205.940	B		8.33	68.54	0-1	
322.722	B	9	8.36	46.78	2-1	2p 3P°— 3s' 3S UV 4	198.821	B	(300)	8.36	70.72	2-1	2p 3P°— 6s' 3S UV 6.05
322.572	B	8	8.34	46.78	1-1		198.764	B	(250w)*	8.34	70.72	1-1	
322.506	B	7	8.33	46.78	0-1		198.740	B		8.33	70.72	0-1	
310.962	P		8.34	48.21	1-0	2p 3P°— 3s' 1S UV 4.01	197.000	B	(400)	8.36	71.29	2-	2p 3P°— 6d' 3D UV 6.06
							196.944	B	(400w)*	8.34	71.29	1-	
							196.921	B		8.33	71.29	0-1	
283.583	B	12	8.36	52.08	2-3	2p 3P°— 3d' 3D UV 5	193.214	B	(350)	8.36	72.53	2-1	2p 3P°— 7s' 3S UV 6.07
283.476	B	11	8.34	52.08	1-2		193.160	B	(300w)*	8.34	72.53	1-1	
283.419	B	10	8.33	52.08	0-1		193.139	B		8.33	72.53	0-1	
276.439	P		8.36	53.21	2-2	2p 3P°— 3d' 1D UV 5.01	192.859	B	(400w)*	8.36	72.64	2-3	2p 3P°— 4p' 3D UV 6.08
276.329	P		8.34	53.21	1-2		192.908	B		8.36	72.63	2-2	
							192.888	B	(400w)*	8.34	72.62	1-1	
							192.941	B		8.36	72.62	2-1	
239.616	B	(500w)	8.36	60.10	2-3	2p 3P°— 3p' 3D UV 5.03	191.951	B	(350)	8.36	72.95	2-	2p 3P°— 7d' 3D UV 6.09
239.632	B		8.34	60.08	1-2		191.898	B	(350w)*	8.34	72.95	1-	
239.659	B		8.33	60.07	0-1		191.868	B		8.33	72.95	0-1	
239.708	B	(400w)*	8.36	60.08	2-2								
239.679	B		8.34	60.07	1-1		191.702	B		8.36	73.03	2-2	2p 3P°— 4p' 3P UV 6.10
239.763	B		8.36	60.07	2-1		191.676	B		8.34	73.02	1-1	
							191.727	B	(400w)*	8.36	73.02	2-1	
237.991	B	(500)	8.36	60.45	2-1	2p 3P°— 4s' 3S UV 5.04	191.748	B		8.34	73.00	1-0	
237.908	B	(400w)*	8.34	60.45	1-1		*191.651	B		8.34	73.03	1-2	
237.873	B	(400w)*	8.33	60.45	0-1		*191.651	B		8.33	73.02	0-1	

Multiplet Table

N IV—Continued

N IV—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac							Vac						
189.437	B	(10)	8.36	73.81	2-1	2p <sup>3</sup> P°—4p' <sup>3</sup> S	166.496	B	(20)	8.36	82.82	2-3	2p <sup>3</sup> P°—7p' <sup>3</sup> D
189.386	B	(5)	8.34	73.81	1-1	UV 6.11	166.540	B	(75)	8.36	82.80	2-2	UV 6.28
189.365	B	(1)	8.33	73.81	0-1								
188.818	B	(300)	8.36	74.02	2-	2p <sup>3</sup> P°—8d <sup>3</sup> D	166.377	B	(20)	8.36	82.88	2-2	2p <sup>3</sup> P°—7p' <sup>3</sup> P
188.762	B	(300w)*	8.34	74.02	1-	UV 6.12	166.337	B	(10)	8.34	82.88	1-2	UV 6.29
188.743	B		8.33	74.02	0-1		164.048	B	(50)	8.36	83.93	2-3	2p <sup>3</sup> P°—8p' <sup>3</sup> D
						UV 6.30							
188.656	B	(250)	8.36	74.08	2-1	2p <sup>3</sup> P°—8s <sup>3</sup> S	163.972	B	(2)	8.36	83.97	2-2	2p <sup>3</sup> P°—8p' <sup>3</sup> P
188.606	B	(200w)*	8.34	74.08	1-1	UV 6.13							UV 6.31
188.583	B	(200w)*	8.33	74.08	0-1								
187.194	B	(20)	8.36	74.59	2-1	2p <sup>3</sup> P°—9s <sup>3</sup> S	162.423	B	(10)	8.36	84.69	2-3	2p <sup>3</sup> P°—9p' <sup>3</sup> D
187.142	B	(10)	8.34	74.59	1-1	UV 6.14							UV 6.32
187.123	B	(10)	8.33	74.59	0-1		162.374	B	(2)	8.36	84.71	2-2	2p <sup>3</sup> P°—9p' <sup>3</sup> P
186.759	B	(300d)	8.36	74.74	2-	2p <sup>3</sup> P°—9d <sup>3</sup> D							UV 6.33
186.709	B	(250d)*	8.34	74.74	1-	UV 6.15	161.286	B	(2d)	8.36	85.23	2-3	2p <sup>3</sup> P°—10p' <sup>3</sup> D
186.690	B	(250d)*	8.33	74.74	0-1								UV 6.34
185.623	B	(5)	8.36	75.15	2-1	2p <sup>3</sup> P°—10s <sup>3</sup> S	161.256	B	(2d)	8.36	85.24	2-2	2p <sup>3</sup> P°—10p' <sup>3</sup> P
185.568	B	(3)	8.34	75.15	1-1	UV 6.16							UV 6.35
185.306	B	(200d)	8.36	75.26	2-	2p <sup>3</sup> P°—10d <sup>3</sup> D	160.451	B	(1d)	8.36	85.63	2-	2p <sup>3</sup> P°—11p' <sup>3</sup> P
185.257	B	(150d)*	8.34	75.26	1-	UV 6.17							UV 6.36
185.237	B	(150d)*	8.33	75.26	0-1		159.833	B	(1d)	8.36	85.93	2-	2p <sup>3</sup> P°—12p' <sup>3</sup> P
184.485	B	(2)	8.36	75.56	2-1	2p <sup>3</sup> P°—11s <sup>3</sup> S							UV 6.37
184.437	B	(1)	8.34	75.56	1-1	UV 6.18	159.366	B	(1d)	8.36	86.15	2-	2p <sup>3</sup> P°—13p' <sup>3</sup> P
184.247	B	(75d)*	8.36	75.65	2-	2p <sup>3</sup> P°—11d <sup>3</sup> D							UV 6.38
184.200	B	(75d)*	8.34	75.65	1-	UV 6.19							
183.450	B	(50d)*	8.36	75.94	2-	2p <sup>3</sup> P°—12d <sup>3</sup> D	Air						
183.402	B	(50d)*	8.34	75.94	1-	UV 6.20	2219.61	P		16.20	21.79	1-2	2p <sup>1</sup> P°—2p' <sup>3</sup> P
							2225.78	P		16.20	21.77	1-1	UV 6.39
182.827	B	(30d)	8.36	76.17	2-	2p <sup>3</sup> P°—13d <sup>3</sup> D	2229.38	P		16.20	21.76	1-0	
182.779	P		8.34	76.17	1-	UV 6.21							
							Vac						
182.323	B	(20d)	8.36	76.36	2-	2p <sup>3</sup> P°—14d <sup>3</sup> D	1718.551	A	20	16.20	23.42	1-2	2p <sup>1</sup> P°—2p' <sup>1</sup> D
182.275	P	(20d)	8.34	76.36	1-	UV 6.22							UV 7
181.943	B	(10d)	8.36	76.50	2-	2p <sup>3</sup> P°—15d <sup>3</sup> D	955.335	A	20	16.20	29.18	1-0	2p <sup>1</sup> P°—2p' <sup>1</sup> S
181.895			8.34	76.50	1-	UV 6.23							UV 8
177.602	B	(100w)*	8.36	78.17	2-3	2p <sup>3</sup> P°—5p' <sup>3</sup> D	405.530	P		16.20	46.78	1-1	2p <sup>1</sup> P°—3s <sup>3</sup> S
177.646	B	(250)	8.36	78.15	2-2	UV 6.24							UV 8.01
177.621	B	(100w)*	8.34	78.14	1-1		387.353	C	4	16.20	48.21	1-0	2p <sup>1</sup> P°—3s <sup>1</sup> S
													UV 9
177.163	B	(200)	8.36	78.34	2-2	2p <sup>3</sup> P°—5p' <sup>3</sup> P							
177.142	B		8.34	78.33	1-1	UV 6.25	345.595	P		16.20	52.08	1-2	2p <sup>1</sup> P°—3d <sup>3</sup> D
177.182	B	(100w)*	8.36	78.33	2-1		345.600	P		16.20	52.08	1-1	UV 9.01
177.119	B	(100w)*	8.34	78.34	1-2								
170.463	B	(50)	8.36	81.09	2-3	2p <sup>3</sup> P°—6p' <sup>3</sup> D	335.052	B	11	16.20	53.21	1-2	2p <sup>1</sup> P°—3d <sup>1</sup> D
170.505	B	(100)	8.36	81.07	2-2	UV 6.26							UV 10
170.249	B	(100)	8.36	81.18	2-2	2p <sup>3</sup> P°—6p' <sup>3</sup> P	285.561	B	(600)	16.20	59.62	1-1	2p <sup>1</sup> P°—3p' <sup>1</sup> P
170.208	B	(50)	8.34	81.18	1-2	2p <sup>3</sup> P°—6p' <sup>3</sup> P							UV 11

