

Thermodynamic Data for Biomass Conversion and Waste Incineration



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**THERMODYNAMIC DATA FOR BIOMASS
CONVERSION AND WASTE INCINERATION**

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Preface

Incinerators have continued to play an important part in reducing the amount and modifying the type of waste discharged to the environment.

The ASME Research Committee on Industrial and Municipal Wastes was established in 1968. This committee recognized the need for greater understanding of combustion fundamentals if engineers are to design better incinerators to meet the challenge of improving the environment. It, therefore, created a subcommittee on fundamental combustion studies.

The first report of the subcommittee, *Combustion Fundamentals for Waste Incineration*, was published in 1974 [74ASM]. The purpose of the report was to help engineers make better calculations and thereby design better incinerators. The report was divided into two parts. Part one covered theoretical engineering methods of calculation and tables of equilibrium products of combustion with practical examples. Part two included the scientific theory and tables of thermodynamic properties.

In a second report of the subcommittee, *Thermodynamic Data for Waste Incineration* [78DOM/EVA], engineers were provided with thermodynamic data on materials that are mixtures of various kinds and are often difficult to describe using a single stoichiometric formula. These materials (i.e., animals, foods, plants, polymers, wood species, etc.) are encountered perhaps more often by engineers engaged in the disposal of municipal wastes than pure substances. The bulk of the data, consisting of gross heats of combustion (heating values) and specific heats, was intended to be helpful in combustion calculations.

In the eight years since the issuance of the second report, biomass and biomass wastes have joined industrial and municipal solid wastes as major sources of solid fuel. In addition, widespread applications of gasification and pyrolysis are expected to join combustion as practical conversion processes in the 1990s.

This report, under the sponsorship of the DOE Office of Renewable Technology, Biofuels and Municipal Waste Technology Division, doubles the number of materials listed, with major emphasis on different forms of biomass, both woody and agricultural. It incorporates almost all of the materials listed in *Thermodynamic Data for Waste Incineration* and now provides information for more than 600 materials.

Contents

	<u>Page</u>
Introduction	1
Units and Definitions	2
Thermodynamic Properties of Waste and Biomass Materials	9
Agricultural Residues	9
Alloys and Metals	33
Animals	55
Biomass-Derived Materials	67
Foods	77
Fossil Materials	103
Inorganic Materials	127
Paper	137
Plant Materials (Non-Woody)	143
Polymers and Plastics	167
Polypeptides and Proteins	191
Refuse	201
Rubber Materials	207
Vegetable Oils	213
Woody and Tree Materials	233
Miscellaneous	305
References	313
Appendix A. A Formula for the Empirical Estimation of the Heats of Combustion of Carbonaceous Materials	323
Appendix B. Additional Information on Heats of Combustion of Biomass Materials	326
Appendix C. Symbols, Units, Conversion Factors, Atomic Weights	331
Name Index	341

Introduction

The general purpose of this collection of thermodynamic data of selected materials is to make property information available to the engineering community on chemical mixtures, polymers, composite materials, solid wastes, biomass, and materials not easily identifiable by a single stoichiometric formula. Workers in many sectors need this type of information: construction engineers who require thermodynamic information on materials, safety engineers assessing the hazard potential of chemicals, chemical engineers concerned with industrial unit processes, and scientists who want thermodynamic data for specific research projects.

The specific purpose of this publication is to provide engineers involved in combustion and thermochemical conversion with appropriate thermodynamic data so that they can dispose of waste materials and utilize biomass for energy in a more effective and environmentally acceptable manner. The effective disposal of waste materials is an important part of the maintenance of a high-quality environment, and combustion/thermochemical conversion offers the most significant means of volume reduction for waste materials when compared to other methods of disposal. In addition, the potential of biomass for energy is being increasingly recognized and realized.

This compilation of thermodynamic data was prepared for the Solar Energy Research Institute (SERI) by the Chemical Thermodynamics Data Center of the National Bureau of Standards. More than 700 materials have been compiled covering properties such as specific heat, gross heat of combustion, heat of fusion, heat of vaporization, and vapor pressure. The information was obtained from the master files of the NBS Chemical Thermodynamics Data Center, the annual issues of the *Bulletin of Chemical Thermodynamics*, intermittent examinations of the *Chemical Abstracts* subject indexes, individual articles by various authors, and other general reference sources.

The compilation is organized into several broad categories; materials are listed alphabetically within each category. For each material the following are given: (1) the physical state, (2) information as to the composition or character of the material, (3) the kind of thermodynamic property reported, (4) the specific property values for the material, and (5) citations to the reference list. A name index is provided to assist a user in finding a specific material.

Several appendices are also included. Appendix A gives an empirical formula that allows heats of combustion of carbonaceous materials to be predicted with surprising accuracy when the elemental composition is known. A spread sheet illustrates this predictability with examples from this report and elsewhere. Appendix B lists some reports containing heats of combustion not included in this publication. Appendix C contains symbols, units, conversion factors, and atomic weights used in evaluating and compiling the thermodynamic data.

Units and Definitions

The notation in the tables for thermodynamic quantities follows, in general, that in *Combustion Fundamentals for Waste Incineration* [74ASM]. In those tables values were reported on a molar basis. Here, because of the lack of definite stoichiometric compositions for most of the materials included, values of the thermodynamic quantities are given on a specific basis, for one gram or one pound (unit mass) of substance. Exceptions are noted. The symbols used are briefly defined below; more extensive discussions are given in [74ASM].

Air-Drying. A process of partial drying of a sample to bring its moisture content near to equilibrium with the atmosphere in which further reduction, division, and characterization of the sample are to take place.

Air-Dry Loss. The decrease in sample mass due to air-drying. This decrease is presumed to be moisture.

Ash. The residue remaining after ignition of a sample determined by a definite prescribed procedure.

As-Received Basis. The test data calculated to the moisture condition of the sample as it arrived in the laboratory and before any laboratory processing or conditioning.

Dry Basis. The test data calculated to theoretical base of no moisture associated with the sample.

Dry, Ash-Free Basis. The test data calculated to a theoretical base of no moisture or ash associated with the sample.

Enthalpy. The enthalpy, H , is defined by the equation: $H = U + PV$, where U is the internal energy of the system, P is the pressure, and V is the volume.

Enthalpy Difference. See Heat Content.

Gross Calorific Value. See Gross Heat of Combustion.

Gross Heat of Combustion. The heat produced by combustion of one unit of substance at constant volume in an oxygen bomb calorimeter under specified conditions. The conditions are: initial oxygen pressure of 2.0-4.0 MPa (20-40 atm), final temperature of 20°-35°C (68°-95°F), products in the form of ash, liquid water, gaseous CO₂ and N₂, and dilute aqueous HCl and H₂SO₄. It is assumed that if significant quantities of metallic elements are combusted, they are converted to their oxides. In the case of materials such as coal, wood, or refuse, if small or trace amounts of metallic elements are present, they are unchanged during combustion and are part of the ash.

In accurate studies, the observed heat is corrected for side reactions and to a standard state in which all gases are at unit fugacity. For most of the data reported here, the precision of the measurements does not warrant such refinement.

Gross Heat of Reaction. The specific isothermal gross heat of reaction at the specified temperature and at constant volume, $q_v(\text{gross})$, is equal to $-\Delta U/M$, where ΔU is the molar change in internal energy of the process, and M is the molecular weight. Usually, the values of q_v (or ΔU) have not been converted to the standard state ($-\Delta U^\circ/M$) [74ASM]. Some of the data are of such low precision, because of sample variability or measurement method, that this correction is impractical.

The numerical values for $q_v(\text{gross})$ are given in J g^{-1} , cal g^{-1} , and Btu lb^{-1} . The joule (J) is the primary SI energy unit. The calorie used is the thermochemical calorie, defined as 4.184 J. The British thermal unit used is the thermochemical Btu. Conversion factors are given in Appendix C.

Heat Content. The difference in enthalpy, for one unit mass of substance, between two temperatures, $(H_T - H_{T(\text{ref})})/M = (q_T - q_{T(\text{ref})})$. $T(\text{ref})$ is the reference temperature, usually 0 K, 273.15 K, or 298.15 K. It is specified as q_0 , q_{273} or $q_{273.15}$, and $q_{298.15}$. If other than the kelvin scale is used, this is indicated as $^\circ\text{C}$, $^\circ\text{F}$, or $^\circ\text{R}$ (Rankine, $T^\circ\text{R} = 1.8 T \text{ K}$).

Heat of Fusion, L_f . The specific latent heat of fusion ($\Delta H_{\text{fus}}/M$) at a pressure of 101325 Pa (1 atm). The value is the heat absorbed (in J, cal, or Btu) when one unit mass of the substance goes from the solid state to the liquid state. For a pure compound, the melting occurs at a single temperature; for the complex materials considered here, the melting process may take place over a temperature range.

Heat of Sublimation, L_s . The specific latent heat of sublimation ($\Delta H_{\text{sub}}/M$). The value is the heat absorbed when one unit mass of the substance goes from the solid state to the gaseous state. The same considerations apply as for L_v .

Heat of Transition, L_t . The specific latent heat of transition ($\Delta H_{\text{trs}}/M$) at a pressure of 101325 Pa (1 atm). The value is the heat absorbed when one unit mass of the substance goes from one solid phase to another solid phase. For a pure compound, the transition occurs at a single temperature; for the complex materials considered here, the transition process may take place over a temperature range.

Heat of Vaporization, L_v . The specific latent heat of vaporization ($\Delta H_{\text{vap}}/M$). The value is the heat absorbed when one unit mass of the substance goes from the liquid state to the gaseous state. If measured calorimetrically, the value will be for a definite temperature and pressure. If derived from the vapor pressure equation through the relation $d(\ln P)/d(1/T) = -\Delta H_{\text{vap}}/R$, the value may be referred to a definite temperature and pressure, depending upon the form of the equation. With the simple form $\ln P = A - B/T$, the value refers to the midpoint of the temperature range over which the equation is

valid. The value thus obtained is for one mole of gaseous species; the average molecular weight must be obtained to calculate the specific heat of vaporization: $L_v = \Delta H_{\text{vap}}/M$.

Internal Energy. When heat, q , is added or removed, and work, w , is done on or by the system, its internal energy, U , is modified according to the equation: $U = q + w$.

Net Calorific Value. See Net Heat of Combustion.

Net Heat of Combustion. The heat produced by combustion of one unit of substance at atmospheric pressure under conditions such that all water in the products remains in the form of vapor. The net heat of combustion is calculated from the gross heat of combustion at 20°C (68°F) by subtracting 572 cal g⁻¹ (1030 Btu lb⁻¹) of water derived from one unit mass of sample, including both the water originally present as moisture and that formed by combustion. This subtracted amount is not equal to the latent heat of vaporization of water (586 cal g⁻¹ at 20°C) because the calculation also reduces the data from the gross value at constant volume to the net value at constant pressure. The appropriate factor for this reduction is 572 cal g⁻¹.

Net Heat of Reaction. The specific isothermal net heat of reaction at the specified temperature and at constant volume. $q_v(\text{net})$ is equal to $-\Delta U/M$, where ΔU is the molar internal energy of the process, and M is the molecular weight. This value differs from $q_v(\text{gross})$ in that water formed is in the gaseous state. The specific isothermal net heat of reaction at the specified temperature and at constant pressure, $q_p(\text{net})$, is equal to $-\Delta H/M$, where ΔH is the molar change in enthalpy of the process, and M is the molecular weight. Where possible, the values of $q_p(\text{net})$ have been converted to the standard state, $(-\Delta H^\circ/M)$ [74ASM]. Most of the data, though, are of such low precision, because of sample variability or measurement method, that the correction is impractical.

Proximate Analysis. The determination by prescribed methods of moisture, volatile matter, fixed carbon (by difference), and ash. Unless otherwise specified, the term proximate analysis does not include determinations of chemical elements or any determinations other than those named.

Residual Moisture. The moisture content remaining in a sample after it has been air-dried and milled down, if necessary, to an analysis sample.

Specific Heat, C_p . The change in enthalpy with temperature at constant pressure (1 atm unless otherwise specified) for one unit mass of substance. $C_p = [\partial(H/M)/\partial T]_p$. At constant volume $C_v = [\partial(U/M)/\partial T]_v$. Numerical values for C_p are given in J g⁻¹ K⁻¹, cal g⁻¹ K⁻¹, and Btu lb⁻¹ °F⁻¹.

Sublimation Pressure. The saturated equilibrium pressure over the solid substance at a given temperature. Values are expressed in pascals (Pa = N·m⁻²) and in Torr (Torr = 133.3224 Pa). The conventional atmosphere is taken as 101325 Pa. One bar is 100,000 Pa.

Temperature. The absolute temperature, T , is based upon the International Practical Temperature Scale. Values are given in kelvins (symbol K). The Celsius ("Centigrade") scale (symbol °C) is used to indicate the temperature or temperature range for many reported measurements. It is defined as $t(^{\circ}\text{C}) = T(\text{K}) - 273.15$. The Fahrenheit scale, provided as a convenience for many measurements, is defined as $t(^{\circ}\text{F}) = 1.8t(^{\circ}\text{C}) + 32$. Unless specifically indicated otherwise, all temperatures T involved in equations are absolute temperature (T , K).

Ultimate Analysis. The determination of the percentages of carbon, hydrogen, nitrogen, sulfur, chlorine, ash, and oxygen in a dry sample. The percentage of oxygen is usually obtained by difference between 100% and the sum of the other determined elemental analyses.

Vapor Pressure. The saturated equilibrium pressure over the liquid substance at a given temperature. Values are expressed in pascals ($\text{Pa} = \text{N}\cdot\text{m}^{-2}$) and in Torr (Torr = 133.3224 Pa). The conventional atmosphere is taken as 101325 Pa.

Volatile Concentration. The determination of the volatile concentration (VCM) as described in 85JEN/EBE differs somewhat from the procedures described in the *ASTM Standard Test Methods*. In 85JEN/EBE, the sample is placed in a covered crucible at 600°C for 6 minutes followed by heating at 950°C for 6 minutes. The loss in weight is the volatile fraction.

Volatile Matter. Those products exclusive of moisture given off by the sample as a gas or vapor determined by definite prescribed procedures. In ASTM D 3175-77, *Standard Test Method for Volatile Matter in the Analysis of Coal and Coke*, the weighed sample is placed in a covered platinum crucible at 950°C for exactly 7 minutes. The loss in weight is the volatile fraction.

Uncertainties. No attempt has been made to assess the overall uncertainty of the data included. For some substances, uncertainties are given for the values; these represent the original authors' estimates and are usually a measure of the reproducibility of their measurements. A large assigned uncertainty usually indicates a variability of sample, not a low precision of measurement.

Use of Enthalpy versus Heat. The term "heat" has been used loosely in the scientific and engineering literature in that it does not differentiate clearly between processes at constant volume (U , internal energy) and those at constant pressure (H , enthalpy). Usage of thermodynamic state functions, such as the internal energy and enthalpy, are clear and unambiguous by their definitions. When preceded by the words "gross" or "net," the word "heat" indicates specific conditions as described in various definitions.

Multiple Sources of Data. Occasionally, several references are found in the literature that report the same thermodynamic property for a particular material. The measured

values are most often not equivalent, and a selection must be made as to which value is preferred. For some materials (such as coals or wood species), the values tabulated are typical values selected from a large number of results for samples of a similar nature. The selection process is based upon the personal and professional opinion of an evaluator after all property information for a material has been collected and examined. Factors taken into consideration are (1) description of the method used to carry out the measurements, (2) characterization of the material, (3) number of measurements performed, (4) treatment of the experimental data, (5) dispersion of the results, and (6) background or experience of the laboratory personnel carrying out the measurements.

Agricultural Residues

ALFALFA, SEED, STRAW; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 72.60, ash content = 7.25, and fixed carbon = 20.15. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 46.76, hydrogen = 5.40, oxygen = 40.72, nitrogen = 1.00, sulfur = 0.02, chlorine = 0.03, and residue (ash) = 6.07.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7937 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4410 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18450 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7468 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4149 \text{ cal g}^{-1} \\q_v(\text{net}) &= 17360 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

ALMOND HULLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 71.33, ash content = 5.78, and fixed carbon = 22.89. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 45.79, hydrogen = 5.36, oxygen = 40.60, nitrogen = 0.96, sulfur = 0.01, chlorine = 0.08, and residue (ash) = 7.20.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7838 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4355 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18220 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7370 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4094 \text{ cal g}^{-1} \\q_v(\text{net}) &= 17130 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

ALMOND, ORCHARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 76.83, ash content = 1.63, and fixed carbon = 21.54. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 51.30, hydrogen = 5.29, oxygen = 40.90, nitrogen = 0.66, sulfur = 0.01, chlorine = 0.04, and residue (ash) = 1.80.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8609 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4783 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20010 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8144 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4524 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18930 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

ALMOND SHELLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 73.45, ash content = 4.81, and fixed carbon = 21.74. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 44.98, hydrogen = 5.97, oxygen = 42.27, nitrogen = 1.16, sulfur = 0.02, and residue (ash) = 5.60.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8337 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4632 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19380 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7817 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4343 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18170 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

BABASSU HUSKS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 79.71, ash content = 1.59, and fixed carbon = 18.70. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 50.31, hydrogen = 5.37, oxygen = 42.29, nitrogen = 0.26, sulfur = 0.04, and residue (ash) = 1.73.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8570 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4761 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19920 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8101 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4500 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18830 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

BARLEY STRAW; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 68.80, ash content = 10.30, and fixed carbon = 20.90. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 39.92, hydrogen = 5.27, oxygen = 43.81, nitrogen = 1.25, and residue (ash) = 9.75.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7447 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4137 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17310 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 6987 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3881 \text{ cal g}^{-1} \\q_v(\text{net}) &= 16240 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

BEAN STRAW; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 75.30, ash content = 5.93, and fixed carbon = 18.77. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 42.97, hydrogen = 5.59, oxygen = 44.93, nitrogen = 0.83, sulfur = 0.01, chlorine = 0.13; and residue (ash) = 5.54.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7511 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4173 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17460 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7021 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3901 \text{ cal g}^{-1} \\q_v(\text{net}) &= 16320 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

BLACK WALNUT, ORCHARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 80.69, ash content = 0.78, and fixed carbon = 18.53. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.80, hydrogen = 5.82, oxygen = 43.25, nitrogen = 0.22, sulfur = 0.01, chlorine = 0.05, and residue (ash) = 0.85.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8531 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4739 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19830 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8023 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4457 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18650 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

CABERNET SAUVIGNON GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 78.63, ash content = 2.17, and fixed carbon = 19.20. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 46.59, hydrogen = 5.85, oxygen = 43.90, nitrogen = 0.83, sulfur = 0.04, chlorine = 0.08, and residue (ash) = 2.71.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8187 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4548 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19030 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7675 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4264 \text{ cal g}^{-1} \\q_v(\text{net}) &= 17840 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

CARDINAL GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 78.17, ash content = 2.22, and fixed carbon = 19.61.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8264 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4591 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19210 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

CHENIN BLANC GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 77.28, ash content = 2.51, and fixed carbon = 20.21. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.02, hydrogen = 5.89, oxygen = 41.93, nitrogen = 0.86, sulfur = 0.07, chlorine = 0.10, and residue (ash) = 3.13.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$q_v(\text{gross}) = 8230 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4572 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19130 \text{ J g}^{-1}$$

net heat of combustion: assume values refer to room temperature.

$$q_v(\text{net}) = 7718 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 4288 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 17940 \text{ J g}^{-1}$$

85JEN/EBE

COCOA HULLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 67.95, ash content = 8.25, and fixed carbon = 23.80. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.23, hydrogen = 5.23, oxygen = 33.19, nitrogen = 2.98, sulfur = 0.12, and residue (ash) = 10.25.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$q_v(\text{gross}) = 8191 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4551 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19040 \text{ J g}^{-1}$$

net heat of combustion: assume values refer to room temperature.

$$q_v(\text{net}) = 7731 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 4295 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 17970 \text{ J g}^{-1}$$

85JEN/EBE

COCONUT FIBER, DUST; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 66.58, ash content = 3.72, and fixed carbon = 29.70. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 50.29, hydrogen = 5.05, oxygen = 39.63, nitrogen = 0.45, sulfur = 0.16, chlorine = 0.28, and residue (ash) = 4.14.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8626 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4792 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20050 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8183 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4546 \text{ cal g}^{-1} \\q_v(\text{net}) &= 19020 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

CORN COBS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 80.10, ash content = 1.36, and fixed carbon = 18.54. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 46.58, hydrogen = 5.87, oxygen = 45.46, nitrogen = 0.47, sulfur = 0.01, chlorine = 0.21, and residue (ash) = 1.40.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8075 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4486 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18770 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7563 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4202 \text{ cal g}^{-1} \\q_v(\text{net}) &= 17580 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

CORN STOVER; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 75.17, ash content = 5.58, and fixed carbon = 19.25. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 43.65, hydrogen = 5.56, oxygen = 43.31, nitrogen = 0.61, sulfur = 0.01, chlorine = 0.60, and residue (ash) = 6.26.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7593 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4218 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17650 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7107 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3948 \text{ cal g}^{-1} \\q_v(\text{net}) &= 16520 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

COTTON GIN TRASH; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 67.30, ash content = 17.60, and fixed carbon = 15.10. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 39.59, hydrogen = 5.26, oxygen = 36.38, nitrogen = 2.09, and residue (ash) = 16.68.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7064 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3924 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16420 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 6604 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3669 \text{ cal g}^{-1} \\q_v(\text{net}) &= 15350 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

COTTON STALKS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 65.40, ash content = 17.30, and fixed carbon = 17.30. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 39.47, hydrogen = 5.07, oxygen = 39.14, nitrogen = 1.20, sulfur = 0.02, and residue (ash) = 15.10.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 6810 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3783 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 15830 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 6363 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3535 \text{ cal g}^{-1} \\q_v(\text{net}) &= 14790 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

ENGLISH WALNUT, ORCHARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 80.82, ash content = 1.08, and fixed carbon = 18.10. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.72, hydrogen = 5.63, oxygen = 43.14, nitrogen = 0.37, sulfur = 0.01, chlorine = 0.06, and residue (ash) = 1.07.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8445 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4692 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19630 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7955 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4419 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18490 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

GEWURZTRAMINER GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 77.27, ash content = 2.47, and fixed carbon = 20.26.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8243 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4579 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19160 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

GRAPE POMACE; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 68.54, ash content = 9.48, and fixed carbon = 21.98. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 52.91, hydrogen = 5.93, oxygen = 30.41, nitrogen = 1.86, sulfur = 0.03, chlorine = 0.05, and residue (ash) = 8.81.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8750 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4861 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20340 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8234 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4575 \text{ cal g}^{-1} \\q_v(\text{net}) &= 19140 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

MACADAMIA SHELLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 75.92, ash content = 0.40, and fixed carbon = 23.68. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 54.41, hydrogen = 4.99, oxygen = 39.69, nitrogen = 0.36, sulfur = 0.01, and residue (ash) = 0.56.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 9039 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5022 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21010 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8604 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4780 \text{ cal g}^{-1} \\q_v(\text{net}) &= 20000 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

MERLOT GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 77.47, ash content = 3.04, and fixed carbon = 19.49.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8105 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4503 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18840 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

OLIVE PITS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 78.65, ash content = 3.16, and fixed carbon = 18.19. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.81, hydrogen = 6.23, oxygen = 43.48, nitrogen = 0.36, sulfur = 0.02, and residue (ash) = 1.10.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 9202 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5112 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21390 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8656 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4809 \text{ cal g}^{-1} \\q_v(\text{net}) &= 20120 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

PEACH PITS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 79.12, ash content = 1.03, and fixed carbon = 19.85. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 53.00, hydrogen = 5.90, oxygen = 39.14, nitrogen = 0.32, sulfur = 0.05, and residue (ash) = 1.59.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8957 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4976 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20820 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8441 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4689 \text{ cal g}^{-1} \\q_v(\text{net}) &= 19620 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

PEANUT HULLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 73.02, ash content = 5.89, and fixed carbon = 21.09. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 45.77, hydrogen = 5.46, oxygen = 39.56, nitrogen = 1.63, sulfur = 0.12, and residue (ash) = 7.46.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8019 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4455 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18640 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7542 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4190 \text{ cal g}^{-1} \\q_v(\text{net}) &= 17530 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

PINOT NOIR GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 76.83, ash content = 2.71, and fixed carbon = 20.46. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 47.14, hydrogen = 5.82, oxygen = 43.03, nitrogen = 0.86, sulfur = 0.01, chlorine = 0.13, and residue (ash) = 3.01.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8196 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4553 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19050 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7684 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4269 \text{ cal g}^{-1} \\q_v(\text{net}) &= 17860 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

PISTACHIO SHELLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 82.03, ash content = 1.13, and fixed carbon = 16.84. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.79, hydrogen = 5.91, oxygen = 43.41, nitrogen = 0.56, sulfur = 0.01, chlorine = 0.04, and residue (ash) = 1.28.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8286 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4603 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19260 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7770 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4316 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18060 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

PRUNE PITS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 76.99, ash content = 0.50, and fixed carbon = 22.51. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.73, hydrogen = 5.90, oxygen = 43.57, nitrogen = 0.32, and residue (ash) = 0.48.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 10015 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5564 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23280 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 9499 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 5277 \text{ cal g}^{-1} \\q_v(\text{net}) &= 22080 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

RIBIER GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 76.97, ash content = 3.03, and fixed carbon = 20.00.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8226 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4570 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19120 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

RICE HULLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 65.47, ash content = 17.86, and fixed carbon = 16.67. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 40.96, hydrogen = 4.30, oxygen = 35.86, nitrogen = 0.40, sulfur = 0.02, chlorine = 0.12, and residue (ash) = 18.34.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 6944 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3858 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16140 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 6569 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3650 \text{ cal g}^{-1} \\q_v(\text{net}) &= 15270 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

RICE STRAW (COLLECTED AFTER HARVEST); solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 69.33, ash content = 13.42, and fixed carbon = 17.25. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 41.78, hydrogen = 4.63, oxygen = 36.57, nitrogen = 0.70, sulfur = 0.08, chlorine = 0.34, and residue (ash) = 15.90.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7004 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3891 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16280 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 6599 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3666 \text{ cal g}^{-1} \\q_v(\text{net}) &= 15340 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

RICE STRAW, WEATHERED (COLLECTED 1/2 YEAR AFTER HARVEST); solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 62.31, ash content = 24.36, and fixed carbon = 13.33. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 34.60, hydrogen = 3.93, oxygen = 35.38, nitrogen = 0.93, sulfur = 0.16, and residue (ash) = 25.00.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 6264 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3480 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 14560 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 5920 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3289 \text{ cal g}^{-1} \\q_v(\text{net}) &= 13760 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

SAFFLOWER STRAW; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 77.05, ash content = 4.65, and fixed carbon = 18.30. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 41.71, hydrogen = 5.54, oxygen = 46.58, nitrogen = 0.62, and residue (ash) = 5.55.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8273 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4596 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19230 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7787 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4326 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18100 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

SUGARCANE BAGASSE; solid; Nine varieties of Indian sugarcane were used. Average ash content, 3.66%; average moisture content, 4.51%. Fibers obtained from shredding cane in a laboratory shredder and washing in running water for 24 hours to remove all soluble substances. Fibers were dried at 100°-105°C (212°-221°F) to constant weight and pulverized to pass through 60 mesh sieve.

gross heat of combustion: assume value refers to room temperature and is on a moisture-free, ash-free basis. Value is an average of gross heats of combustion of nine different varieties bagasse. The uncertainty is given as two times the standard deviation of the mean.

$$\begin{aligned}q_v(\text{gross}) &= 8188 \pm 78 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4549 \pm 43 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19033 \pm 180 \text{ J g}^{-1}\end{aligned}$$

53BHA

SUGARCANE BAGASSE; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 73.78, ash content = 11.27, and fixed carbon = 14.95. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 44.80, hydrogen = 5.35, oxygen = 39.55, nitrogen = 0.38, sulfur = 0.01, chlorine = 0.12, and residue (ash) = 9.79.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned} q_v(\text{gross}) &= 7456 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4142 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17330 \text{ J g}^{-1} \end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{net}) &= 6987 \text{ Btu lb}^{-1} \\ q_v(\text{net}) &= 3881 \text{ cal g}^{-1} \\ q_v(\text{net}) &= 16240 \text{ J g}^{-1} \end{aligned}$$

85JEN/EBE

SUGARCANE BAGASSE; solid; Material is fibrous residue from sugar cane after the cane is harvested and crushed to extract the juice. Mill-run bagasse contains an average of 46%-52% moisture, 43%-52% fiber, and 2%-6% soluble solids (mostly sucrose). Substance is composed of pith (30% dry weight of cane), fiber bundles contained in pith (15% dry weight of cane), true fiber cell rind of stalk (50% dry weight of cane), and dense waxy nonfibrous epidermus (5% dry weight of cane).

gross heat of combustion: Formulas are derived from $q_v(\text{gross})$ of dry, ash-free fiber = 8442 Btu lb⁻¹, $q_v(\text{gross})$ of soluble matter called Brix = 7110 Btu lb⁻¹, average ash content = 3% of dry material, and where S denotes the sucrose and W the moisture content % bagasse.

$$\begin{aligned} q_v(\text{gross}) &= 8190 - 18 S - 81.9 W \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4550 - 10 S - 45.5 W \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19037 - 42 S - 190.4 W \text{ J g}^{-1} \end{aligned}$$

net heat of combustion: Formulas are derived from deduction of latent heat of water vapor from $q_v(\text{gross})$ and where S denotes sucrose and W is moisture content % bagasse.

$$\begin{aligned} q_v(\text{net}) &= 7650 - 18 S - 86.4 W \text{ Btu lb}^{-1} \\ q_v(\text{net}) &= 4250 - 10 S - 48.0 W \text{ cal g}^{-1} \\ q_v(\text{net}) &= 17782 - 42 S - 200.8 W \text{ J g}^{-1} \end{aligned}$$

53PER

THOMPSON SEEDLESS GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 77.39, ash content = 2.25, and fixed carbon = 20.36. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 47.35, hydrogen = 5.77, oxygen = 43.32, nitrogen = 0.77, sulfur = 0.01, chlorine = 0.07, and residue (ash) = 2.71.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8325 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4625 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19350 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7821 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4345 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18180 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

TOKAY GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 76.53, ash content = 2.45, and fixed carbon = 21.02. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 47.77, hydrogen = 5.82, oxygen = 42.63, nitrogen = 0.75, sulfur = 0.03, chlorine = 0.07, and residue (ash) = 2.93.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8307 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4615 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19310 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7795 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4331 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18120 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

Agricultural Residues

WALNUT SHELLS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 78.28, ash content = 0.56, and fixed carbon = 21.16. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.98, hydrogen = 5.71, oxygen = 43.35, nitrogen = 0.21, sulfur = 0.01, chlorine = 0.03, and residue (ash) = 0.71.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8682 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4823 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20180 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8183 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4546 \text{ cal g}^{-1} \\q_v(\text{net}) &= 19020 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

WHEAT DUST, FOOD AND FIBER PROCESSING WASTE; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 69.85, ash content = 13.68, and fixed carbon = 16.47. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 41.38, hydrogen = 5.10, oxygen = 35.19, nitrogen = 3.04, sulfur = 0.19, and residue (ash) = 15.10.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 6969 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3872 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16200 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 6522 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3623 \text{ cal g}^{-1} \\q_v(\text{net}) &= 15160 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

WHEAT STRAW; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 71.30, ash content = 8.90, and fixed carbon = 19.80. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 43.20, hydrogen = 5.00, oxygen = 39.40, nitrogen = 0.61, sulfur = 0.11, chlorine = 0.28, and residue (ash) = 11.40.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7533 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4185 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17510 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7094 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3941 \text{ cal g}^{-1} \\q_v(\text{net}) &= 16490 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

ZINFANDEL GRAPES, VINEYARD PRUNINGS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 76.99, ash content = 3.04, and fixed carbon = 19.49.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8200 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4555 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19060 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

α -BRASS; solid; chemical composition in wt.%; (sample 1): copper, 79.75%; lead, 0.003%; iron, 0.015%; nickel, 0.01%; zinc, 20.22%; (sample 2): copper, 70.42%; tin, 0.045%; lead, 0.05%; iron, 0.02%; nickel, 0.02%; zinc, 29.445%; (sample 3): copper, 65.18%; lead, 0.001%; iron, 0.002%; nickel, 0.002%; zinc, 34.815%.

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
sample 1			
298.15 77	0.0908	0.0908	0.3798
400 260	0.0940	0.0940	0.3935
500 440	0.1014	0.1014	0.4243
600 620	0.1005	0.1005	0.4205
700 800	0.1039	0.1039	0.4347
800 980	0.1056	0.1056	0.4418
sample 2			
298.15 77	0.0905	0.0905	0.3787
400 260	0.0943	0.0943	0.3946
500 440	0.1114	0.1114	0.4661
600 620	0.1011	0.1011	0.4230
700 800	0.1045	0.1045	0.4372
800 980	0.1064	0.1064	0.4452
sample 3			
298.15 77	0.0905	0.0905	0.3787
400 260	0.0941	0.0941	0.3937
500 440	0.1050	0.1050	0.4393
600 620	0.1016	0.1016	0.4251
700 800	0.1060	0.1060	0.4435
800 980	0.1091	0.1091	0.4565

67CHA/HUL

Alloys and Metals

80 NICKEL-20 CHROMIUM; solid; composition: nickel, 77.4%; chromium, 19.52%; iron, 0.45%; manganese, 0.59%; silicon, 1.4%; carbon, 0.04%.

specific heat:

273-423 K (32°-302°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.10191 + 4.222 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.0825 + 7.6 \times 10^{-5} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.3452 + 3.18 \times 10^{-4} T \end{aligned}$$

423-873 K (302°-1112°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.10705 + 2.578 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.0952 + 4.64 \times 10^{-5} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.3983 + 1.941 \times 10^{-4} T \end{aligned}$$

873-1173 K (1112°-1652°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.11390 + 2.567 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.1021 + 4.62 \times 10^{-5} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.4271 + 1.933 \times 10^{-4} T \end{aligned}$$

55DOU/DEV

ALUMINUM; solid; atomic number, 13; atomic wt., 26.98154; density, 2.712 g cm⁻³ (169.3 lb ft⁻³).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is α -corundum, Al₂O₃.

$$\begin{aligned} q_p(\text{gross}) &= 13359 \text{ Btu lb}^{-1} \\ q_p(\text{gross}) &= 7422 \text{ cal g}^{-1} \\ q_p(\text{gross}) &= 31053 \text{ J g}^{-1} \end{aligned}$$

82WAG/EVA

specific heat:

temperature (K) (°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
298 77	0.216	0.216	0.904
500 441	0.238	0.238	0.996
700 801	0.260	0.260	1.087

heat of fusion: at the melting point, 659°C (1218°F).

$$\begin{aligned} L_f &= 171.5 \text{ Btu lb}^{-1} \\ L_f &= 95.25 \text{ cal g}^{-1} \\ L_f &= 398.5 \text{ J g}^{-1} \end{aligned}$$

(more)

α -BRASS; solid; chemical composition in wt.%; (sample 1): copper, 79.75%; lead, 0.003%; iron, 0.015%; nickel, 0.01%; zinc, 20.22%; (sample 2): copper, 70.42%; tin, 0.045%; lead, 0.05%; iron, 0.02%; nickel, 0.02%; zinc, 29.445%; (sample 3): copper, 65.18%; lead, 0.001%; iron, 0.002%; nickel, 0.002%; zinc, 34.815%.

specific heat:

temperature (K) (°F)		C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
sample 1				
298.15	77	0.0908	0.0908	0.3798
400	260	0.0940	0.0940	0.3935
500	440	0.1014	0.1014	0.4243
600	620	0.1005	0.1005	0.4205
700	800	0.1039	0.1039	0.4347
800	980	0.1056	0.1056	0.4418
sample 2				
298.15	77	0.0905	0.0905	0.3787
400	260	0.0943	0.0943	0.3946
500	440	0.1114	0.1114	0.4661
600	620	0.1011	0.1011	0.4230
700	800	0.1045	0.1045	0.4372
800	980	0.1064	0.1064	0.4452
sample 3				
298.15	77	0.0905	0.0905	0.3787
400	260	0.0941	0.0941	0.3937
500	440	0.1050	0.1050	0.4393
600	620	0.1016	0.1016	0.4251
700	800	0.1060	0.1060	0.4435
800	980	0.1091	0.1091	0.4565

67CHA/HUL

Alloys and Metals

80 NICKEL-20 CHROMIUM; solid; composition: nickel, 77.4%; chromium, 19.52%; iron, 0.45%; manganese, 0.59%; silicon, 1.4%; carbon, 0.04%.

specific heat:

273-423 K (32°-302°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.10191 + 4.222 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.0825 + 7.6 \times 10^{-5} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.3452 + 3.18 \times 10^{-4} T \end{aligned}$$

423-873 K (302°-1112°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.10705 + 2.578 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.0952 + 4.64 \times 10^{-5} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.3983 + 1.941 \times 10^{-4} T \end{aligned}$$

873-1173 K (1112°-1652°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.11390 + 2.567 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.1021 + 4.62 \times 10^{-5} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.4271 + 1.933 \times 10^{-4} T \end{aligned}$$

55DOU/DEV

ALUMINUM; solid; atomic number, 13; atomic wt., 26.98154; density, 2.712 g cm⁻³ (169.3 lb ft⁻³).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is α -corundum, Al₂O₃.

$$\begin{aligned} q_p(\text{gross}) &= 13359 \text{ Btu lb}^{-1} \\ q_p(\text{gross}) &= 7422 \text{ cal g}^{-1} \\ q_p(\text{gross}) &= 31053 \text{ J g}^{-1} \end{aligned}$$

82WAG/EVA

specific heat:

temperature (K) (°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
298 77	0.216	0.216	0.904
500 441	0.238	0.238	0.996
700 801	0.260	0.260	1.087

heat of fusion: at the melting point, 659°C (1218°F).

$$\begin{aligned} L_f &= 171.5 \text{ Btu lb}^{-1} \\ L_f &= 95.25 \text{ cal g}^{-1} \\ L_f &= 398.5 \text{ J g}^{-1} \end{aligned}$$

(more)

ALUMINUM - Continued

heat of vaporization: at the boiling point, 2441°C (4426°F).

$$L_v = 4676 \text{ Btu lb}^{-1}$$

$$L_v = 2598 \text{ cal g}^{-1}$$

$$L_v = 10871 \text{ J g}^{-1}$$

vapor pressure:

temperature		P(atm)	P(Pa)	P(psi)
(°C)	(°F)			
1060	1940	10^{-6}	0.1	1.470×10^{-5}
1509	2748	10^{-3}	101.3	1.470×10^{-2}
1743	3169	10^{-2}	1013.3	1.470×10^{-1}
2039	3702	10^{-1}	10132.5	1.470
2441	4426	1.0	101325.	14.696

63HUL/ORR

ALUMINUM 2024-T4; solid; composition: copper, 4.5%; magnesium, 1.5%; manganese, 0.6%; aluminum, 93.4%.

specific heat: -120° to 425°C (-250° to 800°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.1933 + 1.539 \times 10^{-4} T - 2.260 \times 10^{-7} T^2 + 1.903 \times 10^{-10} T^3$$

$$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1}) = 0.198 + 2.52 \times 10^{-4} T - 6.73 \times 10^{-7} T^2 + 1.11 \times 10^{-9} T^3$$

$$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1}) = 0.828 + 10.5 \times 10^{-4} T - 28.2 \times 10^{-7} T^2 + 4.64 \times 10^{-9} T^3$$

58LUC/DEE

ALUMINUM 7075-T6; solid; composition: zinc, 5.5%; magnesium, 2.5%; copper, 1.5%; chromium, 0.3%.

specific heat: -120° to 425°C (-184° to 800°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.1914 + 1.505 \times 10^{-4} T - 1.896 \times 10^{-7} T^2 + 1.715 \times 10^{-10} T^3$$

$$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1}) = 0.196 + 2.50 \times 10^{-4} T - 5.61 \times 10^{-7} T^2 + 1.00 \times 10^{-9} T^3$$

$$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1}) = 0.820 + 10.5 \times 10^{-4} T - 23.5 \times 10^{-7} T^2 + 4.18 \times 10^{-9} T^3$$

58LUC/DEE

Alloys and Metals

CADIUM; solid; atomic number, 48; atomic wt., 112.41; density, 8.642 g cm^{-3} (539.5 lb ft^{-3}).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is cadmium oxide, CdO .

$$q_p(\text{gross}) = 988 \text{ Btu lb}^{-1}$$

$$q_p(\text{gross}) = 549 \text{ cal g}^{-1}$$

$$q_p(\text{gross}) = 2297 \text{ J g}^{-1}$$

82WAG/EVA

specific heat:

temperature		$C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
(K)	($^\circ\text{F}$)			
298	77	0.0552	0.0552	0.231
400	261	0.0577	0.0577	0.242
500	441	0.0603	0.0603	0.252

heat of fusion: at the melting point, 321°C (610°F).

$$L_f = 23.4 \text{ Btu lb}^{-1}$$

$$L_f = 13.0 \text{ cal g}^{-1}$$

$$L_f = 54.4 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point, 2441°C (4426°F).

$$L_v = 382 \text{ Btu lb}^{-1}$$

$$L_v = 212 \text{ cal g}^{-1}$$

$$L_v = 887 \text{ J g}^{-1}$$

vapor pressure:

temperature		P(atm)	P(Pa)	P(psi)
($^\circ\text{C}$)	($^\circ\text{F}$)			
213	415	10^{-6}	0.1	1.470×10^{-5}
385	725	10^{-3}	101.3	1.470×10^{-2}
477	891	10^{-2}	1013.3	1.470×10^{-1}
597	1107	10^{-1}	10132.5	1.470
767	1413	1.0	101325.	14.696

63HUL/ORR

CHROMIUM; solid; atomic number, 24; atomic wt., 51.9961; density, 7.2 g cm^{-3}
(449.5 lb ft^{-3}).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is Cr_2O_3 .

$$q_p(\text{gross}) = 4715 \text{ Btu lb}^{-1}$$

$$q_p(\text{gross}) = 2619 \text{ cal g}^{-1}$$

$$q_p(\text{gross}) = 10959 \text{ J g}^{-1}$$

82WAG/EVA

specific heat:

temperature (K) (°F)	$C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
298 77	0.107	0.107	0.449
500 441	0.123	0.123	0.515
700 801	0.128	0.128	0.538

heat of fusion: at the melting point 1903°C (3457°F).

$$L_f = 170 \text{ Btu lb}^{-1}$$

$$L_f = 96 \text{ cal g}^{-1}$$

$$L_f = 400 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point 2665°C (4829°F).

$$L_v = 2814 \text{ Btu lb}^{-1}$$

$$L_v = 1563 \text{ cal g}^{-1}$$

$$L_v = 6542 \text{ J g}^{-1}$$

vapor pressure:

temperature (°C) (°F)	P(atm)	P(Pa)	P(psi)
1252 2286	10^{-6}	0.1	1.470×10^{-5}
1711 3112	10^{-3}	101.3	1.470×10^{-2}
1937 3519	10^{-2}	1013.3	1.470×10^{-1}
2250 4082	10^{-1}	10132.5	1.470
2665 4829	1.0	101325.	14.696

63HUL/ORR

Alloys and Metals

CONSTANTAN; solid; composition range centering on 55 wt. % copper and 45 wt. % nickel.

specific heat: values refer to specific alloy; 60 wt. % Cu and 40 wt. % Ni; the other constantans should have specific heat within 5% of the following values.

