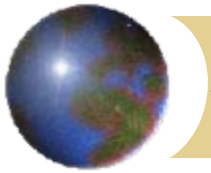


Advanced MARSSIM Topics

HPS Annual Meeting

Providence, RI

Eric W. Abelquist; eric.abelquist@ornl.gov
Oak Ridge Associated Universities



Introduction

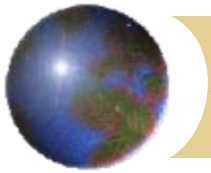
● Advanced MARSSIM Topics

- Building surface survey design for multiple contaminants; DQA using unity rule
- Soil surface survey design for multiple contaminants in Class 1—scan MDC implications
- Double Sampling if survey unit fails statistical test



Final Status Survey

- Objective: Demonstrate that residual radioactivity in **each survey unit** satisfies release criteria
- Builds on data from HSA and survey results from scoping and characterization
- Survey design includes 1) scans to identify hot spots and 2) random (statistical) samples for determining average contamination levels in survey unit



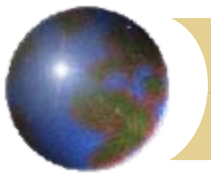
Final Status Survey (cont.)

- Null hypothesis (H_0): Residual radioactivity **exceeds** the release criteria
 - H_0 is treated like a baseline condition, assumed to be true in the absence of strong evidence to the contrary
- Decision errors occur when H_0 is rejected when it is true (Type I), or when H_0 is accepted when it is false (Type II)



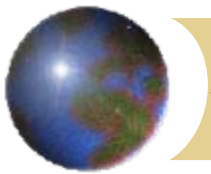
Final Status Survey (cont.)

- Two statistical tests are used to plan and evaluate final status survey data
 - Wilcoxon Rank Sum (two-sample test)
 - Sign Test (one-sample test)
 - 1) When the contaminant is **not** in background, or is present at small fraction of DCGL
 - 2) When surface activity assessment performed with average background subtracted from each measurement



Sign Test Example for Surface Activity Assessments

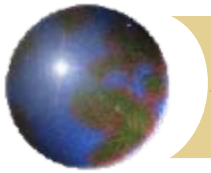
- Concrete floor potentially contaminated with Am-241, Co-60, Cs-137 and SrY-90
- Class 2 survey unit area is 320 m²
- DCGLs: 130 dpm/100 cm² Am-241
11,400 dpm/100 cm² Co-60
34,400 dpm/100 cm² SrY-90
44,000 dpm/100 cm² Cs-137
- Separate alpha and beta measurements with gas proportional detectors



Gross Activity DCGLs

- Gross alpha DCGL same as Am-241
- Gross beta DCGL must consider relationship of Co-60, SrY-90 and Cs-137
- Results of characterization provides relative ratios: 0.3 Co-60, 0.2 SrY-90 and 0.5 Cs-137

$$DCGL = \frac{1}{0.3/11,400 + 0.2/34,400 + 0.5/44,000} = 23,000 \text{ dpm}/100 \text{ cm}^2$$



Surface Material Backgrounds

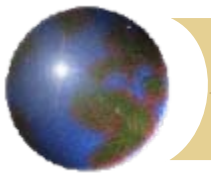
- Background levels are assessed for each surface material encountered in the survey unit (natural radioactivity from Th, U, K-40)
- Group surface types with like background levels (drywall, steel, wood)— as opposed to individual backgrounds for each
- Obtain 10 to 20 measurements of background across the surface material



Survey Instrument DQOs

- Gas proportional detector used for surface activity measurements
- Static MDC (in dpm/100 cm²) should be less than 50% DCGL

$$MDC = \frac{3 + 4.65\sqrt{C_B}}{\varepsilon_i \varepsilon_s T (P.A./100)}$$



Survey Instrument DQOs (cont.)

- Assume ε_i was determined for each beta contaminant: 0.41, 0.59, and 0.46 for Co-60, SrY-90, and Cs-137, respectively
- Determine weighted total efficiency:

| | <u>rad fraction</u> | ε_i | ε_s | <u>weighted ε_{tot}</u> |
|---------|---------------------|------------------|-----------------|--|
| Co-60 | 0.3 | 0.41 | 0.25 | 0.031 |
| Sr/Y-90 | 0.2 | 0.59 | 0.5 | 0.059 |
| Cs-137 | 0.5 | 0.46 | 0.5 | <u>0.115</u> |
| | | Total efficiency | | 0.205 |

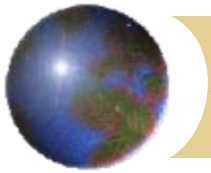


Survey Instrument DQOs (cont.)

- Assume average background counts on concrete floor is 360 cpm
- Calculate beta MDC for a 1-min count:

$$MDC = \frac{3 + 4.65 \sqrt{360}}{(0.205)^{126} / 100} = 350 \text{ dpm} / 100 \text{ cm}^2$$

- Is this MDC less than 50% of $DCGL_W$?
(yes, gross DCGL was 23,000 dpm/100 cm²)



Survey Instrument DQOs (cont.)