Multiplet Table

## N IV—Continued

## N IV—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 82.565	P		16.20	60.08	1-2	2p $^1\text{P}^\circ - 3p' ^3\text{D}$	Vac 209.842	B	(150w)	16.20	75.29	1-2	2p $^1\text{P}^\circ - 10d ^1\text{D}$
82.642	P		16.20	60.07	1-1	UV 11.01							UV 12.16
80.180	P		16.20	60.45	1-1	2p $^1\text{P}^\circ - 4s ^3\text{S}$	208.510	B	(100d)	16.20	75.66	1-2	2p $^1\text{P}^\circ - 11d ^1\text{D}$
						UV 11.02							UV 12.17
74.946	P		16.20	61.30	1-2	2p $^1\text{P}^\circ - 3p' ^3\text{P}$	207.500	B	(20d)	16.20	75.95	1-2	2p $^1\text{P}^\circ - 12d ^1\text{D}$
75.016			16.20	61.28	1-1	UV 11.03							UV 12.18
75.058			16.20	61.28	1-0		206.707	B	(10d)	16.20	76.18	1-2	2p $^1\text{P}^\circ - 13d ^1\text{D}$
74.451	B	(250)	16.20	61.38	1-0	2p $^1\text{P}^\circ - 4s ^1\text{S}$	200.340	B	(300)	16.20	78.09	1-1	2p $^1\text{P}^\circ - 5p' ^1\text{P}$
						UV 11.04							UV 12.20
72.219	P		16.20	61.75	1-1	2p $^1\text{P}^\circ - 3p' ^3\text{S}$	191.228	B	(100)	16.20	81.04	1-1	2p $^1\text{P}^\circ - 6p' ^1\text{P}$
						UV 11.05							UV 12.21
70.994	B	(650)	16.20	61.95	1-2	2p $^1\text{P}^\circ - 3p' ^1\text{D}$	190.625	B	(200)	16.20	81.24	1-2	2p $^1\text{P}^\circ - 6p' ^1\text{D}$
						UV 12							UV 12.22
62.638	P		16.20	63.41	1-2	2p $^1\text{P}^\circ - 4d ^3\text{D}$	186.218	B	(50)	16.20	82.78	1-2	2p $^1\text{P}^\circ - 7p' ^1\text{P}$
62.642	P		16.20	63.41	1-1	UV 12.01							
60.447	B	(600)	16.20	63.81	1-2	2p $^1\text{P}^\circ - 4d ^1\text{D}$	185.853	B	(75)	16.20	82.91	1-2	2p $^1\text{P}^\circ - 7p' ^1\text{D}$
						UV 12.02							UV 12.24
59.824	B	(450)	16.20	63.92	1-0	2p $^1\text{P}^\circ - 3p' ^1\text{S}$	183.146	B	(5d)	16.20	83.90	1-1	2p $^1\text{P}^\circ - 8p' ^1\text{P}$
						UV 12.03							UV 12.25
40.363	B	(200)	16.20	67.78	1-0	2p $^1\text{P}^\circ - 5s ^1\text{S}$	182.894	B	(10)	16.20	83.99	1-2	2p $^1\text{P}^\circ - 8p' ^1\text{D}$
						UV 12.04							UV 12.26
36.068	B	(550)	16.20	68.72	1-2	2p $^1\text{P}^\circ - 5d ^1\text{D}$	180.928	B	(5)	16.20	84.73	1-2	2p $^1\text{P}^\circ - 9p' ^1\text{D}$
						UV 12.05							UV 12.27
27.026	B	(100)	16.20	70.81	1-0	2p $^1\text{P}^\circ - 6s ^1\text{S}$	179.554	B	(2)	16.20	85.25	1-2	2p $^1\text{P}^\circ - 10p' ^1\text{D}$
						UV 12.06							UV 12.28
24.629	B	(450w)	16.20	71.40	1-2	2p $^1\text{P}^\circ - 6d ^1\text{D}$	178.547	B	(1)	16.20	85.64	1-2	2p $^1\text{P}^\circ - 11p' ^1\text{D}$
						UV 12.07							UV 12.29
20.280	B	(400)	16.20	72.49	1-1	2p $^1\text{P}^\circ - 4p' ^1\text{P}$							
						UV 12.08							
220.124	B	(50)	16.20	72.53	1-0	2p $^1\text{P}^\circ - 7s ^1\text{S}$							
						UV 12.09							
218.250	B	(400)	16.20	73.01	1-2	2p $^1\text{P}^\circ - 7d ^1\text{D}$	437.083	P		21.79	50.15	2-1	2p <sup>2</sup> $^3\text{P} - 3p ^1\text{P}^\circ$
						UV 12.10	436.845	P		21.77	50.15	1-1	UV 12.30
							436.706	P		21.76	50.15	0-1	
217.218	B	(500)	16.20	73.28	1-2	2p $^1\text{P}^\circ - 4p' ^1\text{D}$	434.235	P		21.79	50.34	2-2	2p <sup>2</sup> $^3\text{P} - 3p ^3\text{P}^\circ$
						UV 12.11	434.067	P		21.77	50.33	1-1	UV 12.31
215.755	B	(75)	16.20	73.67	1-0	2p $^1\text{P}^\circ - 4p' ^1\text{S}$	434.302	P		21.79	50.33	2-1	
						UV 12.12	434.097	P		21.77	50.33	1-0	
							434.000	P		21.77	50.34	1-2	
214.843	B	(10)	16.20	73.91	1-0	2p $^1\text{P}^\circ - 8s ^1\text{S}$	433.930	P		21.76	50.33	0-1	
						UV 12.13							
214.291	B	(250)	16.20	74.06	1-2	2p $^1\text{P}^\circ - 8d ^1\text{D}$	345.062	B		21.79	57.72	2-2	2p <sup>2</sup> $^3\text{P} - 3s' ^3\text{P}^\circ$
						UV 12.14	345.111	B		21.77	57.70	1-1	UV 13
							345.261	B		21.79	57.70	2-1	
							345.207	B		21.77	57.69	1-0	
211.679	B	(250d)	16.20	74.77	1-2	2p $^1\text{P}^\circ - 9d ^1\text{D}$	344.916	B		21.77	57.72	1-2	
						UV 12.15	345.025	B		21.76	57.70	0-1	

Multiplet Table

N IV - Continued

N IV - Continued

IA	Ref	Int	E P		J	Multiplet No.	IA	Ref	Int	E P		J	Multiplet No.	
			Low	High						Low	High			
vac							Vac							
1365	P		21.79	58.65	2-1	$2p^2 \ ^3P - 3s' \ ^1P^\circ$	217.895	B	(500d)	21.79	78.69	2-	$2p^2 \ ^3P - 5d' \ ^3P^\circ$	
1224	P		21.77	58.65	1-1	UV 13.01	217.836	P		21.77	78.69	1-	UV 15.06	
1141	P		21.76	58.65	0-1									
1003	P		21.79	61.78	2-2	$2p^2 \ ^3P - 3d' \ ^1D^\circ$	210.028	B	(200)	21.79	80.82	2-2	$2p^2 \ ^3P - 6s' \ ^3P^\circ$	
1883	P		21.77	61.78	1-2	UV 13.02	210.056	P		21.77	80.79	1-1	UV 15.07	
1927	P		21.79	62.45	2-2	$2p^2 \ ^3P - 4p \ ^3P^\circ$	210.111	B	(100w)*	21.79	80.79	2-1		
.800	P		21.77	62.45	1-1	UV 13.03	209.976	B		21.77	80.78	1-0		
.916	P		21.79	62.45	2-1		210.024	P		21.76	80.79	0-1		
.793	P		21.77	62.45	1-0									
.811	P		21.77	62.45	1-2		208.150	B	(400w)*	21.79	81.35	2-3	$2p^2 \ ^3P - 6d' \ ^3D^\circ$	
.733	P		21.76	62.45	0-1		208.131	B		21.77	81.34	1-2	UV 15.08	
.124	B		(500w)*	21.79	62.69	2-3	$2p^2 \ ^3P - 3d' \ ^3D^\circ$	208.113	B		21.76	81.34	0-1	
.048	C			21.77	62.68	1-2	UV 14	208.185	P		21.79	81.34	2-2	
.006	B			21.76	62.68	0-1		208.144	P		21.77	81.34	1-1	
.162	B			21.79	62.68	2-2		208.066	B	(400d)	21.79	81.37	2-	$2p^2 \ ^3P - 6d' \ ^3P^\circ$
.078	B			21.77	62.68	1-1		208.012	P		21.77	81.37	1-	UV 15.09
.191	B			21.79	62.68	2-1								
.816	B	(700)		21.79	63.42	2-2	$2p^2 \ ^3P - 3d' \ ^3P^\circ$	203.694	B	(50w)*	21.79	82.65	2-2	$2p^2 \ ^3P - 7s' \ ^3P'$
.657	B		(600w)*	21.77	63.42	1-1	UV 15	203.728	P		21.77	82.63	1-1	UV 15.10
.770	B			21.79	63.42	2-1		203.780	B	(50)	21.79	82.63	2-1	
.634	B			21.77	63.43	1-0		203.642	B	(50w)*	21.77	82.65	1-2	
.704	B			21.77	63.42	1-2		202.595	B	(500w)	21.79	82.98	2-	$2p^2 \ ^3P - 7d' \ ^3D^\circ$
.595	C			21.76	63.42	0-1								UV 15.11
461	B	(500w)*		21.79	71.69	2-2	$2p^2 \ ^3P - 4s' \ ^3P^\circ$	202.485	B	(300d)	21.79	83.02		$2p^2 \ ^3P - 7d' \ ^3P^\circ$
484	B	(500w)*		21.77	71.67	1-1	UV 15.01							UV 15.12
563	B		(450w)*	21.79	71.67	2-1		199.857	B	(50)	21.79	83.82	2-2	$2p^2 \ ^3P - 8s' \ ^3P^\circ$
540	B			21.77	71.66	1-0		199.806	B	(20)	21.77	83.82	1-2	UV 15.13
383	B			21.77	71.69	1-2								
433	B	(500w)*		21.76	71.67	0-1		199.159	B	(450w)	21.79	84.04	2-	$2p^2 \ ^3P - 8d' \ ^3D^\circ$
212	B		(450w)*	21.79	73.62	2-3	$2p^2 \ ^3P - 4d' \ ^3D^\circ$	199.087	B	(200d)	21.79	84.06	2-	$2p^2 \ ^3P - 8d' \ ^3P^\circ$
174	B			21.77	73.61	1-2	UV 15.02						UV 15.14	
146	B			21.76	73.61	0-1		199.087	B					
243	B			21.79	73.61	2-2		197.343	B	(2)	21.79	84.61	2-	$2p^2 \ ^3P - 9s' \ ^3P^\circ$
188	P			21.77	73.61	1-1		196.866	B	(500w)	21.79	84.76	2-	$2p^2 \ ^3P - 9d' \ ^3D^\circ$
259	P			21.79	73.61	2-1		196.802	B	(100d)	21.79	84.79	2-	$2p^2 \ ^3P - 9d' \ ^3P^\circ$
302	B	(600)		21.79	73.71	2-2	$2p^2 \ ^3P - 4d' \ ^3P^\circ$	195.610	B	(1)	21.79	85.17	2-2	$2p^2 \ ^3P - 10s' \ ^3P^\circ$
594	B		(300w)*	21.77	73.71	1-1	UV 15.03	195.258	B	(100d)	21.79	85.28	2-	$2p^2 \ ^3P - 10d' \ ^3D^\circ$
769	B			21.79	73.71	2-1		195.202	B	(20d)	21.79	85.30	2-	UV 15.21
583	B	(500w)*		21.77	73.72	1-0		194.083	B	(75d)	21.79	85.67		$2p^2 \ ^3P - 11d' \ ^3D^\circ$
731	B		21.77	73.71	1-2								UV 15.22	
557	B		21.76	73.71	0-1									
789	B	(450)		21.79	77.69	2-2	$2p^2 \ ^3P - 5s' \ ^3P^\circ$	196.802	B	(100d)	21.79	84.79	2-	$2p^2 \ ^3P - 15.18$
310	P		(300w)*	21.77	77.67	1-1	UV 15.04	195.610	B	(1)	21.79	85.17	2-2	$2p^2 \ ^3P - 15.19$
171	B			21.79	77.67	2-1		195.258	B	(100d)	21.79	85.28	2-	$2p^2 \ ^3P - 15.20$
154	B			21.77	77.66	1-0		195.202	B	(20d)	21.79	85.30	2-	$2p^2 \ ^3P - 15.21$
29	B			21.77	77.69	1-2		194.083	B	(75d)	21.79	85.67		
74	P			21.76	77.67	0-1								
88	B		(400w)*	21.79	78.64	2-3	$2p^2 \ ^3P - 5d' \ ^3D^\circ$	194.083	B					
67	B			21.77	78.63	1-2	UV 15.05							
44	B			21.76	78.62	0-1								
16	B			21.79	78.63	2-2								
79	P			21.77	78.62	1-1								
38	P			21.79	78.62	2-1								