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
1 -457.6	0.000026	0.000026	0.00011
50 -369.4	0.020	0.020	0.083
100 -279.4	0.057	0.057	0.283
200 -99.4	0.87	0.87	0.362

40KEE/KUR

COPPER; solid; atomic number, 29; atomic wt., 63.546; density, 9.92 g cm⁻³ (556.9 lb ft⁻³).

gross heat of combustion: q_p (gross) is equal to the enthalpy of combustion, $-\Delta H_c^0$ at 25°C (77°F); product of combustion is cuprous oxide, Cu₂O.

$$q_p(\text{gross}) = 570.7 \text{ Btu lb}^{-1}$$

$$q_p(\text{gross}) = 317.1 \text{ cal g}^{-1}$$

$$q_p(\text{gross}) = 1326.6 \text{ J g}^{-1}$$

82WAG/EVA

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
298 77	0.0922	0.0922	0.386
500 441	0.0971	0.0971	0.406
700 801	0.1018	0.1018	0.426

heat of fusion: at the melting point 1084°C (1983°F).

$$L_f = 88.4 \text{ Btu lb}^{-1}$$

$$L_f = 49.1 \text{ cal g}^{-1}$$

$$L_f = 205.4 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point 2573°C (4663°F).

$$L_v = 2057 \text{ Btu lb}^{-1}$$

$$L_v = 1143 \text{ cal g}^{-1}$$

$$L_v = 4780 \text{ J g}^{-1}$$

(more)

COPPER - continued

vapor pressure:

temperature (°C)	(°F)	P(atm)	P(Pa)	P(psi)
1118	2044	10^{-6}	0.1	1.470×10^{-5}
1589	2892	10^{-3}	101.3	1.470×10^{-2}
1830	3326	10^{-2}	1013.3	1.470×10^{-1}
2142	3888	10^{-1}	10132.5	1.470
2573	4663	1.0	101325.	14.696

63HUL/ORR

HASTELLOY X; solid; composition: carbon, 0.05%-0.15%; chromium, 20.50%-23.00%; cobalt, 0.05%-2.50%; iron, 17.00%-20.00%; manganese, 1.00% max.; molybdenum, 8.00%-10.00%; silicon, 1.00% max.; tungsten, 0.2%-1.0%; remainder nickel, 42.0%-54.0%.

specific heat: 273-1373 K (32°-2012°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.1037 + 2.4443 \times 10^{-5} T + 4.4886 \times 10^{-3} T^2 + 7.6473 \times 10^{-15} T^3 - 1.1710 \times 10^{-16} T^4 + 7.3033 \times 10^{-19} T^5$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.0924 + 4.438 \times 10^{-5} T - 2.812 \times 10^{-9} T^2 + 1.030 \times 10^{-11} T^3 - 1.885 \times 10^{-14} T^4 + 1.38 \times 10^{-17} T^5$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 0.3866 + 1.8569 \times 10^{-4} T - 1.1765 \times 10^{-8} T^2 + 4.310 \times 10^{-11} T^3 - 7.887 \times 10^{-14} T^4 + 5.77 \times 10^{-17} T^5$$

heat content: 273-1373 K (32°-2012°F)

$$q_T - q_{32}(\text{Btu lb}^{-1}) = 0.1020 T + 8.6309 \times 10^{-6} T^2 - 2.6035 \times 10^{-9} T^3 + 1.9119 \times 10^{-15} T^4 - 2.4321 \times 10^{-17} T^5 + 1.2172 \times 10^{-19} T^6 - 4.0464 (^\circ\text{F})$$

$$q_T - q_{273.2}(\text{cal g}^{-1}) = 0.0924 T + 2.219 \times 10^{-5} T^2 - 9.373 \times 10^{-9} T^3 + 2.575 \times 10^{-12} T^4 - 3.770 \times 10^{-15} T^5 + 2.30 \times 10^{-18} T^6 - 27.1429 (\text{K})$$

$$q_T - q_{273.2}(\text{J g}^{-1}) = 0.3866 T + 9.284 \times 10^{-5} T^2 - 3.922 \times 10^{-8} T^3 + 1.0774 \times 10^{-11} T^4 - 1.5774 \times 10^{-14} T^5 + 9.62 \times 10^{-18} T^6 - 113.5659 (\text{K})$$

64THA/KOH

Alloys and Metals

INCONEL, ANNEALED; solid; composition: carbon, 0.04 wt. %; manganese, 0.35 wt. %; silicon, 0.20 wt. %; chromium, 15 wt. %; nickel, 78 wt. %; iron, 7.00 wt. %.

specific heat: -120° to 982°C (-184° to 1800°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.0967 + 7.366 \times 10^{-5} T - 6.724 \times 10^{-8} T^2 + 2.846 \times 10^{-11} T^3 \\ C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1}) &= 0.099 + 1.25 \times 10^{-4} T - 2.09 \times 10^{-7} T^2 + 1.66 \times 10^{-10} T^3 \\ C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1}) &= 0.414 + 5.23 \times 10^{-4} T - 8.74 \times 10^{-7} T^2 + 6.95 \times 10^{-10} T^3 \end{aligned}$$

58LUC/DEE

INCONEL "X"; solid; composition: carbon, 0.04 wt. %; manganese, 0.70 wt. %; silicon, 0.30 wt. %; chromium, 15.00 wt. %; nickel, 73.00 wt. %; iron, 7.00 wt. %; niobium, 1.00 wt. %; titanium, 2.50 wt. %; aluminum, 0.9 wt. %.

specific heat: -120° to 982°C (-184° to 1800°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.09775 + 7.284 \times 10^{-5} T - 8.098 \times 10^{-8} T^2 + 3.978 \times 10^{-11} T^3 \\ C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1}) &= 0.100 + 1.22 \times 10^{-4} T - 2.50 \times 10^{-7} T^2 + 2.32 \times 10^{-10} T^3 \\ C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1}) &= 0.418 + 5.10 \times 10^{-4} T - 10.5 \times 10^{-7} T^2 + 9.71 \times 10^{-10} T^3 \end{aligned}$$

58LUC/DEE

IRON; solid; atomic number, 26; atomic wt., 55.847; density, 7.86 g cm⁻³ (490.7 lb ft⁻³).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is hematite, Fe₂O₃.

$$\begin{aligned} q_p(\text{gross}) &= 3175 \text{ Btu lb}^{-1} \\ q_p(\text{gross}) &= 1764 \text{ cal g}^{-1} \\ q_p(\text{gross}) &= 7379 \text{ J g}^{-1} \end{aligned}$$

82WAG/EVA

specific heat:

temperature		$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
(K)	(°F)			
298	77	0.107	0.107	0.450
500	441	0.126	0.126	0.526
700	801	0.148	0.148	0.617

heat of fusion: at the melting point 1536°C (2797°F).

$$\begin{aligned} L_f &= 117.0 \text{ Btu lb}^{-1} \\ L_f &= 65.0 \text{ cal g}^{-1} \\ L_f &= 272.0 \text{ J g}^{-1} \end{aligned}$$

(more)

IRON - Continued

heat of vaporization: at the boiling point 2875°C (5207°F).

$$L_v = 2698 \text{ Btu lb}^{-1}$$

$$L_v = 1499 \text{ cal g}^{-1}$$

$$L_v = 6271 \text{ J g}^{-1}$$

vapor pressure:

temperature (°C)	(°F)	P(atm)	P(Pa)	P(psi)
1326	2419	10^{-6}	0.1	1.470×10^{-5}
1829	3324	10^{-3}	101.3	1.470×10^{-2}
2080	3776	10^{-2}	1013.3	1.470×10^{-1}
2417	4383	10^{-1}	10132.5	1.470
2875	5207	1.0	101325.	14.696

63HUL/ORR

IRON, CAST; liquid; composition of cast iron: base iron (Fe), the compound cementite (Fe_3C), and alloying elements of graphite (C) and silicon (Si), and lesser elements such as Mn, P, and S. A typical composition for ductile iron is C = 3.2%-4.2%, Si = 1.1%-3.5%, Mn = 0.3%-0.8%, P = 0.08%, S = 0.02%, and remainder Fe.

heat content: The temperature range is (~1400°-1600°C) (2600°-2900°F); T is in K; the equation applies to all cast iron and is the sum of individual heat content equations where the lesser elements are ignored. X is weight fraction of substance.

$$q_T - q_{32} (\text{Btu lb}^{-1}) = (0.3164T - 1.94) X_{\text{Fe}} + (0.3164T - 5.36) X_{\text{Fe}_3\text{C}} \\ + (0.9004T + 1494.4) X_{\text{C}} + (0.3902T + 989.5) X_{\text{Si}}$$

$$q_T - q_{273} (\text{cal g}^{-1}) = (0.1758T - 1.08) X_{\text{Fe}} + (0.1758T - 2.98) X_{\text{Fe}_3\text{C}} \\ + (0.5002T + 830.2) X_{\text{C}} + (0.2168T + 549.7) X_{\text{Si}}$$

$$q_T - q_{273} (\text{J g}^{-1}) = (0.7357T - 4.53) X_{\text{Fe}} + (0.7357T - 12.47) X_{\text{Fe}_3\text{C}} \\ + (2.0929T + 3473.5) X_{\text{C}} + (0.9072T + 2300.1) X_{\text{Si}}$$

73DUC

Alloys and Metals

LEAD; solid; atomic number, 82; atomic wt., 207.2; density, 11.3 g cm⁻³ (705.5 lb ft⁻³).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is PbO₂.

$$q_p(\text{gross}) = 576 \text{ Btu lb}^{-1}$$

$$q_p(\text{gross}) = 320 \text{ cal g}^{-1}$$

$$q_p(\text{gross}) = 1339 \text{ J g}^{-1}$$

82WAG/EVA

specific heat:

temperature (K)	(°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
298	77	0.0305	0.0305	0.128
500	441	0.0328	0.0328	0.137
600	621	0.0339	0.0339	0.142

heat of fusion: at the melting point 327.4°C (621.3°F).

$$L_f = 9.90 \text{ Btu lb}^{-1}$$

$$L_f = 5.50 \text{ cal g}^{-1}$$

$$L_f = 23.0 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point 1743°C (3169°F).

$$L_v = 368.0 \text{ Btu lb}^{-1}$$

$$L_v = 204.4 \text{ cal g}^{-1}$$

$$L_v = 855.3 \text{ J g}^{-1}$$

vapor pressure:

temperature (°C)	(°F)	P(atm)	P(Pa)	P(psi)
615	1139	10 ⁻⁶	0.1	1.470 × 10 ⁻⁵
956	1753	10 ⁻³	101.3	1.470 × 10 ⁻²
1137	2079	10 ⁻²	1013.3	1.470 × 10 ⁻¹
1388	2530	10 ⁻¹	10132.5	1.470
1743	3169	1.9	101325.	14.696

63HUL/ORR

MERCURY; liquid; atomic number, 80; atomic wt., 200.59; density, 13.5939 g cm⁻³ (848.667 lb ft⁻³).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is red, orthorhombic mercuric oxide, HgO.

$$q_p(\text{gross}) = 194.8 \text{ Btu lb}^{-1}$$

$$q_p(\text{gross}) = 108.2 \text{ cal g}^{-1}$$

$$q_p(\text{gross}) = 452.8 \text{ J g}^{-1}$$

82WAG/EVA

specific heat:

temperature		$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
(K)	(°F)			
298	77	0.0333	0.0333	0.140
500	441	0.0323	0.0323	0.135
600	621	0.0323	0.0323	0.135

heat of fusion: at the melting point -38.86°C (-37.95°F).

$$L_f = 4.922 \text{ Btu lb}^{-1}$$

$$L_f = 2.735 \text{ cal g}^{-1}$$

$$L_f = 11.44 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point 356.58°C (673.84°F).

$$L_v = 127.16 \text{ Btu lb}^{-1}$$

$$L_v = 70.644 \text{ cal g}^{-1}$$

$$L_v = 295.57 \text{ J g}^{-1}$$

vapor pressure:

temperature		P(atm)	P(Pa)	P(psi)
(°C)	(°F)			
14.17	57.51	10 ⁻⁶	0.1	1.470 × 10 ⁻⁵
120.21	248.38	10 ⁻³	101.3	1.470 × 10 ⁻²
175.98	348.76	10 ⁻²	1013.3	1.470 × 10 ⁻¹
250.78	483.40	10 ⁻¹	10132.5	1.470
356.58	673.84	1.0	101325.	14.696

63HUL/ORR

Alloys and Metals

MONEL; solid; corrosion resistant alloy; composition: nickel, 67 wt. %; copper, 30 wt. %; iron, 1.4 wt. %; manganese, 1 wt. %.

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
1 -457.6	0.000026	0.000026	0.00011
50 -369.4	0.019	0.019	0.078
100 -279.4	0.06	0.06	0.24
200 -99.4	0.09	0.09	0.37
300 80.6	0.10	0.10	0.43

40KEE/KUR

MONEL "K"; solid; composition: nickel, 63%-70%; aluminum, 2%-4%; iron, 2.0% (maximum); silicon, 1.0% (maximum); manganese, 1.5% (maximum); carbon, 0.25% (maximum); remainder is copper.

specific heat: -120° to 982°C (-184° to 1800°F)

$$\begin{aligned}
 C_p(\text{Btu lb}^{-1} \text{ °F}^{-1}) &= 0.09479 + 7.150 \times 10^{-5} T - 7.717 \times 10^{-8} T^2 + 3.549 \times 10^{-11} T^3 \\
 C_p(\text{cal g}^{-1} \text{ °C}^{-1}) &= 0.097 + 1.20 \times 10^{-4} T - 2.39 \times 10^{-7} T^2 + 2.07 \times 10^{-10} T^3 \\
 C_p(\text{J g}^{-1} \text{ °C}^{-1}) &= 0.406 + 5.02 \times 10^{-4} T - 10.0 \times 10^{-7} T^2 + 8.66 \times 10^{-10} T^3
 \end{aligned}$$

58LUC/DEE

NICKEL; solid; atomic number, 28; atomic wt., 58.69; density, 8.90 g cm⁻³ (555.6 lb ft⁻³).

gross heat of combustion: q_p (gross) is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is nickel oxide, NiO.

$$\begin{aligned}
 q_p(\text{gross}) &= 1757 \text{ Btu lb}^{-1} \\
 q_p(\text{gross}) &= 976 \text{ cal g}^{-1} \\
 q_p(\text{gross}) &= 4084 \text{ J g}^{-1}
 \end{aligned}$$

84WAG/EVA

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
298 77	0.106	0.106	0.444
500 441	0.126	0.126	0.525
630 675	0.158	0.158	0.663
700 801	0.126	0.126	0.525

(more)

NICKEL - Continued

heat of fusion: at the melting point 1452°C (2626°F).

$$L_f = 129.1 \text{ Btu lb}^{-1}$$

$$L_f = 71.7 \text{ cal g}^{-1}$$

$$L_f = 300.1 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point 2886°C (5227°F).

$$L_v = 2761 \text{ Btu lb}^{-1}$$

$$L_v = 1534 \text{ cal g}^{-1}$$

$$L_v = 6418 \text{ J g}^{-1}$$

vapor pressure:

temperature (°C)	(°F)	P(atm)	P(Pa)	P(psi)
1370	2498	10^{-6}	0.1	1.470×10^{-5}
1882	3420	10^{-3}	101.3	1.470×10^{-2}
2131	3869	10^{-2}	1013.3	1.470×10^{-1}
2444	4431	10^{-1}	10132.5	1.470
2886	5227	1.0	101325.	14.696

63HUL/ORR

STEEL, SAE-1010; solid; composition: carbon, 0.08-0.13 wt. %; manganese, 0.30-0.60 wt. %; phosphorus, 0.035 wt. % (maximum); sulfur, 0.045 wt. % (maximum).

specific heat:

-200° to 700°C (-382° to 1292°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.007185 + 9.739 \times 10^{-5} T - 1.016 \times 10^{-7} T^2 + 7.133 \times 10^{-11} T^3$$

$$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1}) = 0.0102 + 1.64 \times 10^{-4} T - 3.07 \times 10^{-7} T^2 + 4.16 \times 10^{-10} T^3$$

$$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1}) = 0.0427 + 6.86 \times 10^{-4} T - 12.8 \times 10^{-7} T^2 + 17.4 \times 10^{-10} T^3$$

curie temperature: 1415°F; 768°C; 1041.5 K

58LUC/DEE

STEEL, NPL NO. 19; solid; composition: carbon, 0.315%; silicon, 0.20%; manganese, 0.69%; sulfur, 0.036%; phosphorus, 0.039%; chromium, 1.09%; nickel, 0.073%; molybdenum, 0.012%; copper, 0.066%; aluminum, 0.005%; arsenic, 0.028%; remainder is iron; annealed at 860°C (1580°F); density, 7.842 g cm⁻³ at 15°C (59°F).

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
323 122	0.1153	0.1153	0.4824
400 261	0.1232	0.1232	0.5155
490 423	0.1277	0.1277	0.5343
589 601	0.1354	0.1354	0.5665
682 768	0.1471	0.1471	0.6155

59MAR/RIX

STEEL, STAINLESS; solid; En-58C (sample 1): chromium, 17.7%; nickel, 10.9%; manganese, 1.73%; En-58B (sample 2): chromium, 17.8%; nickel, 8.05%; manganese, 1.21%.

specific heat:

Sample 1 (En-58C)

60-190 K (-352° to -118°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{°F}^{-1}) &= 0.11077 + 1.1471 \times 10^{-4} T + 3.1191 \times 10^{-7} T^2 + 1.7884 \times 10^{-9} T^3 \\ C_p (\text{cal g}^{-1} \text{K}^{-1}) &= -0.04976 + 1.7309 \times 10^{-3} T - 6.980 \times 10^{-6} T^2 + 1.043 \times 10^{-8} T^3 \\ C_p (\text{J g}^{-1} \text{K}^{-1}) &= -0.20819 + 7.2421 \times 10^{-3} T - 2.9206 \times 10^{-5} T^2 + 4.364 \times 10^{-8} T^3 \end{aligned}$$

190-320 K (-118° to 116°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{°F}^{-1}) &= 0.10922 + 6.6460 \times 10^{-5} T - 1.5492 \times 10^{-7} T^2 + 4.0758 \times 10^{-10} T^3 \\ C_p (\text{cal g}^{-1} \text{K}^{-1}) &= 0.00635 + 8.4104 \times 10^{-4} T - 2.323 \times 10^{-6} T^2 + 2.377 \times 10^{-9} T^3 \\ C_p (\text{J g}^{-1} \text{K}^{-1}) &= 0.02658 + 3.5189 \times 10^{-3} T - 9.721 \times 10^{-6} T^2 + 9.946 \times 10^{-9} T^3 \end{aligned}$$

Sample 2 (En-58B)

60-190 K (-352° to -118°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{°F}^{-1}) &= 0.10911 + 9.3932 \times 10^{-5} T + 1.9847 \times 10^{-7} T^2 + 1.6202 \times 10^{-9} T^3 \\ C_p (\text{cal g}^{-1} \text{K}^{-1}) &= -0.04950 + 1.6893 \times 10^{-3} T - 6.596 \times 10^{-6} T^2 + 9.449 \times 10^{-9} T^3 \\ C_p (\text{J g}^{-1} \text{K}^{-1}) &= -0.20711 + 7.0680 \times 10^{-3} T - 2.7598 \times 10^{-5} T^2 + 3.9535 \times 10^{-8} T^3 \end{aligned}$$

190-320 K (-118° to 116°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{°F}^{-1}) &= 0.10885 + 6.6472 \times 10^{-5} T - 1.4788 \times 10^{-7} T^2 + 5.1989 \times 10^{-10} T^3 \\ C_p (\text{cal g}^{-1} \text{K}^{-1}) &= -0.00345 + 9.5756 \times 10^{-4} T - 2.802 \times 10^{-6} T^2 + 3.032 \times 10^{-9} T^3 \\ C_p (\text{J g}^{-1} \text{K}^{-1}) &= -0.01443 + 4.0064 \times 10^{-3} T - 1.1725 \times 10^{-5} T^2 + 1.2686 \times 10^{-8} T^3 \end{aligned}$$

66MAR

STEEL, STAINLESS 347; solid; nickel, 11.1%; chromium, 18.3%; manganese, 1.30%; silicon, 0.52%; carbon, 0.08%; remainder is iron.

specific heat: 273-1173 K (32°-1652°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.12451 + 1.894 \times 10^{-5} T - 7.2712/(T + 459.67) \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.1158 + 3.41 \times 10^{-5} T - 4.04 T^{-1} \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.4845 + 1.427 \times 10^{-4} T - 16.90 T^{-1} \end{aligned}$$

55DOU/DEV

STEEL, STAINLESS 446; solid; nickel, 0.32%; chromium, 25.58%; manganese, 0.42%; silicon, 0.68%; carbon, 0.23%; remainder is iron.

specific heat:

273-773 K (32°-932°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.10593 + 5.9667 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.0785 + 1.074 \times 10^{-4} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.3284 + 4.494 \times 10^{-4} T \end{aligned}$$

873-1173 K (1112°-1652°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.1618 + 2209 \times 10^{-0.0078(0.5556T - 17.7778)} \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.1618 + 2209 \times 10^{-0.0078(T-273.2)} \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.6770 + 9242 \times 10^{-0.0078(T-273.2)} \end{aligned}$$

55DOU/DEV

Alloys and Metals

TIN; solid; white; tetragonal; atomic number, 50; atomic wt., 118.71; density, 7.28 g cm^{-3} (454.5 lb ft^{-3}).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is tin dioxide, SnO_2 .

$$q_p(\text{gross}) = 2105 \text{ Btu lb}^{-1}$$

$$q_p(\text{gross}) = 1169 \text{ cal g}^{-1}$$

$$q_p(\text{gross}) = 4892 \text{ J g}^{-1}$$

82WAG/EVA

specific heat:

temperature (K) (°F)	$C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
298 77	0.0543	0.0543	0.227
400 261	0.0580	0.0580	0.243
500 441	0.0617	0.0617	0.258

heat of transition: at the transition point, 13°C (55°F) from Sn (grey cubic) to Sn (white tetragonal).

$$L_t = 7.6 \text{ Btu lb}^{-1}$$

$$L_t = 4.2 \text{ cal g}^{-1}$$

$$L_t = 17.6 \text{ J g}^{-1}$$

heat of fusion: at the melting point, 232°C (450°F).

$$L_f = 25.4 \text{ Btu lb}^{-1}$$

$$L_f = 14.1 \text{ cal g}^{-1}$$

$$L_f = 59.0 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point, 2623°C (4753°F).

$$L_v = 1073 \text{ Btu lb}^{-1}$$

$$L_v = 596 \text{ cal g}^{-1}$$

$$L_v = 2495 \text{ J g}^{-1}$$

vapor pressure:

temperature (°C) (°F)	P(atm)	P(Pa)	P(psi)
1115 2039	10^{-6}	0.1	1.470×10^{-5}
1584 2883	10^{-3}	101.3	1.470×10^{-2}
1836 3337	10^{-2}	1013.3	1.470×10^{-1}
2167 3933	10^{-1}	10132.5	1.470
2623 4753	1.0	101325.	14.696

63HUL/ORR

TITANIUM, Ti-75A; solid; composition: titanium, 99.75%; iron, 0.07%; oxygen, 0.131%; nitrogen, 0.048%; carbon, 0.06%; hydrogen, 0.0068%.

specific heat: 294-1033 K (70°-1400°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.1252 - 6.725 \times 10^{-6} T + 4.799 \times 10^{-8} T^2 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.1384 - 9.1526 \times 10^{-5} T + 1.555 \times 10^{-7} T^2 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.5791 - 3.8294 \times 10^{-4} T + 6.506 \times 10^{-7} T^2 \end{aligned}$$

56LOE

TITANIUM, Ti-150A; solid; composition: titanium, 95.65%; chromium, 2.71%; iron, 1.40%; oxygen, 0.105%; nitrogen, 0.076%; carbon, 0.05%; hydrogen, 0.0092%.

specific heat: 294-1033 K (70°-1400°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.1302 - 6.725 \times 10^{-6} T + 4.799 \times 10^{-8} T^2 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.1434 - 9.1526 \times 10^{-5} T + 1.555 \times 10^{-7} T^2 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.6000 - 3.8294 \times 10^{-4} T + 6.506 \times 10^{-7} T^2 \end{aligned}$$

56LOE

WOODS METAL; solid; low melting fusible alloy; composition: tin, 12.5 wt. %; cadmium, 12.5 wt. %; lead, 25 wt. %; bismuth, 50 wt. %.

specific heat: there is a superconducting transition at 4.8 K (-450.7°F).

temperature (K)	(°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
1.5	-456.7	0.0000048	0.0000048	0.00002
2	-455.8	0.000014	0.000014	0.00006
3	-454	0.000057	0.000057	0.00024
4	-452	0.00015	0.00015	0.00062
6	-448.6	0.00069	0.00069	0.0029
10	-441.4	0.0032	0.0032	0.0134
15	-432.4	0.0071	0.0071	0.0297
20	-423.4	0.0110	0.0110	0.0460

54PAR/QUA

Alloys and Metals

ZINC; solid; atomic number 30; atomic wt., 65.39; density 7.14 g cm^{-3} (445.8 lb ft^{-3}).

gross heat of combustion: $q_p(\text{gross})$ is equal to the enthalpy of combustion, $-\Delta H_C^0$ at 25°C (77°F); product of combustion is zinc oxide, ZnO.

$$q_p(\text{gross}) = 2291.4 \text{ Btu lb}^{-1}$$

$$q_p(\text{gross}) = 1273.0 \text{ cal g}^{-1}$$

$$q_p(\text{gross}) = 5326.2 \text{ J g}^{-1}$$

82WAG/EVA

specific heat:

temperature (K) (°F)	$C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
298 77	0.0928	0.0928	0.388
500 441	0.100	0.100	0.419
600 621	0.104	0.104	0.434

heat of fusion: at the melting point, 321°C (610°F).

$$L_f = 48.6 \text{ Btu lb}^{-1}$$

$$L_f = 27.0 \text{ cal g}^{-1}$$

$$L_f = 113.0 \text{ J g}^{-1}$$

heat of vaporization: at the boiling point, 2441°C (4426°F).

$$L_v = 760.4 \text{ Btu lb}^{-1}$$

$$L_v = 422.4 \text{ cal g}^{-1}$$

$$L_v = 1767.4 \text{ J g}^{-1}$$

vapor pressure:

temperature (°C) (°F)	P(atm)	P(Pa)	P(psi)
286 547	10^{-6}	0.1	1.470×10^{-5}
479 894	10^{-3}	101.3	1.470×10^{-2}
581 1078	10^{-2}	1013.3	1.470×10^{-1}
718 1324	10^{-1}	10132.5	1.470
911 1672	1.0	101325.	14.696

63HUL/ORR

ZIRCALOY-2; solid; composition: tin, 1.46%; iron, 0.130%; chromium, 0.080%; nickel, 0.056%; carbon, 65 ppm; oxygen, 1489 ppm; nitrogen, 40 ppm; hydrogen, 11 ppm; copper, 20 ppm; tungsten, < 20 ppm; aluminum, 40 ppm; silicon, 47 ppm; hafnium, < 125 ppm; remainder is zirconium.

specific heat:

273-908 K (32°-1175°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.06763 + 1.3262 \times 10^{-5} T \\ C_p (\text{cal g}^{-1} \text{ K}^{-1}) &= 0.06153 + 2.3872 \times 10^{-5} T \\ C_p (\text{J g}^{-1} \text{ K}^{-1}) &= 0.25744 + 9.9880 \times 10^{-5} T \end{aligned}$$

908-1083 K (1175°-1490°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.08589 \\ C_p (\text{cal g}^{-1} \text{ K}^{-1}) &= 0.08589 \\ C_p (\text{J g}^{-1} \text{ K}^{-1}) &= 0.35936 \end{aligned}$$

1248-1323 K (1787°-1922°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.08548 \\ C_p (\text{cal g}^{-1} \text{ K}^{-1}) &= 0.08548 \\ C_p (\text{J g}^{-1} \text{ K}^{-1}) &= 0.35765 \end{aligned}$$

heat of transition: temperature range: 810°-975°C (1490°-1787°F), for the $\alpha - \beta$ transition

$$\begin{aligned} L_t &= 19.1 \text{ Btu lb}^{-1} \\ L_t &= 10.6 \text{ cal g}^{-1} \\ L_t &= 44.4 \text{ J g}^{-1} \end{aligned}$$

67ELD/DEE

ZIRCALOY-2 (LOW NICKEL); solid; composition: tin, 1.32%; iron, 0.152%; chromium, 0.99%; nickel, 10 ppm; carbon, 150 ppm; oxygen, 1380 ppm; nitrogen, 36 ppm; copper, 20 ppm; tungsten, < 40 ppm; hafnium, 60 ppm; remainder is zirconium.

specific heat:

273-843 K (32°-1058°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.06843 + 1.1514 \times 10^{-5} T \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.06314 + 2.0726 \times 10^{-5} T \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.26418 + 8.6718 \times 10^{-5} T\end{aligned}$$

873-1083 K (1112°-1490°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.08571 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.08571 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.35861\end{aligned}$$

1248-1323 K (1787°-1922°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.08548 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.08548 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.35765\end{aligned}$$

67ELD/DEE

BARNACLE; *Balanus cariosus*; solid; invertebrate animal; crustacean of the order Cirripedia.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 8136 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4520 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18912 \text{ J g}^{-1}$$

71PAI

BEETLE; *Tenebrio molitor*; solid; an insect of the order Coleoptera.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 11365 \pm 929 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6314 \pm 516 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 26418 \pm 2159 \text{ J g}^{-1}$$

61SLO/RIC

BIVALVE; *Mytilus californianus*; solid; Invertebrate animal composed of two parts that open and shut, such as oysters and clams; mollusks.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 8280 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4600 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19246 \text{ J g}^{-1}$$

71PAI

BRACHIOPOD; *Glottidia pyramidata*; solid; A class of Molluscoida having bivalve shells.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$q_v(\text{gross}) = 7915 \pm 3852 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4397 \pm 2140 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18396 \pm 8954 \text{ J g}^{-1}$$

61SLO/RIC

Animals

CATTLE; solid; results apply to total body of cattle.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

For sample of 100% protein:

$$\begin{aligned}q_v(\text{gross}) &= 9805 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5447 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22790 \text{ J g}^{-1}\end{aligned}$$

For sample of 100% fat:

$$\begin{aligned}q_v(\text{gross}) &= 17098 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9499 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 39744 \text{ J g}^{-1}\end{aligned}$$

61STR

CHITON; *Katherina tunicata*; solid; invertebrate animal; mollusk of the order Polyplacophora.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$\begin{aligned}q_v(\text{gross}) &= 8460 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4700 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19665 \text{ J g}^{-1}\end{aligned}$$

71PAI

CILIATE; *Tetrahymena pyriformis*; solid; Class of Protozoa characterized by presence of cilia; found in any exposed body of water.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 10688 \pm 373 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5938 \pm 207 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 24845 \pm 866 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

CLADOCERA; *Leptodora kindtu*; solid; A group of minute, chiefly fresh-water, entomostracan crustaceans, often know as water fleas.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 10091 \pm 1051 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5605 \pm 584 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23451 \pm 2443 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

COPEPOD; *Calanus helgolandicus*; solid; A large subclass of crustaceans mostly minute in size found in both fresh and salt water.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 9720 \pm 355 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5400 \pm 197 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22594 \pm 824 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

COPEPOD; *Trigriopus californicus*; solid; A large subclass of crustaceans mostly minute in size and found in both fresh and salt water.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 9927 \pm 499 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5515 \pm 277 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23075 \pm 1159 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

FLATWORM; *Dugesia tigrina*; solid; a planarian worm of the phylum Platyhelminthes.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$\begin{aligned}q_v(\text{gross}) &= 11315 \pm 608 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6286 \pm 338 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 26301 \pm 1414 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

FLATWORM, TERRESTRIAL; *Bipalium keuense*; solid; Large worm found in the tropics, having the head end expanded into a semicircular plate.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 10231 \pm 223 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5684 \pm 124 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23782 \pm 519 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

Animals

FLY, CADDIS; *Pycnopsyche guttifer*; solid; insects having aquatic larvae, they are included in the Neuroptera, or constitute the order Trichoptera.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$\begin{aligned}q_v(\text{gross}) &= 10271 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5706 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23874 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

GUPPIE; *Lebistes reticulatus*; solid; A small top minnow of the Barbados, Trinidad, and Venezuela area; frequently kept as an aquarium fish.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 10481 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5823 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 24363 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

HYDRA, GREEN; *Chlorohydra viridissima*; solid; Small fresh-water hydrozoan polyps that contain chlorophyll chromatophores, usually found attached to submerged objects; the body is a simple tube with a mouth at one extremity.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 10312 \pm 445 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5729 \pm 247 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23970 \pm 1033 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

MITE; *Tyroglyphus lintneri*; solid; Small arachnids that are parasitic in nature.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 10454 \pm 803 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5808 \pm 446 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 24301 \pm 1866 \text{ J g}^{-1}\end{aligned}$$

61SLO/RIC

POND MURREL, TAIL; *Channa punctatus*; solid; The specimens of this economically important fresh water fish were 18-20 cm (7-8 in.) in length and captured at Aligarh in northern India. Fish were filleted and musculature tissues taken from the posterior (tail) region. Concentrations of the various chemical constituents are protein = $19.739 \pm (0.137)\%$; fat = $1.706 \pm (0.146)\%$; water = $73.433 \pm (0.523)\%$; ash = $1.533 \pm (0.176)\%$; total carbohydrate = $3.587 \pm (0.535)\%$; glycogen = $233.325 \pm (9.362)$ mg/100 g; cholesterol = $156.823 \pm (12.005)$ mg/g; RNA = $23.469 \pm (3.855)$ μ g/100 mg; DNA = $23.469 \pm (1.113)$ μ g/100 mg. Values in parentheses refer to standard error of the mean; each value is a mean of 12 determinations.

gross heat of combustion: assume values refer to room temperature; value is mean of 12 determinations with standard error of the mean.

$$q_v(\text{gross}) = 20071.8 \pm 401.6 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11151.0 \pm 223.1 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46655.8 \pm 933.5 \text{ J g}^{-1}$$

78MUS/JAF

POND MURREL, TRUNK; *Channa punctatus*; solid; The specimens of this economically important fresh water fish were 18-20 cm (7-8 in.) in length and captured at Aligarh in northern India. Fish were filleted and musculature tissues taken from the apex of the anterior (trunk) region. Concentrations of the various chemical constituents are protein = $18.489 \pm (0.406)\%$; fat = $1.040 \pm (0.101)\%$; water = $76.933 \pm (0.314)\%$; ash = $1.200 \pm (0.152)\%$; total carbohydrate = $2.337 \pm (0.898)\%$; glycogen = $160.366 \pm (6.585)$ mg/100 g; cholesterol = $114.000 \pm (19.425)$ mg/100 g; RNA = $100.672 \pm (2.476)$ μ g/100 mg; DNA = $12.213 \pm (2.464)$ μ g/100 mg. Values in parentheses refer to standard error of the mean; each value is a mean of 12 determinations.

gross heat of combustion: assume values refer to room temperature; value is mean of 12 determinations with standard error of the mean.

$$q_v(\text{gross}) = 17110.8 \pm 476.3 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9506.0 \pm 264.6 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39773.1 \pm 1107.1 \text{ J g}^{-1}$$

78MUS/JAF

Animals

SHEEP, BLOOD; solid; protein and fat composition determined on ash-free dry basis for materials from bodies of 63 sheep; mean composition: protein, 98.80%; fat, 1.20%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 10571 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5873 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 24573 \text{ J g}^{-1}$$

For the % fat range 0.00 to 5.80:

$$q_v(\text{gross}) = [10537 + 28.49 (\% \text{ fat})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [5854 + 15.83 (\% \text{ fat})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [24493 + 66.23 (\% \text{ fat})] \text{ J g}^{-1}$$

For the % protein range 94.20 to 100.00:

$$q_v(\text{gross}) = [13383 - 28.49 (\% \text{ protein})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [7435 - 15.83 (\% \text{ protein})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [31108 - 66.23 (\% \text{ protein})] \text{ J g}^{-1}$$

64PAL/REI

SHEEP, CARCASS; solid; protein and fat composition determined on ash-free dry basis for carcasses of 63 sheep; mean composition: protein, 40.18%; fat, 59.82%

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 14000 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7778 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 32543 \text{ J g}^{-1}$$

For the % fat range 33.32 to 81.69:

$$q_v(\text{gross}) = [9589 + 73.75 (\% \text{ fat})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [5327 + 40.97 (\% \text{ fat})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [22288 + 171.42 (\% \text{ fat})] \text{ J g}^{-1}$$

For the % protein range 18.31 to 66.68:

$$q_v(\text{gross}) = [16963 - 73.75 (\% \text{ protein})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [9424 - 40.97 (\% \text{ protein})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [39430 - 171.42 (\% \text{ protein})] \text{ J g}^{-1}$$

64PAL/REI

SHEEP, HIDE; solid; protein and fat composition determined on ash-free dry basis for material from bodies of 63 sheep; mean composition: protein, 74.05%; fat, 25.95%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 11651 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6473 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 27083 \text{ J g}^{-1}$$

For the % fat range 18.37 to 38.72:

$$q_v(\text{gross}) = [9824 + 69.25 (\% \text{ fat})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [5458 + 38.47 (\% \text{ fat})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [22836 + 160.96 (\% \text{ fat})] \text{ J g}^{-1}$$

For the % protein range 61.28 to 81.63:

$$q_v(\text{gross}) = [16749 - 69.25 (\% \text{ protein})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [9305 - 38.47 (\% \text{ protein})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [38932 - 160.96 (\% \text{ protein})] \text{ J g}^{-1}$$

64PAL/REI

SHEEP, INGESTA-FREE BODY; solid; protein and fat composition determined on ash-free dry basis for bodies of 63 sheep; mean composition: protein, 43.33%; fat, 56.67%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 13790 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7661 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 32054 \text{ J g}^{-1}$$

For the % fat range 28.80 to 79.43:

$$q_v(\text{gross}) = [9682 + 72.45 (\% \text{ fat})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [5379 + 40.25 (\% \text{ fat})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [22506 + 168.41 (\% \text{ fat})] \text{ J g}^{-1}$$

For the % protein range 20.57 to 71.20:

$$q_v(\text{gross}) = [16929 - 72.45 (\% \text{ protein})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [9405 - 40.25 (\% \text{ protein})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [39351 - 168.41 (\% \text{ protein})] \text{ J g}^{-1}$$

64PAL/REI

Animals

SHEEP, VISCERA; solid; protein and fat composition determined on ash-free dry basis for viscera from bodies of 63 sheep; mean composition: protein, 33.50%; fat, 66.50%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 14420 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 8011 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 33518 \text{ J g}^{-1}$$

For the % fat range 26.62 to 87.12:

$$q_v(\text{gross}) = [9770 + 69.86 (\% \text{ fat})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [5428 + 38.81 (\% \text{ fat})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [22711 + 162.38 (\% \text{ fat})] \text{ J g}^{-1}$$

For the % protein range 12.88-73.38:

$$q_v(\text{gross}) = [16762 - 69.86 (\% \text{ protein})] \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = [9312 - 38.81 (\% \text{ protein})] \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = [38961 - 162.38 (\% \text{ protein})] \text{ J g}^{-1}$$

64PAL/REI

SHRIMP, BRINE; *Artenia* sp. (*nauplu*); solid; a brachiopod crustacean.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$q_v(\text{gross}) = 12127 \pm 1553 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6737 \pm 863 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 28188 \pm 3611 \text{ J g}^{-1}$$

61SLO/RIC

SNAIL; *Tegula funebris*; solid; invertebrate animal; gastropod mollusk.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 9144 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5080 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 21255 \text{ J g}^{-1}$$

71PAI

SNAIL, AQUATIC; *Succinea ovalis*; solid; (without shell); a gastropod mollusk.

gross heat of combustion: assume values refer to room temperature and are corrected to an ash-free basis.

$$q_v(\text{gross}) = 9747 \pm 11 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5415 \pm 6 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 22656 \pm 25 \text{ J g}^{-1}$$

61SLO/RIC

SPITBUG; *Philenus leucophthalmus*; solid; a spittle insect.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 12532 \pm 918 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6962 \pm 510 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 29129 \pm 2134 \text{ J g}^{-1}$$

61SLO/RIC

STARFISH; *Pisaster ochraceus*; solid; invertebrate animal; echinoderm of the order Asteroidea.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 3798 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 2110 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 8828 \text{ J g}^{-1}$$

71PAI

α -CELLULOSE, FROM LOBLOLLY PINE WOOD; *Pinus taeda*; solid; modification of cellulose which has the highest degree of polymerization; chief constituent of paper pulp: 46.70% α -cellulose [68McM]; repeating unit: $C_6H_{10}O_5$.

specific heat: 333–413 K (140°–284°F); samples were oven-dried at 100°C (212°F) for 12 hours before measurements were made.

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.2357 + 5.5 \times 10^{-4} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= -0.01708 + 9.9 \times 10^{-4} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= -0.07146 + 4.14 \times 10^{-3} T \end{aligned}$$

70McM

CELLULOSE; solid; Extracted wood of northern red oak (*Quercus rubra*) was divided into three major chemical components and cellulose comprised 42.86%. Material has a repeating unit of ($C_6H_{10}O_5$). The relationship between gross heat of combustion and moisture content (MC) is given by the regression equation: $\ln q_v(\text{Btu lb}^{-1}) = 8.9044 - (0.0022)MC(\%)$.

gross heat of combustion: oven dry basis, assume room temperature, and values are reported in international British thermal units per pound, and converted below into thermochemical units.

$$\begin{aligned} q_v(\text{gross}) &= 7325 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4069 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17026 \text{ J g}^{-1} \end{aligned}$$

78MUR/MAS

CELLULOSE; solid; repeating unit: $C_6H_{10}O_5$; constitutes about 60% of the composition of wood; hydrolysis can reduce cellulose to a cellobiose repeating unit, $C_{12}H_{22}O_{11}$, and ultimately to glucose, $C_6H_{12}O_6$.

gross heat of combustion: at 30°C (86°F)

from cotton linters:

$$\begin{aligned} q_v(\text{gross}) &= 7497 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4165.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17426.4 \text{ J g}^{-1} \end{aligned}$$

from wood pulp:

$$\begin{aligned} q_v(\text{gross}) &= 7509.6 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4172.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17455.6 \text{ J g}^{-1} \end{aligned}$$

50JES/PRO

Biomass-Derived Materials

CELLULOSE; solid; Substance is microcrystalline and a calorimeter calibration test substance, very homogeneous, 99.81% pure, and easily pelletized. Trade name Avicel (FMC Corporation); pH = 5.5 to 7; lot 1018-152 is an acid hydrolyzed derivative of a dissolving grade of wood pulp. The % moisture of 7 samples = 4.910 ± 0.060 (sd.); average concentration of water soluble impurities (fluoride, chloride, nitrate, and sulfate) was 62.46 ppm. The formula for Avicel combustion is $C_6H_{10}O_5(c) + 6O_2(g) + 6CO_2(g) + 5H_2O(liq)$, and formula weight = 162.1439 g/mole.

gross heat of combustion: temperature = 28°C (82°F); 9 measurements made; correction for heat of wetting was made; mean value is given with estimated uncertainty.

$$\begin{aligned}q_v(\text{gross}) &= 7460.17 \pm 4.577 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4144.54 \pm 2.543 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17340.76 \pm 10.64 \text{ J g}^{-1}\end{aligned}$$

81COL/XIH

CELLULOSE DIACETATE; solid; repeating unit: $C_{10}H_{10}O_7$; density, 1.36 g cm^{-3} at 20°C (68°F); 0.04% ash.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 8003.2 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4446.2 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18602.9 \text{ J g}^{-1}\end{aligned}$$

57TAV/LAM

CELLULOSE, HOLOCELLULOSE; FROM LOBLOLLY PINE WOOD; *Pinus taeda*; solid; total water-insoluble carbohydrate constituents of loblolly pine wood; 71.18% holocellulose [68McM]; repeating unit: $C_6H_{10}O_5$.

specific heat: 333-413 K (140°-284°F); samples were oven-dried at 100°C (212°F) for 12 hours before measurements were made.

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.23558 + 5.5 \times 10^{-4} T \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= -0.01724 + 9.9 \times 10^{-4} T \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= -0.07213 + 4.14 \times 10^{-3} T\end{aligned}$$

70McM

CELLULOSE TRIACETATE; solid; repeating unit: $C_{12}H_{16}O_8$.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 8120.7 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4511.5 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18876.1 \text{ J g}^{-1}\end{aligned}$$

57TAV/LAM

CHARCOAL, WOOD; solid; ultimate analysis: carbon, 93.0%; hydrogen, 2.5%; nitrogen and sulfur, 1.5%; moisture, 2%; proximate analysis: fixed carbon, 89%; ash, 1%; volatile matter, 10%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

as received; "good commercial fuel"

$$\begin{aligned} q_v(\text{gross}) &= 14940 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 8300 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 34727 \text{ J g}^{-1} \end{aligned}$$

$$\begin{aligned} q_v(\text{gross}) &= 14490 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 8050 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 33681 \text{ J g}^{-1} \end{aligned}$$

55SPI

COTTON (THREAD); solid; staple fibers surrounding the seeds of various species of *Gossypium*; absorbent cotton is almost pure α -cellulose; $\text{CH}_{1.774}\text{O}_{0.887}$ is elemental analysis of thread used in combustion measurements.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 7290 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4050 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 16945 \text{ J g}^{-1} \end{aligned}$$

$$\begin{aligned} q_v(\text{gross}) &= 7394 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4108 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17188 \text{ J g}^{-1} \end{aligned}$$

62GOO/SCO; 70MAN/RAP

DEXTRIN; solid; general formula: $\text{C}_6\text{H}_{10}\text{O}_5$; partial hydrolysis product of starch containing a variable number of glucose units; dextrin is obtained in several different grades by heating starch for varying lengths of time over the temperature range from 170°-240°C (338°-464°F).

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 7398 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4110 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17196 \text{ J g}^{-1} \end{aligned}$$

55MER/WAT

FILTER PAPER, WHATMAN; solid; Material is No. 41. W. and R. Balston, has fast filter speed, and will retain coarse and gelatinous precipitates. Paper is ashless and consists of almost pure cellulose.

specific heat: mean value in temperature range 25°-75°C (77°-167°F) for four measurements.

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.217 \pm 0.003 \\ C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1}) &= 0.217 \pm 0.003 \\ C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1}) &= 0.908 \pm 0.013 \end{aligned}$$

52NEU

Biomass-Derived Materials

GLYCOGEN; solid; general formula: $C_6H_{10}O_5$; polysaccharide found in the liver and muscles of man and animals; can be hydrolyzed to glucose.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 7538 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4188 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17523 \text{ J g}^{-1}\end{aligned}$$

24MEI/MEY

HEMICELLULOSE; solid; Extracted wood of northern red oak (*Quercus rubra*) was divided into three major chemical components of which hemicellulose comprised 33.33%. The relationship between gross heat of combustion and moisture content (MC) is given by the regression equation: $\ln q_v(\text{Btu lb}^{-1}) = 8.8545 - (0.0103)MC(\%)$.

gross heat of combustion: oven dry basis, assume values refer to room temperature; values are reported in international British thermal units per pound and converted below into thermochemical units.

$$\begin{aligned}q_v(\text{gross}) &= 7170 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3983 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16666 \text{ J g}^{-1}\end{aligned}$$

78MUR/MAS

INULIN; solid; repeating unit: $C_6H_{10}O_5$; similar in physical appearance to starch except upon complete hydrolysis yields fructose instead of glucose; inulin is the chief source of fructose.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 7542 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4190 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17531 \text{ J g}^{-1}\end{aligned}$$

1887BER/VIE

INULIN TRIACETATE; solid; repeating unit: $C_{12}H_{16}O_8$; dried at 120°C (248°F) in vacuum over P_2O_5 .

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 8140 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4522 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18920 \text{ J g}^{-1}\end{aligned}$$

22KAR/FIO

LIGNIN; solid; Extracted wood of northern red oak (*Quercus rubra*) was divided into three major chemical components of which lignin comprised 23.81%. Material is the major noncarbohydrate constituent of wood; it is a highly polymeric substance, with a complex, cross linked, highly aromatic structure of molecular weight about 10,000 derived principally from coniferyl alcohol ($C_{10}H_{12}O_3$) by extensive condensation-polymerization. The relationship between gross heat of combustion and moisture content (MC) is given by the regression equation: $\ln q_v(\text{Btu lb}^{-1}) = 9.0733 - (0.0030)MC(\%)$.

gross heat of combustion: oven dry basis, assume values refer to room temperature; values are reported in international British thermal units per pound and converted below into thermochemical units.

$$\begin{aligned} q_v(\text{gross}) &= 9111 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5062 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21178 \text{ J g}^{-1} \end{aligned}$$

78MUR/MAS

LIGNIN, HARDWOOD; solid; composition: carbon, 60%; hydrogen, 6%; oxygen, 34%; empirical formula: $C_{10}H_{12}O_{4.2}$. No general agreement prevails about the structure of lignin. Studies show that a dioxyphenylpropyl grouping is an important part of the polymer.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 10620 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5900 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 24685 \text{ J g}^{-1} \end{aligned}$$

67RYD; 68GUL

LIGNIN, LOBLOLLY PINE WOOD; *Pinus taeda*; solid; major (29.4% lignin) [68McM] noncarbohydrate constituent of wood; functions as a natural plastic binder for cellulose fibers.

specific heat: 333-413 K (140°-284°F); samples were oven-dried at 100°C (212°F) for 12 hours before measurements were made.

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.2579 + 4.28 \times 10^{-4} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.06133 + 7.7 \times 10^{-4} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.25660 + 3.22 \times 10^{-3} T \end{aligned}$$

70McM

Biomass-Derived Materials

LIGNIN, SOFTWOOD; solid; composition: carbon, 64%; hydrogen, 6%; oxygen, 30%; empirical formula: $C_{10}H_{11.2}O_{3.3}$; no general agreement prevails about the structure of lignin. Studies show that a dioxyphenylpropyl grouping is an important part of the polymer.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 11340 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6300 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 26360 \text{ J g}^{-1}$$

67RYD; 68GUL

MANURE, PIG; solid; faeces from hogs; oven dried; 0% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 7704 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4280 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 17900 \text{ J g}^{-1}$$

73BAC/HAR

STARCH; solid; general formula: $C_6H_{10}O_5$; polysaccharide is widely distributed in the vegetable kingdom and is stored in all grains and tubers.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 7560 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4200 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 17570 \text{ J g}^{-1}$$

55MER/WAT

STARCH TRIACETATE; solid; repeating unit: $C_{12}H_{16}O_8$.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 8098 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4499 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18824 \text{ J g}^{-1}$$

22KAR/FIO

SULFITE LIQUOR, SPENT; aqueous; calcium and magnesium base waste liquor from pulping of wood by sulfite process; gaseous sulfur dioxide, 2%-4%; aqueous sulfite, 2%-7%; aqueous sulfate, 2%-5%; solids, 80%-90%; also lignin sulfonate, calcium and magnesium compounds, and carbohydrates.

gross heat of combustion: assume value refers to room temperature.

55% solids non-neutralized spent liquor

fermented and stripped liquor

$$\begin{aligned} q_v(\text{gross}) &= 8100 - 8370 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4500 - 4650 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18800 - 19500 \text{ J g}^{-1} \end{aligned}$$

$$\begin{aligned} q_v(\text{gross}) &= 8460 - 8775 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4700 - 4875 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19700 - 20400 \text{ J g}^{-1} \end{aligned}$$

69HUL

TANNIN EXTRACT, CHESTNUT; solid; dry powder obtained from concentrated solution produced from treatment of chestnut chips with water.

specific heat: 298 K (77°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.2889 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.2889 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.2088 \end{aligned}$$

55KAN

TANNIN EXTRACT, QUEBRACHO; solid; dry extract from a wood-derived tannin; tannin obtained from *Aspidosperma quebracho* and *Quebracho lorentzi* imported as logs from Argentina.

specific heat: 298 K (77°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.3152 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.3152 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.3188 \end{aligned}$$

55KAN

XYLAN; solid; repeating unit: $\text{C}_5\text{H}_8\text{O}_4$; polysaccharide which often occurs in association with cellulose; xylose is the repeating unit; occurs in large amounts (20%-40%) in cereal straws and brans.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 7637.0 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4242.8 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17751.9 \text{ J g}^{-1} \end{aligned}$$

23KAR/FIO

ALMONDS; *Prunus amygdalus*; solid; 4.4% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 5632 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3129 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 13092 \text{ J g}^{-1}$$

55MER/WAT

BEANS, GREEN; solid; chemical analysis: 87.8% water, 0.26% fat, and 4.98% water soluble solids.

specific heat: 4° to -40°C (40° to -40°F); the initial freezing point = -0.9°C (30.3°F).

temperature		$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1})$	$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1})$
(°C)	(°F)			
4.44	40	0.92	0.92	3.85
-0.94	30.3	0.92	0.92	3.85
-6.67	20	1.43	1.43	5.98
-12.2	10	0.82	0.82	3.43
-17.0	0	0.68	0.68	2.85
-23.3	-10	0.60	0.60	2.51
-28.9	-20	0.56	0.56	2.34
-34.4	-30	0.50	0.50	2.09
-40	-40	0.45	0.45	1.88

49STA

BEANS, NAVY, WHITE, DRY; *Phaseolus vulgaris*; solid; 11.2% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 7020 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3900 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16320 \text{ J g}^{-1}$$

55MER/WAT

BUTTERFAT, SUMMER; solid; Three samples were measured from different sources.

