



# Aerodynamic and Aeroacoustic Properties of Flatback Airfoils

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Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company, for the United States Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.



# Outline

- **Project Goal & Objectives**
- **Blade Program Background**
  - BSDS
  - Flatbacks
- **Wind Tunnel**
- **Models**
- **Test Matrix & Objectives**
- **Preliminary Results**
- **Future Work**
- **Summary**

# Project Goal & Objectives

- **Goal:** Quantify the aerodynamic performance and aeroacoustic emission of a flatback airfoil relative to a conventional sharp trailing edge airfoil
- **Objectives:**
  - Directly measure performance of a flatback airfoil
    - aerodynamic
    - aeroacoustic
  - Directly compare to performance of a conventional airfoil
  - Evaluate effect of simple trailing edge treatment
- **Challenges:**
  - Large separation on blunt trailing edge
  - Highly turbulent/highly 3-D flow

# Blade Research at Sandia National Labs

- **SNL initiated a blade research program in 2002 to investigate the use of carbon fiber and other advanced structural concepts in wind turbine blades**
- **Objective: build stronger, lighter blades**
- **Three 9 m blade designs have been produced**
  - **CX-100 (Carbon eXperimental 100 kW)**
  - **TX-100 (Twist-Bend coupled eXperimental 100 kW)**
  - **BSDS (Blade System Design Study)**
- **Laboratory and field tests have been conducted to evaluate the designs and to validate modeling tools**

# Applications of Blade Innovations

- **Prototype Sub-scale (9 meters) Blades Manufactured**

- **CX-100**

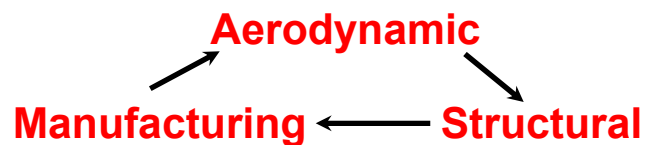
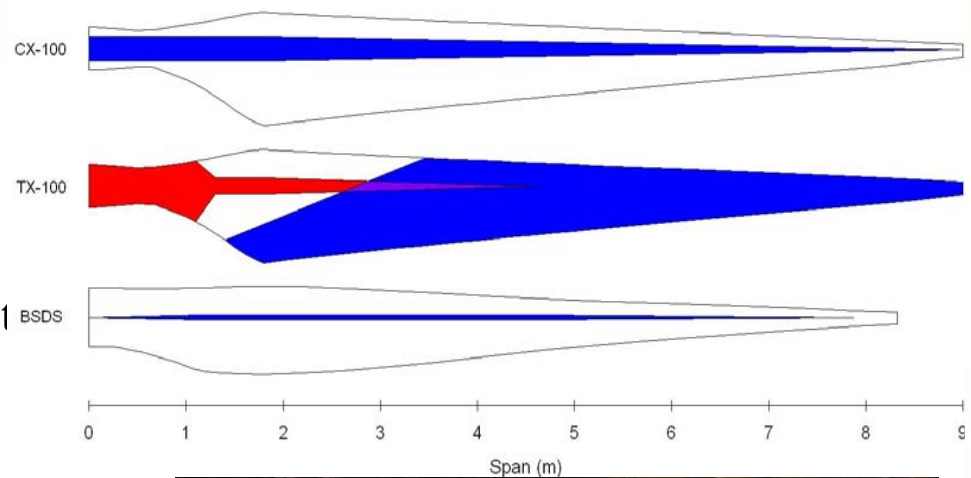
- Carbon spar cap
- Glass skin and shear web