Multiplet Table

## N IV - Continued

## N IV - Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 192.533	B	(10d)	21.79	86.18		$2p^2 \ ^3P - 13d' \ ^3D^\circ$ UV 15.23	Vac 250.121	B	(300)	23.42	72.99	2-2	$2p^2 \ ^1D - 4d' \ ^1D^\circ$ UV 18.12
463.740	B	(650)	23.42	50.15	2-1	$2p^2 \ ^1D - 3p' \ ^1P^\circ$ UV 15.24	248.654	B	(450)	23.42	73.28	2-3	$2p^2 \ ^1D - 4d' \ ^1F^\circ$ UV 18.13
460.532 460.607	P P		23.42	50.34	2-2	$2p^2 \ ^1D - 3p' \ ^3P^\circ$	244.100	B	(300w)	23.42	74.21	2-1	$2p^2 \ ^1D - 4d' \ ^1P^\circ$ UV 18.14
460.607	P		23.42	50.33	2-1	UV 15.25	227.446	P		23.42	77.91	2-1	$2p^2 \ ^1D - 5s' \ ^1P^\circ$ UV 18.15
361.462 361.679	P P		23.42	57.72	2-2	$2p^2 \ ^1D - 3s' \ ^3P^\circ$ UV 15.26	223.421 <sup>a</sup>	P	(500d)	23.42	78.91	2-1	$2p^2 \ ^1D - 5d' \ ^1P^\circ$ UV 18.16
351.931	C	(500w)	23.42	58.65	2-1	$2p^2 \ ^1D - 3s' \ ^1P^\circ$ UV 16	214.414	B	(50d)	23.42	81.24	2-3	$2p^2 \ ^1D - 6d' \ ^1F^\circ$ UV 18.17
323.178	B	(600w)	23.42	61.78	2-2	$2p^2 \ ^1D - 3d' \ ^1D^\circ$ UV 17	213.443 <sup>a</sup>	P	(300d)	23.42	81.50	2-1	$2p^2 \ ^1D - 6d' \ ^1P^\circ$ UV 18.19
317.664 317.653	P P		23.42	62.45	2-2	$2p^2 \ ^1D - 4p' \ ^3P^\circ$	207.812 <sup>a</sup>	P	(200d)	23.42	83.08	2-1	$2p^2 \ ^1D - 7d' \ ^1P^\circ$ UV 18.20
315.708 315.751 315.785	P P P		23.42	62.69	2-3	$2p^2 \ ^1D - 3d' \ ^3D^\circ$	204.354 <sup>a</sup>	B	(150d)	23.42	84.10	2-1	$2p^2 \ ^1D - 8d' \ ^1P^\circ$ UV 18.21
315.060	B	(600)	23.42	62.77	2-3	$2p^2 \ ^1D - 3d' \ ^1F^\circ$ UV 18	201.988	B	(100d)	23.42	84.80	2-1	$2p^2 \ ^1D - 9d' \ ^1P^\circ$ UV 18.22
314.324	B	(20)	23.42	62.86	2-1	$2p^2 \ ^1D - 4p' \ ^1P^\circ$ UV 18.01	200.316	P		23.42	85.31	2-1	$2p^2 \ ^1D - 10d' \ ^1P^\circ$ UV 18.23
309.956 309.907	P P		23.42	63.42	2-2	$2p^2 \ ^1D - 3d' \ ^3P^\circ$							
305.177 305.185	P P		23.42	64.04	2-3	$2p^2 \ ^1D - 4f' \ ^3F^\circ$	591.180	P		29.18	50.15	0-1	$2p^2 \ ^1S - 3p' \ ^1P^\circ$ UV 18.24
303.280	B	(500)	23.42	64.30	2-1	$2p^2 \ ^1D - 3d' \ ^1P^\circ$ UV 18.04	586.104	P		29.18	50.33	0-1	$2p^2 \ ^1S - 3p' \ ^3P^\circ$ UV 18.25
300.318	B	(650)	23.42	64.70	2-3	$2p^2 \ ^1D - 4f' \ ^1F^\circ$ UV 18.05	434.779	P		29.18	57.70	0-1	$2p^2 \ ^1S - 3s' \ ^3P^\circ$ UV 18.26
276.741	B	(10)	23.42	68.22	2-1	$2p^2 \ ^1D - 5p' \ ^1P^\circ$ UV 18.06	420.769	B	(500)	29.18	58.65	0-1	$2p^2 \ ^1S - 3s' \ ^1P^\circ$ UV 18.27
273.140	B	(300)	23.42	68.81	2-3	$2p^2 \ ^1D - 5f' \ ^1F^\circ$ UV 18.07	368.108	B	(450)	29.18	62.86	0-1	$2p^2 \ ^1S - 4p' \ ^1P^\circ$ UV 18.29
260.519	P		23.42	71.01	2-1	$2p^2 \ ^1D - 6p' \ ^1P^\circ$ UV 18.08	353.056	B	(700)	29.18	64.30	0-1	$2p^2 \ ^1S - 3d' \ ^1P^\circ$ UV 18.30
258.320	B	(150)	23.42	71.41	2-3	$2p^2 \ ^1D - 6f' \ ^1F^\circ$ UV 18.09	317.596	B	(200)	29.18	68.22	0-1	$2p^2 \ ^1S - 5p' \ ^1P^\circ$ UV 18.31
255.148	B	(380)	23.42	72.01	2-1	$2p^2 \ ^1D - 4s' \ ^1P^\circ$ UV 18.10	296.418	P		29.18	71.01	0-1	$2p^2 \ ^1S - 6p' \ ^1P^\circ$ UV 18.32
250.566	P		23.42	72.90	2-1	$2p^2 \ ^1D - 7p' \ ^1P^\circ$ UV 18.11							

<sup>a</sup> Observed members of this series are shifted to longer waves by 0.309 Å to 0.052 Å (n=5 to 8), when autoionization is effective.

Multiplet Table

N IV — Continued

N IV — Continued

I A	Ref	Int.	E P		J	Multiplet No.	I A	Ref	Int.	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 289.479	B	(300)	29.18	72.01	0-1	$2p^2 \ ^1S - 4s' \ ^1P^o$ UV 18.33	Air 6380.77	A	8	48.21	50.15	0-1	$3s \ ^1S - 3p \ ^1P^o$ 2
283.599	P		29.18	72.90	0-1	$2p^2 \ ^1S - 7p \ ^1P^o$ UV 18.34	5835.11	P		48.21	50.33	0-1	$3s \ ^1S - 3p \ ^3P^o$ 2.01
275.354	B	(450)	29.18	74.21	0-1	$2p^2 \ ^1S - 4d' \ ^1P^o$ UV 18.35	Vac 1306.909	P		48.21	57.70	0-1	$3s \ ^1S - 3s' \ ^3P^o$ UV 18.48
254.338	B	(100)	29.18	77.91	0-1	$2p^2 \ ^1S - 5s' \ ^1P^o$ UV 18.36	1188.006	A	6	48.21	58.65	0-1	$3s \ ^1S - 3s' \ ^1P^o$ UV 18.49
249.316	B	(300d)	29.18	78.91	0-1	$2p^2 \ ^1S - 5d' \ ^1P^o$ UV 18.37	846.215	P		48.21	62.86	0-1	$3s \ ^1S - 4p \ ^1P^o$ UV 18.50
236.954	B	(150d)	29.18	81.50	0-1	$2p^2 \ ^1S - 6d' \ ^1P^o$ UV 18.38	770.678	P		48.21	64.30	0-1	$3s \ ^1S - 3d' \ ^1P^o$ UV 18.51
230.035	B	(100d)	29.18	83.08	0-1	$2p^2 \ ^1S - 7d' \ ^1P^o$ UV 18.39	619.663	P		48.21	68.22	0-1	$3s \ ^1S - 5p \ ^1P^o$ UV 18.52
225.741	B	(50d)	29.18	84.10	0-1	$2p^2 \ ^1S - 8d' \ ^1P^o$ UV 18.40	520.934	P		48.21	72.01	0-1	$3s \ ^1S - 4s' \ ^1P^o$ UV 18.53
222.893	B	(30d)	29.18	84.80	0-1	$2p^2 \ ^1S - 9d' \ ^1P^o$ UV 18.41	476.909	P		48.21	74.21	0-1	$3s \ ^1S - 4d' \ ^1P^o$ UV 18.54
220.885	B	(2d)	29.18	85.31	0-1	$2p^2 \ ^1S - 10d' \ ^1P^o$ UV 18.42							
Air 670.35	P		—	—			Air 6438.53 6440.11	P		50.15	52.08	1-2	$3p \ ^1P^o - 3d \ ^3D$ 2.02
678.71	A	15	46.78	50.34	1-2	$3s \ ^3S - 3p \ ^3P^o$	4057.759	A	8	50.15	53.21	1-2	$3p \ ^1P^o - 3d \ ^1D$ 3
82.99	A	14	46.78	50.33	1-1	1	Vac 1309.557	A	4	50.15	59.62	1-1	$3p \ ^1P^o - 3p' \ ^1P$ UV 18.55
84.96	A	13	46.78	50.33	1-0								
Vac 33.117	A	4	46.78	57.72	1-2	$3s \ ^3S - 3s' \ ^3P^o$ UV 18.43	1248.868	P		50.15	60.08	1-2	$3p \ ^1P^o - 3p' \ ^3D$ UV 18.56
35.244	A	3	46.78	57.70	1-1		1250.378	P		50.15	60.07	1-1	
36.241	A	2	46.78	57.69	1-0		1203.587	P		50.15	60.45	1-1	$3p \ ^1P^o - 4s \ ^3S$ UV 18.57
91.045	P		46.78	62.45	1-2	$3s \ ^3S - 4p \ ^3P^o$							
91.095	P		46.78	62.45	1-1	UV 18.44	1112.600	P		50.15	61.30	1-2	$3p \ ^1P^o - 3p' \ ^3P$
91.167	P		46.78	62.45	1-0		1113.749	P		50.15	61.28	1-1	
							1114.446	P		50.15	61.28	1-0	
45.020	P		46.78	63.42	1-2	$3s \ ^3S - 3d' \ ^3P^o$							
44.737	P		46.78	63.42	1-1	UV 18.45	1104.542	P		50.15	61.38	1-0	$3p \ ^1P^o - 4s \ ^1S$ UV 18.59
44.566	P		46.78	63.43	1-0								
77.696	P		46.78	71.69	1-2	$3s \ ^3S - 4s' \ ^3P^o$	1069.255	P		50.15	61.75	1-1	$3p \ ^1P^o - 3p' \ ^3S$ UV 18.60
78.106	P		46.78	71.67	1-1	UV 18.46							
78.323	P		46.78	71.66	1-0		1050.602	P		50.15	61.95	1-2	$3p \ ^1P^o - 3p' \ ^1D$ UV 18.61
10.394	P		46.78	73.71	1-2	$3s \ ^3S - 4d' \ ^3P^o$							
10.272	P		46.78	73.71	1-1	UV 18.47	908.057	P		50.15	63.81	1-2	$3p \ ^1P^o - 4d \ ^1D$ UV 18.62
10.217	P		46.78	73.72	1-0								