The oily portion of cow's milk composed of 88% of the glycerides of oleic, stearic, and palmitic acids and 6% of the glycerides of butyric, caproic, caprylic, and capric acids.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	Btu lb $^{-1}$	$H^{\circ}(\text{t})-H^{\circ}(-50^{\circ}\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	17.06	9.48	39.66
0	32	43.72	24.29	101.63
25	77	89.62	49.79	208.32
50	122	117.79	65.44	273.80
55	131	122.17	67.87	283.97

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 44.1 \text{ Btu lb}^{-1}$$

$$L_f = 24.5 \text{ cal g}^{-1}$$

$$L_f = 102.5 \text{ J g}^{-1}$$

55RIE

BUTTERFAT, WINTER; solid; the oily portion of cow's milk composed of 88% of the glycerides of oleic, stearic, and palmitic acids and 6% of the glycerides of butyric, caproic, caprylic, and capric acids. Three samples were measured from different sources.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	Btu lb $^{-1}$	$H^{\circ}(\text{t})-H^{\circ}(-50^{\circ}\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	16.24	9.02	37.74
0	32	41.85	23.25	97.28
25	77	89.50	49.72	208.03
50	122	119.93	66.63	278.78
55	131	124.24	69.02	288.78

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 47.3 \text{ Btu lb}^{-1}$$

$$L_f = 26.3 \text{ cal g}^{-1}$$

$$L_f = 110.0 \text{ J g}^{-1}$$

55RIE

Foods

CABBAGE; *Brassica oleracea* var. *capitata*; solid; 94.6% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 378 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 210 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 880 \text{ J g}^{-1}$$

55MER/WAT

CARROTS; solid; chemical analysis: 83.1% water, 0.18% fat, and 8.71% water soluble solids. Sample was unpeeled and cubed.

specific heat: 4° to -40°C (40° to -40°F); the initial freezing point = -2.3°C (27.8°F).

temperature (°C)	(°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ °C ⁻¹)	C_p (J g ⁻¹ °C ⁻¹)
4.44	40	0.94	0.94	3.93
-2.33	27.8	0.94	0.94	3.93
-6.67	20	2.11	2.11	8.83
-12.2	10	0.98	0.98	4.10
-17.0	0	0.73	0.73	3.05
-23.3	-10	0.58	0.58	2.43
-28.9	-20	0.48	0.48	2.01
-34.4	-30	0.40	0.40	1.67
-40	-40	0.34	0.34	1.42

49STA

CAULIFLOWER; solid; chemical analysis: 92.0% water, 0.14% fat, and 3.64% water soluble solids. Sample contained no leafy material.

specific heat: 4° to -40°C (40° to -40°F); the initial freezing point = -1.1°C (30.0°F).

temperature (°C)	(°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ °C ⁻¹)	C_p (J g ⁻¹ °C ⁻¹)
4.44	40	0.73	0.73	3.05
-1.11	30.0	0.73	0.73	3.05
-6.67	20	1.75	1.75	7.32
-12.2	10	0.82	0.82	3.43
-17.0	0	0.66	0.66	2.76
-23.3	-10	0.58	0.58	2.42
-28.9	-20	0.52	0.52	2.18
-34.4	-30	0.48	0.48	2.01
-40	-40	0.45	0.45	1.88

49STA

CITRUS FRUIT, RINDS AND SEEDS; solid; ultimate analysis: carbon, 44.11%; hydrogen, 5.22%; oxygen, 38.34%; nitrogen, 1.02%; sulfur, 0.11%; ash, 3.18%; moisture, 8.02%; proximate analysis as received: moisture, 8.02%; volatile matter, 71.46%; fixed carbon, 17.34%; ash, 3.18%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 1708 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 949 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 3970 \text{ J g}^{-1}\end{aligned}$$

air dried

$$\begin{aligned}q_v(\text{gross}) &= 7376 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4098 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17146 \text{ J g}^{-1}\end{aligned}$$

66KAI; 68KAI/FRI

COCOA BUTTER; solid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 194. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 38.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature		$H^\circ(t) - H^\circ(-50^\circ\text{C})$		
($^\circ\text{C}$)	($^\circ\text{F}$)	Btu lb $^{-1}$	cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	14.67	8.15	34.10
0	32	33.10	18.39	76.94
25	77	63.76	35.42	148.20
50	122	131.85	73.25	306.47
55	131	136.22	75.68	316.65

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$\begin{aligned}L_f &= 63.0 \text{ Btu lb}^{-1} \\L_f &= 36.0 \text{ cal g}^{-1} \\L_f &= 146.4 \text{ J g}^{-1}\end{aligned}$$

55RIE

COCONUT; *Cocos nucifera*; solid; meat; 19.2% moisture.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 4882 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 2712 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 11347 \text{ J g}^{-1}\end{aligned}$$

55MER/WAT

Foods

CORN (MAIZE), GREEN; *Zea mays*; solid; 76.0% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 2002 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 1112 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 4653 \text{ J g}^{-1}$$

55MER/WAT

COWPEAS; *Vigna sinensis*; solid; 10.0% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 7200 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4000 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16736 \text{ J g}^{-1}$$

55MER/WAT

CUCUMBERS; solid; chemical analysis: 96.1% water, 0.07% fat, and 1.63% water soluble solids. Sample was unpeeled and cubed.

specific heat: 4° to -40°C (40° to -40°F); the initial freezing point = -0.6°C (31.0°F).

temperature (°C)	(°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1})$	$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1})$
4.44	40	0.92	0.92	3.85
- 0.56	31.0	0.92	0.92	3.85
- 6.67	20	1.32	1.32	5.52
-12.2	10	0.70	0.70	2.93
-17.0	0	0.58	0.58	2.43
-23.3	-10	0.53	0.53	2.22
-28.9	-20	0.49	0.49	2.05
-34.4	-30	0.48	0.48	2.01
-40	-40	0.45	0.45	1.88

49STA

EGG ALBUMIN; solid; a crystallizable protein; molecular weight about 33,800; from egg white.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 10280 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5710 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 23891 \text{ J g}^{-1}$$

specific heat: temperature range: 273-298 K (32°-77°F); anhydrous.

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.267$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.267$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 1.117$$

55MER/WAT; 72BER/KLI

EGG YOLK; solid; yellow, semi-solid material of an egg; specific gravity, 0.95; high cholesterol content.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 10510 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5840 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 24435 \text{ J g}^{-1}$$

55MER/WAT

FAT, ANIMAL; solid; mixture of glycerides of fatty acids.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17100 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9500 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39750 \text{ J g}^{-1}$$

55MER/WAT

FAT, BARLEY; solid; ether extracted.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16330 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9070 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 37950 \text{ J g}^{-1}$$

55MER/WAT

Foods

FAT, BEEF; solid.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17100 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9500 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39750 \text{ J g}^{-1}$$

fat obtained by ether extraction

$$q_v(\text{gross}) = 16630 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9240 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 38660 \text{ J g}^{-1}$$

55MER/WAT

FAT, BUTTER; solid; processed from cream of cow's milk; composed mainly of glycerides (90%) of oleic, palmitic, and stearic acids; remainder (10%) is made up of glycerides of butyric, capric, caprylic, and caproic acids. Saponification number 210-230.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16690 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9270 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 38785 \text{ J g}^{-1}$$

55MER/WAT

FAT, FRIED; solid; ultimate analysis: carbon, 73.14%; hydrogen, 11.54%; oxygen, 14.28%; nitrogen, 0.43%; sulfur, 0.07%; ash, 0.00%; proximate analysis as received: moisture, 0.00%; volatile matter, 97.64%; fixed carbon, 2.36%; ash, 0.00%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16480 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9154 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 38300 \text{ J g}^{-1}$$

66KAI

FAT, LARD; liquid; Material was extracted from animal fats to form a commercial lard and the acid value was 0.33 mg KOH/g. Specific gravity (15/15°C) = 0.9145. Fatty acids found in the oil: capric, 0.18%; lauric, 0.11%; myristic, 1.52%; palmitic, 23.73%; palmitoleic, 3.35%; stearic, 15.16%; oleic, 45.42%; linoleic, 8.81%; linolenic, 0.51%; and eicosenoic, 0.74%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17136 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9520 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39832 \text{ J g}^{-1}$$

75KOM/DAN

FAT, LARD; solid; purified internal fat of the hog; fatty acid composition (typical): myristic, 1.1%; palmitic, 30.4%; stearic, 17.9%; oleic, 41.2%; linoleic, 5.7%. Iodine number 46-66.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17260 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9590 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 40120 \text{ J g}^{-1}$$

FAT, MUTTON; solid.

55MER/WAT

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17120 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9510 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39790 \text{ J g}^{-1}$$

fat obtained by ether extraction

$$q_v(\text{gross}) = 16780 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9320 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39000 \text{ J g}^{-1}$$

55MER/WAT

FAT, OAT; *Avena sativa*; solid; ether extract.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16330 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9070 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 37950 \text{ J g}^{-1}$$

55MER/WAT

FAT, PORK; solid.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17100 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9500 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39750 \text{ J g}^{-1}$$

fat obtained by ether extraction

$$q_v(\text{gross}) = 16430 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9130 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 38200 \text{ J g}^{-1}$$

55MER/WAT

Foods

FAT, RYE; *Secale cereale*; solid; ether extract.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16240 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9020 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 37740 \text{ J g}^{-1}$$

55MER/WAT

FAT, WHEAT; *Triticum aestivum*; solid; ether extract.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16330 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9070 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 37950 \text{ J g}^{-1}$$

55MER/WAT

FLOUR, SOY BEAN; *Soia hispida*.

gross heat of combustion: assume values refer to room temperature.

4.17% moisture, 6.5% fat

6.5% moisture, 3.3% fat

$$q_v(\text{gross}) = 6689 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3716 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 15548 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 6264 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3480 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 14560 \text{ J g}^{-1}$$

55MER/WAT

FLOUR, WHEAT; solid; the finely ground and bolted meal of wheat, *Triticum aestivum*;
density, 0.73 g cm^{-3} .

net heat of explosion: nonisothermal in air; temperature $\sim 250^\circ\text{C}$ (482°F).

$$q_p(\text{net}) = 333 \text{ Btu lb}^{-1}$$

$$q_p(\text{net}) = 185 \text{ cal g}^{-1}$$

$$q_p(\text{net}) = 774 \text{ J g}^{-1}$$

specific heat: $100^\circ\text{--}250^\circ\text{C}$ ($212^\circ\text{--}482^\circ\text{F}$)

$$C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) = 0.5$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.5$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 2.1$$

gross heat of combustion: assume values refer to room temperature.

graham, whole grain; 10.5% moisture

semolina; 7.57% moisture

$$q_v(\text{gross}) = 7207 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4004 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16750 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 7488 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4160 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 17405 \text{ J g}^{-1}$$

standard patent; 10.3% moisture

$$q_v(\text{gross}) = 7218 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4010 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16780 \text{ J g}^{-1}$$

55MER/WAT; 69ABR/ABR

FOOD WASTES, VEGETABLE; solid; ultimate analysis: carbon, 49.06%; hydrogen, 6.62%; oxygen, 37.55%; nitrogen, 1.68%; sulfur, 0.20%; ash, 4.8%; proximate analysis as received: moisture, 78.29%; volatile matter, 17.10%; fixed carbon, 3.55%; ash, 1.06%.

gross heat of combustion: assume values refer to room temperature.

as received

dry basis

$$q_v(\text{gross}) = 1796 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 998 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 4175 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 8276 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4598 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19236 \text{ J g}^{-1}$$

66KAI

Foods

GELATIN; solid; an albumin type protein belonging to the scleroprotein class with the questionable formula $C_{76}H_{124}O_{29}N_{24}S$. It occurs in bones and fibrous animal tissue in the form of its anhydride collagen, which is converted into gelatin upon boiling with dilute acids. It is particularly rich in glycine and lysine.

heat of solution: the value is for the material at 25°C (77°F) dissolved in the acid mixture at 75°C (167°F); the result is the average of 5 determinations. The acid mixture contained 5% by weight of HF and 19.95% by weight HCl.

$$\Delta_{\text{sol}}H = 19.13 \pm 0.58 \text{ Btu lb}^{-1}$$

$$\Delta_{\text{sol}}H = 10.63 \pm 0.32 \text{ cal g}^{-1}$$

$$\Delta_{\text{sol}}H = 44.48 \pm 1.34 \text{ J g}^{-1}$$

52NEU

GRAPES, THOMPSON SEEDLESS; solid; chemical analysis: 81.4% water, 0.26% fat, and 15.6% water soluble solids. Sample was whole with short stem.

specific heat: 4° to -40°C (40° to -40°F); no freezing point was observed.

temperature		$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1})$	$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1})$
(°C)	(°F)			
4.44	40	0.89	0.89	3.72
-6.67	20	3.84	3.84	16.07
-12.2	10	1.49	1.49	6.23
-17.0	0	0.95	0.95	3.98
-23.3	-10	0.75	0.75	3.14
-28.9	-20	0.62	0.62	2.59
-34.4	-30	0.56	0.56	2.34
-40	-40	0.52	0.52	2.18

49STA

GROATS, SUN IX; solid; Grain has fat content of 8.1%. The relationship between the grain and the moisture content was determined. One third of the samples were not conditioned, one third were conditioned by adding distilled water and equilibrating for one week, and the rest were dried in a vacuum over CaCl_2 until they reached their respective moisture contents. Moisture content was determined by drying triplicate ground samples in a ventilated oven at 113°C (235°F) for 4 hours.

specific heat: straight line regression equations for the relation between the specific heat and moisture content where C_p is apparent specific heat and M is moisture content (%). The apparent specific heat of water [$C_p(w)$] was calculated from the equation.

$$C_p = 0.0119 M + 0.257 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p = 0.0119 M + 0.257 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.0498 M + 1.075 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 1.447 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p(w) = 1.447 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 6.054 \text{ J g}^{-1} \text{ K}^{-1}$$

54HAS

HERRING OIL; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 193. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 120.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^\circ\text{C}$)	($^\circ\text{F}$)	Btu lb^{-1}	$\text{H}^\circ(\text{t}) - \text{H}^\circ(-50^\circ\text{C})$ cal g^{-1}	J g^{-1}
-50	-58	0.00	0.00	0.00
-25	-13	21.38	11.88	49.71
0	32	51.14	28.41	118.87
25	77	79.81	44.34	185.52
50	122	100.98	56.10	234.72
55	131	105.25	58.47	244.64

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 22.1 \text{ Btu lb}^{-1}$$

$$L_f = 12.3 \text{ cal g}^{-1}$$

$$L_f = 51.5 \text{ J g}^{-1}$$

55RIE

Foods

HOMINY; from corn (maize); *Zea mays*; 10.96% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 7175 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3986 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16677 \text{ J g}^{-1}$$

55MER/WAT

HONEYDEW MELON; solid; chemical analysis: 92.6% water, 0.21% fat, and 2.83% water soluble solids. Sample was cubed, seeds included, no rind.

specific heat: 4° to -40°C (40° to -40°F); the initial freezing point = -0.8°C (30.5°F).

temperature (°C)	temperature (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ °C ⁻¹)	C_p (J g ⁻¹ °C ⁻¹)
4.44	40	0.92	0.92	3.85
-0.83	30.5	0.92	0.92	3.85
-6.67	20	1.85	1.85	7.74
-12.2	10	0.94	0.94	3.93
-17.0	0	0.68	0.68	2.85
-23.3	-10	0.58	0.58	2.43
-28.9	-20	0.53	0.53	2.22
-34.4	-30	0.50	0.50	2.09
-40	-40	0.48	0.48	2.01

49STA

LARD, AMERICAN COMMERCIAL; solid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 202. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 66.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature (°C)	temperature (°F)	Btu lb ⁻¹	$H^\circ(t) - H^\circ(-50^\circ\text{C})$ cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	16.67	9.26	38.74
0	32	48.98	27.21	113.85
25	77	88.54	49.19	205.81
50	122	120.33	66.85	279.70
55	131	124.70	69.28	289.87

heat of fusion: results is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 47.7 \text{ Btu lb}^{-1}$$

$$L_f = 26.5 \text{ cal g}^{-1}$$

$$L_f = 110.9 \text{ J g}^{-1}$$

55RIE

LARD, GERMAN COMMERCIAL; solid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 202. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 49.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature		Btu lb ⁻¹	H°(t)-H°(-50°C)	
(°C)	(°F)		cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	15.73	8.74	36.57
0	32	41.40	23.00	96.23
25	77	78.12	43.40	181.59
50	122	122.90	68.28	285.68
55	131	127.51	70.84	296.39

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 52.6 \text{ Btu lb}^{-1}$$

$$L_f = 29.2 \text{ cal g}^{-1}$$

$$L_f = 122.2 \text{ J g}^{-1}$$

55RIE

MALTING BARLEY; solid; Grain was heavily husked; sample (A) was as harvested from field (germination was 100%), sample (B) was wetted by addition of water or water vapor, and sample (C) was dried in a vacuum at 30°C (86°F).

specific heat: temperature range 273-291 K (32° - 64°F), data are mean values with standard error in parentheses and moisture content (M) on a wet weight basis.

Sample	M	$C_{P,1}$	$C_{P,1}$	$C_{P,1}$
	%	(Btu lb ⁻¹ °F ⁻¹)	(cal g ⁻¹ K ⁻¹)	(J g ⁻¹ K ⁻¹)
A	13.8	0.387(0.0026)	0.387(0.0026)	1.619(0.0109)
B	16.5	0.436(0.0026)	0.436(0.0026)	1.824(0.0109)
C	9.4	0.359(0.0016)	0.359(0.0016)	1.502(0.0067)

54DIS

MARGARINE, TABLE; solid; a butter substitute, an emulsion of fats in milk serum, (the oleo margarine is the liquid fat from which margarine is made by hydrogenation). Two samples were used from different sources.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	Btu lb $^{-1}$	$\text{H}^{\circ}(\text{t})-\text{H}^{\circ}(-50^{\circ}\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	16.70	9.28	38.83
0	32	43.20	24.00	100.42
25	77	83.95	46.64	195.14
50	122	119.05	66.14	276.73
55	131	123.46	68.59	286.98

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 46.4 \text{ Btu lb}^{-1}$$

$$L_f = 25.8 \text{ cal g}^{-1}$$

$$L_f = 107.9 \text{ J g}^{-1}$$

55RIE

MARGARINE, COMMERCIAL; solid; a butter substitute which is an emulsion of fats in milk serum, (the oleomargarine is the liquid fat from which margarine is made by hydrogenation). Three samples were used from different sources.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	Btu lb $^{-1}$	$\text{H}^{\circ}(\text{t})-\text{H}^{\circ}(-50^{\circ}\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	16.16	8.98	37.57
0	32	45.04	25.02	104.68
25	77	91.08	50.60	211.71
50	122	121.43	67.46	282.25
55	131	125.86	69.92	292.55

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 47.5 \text{ Btu lb}^{-1}$$

$$L_f = 26.4 \text{ cal g}^{-1}$$

$$L_f = 110.5 \text{ J g}^{-1}$$

55RIE

MEAL, CORN (MAIZE); *Zea mays*; 11.79% moisture.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 6881 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3823 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 15995 \text{ J g}^{-1} \end{aligned}$$

55MER/WAT

MEAT, COOKED SCRAPS; solid; ultimate analysis: carbon, 59.59%; hydrogen, 9.47%; oxygen, 24.65%; nitrogen, 1.02%; sulfur, 0.19%; ash, 5.08%; proximate analysis as received: moisture, 38.74%; volatile matter, 56.34%; fixed carbon, 1.81%; ash, 3.11%.

gross heat of combustion: assume values refer to room temperature.

as received

dry basis

$$\begin{aligned} q_v(\text{gross}) &= 7628 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4238 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17731 \text{ J g}^{-1} \end{aligned}$$

$$\begin{aligned} q_v(\text{gross}) &= 12450 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 6917 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 28942 \text{ J g}^{-1} \end{aligned}$$

66KAI

OATS; *Avena sativa*; solid; rolled; 8.66% moisture.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 8208 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4560 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19080 \text{ J g}^{-1} \end{aligned}$$

55MER/WAT

OATS, SUN II; solid; Grain has fat content of 4.5%. The relationship between the grain and the moisture content was determined. One third of the samples were not conditioned, one third were conditioned by adding distilled water and equilibrating for one week, and the rest were dried in a vacuum over CaCl_2 until they reached their respective moisture contents. Moisture content was determined by drying triplicate ground samples in a ventilated oven at 113°C (235°F) for 4 hours.

specific heat: straight line regression equations for the relation between the specific heat and moisture content where C_p is apparent specific heat and M is moisture content (%). The apparent specific heat of water [$C_p(w)$] was calculated from the equation for $M = 100\%$.

$$C_p = 0.0078 M + 0.305 \text{ Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}$$

$$C_p = 0.0078 M + 0.305 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.0326 M + 1.276 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 1.085 \text{ Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}$$

$$C_p(w) = 1.085 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 4.540 \text{ J g}^{-1} \text{ K}^{-1}$$

54HAS

PEANUT BUTTER, HARDENED; solid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 189. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 78. Material is called Biskin.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^\circ\text{C}$)	($^\circ\text{F}$)	Btu lb^{-1}	$\text{H}^\circ(\text{t}) - \text{H}^\circ(-50^\circ\text{C})$ cal g^{-1}	J g^{-1}
-50	-58	0.00	0.00	0.00
-25	-13	16.20	9.00	37.66
0	32	42.19	23.44	98.07
25	77	83.20	46.22	193.38
50	122	116.15	64.53	269.99
55	131	120.42	66.90	279.91

heat of fusion: results is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 45.4 \text{ Btu lb}^{-1}$$

$$L_f = 25.2 \text{ cal g}^{-1}$$

$$L_f = 105.4 \text{ J g}^{-1}$$

55RIE

PEANUTS; *Arachis hypogaea*; solid; 4.88% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 5472 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3040 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 12720 \text{ J g}^{-1}$$

55MER/WAT

PEARS, BARTLETT; solid; chemical analysis: 79.4% water, 0.51% fat, and 12.1% water soluble solids. Sample was unpeeled, cored, and cubed.

specific heat: 4° to -40°C (40° to -40°F); no freezing point was recorded.

temperature (°C)	(°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1})$	$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1})$
4.44	40	0.98	0.98	4.10
-6.67	20	3.24	3.24	13.56
-12.2	10	1.20	1.20	5.02
-17.0	0	0.83	0.83	3.47
-23.3	-10	0.63	0.63	2.64
-28.9	-20	0.51	0.51	2.13
-34.4	-30	0.46	0.46	1.93
-40	-40	0.44	0.44	1.84

49STA

PECANS; *Carya illinoensis*; solid; 4.30% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 6392 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3551 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 14857 \text{ J g}^{-1}$$

55MER/WAT

Foods

POTATO, WHITE; solid; proximate analysis: moisture, 79.5%; carbohydrates, 16.7%; protein, 2%; fiber, 0.4%; ash, 0.8%; fat, 0.1%.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 1526 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 848 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 3548 \text{ J g}^{-1} \end{aligned}$$

specific heat: at 303 K (86°F), with a moisture content (W) range of 0.23 to 0.83 wt. fraction.

(W > 0.50)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.216 + 0.780 W \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.216 + 0.780 W \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.904 + 3.264 W \end{aligned}$$

(0.50 > W > 0.20)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.393 + 0.437 W \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.393 + 0.437 W \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.644 + 1.828 W \end{aligned}$$

55MER/WAT; 70YAM

RICE; *Oryza sativa*; solid; white; polished; 12.9% moisture.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 6937 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3854 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 16125 \text{ J g}^{-1} \end{aligned}$$

55MER/WAT

RICE, FULLY FINISHED (ITALIAN ORIGIN); solid; Grain has fat content of 0.4%–2.0%.

The relationship between the grain and the moisture content was determined. One third of the samples were not conditioned, one third were conditioned by adding distilled water and equilibrating for one week, and the rest were dried in a vacuum over CaCl₂ until they reached their respective moisture contents. Moisture content was determined by drying triplicate ground samples in a ventilated oven at 113°C (235°F) for 4 hours.

specific heat: straight line regression equations for the relation between the specific heat and moisture content where C_p is apparent specific heat and M is moisture content (%). The apparent specific heat of water [$C_p(w)$] was calculated from the equation for M = 100%.

$$\begin{aligned} C_p &= 0.009 M + 0.282 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1} \\ C_p &= 0.009 M + 0.282 \text{ cal g}^{-1} \text{ K}^{-1} \\ C_p &= 0.038 M + 1.180 \text{ J g}^{-1} \text{ K}^{-1} \end{aligned}$$

$$\begin{aligned} C_p(w) &= 1.182 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1} \\ C_p(w) &= 1.182 \text{ cal g}^{-1} \text{ K}^{-1} \\ C_p(w) &= 4.946 \text{ J g}^{-1} \text{ K}^{-1} \end{aligned}$$

54HAS

RICE, ROUGH (ITALIAN ORIGIN); solid; Grain has fat content of 0.4%–2.0%. The relationship between the grain and the moisture content was determined. One third of the samples were not conditioned, one third were conditioned by adding distilled water and equilibrating for one week, and the rest were dried in a vacuum over CaCl_2 until they reached their respective moisture contents. Moisture content was determined by drying triplicate ground samples in a ventilated oven at 113°C (235°F) for 4 hours.

specific heat: straight line regression equations for the relation between the specific heat and moisture content where C_p is apparent specific heat and M is moisture content (%). The apparent specific heat of water [$C_p(w)$] was calculated from the equation.

$$C_p = 0.0107 M + 0.265 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p = 0.0107 M + 0.265 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.0448 M + 1.109 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 1.335 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p(w) = 1.335 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 5.586 \text{ J g}^{-1} \text{ K}^{-1}$$

54HAS

RICE, SHELLED (ITALIAN ORIGIN); solid; Grain has fat content of 0.4%–2%. The relationship between the grain and the moisture content was determined. One third of the samples were not conditioned, one third were conditioned by adding distilled water and equilibrating for one week, and the rest were dried in a vacuum over CaCl_2 until they reached their respective moisture contents. Moisture content was determined by drying triplicate ground samples in a ventilated oven at 113°C (235°F) for 4 hours.

specific heat: straight line regression equations for the relation between the specific heat and moisture content where C_p is apparent specific heat and M is moisture content (%). The apparent specific heat of water [$C_p(w)$] was calculated from the equation.

$$C_p = 0.0091 M + 0.287 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p = 0.0091 M + 0.287 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.0381 M + 1.201 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 1.197 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p(w) = 1.197 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 5.008 \text{ J g}^{-1} \text{ K}^{-1}$$

54HAS

Foods

RICE, SWAMP PADDY; solid; Grain was heavily husked rough rice from the Gold Coast area. Sample A was as harvested from field (germination was 41%); sample B was wetted by addition of water or water vapor, and sample C was dried in vacuum at 30°C (86°F) (germination was 39%).

specific heat: temperature range 273-291 K (32°-64°F); data are mean values with standard error in parentheses and moisture content (M) on a wet weight basis (%).

Sample	M %	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
A	11.5	0.377(0.0032)	0.377(0.0032)	1.577(0.0134)
B	14.9	0.417(0.0037)	0.417(0.0037)	1.745(0.0155)
C	9.2	0.358(0.0040)	0.358(0.0040)	1.498(0.0167)

54DIS

WALNUTS, ENGLISH; *Juglans regia*; solid; 3.97% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 5972 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3318 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 13882 \text{ J g}^{-1}$$

55MER/WAT

WHALE OIL, HARDENED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 193. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 72.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature (°C)	(°F)	Btu lb ⁻¹	$H^\circ(t) - H^\circ(-50^\circ\text{C})$ cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	16.02	8.90	37.24
0	32	38.11	21.17	88.58
25	77	71.14	39.52	165.35
50	122	117.43	65.24	272.96
55	131	121.79	67.66	283.09

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 48.6 \text{ Btu lb}^{-1}$$

$$L_f = 27.9 \text{ cal g}^{-1}$$

$$L_f = 113.0 \text{ J g}^{-1}$$

55RIE

WHALE OIL, UNREFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 192. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 120.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature		Btu lb ⁻¹	H°(t)-H°(-50°C)	
(°C)	(°F)		cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	21.22	11.79	49.33
0	32	55.17	30.65	128.24
25	77	84.47	46.93	196.36
50	122	106.09	58.94	246.61
55	131	110.32	61.29	255.44

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 27.4 \text{ Btu lb}^{-1}$$

$$L_f = 15.2 \text{ cal g}^{-1}$$

$$L_f = 63.6 \text{ J g}^{-1}$$

55RIE

WHEAT; *Triticum aestivum*; 8.5% moisture.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 7362 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4090 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 17115 \text{ J g}^{-1}$$

55MER/WAT

WHEAT, BERSEE; solid; Material is a soft white grain of French origin grown as a high-yielding winter or spring variety. Straight line regression equations for computing the specific heat (C_p) at different moisture contents (M) in percent are below. Moisture content was determined in a ventilated oven at 113°C (235°F) for 4 hours and calculated as a percentage of wet weight. Germination was either 100% or 0%.

specific heat: temperature range 273-291 K (32°-64°F). The apparent specific heat of water [$C_p(w)$] was computed from the regression equation by writing M = 100%.

$$M = 23.7\%-33.6\%$$

$$C_p = 0.00731 M + 0.336 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p = 0.00731 M + 0.336 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.03059 M + 1.406 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 1.07 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p(w) = 1.07 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 4.48 \text{ J g}^{-1} \text{ K}^{-1}$$

$$M = 7.7\%-23.7\%$$

$$C_p = 0.01036 M + 0.263 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p = 0.01036 M + 0.263 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.04335 M + 1.100 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 1.30 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p(w) = 1.30 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 5.44 \text{ J g}^{-1} \text{ K}^{-1}$$

$$M = 1.8\%-7.7\%$$

$$C_p = 0.00591 M + 0.297 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p = 0.00591 M + 0.297 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.02473 M + 1.243 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 0.89 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p(w) = 0.89 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = 3.72 \text{ J g}^{-1} \text{ K}^{-1}$$

$$M = 0.0\%-1.8\%$$

$$C_p = 0.00406 M + 0.307 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p = 0.00406 M + 0.307 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 0.01699 M + 1.284 \text{ J g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = -0.10 \text{ Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}$$

$$C_p(w) = -0.10 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p(w) = -0.42 \text{ J g}^{-1} \text{ K}^{-1}$$

54DIS

WHEAT, NO. 1 NORTHERN MANITOBA; solid; Grain had an initial moisture content of 13.7%. Samples of this batch were conditioned by drying in an oven (at either 60° or 113°C) or by addition of liquid water in air-tight jars. Material is a Canadian hard red spring wheat.

specific heat: temperature range 273-291 K (32°-64°F); data are mean values with standard error in parentheses and moisture content (M) is given in % on a wet weight basis.

M %	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
17.5	0.447(0.0027)	0.447(0.0027)	1.870(0.0113)
15.3	0.416(0.0021)	0.416(0.0021)	1.741(0.0088)
13.7	0.398(0.0020)	0.398(0.0020)	1.665(0.0084)
10.1	0.367(0.0039)	0.367(0.0039)	1.536(0.0163)
4.9	0.333(0.0024)	0.333(0.0024)	1.393(0.0100)
1.89	0.318(0.0024)	0.318(0.0024)	1.331(0.0100)
1.29	0.310(0.0029)	0.310(0.0029)	1.297(0.0121)

54DIS

Fossil Materials

ASPHALT; solid; mixture of paraffinic, aromatic, and heterocyclic hydrocarbons (containing oxygen, nitrogen, and sulfur).

specific heat: Venezuelan distilled asphalt.

Softening Point, °F	C_p (Btu lb ⁻¹ °F ⁻¹)			
	32°F	212°F	392°F	572°F
103.1	0.425	0.472	0.520	0.567
144.5	0.409	0.463	0.518	0.572
205.7	0.382	0.455	0.527	0.600

Softening Point, °C	C_p (cal g ⁻¹ C ⁻¹)			
	0°C	100°C	200°C	300°C
39.5	0.425	0.472	0.520	0.567
62.5	0.409	0.463	0.518	0.572
96.5	0.382	0.455	0.527	0.600

Softening Point, °C	C_p (J g ⁻¹ C ⁻¹)			
	0°C	100°C	200°C	300°C
39.5	1.778	1.975	2.176	2.372
62.5	1.711	1.937	2.167	2.393
96.5	1.598	1.904	2.205	2.510

62BAR; 40SAA/HEU

COAL, ANTHRACITE; solid; ultimate analysis of combustible, ash free and moisture free: carbon, 94.39%; hydrogen, 1.77%; oxygen, 2.13%; nitrogen, 0.71%; sulfur, 1.00%; proximate analysis: ash, 7.83%; moisture, 2.80%; volatile matter, 1.3%; loss on air drying, 1.5%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

as received

$$q_v(\text{gross}) = 14890 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 8273 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 34616 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 13310 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7393 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 30931 \text{ J g}^{-1}$$

18POO; 15LOR

Fossil Materials

COAL, BITUMINOUS; solid; National Bureau of Standards (NBS) Standard Reference Material (SRM) 1632a, Residual moisture, 1.145 wt. %; ash content, 22.15 wt. %; sulfur content, 1.48 wt. %.

gross heat of combustion: assume values refer to room temperature; values are on a moisture-free, ash-free basis.

$$q_v(\text{gross}) = 14534 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 8080 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 33806 \text{ J g}^{-1}$$

81KIR/COL

COAL, BITUMINOUS (HIGH GRADE); solid; ultimate analysis of combustible, ash free and moisture free: carbon, 85.09%; hydrogen, 4.99%; oxygen, 6.99%; nitrogen, 1.80%; sulfur, 1.13%; proximate analysis: ash, 2.79%; moisture, 2.18%; volatile matter, 33.4%; loss on air drying, 1.0%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

as received

$$q_v(\text{gross}) = 15600 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 8667 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 36262 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 14830 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 8237 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 34462 \text{ J g}^{-1}$$

18POO; 15LOR

COAL, BITUMINOUS (LOW GRADE); solid; ultimate analysis of combustible, ash free and moisture free: carbon, 76.11%; hydrogen, 4.03%; oxygen, 16.14%; nitrogen, 0.84%; sulfur, 2.88%; proximate analysis: ash, 26.88%; moisture, 10.88%; volatile matter, 32.6%; loss on air drying, 5.4%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

as received

$$q_v(\text{gross}) = 12450 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6915 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 28931 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 7747 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4304 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18008 \text{ J g}^{-1}$$

18POO; 15LOR

COAL, BITUMINOUS (MEDIUM GRADE); solid; (sample 1) ultimate analysis of combustible, ash free and moisture free: carbon, 82.08%; hydrogen, 5.40%; oxygen, 5.98%; nitrogen, 1.32%; sulfur, 5.22%; proximate analysis: ash, 12.97%; moisture, 4.99%; volatile matter, 39.8%; loss on air drying, 1.3%; (sample 2) ultimate analysis of combustible, ash free and moisture free: carbon, 76.55%; hydrogen, 5.26%; oxygen, 11.83%; nitrogen, 1.40%; sulfur, 4.96%; proximate analysis: ash, 23.38%; moisture, 17.30%; volatile matter, 44.6%; loss on air drying, 15.2%.

gross heat of combustion: assume values refer to room temperature.

sample 1, ash free and moisture free

$$\begin{aligned}q_v(\text{gross}) &= 14930 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8296 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 34709 \text{ J g}^{-1}\end{aligned}$$

sample 1, as received

$$\begin{aligned}q_v(\text{gross}) &= 12250 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6806 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 28475 \text{ J g}^{-1}\end{aligned}$$

sample 2, ash free and moisture free

$$\begin{aligned}q_v(\text{gross}) &= 13900 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7723 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 32313 \text{ J g}^{-1}\end{aligned}$$

sample 2, as received

$$\begin{aligned}q_v(\text{gross}) &= 8246 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4581 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19166 \text{ J g}^{-1}\end{aligned}$$

18POO; 15LOR

COAL, CANNEL; solid; ultimate analysis of combustible, ash free and moisture free: carbon, 82.59%; hydrogen, 7.13%; oxygen, 7.57%; nitrogen, 1.33%; sulfur, 1.38%; proximate analysis: ash, 10.49%; moisture, 2.36%; volatile matter, 55.5%; loss on air drying, 1.5%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

$$\begin{aligned}q_v(\text{gross}) &= 15810 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8784 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 36751 \text{ J g}^{-1}\end{aligned}$$

as received

$$\begin{aligned}q_v(\text{gross}) &= 13780 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7655 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 32029 \text{ J g}^{-1}\end{aligned}$$

18POO; 15LOR

COAL, SEMI-ANTHRACITE; solid; ultimate analysis of combustible, ash free and moisture free: carbon, 92.15%; hydrogen, 3.76%; oxygen, 2.17%; nitrogen, 1.18%; sulfur, 0.74%; proximate analysis: ash, 11.50%; moisture, 3.38%; volatile matter, 10.0%; loss on air drying, 2.6%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

$$\begin{aligned}q_v(\text{gross}) &= 15470 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8593 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 35953 \text{ J g}^{-1}\end{aligned}$$

as received

$$\begin{aligned}q_v(\text{gross}) &= 13170 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7314 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 30601 \text{ J g}^{-1}\end{aligned}$$

18POO; 15LOR

Fossil Materials

COAL, SEMI-BITUMINOUS; solid; ultimate analysis of combustible, ash free and moisture free: carbon, 89.79%; hydrogen, 4.76%; oxygen, 2.47%; nitrogen, 2.00%; sulfur, 0.98%; proximate analysis: ash, 6.80%; moisture, 2.60%; volatile matter, 17.5%; loss on air drying, 2.0%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

$$\begin{aligned}q_v(\text{gross}) &= 15860 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8811 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 36867 \text{ J g}^{-1}\end{aligned}$$

as received

$$\begin{aligned}q_v(\text{gross}) &= 14370 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7983 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33401 \text{ J g}^{-1}\end{aligned}$$

18POO; 15LOR

COAL, SUB-BITUMINOUS; solid; ultimate analysis of combustible, ash free and moisture free: carbon, 69.17%; hydrogen, 4.46%; oxygen, 24.35%; nitrogen, 1.66%; sulfur, 0.36%; proximate analysis: ash, 3.71%; moisture, 18.41%; volatile matter, 44.3%; loss on air drying, 10.0%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

$$\begin{aligned}q_v(\text{gross}) &= 11729 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6516 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 27265 \text{ J g}^{-1}\end{aligned}$$

as received

$$\begin{aligned}q_v(\text{gross}) &= 9137 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5076 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21236 \text{ J g}^{-1}\end{aligned}$$

18POO; 15LOR

COKE; solid; produced from the destructive distillation of gas-coal in gas retorts; (sample 1, as received): fixed carbon, 59.56%; sulfur, 0.31%; moisture, 22.30%; ash, 17.56%; volatile matter, 0.58%; (sample 1, dry): fixed carbon, 76.65%; sulfur, 0.40%; ash, 22.60%; volatile matter, 0.75%; (sample 2, as received): fixed carbon, 67.89%; sulfur, 0.51%; ash, 4.45%; moisture, 26.80%; volatile matter, 0.86%; (sample 2, dry): fixed carbon, 92.75%; sulfur, 0.70%; ash, 6.08%; volatile matter, 1.17%; (dry represents sample as drawn from retort before quenching).

gross heat of combustion: assume values refer to room temperature.

sample 1, as received

$$\begin{aligned}q_v(\text{gross}) &= 8687 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4826 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20192 \text{ J g}^{-1}\end{aligned}$$

sample 2, as received

$$\begin{aligned}q_v(\text{gross}) &= 10100 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5612 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23479 \text{ J g}^{-1}\end{aligned}$$

sample 1, dry

$$\begin{aligned}q_v(\text{gross}) &= 11180 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6211 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 25988 \text{ J g}^{-1}\end{aligned}$$

sample 2, dry

$$\begin{aligned}q_v(\text{gross}) &= 13800 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7666 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 32076 \text{ J g}^{-1}\end{aligned}$$

18POO; 11WHI/BAR

COKE; solid; produced from the destructive distillation of bituminous coal in beehive ovens; (sample 1): fixed carbon, 91.43%; volatile carbon, 1.27%; sulfur, 0.51%; ash, 6.09%; (sample 2): fixed carbon, 79.83%; volatile carbon, 1.05%; sulfur, 2.13%; ash, 15.75%; water, 1.22%.

gross heat of combustion: assume values refer to room temperatures; corrected for moisture and ash content.

sample 1

$$\begin{aligned}q_v(\text{gross}) &= 14420 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8011 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33520 \text{ J g}^{-1}\end{aligned}$$

sample 2

$$\begin{aligned}q_v(\text{gross}) &= 13890 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7718 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 32292 \text{ J g}^{-1}\end{aligned}$$

18POO

COKE; solid; produced from the destructive distillation to red heat of petroleum; fixed carbon, 98.05%; volatile carbon, 0.50%.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 14510 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8063 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33734 \text{ J g}^{-1}\end{aligned}$$

18POO

COKE BREEZE; solid; ultimate analysis: carbon, 94.79%; hydrogen, 1.51%; oxygen, 1.48%; nitrogen, 1.19%; sulfur, 1.03%; proximate analysis: ash, 12.05%; moisture, 10.77%; volatile matter, 4.92%; loss on air drying, 10.1%.

gross heat of combustion: assume values refer to room temperature.

ash free and moisture free

$$\begin{aligned}q_v(\text{gross}) &= 14470 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8038 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33632 \text{ J g}^{-1}\end{aligned}$$

as received

$$\begin{aligned}q_v(\text{gross}) &= 11170 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6204 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 25958 \text{ J g}^{-1}\end{aligned}$$

18POO; 15FER

FUEL, AVIATION; liquid; petroleum fraction with B.P. range 175°-350°C (347°-662°F) (kerosine). Military jet fuels labeled JP-3, JP-4, JP-5, etc. Commercial jet fuels labeled as ASTM types A, A-1, or B.

net heat of combustion: A is the aniline point, in degrees Fahrenheit, identifying the minimum equilibrium solution temperature for equal volumes of aniline and sample. G is the API gravity defined as: API gravity (deg) = 141.5/(sp. gr. 60/60°F)-131.5. Tables are provided in ASTM Specification D 1405 to calculate q_p (net) if sulfur impurities are known.