- Assume ϵ_i for alpha measurements calibrated to Th-230 is 0.44, and background is 2 cpm
- Alpha MDC is calculated:

$$MDC = \frac{3 + 4.65\sqrt{2}}{(0.44)(0.25)126 / 100} = 69 \text{ dpm} / 100 \text{ cm}^2$$

- Alpha MDC is just slightly greater than 50% of DCGL for 1-min count



Sign Test Example—DQO Inputs

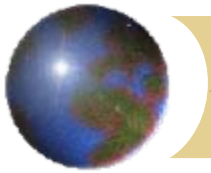
- Unity rule is used for survey design
- Characterization data used for planning:

Survey Unit (in cpm) Reference Area

Gross α 8 ± 5 (1σ) 2.0 ± 0.4 (1σ)

Gross β 1544 ± 562 (1σ) 360 ± 45 (1σ)

- Type I and II decision errors set at 0.05



Convert gross activity DCGLs to cpm using efficiencies

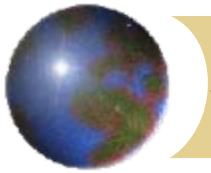
- Gross alpha DCGL:

$$(130 \text{ dpm}/100 \text{ cm}^2)(0.44)(0.25)(126/100) = 18 \text{ cpm}$$

- Gross beta DCGL:

$$(23,000 \text{ dpm}/100 \text{ cm}^2)(0.205)(126/100) = 5940 \text{ cpm}$$

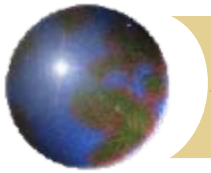
- Since Unity Rule is used: **DCGL = 1**



Calculate the relative shift— Δ/σ

- LBGR is set at expected concentration:
 $(8 - 2)/18 + (1544 - 360)/5940 = 0.53$
- Variability for measurements should consider that Sign test involves subtracting mean background from gross measurement:

$$\sigma_{total} = \sqrt{\sigma_s^2 + \sigma_r^2}$$



Measurement Variability

- ⊕ Gross alpha variability

$$\sigma_{total\ \alpha} = \sqrt{5^2 + 0.4^2} = 5\ cpm$$

- Gross beta variability

$$\sigma_{total\ \beta} = \sqrt{562^2 + 45^2} = 564\ cpm$$



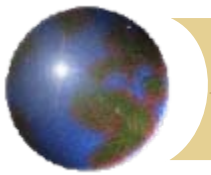
Calculate the relative shift— Δ/σ

➊ Normalized standard deviation is:

$$\sigma^2 = \left(\frac{5}{18}\right)^2 + \left(\frac{564}{5940}\right)^2 = 0.086; \quad \sigma = 0.29$$

➋ $\Delta/\sigma = (1 - 0.53)/0.29 = 1.60$

➌ MARSSIM Table 5.5 provides $N = 17$



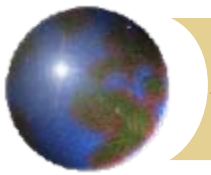
Survey Results for Concrete Floor

| Gross Alpha (cpm) | Gross Alpha (dpm/100 cm2) | Gross Beta (cpm) | Gross Beta (dpm/100 cm2) | Weighted Sum (sum of fractions) |
|----------------------|------------------------------|---------------------|-----------------------------|------------------------------------|
| 1 | -7 | 839 | 1854 | 0.03 |
| 15 | 94 | 2209 | 7158 | 1.03 |
| 2 | 0 | 380 | 77 | 0.00 |
| 1 | -7 | 991 | 2443 | 0.05 |
| 12 | 72 | 540 | 697 | 0.59 |
| 6 | 29 | 2702 | 9067 | 0.62 |
| 23 | 152 | 1856 | 5792 | 1.42 |
| 10 | 58 | 788 | 1657 | 0.52 |
| 3 | 7 | 2400 | 7898 | 0.40 |
| 11 | 65 | 439 | 306 | 0.51 |
| 5 | 22 | 902 | 2098 | 0.26 |
| 8 | 43 | 390 | 116 | 0.34 |
| 2 | 0 | 912 | 2137 | 0.09 |
| 13 | 79 | 450 | 348 | 0.63 |
| 6 | 29 | 1604 | 4816 | 0.43 |
| 4 | 14 | 12223 | 45927 | 2.11 |
| 3 | 7 | 671 | 1204 | 0.11 |
| Average | Average | Average | Average | Average |
| 7 | 39 | 1782 | 5506 | 0.54 |



Data Quality Assessment

- Average gross alpha = 39 dpm/100 cm²
(DCGL = 130 dpm/100 cm²)
- Average gross beta = 5506 dpm/100 cm²
(DCGL = 23,000 dpm/100 cm²)
- Average sum of fractions is 0.54
- Does survey unit pass?
 - How many samples are less than DCGL of 1? **S+ is 14**
 - Critical value is **12**; since $S+ > C.V.$; **survey unit passes**
- DCGL_{EMC} would be evaluated for each hot spot identified



Sign Test Example – Co-60 and Am-241 in Soil (Class 1)

- Site contaminants: Co-60 and Am-241
- Class 1 survey unit area is 1,500 m²
- Two strategies for determining need for additional samples based on scan MDCs
- RESRAD version 5.95 used to get DCGLs:
 - 3.4 pCi/g for Co-60; 11.8 pCi/g for Am-241



Sign Test – DQO Inputs

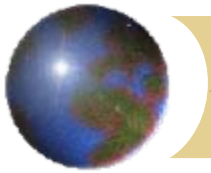
- Unity rule is used for survey design
- Characterization data used for planning:

Survey Unit

Co-60 $1.1 \pm 0.4 (1\sigma)$

Am-241 $3.8 \pm 0.8 (1\sigma)$

- Type I and II decision errors set at 0.05



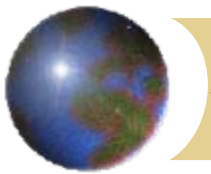
Calculate the relative shift— Δ/σ

- LBGR is set at expected concentration:

$$1.1/3.4 + 3.8/11.8 = 0.65$$

- Standard deviations from survey unit are normalized according to MARSSIM eqn I-17:

$$\sigma^2 = \left(\frac{\sigma_{Co - 60}}{DCGL_{Co - 60}} \right)^2 + \left(\frac{\sigma_{Am - 241}}{DCGL_{Am - 241}} \right)^2$$

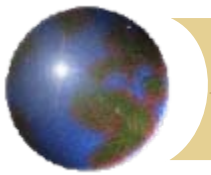


*Calculate the relative shift— Δ/σ
(cont.)*

- Normalized standard deviation is:

$$\sigma^2 = \left(\frac{0.4}{3.4}\right)^2 + \left(\frac{0.8}{11.8}\right)^2 = 0.0184; \quad \sigma = 0.14$$

- $\Delta/\sigma = (1 - 0.65)/0.14 = 2.5$
- MARSSIM Table 5.5 provides $N = 15$



Determining Need for Additional Samples in Class 1 Survey Unit

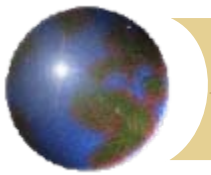
- In Class 1 areas, determine if sample size is sufficient for hot spots that may be present
- Based on n , average area bounded by sample points (a') represents largest hot spot that could exist, and not be sampled
- Requires comparison of **actual** scan MDCs for radionuclides to **required** scan MDCs



Hot Spot Considerations (cont.)

- If **Actual** Scan MDC < **Required** Scan MDC—then initial sample size sufficient
- If Actual Scan MDC > Required Scan MDC—then calculate Area Factor that corresponds to actual Scan MDC:

$$\text{Area Factor} = \frac{\text{Scan MDC}(\text{actual})}{\text{DCGL}_w}$$



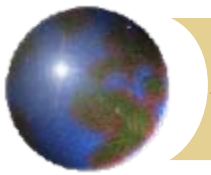
Assess data needs for Elevated Measurement Comparison test

- ⊕ 1.25" x 1.5" NaI used for scans; scan MDC for Co-60 is 5.8 pCi/g and for Am-241 is 45 pCi/g
- Area bounded by systematic samples, a' , is $1500/15 = 100 \text{ m}^2$
- Area factors associated with a' are:
 - 1.22 for Co-60 and 1.34 for Am-241



Area Factors for Co-60 and Am-241 (from RESRAD)

| <u>Area (m²)</u> | <u>Co-60</u> | <u>Am-241</u> |
|-----------------------------|--------------|---------------|
| 3000 | 1 | 1 |
| 1000 | 1.02 | 1.00 |
| 300 | 1.10 | 1.06 |
| 100 | 1.22 | 1.34 |
| 30 | 1.58 | 2.46 |
| 10 | 2.33 | 4.39 |
| 3 | 4.95 | 9.50 |
| 1 | 11.6 | 159 |



Assess data needs for EMC

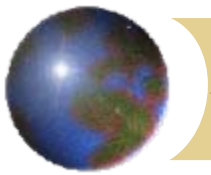
- Determine **required** scan MDC:

($DCGL_W$  Area Factor)

Co-60: $(3.4 \text{ pCi/g})(1.22) = 4.15 \text{ pCi/g}$

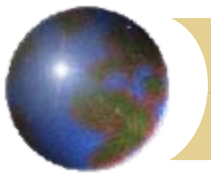
Am-241: $(11.8 \text{ pCi/g})(1.34) = 15.8 \text{ pCi/g}$

- Actual scan MDCs for both radionuclides are greater than the required scan MDCs—additional samples are needed for EMC



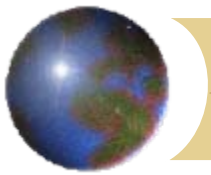
Strategies for Determining Number of Additional Samples

- ⊕ Determine which of the two radionuclides is the “driver” for the additional samples
 - ▣ Calculate ratio of actual-to-required scan MDC
 - ▣ Radionuclide with largest ratio is the driver
- ⊕ Determine reasonable ratio (or range of ratios) between the radionuclides
 - ▣ Scan MDC, DCGL, and area factors are determined for specific radionuclide mixture



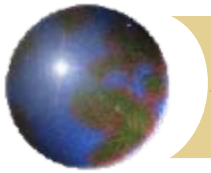
Determine “driver” for the additional samples

- Actual-to-required scan MDCs:
 - Co-60: $5.8/4.15 = 1.4$
 - Am-241: $45/15.8 = 2.8$
- Therefore, Am-241 is the driver
- AF = actual scan MDC/DCGL,
 $AF = 45/11.8 = 3.81$
- Interpolate to get area that corresponds to this AF:
a' is 13.1 m^2 ; new sample size = $1500/13.1 =$
115



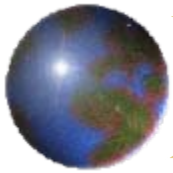
Determine reasonable ratio (or range of ratios) between the radionuclides

- Requires determination of the scan MDC for a specific mixture of Co-60 and Am-241 ...and modeling to determine $DCGL_W$ and area factors for this specific mixture (simply stated, this approach is more work!)
- Let's briefly review scan MDC calculations



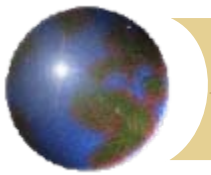
Scan MDC Determination

- Minimum detectable count rate based on signal detection theory & human factors(NUREG –1507)
- Relate MDCR in cpm to minimum detectable exposure rate (MDER) based on NaI characteristics
- Microshield™ to model specific radionuclide(s) concentration and geometry—yields exposure rate
- Scan MDC = $MDER/CF$, where CF is the exposure rate to concentration correction factor