- **TX-100**

- Carbon triax in skin for bend-twist
- Constant thickness glass spar cap

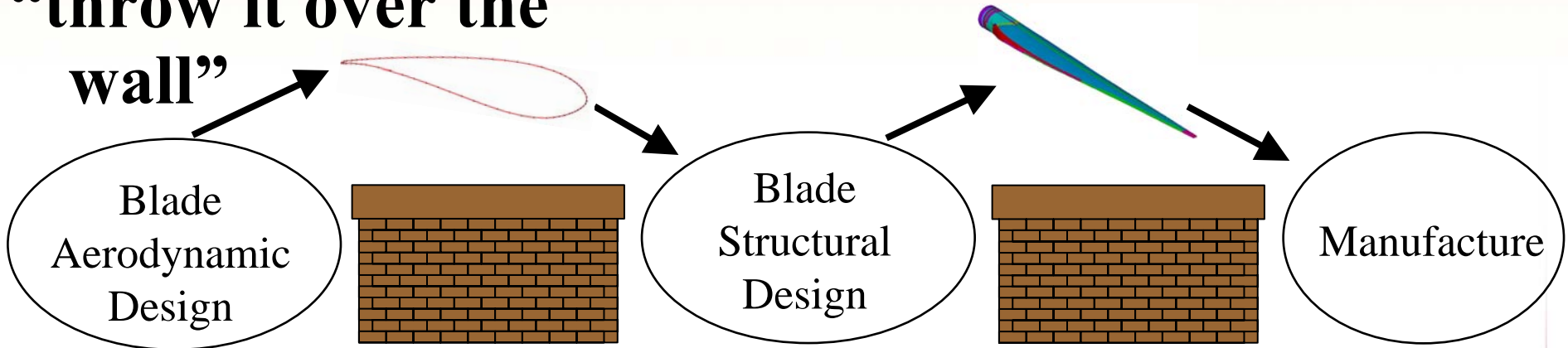
- **BSDS**

- Flatback airfoils
- Constant thickness carbon spar cap
- High performance airfoils
- Large scale architecture
- Highly efficient structural design
- Result of system design approach

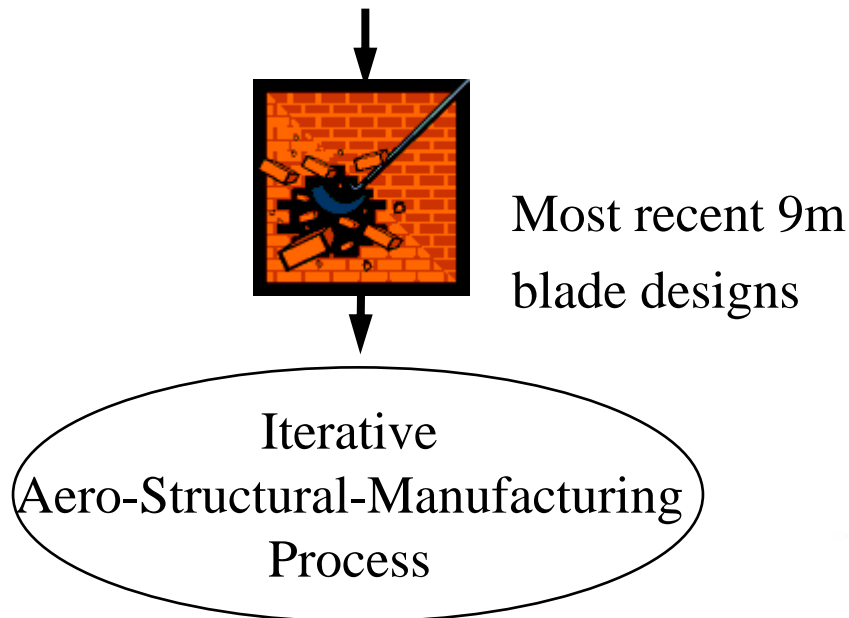


# New Design Approach

**Traditional:**  
“throw it over the wall”



**Integrated:**



# Blade Structural Comparison

| Property                                     | ERS-100 | CX-100 | TX-100 | BSDS  |
|--|---------|--------|--------|-------|
| Weight (lb)                                  | 426     | 383    | 361    | 289   |
| % of Design Load at Failure                  | 110%    | 105%   | 197%   | 310%  |
| Root Failure Moment (kN-m)                   | 122.8   | 117.0  | 121.4  | 203.9 |
| Max. Carbon Tensile Strain at Failure(%)     | NA      | 0.31%  | 0.59%  | 0.73% |
| Max. Carbon Compressive Strain at Failure(%) | NA      | 0.30%  | 0.73%  | 0.87% |
| Maximum Tip Displacement (m)                 | 1.43    | 1.05   | 1.80   | 2.79  |