Aviation gasoline, Grades 100-130 and 115-145:

$$q_p(\text{net}) = [18049 + 0.0833 (A \times G)] \text{ Btu lb}^{-1}$$

$$q_p(\text{net}) = [10027 + 0.0463 (A \times G)] \text{ cal g}^{-1}$$

$$q_p(\text{net}) = [41954 + 0.1938 (A \times G)] \text{ J g}^{-1}$$

Jet fuels:

JP-3

$$q_p(\text{net}) = [17951 + 0.1057 (A \times G)] \text{ Btu lb}^{-1}$$

$$q_p(\text{net}) = [9973 + 0.0587 (A \times G)] \text{ cal g}^{-1}$$

$$q_p(\text{net}) = [41728 + 0.2456 (A \times G)] \text{ J g}^{-1}$$

JP-4

$$q_p(\text{net}) = [17989 + 0.1057 (A \times G)] \text{ Btu lb}^{-1}$$

$$q_p(\text{net}) = [9994 + 0.0587 (A \times G)] \text{ cal g}^{-1}$$

$$q_p(\text{net}) = [41815 + 0.2456 (A \times G)] \text{ J g}^{-1}$$

JP-5

$$q_p(\text{net}) = [17926 + 0.1057 (A \times G)] \text{ Btu lb}^{-1}$$

$$q_p(\text{net}) = [9959 + 0.0587 (A \times G)] \text{ cal g}^{-1}$$

$$q_p(\text{net}) = [41668 + 0.2456 (A \times G)] \text{ J g}^{-1}$$

Kerosine, Jet A or A-1 (see ASTM Speciation D 1655):

$$q_p(\text{net}) = [17932 + 0.10930 (A \times G)] \text{ Btu lb}^{-1}$$

$$q_p(\text{net}) = [9962 + 0.06072 (A \times G)] \text{ cal g}^{-1}$$

$$q_p(\text{net}) = [41680 + 0.25407 (A \times G)] \text{ J g}^{-1}$$

68AST

FUEL, AVIATION; liquid; petroleum fraction with B.P. range 175°-350°C (347°-662°F).

gross heat of combustion: assume values refer to 25°C (77°F).

aviation gasoline, grade 91-96:

$$q_v(\text{gross}) = 20232 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11240 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 47028 \text{ J g}^{-1}$$

aviation gasoline, grade 100-130:

$$q_v(\text{gross}) = 20288 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11271 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 47158 \text{ J g}^{-1}$$

48LET/MAT

FUEL, COED-1 FMC WESTERN KENTUCKY COAL DERIVED; liquid; Material was refined by fractionation. Composition was nitrogen = 40 ppm, sulfur = 0.05 wt. %, aromatics = 24.8%, C₉ to C₁₆ n-alkanes = 3.90 wt. %, and hydrogen = 12.80 wt. %. The freezing point is -48°C (-54°F).

net heat of combustion: assume values refer to room temperature; where net heat of combustion [q (net at 25°C)] = gross heat of combustion [q (gross at 25°C)] - 91.23 H, where H = hydrogen weight % of the sample.

$$q_v(\text{net}) = 18294 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10163 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 42523 \text{ J g}^{-1}$$

76HAZ/HAL

FUEL, COED-2 UTAH COAL DERIVED; liquid; Material was refined by fractionation. Composition was nitrogen = 42 ppm, sulfur = 0.04 wt. %, aromatics = 24.1%, C₉ to C₁₆ n-alkanes = 7.14 wt. %, and hydrogen = 12.98 wt. %. The freezing point is -40°C (-40°F).

net heat of combustion: assume values refer to room temperature; where net heat of combustion [q (net at 25°C)] = gross heat of combustion [q (gross at 25°C)] - 91.23 H, where H = hydrogen weight % of the sample.

$$q_v(\text{net}) = 18327 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10207 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 42705 \text{ J g}^{-1}$$

76HAZ/HAL

Fossil Materials

FUEL, COED-3 WESTERN KENTUCKY COAL DERIVED; liquid; Material was refined by fractionation. Composition was nitrogen = 40 ppm, sulfur = 0.05 wt. %, aromatics = 4.7%, C₉ to C₁₆ n-alkanes = 3.73 wt. %, and hydrogen = 13.34 wt. %. The freezing point is -50°C (-58°F).

net heat of combustion: assume values refer to room temperature; where net heat of combustion [q (net at 25°C)] = gross heat of combustion [q (gross at 25°C)] - 91.23 H, where H = hydrogen weight % of the sample.

$$\begin{aligned}q_v(\text{net}) &= 18383 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 10213 \text{ cal g}^{-1} \\q_v(\text{net}) &= 42730 \text{ J g}^{-1}\end{aligned}$$

76HAZ/HAL

FUEL, COED-4 UTAH COAL DERIVED; liquid; Material was refined by fractionation. Composition was nitrogen = 43 ppm, sulfur = 0.03 wt. %, aromatics = 6.1%, C₉ to C₁₆ n-alkanes = 7.45 wt. %, and hydrogen = 13.62 wt. %. The freezing point is -40°C (-40°F).

net heat of combustion: assume values refer to room temperature; where net heat of combustion [q (net at 25°C)] = gross heat of combustion [q (gross at 25°C)] - 91.23 H, where H = hydrogen weight % of the sample.

$$\begin{aligned}q_v(\text{net}) &= 18465 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 10258 \text{ cal g}^{-1} \\q_v(\text{net}) &= 42921 \text{ J g}^{-1}\end{aligned}$$

76HAZ/HAL

FUEL, COED-5 WESTERN KENTUCKY COAL DERIVED; liquid; Material was refined by fractionation. Composition was nitrogen = 37 ppm, sulfur = 0.03 wt. %, aromatics = 24.1%, C₉ to C₁₆ n-alkanes = 5.48 wt. %, and hydrogen = 12.81 wt. %. The freezing point is -56.7°C (-70°F).

net heat of combustion: assume values refer to room temperature; where net heat of combustion [q (net at 25°C)] = gross heat of combustion [q (gross at 25°C)] - 91.23 H, where H = hydrogen weight % of the sample.

$$\begin{aligned}q_v(\text{net}) &= 18282 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 10157 \text{ cal g}^{-1} \\q_v(\text{net}) &= 42495 \text{ J g}^{-1}\end{aligned}$$

76HAZ/HAL

FUEL, JP-9 RAMJET; liquid; Material is a blend of 10.3 wt. % methylcyclohexane, 68.4 wt. % of exo-tetrahydrodicyclopentadiene, and 21.2 wt. % of the hydrogenated dimers of norbornadiene whose empirical formula is $C_{14}H_{18}$; the empirical formula for the blend is $C_{10.529}H_{16.202}$. Recovery of CO_2 from the combustion products gave a mean value of 99.63₀%.

gross heat of combustion: The reference temperature is 298.15 K (77°F). Value is mean with standard deviation of the mean.

$$q_v(\text{gross}) = 19204.49 \pm 1.40 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10669.16 \pm 0.78 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 44639.77 \pm 3.26 \text{ J g}^{-1}$$

net heat of combustion: The reference temperature is 298.15 K (77°F). Value is mean with standard deviation of the mean.

$$q_v(\text{net}) = 18160.7 \pm 4.3 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10089.3 \pm 2.4 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 42213.6 \pm 10. \text{ J g}^{-1}$$

78SMI/GOO

FUEL, PARAHO OIL SHALE DERIVED; liquid; Material was refined by delayed coking and fractionation. Composition was nitrogen = 680 ppm, sulfur = 0.05 wt. %, aromatics = 26.0%, C_9 to C_{16} n-alkanes = 36.33 wt. %, and hydrogen = 13.74 wt. %. The freezing point is -33.3°C (-28°F).

net heat of combustion: assume values refer to room temperature, where net heat of combustion [q (net at 25°C)] = gross heat of combustion [q (gross at 25°C)] - 91.23 H where H = hydrogen weight % of sample.

$$q_v(\text{net}) = 18532 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10296 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 43077 \text{ J g}^{-1}$$

76HAZ/HAL

FUEL, PETROLEUM-A DERIVED; liquid; Material was produced by drilling. Composition was sulfur = 0.11 wt. %, aromatics = 18.2%, C_9 to C_{16} n-alkanes = 16.00 wt. %. The freezing point is -48.9°C (-56°F).

net heat of combustion: assume values refer to room temperature.

$$q_v(\text{net}) = 18518 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10288 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 43044 \text{ J g}^{-1}$$

76HAZ/HAL

FUEL, RJ-4 RAMJET; liquid; Material, exo-tetrahydrodi (methylcyclopentadiene) is a mixture of isomers in which the location of the methyl groups is unknown. Recovery of CO₂ from combustion products gave a mean value of 99.98₃%.

gross heat of combustion: The reference temperature is 298.15 K (77°F). Value is mean value with standard deviation of the mean.

$$q_v(\text{gross}) = 19396.22 \pm 1.44 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10775.68 \pm 0.80 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45085.45 \pm 3.35 \text{ J g}^{-1}$$

net heat of combustion: The reference temperature is 298.15 K (77°F). Value is mean value with standard deviation of the mean.

$$q_v(\text{net}) = 18275.6 \pm 4.1 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10153.1 \pm 2.3 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 42480.6 \pm 9.6 \text{ J g}^{-1}$$

78SMI/GOO

FUEL, RJ-4 RAMJET; liquid; Material is a complex mixture of isomers, all of formula C₁₂H₂₀. Carbon dioxide recovery from combustion products was 99.98₃ ± 0.00₆% of that expected.

gross heat of combustion: temperature, 298.15 K (77°F).

$$q_v(\text{gross}) = 19427.95 \pm 4.16 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10793.31 \pm 2.31 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45159.20 \pm 9.68 \text{ J g}^{-1}$$

net heat of combustion: temperature, 298.15 K (77°F).

$$q_v(\text{net}) = 18275.39 \pm 4.16 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10152.99 \pm 2.31 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 42480.13 \pm 9.68 \text{ J g}^{-1}$$

77GOO/SCO

FUEL, RJ-4-I RAMJET; liquid; Material, endo-tetrahydrodi (methylcyclopentadiene), is a mixture of isomers in which the location of the methyl groups is unknown. Recovery of CO₂ from combustion products gave a mean value of 99.96₂%.

gross heat of combustion: The reference temperature is 298.15 K (77°F). Value is mean with standard deviation of the mean.

$$q_v(\text{gross}) = 19374.55 \pm 1.03 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10763.64 \pm 0.57 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45035.07 \pm 2.38 \text{ J g}^{-1}$$

(more)

FUEL, RJ-4-I RAMJET - Continued

net heat of combustion: The reference temperature is 298.15 K (77°F). Value is mean with standard deviation of mean.

$$q_v(\text{net}) = 18254.5 \pm 4.0 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10141.4 \pm 2.2 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 42431.6 \pm 9.2 \text{ J g}^{-1}$$

78SMI/GOO

FUEL, RJ-6 RAMJET; liquid; Material is a blend of exo-tetrahydrodicyclopentadiene and the hydrogenated dimers of norbornadiene and used without further drying. The ratio of CO₂ recovered to mass of sample burned was 3.2725 ± 0.0002 (mean and standard deviation of the mean). The empirical formula calculated from this ratio is CH_{1.4259}.

gross heat of combustion: temperature, 298.15 K (77°F).

$$q_v(\text{gross}) = 18959.58 \pm 0.43 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10533.10 \pm 0.24 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 44070.49 \pm 1.00 \text{ J g}^{-1}$$

net heat of combustion: temperature, 298.15 K (77°F).

$$q_v(\text{net}) = 17971.8 \pm 0.4 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 9983.9 \pm 0.2 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 41774.5 \pm 0.9 \text{ J g}^{-1}$$

heat capacity: temperature range 260–340 K (9°–153°F), and C_s is the heat capacity of the substance in equilibrium with its saturated vapor. The root mean square deviation of results was 0.0055 cal g⁻¹ K⁻¹.

$$C_s(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.31378 + 4.97 \times 10^{-4} T$$

$$C_s(\text{cal g}^{-1} \text{ K}^{-1}) = 0.0852880 + 8.948 \times 10^{-4} T$$

$$C_s(\text{J g}^{-1} \text{ K}^{-1}) = 0.3568450 + 3.7438 \times 10^{-3} T$$

79SMI/SCO

FUEL, RJ-6 RAMJET; liquid; Material is a blend of JP-10 (exo-tetrahydrodicyclopentadiene) and 3 hydrogenated dimers of norbornadienes.

heat capacity: Temperature range was 260–467 K (9°–381°F), and uncertainties are standard deviations at either end of the measurement range. The 1961 atomic weights and thermochemical calorie were used.

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.2939 + 6.0905 \times 10^{-4} T \pm 0.00056$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = (0.013913 + 0.10963 \times 10^{-2} T) \pm 0.00056$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = (0.058212 + 0.45869 \times 10^{-2} T) \pm 0.00234$$

80SMI/THO

FUEL, TAR SANDS (ALTERNATIVE JET FUEL); liquid; Canadian sample was refined by delayed coking and fractionation. Partial composition was sulfur = 0.01 wt. %, aromatics = 19.3%, C₉ to C₁₆ n-alkanes = 9.50 wt. %, and hydrogen = 13.50 wt. %. The freezing point is -53.3°C (-64°F).

net heat of combustion: assume values refer to room temperature; where net heat of combustion [q (net at 25°C)] = gross heat of combustion [q (gross at 25°C)] - 91.23 H, where H = hydrogen weight % of the sample.

$$q_v(\text{net}) = 18436 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 10242 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 42853 \text{ J g}^{-1}$$

76HAZ/HAL

GAS, NATURAL; gas; composition in mole percent; (sample A), N₂ = 15.6%, He = 0.84%, CO₂ = 0.03%, CH₄ = 72.2%, C₂H₆ = 6.5%, propane = 3.8%, n-butane = 0.66%, isobutane = 0.28%, pentanes = 0.02%, hexanes = 0.01%, and heptanes = 0.01%. (sample B), N₂ = 2.8%, He = 0.23%, CO₂ = 0.19%, CH₄ = 86.2%, C₂H₆ = 6.2%, propane = 2.7%, n-butane = 0.63%, isobutane = 0.52%, pentanes = 0.32%, hexanes = 0.22%, and heptanes = 0.07%. (sample C), N₂ = 0.24%, He = 0.00%, CO₂ = 0.87%, CH₄ = 94.7%, C₂H₆ = 3.2%, propane = 0.67%, n-butane = 0.12%, isobutane = 0.06%, pentanes = 0.06%, hexanes = 0.06%, and heptanes = 0.04%. (sample D), N₂ = 7.1%, He = 0.32%, CO₂ = 0.49%, CH₄ = 84.3%, C₂H₆ = 5.2%, propane = 1.9%, n-butane = 0.31%, isobutane = 0.28%, pentanes = 0.04%, hexanes = 0.04%, and heptanes = 0.03%.

gross heat of combustion: at 15.56°C (60°F) and 101325 Pa (1 atm); where SCF is standard cubic foot.

sample A

$$q_v(\text{gross}) = 958 \text{ Btu(SCF)}^{-1}$$

$$q_v(\text{gross}) = 8.51 \times 10^6 \text{ cal m}^{-3}$$

$$q_v(\text{gross}) = 35.7 \times 10^6 \text{ J m}^{-3}$$

sample B

$$q_v(\text{gross}) = 1101 \text{ Btu(SCF)}^{-1}$$

$$q_v(\text{gross}) = 9.80 \times 10^6 \text{ cal m}^{-3}$$

$$q_v(\text{gross}) = 41.0 \times 10^6 \text{ J m}^{-3}$$

sample C

$$q_v(\text{gross}) = 1028 \text{ Btu(SCF)}^{-1}$$

$$q_v(\text{gross}) = 9.15 \times 10^6 \text{ cal m}^{-3}$$

$$q_v(\text{gross}) = 38.3 \times 10^6 \text{ J m}^{-3}$$

sample D

$$q_v(\text{gross}) = 999 \text{ Btu(SCF)}^{-1}$$

$$q_v(\text{gross}) = 8.89 \times 10^6 \text{ cal m}^{-3}$$

$$q_v(\text{gross}) = 37.2 \times 10^6 \text{ J m}^{-3}$$

compressibility factor, Z = PV/RT: at 15.56°C (60°F) and 101325 Pa (1 atm).

$$Z (\text{sample A}) = 0.9978$$

$$Z (\text{sample B}) = 0.9974$$

$$Z (\text{sample C}) = 0.9978$$

$$Z (\text{sample D}) = 0.9979$$

61MAS/EAK

GASOLINE; liquid; a mixture of volatile hydrocarbons with boiling points ranging from 60°-198°C (140°-390°F) (branched-chain paraffins, cycloparaffins, and aromatics).

auto-ignition temperature:

octane rating	temperature	
	°C	°F
65	248	478
73	258	496
87	412	774

54SET

GASOLINE; liquid; a mixture of volatile hydrocarbons with boiling points ranging from 140°-390°F (branched-chain paraffins, cycloparaffins, and aromatics).

gross heat of combustion: assume values refer to room temperature.

Production motor gasoline:

regular grade

$$\begin{aligned} q_v(\text{gross}) &= 19990 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 11106 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 46466 \text{ J g}^{-1} \end{aligned}$$

premium grade

$$\begin{aligned} q_v(\text{gross}) &= 20079 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 11155 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 46673 \text{ J g}^{-1} \end{aligned}$$

48LET/MAT

GREASE, APIEZON N; solid; low vapor-pressure residues of paraffin oil distillation products.

specific heat:

In the temperature range: -193° to -73°C (-315° to -99°F).

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = -3.0315 \times 10^{-3} + 1.1378 \times 10^{-3} (t + 459.67) - 1.8554 \times 10^{-6} (t + 459.67)^2 + 2.4581 \times 10^{-9} (t + 459.67)^3$$

$$C_p(\text{cal g}^{-1} \text{ } ^\circ\text{C}^{-1}) = -3.0315 \times 10^{-3} + 2.0481 \times 10^{-3} (t + 459.67) - 6.0115 \times 10^{-6} (t + 459.67)^2 + 1.4336 \times 10^{-8} (t + 459.67)^3$$

$$C_p(\text{J g}^{-1} \text{ } ^\circ\text{C}^{-1}) = -1.2684 \times 10^{-2} + 4.7606 \times 10^{-3} (t + 459.67) - 2.5152 \times 10^{-5} (t + 459.67)^2 + 5.9982 \times 10^{-8} (t + 459.67)^3$$

(more)

GREASE, APIEZON N - Continued

In the temperature range -73° to 57°C , (-99° to 124°F), C_p is anomalous; values are given below

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	$C_p(\text{Btu lb}^{-1} \text{ }^{\circ}\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ }^{\circ}\text{C}^{-1})$	$C_p(\text{J g}^{-1} \text{ }^{\circ}\text{C}^{-1})$
-73	-99	0.281	0.281	1.18
-63	-81	0.301	0.301	1.26
-53	-63	0.344	0.344	1.44
-43	-45	0.392	0.392	1.64
-33	-27	0.421	0.421	1.76
-23	-9	0.445	0.445	1.86
-13	9	0.468	0.468	1.96
-3	27	0.543	0.543	2.27
7	45	0.679	0.679	2.84
17	63	0.853	0.853	3.57
23	73	0.899	0.899	3.76
27	81	0.858	0.858	3.59
37	99	0.626	0.626	2.62
47	117	0.554	0.554	2.32
57	135	0.538	0.538	2.25

69BUN/ASH

GREASE, APIEZON P; solid; low vapor-pressure residues of paraffin oil distillation products; average molecular weight 410 ± 70 .

heat of vaporization: temperature range 40° - 160°C (104° - 320°F).

$$L_v = 152.5 \text{ Btu lb}^{-1}$$

$$L_v = 84.70 \text{ cal g}^{-1}$$

$$L_v = 354.4 \text{ J g}^{-1}$$

vapor pressure: temperature range 40° - 160°C (104° - 320°F).

$$\log_{10} P(\text{Torr}) = 13.91 - 7590 T^{-1} (\text{K})$$

$$\log_{10} P(\text{Pa}) = 16.03 - 7590 T^{-1} (\text{K})$$

57HER/REI

GREASE, APIEZON R; solid; low vapor-pressure residues of paraffin oil distillation products; average molecular weight 660 ± 100 .

heat of vaporization: temperature range 40° - 160° C (104° - 320° F).

$$L_v = 87.98 \text{ Btu lb}^{-1}$$

$$L_v = 48.88 \text{ cal g}^{-1}$$

$$L_v = 204.5 \text{ J g}^{-1}$$

vapor pressure: temperature range 40° - 160° C (104° - 320° F).

$$\log_{10} P(\text{Torr}) = 12.54 - 7050 T^{-1} (\text{K})$$

$$\log_{10} P(\text{Pa}) = 14.66 - 7050 T^{-1} (\text{K})$$

57HER/REI

GREASE, APIEZON S; solid; low vapor-pressure residues of paraffin oil distillation products; average molecular weight 460 ± 60 .

heat of vaporization: temperature range 40° - 160° C (104° - 320° F).

$$L_v = 22.54 \text{ Btu lb}^{-1}$$

$$L_v = 70.08 \text{ cal g}^{-1}$$

$$L_v = 293.2 \text{ J g}^{-1}$$

vapor pressure: temperature range 40° - 160° C (104° - 320° F).

$$\log_{10} P(\text{Torr}) = 12.52 - 7045 T^{-1} (\text{K})$$

$$\log_{10} P(\text{Pa}) = 14.64 - 7045 T^{-1} (\text{K})$$

57HER/REI

GREASE, APIEZON T; solid; low vapor-pressure residues of paraffin oil distillation products; also contains an aluminum soap.

specific heat: specific heat is anomalous between 205 and 320 K.

temperature (K)	($^{\circ}$ F)	C_p (Btu lb $^{-1}$ $^{\circ}$ F $^{-1}$)	C_p (cal g $^{-1}$ K $^{-1}$)	C_p (J g $^{-1}$ K $^{-1}$)
5	-450.4	0.001035	0.001035	0.0004330
50	-369.4	0.07746	0.07746	0.3241
100	-279.4	0.1518	0.1518	0.6351
150	-189.4	0.2149	0.2149	0.8991
200	-99.4	0.2811	0.2811	1.1761
220	-63.4	0.362	0.362	1.515
240	-27.4	0.447	0.447	1.870
260	8.6	0.498	0.498	2.084
280	44.6	0.526	0.526	2.201
300	80.6	0.517	0.517	2.163
320	116.6	0.5022	0.5022	2.101
340	152.6	0.5180	0.5180	2.167
350	170.6	0.5259	0.5259	2.200

67WES/CHI

Fossil Materials

KEROSINE; liquid; mixture of hydrocarbons with boiling points ranging from 180°-300°C (356°-572°F); ultimate composition: carbon, 85.8%; hydrogen, 14.2%; sulfur, 58 ppm; total paraffins, 30.9%; total naphthenes, 64.3%; total aromatics, 4.8%; density, 0.8019 g cm⁻³ at 24°C (75°F); API gravity, 43.5.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 19957 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11087 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46390 \text{ J g}^{-1}$$

73LEN/HIP

LIGNITE; solid; Lignite is also called Brown Coal. (sample 1) ultimate analysis: carbon, 68.32%; hydrogen, 4.00%; oxygen, 25.54%; nitrogen, 1.42%; sulfur, 0.72%; proximate analysis: ash, 13.27%; moisture, 23.30%; volatile matter, 43.5%; loss on air drying, 17.3%; (sample 2) ultimate analysis: carbon, 63.30%; hydrogen, 3.32%; oxygen, 29.86%; nitrogen, 1.35%; sulfur, 2.17%; proximate analysis: ash, 10.12%; moisture, 31.37%; volatile matter, 50.6%; loss on air drying, 14.2%.

gross heat of combustion: assume values refer to room temperature.

sample 1, ash free and moisture free

$$q_v(\text{gross}) = 11040 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6132 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 25656 \text{ J g}^{-1}$$

sample 1, as received

$$q_v(\text{gross}) = 8105 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4503 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18841 \text{ J g}^{-1}$$

sample 2, ash free and moisture free

$$q_v(\text{gross}) = 9635 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5353 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 22399 \text{ J g}^{-1}$$

sample 2, as received

$$q_v(\text{gross}) = 5638 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3132 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 13104 \text{ J g}^{-1}$$

18POO; 15LOR

NAPHTHA, ALASKA; liquid; ultimate analysis: carbon, 86.3%; hydrogen, 13.7%; nitrogen, 0.3 ppm; sulfur, 99 ppm; total paraffins, 39.7%; total naphthenes, 39.6%; total aromatics, 20.5%; density, 0.7703 g cm⁻³ at 24°C (75°F); API gravity, 50.5.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 19514 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10841 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45360 \text{ J g}^{-1}$$

73LEN/HIP

NAPHTHA, AROMATIC; liquid; ultimate analysis: carbon, 90.1%; hydrogen, 9.8%; sulfur, 760 ppm; total paraffins, 0.0%; total naphthenes, 0.0%; total aromatics, 83.1%; total olefins, 16.9%; density, 0.8449 g cm^{-3} at 24°C (75°F); API gravity, 34.5.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 18517 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10287 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 43040 \text{ J g}^{-1}$$

73LEN/HIP

NAPHTHA, HIGH BOILING; liquid; ultimate analysis: carbon, 85.4%; hydrogen, 14.6%; sulfur, 357 ppm; total paraffins, 59.3%; total naphthenes, 30.8%; total aromatics, 9.9%; density, 0.7559 g cm^{-3} at 24°C (75°F); API gravity, 54.2.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 20191 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11217 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46934 \text{ J g}^{-1}$$

73LEN/HIP

NAPHTHA, JET; liquid; ultimate analysis: carbon, 86.05%; hydrogen, 13.95%; sulfur, 132 ppm; total paraffins, 18.6%; total naphthenes, 69.8%; total aromatics, 10.6%; sulfur compounds, 10,000 ppm density, 0.7981 g cm^{-3} at 24°C (75°F); API gravity, 44.4.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 19845 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11025 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46129 \text{ J g}^{-1}$$

73LEN/HIP

NAPHTHA, LOW BOILING; liquid; ultimate analysis: carbon, 85.1%; hydrogen, 14.9%; sulfur, 376 ppm; total paraffins, 61.9%; total naphthenes, 30.6%; total aromatics, 7.6%; density, 0.7559 g cm^{-3} at 24°C (75°F); API gravity, 59.9.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 20277 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11265 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 47132 \text{ J g}^{-1}$$

73LEN/HIP

OIL, CRUDE; liquid; ADMEG, Zakum (export), specific gravity 60/60°F = 0.8256, upper pour point = -15°C, wax content = 7.0 wt. %; Barrow Island, specific gravity 60/60°F = 0.8399, upper pour point < -50°C, wax content < 1 wt. %; Libyan (Tobruk export), specific gravity 60/60°F = 0.8429, upper pour point = 24°C, wax content = 20.0 wt. %; Iranian Light (export), specific gravity 60/60°F = 0.8568, upper pour point = -21°C, wax content = 7.0 wt. %; Kuwait (export), specific gravity 60/60°F = 0.8709, upper pour point = -32°C, wax content = 5.5 wt. %; Iranian Heavy (export), specific gravity 60/60°F = 0.8732, upper pour point = -12°C, wax content = 6.7 wt. %; Alaskan (North Slope), specific gravity 60/60°F = 0.8914, upper pour point = -1°C, wax content = 6.5 wt. %.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 22320 - 3780d^2 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 12400 - 2100d^2 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 51881.6 - 8786.4d^2 \text{ J g}^{-1}\end{aligned}$$

where d is the specific gravity at 60/60°F, equation assumes crude oil to be water, ash, and sulfur free; combustion products are gaseous CO_2 and liquid H_2O .

$$\begin{aligned}q_p'(\text{gross}) &= 1.8 q_v(\text{gross}) - 0.018 q_v(\text{gross})X + 40.5 (\%S) \text{ Btu lb}^{-1} \\q_v'(\text{gross}) &= q_v(\text{gross}) - 0.01 q_v(\text{gross})X + 22.5 (\%S) \text{ cal g}^{-1} \\q_v''(\text{gross}) &= q_v(\text{gross}) - 0.04 q_v(\text{gross})X + 94.1 (\%S) \text{ J g}^{-1}\end{aligned}$$

where $q_v'(\text{gross})$ is heat of combustion at constant volume of crude oil yielding ash, gaseous CO_2 , SO_2 , and liquid H_2O as combustion products; $X = (\% \text{H}_2\text{O} + \% \text{ash} + \%S)$

specific heat: The equation provided is based on over 100 measurements made at the National Bureau of Standards over the temperature range 273-477 K (32°-400°F). The experimental results differ from the values calculated from this equation by less than 2%, with a maximum deviation of 4%; oils from mixed base crudes are in good agreement; oils from paraffin base crudes are systematically high by about 2%; oils from naphthene base crudes are systematically low by about 2%.

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= (0.3880 + 4.5 \times 10^{-4} T)/d^{\frac{1}{2}} \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= (0.1811 + 8.1 \times 10^{-4} T)/d^{\frac{1}{2}} \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= (0.7577 + 3.39 \times 10^{-3} T)/d^{\frac{1}{2}}\end{aligned}$$

where d is the specific gravity at 60/60°F.

29CRA

OIL, FUEL; liquid; ultimate analysis: carbon, 86.9%; hydrogen, 13.1%; sulfur, 172 ppm; total paraffins, 29.8%; total naphthenes, 45.6%; total aromatics, 22.4%; sulfur compounds, 1.3%; density, 0.8553 g cm^{-3} at 24°C (75°F); API gravity 33.0.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 17570 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9763 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 40847 \text{ J g}^{-1}\end{aligned}$$

73LEN/HIP

OIL, GAS; liquid; ultimate analysis: carbon, 86.5%; hydrogen, 13.4%; sulfur, 261 ppm; nitrogen, 3 ppm; total paraffins, 38.8%; total naphthenes, 41.5%; total aromatics, 17.2%; sulfur compounds, 2.4%; density, 0.8415 g cm^{-3} at 24°C (75°F); API gravity, 35.3.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 19759 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10977 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45927 \text{ J g}^{-1}$$

73LEN/HIP

OIL, PARAFFIN; liquid; repeating unit: $\text{CH}_{1.891}$.

gross heat of combustion: 25°C (77°F)

$$q_v(\text{gross}) = 19771 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10984 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45957 \text{ J g}^{-1}$$

60GOO/LAC

OIL, PARAFFIN; liquid; low vapor-pressure residues of paraffin oil distillation products.

Apiezon C: average molecular weight 450 ± 70 ; temperature range $40^\circ\text{-}160^\circ\text{C}$ ($104^\circ\text{-}320^\circ\text{F}$).

heat of vaporization:

$$L_v = 108.45 \text{ Btu lb}^{-1}$$

$$L_v = 60.25 \text{ cal g}^{-1}$$

$$L_v = 252.1 \text{ J g}^{-1}$$

vapor pressure:

$$\log_{10} P(\text{Torr}) = 11.67 - 5925 T^{-1}(\text{K})$$

$$\log_{10} P(\text{Pa}) = 13.79 - 5925 T^{-1}(\text{K})$$

Apiezon E: average molecular weight 290 ± 30 ; temperature range $40^\circ\text{-}160^\circ\text{C}$ ($104^\circ\text{-}320^\circ\text{F}$).

$$L_v = 144.85 \text{ Btu lb}^{-1}$$

$$L_v = 80.47 \text{ cal g}^{-1}$$

$$L_v = 336.7 \text{ J g}^{-1}$$

vapor pressure:

$$\log_{10} P(\text{Torr}) = 9.30 - 5100 T^{-1}(\text{K})$$

$$\log_{10} P(\text{Pa}) = 11.42 - 5100 T^{-1}(\text{K})$$

57HER/REI

OIL, RAW SHALE; solid; Material came from the Anvil Points mine in Colorado and was riffled and split before retorting and combined with benzoic acid in a 1:1 ratio to achieve complete combustion in the bomb calorimeter. Combustion analysis indicated: $\text{H}_2\text{O}(\text{liq})$, $\text{CO}_2(\text{g})$, $\text{N}_2(\text{g})$, and $\text{SO}_2(\text{g})$. Chemical analysis of sulfur shows 67% is present as sulfides, 33% as organic sulfur, and trace amounts as sulfates.

gross heat of combustion: temperature was 25°C (77°F) and estimated standard deviation for three runs is less than 5 cal g^{-1} .

Sample I

$$\begin{aligned} q_v(\text{gross}) &= 2176.2 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 1209.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 5058.5 \text{ J g}^{-1} \end{aligned}$$

Sample II

$$\begin{aligned} q_v(\text{gross}) &= 2182.0 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 1212.2 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 5071.8 \text{ J g}^{-1} \end{aligned}$$

79CRA/ORN

OIL, SPENT SHALE; solid; Material came from the Anvil Points mine in Colorado and was ground mixed and split after experiment was completed to provide representative samples for analysis. To achieve complete combustion, samples were combined with benzoic acid in a 1:1 ratio, and combustion analysis indicated: $\text{H}_2\text{O}(\text{liq})$, $\text{CO}_2(\text{g})$, $\text{N}_2(\text{g})$, and $\text{SO}_2(\text{g})$. Chemical analysis shows that the sulfur present is primarily sulfides with traces of sulfates.

gross heat of combustion: temperature was 25°C (77°F) and estimated standard deviation for three runs is less than 5 cal g^{-1} .

Sample I

$$\begin{aligned} q_v(\text{gross}) &= -118.3 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= -65.7 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= -274.9 \text{ J g}^{-1} \end{aligned}$$

Sample II

$$\begin{aligned} q_v(\text{gross}) &= -27.7 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= -15.4 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= -64.4 \text{ J g}^{-1} \end{aligned}$$

79CRA/ORN

PEAT; solid; raw; highly organic soil containing partially decomposed vegetable matter and having more than 50% combustible content.

gross heat of combustion: assume values refer to room temperature; data are calculated to a dry basis.

sample 1; air-dried; moisture, 8.68%; volatile matter, 50.92%; fixed carbon, 23.79%; ash, 16.61%; sulfur, 0.99%.

$$\begin{aligned}q_v(\text{gross}) &= 8237 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4576 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19146 \text{ J g}^{-1}\end{aligned}$$

18POO

sample 2; brown fibrous; air-dried; moisture, 6.34%; ash, 7.93%; sulfur, 0.69%.

$$\begin{aligned}q_v(\text{gross}) &= 9920 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5511 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23058 \text{ J g}^{-1}\end{aligned}$$

sample 3; black; air-dried; moisture, 6.62%; ash, 24.44%; sulfur, 0.65%.

$$\begin{aligned}q_v(\text{gross}) &= 7695 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4275 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17887 \text{ J g}^{-1}\end{aligned}$$

sample 4; brown; air-dried; moisture, 12.10%; ash, 7.22%; sulfur, 0.83%.

$$\begin{aligned}q_v(\text{gross}) &= 8743 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4857 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20322 \text{ J g}^{-1}\end{aligned}$$

11DAV

Inorganic Materials

BENTONITE, PEMBINA; solid; a colloidal clay (aluminum silicate) containing a montmorillonite.

heat of dehydration: $\Delta H(\text{dehydration})$ is derived from endotherms in the differential thermal analysis (DTA) curve, neglecting endotherms around 110°C (230°F) at which adsorbed water is evolved. Two endothermic peaks appear in the curve giving peak temperatures of 408°C (766°F) and 663°C (1225°F).

$$\begin{aligned}\Delta H(\text{dehydration}) &= 52 \text{ Btu lb}^{-1} \\ \Delta H(\text{dehydration}) &= 29 \text{ cal g}^{-1} \\ \Delta H(\text{dehydration}) &= 121 \text{ J g}^{-1}\end{aligned}$$

54ALL

BENTONITE, WYOMING; solid; a colloidal clay (aluminum silicate) containing sodium montmorillonite, which swells 12-fold when wetted with water.

heat of dehydration: approximate dehydration temperature is 675°C (124°F). $\Delta H(\text{dehydration})$ is derived from endotherms in the differential thermal analysis (DTA) curve, neglecting endotherms around 110°C (230°F) at which adsorbed water is evolved.

$$\begin{aligned}\Delta H(\text{dehydration}) &= 79 \text{ Btu lb}^{-1} \\ \Delta H(\text{dehydration}) &= 44 \text{ cal g}^{-1} \\ \Delta H(\text{dehydration}) &= 184 \text{ J g}^{-1}\end{aligned}$$

54ALL

CEMENT HYDRATES; solid; general formula: $x\text{CaO} \cdot y\text{Al}_2\text{O}_3 \cdot z\text{CaSO}_4 \cdot m\text{CaCO}_3 \cdot n\text{H}_2\text{O}$.
(C=CaO, A=Al₂O₃, H=H₂O, Cs=CaSO₄, and Cc=CaCO₃).

heat of dehydration: gaseous water formed.

	temperature range		moles H ₂ O lost	ΔH (kcal gmol ⁻¹)	ΔH (kJ gmol ⁻¹)	ΔH (Btu lb mol ⁻¹)
	°C	°F				
C _{3.97} AH _{11.0}	120-200	248-392	4	48.9 ± 0.2	204.5 ± 0.8	87935 ± 3 4
	210-290	410-554	3.5	10.2 ± 0.2	42.7 ± 0.8	18361 ± 3 4
C _{2.97} AH _{5.96}	260-350	500-662	4.5	76.9 ± 1.#	321.7 ± 7.5	138331 ± 32 5
C _{3.51} ACs _{2.54} H _{30.4}	65-145	149-293	23	213.9 ± 3.1	895.0 ± 13.0	384850 ± 5590
C _{3.14} ACs _{0.94} H _{12.1}	95-125	203-257	1.6	2.75 ± 0.2	11.51 ± 0.8	4949 ± 3 4
	140-200	284-392	6	34.4 ± 0.7	143.9 ± 2.9	61877 ± 1247
	240-310	464-590	1.5	14.6 ± 0.6	61.1 ± 2.5	26273 ± 10 5
C _{3.53} ACcH _{8.1}	70-170	158-338	2	19.7 ± 2	82.4 ± 8	35432 ± 3440
	250-320	482-608	5	31.0 ± 0.5	129.7 ± 2.1	55771 ± 9 3
C _{1.97} AH _{12.9}	120-160	248-320	5.9	2.4 ± 0.7	10.0 ± 2.9	4300 ± 1247
	230-325	446-617	4.8	76.0 ± 5.8	318.0 ± 24.1	136740 ± 103 3
C _{2.19} AH _{9.3}	45-100	113-212	3	12.9 ± 2.7	54.0 ± 11.3	23220 ± 4859
	125-190	257-374	1.5	14.6 ± 2.3	61.1 ± 9.6	26273 ± 41 8
	250-300	482-572	3.5	6.0 ± 0.7	25.1 ± 2.9	10793 ± 12 7
C _{1.07} AH _{6.3}	120-190	248-374	2	11.2 ± 1.9	46.9 ± 7.9	20167 ± 33 7
	230-300	446-572	3	22.3 ± 1.0	93.3 ± 4.2	40119 ± 18 6
C _{1.03} AH _{3.98}	240-340	464-644	2.8	43.7 ± 2.7	182.8 ± 11.3	78604 ± 48 9

70HEN/STR

CLAY, CHINA; solid; Material is obtained by leaching weathered deposits of granitic rock to remove quartz and mica. Sample is composed mainly of kaolinite (Al₂O₃·2SiO₂·2H₂O) plus impurities.

heat of dehydration: approximate dehydration temperature is 547°C (1017°F).

ΔH (dehydration) is derived from endotherms in the differential thermal analysis (DTA) curve, neglecting endotherms around 110°C (230°F) at which adsorbed water is evolved.

$$\Delta H(\text{dehydration}) = 207 \text{ Btu lb}^{-1}$$

$$\Delta H(\text{dehydration}) = 115 \text{ cal g}^{-1}$$

$$\Delta H(\text{dehydration}) = 481 \text{ J g}^{-1}$$

54ALL

CLAY, HALLOYSITE (DJEBEL DEBAR); solid; Material is a clay mineral with a kaolinite composition.

heat of dehydration: approximate dehydration temperature is 544°C (1011°F). $\Delta H(\text{dehydration})$ is derived from endotherms in the differential thermal analysis (DTA) curve, neglecting endotherms around 110°C (230°F) at which adsorbed water is evolved.

$$\Delta H(\text{dehydration}) = 164 \text{ Btu lb}^{-1}$$

$$\Delta H(\text{dehydration}) = 91 \text{ cal g}^{-1}$$

$$\Delta H(\text{dehydration}) = 381 \text{ J g}^{-1}$$

54ALL

CLAY, K. PLASTIC KAOLIN; solid; Material is a clay mineral composed mainly of kaolinite (40% alumina, 55% silica plus impurities and water).

heat of dehydration: approximate dehydration temperature is 547°C (1017°F). $\Delta H(\text{dehydration})$ is derived from endotherms in the differential thermal analysis (DTA) curve, neglecting endotherms around 110°C (230°F) at which adsorbed water is evolved.

$$\Delta H(\text{dehydration}) = 187 \text{ Btu lb}^{-1}$$

$$\Delta H(\text{dehydration}) = 104 \text{ cal g}^{-1}$$

$$\Delta H(\text{dehydration}) = 435 \text{ J g}^{-1}$$

54ALL

CLAY, MOROCCAN NO. 4; solid; Material is a kaolin type mineral composed of a hydrated aluminum silicate with generalized formula $\text{Al}_2\text{O}_3\text{SiO}_2 \cdot x\text{H}_2\text{O}$, where x indicates a variable amount of water.

heat of dehydration: approximate dehydration temperature is 664°C (1227°F). $\Delta H(\text{dehydration})$ is derived from endotherms in the differential thermal analysis (DTA) curve, neglecting endotherms around 110°C (230°F) at which adsorbed water is evolved.

$$\Delta H(\text{dehydration}) = 41 \text{ Btu lb}^{-1}$$

$$\Delta H(\text{dehydration}) = 23 \text{ cal g}^{-1}$$

$$\Delta H(\text{dehydration}) = 96 \text{ J g}^{-1}$$

54ALL

CLAY, NEWTON ABBOT BALL; solid; Material is a white high-plasticity burning clay composed of hydrated aluminum silicate of generalized formula $\text{Al}_2\text{O}_3\text{SiO}_2 \cdot x\text{H}_2\text{O}$, where x indicates a variable amount of water.

heat of dehydration: approximate dehydration temperature is 542°C (1008°F). $\Delta\text{H}(\text{dehydration})$ is derived from endotherms in the differential thermal analysis (DTA) curve, neglecting endotherms around 110°C (230°F) at which adsorbed water is evolved.

$$\begin{aligned}\Delta\text{H}(\text{dehydration}) &= 128 \text{ Btu lb}^{-1} \\ \Delta\text{H}(\text{dehydration}) &= 71 \text{ cal g}^{-1} \\ \Delta\text{H}(\text{dehydration}) &= 297 \text{ J g}^{-1}\end{aligned}$$

54ALL

GLASS, PYREX; solid (Corning 7740); SiO_2 , 80.66%; B_2O_3 , 12.93%; Na_2O , 3.80%; Al_2O_3 , 2.14%; K_2O , 0.45%.

heat content: 373-850 K (212° - 1071°F)

$$\begin{aligned}q_T - q_{32} \text{ (Btu lb}^{-1}) &= -170.784 + 0.2325 (t + 459.67) + 2.44 \times 10^{-5} (t + 459.67)^2 \\ &\quad - 2.619 \times 10^{-4} (t + 459.67)^{-1} \text{ (t/}^\circ\text{F)} \\ q_T - q_{273.2} \text{ (cal g}^{-1}) &= -94.88 + 0.2325 T + 4.39 \times 10^{-5} T^2 + 8.083 \times 10^3 T^{-1} \text{ (K)} \\ q_T - q_{273.2} \text{ (J g}^{-1}) &= -396.98 + 0.9728 T + 1.837 \times 10^{-4} T^2 + 3.382 \times 10^4 T^{-1} \text{ (K)}\end{aligned}$$

specific heat:

173-293 K (-148° to 68°F)

$$\begin{aligned}C_p \text{ (Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= -0.1788 + 3.829 \times 10^{-4} T - 1.1728 \times 10^{-6} T^2 \\ C_p \text{ (cal g}^{-1} \text{ K}^{-1}) &= -0.245 + 2.63 \times 10^{-3} T - 3.80 \times 10^{-6} T^2 \\ C_p \text{ (J g}^{-1} \text{ K}^{-1}) &= -1.025 + 1.100 \times 10^{-2} T - 1.59 \times 10^{-5} T^2\end{aligned}$$

373-850 K (212° - 1071°F)

$$\begin{aligned}C_p \text{ (Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= 0.2325 + 4.878 \times 10^{-5} (t + 459.67) - 2.619 \times 10^{-4} (t + 459.67)^{-2} \\ C_p \text{ (cal g}^{-1} \text{ K}^{-1}) &= 0.2325 + 8.78 \times 10^{-5} T - 8.083 \times 10^3 T^{-2} \\ C_p \text{ (J g}^{-1} \text{ K}^{-1}) &= 0.9728 + 3.674 \times 10^{-4} T - 3.382 \times 10^4 T^{-2}\end{aligned}$$

68HAG/COO; 63GAT/KRE

GLASS, PYREX; liquid (Corning 7740); SiO₂, 80.66%; B₂O₃, 12.93%; Na₂O, 3.80%; Al₂O₃, 2.14%; K₂O, 0.46%.

specific heat: over the temperature range 850-1200 K (1071°-1701°F), the specific heat appears to be independent of temperature.

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.3471 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.3471 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.4523 \end{aligned}$$

heat content: 850-1200 K (1071°-1701°F)

$$\begin{aligned} q_T - q_{32}(\text{Btu lb}^{-1}) &= -114.55 + 0.3471 T (^\circ\text{F}) \\ q_T - q_{273.2}(\text{cal g}^{-1}) &= -152.28 + 0.3471 T (\text{K}) \\ q_T - q_{273.2}(\text{J g}^{-1}) &= -637.14 + 1.4523 T (\text{K}) \end{aligned}$$

68HAG/COO

GLASS, SODA-LIME; solid (Lillie 1); SiO₂, 73.59%; Na₂O, 16.65%; CaO, 9.76%.

specific heat: 273-850 K (32°-1071°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.1347 + 1.0733 \times 10^{-4} (t + 459.67) + 7.86 \times 10^3 (t + 459.67)^{-2} \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.1347 + 1.932 \times 10^{-4} T + 2.423 \times 10^3 T^{-2} \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.5636 + 8.083 \times 10^{-4} T + 1.0138 \times 10^4 T^{-2} \end{aligned}$$

heat content: 273-850 K (32°-1071°F)

$$\begin{aligned} q_T - q_{32}(\text{Btu lb}^{-1}) &= -65.466 + 0.1347 (t + 459.67) + 5.36 \times 10^{-5} (t + 459.67)^2 \\ &\quad - 7.86 \times 10^3 (t + 459.67)^{-1} (t/^\circ\text{F}) \\ q_T - q_{273.2}(\text{cal g}^{-1}) &= -36.37 + 0.1347 T + 9.66 \times 10^{-5} T^2 - 2.423 \times 10^3 T^{-1} (\text{K}) \\ q_T - q_{273.2}(\text{J g}^{-1}) &= -152.17 + 0.5636 T + 4.042 \times 10^{-4} T^2 - 1.0138 \times 10^4 T^{-1} (\text{K}) \end{aligned}$$

68HAG/COO

GLASS, SODA-LIME; liquid (Lillie 1); SiO₂, 73.59%; Na₂O, 16.65%; CaO, 9.76%.

specific heat: over the temperature range 850 to 1200 K (1071°-1701°F), the specific heat appears to be independent of temperature.

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.3570 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.3570 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.4937 \end{aligned}$$

heat content: 850-1200 K (1071°-1701°F)

$$\begin{aligned} q_T - q_{32}(\text{Btu lb}^{-1}) &= -121.76 + 0.3570 T (^\circ\text{F}) \\ q_T - q_{273.2}(\text{cal g}^{-1}) &= -158.81 + 0.3570 T (\text{K}) \\ q_T - q_{273.2}(\text{J g}^{-1}) &= -664.46 + 1.4937 T (\text{K}) \end{aligned}$$

68HAG/COO

GLASS, VYCOR; solid; SiO₂, 96.3%; B₂O₃, 2.9%; Al₂O₃, 0.4%; other metal oxides, 0.4%.

specific heat: 273-579 K (32°-583°F), mean values

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.16053 + 7.962 \times 10^{-5} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.12393 + 1.4333 \times 10^{-4} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.51852 + 5.9969 \times 10^{-4} T \end{aligned}$$

68CAM/VAN

PORCELAIN; solid; a mixture of clays, quartz, and feldspar, usually containing at least 25% aluminum. Sample 1: SiO₂, 65.14%; Al₂O₃, 28.76%; Fe₂O₃, 1.08%; K₂O, 3.61%; MgO, 1.21%; sample 2: SiO₂, 41.1%; Al₂O₃, 57.1%; Fe₂O₃, 0.3%; MgO, 0.5%; CaO, traces.

specific heat: 273-1873 K (32°-2912°F)

sample 1

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.1711 + 1.2532 \times 10^{-4} T - 2.3804 \times 10^{-8} T^2 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.10848 + 2.6497 \times 10^{-4} T - 7.7124 \times 10^{-8} T^2 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.45388 + 1.10863 \times 10^{-3} T - 3.2269 \times 10^{-7} T^2 \end{aligned}$$

sample 2

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.23608 + 6.2509 \times 10^{-5} T - 1.7546 \times 10^{-9} T^2 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.20698 + 1.1542 \times 10^{-4} T - 5.685 \times 10^{-9} T^2 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.86600 + 4.8292 \times 10^{-4} T - 3.2319 \times 10^{-8} T^2 \end{aligned}$$

28JAE/ROS

ZEOLITE, SILVER A; solid; synthetic ion-exchange resin; hydrated aluminum silicates containing alkali or alkaline earth metals; 90% Ag⁺ relative to Na⁺.

specific heat: at 310 K (98°F); nearly all water eliminated by heating in N₂ at 500°C (932°F).

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.205 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.205 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.858 \end{aligned}$$

72VUC/VUC

ZEOLITE, SODIUM A; solid; synthetic ion-exchange resin; hydrated aluminum silicates containing alkali or alkaline earth metals.

specific heat: at 310 K (98°F); nearly all water eliminated by heating in N₂ at 500°C (932°F).