Multiplet Table

## N IV - Continued

## N IV - Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 900.516	P		50.15	63.92	1-0	3p <sup>1</sup> P° - 3p' <sup>1</sup> S UV 18.63	Vac 948.540 948.244 948.155	A	5	50.34	63.41	2-3	3p <sup>3</sup> P° - 4d <sup>3</sup> D UV 18.79
703.191	P		50.15	67.78	1-0	3p <sup>1</sup> P° - 5s <sup>1</sup> S UV 18.64	720.510 720.327 720.244	A	4	50.33	63.41	1-2	
667.653	P		50.15	68.72	1-2	3p <sup>1</sup> P° - 5d <sup>1</sup> D UV 18.65		P	2	50.33	67.55	1-1	3p <sup>3</sup> P° - 5s <sup>3</sup> S UV 18.80
600.061	P		50.15	70.81	1-0	3p <sup>1</sup> P° - 6s <sup>1</sup> S UV 18.66				50.33	67.55	0-1	
583.601	P		50.15	71.40	1-2	3p <sup>1</sup> P° - 6d <sup>1</sup> D UV 18.67	1323.98 1325.685 1326.964	A	2	52.08	61.44	3-4	3d <sup>3</sup> D - 3d' <sup>3</sup> F° UV 18.81
555.126	P		50.15	72.49	1-1	3p <sup>1</sup> P° - 4p' <sup>1</sup> P UV 18.68	1195.852 1195.567 1195.400	P		52.08	62.45	3-2	3d <sup>3</sup> D - 4p <sup>3</sup> P° UV 18.82
554.137	P		50.15	72.53	1-0	3p <sup>1</sup> P° - 7s <sup>1</sup> S UV 18.69	1168.599 1169.063	A	3	52.08	62.69	3-3	3d <sup>3</sup> D - 3d' <sup>3</sup> D° UV 18.83
542.412	P		50.15	73.01	1-2	3p <sup>1</sup> P° - 7d <sup>1</sup> D UV 18.70	1169.478	A	2	52.08	62.68	2-2	
536.082	P		50.15	73.28	1-2	3p <sup>1</sup> P° - 4p' <sup>1</sup> D UV 18.71	1036.16	A	1	52.08	62.68	1-1	
527.259	P		50.15	73.67	1-0	3p <sup>1</sup> P° - 4p' <sup>1</sup> S UV 18.72	1446.114	A	8w	52.08	64.05		3d <sup>3</sup> D - 4f <sup>3</sup> F° UV 18.84
521.845	P		50.15	73.91	1-0	3p <sup>1</sup> P° - 8s <sup>1</sup> S UV 18.73	1296.600	A	5	53.21	62.77	2-3	3d <sup>1</sup> D - 3d' <sup>1</sup> F° UV 18.86
518.600	P		50.15	74.06	1-2	3p <sup>1</sup> P° - 8d <sup>1</sup> D UV 18.74	1284.218	A	3	53.21	62.86	2-1	3d <sup>1</sup> D - 4p <sup>1</sup> P° UV 18.87
Air							1078.708	A	6	53.21	64.70	2-3	3d <sup>1</sup> D - 4f <sup>1</sup> F° UV 18.88
7122.98	A	5	50.34	52.08	2-3	3p <sup>3</sup> P° - 3d <sup>3</sup> D							
7109.40	A	3	50.33	52.08	1-2								
7103.28	A	2	50.33	52.08	0-1								
7127.27	A	1	50.34	52.08	2-2								
7111.30	A	1	50.33	52.08	1-1								
7129.18	P		50.34	52.08	2-1								
Vac													
1270.280	A	5	50.34	60.10	2-3	3p <sup>3</sup> P° - 3p' <sup>3</sup> D UV 18.75		Air					
1272.160	A	4	50.33	60.08	1-2								
1273.47	A	3	50.33	60.07	0-1								
1272.74	A	2	50.34	60.08	2-2								
1273.716	A	2	50.33	60.07	1-1								
1274.285	P		50.34	60.07	2-1								
1225.719	A	4	50.34	60.45	2-1	3p <sup>3</sup> P° - 4s <sup>3</sup> S UV 18.76							
1225.192	A	3	50.33	60.45	1-1								
1224.960	A	1	50.33	60.45	0-1								
1131.488	P		50.34	61.30	2-2	3p <sup>3</sup> P° - 3p' <sup>3</sup> P UV 18.77							
1132.225	P		50.33	61.28	1-1								
1086.691	A	2	50.34	61.75	2-1	3p <sup>3</sup> P° - 3p' <sup>3</sup> S UV 18.78							
1086.269	A	1	50.33	61.75	1-1								
m1086.084	P	N 1	50.33	61.75	0-1		12727.43	P		58.65	59.62	1-1	3s' <sup>1</sup> P° - 3p' <sup>1</sup> P 7.02

Multiplet Table

N IV -Continued

N IV -Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air 4538.32	P		58.65	61.38	1-0	$3s' \ ^1P^o - 4s \ ^1S$ 7.03	Vac 1702.006	A	5	61.44	68.73	4-	$3d' \ ^3F^o - 5g \ ^3G$ UV 18.91
3747.54	A	6	58.65	61.95	1-2	$3s' \ ^1P^o - 3p' \ ^1D$ 8	1699.03 1696.86	A	4	61.43	68.73	3-	
2402.05	A	5	58.65	63.81	1-2	$3s' \ ^1P^o - 4d \ ^1D$ UV 18.89	1246.51 1244.92 m1243.73	A	3	61.42	68.73	2-	
5736.94	A	4	59.62	61.78	1-2	$3p' \ ^1P^o - 3d' \ ^1D^o$ 9	Air 6119.23	P	2	61.44	71.39	4-	$3d' \ ^3F^o - 6g \ ^3G$ UV 18.92
3823.95	A	0	59.62	62.86	1-1	$3p' \ ^1P^o - 4p \ ^1P^o$ 10	5288.25	P	1	61.43	71.39	3-	
2649.88	P		59.62	64.30	1-1	$3p' \ ^1P^o - 3d' \ ^1P^o$ UV 18.90		N v	1243.73	61.42	71.39	2-	
9222.99	P		60.10	61.44	3-4	$3p' \ ^3D - 3d' \ ^3F^o$ 10.01	12870.47	P		62.45	63.41	2-3	$4p \ ^3P^o - 4d \ ^3D$ 18
9182.16	P		60.08	61.43	2-3		12892.88	P		62.45	63.41	1-2	
9165.07	P		60.07	61.42	1-2		12916.03	P		62.45	63.41	0-1	
9311.55	P		60.10	61.43	3-3								
9247.04	P		60.08	61.42	2-2		2430.41	A	3	62.45	67.55	2-1	$4p \ ^3P^o - 5s \ ^3S$ UV 18.93
9378.29	P		60.10	61.42	3-2		2431.07	A	2	62.45	67.55	1-1	
							2431.55	A	0	62.45	67.55	0-1	
4786.92	P		60.10	62.69	3-3	$3p' \ ^3D - 3d' \ ^3D^o$ 11	2035.57	A	5	62.45	68.54	2-3	$4p \ ^3P^o - 5d \ ^3D$
4762.09	P		60.08	62.68	2-2		2036.10	A	4	62.45	68.54	1-2	
4747.96	P		60.07	62.68	1-1		2036.42	A	1	62.45	68.54	0-1	
4796.66	P		60.10	62.68	3-2								
4769.86	P		60.08	62.68	2-1								
4752.49	P		60.08	62.69	2-3								
4740.26	P		60.07	62.68	1-2								
3735.43	P		60.10	63.42	3-2	$3p' \ ^3D - 3d' \ ^3P^o$ 12	2080.34	A	6	62.77	68.73	3-4	$3d' \ ^1F^o - 5g \ ^1G$ UV 18.95
3707.39	P		60.08	63.42	2-1								
3689.94	P		60.07	63.43	1-0		Vac 1438.37	A	3	62.77	71.39	3-4	$3d' \ ^1F^o - 6g \ ^1G$ UV 18.96
3714.43	P		60.08	63.42	2-2								
3694.14	P		60.07	63.42	1-1								
3701.13	P		60.07	63.42	1-2								
3141.16	A	3p	60.10	64.05	3-4	$3p' \ ^3D - 4f \ ^3F^o$ 12.01	Air 2318.09	A	6w	63.41	68.76		$4d \ ^3D - 5f \ ^3F^o$ UV 18.97
3127.41	A	2p	60.08	64.04	2-3								
3118.79	A	1p	60.07	64.04	1-2								
6219.09	A	4	60.45	62.45	1-2	$4s \ ^2S - 4p \ ^3P^o$ 12.02	2421.65	A	3	63.42	68.54	2-3	$3d \ ^3P^o - 5d \ ^3D$
6215.43	A	3	60.45	62.45	1-1		2424.73	A	2	63.42	68.54	1-2	
6212.41	A	1	60.45	62.45	1-0		2426.54	A	1	63.43	68.54	0-1	
5843.84	P		61.30	63.42	2-2	$3p' \ ^3P - 3d' \ ^3P^o$ 15	2477.69	A	8	63.81	68.81	2-3	$4d \ ^1D - 5f \ ^1F^o$ UV 18.991
5795.09	P		61.28	63.42	1-1								
5826.43	P		61.30	63.42	2-1								
5784.76	P		61.28	63.43	1-0								
5812.31	P		61.28	63.42	1-2								
5776.31	P		61.28	63.42	0-1		2646.956 2646.176 2645.654	A	12 11 10	64.05 64.04 64.04	68.73 68.73 68.73	4- 3- 2-	$4f \ ^3F^o - 5g \ ^3G$ UV 19

Multiplet Table

## N IV—Continued

## N IV—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 1688.11 1687.82 1687.60	A A A	3 2 1	64.05 64.04 64.04	71.39 71.39 71.39	4- 3- 2-	4f <sup>3</sup> F°-6g <sup>3</sup> G UV 20	Air 2884.77	A	4w	68.73	73.02		5g <sup>3</sup> G -7h <sup>3</sup> H° UV 21
Air 3078.25	A	6	64.70	68.73	3-4	4f <sup>1</sup> F°-5g <sup>1</sup> G 19	4707.31	A	4h	68.76	71.39		5f <sup>3</sup> F°-6g <sup>3</sup> G 21
4606.33	A	6	68.73	71.42		5g <sup>3</sup> G -6h <sup>3</sup> H° 20	7582.40	A	2wl	71.39	73.02		6g <sup>3</sup> G -7h <sup>3</sup> H° 22
							7702.96	A	4ws	71.42	73.03		6h <sup>3</sup> H°-7i <sup>3</sup> I 23

**NSRDS-NBS 3, SECTION 4**

**NITROGEN, Z = 7**

A N v      Atomic Energy Levels

B N v      Multiplet Table

## Atomic Energy Levels

### Part A

### NITROGEN

#### N V

Li I sequence; 3 electrons

$Z = 7$

Ground state  $1s^2 2s^2 S_{0\frac{1}{2}}$

$2s^2 S_{0\frac{1}{2}} \mathbf{789537.2 \pm 3.0 \text{ cm}^{-1}, 126.656 \text{ \AA (Vac)}}$

I P 97.888 eV

The analysis is from Hallin, who has observed the spectrum in the range 200 Å to 8000 Å with a theta pinch discharge as source. On the basis of these new measurements he has calculated unperturbed energy levels for the entire term system. The limit quoted above is determined from extended Ritz formulae for levels with  $l=0$  and 1 and from the polarization formula for those with  $l \geq 2$ .

Tilford has observed the spectrum from 128 Å to 266 Å with a low-pressure, high-voltage condensed capillary discharge as source, and extended the observed  $ns$ -series to  $n=10$ , the  $np$ -series to  $n=17$  and the  $nd$ -series to  $n=18$ . From a Ritz-Rydberg formula he derives the limit  $789516 \pm 24 \text{ cm}^{-1}$  as compared with  $789534.4 \text{ cm}^{-1}$  calculated by Hallin from the  $^2S$  series by an extended Ritz formula.

In the table the energy levels obtained from the observations are quoted from Hallin, supplemented by his calculated unperturbed values for the series to  $n=10$ . All calculated values are entered in brackets.

Tilford is quoted for the  $nd^2D$  terms ( $n=9, 10$ ) and for all other  $ns, np, nd$  terms having  $n > 10$ . Hallin notes that in the region 140 Å to 250 Å the difference between his calculated wavelengths and the measurements by Tilford ranges from  $+0.002 \text{ \AA}$  to  $-0.006 \text{ \AA}$ , which introduces appreciable differences in the level values. It has been suggested by Edlén that the large and almost constant intervals observed experimentally by Tilford in the  $nd^2D$  terms, amounting to about  $21 \pm 9 \text{ cm}^{-1}$ , may result from some sort of Stark Effect. The predicted intervals are small for these terms.