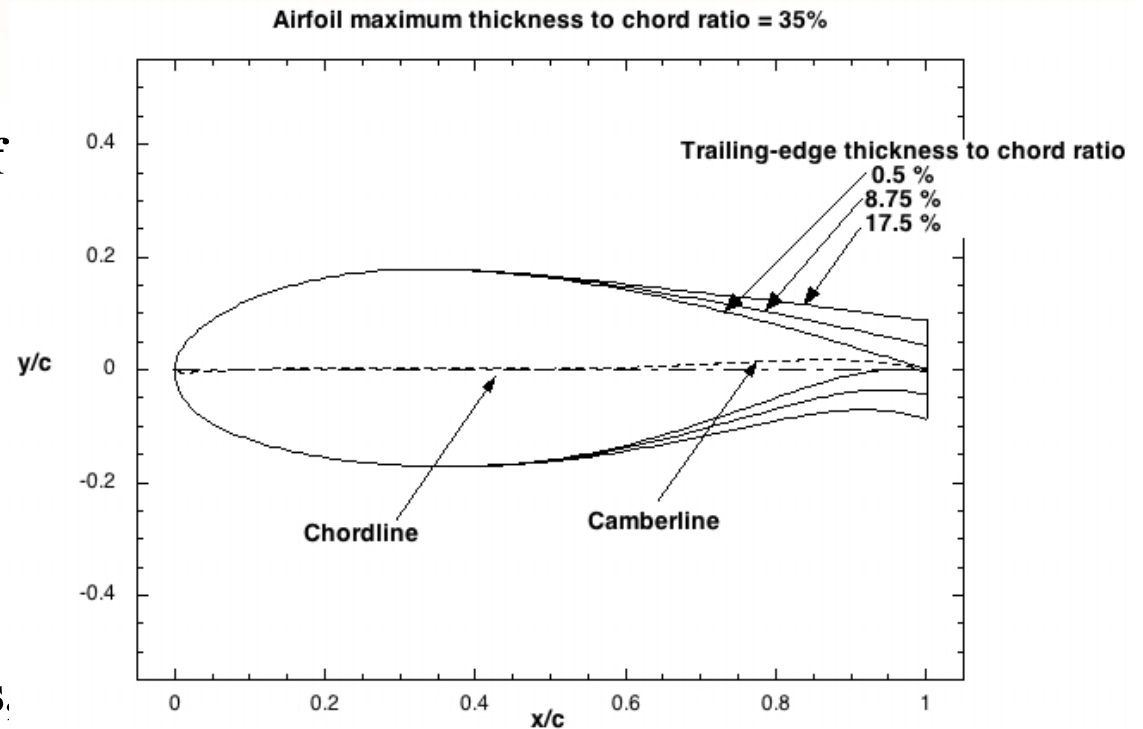
**Integrated aero/structural design process resulted in lighter, less expensive, stronger blade**



# Flatback Airfoils

## Creation of Flatback Airfoils

- Flatback airfoils are created by the symmetric addition of thickness about the camber line
- Different from truncated airfoils which “chop” off the trailing edge and thus lose camber
- This is one solution for increasing thickness. Others, such as thick airfoil families, exist.



\*Study of flatback airfoils performed in collaboration with UC Davis



# Flatback Airfoils

- **Advantages**

- **Structural:**

- Increased sectional area
- Increased sectional moment of inertia
- Shorter chord length