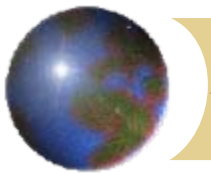
Scan MDCs For 1.25" x 1.5" NaI Detector

| <u>Radionuclide</u> | <u>Scan MDC (pCi/g)</u> |
|-----------------------|-------------------------|
| Cs-137 | 10.4 |
| Am-241 | 44.6 |
| Th-232 | 2.8 |
| Co-60 | 5.8 |
| Processed Uranium | 115 |
| Enriched Uranium (3%) | 137 |
| Ra-226 | 4.5 |



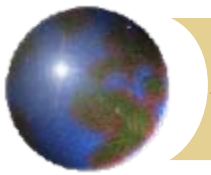
Determine Additional Sample Needs for 30% Am-241 and 70% Co-60

- Based on process knowledge and characterization, 95% confidence level on fractional amount of Am-241: 0.3 to 0.8
- Determine additional sample needs for lower bound ratio: 30% Am and 70% Co
- Calculate scan MDC—expect it to be between 5.8 pCi/g (Co-60) and 45 pCi/g (Am-241): scan MDC = 7.8 pCi/g



Determine Additional Sample Needs for 30% Am and 70% Co (cont.)

- $DCGL_W$ for 30% Am/70% Co = 4.8 pCi/g
- AFs also generated for this mixture; the AF for 100 m² (initial a') is 1.22
- Required scan MDC: $(4.8)(1.22) = 5.9$ pCi/g
—need more samples
- New AF = $7.8/4.8 = 1.62$; new a' is 29 m²;
new sample size = $1500/29 = \mathbf{52}$ samples



Determine Sample Needs for Various Am-241 to Co-60 Ratios

- Scan MDC for multiple radionuclides involves Microshield™ modeling or by observation

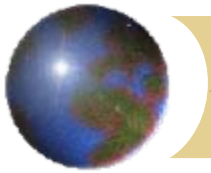
$$\text{scan MDC} = \frac{1}{\frac{f_1}{\text{scan MDC}_1} + \frac{f_2}{\text{scan MDC}_2}}$$

- For mix of 80% Am/20% Co: scan MDC using Microshield™ was 19.1; using eqn it's 19.2 pCi/g



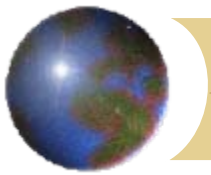
Additional Sample Needs as a Function of Am/Co Mixture

| <u>Mixture</u> | <u>DCGL</u> | <u>Scan MDC</u> | <u>Add'l Samples</u> |
|----------------|-------------|-----------------|----------------------|
| 0%Am | 3.4 | 5.8 | 62 |
| 30%Am | 4.8 | 7.8 | 52 |
| 50%Am | 6.6 | 10.3 | 42 |
| 65%Am | 9.3 | 13.4 | 29 |
| 80%Am | 14.7 | 19.2 | 0 |
| 90%Am | 13.1 | 26.9 | 35 |
| 100%Am | 11.8 | 45 | 115 |



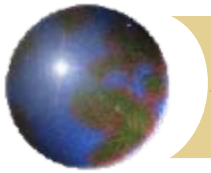
Conclusion: Strategies for Determining Number of Add'l Samples

- ✦ Using Am-241 as the “driver” requires **115** additional samples...no effort to get scan MDC for multiple radionuclides
- ✦ If range of ratios between Am and Co can be justified (e.g., 30 to 80% Am-241), the conservative additional sample size is **52**...but approach requires effort to get scan MDC, DCGL, and Area Factors



If Scan MDC Is NOT Sufficient – Reduce Scan MDC By:

- Slowing scan speed to increase observation interval; however, practical limit of several seconds on observation interval (can't keep on scanning slower)
- Use more sensitive instrument (increase efficiency)
- Accept more false positives, which requires training technicians to pause and flag spots more frequently



What If No Scan Capability At All?

- Radionuclides include alpha and beta emitters (H-3, C-14) and low energy gamma and x-ray emitters (e.g., Fe-55)
- Perform systematic sampling in survey unit & analyze samples, and assess with posting plot
- Perform second stage sampling based on results of first sampling stage
 - ▣ At locations where samples exceed $DCGL_W$
 - ▣ Where posting plot indicates potential for contamination



Other Options if Potential Hot Spots Drive Large Sample Sizes

- ⊕ Consider soil compositing
- ⊕ Consider revising the $DCGL_W$ via dose modeling – use realistic scenarios (environmental pathways) and site-specific parameters

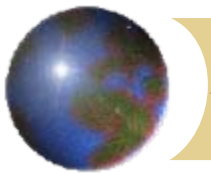


What if you fail the statistical test?

Double Sampling...perhaps

- If the mean $>$ $DCGL_W$, then you fail w/o even performing the statistical test
- Re-do the final status survey—always the case when additional remediation is necessary
- If the mean $<$ $DCGL_W$, can you collect additional samples and perform the statistical test again?