#### REFERENCES

S. G. Tilford, J. Opt. Soc. Am. **53**, No. 9, 1051–1054 (1963). I P, T, C L

R. Hallin, Ark. Fys. (Stockholm) **31**, No. 36, 511–526 (1966). I P, T, C L, G D, Stark Effect

#### N V

#### N V

Config.	Desig.	$J$	Level	Interval	Config.	Desig.	$J$	Level	Interval
2s	$2s^2 S$	$0\frac{1}{2}$	0.0		4p	$4p^2 P^o$	$0\frac{1}{2}$ $1\frac{1}{2}$	$615141.0$ $615173.8$	32.8
2p	$2p^2 P^o$	$0\frac{1}{2}$ $1\frac{1}{2}$	90463.2 80721.9	258.7	4d	$4d^2 D$	$1\frac{1}{2}$ $2\frac{1}{2}$	617916.3 617925.5	9.2
3s	$3s^2 S$	$0\frac{1}{2}$	456126.6						
3p	$3p^2 P^o$	$0\frac{1}{2}$ $1\frac{1}{2}$	477765.7 477842.0	76.3	4f	$4f^2 F^o$	$2\frac{1}{2}$ $3\frac{1}{2}$	$618059.3$ $618064.1$	[4.8]
3d	$3d^2 D$	$1\frac{1}{2}$ $2\frac{1}{2}$	484404.3 484426.3	22.0	5s	$5s^2 S$	$0\frac{1}{2}$	673886.2	
4s	$4s^2 S$	$0\frac{1}{2}$	606348.8		5p	$5p^2 P^o$	$0\frac{1}{2}$ $1\frac{1}{2}$	$678300.4$ $678316.5$	16.1

A7 v-1

### Atomic Energy Levels

#### N V - Continued

#### N V - Continued

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval
5d	5d <sup>2</sup> D	1½ 2½	[679712.7] 679717.6	[4.9]	9s	9s <sup>2</sup> S	0½	[754677.0]	
5f	5f <sup>2</sup> F°	2½, 3½	679790.4		9p	9p <sup>2</sup> P°	0½ 1½	[755411.5] [755414.3]	[2.8]
5g	5g <sup>2</sup> G	3½, 4½	679802.3		9d	9d <sup>2</sup> D	1½ 2½	755608 755633	25
6s	6s <sup>2</sup> S	0½	709939.2		9f	9f <sup>2</sup> F°	2½, 3½	[755666.5]	
6p	6p <sup>2</sup> P°	0½ 1½	712463.2 712472.6	9.4	9g	9g <sup>2</sup> G	3½, 4½	[755667.9]	
6d	6d <sup>2</sup> D	1½ 2½	713279.3 713281.5	2.2	9h	9h <sup>2</sup> H°	4½, 5½	[755668.4]	
6f	6f <sup>2</sup> F°	2½, 3½	713324.7		9i	9i <sup>2</sup> I	5½, 6½	[755668.6]	
6g	6g <sup>2</sup> G	3½, 4½	713328.9		9k	9k <sup>2</sup> K°	6½, 7½	[755668.7]	
6h	6h <sup>2</sup> H°	4½, 5½	713334.8		10s	10s <sup>2</sup> S	0½	[761382.7]	
7s	7s <sup>2</sup> S	0½	731425.4		10p	10p <sup>2</sup> P°	0½ 1½	[761916.3] [761918.3]	[2.0]
7p	7p <sup>2</sup> P°	0½ 1½	[733003.3] [733009.2]	[5.9]	10d	10d <sup>2</sup> D	1½ 2½	762048 762071	23
7d	7d <sup>2</sup> D	1½ 2½	[733515.4] [733517.2]	[1.8]	10f	10f <sup>2</sup> F°	2½, 3½	[762102.1]	
7f	7f <sup>2</sup> F°	2½, 3½	733542.7		10g	10g <sup>2</sup> G	3½, 4½	[762103.1]	
7g	7g <sup>2</sup> C	3½, 4½	[733549.0]		10h	10h <sup>2</sup> H°	4½, 5½	[762103.5]	
7h	7h <sup>2</sup> H°	4½, 5½	[733549.9]		10i	10i <sup>2</sup> I	5½, 6½	[762103.6]	
7i	7i <sup>2</sup> I	5½, 6½	[733550.4]		10k	10k <sup>2</sup> K°	6½, 7½	[762103.7]	
8s	8s <sup>2</sup> S	0½	[745255.6]		10l	10l <sup>2</sup> L	7½, 8½	[762103.8]	
8p	8p <sup>2</sup> P°	0½ 1½	[746306.0] [746309.9]	[3.9]	11p	11p <sup>2</sup> P°	0½, 1½	766687	
8d	8d <sup>2</sup> D	1½ 2½	[746648.5] [746649.7]	[1.2]	11d	11d <sup>2</sup> D	1½, 2½	766866	
8f	8f <sup>2</sup> F°	2½, 3½	[746669.2]		12p	12p <sup>2</sup> P°	0½, 1½	770347	
8g	8g <sup>2</sup> G	3½, 4½	[746671.3]		12d	12d <sup>2</sup> D	1½, 2½	770483	
8h	8h <sup>2</sup> H°	4½, 5½	[746671.9]		13p	13p <sup>2</sup> P°	0½, 1½	773174	
8i	8i <sup>2</sup> I	5½, 6½	[746672.2]		13d	13d <sup>2</sup> D	1½, 2½	773282	
8k	8k <sup>2</sup> K°	6½, 7½	[746672.4]		14p	14p <sup>2</sup> P°	0½, 1½	775465	
					14d	14d <sup>2</sup> D	1½, 2½	775581	
					15p	15p <sup>2</sup> P°	0½, 1½	777230	

Atomic Energy Levels

**N v - Continued**

**N v - Continued**

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval
15d	15d <sup>2</sup> D	1½, 2½	777490		17d	17d <sup>2</sup> D	1½, 2½	780117	
16p	16p <sup>2</sup> P°	0½, 1½	778634		18d	18d <sup>2</sup> D	1½, 2½	781067	
16d	16d <sup>2</sup> D	1½, 2½	778847		.....	.....	.....	.....	.....
17p	17p <sup>2</sup> P°	0½, 1½	779855		N VI ( <sup>1</sup> S <sub>0</sub> )	<b>Limit</b> .....	.....	<b>789537.2 ± 3.0</b>	

July 1970.

### Multiplet Table

Part B

### NITROGEN

#### N V ( $Z = 7$ )

I P 91.888eV      Limit  $789537.2 \pm 3.0$        $126.656 \text{ \AA}$  (Vac)

Anal A      List A      July 1970

#### REFERENCES

- A R. Hallin, Ark. Fys. (Stockholm) **31**, No. 36, 511–526 (1966). I P, T, C L, G D, I; W L 140 Å to 7618 Å
- B S. G. Tilford, J. Opt. Soc. Am. **53**, No. 9, 1051–1054 (1963). I P, T, C L, (I); W L 128 Å to 1242 Å. (Note that intensities from Reference B are entered in parentheses).
- P Predicted wavelengths from Ref A, Table 4 and from calculated unperturbed energy levels in Ref A, Table 5.

New Multiplet Numbers, not inserted between older ones, start with UV 7 and 13.

\*Blend

\* and § Blend of N V and N IV

N V									N V								
I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.				
			Low	High						Low	High						
Vac 238.821‡ 242.804	A A	20 19	0.00 0.00	10.01 9.98	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 2p^2P^o$ UV 1	Vac 131.254	B	(5)	0.00 94.46	$0\frac{1}{2}-$ $2s^2S - 10p^2P^o$ UV 3.06						
209.274 209.308	P P	(80) (80)	0.00 0.00	59.24 59.23	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 3p^2P^o$ UV 2	130.431	B	(4)	0.00 95.05	$0\frac{1}{2}-$ $2s^2S - 11p^2P^o$ UV 3.07						
162.556 162.564	P P	(48) (48)	0.00 0.00	76.27 76.27	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 4p^2P^o$ UV 3	129.811	B	(3)	0.00 95.51	$0\frac{1}{2}-$ $2s^2S - 12p^2P^o$ UV 3.08						
147.424 147.427	P P	(24) (24)	0.00 0.00	84.10 84.10	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 5p^2P^o$ UV 3.01	129.337	B	(2)	0.00 95.86	$0\frac{1}{2}-$ $2s^2S - 13p^2P^o$ UV 3.09						
140.356 140.358	P P	(16) (16)	0.00 0.00	88.33 88.33	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 6p^2P^o$ UV 3.02	128.954	B	(1)	0.00 96.14	$0\frac{1}{2}-$ $2s^2S - 14p^2P^o$ UV 3.10						
136.429	B	(8)	0.00	90.88	$0\frac{1}{2}-$	$2s^2S - 7p^2P^o$ UV 3.03	128.662	B	(1)	0.00 96.36	$0\frac{1}{2}-$ $2s^2S - 15p^2P^o$ UV 3.11						
133.994	B	(7)	0.00	92.53	$0\frac{1}{2}-$	$2s^2S - 8p^2P^o$ UV 3.04	128.430	B	(0)	0.00 96.54	$0\frac{1}{2}-$ $2s^2S - 16p^2P^o$ UV 3.12						
132.383	B	(6)	0.00	93.66	$0\frac{1}{2}-$	$2s^2S - 9p^2P^o$ UV 3.05	128.229	B	(0)	0.00 96.69	$0\frac{1}{2}-$ $2s^2S - 17p^2P^o$ UV 3.13						

Multiplet Table

## N v -Continued

## N v -Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.	
			Low	High						Low	High			
Vac														
266.379	A	(84)	10.01	56.55	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 3s^2S$	Vac	143.241	B	(1)	10.01	96.56	$\frac{1}{2}-$	$2p^2P^o - 16d^2D$
266.196	A	(80)	9.98	56.55	$0\frac{1}{2}-0\frac{1}{2}$	UV 4								UV 24
247.706	A	(100)	10.01	60.06	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 3d^2D$	142.981	B	(0)	10.01	96.72	$\frac{1}{2}-$	$2p^2P^o - 17d^2D$	
247.561	A	(85)	9.98	60.06	$0\frac{1}{2}-1\frac{1}{2}$	UV 5								UV 25
190.249	P	(32)	10.01	75.18	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 4s^2S$	142.797	B	(0)	10.01	96.84	$\frac{1}{2}-$	$2p^2P^o - 18d^2D$	
190.155	P	(20)	9.98	75.18	$0\frac{1}{2}-0\frac{1}{2}$	UV 5.01								UV 26
186.149	P	(62)	10.01	76.61	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 4d^2D$								
186.063	P	(52)	9.98	76.61	$0\frac{1}{2}-1\frac{1}{2}$	UV 6								
168.587	P	(12)	10.01	83.55	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 5s^2S$	Air							
168.514	P	(5)	9.98	83.55	$0\frac{1}{2}-0\frac{1}{2}$	UV 7	4603.73	A	12	56.55	59.24	$0\frac{1}{2}-1\frac{1}{2}$	$3s^2S - 3p^2P^o$	
166.946	P	(52)	10.01	84.27	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 5d^2D$	4619.98	A	10	56.55	59.23	$0\frac{1}{2}-0\frac{1}{2}$	1	
166.875	P	(44)	9.98	84.27	$0\frac{1}{2}-1\frac{1}{2}$	UV 8	Vac							
158.928	P	(7)	10.01	88.02	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 6s^2S$	628.744	A	5	56.55	76.27	$0\frac{1}{2}-1\frac{1}{2}$	$3s^2S - 4p^2P^o$	
158.862	P	(4)	9.98	88.02	$0\frac{1}{2} \ 0\frac{1}{2}$	UV 9	628.874	A	3	56.55	76.27	$0\frac{1}{2}-0\frac{1}{2}$	UV 27	
158.088	P	(36)	10.01	88.43	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 6d^2D$	450.072	P	3*	56.55	84.10	$0\frac{1}{2}-1\frac{1}{2}$	$3s^2S - 5p^2P^o$	
158.024	P	(24)	9.98	88.43	$0\frac{1}{2}-1\frac{1}{2}$	UV 10	450.105	P	3*	56.55	84.10	$0\frac{1}{2}-0\frac{1}{2}$	UV 28	
153.683	B	(6)	10.01	90.68	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 7s^2S$	390.102	P		56.55	88.33	$0\frac{1}{2}-1\frac{1}{2}$	$3s^2S - 6p^2P^o$	
153.624	B	(3)	9.98	90.68	$0\frac{1}{2}-0\frac{1}{2}$	UV 11	390.116	P		56.55	88.33	$0\frac{1}{2}-0\frac{1}{2}$	UV 29	
153.192	B	(28)	10.01	90.94	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 7d^2D$								
153.136	B	(18)	9.98	90.94	$0\frac{1}{2}-1\frac{1}{2}$	UV 12								
150.488	B	(5)	10.01	92.40	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 8s^2S$	Air	15185.80	P		59.24	60.06	$\frac{1}{2}-2\frac{1}{2}$	$3p^2P^o - 3d^2D$
150.429	B	(2)	9.98	92.40	$0\frac{1}{2}-0\frac{1}{2}$	UV 13		15061.34	P		59.23	60.06	$0\frac{1}{2}-1\frac{1}{2}$	1.01
150.171	B	(14)	10.01	92.57	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 8d^2D$	Vac							
150.116	B	(7)	9.98	92.57	$0\frac{1}{2}-1\frac{1}{2}$	UV 14	778.172	A	2	59.24	75.18	$\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 4s^2S$	
148.387	B	(4)	10.01	93.57	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 9s^2S$		777.712	A	1	59.23	75.18	$0\frac{1}{2}-0\frac{1}{2}$	UV 30
148.328	B	(1)	9.98	93.57	$0\frac{1}{2}-0\frac{1}{2}$	UV 15	713.860	A	8	59.24	76.61	$\frac{1}{2}-2\frac{1}{2}$	$3p^2P^o - 4d^2D$	
148.168	B	(7)	10.01	93.68	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 9d^2D$		713.518	A	6	59.23	76.61	$0\frac{1}{2}-1\frac{1}{2}$	UV 31
148.116	B	(4)	9.98	93.68	$0\frac{1}{2}-1\frac{1}{2}$	UV 16	510.096	P		59.24	83.55	$\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 5s^2S$	
146.921	B	(3)	10.01	94.40	$\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 10s^2S$		509.896	P		59.23	83.55	$0\frac{1}{2}-0\frac{1}{2}$	UV 32
146.767	B	(6)	10.01	94.48	$\frac{1}{2}-2\frac{1}{2}$	$2p^2P^o - 10d^2D$		495.356	P		59.24	84.27	$\frac{1}{2}-2\frac{1}{2}$	$3p^2P^o - 5d^2D$
146.716	B	(3)	9.98	94.48	$0\frac{1}{2}-1\frac{1}{2}$	UV 18	495.180	P		59.23	84.27	$0\frac{1}{2}-1\frac{1}{2}$	UV 33	
145.742	B	(5)	10.01	95.08	$\frac{1}{2}-$	$2p^2P^o - 11d^2D$		430.857	P		59.24	88.02	$\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 6s^2S$
144.978	B	(4)	10.01	95.53	$\frac{1}{2}-$	$2p^2P^o - 12d^2D$		430.714	P		59.23	88.02	$0\frac{1}{2}-0\frac{1}{2}$	UV 34
144.392	B	(3)	10.01	95.87	$\frac{1}{2}-$	$2p^2P^o - 13d^2D$		424.75	A	2	59.24	90.68	$\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 7s^2S$
143.914	B	(2)	10.01	96.16	$\frac{1}{2}-$	$2p^2P^o - 14d^2D$		424.61	A	1	59.23	90.68	$0\frac{1}{2}-0\frac{1}{2}$	UV 36
143.520	B	(1)	10.01	96.39	$\frac{1}{2}-$	$2p^2P^o - 15d^2D$		391.123	P		59.24	90.94	$\frac{1}{2}-2\frac{1}{2}$	$3p^2P^o - 7d^2D$
						UV 22		391.008	P		59.23	90.94	$0\frac{1}{2}-1\frac{1}{2}$	UV 37
								764.840	P		60.06	76.27	$2\frac{1}{2}-1\frac{1}{2}$	$3d^2D - 4p^2P^o$
								764.896	P		60.06	76.27	$1\frac{1}{2}-0\frac{1}{2}$	UV 38