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= 0.227 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.227 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.950\end{aligned}$$

72VUC/VUC

Paper

BROWN PAPER; solid; ultimate analysis in percent by weight: carbon, 44.90%; hydrogen, 6.08%; oxygen, 47.84%; nitrogen, 0.00%; sulfur, 0.11%; ash, 1.07%; proximate analysis as received in percent by weight: moisture, 5.83%; volatile matter, 83.92%; fixed carbon, 9.24%; ash, 1.01%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 7261 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4034 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16877 \text{ J g}^{-1}\end{aligned}$$

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 7711 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4284 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17924 \text{ J g}^{-1}\end{aligned}$$

66KAI

CORRUGATED BOX; solid; ultimate analysis in percent by weight: carbon, 43.73%; hydrogen, 5.70%; oxygen, 44.93%; nitrogen, 0.09%; sulfur, 0.21%; ash, 5.34%; proximate analysis as received in percent by weight: moisture, 5.20%; volatile matter, 77.47%; fixed carbon, 12.27%; ash, 5.06%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 7047 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3915 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16382 \text{ J g}^{-1}\end{aligned}$$

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 7434 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4130 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17280 \text{ J g}^{-1}\end{aligned}$$

66KAI

FOOD CARTONS; solid; ultimate analysis in percent by weight: carbon, 44.74%; hydrogen, 6.10%; oxygen, 41.92%; nitrogen, 0.15%; sulfur, 0.16%; ash, 6.93%; proximate analysis as received in percent by weight: moisture, 6.11%; volatile matter, 75.59%; fixed carbon, 11.80%; ash, 6.50%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 7263 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4035 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16882 \text{ J g}^{-1}\end{aligned}$$

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 7735 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4297 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17980 \text{ J g}^{-1}\end{aligned}$$

66KAI

JUNK MAIL; solid; ultimate analysis in percent by weight: carbon, 37.87%; hydrogen, 5.41%; oxygen, 42.74%; nitrogen, 0.17%; sulfur, 0.09%; ash, 13.72%; proximate analysis as received in percent by weight: moisture, 4.56%; volatile matter, 73.32%; fixed carbon, 9.03%; ash, 13.09%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 6093 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3385 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 14161 \text{ J g}^{-1}\end{aligned}$$

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 6383 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3546 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 14835 \text{ J g}^{-1}\end{aligned}$$

66KAI

MAGAZINE; solid; ultimate analysis in percent by weight: carbon, 32.91%; hydrogen, 4.95%; oxygen, 38.55%; nitrogen, 0.07%; sulfur, 0.09%; ash, 23.43%; proximate analysis as received in percent by weight: moisture, 4.11%; volatile matter, 66.39%; fixed carbon, 7.03%; ash, 22.47%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 5258 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 2921 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 12221 \text{ J g}^{-1}\end{aligned}$$

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 5483 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3046 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 12746 \text{ J g}^{-1}\end{aligned}$$

66KAI

NEWSPRINT; solid; ultimate analysis in percent by weight: carbon, 49.14%; hydrogen, 6.10%; oxygen, 43.03%; nitrogen, 0.05%; sulfur, 0.16%; ash, 1.52%; proximate analysis as received in percent by weight: moisture, 5.97%; volatile matter, 81.12%; fixed carbon, 11.48%; ash, 1.43%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 7979 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4433 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18548 \text{ J g}^{-1}\end{aligned}$$

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 8485 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4714 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19724 \text{ J g}^{-1}\end{aligned}$$

66KAI

PLASTIC COATED PAPER; solid; ultimate analysis in percent by weight: carbon, 45.30%; hydrogen, 6.17%; oxygen, 45.50%; nitrogen, 0.18%; sulfur, 0.08%; ash, 2.77%; proximate analysis as received in percent by weight: moisture, 4.71%; volatile matter, 84.20%; fixed carbon, 8.45%; ash, 2.64%.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 7346 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4081 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17075 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}q_v(\text{gross}) &= 7708 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4282 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17917 \text{ J g}^{-1}\end{aligned}$$

66KAI

WAXED MILK CARTONS; solid; ultimate analysis in percent by weight: carbon, 59.18%; hydrogen, 9.25%; oxygen, 30.13%; nitrogen, 0.12%; sulfur, 0.10%; ash, 1.22%; proximate analysis as received in percent by weight: moisture, 3.45%; volatile matter, 90.92%; fixed carbon, 4.46%; ash, 1.17%.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 11330 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6297 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 26347 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}q_v(\text{gross}) &= 11740 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6522 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 27289 \text{ J g}^{-1}\end{aligned}$$

66KAI

Plant Materials (Non-Woody)

ALGAE; solid; chlorophyll-bearing organisms occurring in both salt and fresh water; contain minerals, proteins, lipids, amino acids; a source of iodine.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

Ulva rigida (green alga)

$$\begin{aligned} q_v(\text{gross}) &= 6750 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3750 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 15690 \text{ J g}^{-1} \end{aligned}$$

Fucus distichus (brown)

$$\begin{aligned} q_v(\text{gross}) &= 6174 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3430 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 14351 \text{ J g}^{-1} \end{aligned}$$

Alaria nana (brown)

$$\begin{aligned} q_v(\text{gross}) &= 5850 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3250 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 13598 \text{ J g}^{-1} \end{aligned}$$

71PAI

ARCHANGEL (WOOD BETONY OR BLIND NETTLE); *Stachys sylvatica*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned} q_v(\text{gross}) &= 7393 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4107 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17184 \text{ J g}^{-1} \end{aligned}$$

73PAU/BRE

BIG SAGEBRUSH; *Artemisia tridentata*; solid; Samples of current year's annual growth and woody tissue of large rangeland shrubs were collected from 11 sites in several intermountain states. Surface soil pH = 7.2 - 7.7; soil class is sand-silt loam. Mean content of current year's growth: ash, 6.7%; sulfur, 0.17%; moisture, 56%. Mean content of woody tissue: ash, 3.1%; sulfur, 0.03%; moisture, 25%.

gross heat of combustion: oven-dry weight; assume values refer to room temperature; value is mean of an average of values from 3 to 5 plants from each site.

current year's growth

$$\begin{aligned} q_v(\text{gross}) &= 8456 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4698 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19656 \text{ J g}^{-1} \end{aligned}$$

woody tissue

$$\begin{aligned} q_v(\text{gross}) &= 8350 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4639 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19410 \text{ J g}^{-1} \end{aligned}$$

82VAN/BAR

Plant Materials (Non-Woody)

BIG SAGEBRUSH, FOLIAGE; *Artemisia tridentata*; solid; freeze-dried to < 10% moisture content. Composition is ash = 7.10% and char yield = 25.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 9440 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5240 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21940 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 14350 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7970 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33350 \text{ J g}^{-1}\end{aligned}$$

82SUS

BIG SAGEBRUSH, STEMS; *Artemisia tridentata*; solid; Stem samples were branches less than 0.25 inch diameter with foliage removed and freeze dried to < 10% moisture content. Composition is ash = 2.83% and char yield = 27.1%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 8590 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4770 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19960 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 14420 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8010 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33520 \text{ J g}^{-1}\end{aligned}$$

82SUS

BRACKEN FERN, FRONDS; *Pteridium aquilinum*; solid; Cured samples were air-dried at room temperature. Composition is ash = 9.24% and char yield = 38.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 8620 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4790 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20030 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13190 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7330 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 30650 \text{ J g}^{-1}\end{aligned}$$

82SUS

BROAD-LEAVED STITCHWORT (WOOD STARWORT); *Stellaria nemorum*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 6458 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3588 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 15012 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

BULBIFEROUS TOOTHWORT (TOOTH-CRESS); *Cardamine bulbifera*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has a vernal (spring) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7378 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4099 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17150 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

CATTAILS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 71.57, ash content = 7.90, and fixed carbon = 20.53. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 42.99, hydrogen = 5.25, oxygen = 42.47, nitrogen = 0.74, sulfur = 0.04, chlorine = 0.38, and residue (ash) = 8.13.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7662 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4257 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17810 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7017 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3898 \text{ cal g}^{-1} \\q_v(\text{net}) &= 16310 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

CHEATGRASS, CURED; *Bromus tectorum*; solid; Material is aerial plant air-dried at room temperature. Composition is ash = 6.46% and char yield = 21.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 8330 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4630 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19360 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 14100 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7830 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32770 \text{ J g}^{-1} \end{aligned}$$

82SUS

CLOVERROOT (HERB BENNET); *Geum urbanum*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned} q_v(\text{gross}) &= 7418 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4121 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17242 \text{ J g}^{-1} \end{aligned}$$

73PAU/BRE

COCKS-FOOT GRASS; *Dactylis polygama*; solid; Material is a herb, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content = 12.4%, was determined at 500°C (932°F) while the temperature was increased stepwise.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature, the number of measurements is 3.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
aboveground living material				
$q_v(\text{gross}) =$	7636	8725	36.2	Btu lb ⁻¹
$q_v(\text{gross}) =$	4242	4847	20.1	cal g ⁻¹
$q_v(\text{gross}) =$	17749	20280	84.1	J g ⁻¹

(more)

COCKS-FOOT GRASS - Continued

	dry weight basis	ash-free dry weight basis	std dev. of mean	
aboveground dead material				
$q_v(\text{gross}) =$	7306	8680	72.9	Btu lb ⁻¹
$q_v(\text{gross}) =$	4059	4822	40.5	cal g ⁻¹
$q_v(\text{gross}) =$	16983	20175	169	J g ⁻¹
roots				
$q_v(\text{gross}) =$	7681	8620	85.1	Btu lb ⁻¹
$q_v(\text{gross}) =$	4267	4789	47.3	cal g ⁻¹
$q_v(\text{gross}) =$	17853	20037	198	J g ⁻¹

75PAP

COLTSFOOT; *Tussilago farfara*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$q_v(\text{gross}) = 6595 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3664 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 15330 \text{ J g}^{-1}$$

73PAU/BRE

COWSLIP LUNGWORT; *Pulmonaria rubra*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$q_v(\text{gross}) = 7200 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4000 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16736 \text{ J g}^{-1}$$

73PAU/BRE

Plant Materials (Non-Woody)

DOG VIOLET; *Viola reichenbachiana*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7171 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3984 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16669 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

ENCHANTER'S NIGHTSHADE; *Circaea lutetiana*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7690 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4272 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17874 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

FOURWING SALTBUSH; *Atriplex canescens*; solid; Samples of current year's annual growth and woody tissue of large rangeland shrubs were collected from 7 sites in several intermountain states. Surface soil pH = 7.0 - 8.2; soil class is sand-silt loam. Mean content of current year's growth: ash, 9.9%; sulfur, 0.35%; moisture, 57.3%. Mean content of woody tissue: ash, 3.5%; sulfur, 0.08%; moisture, 29.5%.

gross heat of combustion: oven-dry weight; assume values refer to room temperature; value is mean of an average of values from 3 to 5 plants from each site.

current year's growth

$$\begin{aligned}q_v(\text{gross}) &= 7765 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4315 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18050 \text{ J g}^{-1}\end{aligned}$$

woody tissue

$$\begin{aligned}q_v(\text{gross}) &= 8109 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4505 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18849 \text{ J g}^{-1}\end{aligned}$$

82VAN/BAR

GALLBERRY, FOLIAGE; *Plex glabra*; solid; freeze dried to < 10% moisture content.

Composition is ash = 2.27% and char yield = 25.4%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 9960 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5530 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23140 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 14460 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8030 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33610 \text{ J g}^{-1}\end{aligned}$$

82SUS

GERMANDER SPEEDWELL (ANGEL'S-EYE); *Veronica chamaedrys*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7783 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4324 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18092 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

GLABER CRESS; *Cardamine glanduligera*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has a vernal (spring) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7574 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4208 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17606 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

GRASS, LAWN CLIPPINGS; solid; ultimate analysis: carbon, 48.18%; hydrogen, 5.96%; oxygen, 36.43%; nitrogen, 4.46%; sulfur, 0.42%; ash, 6.55%; proximate analysis on an as received basis: moisture, 75.24%; volatile matter, 18.64%; fixed carbon, 4.50%; ash, 1.62%.

gross heat of combustion: assume values refer to room temperature.

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 8312 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4618 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19322 \text{ J g}^{-1}\end{aligned}$$

as received

$$\begin{aligned}q_v(\text{gross}) &= 2059 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 1144 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 4787 \text{ J g}^{-1}\end{aligned}$$

66KAI

GREASEWOOD; *Sarcobatus vermiculatus*; solid; Samples of current year's annual growth and woody tissue of large rangeland shrubs were collected from 3 sites in several intermountain states. Surface soil pH = 7.9 - 9.5; soil class is sandy loam-clay loam. Mean content of current year's growth: ash, 20.2%; sulfur, 0.46%; moisture, 0.46%. Mean content of woody tissue: ash, 1.7%; sulfur, 0.24%; moisture, 34.0%.

gross heat of combustion: oven-dry weight; assume values refer to room temperature; value is mean of an average of values from 3 to 5 plants from each site.

current year's growth

$$\begin{aligned}q_v(\text{gross}) &= 6599 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3666 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 15339 \text{ J g}^{-1}\end{aligned}$$

woody tissue

$$\begin{aligned}q_v(\text{gross}) &= 8507 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4726 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19774 \text{ J g}^{-1}\end{aligned}$$

82VAN/BAR

HERB ROBERT (RED ROBIN); *Geranium robertianum*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7112 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3951 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16531 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

HERBS, ALPINE TUNDRA; solid; Samples of 20 species of herbs were collected in the alpine tundra of Mt. Washington, N.H. Mean lipid content was $1.43 \pm 0.1\%$ of volatile-free dry weight. Samples ground and oven-dried at 80°C (176°F).

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$\begin{aligned}q_v(\text{gross}) &= 8282 \pm 52 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4601 \pm 29 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19251 \pm 121 \text{ J g}^{-1}\end{aligned}$$

62BLI

IDAHO FESCUE, CURED; *Festuca idahoensis*; solid; Material is aerial plant air dried at room temperature. Composition is ash = 9.45% and char yield = 24.6%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 8670 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4820 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20160 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 14340 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7970 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33340 \text{ J g}^{-1}\end{aligned}$$

82SUS

IRISH SHAMROCK (EUROPEAN WOOD SORREL); *Oxalis acetosella*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7783 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4324 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18092 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

Plant Materials (Non-Woody)

JUPITER'S-DISTAFF; *Salvia glutinosa*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 8158 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4532 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18962 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

LADY FERN; *Athyrium filix-femina*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7335 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4075 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17050 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

LETTUCE MURALIS; *Mycelis muralis*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 8042 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4468 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18694 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

MALE FERN; *Dryopteris filix-mas*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7808 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4338 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18150 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

MEADOW-RUE ISOPYRUM; *Isopyrum thalictroides*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has a vernal (spring) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7969 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4427 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18523 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

MELIC GRASS; *Melica uniflora*; solid; Material is a herb, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of aboveground living material = 8.1%; aboveground dead material = 12.2%; roots = 7.6%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature, the number of measurements is 3.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
aboveground living material				
$q_v(\text{gross}) =$	7709	8397	7.7	Btu lb ⁻¹
$q_v(\text{gross}) =$	4283	4665	4.3	cal g ⁻¹
$q_v(\text{gross}) =$	17920	19518	18	J g ⁻¹

(more)

MELIC GRASS - Continued

	dry weight basis	ash-free dry weight basis	std dev. of mean	
aboveground dead material				
$q_v(\text{gross}) =$	7657	8730	57.6	Btu lb ⁻¹
$q_v(\text{gross}) =$	4254	4850	32.0	cal g ⁻¹
$q_v(\text{gross}) =$	17799	20292	134	J g ⁻¹
roots				
$q_v(\text{gross}) =$	7972	8631	15	Btu lb ⁻¹
$q_v(\text{gross}) =$	4429	4795	8.5	cal g ⁻¹
$q_v(\text{gross}) =$	18531	20062	36	J g ⁻¹

75PAP

MERCURIALIS PERENNIS; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period, and is a European poisonous plant with the foliage yielding an unstable blue dye.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$q_v(\text{gross}) = 6709 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3727 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 15594 \text{ J g}^{-1}$$

73PAU/BRE

MOSSES, ALPINE TUNDRA; solid; Samples of 7 species of mosses were collected in the alpine tundra of Mt. Washington, N.H. Mean lipid content was 1.0% of the volatile-free dry weight. Samples were ground and air-dried at 80°C (176°F).

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 7938 \pm 130 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4410 \pm 70 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18450 \pm 293 \text{ J g}^{-1}$$

62BLI

MOUNTAIN RUSH; *Carex montana*; solid; Material is a herb, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of aboveground living material = 8.4%; aboveground dead material = 14.7%; roots = 6.3%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature, the number of measurements is 3.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
aboveground living material				
$q_v(\text{gross}) =$	7580	8689	5.6	Btu lb ⁻¹
$q_v(\text{gross}) =$	4222	4827	3.1	cal g ⁻¹
$q_v(\text{gross}) =$	17667	20196	13	J g ⁻¹
aboveground dead material				
$q_v(\text{gross}) =$	7092	8305	13.2	Btu lb ⁻¹
$q_v(\text{gross}) =$	3940	4614	73.5	cal g ⁻¹
$q_v(\text{gross}) =$	16485	19305	308	J g ⁻¹
roots				
$q_v(\text{gross}) =$	8042	8575	140	Btu lb ⁻¹
$q_v(\text{gross}) =$	4468	4764	77.5	cal g ⁻¹
$q_v(\text{gross}) =$	18694	19933	324	J g ⁻¹

75PAP

PLANTS, FLOWER GARDEN; solid; ultimate analysis: carbon, 46.65%; hydrogen, 6.61%; oxygen, 40.18%; nitrogen, 1.21%; sulfur, 0.26%; ash, 5.09%; proximate analysis as received: moisture, 53.94%; volatile matter, 35.64%; fixed carbon, 8.08%; ash, 2.34%.

gross heat of combustion: assume values refer to room temperature.

as received	dry basis
$q_v(\text{gross}) = 3699 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 8032 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 2055 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 4462 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 8599 \text{ J g}^{-1}$	$q_v(\text{gross}) = 18671 \text{ J g}^{-1}$

66KAI

Plant Materials (Non-Woody)

PLANTS, VASCULAR AQUATIC; solid; plants taken from Par Pond, U.S. AEC Savannah River Plant, near Aiken, S.C.; samples dried at 60°C (140°F) and pulverized to pass 40 mesh screen.

gross heat of combustion: assume values refer to room temperature.

Species	Protein Content g (100 g dry wt.)	(Btu lb ⁻¹)	q _v (gross) (cal g ⁻¹)	(J g ⁻¹)
<i>Typha latifolia</i>	4.0	7672	4262	17832
<i>Hydrotrida carolinensis</i>	10.5	7304	4058	16979
<i>Brasenia schreberi</i>	10.9	7247	4026	16845
<i>Utricularia inflata</i>	11.4	7241	4023	16832
<i>Nelumbo lutea</i>	12.1	7609	4227	17686
<i>Myriophyllum heterophyllum</i>	13.5	7130	3961	16573
<i>Eleocharis acicularis</i>	14.1	7661	4256	17807
<i>Najas guadalupensis</i>	14.4	7052	3918	16393
<i>Nymphaea odorata</i>	14.6	7524	4180	17489
<i>Ceratophyllum demersum</i>	17.1	7031	3906	16343
<i>Nuphar advena</i>	21.6	7767	4315	18054

70BOY

RUBBER RABBITBRUSH; *Chrysothamnus nauseosus*; solid; Samples of current year's annual growth and woody tissue of large rangeland shrubs were collected from 6 sites in several intermountain states. Surface soil pH = 7.5 - 7.9; solid class is sandy-clay loam. Mean content of current year's growth: ash, 7.4%; sulfur, 0.20%; moisture, 55.0%. Mean content of woody tissue: ash, 2.7%; sulfur, 0.04%; moisture, 44.7%.

gross heat of combustion: oven-dry weight; assume values refer to room temperature; value is mean of an average of values from 3 to 5 plants from each site.

current year's growth

$$q_v(\text{gross}) = 8698 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4832 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 20217 \text{ J g}^{-1}$$

woody tissue

$$q_v(\text{gross}) = 8420 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4678 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19573 \text{ J g}^{-1}$$

82VAN/BAR

SAW-PALMETTO, FRONDS; *Serenoa repens*; solid; Samples were freeze dried to < 10% moisture content. Composition is ash = 5.37% and char yield = 33.3%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$q_v(\text{gross}) = 9150 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5080 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 21270 \text{ J g}^{-1}$$

char (from 500°C heating)

$$q_v(\text{gross}) = 13890 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7720 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 32290 \text{ J g}^{-1}$$

82SUS

SEDGE GRASS; *Carex michelii*; solid; Material is a herb, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of aboveground living material = 9.0%; aboveground dead material = 10.6%; roots = 8.3%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature, the number of measurements is 3.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
aboveground living material				
$q_v(\text{gross}) =$	7817	8492	6.3	Btu lb ⁻¹
$q_v(\text{gross}) =$	4343	4718	3.5	cal g ⁻¹
$q_v(\text{gross}) =$	18171	19740	15	J g ⁻¹
aboveground dead material				
$q_v(\text{gross}) =$	7893	8827	38.7	Btu lb ⁻¹
$q_v(\text{gross}) =$	4385	4904	21.5	cal g ⁻¹
$q_v(\text{gross}) =$	18347	20518	90.0	J g ⁻¹
roots				
$q_v(\text{gross}) =$	7983	8707	67.1	Btu lb ⁻¹
$q_v(\text{gross}) =$	4435	4837	37.3	cal g ⁻¹
$q_v(\text{gross}) =$	18556	20238	156	J g ⁻¹

75PAP

SHRUBS, DECIDUOUS; ALPINE TUNDRA; solid; Samples of 9 species of shrubs were collected in the alpine tundra of Mt. Washington, N.H. Mean lipid content was 1.97 ± 0.3% of the volatile-free dry weight. Samples were ground and oven-dried at 80°C (176°F).

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 8878 \pm 89 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4932 \pm 33 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 20635 \pm 138 \text{ J g}^{-1}$$

62BLI

Plant Materials (Non-Woody)

SHRUBS, EVERGREEN; ALPINE TUNDRA; solid; Samples of 11 species of shrubs were collected in the alpine tundra of Mt. Washington, N.H. Mean lipid content was $3.72 \pm 0.5\%$ of the volatile-free dry weight. Samples were ground and oven-dried at 80°C (176°F).

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$\begin{aligned}q_v(\text{gross}) &= 9176 \pm 86 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5098 \pm 48 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21330 \pm 201 \text{ J g}^{-1}\end{aligned}$$

62BLI

SHRUBS, EVERGREEN; CUTTINGS; solid; ultimate analysis: carbon, 48.51%; hydrogen, 6.54%; oxygen, 40.44%; nitrogen, 1.71%; sulfur, 0.19%; ash, 2.61%; proximate analysis as received: moisture, 69.00%; volatile matter, 25.18%; fixed carbon, 5.01%; ash, 0.81%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned}q_v(\text{gross}) &= 2709 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 1505 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 6299 \text{ J g}^{-1}\end{aligned}$$

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 8741 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4856 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20318 \text{ J g}^{-1}\end{aligned}$$

66KAI

SOW-TEAT STRAWBERRY (WOODLAND STRAWBERRY); *Fragaria vesca*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7538 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4188 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17523 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

SPREADING RABBITBRUSH; *Chrysothamnus linifolius*; solid; Samples of current year's annual growth and woody tissue of large rangeland shrubs were collected from 2 sites in several intermountain states. Surface soil pH = 7.3 - 7.7; soil class is loamy sand-silt loam. Mean moisture content of current year's growth, 59.2%; of woody tissue, 52.7%.

gross heat of combustion: oven-dry weight; assume values refer to room temperature; value is mean of an average of values from 3 to 5 plants from each site.

current year's growth

woody tissue

$$\begin{aligned}q_v(\text{gross}) &= 8062 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4479 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18740 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}q_v(\text{gross}) &= 8206 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4559 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19075 \text{ J g}^{-1}\end{aligned}$$

82VAN/BAR

SPURGE ALMOND; *Euphorbia amygdaloides*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 8069 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4483 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18757 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

STINGING NETTLE; *Urtica dioica*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 6847 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3804 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 15916 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

SUDAN GRASS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 72.75, ash content = 8.65, and fixed carbon = 18.60. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 44.58, hydrogen = 5.35, oxygen = 39.18, nitrogen = 1.21, sulfur = 0.08, chlorine = 0.13, and residue (ash) = 9.47.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7447 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4156 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17390 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7017 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 3898 \text{ cal g}^{-1} \\q_v(\text{net}) &= 16310 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

SWEET WOODRUFF; *Galium odoratum*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7281 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4045 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16924 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

TALL OXEYE; *Telekia speciosa*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7634 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4241 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17744 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

TOUCH-ME-NOT; *Impatiens noli-tangere*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 7963 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4424 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18510 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

WHITE BUTTERBUR; *Petasites albus*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 6802 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3779 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 15811 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

WINDFLOWER (WOOD ANEMONE); *Anemone nemorosa*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has a vernal (spring) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned}q_v(\text{gross}) &= 8134 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4519 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18907 \text{ J g}^{-1}\end{aligned}$$

73PAU/BRE

Plant Materials (Non-Woody)

WOOD BLUEGRASS; *Poa nemoralis*; solid; Material is a herb, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of aboveground living material = 6.0%; aboveground dead material = 8.7%; roots = 11.0%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature, the number of measurements is 3.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
aboveground living material				
$q_v(\text{gross}) =$	7884	8390	56.3	Btu lb ⁻¹
$q_v(\text{gross}) =$	4380	4661	31.3	cal g ⁻¹
$q_v(\text{gross}) =$	18326	19502	131	J g ⁻¹
aboveground dead material				
$q_v(\text{gross}) =$	7888	8636	27.0	Btu lb ⁻¹
$q_v(\text{gross}) =$	4382	4798	15.0	cal g ⁻¹
$q_v(\text{gross}) =$	18334	20075	62.8	J g ⁻¹
roots				
$q_v(\text{gross}) =$	8050	9025	82.6	Btu lb ⁻¹
$q_v(\text{gross}) =$	4472	5014	45.9	cal g ⁻¹
$q_v(\text{gross}) =$	18711	20979	192	J g ⁻¹

75PAP

WOOD SEDGE; *Carex sylvatica*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$q_v(\text{gross}) = 7515 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4175 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 17468 \text{ J g}^{-1}$$

73PAU/BRE

YELLOW ARCHANGEL (DEAD NETTLE); *Lamium galeobdolon*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has an aestival (summer) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned} q_v(\text{gross}) &= 7879 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4377 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18313 \text{ J g}^{-1} \end{aligned}$$

73PAU/BRE

YELLOW WOOD ANEMONE; *Anemone ranunculoides*; solid; Material is an integral part of the ecosystem at the herbaceous layer level of the mixed fir and beech forest in the Pulmonario (rubro) Abieti-Fagetum area of the Bucegi mountains (two different stations) in Romania. The plants have the following constitution: 33% of the weight is represented by the stem axis and 67% by leaves. The species has a vernal (spring) type vegetation period.

gross heat of combustion: assume values refer to room temperature and values are calculated to a dry basis.

$$\begin{aligned} q_v(\text{gross}) &= 8158 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4532 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18962 \text{ J g}^{-1} \end{aligned}$$

73PAU/BRE

Polymers and Plastics

ARALDITE; solid; proprietary trade name for a series of epoxy resins used for casting, encapsulating, laminating, surface coating and as an adhesive.

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
1.5 -456.7	0.000014	0.000014	0.00006
2 -455.8	0.000057	0.000057	0.00024
3 -454	0.00021	0.00021	0.00089
4 -452	0.0054	0.0054	0.00225
6 -448.6	0.0020	0.0020	0.0082
8 -445	0.0040	0.0040	0.0169
10 -441.4	0.0065	0.0065	0.0272
15 -432.4	0.0130	0.0130	0.0542
20 -423.4	0.0194	0.0194	0.0811

54PAR/QUA

BAKELITE VARNISH, FORMITE VIII05; solid; trademark for synthetic resin of the phenol-formaldehyde type.

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
4 -452	0.0011	0.0011	0.0046
6 -448.6	0.0021	0.0021	0.0086
8 -445	0.0032	0.0032	0.0134
10 -441.4	0.0046	0.0046	0.0192
15 -432.4	0.0100	0.0100	0.0418
20 -423.4	0.0159	0.0159	0.0667
30 -405.4	0.029	0.029	0.121
40 -387.4	0.043	0.043	0.179
50 -369.4	0.057	0.057	0.237
70 -333.4	0.083	0.083	0.347
90 -297.4	0.017	0.017	0.449

53HIL/SMI

BUTADIENE-STYRENE COPOLYMER, GL-622; solid; composition: carbon, 90.100%; hydrogen, 9.170%; sulfur, 0.081%; oxygen, 0.14%; ash, 0.111%; styrene, 42.98%; phenyl- β -naphthylamine, 0.1%; polymerized at 50°C (122°F).

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
5 -450	0.00081	0.00081	0.0034
50 -370	0.076	0.076	0.318
100 -280	0.136	0.136	0.569
150 -190	0.190	0.190	0.794
200 -100	0.244	0.244	1.022
220 -64	0.268	0.268	1.122
255 -1	0.405	0.405	1.694

for temperature range: 255-330 K (0°-135°F)

$$C_p(\text{Btu lb}^{-1} \text{ °F}^{-1}) = 0.506 + 2.77 \times 10^{-5} T + 3.688 \times 10^{-7} T^2$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.316 + 4.37 \times 10^{-5} T + 1.195 \times 10^{-6} T^2$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 1.322 + 1.83 \times 10^{-4} T + 5.000 \times 10^{-6} T^2$$

55FUR/McC

BUTADIENE-STYRENE COPOLYMER, X-454; solid; composition: carbon, 88.869%; hydrogen, 10.872%; sulfur, 0.056%; oxygen, 0.235%; ash, 0.18%; styrene, 8.58%; phenyl- β -naphthylamine, 0.1%; polymerized at 5°C (36°F).

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
50 -370	0.084	0.084	0.351
100 -280	0.153	0.153	0.464
150 -190	0.220	0.220	0.92
200 -100	0.373	0.373	1.56
250 -10	0.423	0.423	1.77
300 80	0.464	0.464	1.94
330 134	0.485	0.485	2.03

53bFUR/McC

BUTADIENE-STYRENE COPOLYMER, X-478; solid; composition: carbon, 89.443%; hydrogen, 10.4008%; sulfur, 0.048%; oxygen, 0.15%; ash, 0.098%; styrene, 22.61%; phenyl- β -naphthylamine, 0.1%; polymerized at 5°C (41°F).

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
15 -433	0.016	0.016	0.067
50 -370	0.081	0.081	0.338
100 -280	0.147	0.147	0.617
150 -190	0.209	0.209	0.874
195 -109	0.262	0.262	1.096
225 -55	0.405	0.405	1.693

225-330 K (-54° to 135°F)

$$C_p \text{ (Btu lb}^{-1} \text{ °F}^{-1}) = 0.4228 + 3.812 \times 10^{-5} T + 3.483 \times 10^{-7} T^2$$

$$C_p \text{ (cal g}^{-1} \text{ K}^{-1}) = 0.3337 + 6.29 \times 10^{-5} T + 1.1205 \times 10^{-6} T^2$$

$$C_p \text{ (J g}^{-1} \text{ K}^{-1}) = 1.396 + 2.632 \times 10^{-4} T + 4.6882 \times 10^{-6} T^2$$

55FUR/McC

BUTENE-1-POLYSULFONE; solid; repeating unit: C₄H₈O₂S.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 10347 \pm 6.8 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5748.3 \pm 3.8 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 24050.9 \pm 15.9 \text{ J g}^{-1}$$

59IVI/KEI

cis-BUTENE-2-POLYSULFONE; solid; repeating unit: C₄H₈O₂S.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 10340 \pm 4.7 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5744.6 \pm 2.6 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 24035.4 \pm 10.9 \text{ J g}^{-1}$$

59IVI/KEI

trans-BUTENE-2-POLYSULFONE; solid; repeating unit: C₄H₈O₂S.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 10342 \pm 4.5 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5745.7 \pm 2.5 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 24040.0 \pm 10.5 \text{ J g}^{-1}$$

59IVI/KEI

iso-BUTENE POLYSULFONE (2-methylpropene polysulfone); solid; repeating unit:
 $C_4H_8O_2S$.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 10356 \pm 5.2 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5753.2 \pm 2.9 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 24071.4 \pm 12.1 \text{ J g}^{-1} \end{aligned}$$

59IVI/KEI

CELLULOID; solid; Celanese Corp. of America trade name; a solid solution of cellulose nitrate and camphor or other related plasticizers.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 7603 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4224 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17673 \text{ J g}^{-1} \end{aligned}$$

15ROT/WAL

DELRIN; solid; (polyoxymethylene); E.I. duPont de Nemours and Company trade name; crystallized resin granules, 99.3%; unspecified organic additives, 0.7%; repeating unit:
 CH_2O .

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 7284.8 \pm 1 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4047.1 \pm 0.8 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 16933.3 \pm 3.3 \text{ J g}^{-1} \end{aligned}$$

63PAR/MOS

DICYANDIAMIDE (TECHNICAL); solid; elementary analysis: carbon, 28.97%; hydrogen, 4.44%; nitrogen, 66.60%; formula $C_2H_4N_4$.

gross heat of combustion: at 25°C (77°F)

unhardened

$$\begin{aligned} q_v(\text{gross}) &= 6723.7 \pm 3.1 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3735.4 \pm 1.7 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 15628.9 \pm 7.1 \text{ J g}^{-1} \end{aligned}$$

hardened

$$\begin{aligned} q_v(\text{gross}) &= 6772.3 \pm 3.8 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3762.4 \pm 2.1 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 15741.9 \pm 8.8 \text{ J g}^{-1} \end{aligned}$$

67FRA/MIS

DURETHAN U20; solid; a polyurethane from 1,4-butanediol and hexamethyldiisocyanate; formula $C_{12}H_{22}O_4N_2$.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned}q_v(\text{gross}) &= 11199 \pm 3.4 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 6221.4 \pm 1.9 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 26030.3 \pm 7.9 \text{ J g}^{-1}\end{aligned}$$

67FRA/MIS

EPILOX EGI, HARDENED; solid; empirical formula $C_{39}H_{40}O_{8.5}$; the unhardened resin plus phthalic anhydride.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned}q_v(\text{gross}) &= 13021 \pm 3.4 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7233.9 \pm 1.9 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 30266.6 \pm 7.9 \text{ J g}^{-1}\end{aligned}$$

67FRA/MIS

EPILOX EGI, UNHARDENED; solid; elementary analysis: carbon, 74.74%; hydrogen, 7.27%; oxygen, 17.99%; a diepoxide from epichlorhydrin plus 4,4'-dihydroxydiphenyl-2,2'-propane; empirical formula $C_{31}H_{36}O_{5.5}$.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned}q_v(\text{gross}) &= 14161 \pm 4.5 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7867.0 \pm 2.5 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 32915.5 \pm 10.5 \text{ J g}^{-1}\end{aligned}$$

67FRA/MIS

GLYPTAL; solid; trademark for synthetic resins and plasticizers prepared from a polyhydric alcohol and phthalic anhydride.

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
1 -457.6	0.0000072	0.0000072	0.00003
2 -455.8	0.000048	0.000048	0.0002
3 -454	0.0002	0.0002	0.0007
4 -452	0.0005	0.0005	0.002
6 -448.6	0.002	0.002	0.007
8 -445	0.003	0.003	0.014
10 -441.4	0.005	0.005	0.02
15 -432.4	0.014	0.014	0.06
20 -423.4	0.03	0.03	0.11
30 -405.4	0.05	0.05	0.20
40 -387.4	0.07	0.07	0.29
60 -351.4	0.12	0.12	0.49
80 -315.4	0.19	0.19	0.79
100 -279.4	0.275	0.275	1.15

59KEE/SEI

LUCITE; solid; (polymethylmethacrylate); (E.I. duPont de Nemours and Company trade name); repeating unit: C₅H₈O₂.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 11462 \pm 4.1 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6367.8 \pm 2.3 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 26642.9 \pm 9.6 \text{ J g}^{-1}$$

specific heat: assume values refer to room temperature.

$$C_p(\text{Btu lb}^{-1} \text{ °F}^{-1}) = 0.343$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.343$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 1.435$$

67FRA/MIS; 38GUC/FOR

MELINEX FILM; solid; Material measured was a polyester 0.001 in. thick, with an empirical formula $(C_{10}H_8O_4)_n$.

gross heat of combustion: temperature = 298.15 K (77°F), pressure = 30 atm oxygen, result had a mean CO_2 recovery of 99.746%.

$$q_v(\text{gross}) = 9864.3 \pm 2.6 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5480.1 \pm 1.4 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 22928.9 \pm 6 \text{ J g}^{-1}$$

75AND/BAR

2,5-METHYLOLMELAMINE, HARDENED; solid; elementary analysis: carbon, 34.19%; hydrogen, 5.27%; oxygen, 17.07%; nitrogen, 43.47%; empirical formula $C_{11}H_{20}O_4N_{12}$; a melamine-formaldehyde polymer.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 6950.9 \pm 2.3 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3861.6 \pm 1.3 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16156.9 \pm 5.4 \text{ J g}^{-1}$$

67FRA/MIS

2,5-METHYLOLMELAMINE, UNHARDENED; solid; elementary analysis: carbon, 32.70%; hydrogen, 5.53%; oxygen, 20.51%; nitrogen, 41.26%; empirical formula $C_{5.5}H_{11}O_{2.5}N_6$; a melamine-formaldehyde polymer.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 6699.2 \pm 2.2 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3721.8 \pm 1.2 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 15572.0 \pm 5.0 \text{ J g}^{-1}$$

67FRA/MIS

MYLAR FILM; solid; E. I. duPont de Nemours and Company trade name; Repeating unit is $(C_{12}H_{12}O_4)_n$. Material measured was 100-gauge, type A polyester film and is a copolymer of ethylene glycol and terephthalic acid.

gross heat of combustion: temperature = 25°C (77°F), oxygen pressure = 30 atm, value given is expressed as a function of humidity (where RH is relative humidity in %).

$$q_v(\text{gross}) = -9862.74 + 0.4543RH \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = -5479.30 + 0.2524RH \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = -22925.39 + 1.0560RH \text{ J g}^{-1}$$

70MAN/RAP

NORYL RESIN III; solid; (E.I. duPont de Nemours and Company trade name);
 composition: polystyrene, 47%; polyphenylene oxide, 47%; polybutadiene, 5%;
 polyethylene, 1%.

heat of fusion: 83°-103°C (181°-217°F)

$$L_f = 0.4 \text{ Btu lb}^{-1}$$

$$L_f = 0.2 \text{ cal g}^{-1}$$

$$L_f = 0.8 \text{ J g}^{-1}$$

specific heat:

temperature		C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
(K)	(°F)			
194	-110	0.178	0.178	0.745
277	39	0.242	0.242	1.013
298	77	0.282	0.282	1.205
323	122	0.316	0.316	1.322
373	212	0.393	0.393	1.644
424	304	0.439	0.439	1.837
482	408	0.483	0.483	2.021
519	475	0.503	0.503	2.105

specific heat change at glass transition temperature:

temperature		C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
(K)	(°F)			
212	- 78	0.005	0.005	0.021
414	286	0.044	0.044	0.184

70BAI

NYLON-6; solid; (poly-ε-caprolactam); repeating unit: C₆H₁₁NO.

gross heat of combustion: at 20°C (68°F)

slow condensation

$$\begin{aligned} q_v(\text{gross}) &= 13640 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7575 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 31694 \text{ J g}^{-1} \end{aligned}$$

rapid condensation

$$\begin{aligned} q_v(\text{gross}) &= 13660 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7587 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 31744 \text{ J g}^{-1} \end{aligned}$$

Miramid H: 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 13417 \pm 5.0 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7454.1 \pm 2.8 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 31188.0 \pm 11.7 \text{ J g}^{-1} \end{aligned}$$

specific heat: 273-433 K (32°-320°F); amorphous nylon-6.

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= -0.047 + 8.3 \times 10^{-4} T \\ C_p(\text{cal g}^{-1} \text{ deg}^{-1}) &= -0.085 + 1.5 \times 10^{-3} T \\ C_p(\text{J g}^{-1} \text{ deg}^{-1}) &= -0.356 + 6.3 \times 10^{-3} T \end{aligned}$$

melting point: maximum melting temperature is 225°C (437°F)

heat of fusion: at 225°C (437°F)

$$\begin{aligned} L_f &= 81 \text{ Btu lb}^{-1} \\ L_f &= 45 \text{ cal g}^{-1} \\ L_f &= 188 \text{ J g}^{-1} \end{aligned}$$

57KAC; 55MAR/SMI; 67FRA/MIS

NYLON-6; liquid; (poly-ε-caprolactam); repeating unit: C₆H₁₁NO.

specific heat: 433-553 K (320°-536°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.5708 + 1.867 \times 10^{-4} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.485 + 3.36 \times 10^{-4} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 2.029 + 1.406 \times 10^{-3} T \end{aligned}$$

55MAR/SMI

NYLON-6,6; solid; (polyhexamethylenedipamide); repeating unit: $C_{12}H_{22}N_2O_2$; average mol. wt. 11000.

gross heat of combustion: at 20°C (68°F)

$$q_v(\text{gross}) = 13650 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7581 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 31719 \text{ J g}^{-1}$$

Ultramid A

$$q_v(\text{gross}) = 13579 \pm 4.3 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7543.8 \pm 2.4 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 31563.3 \pm 10.0 \text{ J g}^{-1}$$

specific heat: 273-553 K (32°-536°F)

Annealed Sample
(K) (°F)

Annealed Sample		C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
273	32	0.311	0.311	1.301
293	68	0.333	0.333	1.393
313	104	0.367	0.367	1.536
333	140	0.424	0.424	1.774
353	176	0.468	0.468	1.958
373	212	0.505	0.505	2.113
393	248	0.548	0.548	2.293
413	284	0.583	0.583	2.439
433	320	0.642	0.642	2.686
453	356	0.620	0.620	2.594
473	392	0.646	0.646	2.703
493	428	0.664	0.664	2.778
513	464	0.80	0.80	3.347
523	482	1.13	1.13	4.728
533	500	2.75	2.75	11.51
543	518	1.3	1.3	5.439
553	536	0.75	0.75	3.138

Drawn Sample
(K) (°F)

273	32	0.302	0.302	1.264
293	68	0.345	0.345	1.443
313	104	0.376	0.376	1.573
333	140	0.420	0.420	1.757
353	176	0.458	0.458	1.916

(more)

NYLON-6,6 - Continued

Drawn Sample		C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
(K)	(°F)			
373	212	0.479	0.479	2.004
393	248	0.503	0.503	2.105
413	284	0.528	0.528	2.209
433	320	0.542	0.542	2.268
453	356	0.560	0.560	2.343
473	392	0.582	0.582	2.435
493	428	0.567	0.567	2.372
513	464	0.676	0.676	2.828
523	482	1.55	1.55	6.485
533	500	6.5	6.5	27.20
543	518	1.35	1.35	5.648
553	536	0.75	0.75	3.138

melting point:

	Drawn Filaments	Annealed
M.P., °C	259	262
M.P., °F	498	504
Melting Range, °C	18	30
Melting Range, °F	32	54

heat of fusion:

	Drawn Filaments	Annealed
L_f (Btu lb ⁻¹)	53.1	59.9
L_f (cal g ⁻¹)	29.5	33.3
L_f (J g ⁻¹)	165.3	139.3

57KAC; 53WIL/DOL; 67FRA/MIS

NYLON-6,10; solid; ribbon; (polyhexamethylenesebacamide); repeating unit:
 $C_{16}H_{30}N_2O_2$; average mol. wt. 9250.

specific heat: ribbon

temperature (K)	(°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
273	32	0.327	0.327	1.368
293	68	0.373	0.373	1.561
313	104	0.420	0.420	1.757
333	140	0.486	0.486	2.033
353	176	0.512	0.512	2.142
373	212	0.518	0.518	2.167
393	248	0.531	0.531	2.222
413	284	0.561	0.561	2.347
433	320	0.592	0.592	2.477
453	356	0.588	0.588	2.460
473	392	0.686	0.686	2.870
493	428	1.95	1.95	8.159
513	464	0.737	0.737	3.084
523	482	0.639	0.639	2.674
533	500	0.627	0.627	2.623
543	518	0.632	0.632	2.644
553	536	0.639	0.639	2.674

melting point: 225°C (437°F); melting range 30°-40°C (54°-72°F)

heat of fusion: ribbon

L_f (Btu lb ⁻¹)	□ 47.3
L_f (cal g ⁻¹)	□ 26.3
L_f (J g ⁻¹)	□ 110.0

53WIL/DOL

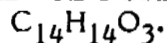
PHENOL-FORMALDEHYDE RESIN, HARDENED (EDELKUNSTHARZ B); solid; empirical formula $C_{13}H_{12}O_2$.

gross heat of combustion: at 25°C (77°F)

q_v (gross)	= 13598 ± 3.8 Btu lb ⁻¹
q_v (gross)	= 7554.3 ± 2.1 cal g ⁻¹
q_v (gross)	= 31607.2 ± 8.8 J g ⁻¹

67FRA/MIS

PHENOL-FORMALDEHYDE RESIN, UNHARDENED; solid; empirical formula



gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 12968 \pm 3.6 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7204.2 \pm 2.0 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 30142.4 \pm 8.4 \text{ J g}^{-1}$$

67FRA/MIS

POLYACENAPHTHYLENE; solid; amorphous; repeating unit: $C_{12}H_8$; degree of polymerization ~600 units.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 16898 \pm 3.6 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9388.0 \pm 2.0 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39279.4 \pm 8.4 \text{ J g}^{-1}$$

68JOS

POLYALLYLPHTHALATE; solid; empirical formula $C_{14}H_{14}O$.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 11934 \pm 3.8 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 6629.8 \pm 2.1 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 27739.1 \pm 8.8 \text{ J g}^{-1}$$

67FRA/MIS

POLYBUTADIENE 41°F; solid; analysis: carbon, 88.47%; hydrogen, 11.160%; sulfur, 0.083%; oxygen, 0.12%; ash, 0.34%; phenyl- β -naphthylamine, 0.10%; repeating unit: C_4H_6 ; polymerization is carried out at 5°C (41°F).

specific heat:

temperature (K)	(°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
50	-370	0.08532	0.08532	0.3570
100	-280	0.15832	0.15832	0.6624
150	-190	0.22416	0.22416	0.9379
200	-100	0.359	0.359	1.50
250	-10	0.433	0.433	1.81
300	80	0.471	0.471	1.97
330	134	0.4940	0.4940	2.067

53aFUR/McC

POLYBUTADIENE 122°F; solid; analysis: carbon, 88.66%; hydrogen, 11.180%; sulfur, 0.150%; oxygen, 0.145%; ash, 0.097%; phenyl- β -naphthylamine, 0.12%; repeating unit: C_4H_6 ; polymerization carried out at 50°C (132°F).