[Answer: Yes, provided that it was agreed upon with the regulator during the DQO process]



Two-Stage or Double Sampling for Final Status Surveys

- Two-stage sampling: survey design is specifically intended to be conducted in two stages
- Double sampling: when the survey design is one-stage design, but an allowance is made for a second set of samples to be taken
- Type I error increases with double sampling, but by no more than a factor of two



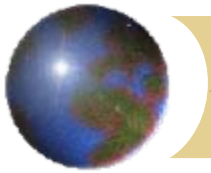
Draft NRC NUREG-1757, vol. 2, Appendix C

- "...double sampling should not be used as a substitute for adequate planning. If it is to be allowed, this should be agreed upon with NRC staff as part of the DQO process." (p. C-6)
- Note double sampling allows for one more set of additional samples...i.e., no triple sampling
- Additional samples should be collected randomly, and added to initial sample data set



Double Sampling Notes

- Double sampling should never be necessary for Class 2 or 3 survey units (data should all be less than $DCGL_W$ in these SUs)
- Statistical failures can occur as a result of poor characterization efforts; bad estimates of mean and std dev in the SU—so while the mean may be less than $DCGL_W$, the sample size is too small to reject the H_0 for the actual std dev in the SU (assess by retrospective power curve)



Double Sampling Example

- Survey design using WRS test for Th-232, $DCGL_W = 7$ pCi/g
- Limited characterization results in 4.1 pCi/g mean and 1.7 pCi/g std dev in survey unit; bkg had Th-232 concentration of 1.1 pCi/g (net 3 pCi/g in survey unit—set LBGR at 3 pCi/g)
- Relative shift: $\Delta/\sigma = (7-3)/1.7 = 2.35$;
Type I error = 0.025; Type II error = 0.1
- $N/2 = 11$ samples

WRS TEST Sample Size and Prospective Power Curve Design

This step calculates the WRS Test sample size and prospective power curve. Enter values for the DQO parameters, then click the calculate button at the bottom. When you are satisfied with this design, click the NEXT button.

Enter Values

LBGR:

Alpha:

Beta:

Calculations

DCGL:

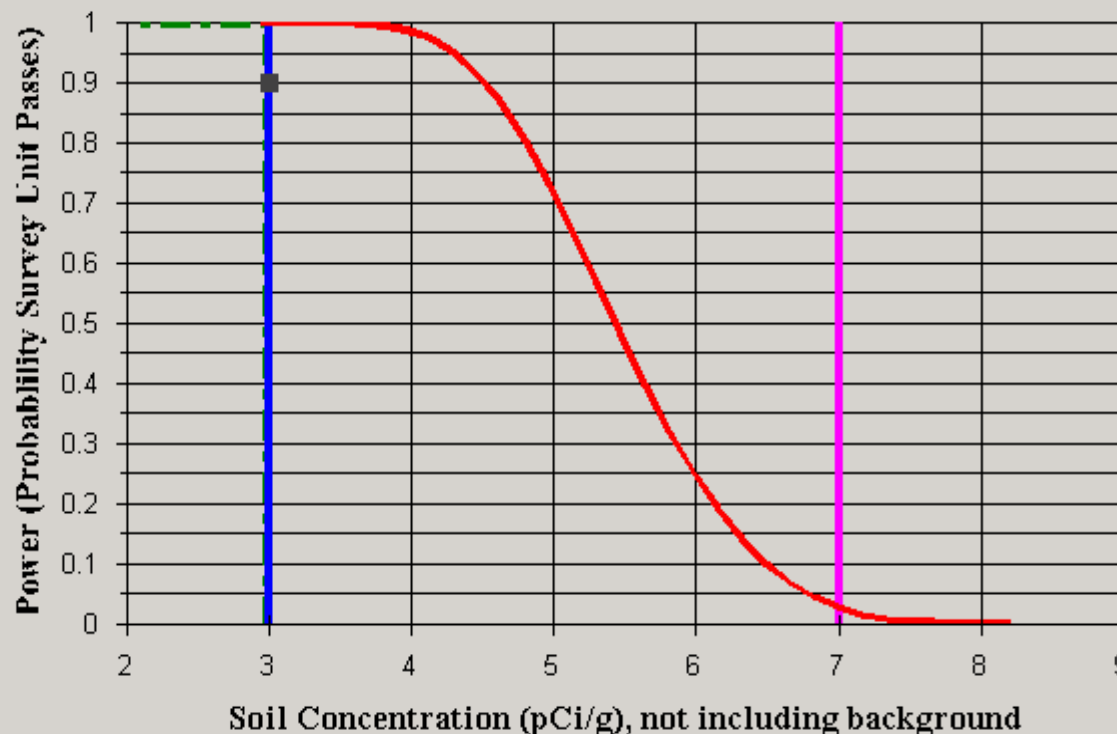
Sigma:

Δ / σ :

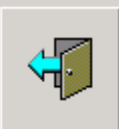
Pr:

N/2:

Calculate Sample Size/Update Prospective Power Curve



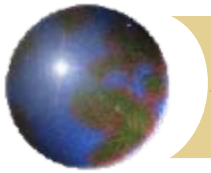
- Prospective Power
- DCGL
- - - Estimated Power
- LBGR
- 1-beta



Enable Training Card Help

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Double Sampling Example

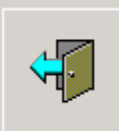
- Survey design was implemented and 11 samples collected in SU and bkg, but actual standard deviation turns out to be 3.06 pCi/g (1.7 pCi/g was planned)
- The retrospective power curve illustrates the impact of this significant underestimate of standard deviation

Basic Statistical Quantities Summary

Summarizes the basic statistical quantities such as the mean, median, minimum value, maximum value, and standard deviation for the systematic sample, reference area samples if applicable and the estimated values provided from the DQO process.

| Statistic | Survey Unit | Background | DQO Results |
|--------------------|-------------|------------|-------------|
| Sample Number | 11 | 11 | N/2=11 |
| Mean (pCi/g) | 5.08 | 0.87 | 3 |
| Median (pCi/g) | 5.20 | 0.90 | N/A |
| Std Dev (pCi/g) | 3.06 | 0.43 | 1.7 |
| High Value (pCi/g) | 9.20 | 1.50 | N/A |
| Low Value (pCi/g) | 1.70 | 0.20 | N/A |

Because the difference between a survey unit measurement and a reference area measurement exceeds the DCGLw AND the difference of the survey unit average and reference area average is less than DCGLw, the WRS Test will be conducted after reviewing the retrospective power curve.