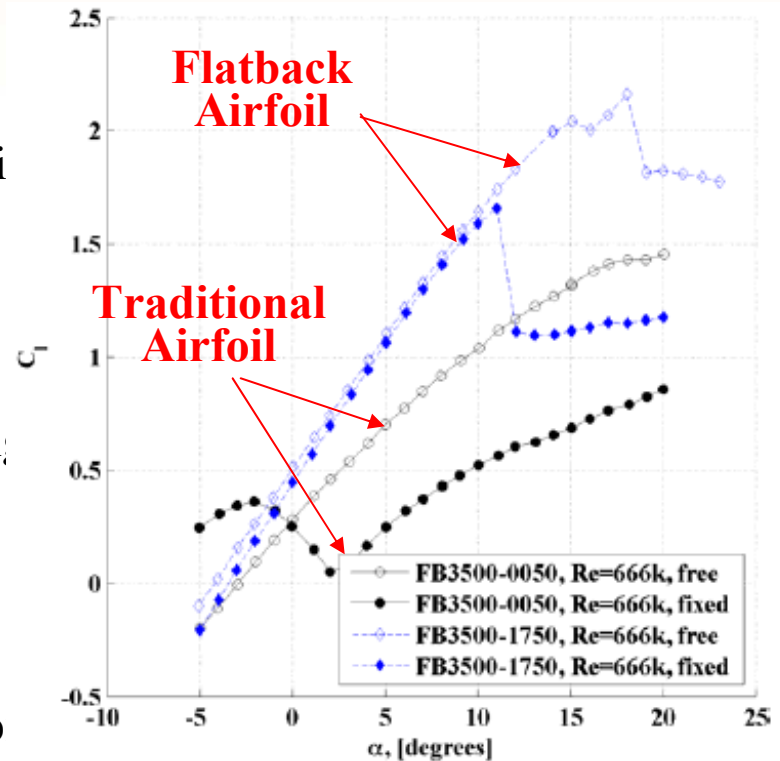
- **Aerodynamic:**

- Increased maximum lift coefficient
- Reduced sensitivity to surface soiling

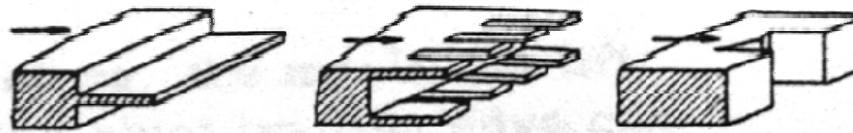
- **Disadvantages**

- Increased drag
- Unknown and complex 3D base flow
- Greater aeroacoustic (noise) generation

## Experimental Data



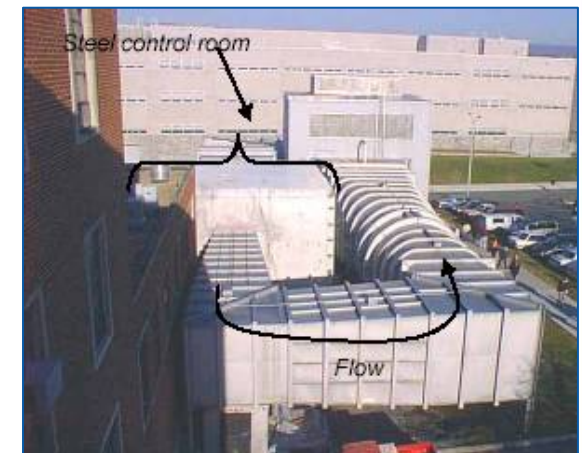
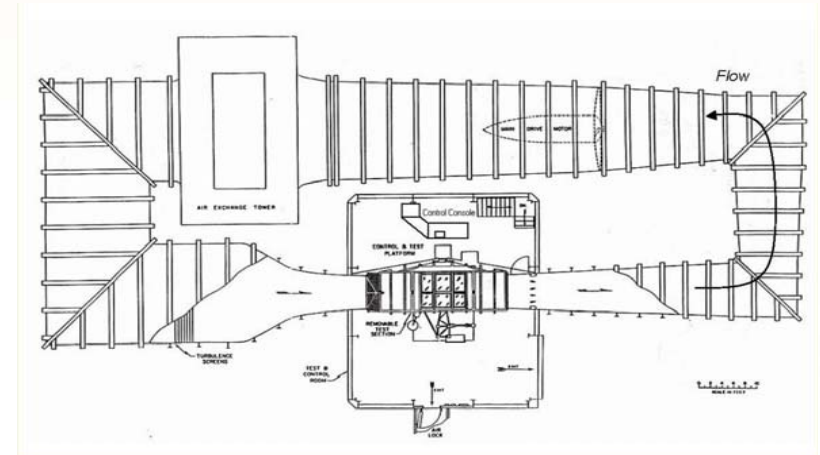
## Possible Trailing Edge Treatments to Reduce Drag



Source: Tanner (1973)