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
50 -370	0.08640	0.08640	0.3615
100 -280	0.15777	0.15777	0.6601
150 -190	0.22299	0.22299	0.9330
200 -100	0.3967	0.3967	1.66
250 -10	0.4326	0.4326	1.81
300 80	0.4680	0.4680	1.958
330 134	0.4919	0.4919	2.058

53aFUR/McC

POLY-1-BUTENE; solid; isotactic; 34% crystallinity; repeating unit: C_4H_8 ; degree of polymerization ~800 units.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 19996.9 \pm 0.9 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11109.4 \pm 0.5 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46481.7 \pm 2.1 \text{ J g}^{-1}$$

68JOS

POLY-iso-BUTENE; (Sample 1) viscous liquid; mol. wt. ~4900; (Sample 2) amorphous solid, rubberlike; mol. wt. ~200000; 0.033% ash; (Sample 3) solid; Opanol B 100; repeating unit: C_4H_8 .

gross heat of combustion: at 25°C (77°F)

Sample 1

$$q_v(\text{gross}) = 20123.6 \pm 2.3 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11179.8 \pm 1.3 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46776.3 \pm 5.4 \text{ J g}^{-1}$$

Sample 3

$$q_v(\text{gross}) = 20122.4 \pm 7.7 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11179.1 \pm 4.3 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46773.4 \pm 18.0 \text{ J g}^{-1}$$

Sample 2

$$q_v(\text{gross}) = 20116.4 \pm 3.6 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11175.8 \pm 2.0 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46759.5 \pm 8.3 \text{ J g}^{-1}$$

49PAR/MOS; 67FRA/MIS

POLY-1,1-DICHLOROETHYLENE (polyvinylidene chloride); solid; repeating unit:
 $C_2H_2Cl_2$; purity 99.9 mol %.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 4527.2 \pm 3.8 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 2515.1 \pm 2.1 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 10523.2 \pm 8.8 \text{ J g}^{-1} \end{aligned}$$

58SIN/STU

POLY-1,1-DIFLUOROETHYLENE (polyvinylidene fluoride); solid; repeating unit:
 $C_2H_2F_2$; particle size 100 mesh.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 6352.4 \pm 0.7 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 3529.1 \pm 0.4 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 14765.8 \pm 1.7 \text{ J g}^{-1} \end{aligned}$$

64GOO/LAC

POLY-2,6-DIMETHYLPHENYLENE ETHER; solid; repeating unit: C_8H_8O ; 20%
 crystallinity; degree of polymerization ~300 units.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 14892 \pm 2.5 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 8273.2 \pm 1.4 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 34615.1 \pm 5.9 \text{ J g}^{-1} \end{aligned}$$

68JOS

POLY-4,4'-DIOXYDIPHENYL-2,2-PROPANE CARBONATE; solid; empirical formula
 $C_{16}H_{14}O_3$.

gross heat of combustion: at 25°C (77°F)

PKU T 22

Makrolon; solid.

$$\begin{aligned} q_v(\text{gross}) &= 13336 \pm 3.8 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7408.7 \pm 2.1 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 30998.0 \pm 8.8 \text{ J g}^{-1} \end{aligned}$$

$$\begin{aligned} q_v(\text{gross}) &= 13336 \pm 3.6 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7408.7 \pm 2.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 30998.0 \pm 8.4 \text{ J g}^{-1} \end{aligned}$$

Lexan; General Electric trade name; 20% crystallinity; degree of polymerization ~150
 units.

$$\begin{aligned} q_v(\text{gross}) &= 13307 \pm 2.5 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7392.9 \pm 1.4 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 30931.9 \pm 5.9 \text{ J g}^{-1} \end{aligned}$$

68JOS; 67FRA/MIS

POLY-ε-ENANTHOLACTAM; solid; repeating unit: C₇H₁₃NO.

gross heat of combustion: at 20°C (68°F)

$$q_v(\text{gross}) = 14359 \pm 9.9 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7977.2 \pm 5.5 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 33376.6 \pm 23.0 \text{ J g}^{-1}$$

57KAC

POLYETHYLENE; solid; NBS Standard Reference Material (SRM) 1475; linear polymer; wt.-ave. molecular weight, 52000; methyl group content, 0.15 methyl groups per 100 carbon atoms; ash content, 0.002%; 111 ppm of anti-oxidant [tetrakis-(methylene-3-(3', 5'-di-tert-butyl-4'-hydroxyphenyl) propionate) methane] added to polymer by manufacturer; density at 23°C (73°F), 0.9784 g cm⁻³; degree of crystallinity determined to be 72%; repeating unit: C₂H₄.

gross heat of combustion: at 25°C (77°F)

SRM 1475, crystallinity 72%

$$q_v(\text{gross}) = 19932.7 \pm 3.8 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11073.7 \pm 2.1 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46332.4 \pm 8.8 \text{ J g}^{-1}$$

SRM 1475 modified by recrystallization under high pressure; crystallinity 96%.

$$q_v(\text{gross}) = 19905.5 \pm 3.6 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 11058.6 \pm 2.0 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 46269.1 \pm 8.1 \text{ J g}^{-1}$$

specific heat: SRM 1475

temperature (K)	(°F)	C _p (Btu lb ⁻¹ °F ⁻¹)	C _p (cal g ⁻¹ K ⁻¹)	C _p (J g ⁻¹ K ⁻¹)
10	-442	0.0029	0.0029	0.0123
100	-280	0.1632	0.1632	0.6829
200	-100	0.2839	0.2839	1.1877
250	- 10	0.3537	0.3537	1.4800
273.15	32	0.3936	0.3936	1.6468
298.15	77	0.4376	0.4376	1.8308
320	116	0.4790	0.4790	2.0040
360	188	0.5904	0.5904	2.4702

74SPL/JOH; 73CHA/BES

POLYETHYLENE; solid; (sample 1) high pressure; mol. wt. 18000-20000; crystallinity 50%; (sample 2) linear; Marlex; crystallinity 98%; (sample 3) low density; (sample 4) high density, Mirathen H; repeating unit: C_2H_4 .

gross heat of combustion: at 25°C (77°F)

sample 1

$$\begin{aligned}q_v(\text{gross}) &= 19968.5 \pm 1.4 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 11093.6 \pm 0.8 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 46415.6 \pm 3.3 \text{ J g}^{-1}\end{aligned}$$

sample 2

$$\begin{aligned}q_v(\text{gross}) &= 19945.6 \pm 3.6 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 11080.9 \pm 2.0 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 46362.5 \pm 8.4 \text{ J g}^{-1}\end{aligned}$$

sample 3

$$\begin{aligned}q_v(\text{gross}) &= 19876.9 \pm 6.3 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 11042.7 \pm 3.5 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 46202.7 \pm 14.6 \text{ J g}^{-1}\end{aligned}$$

sample 4

$$\begin{aligned}q_v(\text{gross}) &= 19985.2 \pm 8.3 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 11102.9 \pm 4.6 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 46485.5 \pm 19.2 \text{ J g}^{-1}\end{aligned}$$

49PAR/MOS; 63PAR/MOS; 67FRA/MIS

POLY- α -METHYL STYRENE; solid; anionic; amorphous; samples with different degrees of polymerization, ~34000 units and ~13000 units gave the same heat of combustion; repeating unit: C_9H_{10} .

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned}q_v(\text{gross}) &= 18201.2 \pm 5.0 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 10111.8 \pm 2.8 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 42307.8 \pm 11.7 \text{ J g}^{-1}\end{aligned}$$

68JOS

POLY(OXY-2-METHYL-1,4-CYCLOHEXYLENE); solid; Repeating unit $(C_7H_{12}O)_n$ was formed from endo-2-methyl-7-oxabicyclo [2.2.1] heptane by polymerization in CH_2Cl_2 . Density was 0.823 g cm^{-3} , and material was a white powdery solid.

gross heat of combustion: temperature = 25°C (77°F), pressure was 30 atm oxygen, mean value was based on percentage recovery of CO_2 .

$$\begin{aligned}q_v(\text{gross}) &= 16030.69 \pm 3.94 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8905.94 \pm 2.19 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 37262.45 \pm 9.15 \text{ J g}^{-1}\end{aligned}$$

heat of polymerization: temperature = 25°C (77°F), $nC_7H_{12}O(\text{liq}) \rightarrow (C_7H_{12}O)_n(\text{solid})$

$$\begin{aligned}\Delta H(\text{polymerization}) &= -127.7 \pm 14.2 \text{ Btu lb}^{-1} \\ \Delta H(\text{polymerization}) &= -70.95 \pm 7.9 \text{ cal g}^{-1} \\ \Delta H(\text{polymerization}) &= -296.9 \pm 33.0 \text{ J g}^{-1}\end{aligned}$$

75AND/BAR

POLYPROPYLENE; solid; repeating unit: C_3H_6 .

gross heat of combustion: at 25°C (77°F)

isotactic; 58% crystallinity

$$\begin{aligned} q_v(\text{gross}) &= 19948.3 \pm 4 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 11082.4 \pm 2.2 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 46368.8 \pm 9.2 \text{ J g}^{-1} \end{aligned}$$

degree of polymerization ~4000 units

$$\begin{aligned} q_v(\text{gross}) &= 19944.9 \pm 4 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 11080.5 \pm 2.2 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 46360.8 \pm 9.2 \text{ J g}^{-1} \end{aligned}$$

Polypropylene VK166, untangled

$$\begin{aligned} q_v(\text{gross}) &= 19838 \pm 9.2 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 11021.2 \pm 5.1 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 46112.7 \pm 21.3 \text{ J g}^{-1} \end{aligned}$$

63PAR/MOS; 67FRA/MIS

POLYSTYRENE; solid; repeating unit: C_8H_8 .

gross heat of combustion: at 25°C (77°F)

isotactic, 40% crystallinity

$$\begin{aligned} q_v(\text{gross}) &= 17838 \pm 5.6 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 9909.9 \pm 3.1 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 41463.0 \pm 13.0 \text{ J g}^{-1} \end{aligned}$$

isotactic, amorphous

$$\begin{aligned} q_v(\text{gross}) &= 17853 \pm 4.3 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 9918.5 \pm 2.4 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 41499.0 \pm 10.0 \text{ J g}^{-1} \end{aligned}$$

atactic, amorphous

$$\begin{aligned} q_v(\text{gross}) &= 17858 \pm 2.5 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 9921.2 \pm 1.4 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 41510.3 \pm 5.9 \text{ J g}^{-1} \end{aligned}$$

polystyrol BW

$$\begin{aligned} q_v(\text{gross}) &= 17860 \pm 7.2 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 9922.4 \pm 4.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 41515.3 \pm 16.7 \text{ J g}^{-1} \end{aligned}$$

polystyrol P70

$$\begin{aligned} q_v(\text{gross}) &= 17821 \pm 5.4 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 9900.5 \pm 3.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 41423.7 \pm 12.6 \text{ J g}^{-1} \end{aligned}$$

67FRA/MIS; 68JOS

POLYUREA (POLYHARNSTOFF); solid; empirical formula $C_{15}H_{18}O_4N_4$; a polymer of adipic acid diamide plus (2,4-2,6)-toluene diisocyanate.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned} q_v(\text{gross}) &= 10717 \pm 3.1 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5954.0 \pm 1.7 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 24911.5 \pm 7.1 \text{ J g}^{-1} \end{aligned}$$

67FRA/MIS

POLYVINYL CHLORIDE; solid; Repeating unit is $(-\text{CH}_2\text{CHCl}-)_n$, it is a synthetic thermoplastic polymer. Purity is 99.7 mole %.

gross heat of combustion: temperature is 25°C (77°F), and value given is per monomer unit.

$$\begin{aligned} q_v(\text{gross}) &= 7874.7 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4374.8 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18304.3 \text{ J g}^{-1} \end{aligned}$$

58SIN/STU

PROPARGYL AZIDE POLYMER; solid; Polymer was formed when an alcohol-water solution of propargyl bromide and sodium azide was refluxed and the product $(\text{C}_3\text{H}_3\text{N}_3)_n$ appears to be primarily a 4-methylene-1,2,3-triazole polymer (the 5 methylene configuration is also possible). Analysis found C = 44.04, H = 4.07, N = 49.57, and O = 1.97 wt.% (oxygen is due to water that is occluded or chemically bound).

gross heat of combustion: assume values refer to room temperature; sample was dried under vacuum at 100°C; mean values were corrected for HNO_3 formation.

$$\begin{aligned} q_v(\text{gross}) &= 9454 \pm 22 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5252 \pm 12 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21974 \pm 50 \text{ J g}^{-1} \end{aligned}$$

73HOU/HUM

RESIN, ABS I; solid; copolymer of styrene-acrylonitrile = 76% and polybutadiene = 15%.

specific heat:

temperature (K) (°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
163 -166	0.184	0.184	0.770
217 - 69	0.240	0.240	1.004
277 39	0.311	0.311	1.301
298 77	0.338	0.338	1.414
328 131	0.373	0.373	1.561
380 225	0.492	0.492	2.059
430 315	0.518	0.518	2.167
477 399	0.541	0.541	2.264

specific heat change at glass transition temperature:

temperature (K) (°F)	$\Delta C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$\Delta C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$\Delta C_p(\text{J g}^{-1} \text{ K}^{-1})$
188 -121	0.014	0.014	0.059
377 217	0.069	0.069	0.289

70BAI

RILSAN; solid; (poly-11-aminodecanoic acid); empirical formula $C_{11}H_{21}ON$.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 15913 \pm 4 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 8840.3 \pm 2.2 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 36987.8 \pm 8.4 \text{ J g}^{-1}$$

67FRA/MIS

TEFLON; solid; (E.I. duPont de Nemours and Company trade name);
(polytetrafluoroethylene); repeating unit: C_2F_4 ; density, 2.2 g cm^{-3} .

gross heat of combustion in oxygen: at 25°C (77°F); combustion products are gaseous carbon dioxide and carbon tetrafluoride.

$$q_v(\text{gross}) = 2154.1 \pm 18 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 1196.7 \pm 10.0 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 5007.0 \pm 42 \text{ J g}^{-1}$$

gross heat of combustion in fluorine: 25°C (77°F); combustion product is carbon tetrafluoride.

$$q_v(\text{gross}) = 4461.8 \pm 1.3 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 2478.8 \pm 0.7 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 10371.3 \pm 3.1 \text{ J g}^{-1}$$

specific heat:

temperature (K) (°F)	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
50 -370	0.04821	0.04821	0.2017
100 -280	0.09218	0.09218	0.3857
150 -190	0.13380	0.13380	0.5598
200 -100	0.17706	0.17706	0.7408
250 -10	0.21076	0.21076	0.8818
270 26	0.22768	0.22768	0.9526
280 44	0.24187	0.24187	1.012
310 98	0.24402	0.24402	1.021
330 134	0.24809	0.24809	1.038
360 188	0.25669	0.25669	1.074

transition temperatures:

293 K (20°C) (68°F)

303 K (30°C) (86°F)

heat of transition: for the temperature range 280-310 K.

$$L_f = 15.7 \text{ Btu lb}^{-1}$$

$$L_f = 8.72 \text{ cal g}^{-1}$$

$$L_f = 36.5 \text{ J g}^{-1}$$

67DOM/ARM; 52FUR/McC

TROCKENLEIM (DRYING GLUE); solid; elementary analysis: carbon, 35.49%; hydrogen, 6.19%; oxygen, 30.91%; nitrogen, 27.41%; a urea-formaldehyde resin; empirical formula $C_3H_6O_2N_2$.

gross heat of combustion: at 25°C (77°F)

$$q_v(\text{gross}) = 6840.7 \pm 3.6 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3800.4 \pm 2.0 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 15900.9 \pm 8.4 \text{ J g}^{-1}$$

67FRA/MIS

Polypeptides and Proteins

BOVINE CHYMOTRYPSINOGEN A; solid; Anhydrous material is a protein from beef pancreas made up of 245 amino acids with mol. wt. of 25646.

specific heat:

temperature (K)	(°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
10	-442	0.00448	0.00448	0.01874
100	-280	0.1120	0.1120	0.4686
150	-190	0.1696	0.1696	0.7096
200	-100	0.2153	0.2153	0.9008
250	- 10	0.2617	0.2617	1.9050
298.15	77	0.3090	0.3090	1.2929
300	80	0.3109	0.3109	1.3008

69HUT/COL

CASEIN, MILK; solid; carbon, 53%; hydrogen, 7%; oxygen, 22.65%; nitrogen, 15.7%; sulfur, 0.8%; phosphorus, 0.85%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 10210 \pm 360 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5670 \pm 200 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 23700 \pm 800 \text{ J g}^{-1}$$

55MER/WAT

CHYMOTRYPSIN; nonaqueous; A proteolytic enzyme found in the intestine that catalyzes the hydrolysis of various proteins (especially casein) to form polypeptides and amino acids.

heat of denaturation: protein solution is 0.180 mass % in a 0.1 mol dm⁻³ glycine buffer with pH = 3.5.

$$\Delta H \text{ denaturation} = 11.43 \text{ Btu lb}^{-1}$$

$$\Delta H \text{ denaturation} = 6.35 \text{ cal g}^{-1}$$

$$\Delta H \text{ denaturation} = 26.57 \text{ J g}^{-1}$$

specific heat: the apparent molal specific heat of a protein solution of 0.180 mass % in a 0.1 mol dm⁻³ glycine buffer at pH = 3.5; thermochemical calorie used.

temperature (K)	(°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
298	77	0.31 ± 0.01	0.31 ± 0.01	1.30 ± 0.04
313	104	0.34 ± 0.01	0.34 ± 0.01	1.42 ± 0.04

75PRI/PLO

COLLAGEN; solid; fibrous protein that comprises the major portion of the white fiber in connective tissues of the animal body; chief amino acids present are proline, hydroxyproline, and glycine; converted to gelatine by boiling with water.

specific heat: 298 K (77°F)

moisture content (wt. %)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
0	0.3723	0.3723	1.5577
1.02	0.3490	0.3490	1.4602
1.96	0.3659	0.3659	1.5309
4.56	0.4014	0.4014	1.6795
6.49	0.4061	0.4061	1.6991
17.03	0.4280	0.4280	1.7908

55KAN

GELATINE; solid; a protein obtained from collagen by boiling skin, ligaments, tendons, bones, etc. with water; can absorb 5 to 10 times its weight of water.

gross heat of combustion: assume values refer to room temperature.

As received: ash content, 0.6%-0.8%; water content not determined.

$$q_v(\text{gross}) = 7920 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4400 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18410 \text{ J g}^{-1}$$

Ash free and moisture free

$$q_v(\text{gross}) = 9270 \pm 180 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5150 \pm 100 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 21550 \pm 400 \text{ J g}^{-1}$$

15ROT/WAL

GLIADIN; solid; also called prolamin; simple vegetable protein found in gluten; typical composition: carbon, 52.7%; hydrogen, 6.9%; oxygen, 21.7%; nitrogen, 17.7%; sulfur, 1.0%.

gross heat of combustion:

variation with thermal denaturation temperature.

denaturation temperature		Btu lb ⁻¹	q _v (gross) cal g ⁻¹	J g ⁻¹
(°C)	(°F)			
30	86	10775	5986.3	25046.7
35	95	10640	5911.3	24732.9
50	122	10399	5777.2	24171.8
70	158	10457	5809.3	24306.1
110	230	10535	5852.8	24488.1

variation with concentration of aqueous alcohol used in extraction.

alcohol %	Btu lb ⁻¹	q _v (gross) cal g ⁻¹	J g ⁻¹
40	10600	5891	24648
50	10560	5869	24556
60	10700	5942	24861
70	10850	6028	24221

66PON

GLUTEN; solid; mixture of proteins found in the seeds of cereal grains [wheat, corn (maize), etc.] which remains after washing the starch out of flour with water; amino acids of gluteins are glutamic acid, leucine, proline, and arginine.

gross heat of combustion: variation with thermal denaturation temperature.

denaturation temperature		Btu lb ⁻¹	q _v (gross) cal g ⁻¹	J g ⁻¹
(°C)	(°F)			
30	86	10436	5797.9	24258.4
35	95	10572	5873.2	24573.5
50	122	10168	5648.8	23634.6
70	158	10298	5721.1	23937.1
110	230	10403	5779.6	24181.8

66PON

GLUTENIN; solid; wheat protein soluble in dilute alkalis.

gross heat of combustion: variation with thermal denaturation temperature.

denaturation temperature		Btu lb ⁻¹	q _v (gross)	
(°C)	(°F)		cal g ⁻¹	J g ⁻¹
30	86	10278	5710.1	23891.1
35	95	10315	5730.3	23975.6
50	122	10050	5583.1	23359.7
70	158	10177	5654.0	23656.3
110	230	10260	5699.9	23848.4

66PON

INSULIN, BOVINE ZINC; solid; the anhydrous material from beef pancreas made up of 16 amino acids arranged in two chains connected by sulfur bridges, (C₅₀₈H₇₅₂O₁₅₀N₁₃₀S₁₂Zn). The ash content = 0.95%; zinc present (as ZnO) = 0.67%.

specific heat:

temperature		C _p (Btu lb ⁻¹ °F ⁻¹)	C _p (cal g ⁻¹ K ⁻¹)	C _p (J g ⁻¹ K ⁻¹)
(K)	(°F)			
10	-442	0.00475	0.00475	0.01987
100	-280	0.1192	0.1192	0.4987
200	-100	0.2089	0.2089	0.8740
250	-10	0.2541	0.2541	1.0632
298.15	77	0.2996	0.2996	1.2535
300	80	0.3014	0.3014	1.2611

69HUT/COL

PHENYLALANINE POLYMER; solid; repeating unit: C₉H₉NO.

gross heat of combustion: at 25°C (77°F)

benzene soluble

$$q_v(\text{gross}) = 13506 \pm 11 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7503.2 \pm 6.0 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 31393.4 \pm 25.1 \text{ J g}^{-1}$$

benzene insoluble

$$q_v(\text{gross}) = 13462 \pm 12 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7479.1 \pm 6.9 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 31292.6 \pm 28.9 \text{ J g}^{-1}$$

52BRE/TER

POLY-N-ETHYL-N-METHYL PROPIONAMIDE; solid; density, 1.44 g cm^{-3} ; repeating unit: $\text{C}_6\text{H}_{13}\text{NO}$.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned}q_v(\text{gross}) &= 14525 \pm 1.8 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8069.3 \pm 1.0 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33762.0 \pm 4.2 \text{ J g}^{-1}\end{aligned}$$

59KOZ/SKU

SARCOSINE POLYMER; solid; repeating unit: $\text{C}_3\text{H}_5\text{NO}$.

gross heat of combustion: at 25°C (77°F)

$$\begin{aligned}q_v(\text{gross}) &= 10128 \pm 7.6 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5626.4 \pm 4.2 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23540.9 \pm 17.6 \text{ J g}^{-1}\end{aligned}$$

52BRE/TER

VITELLIN; solid; globulin protein from egg yolk; typical composition: water, 49.4%; protein, 16.3%; fat, 31.9%; carbohydrate, 0.7%; remainder includes small amounts of elements such as phosphorus, sulfur, iron, and calcium.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 10370 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5760 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 24100 \text{ J g}^{-1}\end{aligned}$$

55MER/WAT

WOOL; solid; staple fibers obtained from the fleece of sheep (and also alpaca, vicuna, and certain goats); protein chains (keratin) bound together by disulfide cross linkages; chief amino acids: cysteine and cystine, 15%; glutamic acid, 16%; arginine, 10%; proline, 8%; leucine, 8%; sulfur content of wool sample, 3.5%.

gross heat of combustion: assume values refer to room temperature; dry basis, sulfur product aqueous H_2SO_4 .

$$\begin{aligned}q_v(\text{gross}) &= 9898 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5499 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23008 \text{ J g}^{-1}\end{aligned}$$

31PAS/KON

WOOL ACETATE; solid; salt formed from reaction of wool with acetic acid; 0.30% acetate.

gross heat of combustion: assume values refer to room temperature; sulfur product aqueous H_2SO_4 .

$$\begin{aligned}q_v(\text{gross}) &= 9882 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5490 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22970 \text{ J g}^{-1}\end{aligned}$$

31PAS/KON

WOOL β -NAPHTHALENE SULFONATE; solid; salt formed from reaction of wool with β -naphthalenesulfonic acid; 19.9% β -naphthalenesulfonate.

gross heat of combustion: assume values refer to room temperature; sulfur product aqueous H_2SO_4 .

$$\begin{aligned}q_v(\text{gross}) &= 9868 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5482 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22937 \text{ J g}^{-1}\end{aligned}$$

31PAS/KON

WOOL OXALATE; solid; salt formed from reaction of wool with oxalic acid; 2.22% oxalate.

gross heat of combustion: assume values refer to room temperature; sulfur product aqueous H_2SO_4 .

$$\begin{aligned}q_v(\text{gross}) &= 9648 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5360 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22426 \text{ J g}^{-1}\end{aligned}$$

31PAS/KON

WOOL PICRATE; solid; salt formed from reaction of wool with picric acid; 18.4% picrate.

gross heat of combustion: assume values refer to room temperature; sulfur product aqueous H_2SO_4 .

$$\begin{aligned}q_v(\text{gross}) &= 9077 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5043 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21100 \text{ J g}^{-1}\end{aligned}$$

31PAS/KON

WOOL PROTEIN; solid; material is a keratin containing 14.3% cystine, 3.9% sulfur, and 16.85% nitrogen.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$q_v(\text{gross}) = 10100 \pm 4.1 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5609 \pm 2.3 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 23468 \pm 9.6 \text{ J g}^{-1}$$

64PAL/REI

WOOL SULFATE; solid; salt formed from reaction of wool with sulfuric acid, 2.21% sulfate.

gross heat of combustion: assume values refer to room temperature, sulfur product aqueous H_2SO_4 .

$$q_v(\text{gross}) = 9625 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5347 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 22372 \text{ J g}^{-1}$$

31PAS/KON

WOOL p-TOLUENESULFONATE; solid; salt formed from reaction of wool with p-toluene-sulfonic acid; 6.6% p-toluenesulfonate.

gross heat of combustion: assume values refer to room temperature; sulfur product aqueous H_2SO_4 .

$$q_v(\text{gross}) = 9824 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5458 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 22836 \text{ J g}^{-1}$$

31PAS/KON

Refuse

REFUSE; solid; Samples are dry shredded garbage (essentially free of glass and metals). The refuse material contained significant amounts of reduced carbonaceous materials such as plastics, waxes, and oils.

gross heat of combustion: value is average of two trials, assume values refer to room temperature.

sample A

$$\begin{aligned}q_v(\text{gross}) &= 7959 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4422 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18500 \text{ J g}^{-1}\end{aligned}$$

sample B

$$\begin{aligned}q_v(\text{gross}) &= 8540 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4744 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19850 \text{ J g}^{-1}\end{aligned}$$

sample C

$$\begin{aligned}q_v(\text{gross}) &= 8621 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4790 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20040 \text{ J g}^{-1}\end{aligned}$$

sample D

$$\begin{aligned}q_v(\text{gross}) &= 8626 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4792 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20050 \text{ J g}^{-1}\end{aligned}$$

77JEN/EAT

REFUSE-DERIVED FUEL; solid; Refuse-derived fuel-3 (RDF-3) was obtained from the National Center for Resource Recovery (NCRR), Washington, D.C. Sample was air-dried and processed to 0.5 mm particle size for laboratory test analysis.

gross heat of combustion: assume values refer to room temperature; values are on a moisture-free, ash-free basis.

Sample 1, tested during June and July 1978. Residual moisture, 5.031 wt. %; ash content, 24.18 wt. %; sulfur content, 0.13 wt. %.

$$\begin{aligned}q_v(\text{gross}) &= 9796 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5446 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22785 \text{ J g}^{-1}\end{aligned}$$

Sample 2, tested during Dec. 1978 and Jan. 1979. Residual moisture, 6.090 wt. %; ash content, 14.62 wt. %; sulfur content, 0.14 wt. %.

$$\begin{aligned}q_v(\text{gross}) &= 9253 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5144 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21522 \text{ J g}^{-1}\end{aligned}$$

Sample 3, tested during 1979. Residual moisture, 5.265 wt. %; ash content, 11.80 wt. %; sulfur content, 0.095 wt. %.

$$\begin{aligned}q_v(\text{gross}) &= 8062 \text{ Btu}^{-1} \\q_v(\text{gross}) &= 4482 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18752 \text{ J g}^{-1}\end{aligned}$$

81KIR/COL

REFUSE-DERIVED FUEL; solid; Refuse-derived fuel-3 (RDF-3) was obtained from Americology, Milwaukee, Wis. Sample was air-dried and processed to 0.5 mm particle size for laboratory test analysis.

gross heat of combustion: assume values refer to room temperature; values are on a moisture-free, ash-free basis.

Sample 1, residual moisture, 4.796 wt. %; ash content, 22.52 wt. %; sulfur content, 0.48 wt. %.

$$\begin{aligned} q_v(\text{gross}) &= 9438 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5247 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21953 \text{ J g}^{-1} \end{aligned}$$

Sample 2, residual moisture, 3.006 wt. %; ash content, 29.65 wt. %; sulfur content, 0.24 wt. %.

$$\begin{aligned} q_v(\text{gross}) &= 9392 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5221 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21846 \text{ J g}^{-1} \end{aligned}$$

Sample 3, tested during 1979. Residual moisture, 5.265 wt. %; ash content, 11.80 wt. %; sulfur content, 0.095 wt. %.

$$\begin{aligned} q_v(\text{gross}) &= 9525 \text{ Btu}^{-1} \\ q_v(\text{gross}) &= 5295 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 22155 \text{ J g}^{-1} \end{aligned}$$

81KIR/COL

REFUSE-DERIVED FUEL; solid; Refuse-derived fuel-3 (RDF-3) was obtained from the Baltimore County Resource Recovery Facility, Cockeysville, Md., operated by Teledyne National. Sample was air-dried and processed to 0.5 mm particle size for laboratory test analysis. Residual moisture, 5.065 wt. %; ash content, 15.87 wt. %; sulfur content, 0.14 wt. %.

gross heat of combustion: assume values refer to room temperature; values are on a moisture-free, ash-free basis.

$$\begin{aligned} q_v(\text{gross}) &= 10553 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5867 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 24546 \text{ J g}^{-1} \end{aligned}$$

81KIR/COL

REFUSE-DERIVED FUEL; solid; A sample of ECO FUEL-II RDF was obtained from Combustion Equipment Associates, Bridgeport, Conn. and has a particle size of about 0.42 mm (-40 mesh). Residual moisture, 1.627 wt. %; ash content, 13.71 wt. %; sulfur content, 0.46 wt. %.

gross heat of combustion: assume values refer to room temperature; values are on a moisture-free, ash-free basis.

$$\begin{aligned}q_v(\text{gross}) &= 9451 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5254 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21983 \text{ J g}^{-1}\end{aligned}$$

81KIR/COL

REFUSE-DERIVED FUEL; solid; A synthetic refuse-derived fuel (RDF) has been developed at the National Bureau of Standards (NBS) and is designated as a standard reference material (SRM 1657). The composition of the synthetic RDF is approximately 80 mass % microcrystalline cellulose, 15 mass % silica, and 5 mass % alumina. All components have a nominal particle size of 50 micrometers. Residual moisture content, 3.7 mass %; ash content, 20.34 ± 0.54 mass %, dry basis.

gross heat of combustion: values refer to 25°C (77°F).

$$\begin{aligned}q_v(\text{gross}) &= 5963 \text{ Btu lb}^{-1} \text{ (dry-basis)} & q_v(\text{gross}) &= 7481 \text{ Btu lb}^{-1} \text{ (dry, ash-free)} \\q_v(\text{gross}) &= 3315 \text{ cal g}^{-1} \text{ (dry-basis)} & q_v(\text{gross}) &= 4159 \text{ cal g}^{-1} \text{ (dry, ash-free)} \\q_v(\text{gross}) &= 13870 \text{ J g}^{-1} \text{ (dry-basis)} & q_v(\text{gross}) &= 17400 \text{ J g}^{-1} \text{ (dry, ash-free)}\end{aligned}$$

85COL

REFUSE, MUNICIPAL; solid; waste from the city of St. Louis; particle size of 1.5 in. and less, magnetic metal removed; (batch 1) from 210 samples collected April 1972 through February 1973, unclassified material, with only magnetic metal removed; moisture, 9.3%-50.0%; sulfur, 0.01%-0.40%; chlorine, 0.13%-0.95%; ash, 12.1%-52.2%; (batch 2) from 99 samples collected November 1973 through January 1974, classified material; heavy fraction of waste removed by air-density separation; light fraction only: moisture, 11.1%-66.3%; sulfur, 0.05%-0.28%; chlorine, 0.14%-0.94%; ash, 7.6%-21.4%.

gross heat of combustion: assume values refer to room temperature.

batch 1

$$\begin{aligned}\text{minimum } q_v(\text{gross}) &= 3029 \text{ Btu lb}^{-1} \\ \text{minimum } q_v(\text{gross}) &= 1683 \text{ cal g}^{-1} \\ \text{minimum } q_v(\text{gross}) &= 7041 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}\text{maximum } q_v(\text{gross}) &= 7430 \text{ Btu lb}^{-1} \\ \text{maximum } q_v(\text{gross}) &= 4128 \text{ cal g}^{-1} \\ \text{maximum } q_v(\text{gross}) &= 17270 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}\text{average } q_v(\text{gross}) &= 4675 \text{ Btu lb}^{-1} \\ \text{average } q_v(\text{gross}) &= 2597 \text{ cal g}^{-1} \\ \text{average } q_v(\text{gross}) &= 10867 \text{ J g}^{-1}\end{aligned}$$

batch 2

$$\begin{aligned}\text{minimum } q_v(\text{gross}) &= 2295 \text{ Btu lb}^{-1} \\ \text{minimum } q_v(\text{gross}) &= 1275 \text{ cal g}^{-1} \\ \text{minimum } q_v(\text{gross}) &= 5333 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}\text{maximum } q_v(\text{gross}) &= 7598 \text{ Btu lb}^{-1} \\ \text{maximum } q_v(\text{gross}) &= 4221 \text{ cal g}^{-1} \\ \text{maximum } q_v(\text{gross}) &= 17661 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}\text{average } q_v(\text{gross}) &= 5020 \text{ Btu lb}^{-1} \\ \text{average } q_v(\text{gross}) &= 2789 \text{ cal g}^{-1} \\ \text{average } q_v(\text{gross}) &= 11669 \text{ J g}^{-1}\end{aligned}$$

74WIS/SUT

Refuse

REFUSE, MUNICIPAL; solid; waste from an English town; (sample 1) (on dry basis): paper, 29.6%; rags, 5.3%; vegetable matter, 5.1%; animal matter, 1.3%; wood, etc., 3.5%; coal, coke, cinders, 16.5%; metal, 4.9%; glass, pottery, and other non-combustible matter, 23.7%; fines, passing 1/4 in. \times 1/4 in. square mesh, 10.1%; moisture, 34.0%; (sample 2) (on dry basis): paper, 4.8%; rags, 0.3%; vegetable matter, 1.0%; animal matter, 0.7%; wood, etc., 0.8%; coal, coke cinders, 36.1%; metal, 0.9%; glass, pottery, and other non-combustible material, 10.0%; fines, passing 1/4 in. \times 1/4 in. square mesh, 45.4%; moisture, 17.2%.

gross heat of combustion: assume values refer to room temperature.

sample 1 (dry basis)

$$\begin{aligned}q_v(\text{gross}) &= 5598 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3110 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 13012 \text{ J g}^{-1}\end{aligned}$$

sample 2 (dry basis)

$$\begin{aligned}q_v(\text{gross}) &= 7308 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4060 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16987 \text{ J g}^{-1}\end{aligned}$$

55SPI

Rubber Materials

DISCARDED AUTOMOBILES TIRES; solid; The destructive distillation of tires resulted in a solid residue, an organic liquid, and a combustible gas of undetermined heating value (the process produced a mass loss of 65%). There are four types of rubber used in tires: natural, styrene-butadiene, polyisoprene, and polybutadiene. A typical compounding formula for passenger tire treads made out of natural rubber: smoked sheet (57.6%), reogen (1.2%), stearic acid (1.4%), zinc oxide (2%), agerite resin D (0.9%), agerite HP (0.3%), antozite 675 (2.3%), microcrystalline wax (0.6%), philrich 5 (2.9%), HAF (28.8%), sulfur (1.4%), amax No. 1 (0.3%), and redax (0.3%). Gross heats of combustion were determined for the solid residue and organic liquid.

gross heat of combustion:

solid residue

$$q_v(\text{gross}) = 17000 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9600 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 40000 \text{ J g}^{-1}$$

organic liquid

$$q_v(\text{gross}) = 13000 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7200 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 30000 \text{ J g}^{-1}$$

74COL/DOW

GR-S RUBBER; solid; composed of 1-3 butadiene and 25 wt. % styrene. Analysis of material gave the following in percent by weight: carbon = 88.954, hydrogen = 10.2607, ash = 0.37, soap as sodium oleate = 0.42, fatty acid as oleic acid = 0.92, modifier = 0.44, phenyl-beta-naphthylamine = 0.50, and amount soluble in ethanol-toluene azeotrope = 5.6.

specific heat:

temperature		$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
(K)	($^\circ\text{F}$)			
5	-450.4	0.0010	0.0010	0.004
10	-441.4	0.0067	0.0067	0.028
50	-369.4	0.081	0.081	0.338
100	-279.4	0.146	0.146	0.612
200	-99.4	0.268	0.268	1.12
300	80.6	0.454	0.454	1.90

44RAN/FER

PURIFIED NATURAL RUBBER HYDROCARBON; solid; prepared by digestion of latex with steam at 190°C (374°F) and extraction of resins and products of hydrolysis with alcohol and water. Nitrogen content was about 0.03%; ash content average 0.12%; benzene-insoluble constituents averaged 0.1%-0.3%.

specific heat:

temperature (K) (°F)	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
15 -432	0.017	0.017	0.073
20 -423	0.028	0.028	0.117
50 -369	0.084	0.084	0.352
100 -279	0.154	0.154	0.646
200 - 99	0.344	0.344	1.44
300 80	0.452	0.452	1.89

heat of fusion: at 110°C (51.8°F).

$$L_f = 7.18 \text{ Btu lb}^{-1}$$

$$L_f = 3.99 \text{ cal g}^{-1}$$

$$L_f = 16.7 \text{ J g}^{-1}$$

35BEK/MAT

RUBBER; solid; (sample 1): latex, digested with water at 190°C (374°F), extracted with water and ethanol; soluble in ether; 0.02% ash; (sample 2): latex, trypsin treated; 75% ether soluble, 25% ether insoluble.

gross heat of combustion: 30°C (86°F)

sample 1, 0.02% ash

$$q_v(\text{gross}) = 19465 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10814 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45247 \text{ J g}^{-1}$$

sample 2, 0.4% ash

$$q_v(\text{gross}) = 19355 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10753 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 44991 \text{ J g}^{-1}$$

sample 2, 0.15% ash

$$q_v(\text{gross}) = 19411 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10784 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45120 \text{ J g}^{-1}$$

sample 2, ether soluble fraction, 0.1% ash

$$q_v(\text{gross}) = 19444 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10802 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45196 \text{ J g}^{-1}$$

sample 2, ether insoluble fraction, 0.7% ash

$$q_v(\text{gross}) = 19343 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10746 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 44961 \text{ J g}^{-1}$$

sample 2, ether insoluble fraction, 1.8% ash

$$q_v(\text{gross}) = 19129 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 10627 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 44464 \text{ J g}^{-1}$$

34JES/CUM

RUBBER-SULFUR COMPOUNDS; solid; repeating unit: $[(C_5H_8)_x S_y]$; x varies between 1 and 4; y varies between 0 and 3; maximum sulfur content ~32%.

gross heat of combustion: at 30°C (86°F), sulfur as gaseous SO₂.

$$q_v(\text{gross}) = 10791 - 9041 m \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 45150 - 37828 m \text{ J g}^{-1}$$

m is grams of sulfur per gram of compound

34JES/CUM

TIRE; solid; typical compounding formulae for passenger tire treads.

	Natural rubber %	SBR cis-polybutadiene* %
Smoked sheet	57.6	-
SBR 1712	-	46.8
cis-Polybutadiene	-	11.3
Reogen	1.2	-
K-Stay G	-	2.3
Stearic acid	1.4	0.9
Zinc oxide	2	1.4
Agerite resin D	0.9	0.7
Agerite HP	0.3	0.2
Antozite 67S	2.3	1.8
Microcrystalline wax	0.6	0.5
Philrich 5	2.9	3.2
HAF	28.8	-
ISAF	-	29.5
Sulfur	1.4	0.8
Amax No. 1	0.3	-
Amax	-	0.7
Redax	0.3	-

*SBR is styrene-butadiene rubber

gross heat of decomposition: at 375°C (707°F) the mean value is for random samples of black-sidewall tire tread; products are a liquid distillate with a heat of combustion $q_v = 40000 \text{ J g}^{-1}$ (10000 cal g⁻¹) (18000 Btu lb⁻¹) and a combustible gas.

$$q_v(\text{gross}) = 1260 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 700 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 3000 \text{ J g}^{-1}$$

gross heat of combustion: value for the tire residue remaining after heating to 1000°C (1832°F).

$$q_v(\text{gross}) = 14000 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7800 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 32640 \text{ J g}^{-1}$$

74COL/DOW

Vegetable Oils

BARLEY OIL; liquid; oil from barley, *Hordeum vulgare*; obtained by ether extraction.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 16330 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9070 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 37950 \text{ J g}^{-1}\end{aligned}$$

55MER/WAT

CASTOR OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 1.09, stearic = 3.10, oleic = 4.85, linoleic = 1.27, and ricinoleic = 89.60. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.21, the phosphorus = 3.0 ppm, peroxide value (milli-equivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 9.6, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.22, ash (% by weight) = 0.01, and sulfur (% by weight) = 0.01. Density = 0.9537 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 16036 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 8909 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 37274 \text{ J g}^{-1}\end{aligned}$$

82GOE/SCH

CASTOR OIL; liquid; oil from seeds of the castor bean, *Ricinus communis*; chief constituent: glyceride of ricinoleic acid (12-hydroxyoleic acid). Saponification number 175-183. Iodine number 83 after heating at 100°C (212°F) for 3 to 6 hours at 2-3 mm pressure; density is 0.945-0.965 g cm⁻³ at 25°C (77°F).

specific heat: 298-548 K (77°-527°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.41281 + 1.2259 \times 10^{-3} T - 3.4892 \times 10^{-6} T^2 + 3.8820 \times 10^{-9} T^3 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= -1.265 + 0.01241 T - 2.8650 \times 10^{-5} T^2 + 2.264 \times 10^{-8} T^3 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= -5.292 + 0.05192 T - 1.1987 \times 10^{-4} T^2 + 9.474 \times 10^{-8} T^3\end{aligned}$$

46CLA/WAL

COCONUT OIL; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 255. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 10.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	Btu lb $^{-1}$	$H^{\circ}(t)-H^{\circ}(-50^{\circ}\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	15.21	8.45	35.35
0	32	37.30	20.72	86.69
25	77	89.62	49.79	208.32
50	122	124.97	69.43	290.50
55	131	129.22	71.79	300.37

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 55.1 \text{ Btu lb}^{-1}$$

$$L_f = 30.6 \text{ cal g}^{-1}$$

$$L_f = 128.0 \text{ J g}^{-1}$$

55RIE

COCONUT OIL; liquid; extracted from coconut meat, *Cocos nucifera*; mixture of glycerides of lauric (~48%) and myristic (~17.5%) acids; remainder made up of glycerides of caprylic, capric, palmitic, stearic, oleic, and linoleic acids. Saponification number 253-262.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16330 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9070 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 37950 \text{ J g}^{-1}$$

55MER/WAT

CORN OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 11.67, stearic = 1.85, oleic = 25.16, linoleic = 60.60, linolenic = 0.48, and arachidic = 0.24. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.11, the phosphorus = 7.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 18.4, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.24, ash (% by weight) = 0.01, and sulfur (% by weight) = 0.01. Density = 0.9095 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 16993 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9441 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 39500 \text{ J g}^{-1}\end{aligned}$$

82GOE/SCH

CORN OIL (MAIZE); liquid; extracted from corn (maize), *Zea mays*; typical analysis: triglycerides, 98.6%; unsaponifiable, 1.4%; sitosterol, 1%; fatty acid composition: palmitic, 2%; stearic, 3.5%; oleic, 46.3%; linoleic, 42.0%; Iodine number 117-130.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 16700 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9280 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 38830 \text{ J g}^{-1}\end{aligned}$$

55MER/WAT

COTTONSEED OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 28.33, stearic = 0.89, oleic = 13.27, and linoleic = 57.51. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.07, the phosphorus = 8.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 64.8, water and sediment (% by volume) = 0.04, carbon residue (% by weight) = 0.24, ash (% by weight) = 0.01, and sulfur (% by weight) = 0.01. Density = 0.9148 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 16980 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9433 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 39468 \text{ J g}^{-1}\end{aligned}$$

82GOE/SCH

Vegetable Oils

COTTONSEED OIL, HYDROGENATED; liquid; yellow oil from various *Gossypium* species; chief constituents are glycerides of palmitic (~21%); oleic (~33%); stearic (~2%); and linoleic (~44%) acids; density, 0.91-0.92 g cm⁻³; before measurement, oil was heated at 100°C (212°F) for 3 to 6 hours at 2-3 mm of Hg to remove moisture. Iodine number 6.5.

specific heat: 353-543 K (176°-518°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.4962 + 8.859 \times 10^{-5} T + 3.8265 \times 10^{-7} T^2 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.5363 - 4.7376 \times 10^{-4} T + 1.2398 \times 10^{-6} T^2 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 2.2439 - 1.9822 \times 10^{-3} T + 5.1875 \times 10^{-6} T^2\end{aligned}$$

46CLA/WAL

COTTONSEED OIL, REFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 195. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 107.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature		H°(t)-H°(-50°C)		
(°C)	(°F)	Btu lb ⁻¹	cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	23.74	13.19	55.19
0	32	60.16	33.42	139.83
25	77	86.62	48.12	201.33
50	122	107.86	59.92	250.71
55	131	112.16	62.31	260.71

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$\begin{aligned}L_f &= 30.2 \text{ Btu lb}^{-1} \\L_f &= 16.8 \text{ cal g}^{-1} \\L_f &= 70.3 \text{ J g}^{-1}\end{aligned}$$

55RIE

CRAMBE OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 2.07, stearic = 0.70, oleic = 18.86, linoleic = 9.00, linolenic = 6.85, arachidic = 2.09, behenic = 0.80, lignoceric = 1.12, and erucic = 58.51. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.36, the phosphorus = 12.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 26.5, water and sediment (% by volume) = 0.2, carbon residue (% by weight) = 0.23, ash (% by weight) = 0.05, and sulfur (% by weight) = 0.01. Density = 0.9044 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 17416 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9675 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 40482 \text{ J g}^{-1}\end{aligned}$$

82GOE/SCH

GROUND NUT SEED OIL; liquid; Material was extracted from industrially stored oil seeds and the acid value was 10.1 mg KOH/g. Specific gravity, (15/15°C) = 0.9210. Fatty acids found in the oil: lauric (0.15%), linoleic (37.00%), palmitic (17.40%), palmitoleic (0.60%), stearic (2.30%), oleic (39.00%), linolenic (1.38%), eicosenoic (2.62%), and erucic (0.55%).

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 17118 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9510 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 39790 \text{ J g}^{-1}\end{aligned}$$

75KOM/DAN

HIGH OLEIC SAFFLOWER OIL; liquid; The vegetable oil is a genetic variant of normal safflower oil and has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 5.46, stearic = 1.75, oleic = 79.36, linoleic = 12.86, arachidic = 0.23, and myristic = 0.34. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.26, the phosphorus = 0.42 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 13.6, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.24, ash (% by weight) = 0.001, and sulfur (% by weight) = 0.02. Density = 0.9021 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 17000 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9445 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 39516 \text{ J g}^{-1}\end{aligned}$$

82GOE/SCH

Vegetable Oils

LINSEED OIL; liquid; Material was extracted from industrially stored oil seeds and the acid value was 3.81 mg KOH/g. Density (15°C) = 0.929 g cm⁻³. Fatty acids found in the oil: palmitic (8.77%), stearic (5.67%), oleic (21.98%), linoleic (12.26%), and linolenic (51.32%).

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 17073 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9485 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 39685 \text{ J g}^{-1}\end{aligned}$$

75KOM/DAN

LINSEED OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 4.92, stearic = 2.41, oleic = 19.70, linoleic = 18.03, and linolenic = 54.94. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.20, the phosphorus = 6.0 ppm, peroxide value (milli-equivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 33.7, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.22, ash (% by weight) = 0.01, and sulfur (% by weight) = 0.01. Density = 0.9236 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 16910 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 9395 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 39307 \text{ J g}^{-1}\end{aligned}$$

82GOE/SCH

LINSEED OIL; liquid; (flaxseed oil); obtained from dried seeds of flax, *Linum usitatissimum*; chief constituents are glycerides of linoleic (~61.5%), linolenic (~25.0%), palmitic (~5%), oleic (~5%), and stearic (~3.5%) acids; iodine number 172.1; density, 0.930-0.938 g cm⁻³.

specific heat: sample was heated at 100°C (212°F) for 3 to 6 hours under a pressure of 2-3 mm of Hg to remove moisture; equations valid 30°-270°C (86°-518°F).