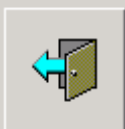
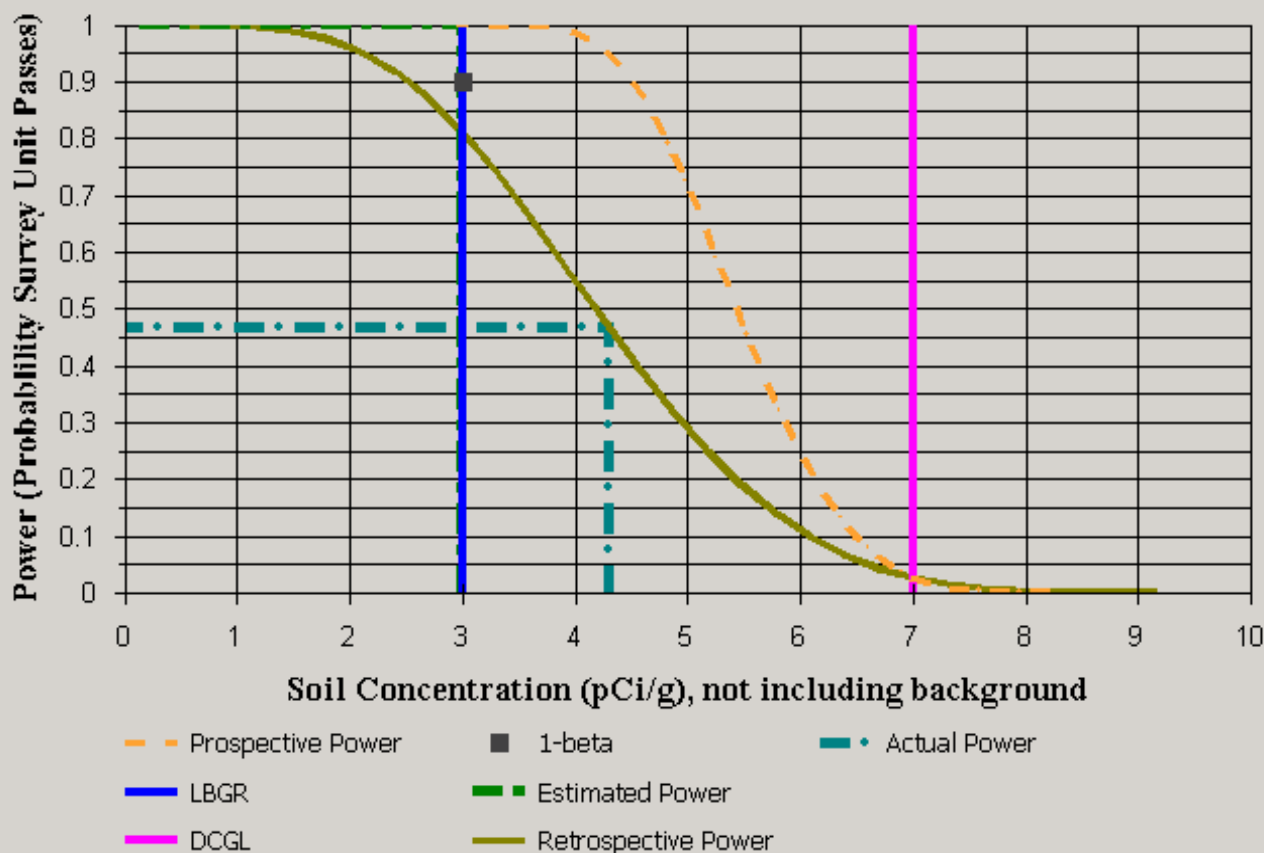
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Retrospective Power Curve Design

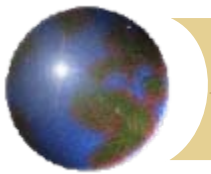
This step compares the retrospective power curve with the prospective power curve for the selected survey unit. The legend below will assist in the interpretation .



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Double Sampling Example

- The retrospective power curve shows that the actual net concentration is 4.2 pCi/g (not 3 pCi/g), but still less than the $DCGL_W$
- The increased std dev (3.06 vs. 1.7) results in the “shallow” retrospective power curve
- The probability of passing at the actual concentration of 4.2 pCi/g is $\sim 47\%$

Statistical Test Summary

Summarizes the results of the WRS Test.

The result of the statistical test is the decision to reject or not to reject the null hypothesis (indicated by Pass or Fail, respectively).