# Virginia Tech Stability Wind Tunnel

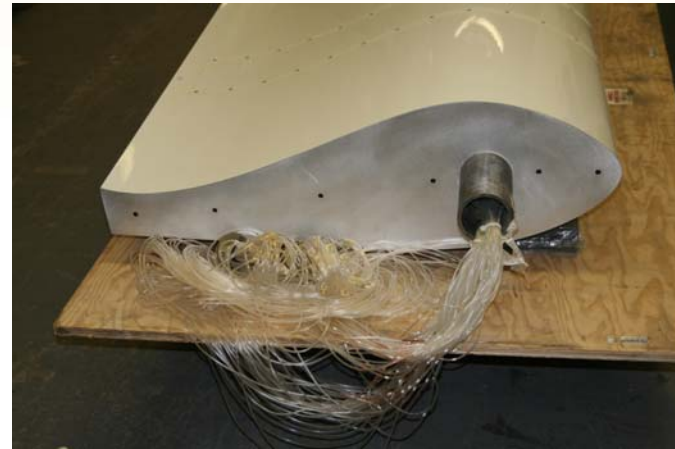
- **Continuous flow**
- **6 ft X 6 ft test section**
- **170 mph maximum velocity**
- **Modified for aeroacoustic testing**
- **Kevlar windows in test section**
  - **Confine flow/transmit sound**
- **Extensive efforts to quiet tunnel**



# Wind Tunnel Models

- **36-in chord**
- **Steel frame, fiberglass surface**
- **80 pressure taps per airfoil**
  - Pressure and suction surfaces
- **3 Model configurations**
  - 1.7% thick Trailing Edge (“sharp”)
  - 10% thick Trailing Edge (“flatback”)
  - Flatback with Splitter Plate
- **Accuracy of profiles not yet established**

**Flatback Model**



**Flatback model with Splitter Plate**



# Data Acquisition

- **Model mounted vertically in test section**
- **Instrumentation**
  - Surface pressures measured with scanivalve.
  - Wake pressures measured with traverse system.
  - Boundary layer velocity profiles measured with hot wire traverse system.
  - Boundary layer turbulence characteristics (spectra) measured with hot wire.
- **Noise data obtained with 63 microphone phased array**

Kevlar Wall



**Model in Wind Tunnel**



**Phased Array**

# Measurement Conditions

- Define aerodynamic performance
  - $C_d$  min
  - $C_l/C_d$  max
  - $C_l$  max
- Measure noise generation
- Clean surface
- Tripped boundary layer
  - 0.5 mm thick zig-zag tape
- Three Reynolds numbers (scaling of noise with velocity)

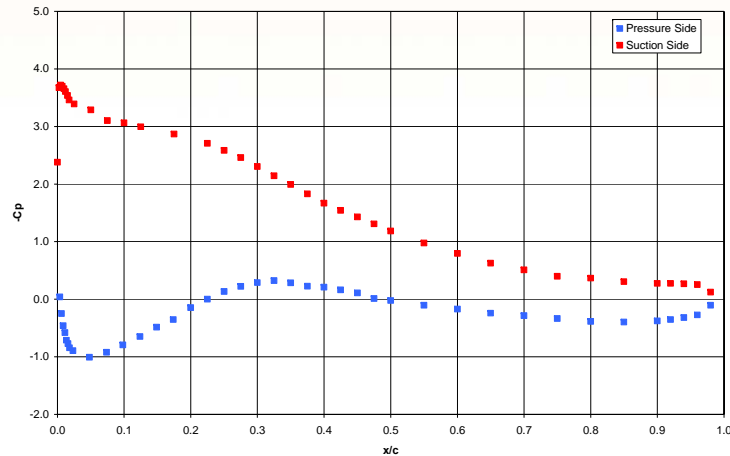
| <i>Measurements Obtained in Sandia Test</i> |                     |                       |                          |                             |                |                                    |                     |
|---|---------------------|-----------------------|--------------------------|-----------------------------|----------------|------------------------------------|---------------------|
| DU97-W-300 Airfoil                          |                     |                       |                          |                             |                |                                    |                     |
| Configuration                               |                     |                       | Measurements             |                             |                |                                    |                     |
| Effective Angle of Attack                   | Boundary Layer Trip | Chord Reynolds Number | Phased Array Microphones | Model Pressure Distribution | Wake Pressures | TE Hot-wire Boundary Layer Profile | TE Hot-wire Spectra |
| 4   | None                | $1.6 \times 10^6$     |                          |                             |                |                                    |                     |
| 4   | None                | $2.4 \times 10^6$     | X                        | X                           |                |                                    |                     |
| 4   | None                | $3.2 \times 10^6$     | X                        | X                           | X              | X                                  | X                   |
| 8   | None                | $1.6 \times 10^6$     | X                        | X                           | X              | X                                  | X                   |
| 8   | None                | $2.4 \times 10^6$     | X                        | X                           |                |                                    |                     |
| 8   | None                | $3.2 \times 10^6$     | X                        | X                           | X              | X                                  | X                   |
| 12  | None                | $1.6 \times 10^6$     |                          |                             |                |                                    |                     |
| 12  | None                | $3.2 \times 10^6$     | X                        | X                           |                | X                                  | X                   |
| 4   | Tripped             | $1.6 \times 10^6$     |                          |                             |                |                                    |                     |
| 4   | Tripped             | $3.2 \times 10^6$     | X                        |                             |                |                                    |                     |
| 8   | Tripped             | $1.6 \times 10^6$     | X                        |                             |                | X                                  | X                   |
| 8   | Tripped             | $2.4 \times 10^6$     | X                        | X                           |                |                                    |                     |
| 8   | Tripped             | $3.2 \times 10^6$     | X                        | X                           |                | X                                  | X                   |