Multiplet Table

## N V -Continued

## N V -Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 748.291 748.195	A A	9 8	60.06 60.06	76.63 76.63	$\frac{1}{2}-\frac{3}{2}$ $\frac{1}{2}-\frac{1}{2}$	$3d^2D - 4f^2F^o$ UV 39	Air 2590.81 2591.44	A A	2 1	83.55 83.55	88.33 88.33	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$5s^2S - 6p^2P^o$ UV 55
515.757 515.741	P P		60.06 60.06	84.10 84.10	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$3d^2D - 5p^2P^o$ UV 40							
511.834	A	5	60.06	84.28		$3d^2D - 5f^2F^o$ UV 41	3161.38 3159.75	A A	3 2	84.10 84.10	88.02 88.02	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$5p^2P^o - 6s^2S$ 2
436.85	A	4	60.06	88.44		$3d^2D - 6f^2F^o$ UV 42	2859.16 2858.03	A A	5l 4	84.10 84.10	88.43 88.43	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$5p^2P^o - 6d^2D$ UV 56
Air 1327.57 1368.92	P P		75.18 75.18	76.27 76.27	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4s^2S - 4p^2P^o$ 1.02	Vac 1882.92 1882.36	A A	1 0	84.10 84.10	90.68 90.68	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$5p^2P^o - 7s^2S$ UV 57
Vac 1389.514 1389.822	A A	3 2	75.18 75.18	84.10 84.10	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4s^2S - 5p^2P^o$ UV 43							
942.278 942.361	P P		75.18 75.18	88.33 88.33	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4s^2S - 6p^2P^o$ UV 44	Air 2974.52	A	6p	84.27	88.44		$5d^2D - 6f^2F^o$ UV 59
1703.218 1702.258	A A	4 3*	76.27 76.27	83.55 83.55	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4p^2P^o - 5s^2S$ UV 45	Vac 1857.88 1857.69	A A	3l 3l	84.27 84.27	90.95 90.95	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$5d^2D - 7f^2F^o$ UV 60
1549.336 1548.647	A P	6	76.27 76.27	84.27 84.27	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4p^2P^o - 5d^2D$ UV 46	Air 2980.78	A	8wl	84.28	88.44		$5f^2F^o - 6g^2G$ UV 61
1055.229 1054.871	P P		76.27 76.27	88.02 88.02	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4p^2P^o - 6s^2S$ UV 47	Vac 1860.37	A	6w	84.28	90.95		$5f^2F^o - 7g^2G$ etc. UV 62 etc.
019.278 018.973	P P		76.27 76.27	88.43 88.43	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4p^2P^o - 6d^2D$ UV 48	Vac 1495.5	A	2w	84.28	92.57		$5f^2F^o - 8g^2G$ etc. UV 63 etc.
655.879 656.065	P P	2* 2*	76.61 76.61	84.10 84.10	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$4d^2D - 5p^2P^o$ UV 49							
616.328	A	9wl	76.61	84.28		$4d^2D - 5f^2F^o$ UV 50	Air 2981.31	A	10wl	84.28	88.44		$5g^2G - 6h^2H^o$ UV 64
048.20	A	2w	76.61	88.44		$4d^2D - 6f^2F^o$ UV 51	Vac 1860.37	A	6w	84.28	90.95		$5g^2G - 7h^2H^o$ etc. UV 65 etc.
621.966	A	1	76.63	84.27		$4f^2F^o - 5d^2D$ UV 52	1495.5	A	2w	84.28	92.57		$5g^2G - 8h^2H^o$ etc. UV 66 etc.
619.688	A	12wl	76.63	84.28		$4f^2F^o - 5g^2G$ UV 53							
049.65	A	3w	76.63	88.44		$4f^2F^o - 6g^2G$ UV 54	Air 4333.38 4334.49	P P		88.02 88.02	90.88 90.88	$\frac{1}{2}-\frac{1}{2}$ $\frac{1}{2}-\frac{1}{2}$	$6s^2S - 7p^2P^o$ 3

Multiplet Table

## Nv — Continued

## Nv — Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air 5274.66 5272.04	P P		88.33 88.33	90.68 90.68	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$6p^2P^o - 7s^2S$ 4	Air 4944.49	P		88.44	90.95		$6g^2G - 7h^2H^o$ etc. 10 etc.
4750.57 4748.86	P P		88.33 88.33	90.94 90.94	$1\frac{1}{2}-2\frac{1}{2}$ $0\frac{1}{2}-1\frac{1}{2}$	$6p^2P^o - 7d^2D$ 5	4944.71	P		—	—		$6h^2H^o - 7i^2I$ etc. 10.01 etc.
5067.60 5068.40	P P		88.43 88.43	90.88 90.88	$2\frac{1}{2}-1\frac{1}{2}$ $1\frac{1}{2}-0\frac{1}{2}$	$6d^2D - 7p^2P^o$ 6				—	—		
4933.36 4932.68	P P		88.43 88.43	90.95 90.95	$2\frac{1}{2}-$ $1\frac{1}{2}-2\frac{1}{2}$	$6d^2D - 7f^2F^o$ 7	6716.95 6718.71	P P		90.68 90.68	92.53 92.53	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$7s^2S - 8p^2P^o$ 11
4951.32 4951.76	P P		88.44 88.44	90.94 90.94	$-2\frac{1}{2}$ $2\frac{1}{2}-1\frac{1}{2}$	$6f^2F^o - 7d^2D$ 8	7329.09 7326.57	P P		—	—		$7p^2P^o - 8d^2D$ 12
4944.56	A	9w	88.44	90.95		$6f^2F^o - 7g^2G$ etc. 9 etc.				90.88 90.88	92.57 92.57	$1\frac{1}{2}-2\frac{1}{2}$ $0\frac{1}{2}-1\frac{1}{2}$	
2998.43	A	5w	88.44	92.57		$6f^2F^o - 8g^2G$ etc. 9.01 etc.	7618.46	A	5w	90.95	92.57		$7g^2G - 8h^2H^o$ etc. 13 etc.

**NSRDS-NBS 3, SECTION 4**

**NITROGEN, Z = 7**

**A N VI Atomic Energy Levels**

**B N VI Multiplet Table**

## Atomic Energy Levels

Part A

### NITROGEN

#### N VI

He I sequence; 2 electrons

Z = 7

Ground state  $1s^2 \text{ } ^1\text{S}_0$

$1s^2 \text{ } ^1\text{S}_0$  **4452758 cm<sup>-1</sup>, 22.458 Å (Vac)**

I P 552.057 eV

In 1940 Tyrén reported his observations of the first three members of the singlet series, and the intersystem combination  $1s^2 \text{ } ^1\text{S}_0 - 2p \text{ } ^3\text{P}_1$ , in the range 23 Å to 29 Å. The resulting energy levels are given in Edlén's 1952 paper and are quoted here.

Bockasten and his colleagues have observed the triplet  $2s \text{ } ^3\text{S} - 2p \text{ } ^3\text{P}^\circ$  in a theta-pinch discharge as source. Their wavelengths have been used to obtain the levels  $2p \text{ } ^3\text{P}_{\frac{1}{2}, \frac{3}{2}}$ . The third line of the group is blended with N III. For this reason, Edlén's estimated value is quoted for  $2p \text{ } ^3\text{P}_0^\circ$  and entered in brackets in the table. The difference, o-c, is only  $-6 \text{ cm}^{-1}$ .

The remaining levels are based on the observations reported in 1966 by Fawcett and Irons. The center of gravity of the  $2p \text{ } ^3\text{P}^\circ$  term, 3438480 cm<sup>-1</sup> has been used to evaluate the  $nd \text{ } ^3\text{D}$  terms. These authors give calculated wavelengths for the combinations with terms  $np \text{ } ^3\text{P}^\circ$  and  $nd \text{ } ^3\text{D}$  to  $n = 10$ , but further observations are needed to extend the analysis.

The limit is from the theoretical work by Pekeris on the "Ground State of Two-Electron Atoms."

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- F. Tyrén, Nova Acta. Reg. Soc. Sci. Uppsala [IV] **12**, No. 1, 24–26 (1940). I P, T, C L
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- C. L. Pekeris, Phys. Rev. **112**, No. 5, 1649–1658 (1958). I P. Theory
- K. Bockasten, R. Hallin, K. B. Johansson and P. Tsui, Phys. Lett. **8**, No. 3, 181–182 (1964). C L
- B. C. Fawcett, F. E. Irons, Proc. Phys. Soc. (London) **89**, Part 4, No. 566, 1063–1064 (L) (1966).