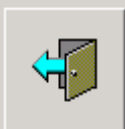
| Data | Type | Adjusted Data | Rank | Ref Rank |
|------|------|---------------|------|----------|
| 0.2 | R | 7.2 | 9.5 | 9.5 |
| 0.2 | R | 7.2 | 9.5 | 9.5 |
| 0.6 | R | 7.6 | 11 | 11 |
| 0.8 | R | 7.8 | 12.5 | 12.5 |
| 0.8 | R | 7.8 | 12.5 | 12.5 |
| 0.9 | R | 7.9 | 14.5 | 14.5 |
| 0.9 | R | 7.9 | 14.5 | 14.5 |

Sum of Ranks:

Sum of Ref Ranks:

Critical Value:

Result:



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Double Sampling Example

- $W_r = 154$; $CV = 156$ —SU just fails (remember SU passes if $W_r > CV$)
- Now calculate WRS sample size based on actual std dev and desired power ($> 70\%$) at actual concentration in SU (use COMPASS Practice)
- $N/2 = 17$ for revised DQOs and actual data
- Already have 11 samples, so need to collect 6 additional random samples in both the SU and reference area
- Regulator has approved Type I errors up to 0.05

Statistical Tests and Prospective Power Practice

Enter the values required below. After these values are entered, you can view the prospective power curve on the right. Click the help button for detailed descriptions of each field.

Enter Values

Test:

DCGL:

LBGR:

Sigma:

Alpha:

Beta:

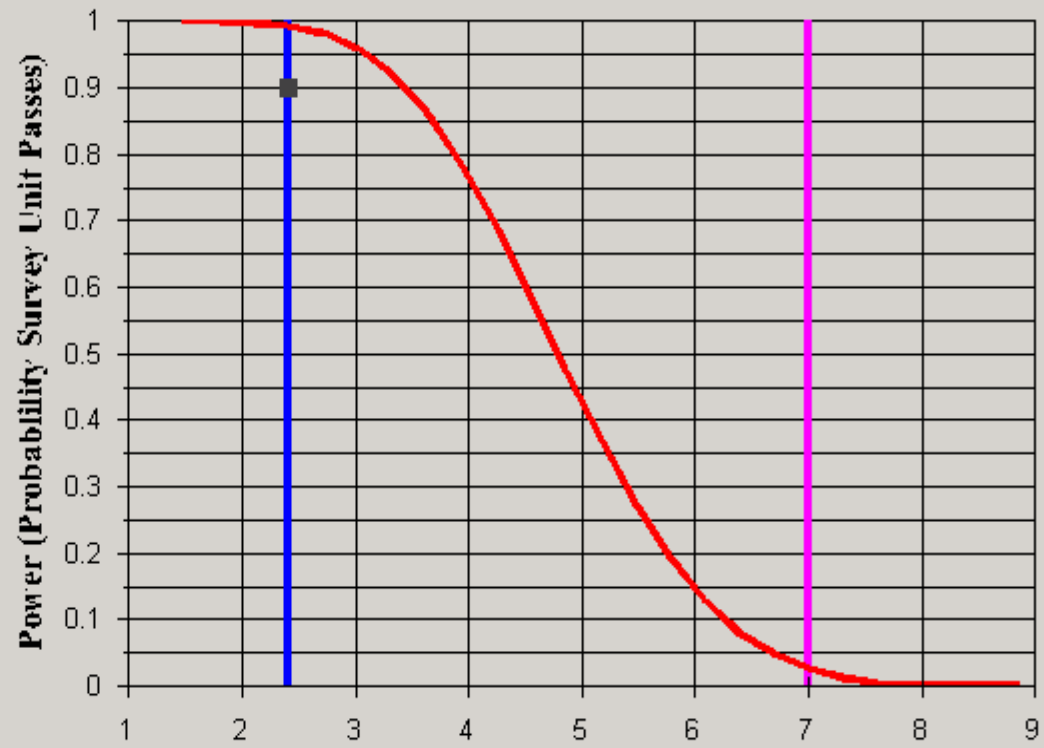
Units:

Calculations

Δ / σ :

Pr:

N/2:



Calculate Sample Size/Update Prospective Power Curve



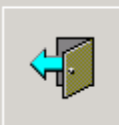
- Prospective Power
- DCGL
- LBGR
- 1-beta

Basic Statistical Quantities Summary

Summarizes the basic statistical quantities such as the mean, median, minimum value, maximum value, and standard deviation for the systematic sample, reference area samples if applicable and the estimated values provided from the DQO process.

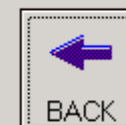
| Statistic | Survey Unit | Background | DQO Results |
|--------------------|-------------|------------|-------------|
| Sample Number | 17 | 17 | N/2=11 |
| Mean (pCi/g) | 5.15 | 0.86 | 3 |
| Median (pCi/g) | 5.20 | 0.90 | N/A |
| Std Dev (pCi/g) | 2.54 | 0.39 | 1.7 |
| High Value (pCi/g) | 9.20 | 1.50 | N/A |
| Low Value (pCi/g) | 1.70 | 0.20 | N/A |

Because the difference between a survey unit measurement and a reference area measurement exceeds the DCGLw AND the difference of the survey unit average and reference area average is less than DCGLw, the WRS Test will be conducted after reviewing the retrospective power curve.