Measurement Matrix for Sharp Airfoil



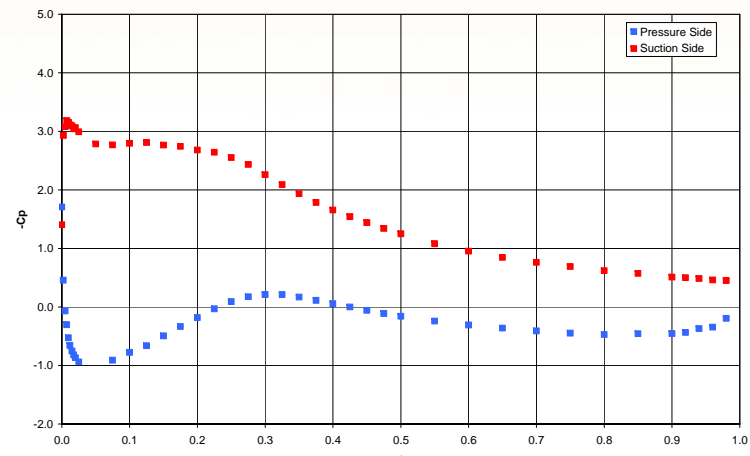
# Preliminary Surface Pressure Results

$\alpha = 12^\circ$ , no boundary layer trip



Sharp Trailing Edge

$\alpha = 10^\circ$ , boundary layer trip



Flatback

- Reynolds number =  $3.2 \times 10^6$
- Pressure recovery for flatback occurs aft of trailing edge