### Atomic Energy Levels

**N VI**

**N VI**

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Internal
1s <sup>2</sup>	1s <sup>2</sup> 1S	0	0		1s 3p	3p 1P <sup>o</sup>	1	4016390	
1s 2s	2s 3S	1	3385890		1s 4p	4p 3P <sup>o</sup>	0, 1, 2	4202620	
1s 2p	2p 3P <sup>o</sup>	0 1 2	[3438310] 3438320 3438610	[10] 290	1s 4d	4d 3D	1, 2, 3	4205820	
1s 2p	2p 1P <sup>o</sup>	1	3473790		1s 4p	4p 1P <sup>o</sup>	1	4206810	
1s 3p	3p 3P <sup>o</sup>	0, 1, 2	4006160		1s 5p	5p 3P <sup>o</sup>	1, 2, 3	4293080	
1s 3d	3d 3D	1, 2, 3	4013460		1s 5d	5d 3D	1, 2, 3	4294570	
					N VII ( <sup>2</sup> S <sub>1/2</sub> )	Limit	.....	<b>4452758</b>	

July 1970

### Multiplet Table

Part B

### NITROGEN

#### N VI ( $Z=7$ )

IP 552.057 eV    Limit 4452758 cm<sup>-1</sup>    22.458 Å

Anal C    List A    July 1970

#### REFERENCES

- A F. Tyrén, Nova Acta Reg. Soc. Sci. Uppsala [IV] **12**, No. 1, 24–26 (1940). IP, T, CL; WL 23 Å to 29 Å
  - B K. Bockasten, R. Hallin, K. B. Johansson and P. Tsui, Phys. Lett. **8**, No. 3, 181–182 (1964). CL, I; WL 1896 Å to 1907 Å
  - C B. C. Fawcett, F. E. Irons, Proc. Phys. Soc. (London) **89**, Part 4, No. 566, 1063–1064 (1966). CL; WL 97 Å to 173 Å
- \* and § Blend N III and N VI

#### N VI

#### N VI

IA	Ref	Int	EP		J	Multiplet No.	IA	Ref	Int	EP		J	Multiplet No.
			Low	High						Low	High		
Vac 29.084	A		0.00	426.29	0-1	$1s^2 {}^1S - 2p {}^3P^o$ 1	Vac 161.22	C		419.79	496.69	1-	$2s {}^3S - 3p {}^3P^o$ 6
28.787‡	A		0.00	430.68	0-1	$1s^2 {}^1S - 2p {}^1P^o$ 2	122.44	C		419.79	521.05	1-	$2s {}^3S - 4p {}^3P^o$ 7
24.898	A		0.00	497.96	0-1	$1s^2 {}^1S - 3p {}^1P^o$ 3	110.23	C		419.79	532.26	1-	$2s {}^3S - 5p {}^3P^o$ 8
23.771	A		0.00	521.56	0-1	$1s^2 {}^1S - 4p {}^1P^o$ 4	173.92	C		426.31	497.59		$2p {}^3P^o - 3d {}^3D$ 9
1896.82	B	3	419.79	426.32	1-2	$2s {}^3S - 2p {}^3P^o$ 5	130.32	C		426.31	521.44		$2p {}^3P^o - 4d {}^3D$ 10
1907.34	B	2	419.79	426.29	1-1		116.81	C		426.31	532.45		$2p {}^3P^o - 5d {}^3D$ 11
1907.87§	B	2	419.79	426.29	1-0								

NSRDS-NBS 3, SECTION 4

**NITROGEN, Z = 7**

A N VII Atomic Energy Levels

B N VII Multiplet Table

## Atomic Energy Levels

### Part A

### NITROGEN

#### N VII

H I sequence; 1 electron

$Z = 7$

Ground state  $1s^2S_{0\frac{1}{2}}$

$1s^2S_{0\frac{1}{2}}$  **5380089** cm<sup>-1</sup>, 18.587 Å (Vac)

I P 667.029 eV

In 1940 Tyrén reported his observation of the first member of the Lyman series. This line was also detected in 1963 in the Zeta spectrum by the workers at Culham Laboratory, during the initial phase of their study of high-temperature plasmas. The first two members of this series, at 24.8 Å and 20.8 Å respectively, were identified in the far ultraviolet solar spectrum by R. L. Blake and his colleagues in 1964.

The terms listed below have been calculated by J. D. Garcia and J. E. Mack in their extensive paper on the H-like spectra, H I to Ca XX. Their values refer to the isotope <sup>14</sup>N VII for which they used the value  $R = 109733.00982$ .

Edlén has, also, calculated centre-of-gravity wavelengths of the Lyman lines  $1s - np$ ,  $n = 2$  to 7 for the natural isotope mixture, but the difference is negligible for N VII.

#### REFERENCES

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- B. Edlén, Ark. Fys. (Stockholm) **31**, No. 35, 509–510 (1966). C L

#### N VII

#### N VII

Config.	Desig.	$J$	Level	Interval	Config.	Desig.	$J$	Level	Interval	
1s	$1s^2S$	$0\frac{1}{2}$	0		4p	$4p^2P^o$	$0\frac{1}{2}$	5043853	6	
$2p$	$2p^2P^o$	$0\frac{1}{2}$	4034761	45	4s	$4s^2S$	$0\frac{1}{2}$	5043859	104	
2s	$2s^2S$	$0\frac{1}{2}$	4034806		$4p, 4d$	$4d^2D$	$4p^2P^o$	$1\frac{1}{2}$	5043963	36
$2p$	$2p^2P^o$	$1\frac{1}{2}$	4035641	835	$4d, 4f$	$4d^2D$	$4f^2F^o$	$2\frac{1}{2}$	5043999	19
					$4f$	$4f^2F^o$	$3\frac{1}{2}$	5044018		
$3p$	$3p^2P^o$	$0\frac{1}{2}$	4782263	13	5p	$5p^2P^o$	$0\frac{1}{2}$	5164916	3	
3s	$3s^2S$	$0\frac{1}{2}$	4782276		5s	$5s^2S$	$0\frac{1}{2}$	5164919	54	
$3d$	$3d^2D$	$1\frac{1}{2}$	4782523	247	$5p, 5d$	$5d^2D$	$5p^2P^o$	$1\frac{1}{2}$	5164973	18
$3p$	$3p^2P^o$	$1\frac{1}{2}$	4782524	1	$5d, 5f$	$5d^2D$	$5f^2F^o$	$2\frac{1}{2}$	5164991	10
$3d$	$3d^2D$	$2\frac{1}{2}$	4782610	86	$5f, 5g$	$5g^2G$	$5f^2F^o$	$3\frac{1}{2}$	5165001	5
					$5g$	$5g^2G$	$5g^2G$	$4\frac{1}{2}$	5165006	

# Atomic Energy Levels

## NVII – Continued

## N VII—Continued

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval
6p		6p $^2P^{\circ}$	0 $\frac{1}{2}$	5230673					
6s	6s $^2S$	0 $\frac{1}{2}$	5230675	2	11p	11p $^2P^{\circ}$	0 $\frac{1}{2}$	5335641	1
6d	6d $^2D$	1 $\frac{1}{2}$	5230705	30	11s	11s $^2S$	0 $\frac{1}{2}$	5335642	9
6p		6p $^2P^{\circ}$	1 $\frac{1}{2}$	5230706	etc.		10 $\frac{1}{2}$	to 51	
6d, 6f	6d $^2D$	2 $\frac{1}{2}$	5230716	10	12p	12p $^2P^{\circ}$	0 $\frac{1}{2}$	5342741	1
6f, 6g	6g $^2G$	3 $\frac{1}{2}$	5230722	6	12s	12s $^2S$	0 $\frac{1}{2}$	5342742	7
6g, 6h	6g $^2G$	4 $\frac{1}{2}$	5230725	3	etc.		11 $\frac{1}{4}$	to 49	
6h		6h $^2H^{\circ}$	5 $\frac{1}{2}$	5230727					
7p		7p $^2P^{\circ}$	0 $\frac{1}{2}$	5270319		13s, 13p	13s $^2S$	0 $\frac{1}{2}$	5348267
7s	7s $^2S$	0 $\frac{1}{2}$	5270320	1	etc.		12 $\frac{1}{2}$	to 72	5
7p, 7d	7d $^2D$	1 $\frac{1}{2}$	5270340	20	14s, 14p	14s $^2S$	0 $\frac{1}{2}$	5352651	
7d, 7f	7d $^2D$	2 $\frac{1}{2}$	5270346	6	etc.		13 $\frac{1}{2}$	to 55	4
7f, 7g	7g $^2G$	3 $\frac{1}{2}$	5270350	4	15s, 15p	15s $^2S$	0 $\frac{1}{2}$	5356187	
7g, 7h	7g $^2G$	4 $\frac{1}{2}$	5270352	2	etc.		14 $\frac{1}{2}$	to 91	4
7h, 7i	7i $^2I$	5 $\frac{1}{2}$	5270353	1	16s, 16p	16s $^2S$	0 $\frac{1}{2}$	5359082	
7i	7i $^2I$	6 $\frac{1}{2}$	5270354	1	etc.		15 $\frac{1}{2}$	to 85	3
8p		8p $^2P^{\circ}$	0 $\frac{1}{2}$	5296049					
8s	8s $^2S$	0 $\frac{1}{2}$	5296050	1					
8p, 8d	8d $^2D$	1 $\frac{1}{2}$	5296063	13	17s, 17p	17s $^2S$	0 $\frac{1}{2}$	5361481	
8d, 8f	8d $^2D$	2 $\frac{1}{2}$	5296068	5	etc.		16 $\frac{1}{2}$	to 83	2
8f, 8g	8g $^2G$	3 $\frac{1}{2}$	5296070	2	18s, 18p	18s $^2S$	0 $\frac{1}{2}$	5363491	
8g, 8h	8g $^2G$	4 $\frac{1}{2}$	5296071	1	etc.		17 $\frac{1}{2}$	to 93	2
8h, 8i	8i $^2I$	5 $\frac{1}{2}$	5296072	1	19s, 19p	19s $^2S$	0 $\frac{1}{2}$	5365192	
8i, 8k	8i $^2I$	6 $\frac{1}{2}$	5296073	0	etc.		18 $\frac{1}{2}$	to 94	2
8k		8k $^2K^{\circ}$	7 $\frac{1}{2}$	5296073					
9p		9p $^2P^{\circ}$	0 $\frac{1}{2}$	5313689					
9s	9s $^2S$	0 $\frac{1}{2}$	5313690	1					
9p, 9d	9d $^2D$	1 $\frac{1}{2}$	5313699	9	20s, 20p	20s $^2S$	0 $\frac{1}{2}$	5366645	
9d, 9f	9d $^2D$	2 $\frac{1}{2}$	5313702	3	etc.		19 $\frac{1}{2}$	to 46	1
9f, 9g	9g $^2G$	3 $\frac{1}{2}$	5313704	2					
9g, 9h	9g $^2G$	4 $\frac{1}{2}$	5313705	1					
9h, 9i	9i $^2I$	5 $\frac{1}{2}$	5313705	0					
9i, 9k	9i $^2I$	6 $\frac{1}{2}$	5313706	1					
9k, 9l	9l $^2L$	7 $\frac{1}{2}$	5313706	0					
9l	9l $^2L$	8 $\frac{1}{2}$	5313706	0					
10p		10p $^2P^{\circ}$	0 $\frac{1}{2}$	5326306					
10s	10s $^2S$	0 $\frac{1}{2}$	5326307	1					
10d	10d $^2D$	1 $\frac{1}{2}$	5326313	6					
10p		10p $^2P^{\circ}$	1 $\frac{1}{2}$	5326314					
10d, 10f	10d $^2D$	2 $\frac{1}{2}$	5326316	2					
10f, 10g	10g $^2G$	3 $\frac{1}{2}$	5326317	1					
10g, 10h	10g $^2G$	4 $\frac{1}{2}$	5326318	1					
10h, 10i	10i $^2I$	5 $\frac{1}{2}$	5326318	0					
10i, 10k	10i $^2I$	6 $\frac{1}{2}$	5326319	1					
10k, 10l	10l $^2L$	7 $\frac{1}{2}$	5326319	0					
10l, 10m	10l $^2L$	8 $\frac{1}{2}$	5326319	0					
10m		10m $^2M^{\circ}$	9 $\frac{1}{2}$	5326319					
						$\infty = Limit$			5380089

April 1970.