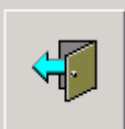
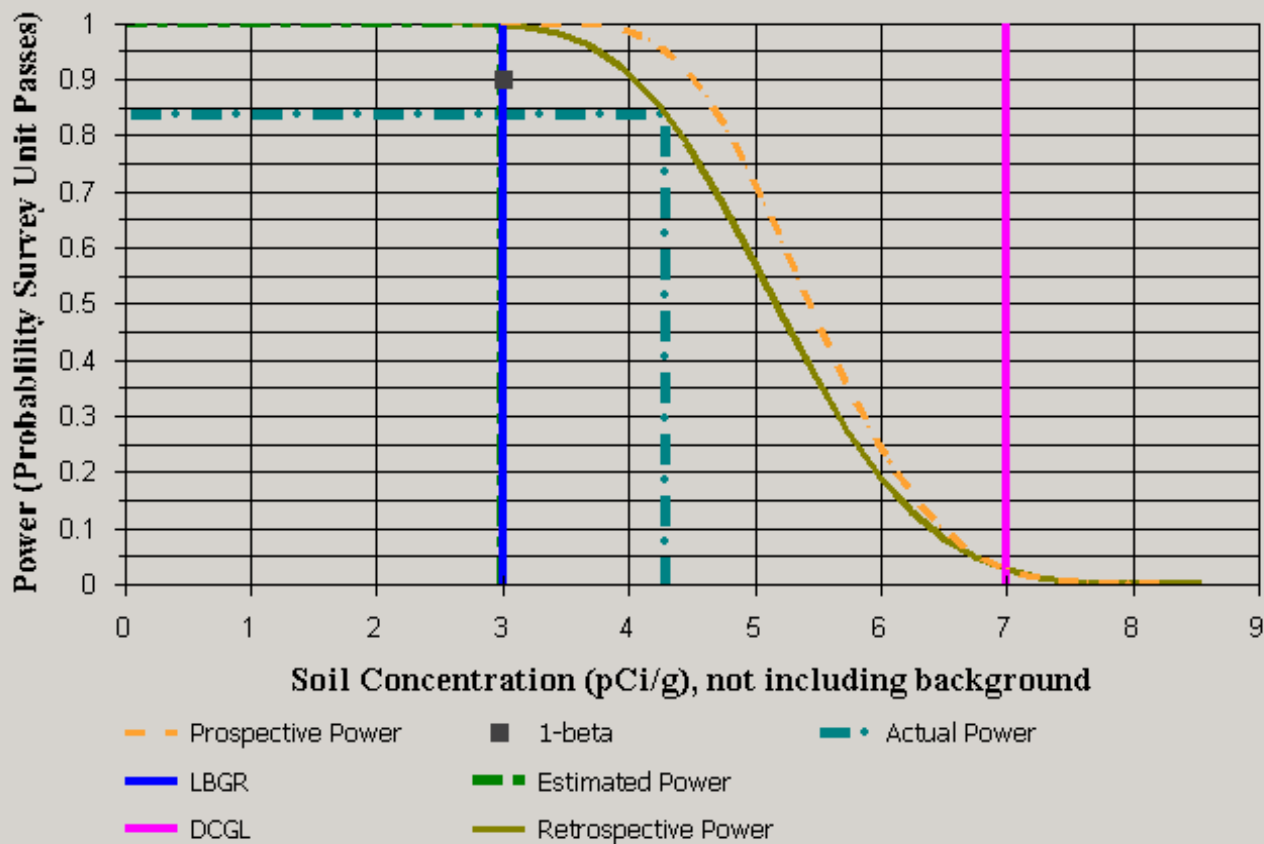
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Retrospective Power Curve Design

This step compares the retrospective power curve with the prospective power curve for the selected survey unit. The legend below will assist in the interpretation .



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Statistical Test Summary

Summarizes the results of the WRS Test.

The result of the statistical test is the decision to reject or not to reject the null hypothesis (indicated by Pass or Fail, respectively).

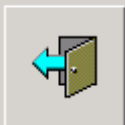
| Data | Type | Adjusted Data | Rank | Ref Rank |
|------|------|---------------|------|----------|
| 0.2 | R | 7.2 | 15.5 | 15.5 |
| 0.2 | R | 7.2 | 15.5 | 15.5 |
| 0.4 | R | 7.4 | 17 | 17 |
| 0.6 | R | 7.6 | 18 | 18 |
| 0.7 | R | 7.7 | 19.5 | 19.5 |
| 0.7 | R | 7.7 | 19.5 | 19.5 |
| 0.8 | R | 7.8 | 21.5 | 21.5 |

Sum of Ranks:

Sum of Ref Ranks:

Critical Value:

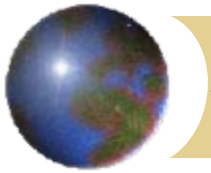
Result:



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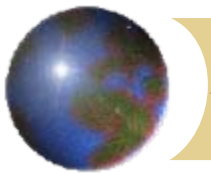
v1.0.0





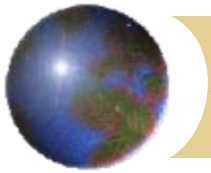
Conclusions from Double Sampling Example

- The survey unit passed the second time around—after 6 more samples were randomly collected and added to data set
- Retrospective power curve is a diagnostic tool to assess survey unit failures
- The overall Type I error (after double sampling) is greater than 0.025, but less than 0.05



Final Thoughts on Advanced MARSSIM Topics

- MARSSIM lessons learned are being made available—ORS journal (June 2003); DDSC web site (<http://www.ornl.gov/ddsc/>); NUREG-1757; COMPASS; NRC's improved D&D web site
- Additional work needed with scan MDCs, subsurface contamination, dose modeling and area factors—share/publish your MARSSIM experiences



References

- Operational Radiation Safety, June 2003
- "Decommissioning Health Physics: A Handbook for MARSSIM Users." Institute of Physics, Bristol, UK; July 2001
- HP Newsletter "Double Sampling - A Statistical Approach for MARSSIM Users" July 2003