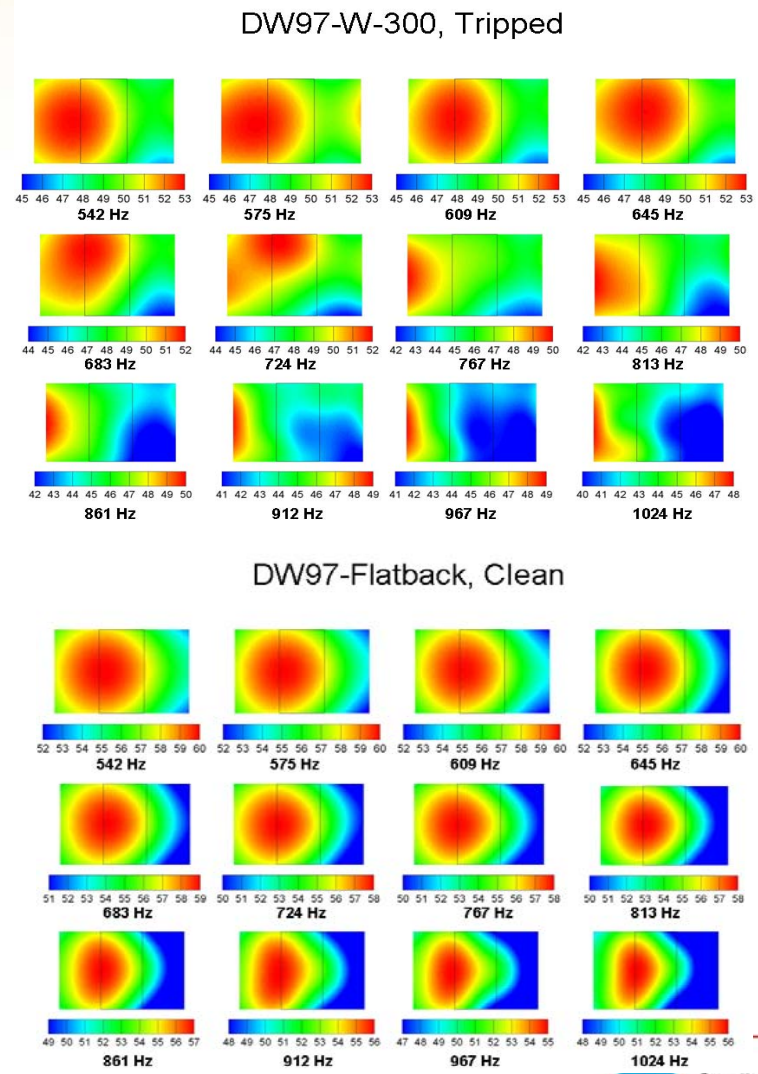
# Beam Forming Data Reduction

- **All microphones sampled simultaneously at 25,600 Hz**
- **Data split into blocks of 8192 samples**
- **FFT performed on each block to determine spectral content**
- **Microphone spacing and delay times required for sound to reach each microphone permits identification of noise sources**



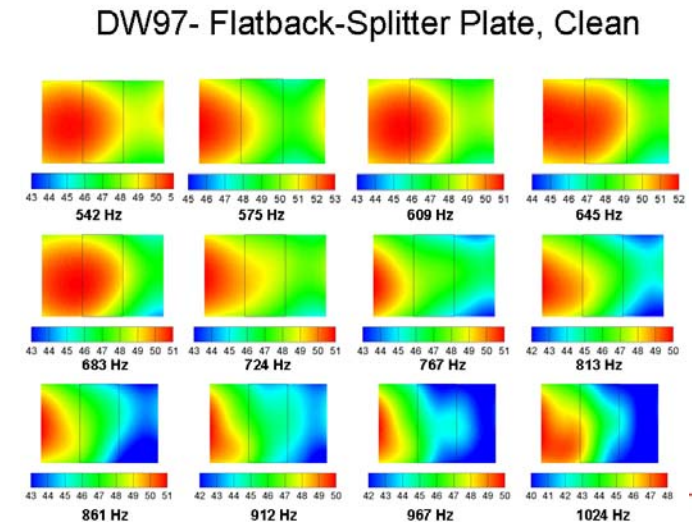
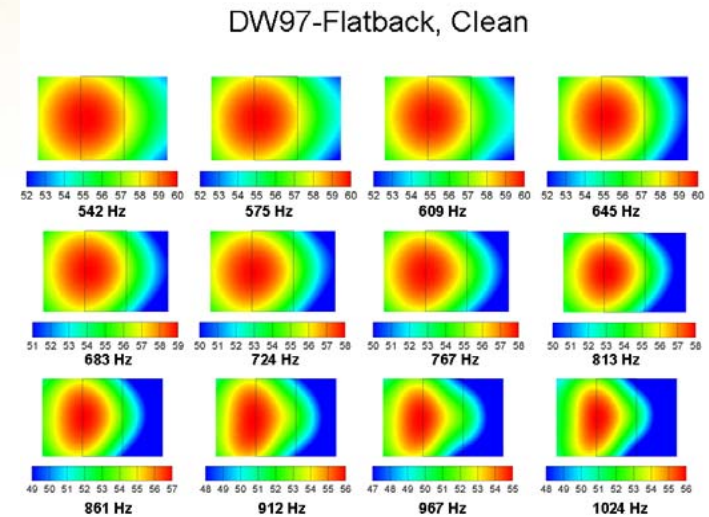
# Preliminary Beam Forming Results

- Flow is from right to left
- LE and TE shown by vertical lines
- Highest noise level always in red
- Note changes in SPL levels for flatback
- Highest noise levels are at trailing edge