Multiplet Table

Part B

NITROGEN

**N VII (Z=7)**

I P 667.029 eV      Limit 5380089 cm<sup>-1</sup>      18.587 Å (Vac)

Anal A      List B      April 1970

REFERENCES

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B. Edlén, Ark. Fys. (Stockholm) **31**, No. 35, 509–510 (1966). C L

**N VII**

**N VII**

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 24.7792	A		0.00	500.34	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	1s <sup>2</sup> S – 2p <sup>2</sup> P°	Vac 18.6976	A		0.00	663.08	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 13p <sup>2</sup> P° 12
24.7846	A		0.00	500.23	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	1s <sup>2</sup> S – 2p <sup>2</sup> P° 1							
20.9095	A		0.00	592.94	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	1s <sup>2</sup> S – 3p <sup>2</sup> P°	18.6823	A		0.00	663.63	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 14p <sup>2</sup> P° 13
20.9106	A		0.00	592.91	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	1s <sup>2</sup> S – 3p <sup>2</sup> P° 2							
19.8257	A		0.00	625.36	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	1s <sup>2</sup> S – 4p <sup>2</sup> P°	18.6700	A		0.00	664.07	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 15p <sup>2</sup> P° 14
19.8261	A		0.00	625.34	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	1s <sup>2</sup> S – 4p <sup>2</sup> P° 3							
19.3612	A		0.00	640.36	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	1s <sup>2</sup> S – 5p <sup>2</sup> P°	18.6599	A		0.00	664.42	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 16p <sup>2</sup> P° 15
19.3614	A		0.00	640.35	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	1s <sup>2</sup> S – 5p <sup>2</sup> P° 4							
19.1179	A		0.00	648.51	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	1s <sup>2</sup> S – 6p <sup>2</sup> P°	18.6516	A		0.00	664.72	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 17p <sup>2</sup> P° 16
19.1180	A		0.00	648.50	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	1s <sup>2</sup> S – 6p <sup>2</sup> P° 5							
18.9741	A		0.00	653.42	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	1s <sup>2</sup> S – 7p <sup>2</sup> P°	18.6446	A		0.00	664.97	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 18p <sup>2</sup> P° 17
18.9742	A		0.00	653.42	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	1s <sup>2</sup> S – 7p <sup>2</sup> P° 6							
18.8819	A		0.00	656.61	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	1s <sup>2</sup> S – 8p <sup>2</sup> P°	18.6387	A		0.00	665.18	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 19p <sup>2</sup> P° 18
18.8820	A		0.00	656.61	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	1s <sup>2</sup> S – 8p <sup>2</sup> P° 7							
18.8193	A		0.00	658.80	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 9p <sup>2</sup> P°	18.6336	A		0.00	665.36	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 20p <sup>2</sup> P° 19
18.7747	A		0.00	660.36	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 10p <sup>2</sup> P°							
					9								
18.7419	A		0.00	661.52	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 11p <sup>2</sup> P°	133.934	A		500.34	592.91	1 $\frac{1}{2}$ –0 $\frac{1}{2}$	2p <sup>2</sup> P° – 3s <sup>2</sup> S 20
					10		133.777	A		500.23	592.91	0 $\frac{1}{2}$ –0 $\frac{1}{2}$	
18.7170	A		0.00	662.40	0 $\frac{1}{2}$ –	1s <sup>2</sup> S – 12p <sup>2</sup> P°	133.874	A		500.34	592.95	1 $\frac{1}{2}$ –2 $\frac{1}{2}$	2p <sup>2</sup> P° – 3d <sup>2</sup> D 21
					11		133.732	A		500.23	592.94	0 $\frac{1}{2}$ –1 $\frac{1}{2}$	
							133.890	A		500.34	592.94	1 $\frac{1}{2}$ –1 $\frac{1}{2}$	

Multiplet Table

## N VII—Continued

## N VII—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 99.185 99.098	A A		500.34 500.23	625.34 625.34	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 4s^2S$ 22	Vac 75.701	A		500.30	664.07		$2p^2P^o - 15d^2D$ etc. 42 etc.
99.134	A		500.30	625.36		$2p^2P^o - 4d^2D$ etc. 23 etc.				500.24	592.24	$0\frac{1}{2}-1\frac{1}{2}$	$2s^2S - 3p^2P^o$ 43
88.552 88.483	A A		500.34 500.23	640.35 640.35	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 5s^2S$ 24	133.740 133.787	A A		500.24 500.24	592.91	$0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 4p^2P^o$ 44
88.515	A		500.30	640.36		$2p^2P^o - 5d^2D$ etc. 25 etc.	99.093 99.103	A A		500.24 500.24	625.36 625.34	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 5p^2P^o$ 45
83.680 83.618	A A		500.34 500.23	648.50 648.50	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 6s^2S$ 26	88.482 88.487	A A		500.24 500.24	640.36 640.35	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 6p^2P^o$ 46
83.648	A		500.30	648.51		$2p^2P^o - 6d^2D$ etc. 27 etc.	83.619 83.621	A A		500.24 500.24	648.51 648.50	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 7p^2P^o$ 47
80.993 80.935	A A		500.34 500.23	653.42 653.42	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 7s^2S$ 28	80.937 80.938	A A		500.24 500.24	653.42 653.42	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 8p^2P^o$ 48
80.963	A		500.30	653.42		$2p^2P^o - 7d^2D$ etc. 29 etc.	79.286 79.287	A A		500.24 500.24	656.61 656.61	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 9p^2P^o$ 49
79.339 79.284	A A		500.34 500.23	656.61 656.61	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 8s^2S$ 30	78.193 78.132	A A		500.24 500.24	658.80 658.80	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2s^2S - 10p^2P^o$ 50
79.311	A		500.30	656.61		$2p^2P^o - 8d^2D$ etc. 31 etc.	77.429	A		500.24	660.36	$0\frac{1}{2}-$	
78.244 78.190	A A		500.34 500.23	658.80 658.80	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 9s^2S$ 32	382.651 382.269	A A		592.94 592.91	625.34 625.34	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 4s^2S$ 51
78.217	A		500.30	658.80		$2p^2P^o - 9d^2D$ etc. 33 etc.	261.510 261.331	A A		592.94 592.91	640.35 640.35	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 5s^2S$ 52
77.479 77.427	A A		500.34 500.23	660.36 660.36	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 10s^2S$ 34	223.139 223.009	A A		592.94 592.91	648.50 648.50	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 6s^2S$ 53
77.453	A		500.30	660.36		$2p^2P^o - 10d^2D$ etc. 35 etc.	205.004 204.894	A A		592.94 592.91	653.42 653.42	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 7s^2S$ 54
76.923 76.871	A A		500.34 500.23	661.52 661.52	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 11s^2S$ 36	194.732 194.633	A A		592.94 592.91	656.61 656.61	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 8s^2S$ 55
76.897	A		500.30	661.52		$2p^2P^o - 11d^2D$ etc. 37 etc.	188.265 188.173	A A		592.94 592.91	658.80 658.80	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 9s^2S$ 56
76.505 76.454	A A		500.34 500.23	662.40 662.40	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$2p^2P^o - 12s^2S$ 38	183.897 183.809	A A		592.94 592.91	660.36 660.36	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3p^2P^o - 10s^2S$ 57
76.480	A		500.30	662.40		$2p^2P^o - 12d^2D$ etc. 39 etc.							
76.158	A		500.30	663.08		$2p^2P^o - 13d^2D$ etc. 40 etc.	382.136 382.297	A A		592.91 592.91	625.36 625.34	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3s^2S - 4p^2P^o$ 58
75.904	A		500.30	663.63		$2p^2P^o - 14d^2D$ etc. 41 etc.	261.303 261.342	A A		592.91 592.91	640.36 640.35	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3s^2S - 5p^2P^o$ 59

## Multiplet Table

N VII - Continued													
IA	Ref	Int	EP		J	Multiplet No.	IA	Ref	Int	EP		J	Multiplet No.
			Low	High						Low	High		
Vac 223.000 223.017	A A		592.91 592.91	648.51 648.50	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3s^2S-6p^2P^\circ$ 60	Vac 396.677	A		625.36	656.61		$4d^2D-8f^2F^\circ$ etc. 78 etc.
204.891 204.900	A A		592.91 592.91	653.42 653.42	$0\frac{1}{2}-1\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$3s^2S-7p^2P^\circ$ 61	370.741	A		625.36	658.80		$4d^2D-9f^2F^\circ$ etc. 79 etc.
382.445	A		592.95	625.36		$3d^2D-4f^2F^\circ$ etc. 62 etc.	354.177	A		625.36	660.36		$4d^2D-10f^2F^\circ$ etc. 80 etc.
261.449	A		592.95	640.36		$3d^2D-5f^2F^\circ$ etc. 63 etc.	1522.024	A		640.36	648.50	$1\frac{1}{2}-0\frac{1}{2}$	$5p^2P^\circ-6s^2S$
223.106	A		592.95	648.51		$3d^2D-6f^2F^\circ$ etc. 64 etc.	1520.704	A		640.35	648.50	$0\frac{1}{2}-0\frac{1}{2}$	81
204.980	A		592.95	653.42		$3d^2D-7f^2F^\circ$ etc. 65 etc.	949.244 948.731	A A		640.36 640.35	653.42 653.42	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$5p^2P^\circ-7s^2S$
194.713	A		592.95	656.61		$3d^2D-8f^2F^\circ$ etc. 66 etc.	762.910 762.579	A A		640.36 640.35	656.61 656.61	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$5p^2P^\circ-8s^2S$
188.248	A		592.95	658.80		$3d^2D-9f^2F^\circ$ etc. 67 etc.	672.418 672.160	A A		640.36 640.35	658.80 658.80	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	82
183.881	A		592.95	660.36		$3d^2D-10f^2F^\circ$ etc. 68 etc.	619.832 619.613	A A		640.36 640.35	660.36 660.36	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$5p^2P^\circ-10s^2S$
826.747 825.996	A A		625.36 625.34	640.35 640.35	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ-5s^2S$ 69	1521.41	A		640.36	648.51		$5d^2D-6f^2F^\circ$ etc. 86 etc.
535.584 535.269	A A		625.36 625.34	648.50 648.50	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ-6s^2S$ 70	949.134	A		640.36	653.42		$5d^2D-7f^2F^\circ$ etc. 87 etc.
441.780 441.565	A A		625.36 625.34	653.42 653.42	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ-7s^2S$ 71	762.884	A		640.36	656.61		$5d^2D-8f^2F^\circ$ etc. 88 etc.
396.688 396.515	A A		625.36 625.34	656.61 656.61	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ-8s^2S$ 72	672.420	A		640.36	658.80		$5d^2D-9f^2F^\circ$ etc. 89 etc.
370.745 370.594	A A		625.36 625.34	658.80 658.80	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ-9s^2S$ 73	619.844	A		640.36	660.36		$5d^2D-10f^2F^\circ$ etc. 90 etc.
354.178 354.040	A A		625.36 625.34	660.36 660.36	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ-10s^2S$ 74							
							Air						
							2523.601 2521.500	A A		648.51 648.50	653.42 653.42	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$6p^2P^\circ-7s^2S$ 91
826.385	A		625.36	640.36		$4d^2D-5f^2F^\circ$ etc. 75 etc.	1530.362 1529.590	A A		648.51 648.50	656.61 656.61	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$6p^2P^\circ-8s^2S$ 92
535.510	A		625.36	648.51		$4d^2D-6f^2F^\circ$ etc. 76 etc.	1205.052 1204.573	A A		648.51 648.50	658.80 658.80	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$6p^2P^\circ-9s^2S$ 93
441.753	A		625.36	653.42		$4d^2D-7f^2F^\circ$ etc. 77 etc.	1046.014 1045.653	A A		648.51 648.50	660.36 660.36	$1\frac{1}{2}-0\frac{1}{2}$ $0\frac{1}{2}-0\frac{1}{2}$	$6p^2P^\circ-10s^2S$ 94