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.41604 + 6.9526 \times 10^{-4} T - 1.6518 \times 10^{-6} T^2 + 2.1420 \times 10^{-9} T^3 \\C_p(\text{cal g}^{-1} \text{ } ^\circ\text{K}^{-1}) &= -0.4606 + 6.4288 \times 10^{-3} T - 1.4922 \times 10^{-5} T^2 + 1.2492 \times 10^{-8} T^3 \\C_p(\text{J g}^{-1} \text{ } ^\circ\text{K}^{-1}) &= -1.9272 + 2.6898 \times 10^{-2} T - 6.2434 \times 10^{-5} T^2 + 5.2267 \times 10^{-8} T^3\end{aligned}$$

46CLA/WAL

LINSEED OIL, UNREFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 190. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 176.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	Btu lb $^{-1}$	$\text{H}^{\circ}(\text{t})-\text{H}^{\circ}(-50^{\circ}\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	18.58	10.32	43.18
0	32	67.01	37.23	155.77
25	77	87.71	48.73	203.89
50	122	108.41	60.23	252.00
55	131	112.61	62.56	261.75

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 32.8 \text{ Btu lb}^{-1}$$

$$L_f = 18.2 \text{ cal g}^{-1}$$

$$L_f = 76.1 \text{ J g}^{-1}$$

55RIE

OAT OIL; liquid; obtained from oats, *Avena sativa*; obtained by ether extraction.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16070 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 8930 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 37365 \text{ J g}^{-1}$$

55MER/WAT

OLIVE OIL; liquid; mixture of glycerides of several fatty acids; chiefly glycerides of oleic acid, with lesser amounts of palmitic, stearic, and linoleic acids. Saponification number 185-196.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17050 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9470 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39620 \text{ J g}^{-1}$$

55MER/WAT

Vegetable Oils

OLIVE OIL, ITALIAN; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 194. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 96.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature (°C)	(°F)	Btu lb ⁻¹	H°(t)-H°(-50°C) cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	17.10	9.50	39.75
0	32	62.08	34.49	144.31
25	77	91.51	50.84	212.71
50	122	112.73	62.63	262.04
55	131	117.02	65.01	272.00

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 36.5 \text{ Btu lb}^{-1}$$

$$L_f = 20.3 \text{ cal g}^{-1}$$

$$L_f = 84.9 \text{ J g}^{-1}$$

55RIE

PALM OIL, HARDENED; solid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 199. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 60.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature (°C)	(°F)	Btu lb ⁻¹	H°(t)-H°(-50°C) cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	16.24	9.02	37.74
0	32	36.99	20.55	85.98
25	77	73.98	41.10	171.96
50	122	126.58	70.32	294.22
55	131	131.02	72.79	304.55

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 57.2 \text{ Btu lb}^{-1}$$

$$L_f = 31.8 \text{ cal g}^{-1}$$

$$L_f = 133.1 \text{ J g}^{-1}$$

55RIE

PALM OIL, UNREFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 200. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 55.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature		Btu lb ⁻¹	H°(t)-H°(-50°C)	
(°C)	(°F)		cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	16.25	9.03	37.78
0	32	38.75	21.53	90.08
25	77	89.68	49.82	208.45
50	122	118.71	65.95	275.93
55	131	123.07	68.37	286.06

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 46.4 \text{ Btu lb}^{-1}$$

$$L_f = 25.8 \text{ cal g}^{-1}$$

$$L_f = 107.9 \text{ J g}^{-1}$$

55RIE

PALM-KERNEL OIL; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 242. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 16.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature		Btu lb ⁻¹	H°(t)-H°(-50°C)	
(°C)	(°F)		cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	15.57	8.65	36.19
0	32	40.14	22.30	93.30
25	77	94.14	52.30	218.82
50	122	124.97	69.43	290.50
55	131	129.38	71.88	300.75

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 57.6 \text{ Btu lb}^{-1}$$

$$L_f = 32.0 \text{ cal g}^{-1}$$

$$L_f = 133.9 \text{ J g}^{-1}$$

55RIE

Vegetable Oils

PEANUT OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 11.38, stearic = 2.39, oleic = 48.28, linoleic = 31.95, linolenic = 0.93, arachidic = 1.32, behenic = 2.52, and lignoceric = 1.23. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.20, the phosphorus = 9.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 82.7, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.24, ash (% by weight) = 0.005, and sulfur (% by weight) = 0.01. Density = 0.9026 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17115 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9508 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39782 \text{ J g}^{-1}$$

82GOE/SCH

PEANUT OIL, UNREFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 192. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 92.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^\circ\text{C}$)	($^\circ\text{F}$)	Btu lb $^{-1}$	$H^\circ(t) - H^\circ(-50^\circ\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	16.85	9.36	39.16
0	32	66.74	37.08	155.14
25	77	90.38	50.21	210.08
50	122	112.12	62.29	260.62
55	131	116.53	64.74	270.87

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 34.2 \text{ Btu lb}^{-1}$$

$$L_f = 19.0 \text{ cal g}^{-1}$$

$$L_f = 79.5 \text{ J g}^{-1}$$

55RIE

PERILLA OIL; liquid; obtained from seeds of *Perilla ocimoides*; chief constituents are glycerides of linoleic (~39%) and linolenic (~46%) acids, with small amounts of palmitic (~8%) and oleic (8%) acids; density, 0.93-0.94 g cm⁻³; before measurement, oil was heated at 100°C (212°F) for 3 to 6 hours at 2-3 mm of Hg to remove moisture. Iodine number 186.2.

specific heat: 279-543 K (43°-518°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.5350 + 1.499 \times 10^{-4} T + 3.086 \times 10^{-7} T^2 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.4082 - 2.410 \times 10^{-4} T + 1.000 \times 10^{-6} T^2 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.7081 - 1.008 \times 10^{-3} T + 4.184 \times 10^{-6} T^2 \end{aligned}$$

46CLA/WAL

POPPY SEED OIL, BLEACHED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 193. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 146.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature (°C)	(°F)	Btu lb ⁻¹	H°(t)-H°(-50°C) cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	20.09	11.16	46.69
0	32	68.58	38.10	159.41
25	77	89.39	49.66	207.78
50	122	110.11	61.17	255.94
55	131	114.30	63.50	265.68

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$\begin{aligned} L_f &= 33.3 \text{ Btu lb}^{-1} \\ L_f &= 18.5 \text{ cal g}^{-1} \\ L_f &= 77.4 \text{ J g}^{-1} \end{aligned}$$

55RIE

Vegetable Oils

RAPE OIL, REFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 175. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 105.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^{\circ}\text{C}$)	($^{\circ}\text{F}$)	Btu lb $^{-1}$	$H^{\circ}(\text{t})-H^{\circ}(-50^{\circ}\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	16.69	9.27	38.79
0	32	47.75	26.53	111.00
25	77	91.10	50.61	211.75
50	122	112.46	62.48	261.42
55	131	116.77	64.87	271.42

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 35.6 \text{ Btu lb}^{-1}$$

$$L_f = 19.8 \text{ cal g}^{-1}$$

$$L_f = 82.8 \text{ J g}^{-1}$$

55RIE

RAPESEED OIL; liquid; Material was extracted from industrially stored oil seeds and the acid value was 10.77 mg KOH/g. The specific gravity ($15/15^{\circ}\text{C}$) = 0.9134. Fatty acids found in the oil: palmitic (3.84%), palmitoleic (0.32%), stearic (1.49%), oleic (14.77%), linoleic (15.12%), linolenic (6.29%), eicosenoic (9.44%), and erucic (47.93%).

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17487 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9715 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 40648 \text{ J g}^{-1}$$

75KOM/DAN

RAPSEED OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 3.49, stearic = 0.85, oleic = 64.40, linoleic = 22.30, and linolenic = 8.23. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 1.14, the phosphorus = 18.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 30.2, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.30, ash (% by weight) = 0.054, and sulfur (% by weight) = 0.01. Density = 0.9115 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17083 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9491 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39709 \text{ J g}^{-1}$$

82GOE/SCH

RYE OIL; liquid; oil extracted from rye grain, *Secale cereale*.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16780 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9320 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 38990 \text{ J g}^{-1}$$

obtained by ether extraction

$$q_v(\text{gross}) = 16560 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9200 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 38495 \text{ J g}^{-1}$$

55MER/WAT

SAFFLOWER OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 8.60, stearic = 1.93, oleic = 11.58, and linoleic = 77.89. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.70, the phosphorus = 20.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 56.4, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.25, ash (% by weight) = 0.006, and sulfur (% by weight) = 0.01. Density = 0.9144 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17001 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9445 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39519 \text{ J g}^{-1}$$

82GOE/SCH

Vegetable Oils

SESAME OIL; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 189. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 110.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature		Btu lb ⁻¹	H°(t)-H°(-50°C)	
(°C)	(°F)		cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	18.47	10.26	42.93
0	32	64.40	35.78	149.70
25	77	86.83	48.24	201.84
50	122	107.89	59.94	250.79
55	131	112.19	62.33	260.79

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 29.3 \text{ Btu lb}^{-1}$$

$$L_f = 16.3 \text{ cal g}^{-1}$$

$$L_f = 68.2 \text{ J g}^{-1}$$

55RIE

SESAME OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 13.10, stearic = 3.92, oleic = 52.84, and linoleic = 30.14. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 4.96, the phosphorus = 10.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 22.4, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.25, ash (% by weight) = 0.01, and sulfur (% by weight) = 0.01. Density = 0.9133 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16928 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9405 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39349 \text{ J g}^{-1}$$

82GOE/SCH

SOYBEAN OIL; liquid; the bean of *Soia hispida* (*Leguminosae*); average composition: proteins, 40%; oils, 18%; phosphatides, 2%; remainder urease, raffinose, stachyose, saponins, phytosterins, and isoflavone; density is 0.925 g cm^{-3} at 15°C (50°F). Saponification number 189-193.5; iodine number 122-134.

specific heat: sample was heated at 100°C (212°F) for 3 to 6 hours under a pressure of 2-3 mm of Hg to remove moisture.

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= 0.47779 + 5.2622 \times 10^{-4} T - 4.8470 \times 10^{-7} T^2 + 9.7171 \times 10^{-10} T^3 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.03911 + 2.858 \times 10^{-3} T - 5.912 \times 10^{-6} T^2 + 5.667 \times 10^{-9} T^3 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.16362 + 1.1957 \times 10^{-2} T - 2.474 \times 10^{-5} T^2 + 2.371 \times 10^{-8} T^3 \end{aligned}$$

46CLA/WAL

SOYBEAN OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 11.75, stearic = 3.15, oleic = 22.26, linoleic = 55.53, and linolenic = 6.31. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.20, the phosphorus = 32.0 ppm, peroxide value (milli-equivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 44.5, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.27, ash (% by weight) = 0.01, and sulfur (% by weight) = 0.01. Density = 0.9138 kg/L .

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 17046 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 9470 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 39623 \text{ J g}^{-1} \end{aligned}$$

82GOE/SCH

SOYBEAN OIL, REFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 190. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 133.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature ($^\circ\text{C}$)	($^\circ\text{F}$)	Btu lb $^{-1}$	$H^\circ(t) - H^\circ(-50^\circ\text{C})$ cal g $^{-1}$	J g $^{-1}$
-50	-58	0.00	0.00	0.00
-25	-13	18.34	10.19	42.64
0	32	65.52	36.40	152.30
25	77	87.73	48.74	203.93
50	122	108.74	60.41	252.76
55	131	112.95	62.75	262.55

(more)

Vegetable Oils

SOYBEAN OIL, REFINED - Continued

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 32.2 \text{ Btu lb}^{-1}$$

$$L_f = 17.9 \text{ cal g}^{-1}$$

$$L_f = 74.9 \text{ J g}^{-1}$$

55RIE

SUNFLOWER OIL; liquid; The vegetable oil has a chemical composition of up to 3 fatty acids linked to a glycerine molecule with ester linkages; the fatty acid composition in percent by weight is palmitic = 6.08, stearic = 3.26, oleic = 16.93, and linoleic = 73.73. The acid value (number of mg of KOH needed to neutralize free fatty acids in 1 g sample) = 0.15, the phosphorus = 15.0 ppm, peroxide value (milliequivalents of peroxide per 1000 g sample that oxidize KI during test conditions) = 10.7, water and sediment (% by volume) = trace, carbon residue (% by weight) = 0.23, ash (% by weight) = 0.01, and sulfur (% by weight) = 0.01. Density = 0.9161 kg/L.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17026 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9459 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39575 \text{ J g}^{-1}$$

82GOE/SCH

SUNFLOWER, SEED OIL; liquid; Material was extracted from industrially stored oil seeds and the acid value was 3.81 mg KOH/g. Specific gravity (15/15°C) = 0.9208. Fatty acids found in the oil: palmitic (7.06%), stearic (9.41%), oleic (23.33%), linoleic (56.66%), and linolenic (2.10%).

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 17226 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9570 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 40041 \text{ J g}^{-1}$$

75KOM/DAN

SUNFLOWER OIL, UNREFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 186. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 135.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature (°C)	(°F)	Btu lb ⁻¹	H°(t)-H°(-50°C) cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	16.92	9.40	39.33
0	32	69.48	38.60	161.50
25	77	90.14	50.08	209.53
50	122	111.22	61.79	258.53
55	131	115.47	64.15	268.40

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 34.2 \text{ Btu lb}^{-1}$$

$$L_f = 19.0 \text{ cal g}^{-1}$$

$$L_f = 79.5 \text{ J g}^{-1}$$

55RIE

TUNG OIL; liquid; a yellow drying oil from the nuts of the trees *Aleurites cordata* and *Aleurites fordii*; glycerides of eleostearic (~80%); palmitic (~4%); stearic (~1%); and oleic (~15%) acids; density, 0.936-0.942 g cm⁻³; before measurement, oil was heated at 100°C (212°F) for 3 to 6 hours at 2-3 mm of Hg pressure to remove moisture. Iodine number 154.4.

specific heat: 293-473 K (68°-392°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.37651 + 7.9928 \times 10^{-4} T - 1.9479 \times 10^{-6} T^2 + 2.0881 \times 10^{-9} T^3$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = -0.6053 + 7.0447 \times 10^{-3} T - 1.5641 \times 10^{-5} T^2 + 1.2178 \times 10^{-8} T^3$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = -2.5324 + 2.9475 \times 10^{-2} T - 6.4687 \times 10^{-5} T^2 + 5.0954 \times 10^{-8} T^3$$

46CLA/WAL

Vegetable Oils

WHEAT OIL; liquid; from wheat grain, *Triticum aestivum*.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 16850 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9360 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 39162 \text{ J g}^{-1}$$

oil obtained by ether extraction

$$q_v(\text{gross}) = 16330 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 9070 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 37950 \text{ J g}^{-1}$$

55MER/WAT

Woody and Tree Materials

ALDER, EUROPEAN BLACK; *Alnus glutinosa*; solid; Each tree was separated into small parts (being less than 0.64 cm (1/4 in.) in diameter and roughly equivalent to tops and branches) and large parts with the weighted proportion of small (25%) and large (75%) material in the whole tree. Overall mean specific gravity for whole tree = 0.37 (oven dry weight and green volume). Bark proportion of whole tree = 23%.

gross heat of combustion: oven-dried, assume values refer to room temperature.

small parts

$$\begin{aligned}q_v(\text{gross}) &= 7965 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4425 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18514 \text{ J g}^{-1}\end{aligned}$$

large parts

$$\begin{aligned}q_v(\text{gross}) &= 8248 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4582 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19171 \text{ J g}^{-1}\end{aligned}$$

whole tree

$$\begin{aligned}q_v(\text{gross}) &= 8177 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4543 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19008 \text{ J g}^{-1}\end{aligned}$$

81GEY

ALDER, RED; BARK; *Alnus rubra*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 3.1%; moisture content = 5.8%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 7947 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4415 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18472 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

ASH; *Fraxinus excelsior*; solid; ultimate analysis: carbon, 49.18%; hydrogen, 6.27%; nitrogen, 0.07%; ash, 0.57%.

gross heat of combustion: 20°C (68°F); air-dried at 110°-115°C (230°-240°F), ash free.

$$\begin{aligned}q_v(\text{gross}) &= 8507 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4726 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19774 \text{ J g}^{-1}\end{aligned}$$

1883GOT

Woody and Tree Materials

ASH, GREEN; *Fraxinus pennsylvanica*; solid; Mean age = 12 years, mean basal stem diameter = 7.0 cm, mean stem bark (proportion of dry weight) = 12.3%, ash content (proportion of oven dry weight) of components of sample: wood = 0.71%, branches = 1.9%, twigs = 2.2%, bark = 6.7% and leaves = 4.9%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned}q_v(\text{gross}) &= 8582 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4768 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19949 \text{ J g}^{-1}\end{aligned}$$

bark:

$$\begin{aligned}q_v(\text{gross}) &= 8312 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4618 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19322 \text{ J g}^{-1}\end{aligned}$$

branches:

$$\begin{aligned}q_v(\text{gross}) &= 8743 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4857 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20322 \text{ J g}^{-1}\end{aligned}$$

twigs:

$$\begin{aligned}q_v(\text{gross}) &= 8672 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4818 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20159 \text{ J g}^{-1}\end{aligned}$$

leaves:

$$\begin{aligned}q_v(\text{gross}) &= 9214 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5119 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21418 \text{ J g}^{-1}\end{aligned}$$

79NEE/STE

ASH, GREEN; *Fraxinus pennsylvanica*; solid; Material was collected from the southern Atlantic and Gulf coastal plains in bottom-, swamp- and wet flat-land natural stand sites. Samples were dried at 70°C (158°F) to a constant weight; reported values were averaged over all positions of similar plant tissue for each tree and six trees per species were used.

gross heat of combustion: assume values refer to room temperature; values are on a dry weight basis.

bole wood

$$\begin{aligned}q_v(\text{gross}) &= 8356 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4642 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19422 \text{ J g}^{-1}\end{aligned}$$

bole bark

$$\begin{aligned}q_v(\text{gross}) &= 8235 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4575 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19142 \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 8422 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4679 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19577 \text{ J g}^{-1}\end{aligned}$$

branch wood

$$\begin{aligned}q_v(\text{gross}) &= 8449 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4694 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19640 \text{ J g}^{-1}\end{aligned}$$

branch bark

$$\begin{aligned}q_v(\text{gross}) &= 8426 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4681 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19585 \text{ J g}^{-1}\end{aligned}$$

82GOW/FRE

ASH, WHITE; *Fraxinus americana*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, one at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight.

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned}q_v(\text{gross}) &= 8433 (108) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4685 (60) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19602 (251) \text{ J g}^{-1}\end{aligned}$$

bole without bark

$$\begin{aligned}q_v(\text{gross}) &= 8395 (59) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4664 (33) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 190514 (138) \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 8638 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4799 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20079 \text{ J g}^{-1}\end{aligned}$$

branch with bark

$$\begin{aligned}q_v(\text{gross}) &= 8654 (128) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4808 (71) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20117 (297) \text{ J g}^{-1}\end{aligned}$$

branch without bark

$$\begin{aligned}q_v(\text{gross}) &= 8680 (175) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4822 (97) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20175 (406) \text{ J g}^{-1}\end{aligned}$$

81MUS/HOC

ASH, WHITE; *Fraxinus americana*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.63 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.327 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.327 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.368\end{aligned}$$

12DUN

ASPEN, QUAKING; *Populus tremuloides*; solid; air-dried at 105°-110°C (221°-230°F), density, 0.43 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.329$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.329$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 1.377$$

12DUN

ASPEN, QUAKING; BARK; *Populus tremuloides*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 2.8%; moisture content = 5.5%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$q_v(\text{gross}) = 8433 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4685 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19602 \text{ J g}^{-1}$$

55CHA/MIT

ASPEN, QUAKING; FOLIAGE; *Populus tremuloides*; solid; freeze-dried to < 10% moisture content. Composition is ash = 4.97% and char yield = 27.8%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$q_v(\text{gross}) = 9740 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5410 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 22650 \text{ J g}^{-1}$$

char (from 500°C heating)

$$q_v(\text{gross}) = 13940 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7740 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 32400 \text{ J g}^{-1}$$

82SUS

ASPEN, TREMBLING; *Populus tremuloides*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, and at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight.

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned}q_v(\text{gross}) &= 8782 (50) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4879 (28) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20414 (117) \text{ J g}^{-1}\end{aligned}$$

bole without bark

$$\begin{aligned}q_v(\text{gross}) &= 8905 (56) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4947 (31) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20698 (130) \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 9648 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5360 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22426 \text{ J g}^{-1}\end{aligned}$$

branch with bark

$$\begin{aligned}q_v(\text{gross}) &= 8957 (61) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4976 (34) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20820 (142) \text{ J g}^{-1}\end{aligned}$$

branch without bark

$$\begin{aligned}q_v(\text{gross}) &= 8773 (32) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4874 (18) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20393 (75) \text{ J g}^{-1}\end{aligned}$$

81MUS/HOC

BEECH; *Fagus atropunicea*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.75 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.326 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.326 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.364\end{aligned}$$

12DUN

Woody and Tree Materials

BEECH; *Fagus silvatica*; solid; ultimate analysis: carbon, 49.06%; hydrogen, 6.11%; nitrogen, 0.09%; ash, 0.57%.

gross heat of combustion: 20°C (68°F), air-dried at 110°-115°C (230°-240°F), ash free.

$$q_v(\text{gross}) = 8624 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4791 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 20046 \text{ J g}^{-1}$$

1883GOT

BEEFWOOD (SHE-OAK); *Casuarina equisetifolia*; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 78.94, ash content = 1.40, and fixed carbon = 19.66. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.61, hydrogen = 5.83, oxygen = 43.36, nitrogen = 0.59, sulfur = 0.02, chlorine = 0.16, and residue (ash) = 1.43.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$q_v(\text{gross}) = 8363 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4646 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19440 \text{ J g}^{-1}$$

net heat of combustion: assume values refer to room temperature.

$$q_v(\text{net}) = 7856 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 4364 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 18260 \text{ J g}^{-1}$$

85JEN/EBE

BIRCH; *Betula alba*; solid; ultimate analysis: carbon, 48.88%; hydrogen, 6.06%; nitrogen, 0.10%; ash, 0.29%; oxygen, 44.67%.

gross heat of combustion: 20°C (68°F), air-dried at 110°-115°C (230°-240°F), ash free.

$$\begin{aligned}q_v(\text{gross}) &= 8588 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4771 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19962 \text{ J g}^{-1}\end{aligned}$$

1883GOT

air dried one hour at 105°C (221°F)

$$\begin{aligned}q_v(\text{gross}) &= 8458 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4699 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19661 \text{ J g}^{-1}\end{aligned}$$

22PAR/DAV

BIRCH, PAPER; *Betula papyrifera*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, and at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight.

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned}q_v(\text{gross}) &= 9207 (56) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5115 (31) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21401 (130) \text{ J g}^{-1}\end{aligned}$$

branch with bark

$$\begin{aligned}q_v(\text{gross}) &= 9245 (70) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5136 (39) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21489 (163) \text{ J g}^{-1}\end{aligned}$$

bole without bark

$$\begin{aligned}q_v(\text{gross}) &= 8948 (86) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4971 (48) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20799 (201) \text{ J g}^{-1}\end{aligned}$$

branch without bark

$$\begin{aligned}q_v(\text{gross}) &= 9074 (54) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5041 (30) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21092 (126) \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 9428 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5238 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21916 \text{ J g}^{-1}\end{aligned}$$

81MUS/HOC

BIRCH, PAPER; BARK; *Betula papyrifera*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 1.5%; moisture content = 4.8%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned} q_v(\text{gross}) &= 9434 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5241 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21928 \text{ J g}^{-1} \end{aligned}$$

55CHA/MIT

BIRCH, YELLOW; *Betula alleghaniensis*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, one at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight.

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned} q_v(\text{gross}) &= 8838 (175) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4910 (97) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20543 (406) \text{ J g}^{-1} \end{aligned}$$

bole without bark

$$\begin{aligned} q_v(\text{gross}) &= 8498 (133) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4721 (74) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19753 (310) \text{ J g}^{-1} \end{aligned}$$

foliage

$$\begin{aligned} q_v(\text{gross}) &= 8503 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4724 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19765 \text{ J g}^{-1} \end{aligned}$$

branch with bark

$$\begin{aligned} q_v(\text{gross}) &= 9002 (247) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5001 (137) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20924 (573) \text{ J g}^{-1} \end{aligned}$$

branch without bark

$$\begin{aligned} q_v(\text{gross}) &= 8917 (101) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4954 (56) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20728 (234) \text{ J g}^{-1} \end{aligned}$$

81MUS/HOC

BIRCH, YELLOW; BARK; *Betula alleghaniensis*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 1.7%; moisture content = 5.2%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 9076 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5042 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21096 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

BLACKGUM; *Nyssa sylvatica*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.52 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= 0.325 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.325 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.360\end{aligned}$$

12DUN

BLACKGUM; *Nyssa sylvatica*; solid; Material was collected from the southern Atlantic and Gulf coastal plains in bottom-, swamp- and wet flat-land natural stand sites. Samples were dried at 70°C (158°F) to a constant weight; reported values were averaged over all positions of similar plant tissue for each tree and six trees per species were used.

gross heat of combustion: assume values refer to room temperature; values are on a dry weight basis.

bole wood

$$\begin{aligned}q_v(\text{gross}) &= 8465 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4703 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19677 \text{ J g}^{-1}\end{aligned}$$

bole bark

$$\begin{aligned}q_v(\text{gross}) &= 8397 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4665 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19518 \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 8991 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4995 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20899 \text{ J g}^{-1}\end{aligned}$$

branch wood

$$\begin{aligned}q_v(\text{gross}) &= 8564 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4758 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19907 \text{ J g}^{-1}\end{aligned}$$

branch bark

$$\begin{aligned}q_v(\text{gross}) &= 8456 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4809 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20121 \text{ J g}^{-1}\end{aligned}$$

82GOW/FRE

BLACKGUM, BARK; *Nyssa sylvatica*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 7.2%; moisture content = 6.0%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned} q_v(\text{gross}) &= 7936 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4409 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18447 \text{ J g}^{-1} \end{aligned}$$

55CHA/MIT

BOXELDER; *Acer negundo*; solid; Each tree was separated into small parts (being less than 0.64 cm (1/4 in.) in diameter and roughly equivalent to tops and branches) and large parts with the weighted proportion of small (25%) and large (75%) material in the whole tree. Overall mean specific gravity for whole tree = 0.36 (oven dry weight and green volume). Bark proportion of whole tree = 14%.

gross heat of combustion: oven-dried, assume values refer to room temperature.

small parts

$$\begin{aligned} q_v(\text{gross}) &= 7981 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4434 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18552 \text{ J g}^{-1} \end{aligned}$$

large parts

$$\begin{aligned} q_v(\text{gross}) &= 8190 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4550 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19037 \text{ J g}^{-1} \end{aligned}$$

whole tree

$$\begin{aligned} q_v(\text{gross}) &= 8138 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4521 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18916 \text{ J g}^{-1} \end{aligned}$$

81GEY

BOXELDER; *Acer negundo*; solid; mean age = 11 years, mean basal stem diameter = 8.97 cm, mean stem bark (proportion of dry weight) = 9.13%, ash content (proportion of oven dry weight) of components of sample: wood = 0.78%, branches = 1.6%, twigs = 2.9%, bark = 9.5%, and leaves = 6.2%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned} q_v(\text{gross}) &= 8809 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4894 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20477 \text{ J g}^{-1} \end{aligned}$$

twigs:

$$\begin{aligned} q_v(\text{gross}) &= 8708 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4838 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20242 \text{ J g}^{-1} \end{aligned}$$

bark:

$$\begin{aligned} q_v(\text{gross}) &= 7778 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4321 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18079 \text{ J g}^{-1} \end{aligned}$$

leaves:

$$\begin{aligned} q_v(\text{gross}) &= 9050 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5028 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21037 \text{ J g}^{-1} \end{aligned}$$

branches:

$$\begin{aligned} q_v(\text{gross}) &= 8786 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4881 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20422 \text{ J g}^{-1} \end{aligned}$$

79NEE/STE

CABBAGE WOOD; *Ligustrum vulgare*; solid; Material is a shrub, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of stem and branch wood = 0.7%; stem and branch bark = 4.9%; leaf = 9.0%; root = 6.8%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
stem and branch wood (4 measurements)				
$q_v(\text{gross}) =$	8318	8375	57.2	Btu lb ⁻¹
$q_v(\text{gross}) =$	4621	4653	31.8	cal g ⁻¹
$q_v(\text{gross}) =$	19334	19468	133	J g ⁻¹
stem and branch bark (4 measurements)				
$q_v(\text{gross}) =$	8194	8624	96.7	Btu lb ⁻¹
$q_v(\text{gross}) =$	4552	4791	53.7	cal g ⁻¹
$q_v(\text{gross}) =$	19046	20046	225	cal g ⁻¹

(more)

Woody and Tree Materials

CABBAGE WOOD - Continued

	dry weight basis	ash-free dry weight basis	std dev. of mean	
leaf (5 measurements)				
$q_v(\text{gross}) =$	8438	9268	67.7	Btu lb ⁻¹
$q_v(\text{gross}) =$	4688	5149	37.6	cal g ⁻¹
$q_v(\text{gross}) =$	19615	21543	157	J g ⁻¹
root (4 measurements)				
$q_v(\text{gross}) =$	8168	8771	51.5	Btu lb ⁻¹
$q_v(\text{gross}) =$	4538	4873	28.6	cal g ⁻¹
$q_v(\text{gross}) =$	18987	20389	120	J g ⁻¹

75PAP

CEDAR, RED; *Juniperus virginiana*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.46 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.324$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.324$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 1.356$$

12DUN

CHAMISE, FOLIAGE; *Adenostoma fasciculatum*; solid; freeze dried to < 10% moisture content. Composition is ash = 3.50% and char yield = 28.6%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9430 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13490 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5240 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7490 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 21910 \text{ J g}^{-1}$	$q_v(\text{gross}) = 31350 \text{ J g}^{-1}$

82SUS

CHAPARRAL; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 75.19, ash content = 6.13, and fixed carbon = 18.68. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 46.90, hydrogen = 5.08, oxygen = 40.17, nitrogen = 0.54, sulfur = 0.03, chlorine = 0.02, and residue (ash) = 7.26.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$q_v(\text{gross}) = 8006 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4448 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18610 \text{ J g}^{-1}$$

net heat of combustion: assume values refer to room temperature.

$$q_v(\text{net}) = 7563 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 4202 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 17580 \text{ J g}^{-1}$$

85JEN/EBE

CHERRY; genus *Prunus*; solid.

gross heat of combustion: assume values refer to room temperature.

as received: 8.85% moisture

air dried one hour at 105°C (221°F)

$$q_v(\text{gross}) = 7866 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4370 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18282 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 8629 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4794 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 20058 \text{ J g}^{-1}$$

1883GOT

Woody and Tree Materials

CHERRY, BLACK; *Prunus serotina*; solid; mean age = 12.3 years, mean basal stem diameter = 8.9 cm, mean stem bark (proportion of dry weight) = 9.9%, ash content (proportion of oven dry weight) of components of sample: wood = 0.41%, branches = 0.8%, twigs = 1.7%, bark = 4.2%, and leaves = 5.6%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned} q_v(\text{gross}) &= 8579 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4766 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19941 \text{ J g}^{-1} \end{aligned}$$

twigs:

$$\begin{aligned} q_v(\text{gross}) &= 8759 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4866 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20359 \text{ J g}^{-1} \end{aligned}$$

bark:

$$\begin{aligned} q_v(\text{gross}) &= 8906 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4948 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20702 \text{ J g}^{-1} \end{aligned}$$

leaves:

$$\begin{aligned} q_v(\text{gross}) &= 9418 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5232 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21891 \text{ J g}^{-1} \end{aligned}$$

branches:

$$\begin{aligned} q_v(\text{gross}) &= 8714 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4841 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20255 \text{ J g}^{-1} \end{aligned}$$

79NEE/STE

CHERRY, CORNELIAN; *Cornus mas*; solid; Material is a tree, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of stem and branch wood = 0.7%; stem and branch bark = 10.0%; leaf = 14.0%; root = 8.3%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
stem and branch wood (3 measurements)				
$q_v(\text{gross}) =$	8404	8462	20.3	Btu lb ⁻¹
$q_v(\text{gross}) =$	4669	4701	11.3	cal g ⁻¹
$q_v(\text{gross}) =$	19535	19669	47.3	J g ⁻¹
stem and branch bark (4 measurements)				
$q_v(\text{gross}) =$	8172	8987	29.5	Btu lb ⁻¹
$q_v(\text{gross}) =$	4540	4993	16.4	cal g ⁻¹
$q_v(\text{gross}) =$	18995	20891	68.6	J g ⁻¹

(more)

CHERRY, CORNELIAN - Continued

	dry weight basis	ash-free dry weight basis	std dev. of mean	
leaf (5 measurements)				
$q_v(\text{gross}) =$	7177	8343	66.8	Btu lb ⁻¹
$q_v(\text{gross}) =$	3987	4635	37.1	cal g ⁻¹
$q_v(\text{gross}) =$	16682	19393	155	J g ⁻¹
root (4 measurements)				
$q_v(\text{gross}) \square$	8008	8726	23.4	Btu lb ⁻¹
$q_v(\text{gross}) \square$	4449	4848	13.0	cal g ⁻¹
$q_v(\text{gross}) =$	18615	20284	54.4	J g ⁻¹

75PAP

CHESTNUT; *Castanea dentata*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.32 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.317$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) \square = 0.317$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 1.326$$

12DUN

COCOBOLA NEGRA; *Lecythis costaricensis*; solid; from Costa Rica; air-dried at 105°-110°C (221°-230°F); density, 0.92 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.327$$

$$C_p(\text{cal g}^{-1} \text{ K}^{-1}) = 0.327$$

$$C_p(\text{J g}^{-1} \text{ K}^{-1}) = 1.368$$

12DUN

Woody and Tree Materials

COTTONWOOD, MISSOURI; *Populus deltoides*; solid; Each tree was separated into small parts (being less than 0.64 cm (1/4 in.) in diameter and roughly equivalent to tops and branches) and large parts with the weighted proportion of small (25%) and large (75%) material in the whole tree. Overall mean specific gravity for whole tree = 0.32 (oven dry weight and green volume). Bark proportion of whole tree = 19%.

gross heat of combustion: oven-dried, assume values refer to room temperature.

small parts

$$\begin{aligned}q_v(\text{gross}) &= 8451 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4695 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19644 \text{ J g}^{-1}\end{aligned}$$

large parts

$$\begin{aligned}q_v(\text{gross}) &= 7949 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4416 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18477 \text{ J g}^{-1}\end{aligned}$$

whole tree

$$\begin{aligned}q_v(\text{gross}) &= 8075 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4486 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18769 \text{ J g}^{-1}\end{aligned}$$

81GEY

COTTONWOOD, NEBRASKA; *Populus deltoides*; solid; Each tree was separated into small parts (being less than 0.64 cm (1/4 in.) in diameter and roughly equivalent to tops and branches) and large parts with the weighted proportion of small (25%) and large (75%) material in the whole tree. Overall mean specific gravity for whole tree = 0.36 (oven dry weight and green volume). Bark proportion of whole tree = 28%.

gross heat of combustion: oven-dried, assume values refer to room temperature.

small parts

$$\begin{aligned}q_v(\text{gross}) &= 7893 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4385 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18347 \text{ J g}^{-1}\end{aligned}$$

large parts

$$\begin{aligned}q_v(\text{gross}) &= 7718 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4288 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17941 \text{ J g}^{-1}\end{aligned}$$

whole tree

$$\begin{aligned}q_v(\text{gross}) &= 7762 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4312 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18041 \text{ J g}^{-1}\end{aligned}$$

81GEY

DOGWOOD, BLOOD-TWIG; *Cornus sanguinea*; solid; Material is a shrub, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of stem and branch wood = 0.6%; stem and branch bark = 6.3%; leaf = 14.1%; root = 8.3%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
stem and branch wood (3 measurements)				
$q_v(\text{gross}) =$	8300	8341	50.6	Btu lb ⁻¹
$q_v(\text{gross}) =$	4611	4634	28.1	cal g ⁻¹
$q_v(\text{gross}) =$	19292	19389	118	J g ⁻¹
stem and branch bark (5 measurements)				
$q_v(\text{gross}) =$	8525	9104	48.4	Btu lb ⁻¹
$q_v(\text{gross}) =$	4736	6058	26.9	cal g ⁻¹
$q_v(\text{gross}) =$	19815	21163	113	J g ⁻¹
leaf (5 measurements)				
$q_v(\text{gross}) =$	7414	8633	49.3	Btu lb ⁻¹
$q_v(\text{gross}) =$	4119	4796	27.4	cal g ⁻¹
$q_v(\text{gross}) =$	17234	20066	115	J g ⁻¹
root (3 measurements)				
$q_v(\text{gross}) =$	7861	8570	27.0	Btu lb ⁻¹
$q_v(\text{gross}) =$	4367	4761	15.0	cal g ⁻¹
$q_v(\text{gross}) =$	18272	19920	62.8	J g ⁻¹

75PAP

ELM, AMERICAN; BARK; *Ulmus americana*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 9.5%; moisture content = 6.7%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash content; hence, are on an as-determined basis.

$$\begin{aligned}
 q_v(\text{gross}) &= 6921 \text{ Btu lb}^{-1} \\
 q_v(\text{gross}) &= 3845 \text{ cal g}^{-1} \\
 q_v(\text{gross}) &= 16087 \text{ J g}^{-1}
 \end{aligned}$$

55CHA/MIT

ELM, WHITE; *Ulmus americana*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.64 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.325 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.325 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.360 \end{aligned}$$

12DUN

EUCALYPTUS CAMALDULENSIS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 81.42, ash content = 0.76, and fixed carbon = 17.82. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.00, hydrogen = 5.87, oxygen = 43.97, nitrogen = 0.30, sulfur = 0.01, chlorine = 0.13, and residue (ash) = 0.72.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned} q_v(\text{gross}) &= 8355 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4641 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19420 \text{ J g}^{-1} \end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{net}) &= 7843 \text{ Btu lb}^{-1} \\ q_v(\text{net}) &= 4357 \text{ cal g}^{-1} \\ q_v(\text{net}) &= 18230 \text{ J g}^{-1} \end{aligned}$$

85JEN/EBE

EUCALYPTUS GLOBULUS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 81.60, ash content = 1.10, and fixed carbon = 17.30. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.18, hydrogen = 5.92, oxygen = 44.18, nitrogen = 0.39, sulfur = 0.01, chlorine = 0.20, and residue (ash) = 1.12.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8273 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4596 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19230 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7757 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4309 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18030 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

EUCALYPTUS GRANDIS; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 82.55, ash content = 0.52, and fixed carbon = 16.93. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.33, hydrogen = 5.89, oxygen = 45.13, nitrogen = 0.15, sulfur = 0.01, chlorine = 0.08, and residue (ash) = 0.41.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8325 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4625 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19350 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7808 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4338 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18150 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

EXCELSIOR, DEAD WOOD; *Populus spp.*; solid; Dead wood was air-dried at room temperature. Composition is ash = 0.35% and char yield = 15.4%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 8430 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4680 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19600 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13930 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7740 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32370 \text{ J g}^{-1} \end{aligned}$$

82SUS

FIR; *Pinus silvestri*; solid; ultimate analysis: carbon, 50.36%; hydrogen, 5.92%; nitrogen, 0.05%; ash, 0.28%.

gross heat of combustion: 20°C (68°F); air-dried at 110°-115°C (230°-240°F), ash free.

$$\begin{aligned} q_v(\text{gross}) &= 9068 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5038 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21079 \text{ J g}^{-1} \end{aligned}$$

1883GOT

FIR, BALSAM; BARK; *Abies balsamea*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 2.3%; moisture content = 6.5%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned} q_v(\text{gross}) &= 8861 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4923 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20598 \text{ J g}^{-1} \end{aligned}$$

55CHA/MIT

FIR, BALSAM; NEEDLES; *Abies balsamea*; solid; Samples were removed from 7-year-old trees and had a concentration (in milligrams per gram ash-free dry weight) of starch = 41.7, total sugar = 130.7, crude fat = 101.0, and nitrogen = 8.8.

gross heat of combustion: values refer to ash-free dry weight and assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 9182 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5101 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21343 \text{ J g}^{-1} \end{aligned}$$

78SHA/LIT

FIR, DOUGLAS; *Pseudotsuga taxifolia*; solid; air-dried at 105°-110°C (221°-230°F), density, 0.48 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$C_p (\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) = 0.327$$

$$C_p (\text{cal g}^{-1} \text{ K}^{-1}) = 0.327$$

$$C_p (\text{J g}^{-1} \text{ K}^{-1}) = 1.368$$

12DUN

FIR, DOUGLAS; *Pseudotsuga menzeisii*; solid; Wood was air-dried at room temperature. Composition is ash = 0.15% and char yield = 20.1%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

char (from 500°C heating)

$$q_v(\text{gross}) = 8710 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 13720 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4840 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 7620 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 20250 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 31900 \text{ J g}^{-1}$$

82SUS

FIR, DOUGLAS; BARK; *Pseudotsuga menzeisii*; solid; Bark samples were air-dried at room temperature. Composition is ash = 1.25% and char yield = 37.2%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

char (from 500°C heating)

$$q_v(\text{gross}) = 10310 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 12860 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5730 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 7140 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 23960 \text{ J g}^{-1}$$

$$q_v(\text{gross}) = 29890 \text{ J g}^{-1}$$

82SUS

FIR, DOUGLAS; FOLIAGE; *Pseudotsuga menzeisii*; solid; freeze-dried to < 10% moisture content. Composition is ash = 4.25% and char yield = 29.2%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9590 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13640 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5330 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7580 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 22300 \text{ J g}^{-1}$	$q_v(\text{gross}) = 31710 \text{ J g}^{-1}$

82SUS

FIR, DOUGLAS; LUMBER; *Pseudotsuga menzeisii*; solid; Lumber was air-dried at room temperature. Composition is ash = 0.18% and char yield = 22.2%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 8640 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13740 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 4800 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7630 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 20090 \text{ J g}^{-1}$	$q_v(\text{gross}) = 31940 \text{ J g}^{-1}$

82SUS

FIR, DOUGLAS; ROTTEN WOOD; *Pseudotsuga menzeisii*; solid; Samples were air-dried at room temperature. Composition is ash = 0.16% and char yield = 40.6%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9920 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13360 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5510 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7420 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 23050 \text{ J g}^{-1}$	$q_v(\text{gross}) = 31050 \text{ J g}^{-1}$

82SUS

FIR, DOUGLAS; STEMS; *Pseudotsuga menzeisii*; solid; Stem samples were branches < 0.25 in. diameter with foliage removed and freeze-dried to < 10% moisture content. Composition is ash = 2.57% and char yield = 27.9%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 9630 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5350 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22380 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13640 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7580 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 31710 \text{ J g}^{-1}\end{aligned}$$

82SUS

FIR, GRAND; *Abies grandis*; solid; Wood sample was air-dried at room temperature. Composition is ash = 0.49% and char yield = 20.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 8710 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4840 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20250 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13770 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7650 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 32000 \text{ J g}^{-1}\end{aligned}$$

82SUS

FIR, WHITE; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 83.17, ash content = 0.25, and fixed carbon = 16.58. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.00, hydrogen = 5.98, oxygen = 44.75, nitrogen = 0.05, sulfur = 0.01, chlorine = 0.01, and residue (ash) = 0.02.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8583 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4768 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19950 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8062 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4479 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18740 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

FIR, WHITE; *Abies concolor*; solid; Wood samples were air-dried at room temperature. Composition is ash = 0.55% and char yield = 22.1%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 8850 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4920 \text{ cal g}^{-1} \\q_v(\text{Gross}) &= 20570 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 14270 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7930 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 33180 \text{ J g}^{-1}\end{aligned}$$

82SUS

FIR, WHITE; *Abies concolor*; solid; Material was obtained from Whitaker's Forest in Tulare County, California, with predominant soil series of Shaver sandy loam derived from granitic parent material. The layer was collected from the understory of the forest floor. Average yearly decomposition of the forest floor for white fir is: litter, 6.67%; duff, 1.46%.

gross heat of combustion: assume values refer to room temperature; ash-free.

branch-twig

$$\begin{aligned}q_v(\text{gross}) &= 8990 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4939 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20665 \text{ J g}^{-1}\end{aligned}$$

litter

$$\begin{aligned}q_v(\text{gross}) &= 9338 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5188 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21707 \text{ J g}^{-1}\end{aligned}$$

duff

$$\begin{aligned}q_v(\text{gross}) &= 9238 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5132 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21472 \text{ J g}^{-1}\end{aligned}$$

78AGE/WAK

FIR, WHITE; ROTTEN WOOD; *Abies concolor*; solid; Samples were air-dried at room temperature. Composition is ash = 0.15% and char yield = 21.3%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 8750 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4860 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20340 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13720 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7620 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 31900 \text{ J g}^{-1}\end{aligned}$$

82SUS

HEMLOCK, EASTERN; BARK; *Tsuga canadensis*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 1.6%; moisture content = 6.2%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 8802 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4890 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20460 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

HEMLOCK, WESTERN; *Tsuga heterophylla*; solid; air-dried at 105°-110°C (221°-230°F) density, 0.45 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.322 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.322 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.347\end{aligned}$$

gross heat of combustion: assume values refer to room temperature; air-dried.

$$\begin{aligned}q_v(\text{gross}) &= 8626 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4792 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20050 \text{ J g}^{-1}\end{aligned}$$

12DUN; 68KAI/FRI; 66FRY

HEVEA (RUBBER TREE); solid; Material came from mature trees growing on Rengam series soils in Kuala Lumpur, Malaysia. Samples were oven-dried at 80°C (176°F) to constant weight, milled to a powder and pelleted in units of about 1 g each.

gross heat of combustion: dry weight basis, used 30 atm oxygen; assume values refer to room temperature.

branch bark

$$\begin{aligned}q_v(\text{gross}) &= 7765 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4314 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18050 \text{ J g}^{-1}\end{aligned}$$

branch wood

$$\begin{aligned}q_v(\text{gross}) &= 8037 \pm 30.2 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4465 \pm 16.8 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18682 \pm 70.3 \text{ J g}^{-1}\end{aligned}$$

leaves

$$\begin{aligned}q_v(\text{gross}) &= 9000 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5000 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20920 \text{ J g}^{-1}\end{aligned}$$

main-stem bark

$$\begin{aligned}q_v(\text{gross}) &= 7675 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4264 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17841 \text{ J g}^{-1}\end{aligned}$$

main-stem wood

$$\begin{aligned}q_v(\text{gross}) &= 7974 \pm 30.2 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4430 \pm 16.8 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18535 \pm 70.3 \text{ J g}^{-1}\end{aligned}$$

petioles

$$\begin{aligned}q_v(\text{gross}) &= 8377 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4654 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19472 \text{ J g}^{-1}\end{aligned}$$

trunk bark

$$\begin{aligned}q_v(\text{gross}) &= 7875 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4375 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18305 \text{ J g}^{-1}\end{aligned}$$

trunk wood

$$\begin{aligned}q_v(\text{gross}) &= 8062 \pm 30.2 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4479 \pm 16.8 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18740 \pm 70.3 \text{ J g}^{-1}\end{aligned}$$

83LEO

HEVEA (RUBBER TREE), CLONE RRIM 527; solid; Material came from mature trees growing on Rengam series soils in Kuala Lumpur, Malaysia. Samples were oven-dried at 80°C (176°F) to constant weight, milled to a powder, and pelleted in units of about 1 g each.

gross heat of combustion: dry weight basis; used 30 atm oxygen; assume values refer to room temperature.

trunk and main-stem plant parts

$$\begin{aligned}q_v(\text{gross}) &= 7897 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4387 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18355 \text{ J g}^{-1}\end{aligned}$$

leaves plus petioles plant parts

$$\begin{aligned}q_v(\text{gross}) &= 8689 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4827 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20196 \text{ J g}^{-1}\end{aligned}$$

branches

$$\begin{aligned}q_v(\text{gross}) &= 7870 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4372 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18292 \text{ J g}^{-1}\end{aligned}$$

83LEO

HEVEA (RUBBER TREE), CLONE RRIM 707; solid; Material came from mature trees growing on Rengam series soils in Kuala Lumpur, Malaysia. Samples were oven-dried at 80°C (176°F) to constant weight, milled to a powder, and pelleted in units of about 1 g each.

gross heat of combustion: dry weight basis; used 30 atm oxygen; assume values refer to room temperature.

trunk and main-stem plant parts

$$\begin{aligned} q_v(\text{gross}) &= 7987 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4437 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18564 \text{ J g}^{-1} \end{aligned}$$

branches

$$\begin{aligned} q_v(\text{gross}) &= 7906 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4392 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18376 \text{ J g}^{-1} \end{aligned}$$

leaves plus petioles plant parts

$$\begin{aligned} q_v(\text{gross}) &= 9094 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5052 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21138 \text{ J g}^{-1} \end{aligned}$$

83LEO

HICKORY; genus *Carya*; solid.

gross heat of combustion: assume values refer to room temperature.

as received: 10.30% moisture

$$\begin{aligned} q_v(\text{gross}) &= 7583 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4213 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17626 \text{ J g}^{-1} \end{aligned}$$

air-dried one hour at 105°C (221°F)

$$\begin{aligned} q_v(\text{gross}) &= 8455 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4697 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19652 \text{ J g}^{-1} \end{aligned}$$

22PAR/DAV

Woody and Tree Materials

HICKORY; *Carya spp.*; solid; Material was collected from the southern Atlantic and Gulf coastal plains in bottom-, swamp- and wet flat-land natural stand sites. Samples were dried at 70°C (158°F) to a constant weight; reported values were averaged over all positions of similar plant tissue for each tree and six trees per species were used.

gross heat of combustion: assume values refer to room temperature; values are on a dry weight basis.