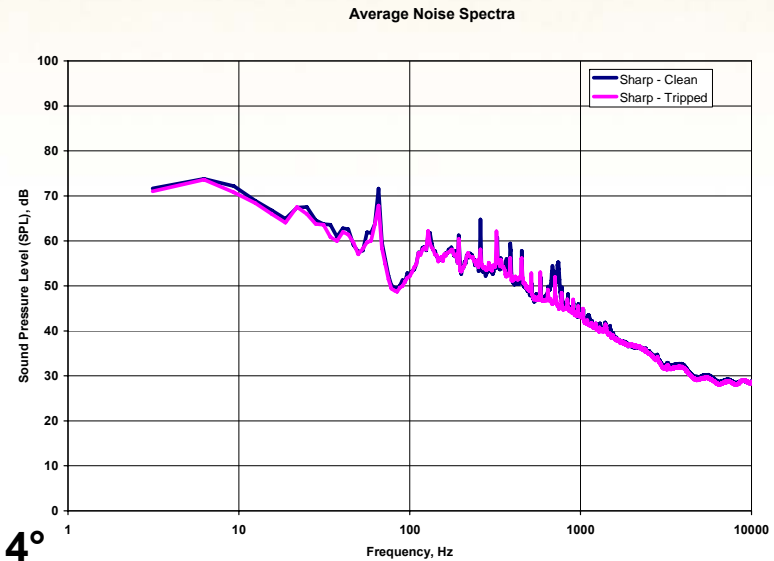
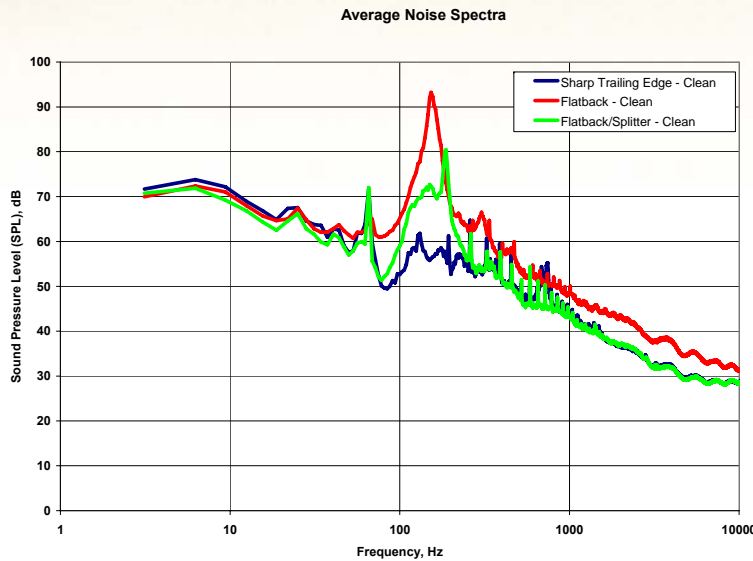


# Preliminary Beam Forming Results

- Flow is from right to left
- LE and TE shown by vertical lines
- Highest noise level always in red
- Note drop in SPL levels for splitter plate
- Highest noise levels are still at trailing edge, but not as intense



# Preliminary Noise Spectra



$\alpha = 4^\circ$

- Integrated spectra (average of 100 calculations) from single microphone
- Background tunnel noise still included
- Extraneous noise spikes still included

| Airfoil              | Sound Level |
|----------------------|-------------|
| DU97-W-300           | <u>74</u>   |
| DU97 Flatback        | <u>90</u>   |
| Flatback w/ Splitter | <u>79</u>   |

# Future Work

- **Complete data validation and reduction**
- **Clean up noise data**
- **Compare experimental aerodynamic performance with CFD models and reconcile differences**
- **Use hot wire velocity and spectral data as initial conditions for computational aeroacoustic analysis**
- **Extend trailing edge bluntness noise generation correlation of Brooks, et al from 1% thick to 10% thick trailing edge**
- **Compare noise generated by blade with flatback sections to that generated by blade with only conventional sections**
- **Test other trailing edge treatments with noise reduction focus**

# Summary

- **SNL Blade Research effort resulted in design innovations**
  - Flatback airfoil
  - Structurally efficient
  - Reduced weight
- **Flatback airfoils raise concerns**
  - Aerodynamic performance
  - Noise generation
- **Direct measurement shows**
  - Flatback noise is much higher than sharp TE noise (90 dB vs 74 dB)
  - Splitter plate drops noise significantly (down to 79 dB)
- **Only preliminary data is available at this time.**
- **Much additional data reduction & validation work remains.**



# Thank you

## Questions??

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