bole wood

$$\begin{aligned}q_v(\text{gross}) &= 8309 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4616 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19313 \text{ J g}^{-1}\end{aligned}$$

bole bark

$$\begin{aligned}q_v(\text{gross}) &= 7538 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4188 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17523 \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 8237 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4576 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19146 \text{ J g}^{-1}\end{aligned}$$

branch wood

$$\begin{aligned}q_v(\text{gross}) &= 8122 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4512 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18878 \text{ J g}^{-1}\end{aligned}$$

branch bark

$$\begin{aligned}q_v(\text{gross}) &= 7565 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4203 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17595 \text{ J g}^{-1}\end{aligned}$$

82GOW/FRE

HORNBEAM; *Carpinus betulus*; solid; ultimate analysis: carbon, 48.99%; hydrogen, 6.20%; nitrogen, 0.06%; ash, 0.50%.

gross heat of combustion: 20°C (68°F), air-dried 110°-115°C (230°-240°F), ash free.

$$\begin{aligned}q_v(\text{gross}) &= 8536 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4742 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19841 \text{ J g}^{-1}\end{aligned}$$

1883GOT

JUNIPER, UTAH; BARK; *Juniperus osteosperma*; solid; Bark was air-dried at room temperature. Composition is ash = 17.74% and char yield = 27.9%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 9260 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5150 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21530 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13720 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7620 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 31880 \text{ J g}^{-1}\end{aligned}$$

82SUS

JUNIPER, UTAH; FOLIAGE; *Juniperus osteosperma*; solid; freeze-dried to < 10% moisture content. Composition is ash = 4.22% and char yield = 24.5%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 10020 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5560 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 23280 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13160 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7310 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 30590 \text{ J g}^{-1} \end{aligned}$$

82SUS

JUNIPER, UTAH; STEMS; *Juniperus osteosperma*; solid; Stem samples were branches less than 0.25 in. diameter with foliage removed and freeze-dried to < 10% moisture content. Composition is ash = 6.05% and char yield = 26.2%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 8890 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4940 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20660 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13310 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7390 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 30930 \text{ J g}^{-1} \end{aligned}$$

82SUS

LARCH; *Larix occidentalis*; solid; Wood was air-dried at room temperature. Composition is ash = 0.19% and char yield = 20.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 8530 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4740 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19830 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13890 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7720 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32290 \text{ J g}^{-1} \end{aligned}$$

82SUS

LARCH, BARK; *Larix occidentalis*; solid; Bark samples were freeze-dried at room temperature. Composition is ash = 1.20% and char yield = 37.3%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 10250 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5690 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23820 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13140 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7300 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 30540 \text{ J g}^{-1}\end{aligned}$$

82SUS

LARCH, LUMBER; *Larix occidentalis*; solid; Wood was air-dried at room temperature. Composition is ash = 0.17% and char yield = 23.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 8700 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4830 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20220 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13830 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7680 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 32150 \text{ J g}^{-1}\end{aligned}$$

82SUS

LARCH, WESTERN; BARK; *Larix occidentalis*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 1.6%; moisture content = 6.7%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 8204 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4558 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19071 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

LEAVES, TREE; RIPE HARDWOOD MIXTURE; solid; ultimate analysis: carbon, 52.15%; hydrogen, 6.11%; oxygen, 30.34%; nitrogen, 6.99%; sulfur, 0.16%; ash, 4.25%; proximate analysis as received: moisture, 9.97%; volatile matter, 66.92%; fixed carbon, 19.29%; ash, 3.82%.

gross heat of combustion: assume values refer to room temperature.

as received

$$\begin{aligned} q_v(\text{gross}) &= 7990 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4439 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18571 \text{ J g}^{-1} \end{aligned}$$

dry basis

$$\begin{aligned} q_v(\text{gross}) &= 8874 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4930 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20629 \text{ J g}^{-1} \end{aligned}$$

66KAI

LITTER FALL; solid; Material was collected for one year in a 79-year-old, low-altitude, New Zealand *Nothofagus solandri* variety forest. An even-aged stand of *Nothofagus* with a sparse subcanopy vegetation was chosen having the following percentage of ground covers (rejecting tree base points); litter or soil, 95.2%; bryophytes, 4.0%; exposed roots, 0.4%; and vascular plants, 0.4%. Throughfall was taken as suspended and dissolved material rainwashed from the plants, including material from rainfall, surface-washings from plants, and recretions from leaves.

gross heat of combustion: dry weight and assume values refer to room temperature.

branch material

$$\begin{aligned} q_v(\text{gross}) &= 8500 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4700 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19700 \text{ J g}^{-1} \end{aligned}$$

floral material

$$\begin{aligned} q_v(\text{gross}) &= 8600 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4800 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20100 \text{ J g}^{-1} \end{aligned}$$

samples with negligible amounts of throughfall

$$\begin{aligned} q_v(\text{gross}) &= 8600 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4800 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20100 \text{ J g}^{-1} \end{aligned}$$

samples with intermediate amounts of throughfall

$$\begin{aligned} q_v(\text{gross}) &= 8300 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4600 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19200 \text{ J g}^{-1} \end{aligned}$$

(more)

LITTER FALL - Continued

samples with large amounts of throughfall

$$q_v(\text{gross}) = 7700 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4300 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18000 \text{ J g}^{-1}$$

72BAG

LOCUST, BLACK; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 80.94, ash content = 0.80, and fixed carbon = 18.26. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 50.73, hydrogen = 5.71, oxygen = 41.93, nitrogen = 0.57, sulfur = 0.01, chlorine = 0.08, and residue (ash) = 0.97.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$q_v(\text{gross}) = 8479 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4711 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19710 \text{ J g}^{-1}$$

net heat of combustion: assume values refer to room temperature.

$$q_v(\text{net}) = 7980 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 4434 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 18550 \text{ J g}^{-1}$$

85JEN/EBE

MADRONE; *Arbutus menzeisii*; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 82.99, ash content = 0.57, and fixed carbon = 16.44. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.00, hydrogen = 5.96, oxygen = 44.95, nitrogen = 0.06, sulfur = 0.02, chlorine = 0.01, and residue (ash) = 1.00.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$q_v(\text{gross}) = 8350 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4639 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19410 \text{ J g}^{-1}$$

net heat of combustion: assume values refer to room temperature.

$$q_v(\text{net}) = 7830 \text{ Btu lb}^{-1}$$

$$q_v(\text{net}) = 4350 \text{ cal g}^{-1}$$

$$q_v(\text{net}) = 18200 \text{ J g}^{-1}$$

85JEN/EBE

MAI CHAMPAH; *Michelia*; solid; from Thailand; air-dried at 105°-110°C (221°-230°F); density, 0.32 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned} C_p (\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.323 \\ C_p (\text{cal g}^{-1} \text{ K}^{-1}) &= 0.323 \\ C_p (\text{J g}^{-1} \text{ K}^{-1}) &= 1.351 \end{aligned}$$

12DUN

MANZANITA; *Arctostaphylos*; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 81.29, ash content = 0.82, and fixed carbon = 17.89. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.18, hydrogen = 5.94, oxygen = 44.68, nitrogen = 0.17, sulfur = 0.02, chlorine = 0.01, and residue (ash) = 1.00.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned} q_v(\text{gross}) &= 8303 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4613 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19300 \text{ J g}^{-1} \end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{net}) &= 7783 \text{ Btu lb}^{-1} \\ q_v(\text{net}) &= 4324 \text{ cal g}^{-1} \\ q_v(\text{net}) &= 18090 \text{ J g}^{-1} \end{aligned}$$

85JEN/EBE

MANZANITA, GREENLEAF; FOLIAGE; *Arctostaphylos glandulosa*; solid; freeze-dried to < 10% moisture content. Composition is ash = 3.19% and char yield = 30.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 9350 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5190 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21730 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13940 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7750 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 31410 \text{ J g}^{-1} \end{aligned}$$

82SUS

MAPLE; genus, *Acer*; solid; ultimate analysis: carbon, 50.40%; hydrogen, 5.90%; oxygen, 39.10%; nitrogen, 0.50%; sulfur, 0.0%; ash, 4.10%; proximate analysis as received in percent by weight: moisture, 0.0%; volatile matter, 76.1%; fixed carbon, 19.6%; ash, 4.3%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 8195 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4553 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19050 \text{ J g}^{-1}$$

68KAI/FRI; 66FRY

MAPLE, HEDGE; *Acer campestre*; solid; Material is a tree, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of stem and branch wood = 1.2%; stem and branch bark = 9.7%; leaf = 10.3%; root = 10.0%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
stem and branch wood (4 measurements)				
$q_v(\text{gross}) =$	8343	8440	30.1	Btu lb ⁻¹
$q_v(\text{gross}) =$	4635	4689	16.7	cal g ⁻¹
$q_v(\text{gross}) =$	19393	19619	69.9	J g ⁻¹
stem and branch bark (5 measurements)				
$q_v(\text{gross}) =$	7607	8429	49.9	Btu lb ⁻¹
$q_v(\text{gross}) =$	4226	4683	27.7	cal g ⁻¹
$q_v(\text{gross}) =$	17682	19594	116	J g ⁻¹
leaf (6 measurements)				
$q_v(\text{gross}) =$	7837	8732	5.4	Btu lb ⁻¹
$q_v(\text{gross}) =$	4354	4851	3.0	cal g ⁻¹
$q_v(\text{gross}) =$	18217	20297	13	J g ⁻¹
root (4 measurements)				
$q_v(\text{gross}) =$	7879	8750	77.8	Btu lb ⁻¹
$q_v(\text{gross}) =$	4377	4861	43.2	cal g ⁻¹
$q_v(\text{gross}) =$	18313	20338	181	J g ⁻¹

75PAP

MAPLE, RED; *Acer rubrum*; solid; mean age = 12.7 years, mean basal stem diameter = 7.8 cm, mean stem bark (proportion of dry weight) = 10.7%, ash content (proportion of oven dry weight) of components of sample: wood = 0.51%, branches = 1.4%, twigs = 2.1%, bark = 6.5%, and leaves = 5.2%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned}q_v(\text{gross}) &= 8654 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4808 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20117 \text{ J g}^{-1}\end{aligned}$$

bark:

$$\begin{aligned}q_v(\text{gross}) &= 8203 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4557 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19066 \text{ J g}^{-1}\end{aligned}$$

branches:

$$\begin{aligned}q_v(\text{gross}) &= 8568 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4760 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19916 \text{ J g}^{-1}\end{aligned}$$

twigs:

$$\begin{aligned}q_v(\text{gross}) &= 8586 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4770 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19958 \text{ J g}^{-1}\end{aligned}$$

leaves:

$$\begin{aligned}q_v(\text{gross}) &= 8957 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4976 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20820 \text{ J g}^{-1}\end{aligned}$$

79NEE/STE

MAPLE, RED; *Acer rubrum*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, and at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned}q_v(\text{gross}) &= 8626 (25) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4792 (14) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20050 (59) \text{ J g}^{-1}\end{aligned}$$

bole without bark

$$\begin{aligned}q_v(\text{gross}) &= 8737 (38) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4854 (21) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20309 (88) \text{ J g}^{-1}\end{aligned}$$

branch with bark

$$\begin{aligned}q_v(\text{gross}) &= 8667 (47) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4815 (26) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20146 (109) \text{ J g}^{-1}\end{aligned}$$

branch without bark

$$\begin{aligned}q_v(\text{gross}) &= 8734 (43) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4852 (24) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20301 (100) \text{ J g}^{-1}\end{aligned}$$

(more)

MAPLE, RED - Continued

foliage

$$q_v(\text{gross}) = 9119 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5066 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 21196 \text{ J g}^{-1}$$

81MUS/HOC

MAPLE, RED; *Acer rubrum*; solid; Material was collected from the southern Atlantic and Gulf coastal plains in bottom-, swamp- and wet flat-land natural stand sites. Samples were dried at 70°C (158°F) to a constant weight; reported values were averaged over all positions of similar plant tissue for each tree and six trees per species were used.

gross heat of combustion: assume values refer to room temperature; values are on a dry weight basis.

bole wood

$$q_v(\text{gross}) = 8437 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4687 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19610 \text{ J g}^{-1}$$

branch wood

$$q_v(\text{gross}) = 8345 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4636 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19397 \text{ J g}^{-1}$$

bole bark

$$q_v(\text{gross}) = 7650 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4250 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 17782 \text{ J g}^{-1}$$

branch bark

$$q_v(\text{gross}) = 8001 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4445 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18598 \text{ J g}^{-1}$$

foliage

$$q_v(\text{gross}) = 8764 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4869 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 20372 \text{ J g}^{-1}$$

82GOW/FRE

MAPLE, SILVER; *Acer saccharinum*; solid; Each tree was separated into small parts (being less than 0.64 cm (1/4 in.) in diameter and roughly equivalent to tops and branches) and large parts with the weighted proportion of small (25%) and large (75%) material in the whole tree. Overall mean specific gravity for whole tree = 0.40 (oven dry weight and green volume). Bark proportion of whole tree = 19%.

gross heat of combustion: oven-dried, assume values refer to room temperature.

small parts

$$\begin{aligned} q_v(\text{gross}) &= 8071 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4484 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18761 \text{ J g}^{-1} \end{aligned}$$

large parts

$$\begin{aligned} q_v(\text{gross}) &= 8006 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4448 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18610 \text{ J g}^{-1} \end{aligned}$$

whole tree

$$\begin{aligned} q_v(\text{gross}) &= 8023 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4457 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18648 \text{ J g}^{-1} \end{aligned}$$

81GEY

MAPLE, SUGAR; *Acer saccharum*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.66 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.327 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.327 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.368 \end{aligned}$$

12DUN

MAPLE, SUGAR; *Acer saccharum*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, one at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight.

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned}q_v(\text{gross}) &= 8705 (158) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4836 (88) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20234 (368) \text{ J g}^{-1}\end{aligned}$$

bole without bark

$$\begin{aligned}q_v(\text{gross}) &= 8773 (52) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4874 (29) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20393 (121) \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 9020 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5011 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20966 \text{ J g}^{-1}\end{aligned}$$

branch with bark

$$\begin{aligned}q_v(\text{gross}) &= 8771(184) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4873 (102) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20389 (427) \text{ J g}^{-1}\end{aligned}$$

branch without bark

$$\begin{aligned}q_v(\text{gross}) &= 8863 (103) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4924 (57) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20602 (238) \text{ J g}^{-1}\end{aligned}$$

81MUS/HOC

MAPLE, SUGAR; BARK; *Acer saccharum*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 6.3%; moisture content = 6.0%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 7301 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4056 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16970 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

MAPLE, TATARIAN; *Acer tataricum*; solid; Material is a tree, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of stem and branch wood = 0.6%; stem and branch bark = 7.5%; leaf = 5.61%; root = 5.8%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
stem and branch wood (3 measurements)				
$q_v(\text{gross}) =$	8298	8341	52.9	Btu lb ⁻¹
$q_v(\text{gross}) =$	4610	4634	29.4	cal g ⁻¹
$q_v(\text{gross}) =$	19288	19389	123	J g ⁻¹
stem and branch bark (5 measurements)				
$q_v(\text{gross}) =$	7970	8611	114	Btu lb ⁻¹
$q_v(\text{gross}) =$	4428	4784	63.5	cal g ⁻¹
$q_v(\text{gross}) =$	18527	20016	266	J g ⁻¹
leaf (6 measurements)				
$q_v(\text{gross}) =$	8046	8525	110	Btu lb ⁻¹
$q_v(\text{gross}) =$	4470	4736	61.2	cal g ⁻¹
$q_v(\text{gross}) =$	18720	19815	256	J g ⁻¹
root (3 measurements)				
$q_v(\text{gross}) =$	7754	8235	57.8	Btu lb ⁻¹
$q_v(\text{gross}) =$	4308	4575	32.1	cal g ⁻¹
$q_v(\text{gross}) =$	18025	19142	134	J g ⁻¹

75PAP

OAK; *Quercus pedunculata*; solid; ultimate analysis: carbon, 50.16%; hydrogen, 6.02%; nitrogen, 0.09%; ash, 0.37%.

gross heat of combustion: 20°C (68°F); air-dried at 110°-115°C (230°-240°F); ash free.

$$q_v(\text{gross}) = 8296 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4609 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19284 \text{ J g}^{-1}$$

species not identified; room temperature; air-dried one hour at 105°C (221°F).

$$q_v(\text{gross}) = 8561 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4756 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 19899 \text{ J g}^{-1}$$

22PAR/DAV

OAK, BLACK; DEAD FOLIAGE; *Quercus velutina*; The litter was air dried at room temperature. Composition is ash = 3.46% and char yield = 28.9%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$q_v(\text{gross}) = 9150 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5080 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 21270 \text{ J g}^{-1}$$

char (from 500°C heating)

$$q_v(\text{gross}) = 13290 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 7380 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 30880 \text{ J g}^{-1}$$

82SUS

OAK, DURMAST; *Quercus petraea*; solid; Material is a tree, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of trunk wood = 0.5%; branch wood = 1.0%; trunk bark = 10.4%; branch bark = 9.0%; twig = 3.7%; light-adapted leaf = 6.1%; shade-adapted leaf = 6.5%; acorns = 2.6%; root = 6.9%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
trunk wood (4 measurements)				
$q_v(\text{gross}) =$	8545	8582	35.8	Btu lb ⁻¹
$q_v(\text{gross}) =$	4747	4768	19.9	cal g ⁻¹
$q_v(\text{gross}) =$	19861	19949	83.3	J g ⁻¹
branch wood (3 measurements)				
$q_v(\text{gross}) =$	8518	8620	38.0	Btu lb ⁻¹
$q_v(\text{gross}) =$	4732	4789	21.1	cal g ⁻¹
$q_v(\text{gross}) =$	19799	20037	88.3	J g ⁻¹
trunk bark (4 measurements)				
$q_v(\text{gross}) =$	7997	8926	30.1	Btu lb ⁻¹
$q_v(\text{gross}) =$	4443	4959	16.7	cal g ⁻¹
$q_v(\text{gross}) =$	18590	20748	69.9	J g ⁻¹
branch bark (4 measurements)				
$q_v(\text{gross}) =$	7675	8440	54.5	Btu lb ⁻¹
$q_v(\text{gross}) =$	4264	4689	30.3	cal g ⁻¹
$q_v(\text{gross}) =$	17841	19619	127	J g ⁻¹
twig (4 measurements)				
$q_v(\text{gross}) =$	8363	8694	85.0	Btu lb ⁻¹
$q_v(\text{gross}) =$	4646	4830	47.2	cal g ⁻¹
$q_v(\text{gross}) =$	19439	20209	197	J g ⁻¹
light-adapted leaf (5 measurements)				
$q_v(\text{gross}) =$	8698	9259	74.3	Btu lb ⁻¹
$q_v(\text{gross}) =$	4832	5144	41.3	cal g ⁻¹
$q_v(\text{gross}) =$	20217	21522	173	J g ⁻¹

(more)

OAK, DURMAST - Continued

	dry weight basis	ash-free dry weight basis	std dev. of mean	
shade-adapted leaf (5 measurements)				
$q_v(\text{gross}) =$	8329	8905	59.0	Btu lb ⁻¹
$q_v(\text{gross}) =$	4627	4947	32.8	cal g ⁻¹
$q_v(\text{gross}) =$	19359	20698	137	J g ⁻¹
acorns (3 measurements)				
$q_v(\text{gross}) =$	8377	8604	15	Btu lb ⁻¹
$q_v(\text{gross}) =$	4654	4780	8.1	cal g ⁻¹
$q_v(\text{gross}) =$	19472	20000	34	J g ⁻¹
root (3 measurements)				
$q_v(\text{gross}) =$	8089	8692	47.7	Btu lb ⁻¹
$q_v(\text{gross}) =$	4494	4829	26.5	cal g ⁻¹
$q_v(\text{gross}) =$	18803	20205	111	J g ⁻¹

75PAP

OAK, NORTHERN RED; *Quercus rubra*; solid; Material was extractive-free wood (EFW) comprising cellulose, 42.86%; hemicellulose, 33.33%; and lignin, 23.81%. The relationship between gross heat of combustion and moisture content (MC) is given by: $\ln q_v(\text{Btu lb}^{-1}) = 9.0389 - (0.0107)\text{MC}(\%)$ for EFW.

gross heat of combustion: oven-dry basis, assume values refer to room temperature; values are reported in international British thermal units per pound and converted below into thermochemical units.

$$\begin{aligned} q_v(\text{gross}) &= 8581 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4767 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19945 \text{ J g}^{-1} \end{aligned}$$

78MUR/MAS

OAK, NORTHERN RED; BARK; *Quercus rubra*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 5.4%; moisture content = 4.4%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned} q_v(\text{gross}) &= 8030 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4461 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18665 \text{ J g}^{-1} \end{aligned}$$

55CHA/MIT

OAK, RED; *Quercus rubra*; solid; air-dried at 105°-110°C (221°-230°F), density, 0.62 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.331 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.331 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.385 \end{aligned}$$

12DUN

OAK, RED; *Quercus rubra*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, and at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight.

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned} q_v(\text{gross}) &= 8780 (45) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4878 (25) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20410 (105) \text{ J g}^{-1} \end{aligned}$$

bole without bark

$$\begin{aligned} q_v(\text{gross}) &= 8654 (45) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4808 (25) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20117 (105) \text{ J g}^{-1} \end{aligned}$$

foliage

$$\begin{aligned} q_v(\text{gross}) &= 8941 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4967 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20782 \text{ J g}^{-1} \end{aligned}$$

branch with bark

$$\begin{aligned} q_v(\text{gross}) &= 8797 (56) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4887 (31) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20447 (130) \text{ J g}^{-1} \end{aligned}$$

branch without bark

$$\begin{aligned} q_v(\text{gross}) &= 8654 (56) \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4808 (31) \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20117 (130) \text{ J g}^{-1} \end{aligned}$$

81MUS/HOC

Woody and Tree Materials

OAK, TAN; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 80.93, ash content = 1.67, and fixed carbon = 17.40. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 47.81, hydrogen = 5.93, oxygen = 44.12, nitrogen = 0.12, sulfur = 0.01, chlorine = 0.01, and residue (ash) = 2.00.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8144 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4524 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18930 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7628 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4238 \text{ cal g}^{-1} \\q_v(\text{net}) &= 17730 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

OAK, TAN; BARK; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 73.11, ash content = 3.49, and fixed carbon = 23.40.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 7916 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4398 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18400 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

OAK, TAN; SAPWOOD; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 83.61, ash content = 1.03, and fixed carbon = 15.36.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8204 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4558 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19070 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

OAK, TURKEY; *Quercus cerris*; solid; Material is a tree, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of trunk wood = 1.1%; trunk bark = 8.4%; branch wood = 1.3%; branch bark = 8.3%; twig = 5.3%; light-adapted leaf = 5.4%; shade-adapted leaf = 6.2%; acorns = 2.1%; root = 4.6%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
trunk wood (3 measurements)				
$q_v(\text{gross}) =$	8523	8617	30.4	Btu lb ⁻¹
$q_v(\text{gross}) =$	4735	4787	16.9	cal g ⁻¹
$q_v(\text{gross}) =$	19811	20029	70.7	J g ⁻¹
trunk bark (7 measurements)				
$q_v(\text{gross}) =$	8386	9146	43.2	Btu lb ⁻¹
$q_v(\text{gross}) =$	4659	5081	24.0	cal g ⁻¹
$q_v(\text{gross}) =$	19493	21259	100	J g ⁻¹
branch wood (3 measurements)				
$q_v(\text{gross}) =$	8395	8510	57.1	Btu lb ⁻¹
$q_v(\text{gross}) =$	4664	4728	31.7	cal g ⁻¹
$q_v(\text{gross}) =$	19514	19782	133	J g ⁻¹
branch bark (4 measurements)				
$q_v(\text{gross}) =$	7708	8404	43.2	Btu lb ⁻¹
$q_v(\text{gross}) =$	4282	4669	24.0	cal g ⁻¹
$q_v(\text{gross}) =$	17916	19535	100	J g ⁻¹
twig (4 measurements)				
$q_v(\text{gross}) =$	8332	8807	99.2	Btu lb ⁻¹
$q_v(\text{gross}) =$	4629	4893	55.1	cal g ⁻¹
$q_v(\text{gross}) =$	19368	20472	231	J g ⁻¹
light-adapted leaf (5 measurements)				
$q_v(\text{gross}) =$	8901	9412	41.2	Btu lb ⁻¹
$q_v(\text{gross}) =$	4945	5229	22.9	cal g ⁻¹
$q_v(\text{gross}) =$	20690	21878	95.8	J g ⁻¹

(more)

OAK, TURKEY - Continued

	dry weight basis	ash-free dry weight basis	std dev. of mean	
shade-adapted leaf (5 measurements)				
$q_v(\text{gross}) =$	8653	9227	48.6	Btu lb ⁻¹
$q_v(\text{gross}) =$	4807	5126	27.0	cal g ⁻¹
$q_v(\text{gross}) =$	20112	21447	113	J g ⁻¹
acorns (3 measurements)				
$q_v(\text{gross}) =$	8118	8289	15	Btu lb ⁻¹
$q_v(\text{gross}) =$	4510	4605	8.1	cal g ⁻¹
$q_v(\text{gross}) =$	18870	19267	34	J g ⁻¹
root (3 measurements)				
$q_v(\text{gross}) =$	8233	8627	34.7	Btu lb ⁻¹
$q_v(\text{gross}) =$	4574	4793	19.3	cal g ⁻¹
$q_v(\text{gross}) =$	19138	20054	80.7	J g ⁻¹

75PAP

OAK, WATER; *Quercus nigra*; solid; mean age = 11.3 years, mean basal stem diameter = 9.8 cm, mean stem bark (proportion of dry weight) = 14.8%, ash content 1.7%, twigs = 2.6%, bark = 6.1%, and leaves = 3.3%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned} q_v(\text{gross}) &= 8599 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4777 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19987 \text{ J g}^{-1} \end{aligned}$$

bark:

$$\begin{aligned} q_v(\text{gross}) &= 8320 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4622 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19338 \text{ J g}^{-1} \end{aligned}$$

branches:

$$\begin{aligned} q_v(\text{gross}) &= 8561 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4756 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19899 \text{ J g}^{-1} \end{aligned}$$

twigs:

$$\begin{aligned} q_v(\text{gross}) &= 8672 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4818 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20159 \text{ J g}^{-1} \end{aligned}$$

leaves:

$$\begin{aligned} q_v(\text{gross}) &= 9151 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5084 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21271 \text{ J g}^{-1} \end{aligned}$$

79NEE/STE

OAK, WATER; *Quercus nigra*; solid; Material was collected from the southern Atlantic and Gulf coastal plains in bottom-, swamp- and wet flat-land natural stand sites. Samples were dried at 70°C (158°F) to a constant weight; reported values were averaged over all positions of similar plant tissue for each tree and six trees per species were used.

gross heat of combustion: assume values refer to room temperature; values are on a dry weight basis.

bole wood

$$\begin{aligned}q_v(\text{gross}) &= 8289 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4605 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19267 \text{ J g}^{-1}\end{aligned}$$

bole bark

$$\begin{aligned}q_v(\text{gross}) &= 8393 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4663 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19510 \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 8581 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4767 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19945 \text{ J g}^{-1}\end{aligned}$$

branch wood

$$\begin{aligned}q_v(\text{gross}) &= 8237 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4576 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19146 \text{ J g}^{-1}\end{aligned}$$

branch bark

$$\begin{aligned}q_v(\text{gross}) &= 8318 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4621 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19334 \text{ J g}^{-1}\end{aligned}$$

82GOW/FRE

OAK, WHITE; *Quercus alba*; solid; air-dried at 105°-110°C (221°-230°F), density, 0.78 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.325 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.325 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.360\end{aligned}$$

12DUN

OAK, WHITE; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 81.28, ash content = 1.52, and fixed carbon = 17.20. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.48, hydrogen = 5.38, oxygen = 43.13, nitrogen = 0.35, sulfur = 0.01, chlorine = 0.04, and residue (ash) = 1.61.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8355 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4641 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19420 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7886 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4381 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18330 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

OAK, WHITE; BARK; *Quercus alba*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 10.7%; moisture content = 6.5%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 6995 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3886 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16259 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

PINE, EASTERN WHITE; *Pinus strobus*; solid; Material came from various locations in New Hampshire. Bole samples were composed of cross sections taken from four positions along length of each tree (at the base, one-third, two-thirds, one at top of the stem). Branch samples were composed of cross sections taken from four positions along length of each of four branches (one branch from four positions in the live crown of the tree). Bark was removed from half of each bole and branch sample and all samples were oven-dried at 85°C (185°F) to a constant weight.

gross heat of combustion: Assume values refer to room temperature, thermochemical calorie used and values were expressed on a dry matter basis and adjusted for heat of formation of nitric acid. All tests were made at 99% confidence level and numbers in parentheses are standard errors.

bole with bark

$$\begin{aligned}q_v(\text{gross}) &= 9049 (59) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5027 (33) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21033 (138) \text{ J g}^{-1}\end{aligned}$$

bole without bark

$$\begin{aligned}q_v(\text{gross}) &= 9031 (58) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5017 (32) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20991 (134) \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 9407 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5226 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21866 \text{ J g}^{-1}\end{aligned}$$

branch with bark

$$\begin{aligned}q_v(\text{gross}) &= 9679 (56) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5377 (31) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 22497 (130) \text{ J g}^{-1}\end{aligned}$$

branch without bark

$$\begin{aligned}q_v(\text{gross}) &= 9182 (49) \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5101 (27) \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21343 (113) \text{ J g}^{-1}\end{aligned}$$

81MUS/HOC

PINE, JACK; BARK; *Pinus banksiana*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 1.7%; moisture content = 6.6%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 8761 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4867 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20364 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

Woody and Tree Materials

PINE LITTER, DUFF; solid; Material is partially decomposed pine litter called the "F" layer air-dried at room temperature. Composition is ash = 31.91% and char yield = 38.8%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 10010 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5560 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23260 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13530 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7520 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 31450 \text{ J g}^{-1}\end{aligned}$$

82SUS

PINE, LOBLOLLY; *Pinus taeda*; solid; unextracted specific gravity, 0.49 (oven dry weight and green volume).

specific heat: 333-413 K (140°-284°F); samples were oven-dried at 100°C (212°F) for 12 hours before measurements were made.

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= 0.25406 + 5.2761 \times 10^{-4} T \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.01153 + 9.497 \times 10^{-4} T \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.04824 + 3.9735 \times 10^{-3} T\end{aligned}$$

69McM

PINE, LOBLOLLY; EXTRACTIVES; *Pinus taeda*; solid; residue obtained from alcohol-benzene extraction of loblolly pine wood; mean extractive content, 6.08% [68McM].

specific heat: 333-413 K (140°-284°F); samples were oven-dried at 100°C (212°F) for 12 hours before measurements were made.

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= 0.34781 + 6.06 \times 10^{-4} T \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.06945 + 1.09 \times 10^{-3} T \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.29058 + 4.56 \times 10^{-3} T\end{aligned}$$

70McM

PINE, LODGEPOLE; BARK; *Pinus contorta*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 2.0%; moisture content = 5.6%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 10190 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5661 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 23686 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

PINE, LODGEPOLE; FOLIAGE; *Pinus contorta*; solid; freeze-dried to < 10% moisture content. Composition is ash = 2.21% and char yield = 29.2%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9530 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13810 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5290 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7670 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 22140 \text{ J g}^{-1}$	$q_v(\text{gross}) = 32110 \text{ J g}^{-1}$

82SUS

PINE, LODGEPOLE; NEEDLES; *Pinus contorta*; solid; Samples were taken at mid-crown position, in May and November, at 6300 and 5700 feet altitude, and from young and old trees. Crude protein levels averaged 4.52% of air-dry weight. Material was frozen and subsequently dried or preserved in 70% alcohol and then dried.

gross heat of combustion: air-dried weight, assume values refer to room temperature.

$q_v(\text{gross}) = 8951 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 4973 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 20807 \text{ J g}^{-1}$

68BOA/KIC

PINE, LONGLEAF; *Pinus palustris*; solid; air-dried at 105°-110°C (221°-230°F), density, 0.68 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	= 0.337
$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	= 0.337
$C_p(\text{J g}^{-1} \text{ K}^{-1})$	= 1.410

12DUN

PINE, PINYON; FOLIAGE; *Pinus edulis*; solid; freeze dried to < 10% moisture content. Composition is ash = 3.22% and char yield = 26.7%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9470 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13510 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5260 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7510 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 22020 \text{ J g}^{-1}$	$q_v(\text{gross}) = 31400 \text{ J g}^{-1}$

82SUS

PINE, PINYON; STEMS; *Pinus edulis*; solid; Stem samples were branches < 0.25 in. diameter with foliage removed and freeze-dried to < 10% moisture content. Composition is ash = 2.23% and char yield = 22.3%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 9630 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5350 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 22390 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13940 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7740 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32400 \text{ J g}^{-1} \end{aligned}$$

82SUS

PINE, PONDEROSA; *Pinus ponderosa*; solid; Samples were conditioned to moisture equilibrium at 27°C (80°F) and 30% relative humidity; moisture content of wood ~6%.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 8327 \pm 68 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4626 \pm 38 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19355 \pm 159 \text{ J g}^{-1} \end{aligned}$$

67ROB; 64BRO

PINE, PONDEROSA; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 82.54, ash content = 0.29, and fixed carbon = 17.17. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 49.25, hydrogen = 5.99, oxygen = 44.36, nitrogen = 0.06, sulfur = 0.03, chlorine = 0.01, and residue (ash) = 0.30.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned} q_v(\text{gross}) &= 8613 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4785 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20020 \text{ J g}^{-1} \end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{net}) &= 8088 \text{ Btu lb}^{-1} \\ q_v(\text{net}) &= 4493 \text{ cal g}^{-1} \\ q_v(\text{net}) &= 18800 \text{ J g}^{-1} \end{aligned}$$

85JEN/EBE

PINE, PONDEROSA; *Pinus ponderosa*; solid; Wood was air-dried at room temperature. Composition is ash = 0.33% and char yield = 19.5%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 8960 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 14130 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 4980 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7850 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 20820 \text{ J g}^{-1}$	$q_v(\text{gross}) = 32850 \text{ J g}^{-1}$

82SUS

PINE, PONDEROSA; *Pinus ponderosa*; solid; Material was obtained from Whitaker's Forest in Tulare County, California, with predominant soil series of Shaver sandy loam derived from granitic parent material. The layer was collected from the understory of the forest floor. Average yearly decomposition of the forest floor for ponderosa pine is: litter, 11.16%; duff, 2.80%.

gross heat of combustion: assume values refer to room temperature; ash-free.

branch-twig	litter
$q_v(\text{gross}) = 9029 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 9283 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5016 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 5157 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 20987 \text{ J g}^{-1}$	$q_v(\text{gross}) = 21577 \text{ J g}^{-1}$

duff

$$q_v(\text{gross}) = 10240 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 5689 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 23803 \text{ J g}^{-1}$$

78AGE/WAK

PINE, PONDEROSA; AZ 78 FOLIAGE; *Pinus ponderosa*; solid; freeze-dried to < 10% moisture content. Composition is ash = 2.39% and char yield = 25.2%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9470 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13990 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5260 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7770 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 22010 \text{ J g}^{-1}$	$q_v(\text{gross}) = 32510 \text{ J g}^{-1}$

82SUS

PINE, PONDEROSA; BARK; *Pinus ponderosa*; solid; Bark samples were air-dried at room temperature. Composition is ash = 0.52% and char yield = 46.9%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 9470 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5260 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 22010 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13110 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7280 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 30470 \text{ J g}^{-1} \end{aligned}$$

82SUS

PINE, PONDEROSA; CA 77 FOLIAGE; *Pinus ponderosa*; solid; freeze-dried to < 10% moisture content. Composition is ash = 2.63% and char yield = 29.4%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 8840 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4910 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20550 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 14190 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7880 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32980 \text{ J g}^{-1} \end{aligned}$$

82SUS

PINE, PONDEROSA; DEAD FOLIAGE; *Pinus ponderosa*; solid; The litter was air-dried at room temperature. Composition is ash = 3.75% and char yield = 26.5%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 9860 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5480 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 22910 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13740 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7630 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 31940 \text{ J g}^{-1} \end{aligned}$$

82SUS

PINE, PONDEROSA; HEARTWOOD LUMBER; *Pinus ponderosa*; solid; Lumber was air-dried at room temperature. Composition is ash = 0.24% and char yield = 20.3%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9020 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 14120 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5010 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7840 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 20970 \text{ J g}^{-1}$	$q_v(\text{gross}) = 32820 \text{ J g}^{-1}$

82SUS

PINE, PONDEROSA; MT 77 FOLIAGE; *Pinus ponderosa*; solid; freeze-dried to < 10% moisture content. Composition is ash = 2.94% and char yield = 29.0%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9640 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 14030 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5350 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7790 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 22400 \text{ J g}^{-1}$	$q_v(\text{gross}) = 32600 \text{ J g}^{-1}$

82SUS

PINE, PONDEROSA; MT 78 FOLIAGE; *Pinus ponderosa*; solid; freeze-dried to < 10% moisture content. Composition is ash = 2.61% and char yield = 26.9%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel	char (from 500°C heating)
$q_v(\text{gross}) = 9580 \text{ Btu lb}^{-1}$	$q_v(\text{gross}) = 13990 \text{ Btu lb}^{-1}$
$q_v(\text{gross}) = 5320 \text{ cal g}^{-1}$	$q_v(\text{gross}) = 7770 \text{ cal g}^{-1}$
$q_v(\text{gross}) = 22270 \text{ J g}^{-1}$	$q_v(\text{gross}) = 32510 \text{ J g}^{-1}$

82SUS

PINE, SLASH; BARK; *Pinus elliottii*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 0.6%; moisture content = 6.4%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 9002 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5001 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20924 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

PINE, SLASH; FOLIAGE; *Pinus elliottii*; solid; freeze-dried to < 10% moisture content. Composition is ash = 1.54% and char yield = 29.5%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned}q_v(\text{gross}) &= 9300 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5170 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21610 \text{ J g}^{-1}\end{aligned}$$

char (from 500°C heating)

$$\begin{aligned}q_v(\text{gross}) &= 13640 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 7580 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 31700 \text{ J g}^{-1}\end{aligned}$$

82SUS

PINE, SUGAR; *Pinus lambertiana*; solid; Material was obtained from Whitaker's Forest in Tulare County, California, with predominant soil series of Shaver sandy loam derived from granitic parent material. The layer was collected from the understory of the forest floor. Average yearly decomposition of the forest floor for sugar pine is: litter, 8.60%; duff, 2.56%.

gross heat of combustion: assume values refer to room temperature; ash free.

branch-twig

$$\begin{aligned}q_v(\text{gross}) &= 9220 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5122 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21430 \text{ J g}^{-1}\end{aligned}$$

litter

$$\begin{aligned}q_v(\text{gross}) &= 9268 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5249 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21543 \text{ J g}^{-1}\end{aligned}$$

duff

$$\begin{aligned}q_v(\text{gross}) &= 9365 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5203 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21769 \text{ J g}^{-1}\end{aligned}$$

78AGE/WAK

PINE, WESTERN WHITE; DEAD FOLIAGE; *Pinus monticola*; solid; The litter was air-dried at room temperature. Composition is ash = 3.53% and char yield = 34.0%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 9360 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5200 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 21760 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13370 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7430 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 31080 \text{ J g}^{-1} \end{aligned}$$

82SUS

PINE, WHITE; *Pinus strobus*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.25 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.331 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.331 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.385 \end{aligned}$$

12DUN

PINE, WHITE; SAWDUST; *Pinus strobus*; proximate analysis, as delivered: moisture, 7.0%; volatile matter, 78.76%; fixed carbon, 14.10%; ash, 0.14%.

gross heat of combustion: air-dried; assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 8266 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4592 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19213 \text{ J g}^{-1} \end{aligned}$$

68KAI/FRI; 66FRY

POPLAR; genus *Populus*; solid.

gross heat of combustion: assume values refer to room temperature.

as received: 10.69% moisture

$$\begin{aligned} q_v(\text{gross}) &= 7722 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4290 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17948 \text{ J g}^{-1} \end{aligned}$$

air-dried one hour at 105°C (221°F)

$$\begin{aligned} q_v(\text{gross}) &= 8645 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4803 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20096 \text{ J g}^{-1} \end{aligned}$$

22PAR/DAV

POPLAR; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 82.32, ash content = 1.33, and fixed carbon = 16.35. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 48.45, hydrogen = 5.85, oxygen = 43.69, nitrogen = 0.47, sulfur = 0.01, chlorine = 0.10, and residue (ash) = 1.43.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8337 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4632 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19380 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 7826 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4348 \text{ cal g}^{-1} \\q_v(\text{net}) &= 18190 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

POPLAR, YELLOW; *Liriodendron tulipifera*; solid; mean age = 14 years, mean basal stem diameter = 9.7 cm, mean stem bark (proportion of dry weight) = 20.4%, ash content (proportion of oven dry weight) of components of sample: wood = 0.63%, branches = 1.4%, twigs = 2.4%, bark = 4.3%, and leaves = 5.2%.

gross heat of combustion: oven-dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned}q_v(\text{gross}) &= 8674 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4819 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20162 \text{ J g}^{-1}\end{aligned}$$

twigs:

$$\begin{aligned}q_v(\text{gross}) &= 8608 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4782 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20008 \text{ J g}^{-1}\end{aligned}$$

bark:

$$\begin{aligned}q_v(\text{gross}) &= 8336 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4631 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19376 \text{ J g}^{-1}\end{aligned}$$

leaves:

$$\begin{aligned}q_v(\text{gross}) &= 9121 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5067 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21200 \text{ J g}^{-1}\end{aligned}$$

branches:

$$\begin{aligned}q_v(\text{gross}) &= 8640 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4800 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20083 \text{ J g}^{-1}\end{aligned}$$

79NEE/STE

POPULUS HYBRIDS; solid; Sample specimens were composite wood/bark from 4-year-old trees of seven hybrids. Average ash content is 0.80% of oven-dry weight. Selected nutrients given in percent of oven-dry weight are phosphorus, 0.08; potassium, 0.35; calcium, 0.59; magnesium, 0.06; and total extractives, 12.2. Holocellulose and pentosan are 67.1% and 16.2% extractive free oven-dry weight, respectively.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 8386 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4659 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19493 \text{ J g}^{-1}\end{aligned}$$

79BOW/BLA

REDBUD; *Cercis canadensis*; solid; mean age = 10.3 years, mean basal stem diameter = 6.5 cm, mean stem bark (proportion of dry weight) = 9.2%, ash content (proportion of oven dry weight) of components of sample: wood = 0.96%, branches = 1.5%, twigs = 2.2%, bark = 5.5%, and leaves = 5.6%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned}q_v(\text{gross}) &= 8755 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4864 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20351 \text{ J g}^{-1}\end{aligned}$$

bark:

$$\begin{aligned}q_v(\text{gross}) &= 8336 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4631 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19376 \text{ J g}^{-1}\end{aligned}$$

branches:

$$\begin{aligned}q_v(\text{gross}) &= 8528 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4738 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19824 \text{ J g}^{-1}\end{aligned}$$

twigs:

$$\begin{aligned}q_v(\text{gross}) &= 8525 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4736 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19815 \text{ J g}^{-1}\end{aligned}$$

leaves:

$$\begin{aligned}q_v(\text{gross}) &= 9158 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5088 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21288 \text{ J g}^{-1}\end{aligned}$$

79NEE/STE

REDWOOD; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 79.72, ash content = 0.36, and fixed carbon = 19.92. Also the ultimate analysis of the elemental composition of the fuel (values in percent by weight dry basis) is carbon = 50.64, hydrogen = 5.98, oxygen = 42.88, nitrogen = 0.05, sulfur = 0.03, chlorine = 0.02, and residue (ash) = 0.40.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8914 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4952 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20720 \text{ J g}^{-1}\end{aligned}$$

net heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{net}) &= 8393 \text{ Btu lb}^{-1} \\q_v(\text{net}) &= 4663 \text{ cal g}^{-1} \\q_v(\text{net}) &= 19510 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

REDWOOD, BARK; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 68.44, ash content = 1.60, and fixed carbon = 29.96.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8424 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4680 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19580 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

REDWOOD, HEARTWOOD; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 80.28, ash content = 0.17, and fixed carbon = 19.55.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 9095 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5053 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21140 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

REDWOOD, MILL WASTES; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 81.19, ash content = 0.18, and fixed carbon = 18.63.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 9026 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5014 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20980 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

REDWOOD, SAPWOOD; solid; Material is considered biomass fuel and has proximate analysis values (in percent by weight dry basis) for volatile concentration (VCM) = 80.12, ash content = 0.67, and fixed carbon = 19.21.

gross heat of combustion: assume values refer to room temperature; determination performed at 30 atm O₂, and corrections applied for the formation of nitric and sulfuric acids.

$$\begin{aligned}q_v(\text{gross}) &= 8738 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4854 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20310 \text{ J g}^{-1}\end{aligned}$$

85JEN/EBE

SEQUOIA, GIANT; *Sequoiadendron giganteum*; solid; Material was obtained from Whitaker's Forest in Tulare County, California, with predominant soil series of Shaver sandy loam derived from granitic parent material. The layer was collected from the understory of the forest floor. Average yearly decomposition of the forest floor for giant sequoia is: litter, 2.77%; duff, 11.40%.

gross heat of combustion: assume values refer to room temperature; ash-free.

branch-twig

duff

$$\begin{aligned}q_v(\text{gross}) &= 8885 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4936 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20652 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}q_v(\text{gross}) &= 9225 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5123 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21435 \text{ J g}^{-1}\end{aligned}$$

litter

$$\begin{aligned}q_v(\text{gross}) &= 9196 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5109 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21376 \text{ J g}^{-1}\end{aligned}$$

78AGE/WAK

SOUTHERN HARDWOOD, SAWMILL RESIDUE, FRESH; solid; Material is mixed sawdust and bark residue coming directly from the mill (generated the same day) collected from 6 mills around Baton Rouge, Louisiana. The average moisture content is 107%; when moderately packed the average density = 24.0 lb ft^{-3} .

gross heat of combustion: oven-dry weight, assume values refer to room temperature, and value is an average.

$$\begin{aligned} q_v(\text{gross}) &= 8017 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4454 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18635 \text{ J g}^{-1} \end{aligned}$$

76CAS/CHO

SOUTHERN HARDWOOD, SAWMILL RESIDUE, PILED; solid; Material is mixed sawdust and bark residue from hardwood trees after it has been piled and exposed to the weather, collected from 6 sawmills near Baton Rouge, Louisiana. The average moisture content is 184%; average density = 29.4 lb ft^{-3} .

gross heat of combustion: oven-dry weight; assume values refer to room temperature, and value is an average.

$$\begin{aligned} q_v(\text{gross}) &= 8046 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4470 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 18702 \text{ J g}^{-1} \end{aligned}$$

76CAS/CHO

SPRUCE, BALSAM; *Abies lasiocarpa*; solid; ultimate analysis: carbon, 51.41%; hydrogen, 6.41%; nitrogen, 1.44%; sulfur, 0.19%; ash, 3.07%; moisture, 3.76%; proximate analysis as received: moisture, 74.35%; volatile matter, 20.20%; fixed carbon, 4.13%; ash, 0.82%.

gross heat of combustion: assume values refer to room temperature.

air-dried at 80°C (176°F)

as received

$$\begin{aligned} q_v(\text{gross}) &= 9547 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 5304 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 22191 \text{ J g}^{-1} \end{aligned}$$

$$\begin{aligned} q_v(\text{gross}) &= 2448 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 1360 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 5692 \text{ J g}^{-1} \end{aligned}$$

68KAI/FRI

SPRUCE, BLACK; BARK; *Picea mariana*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 2.0%; moisture content = 6.5%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned} q_v(\text{gross}) &= 8246 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4581 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19167 \text{ J g}^{-1} \end{aligned}$$

55CHA/MIT

SPRUCE, ENGELMANN; BARK; *Picea engelmannii*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 2.5%; moisture content = 5.5%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 8359 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4644 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19430 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

SPRUCE, NORWAY; *Pinus abies*; solid; carbon, 50.31%; hydrogen, 6.20%; nitrogen, 0.04%; ash, 0.37%.

gross heat of combustion: at 20°C (68°F); air-dried at 110°-115°C (230°-240°F); ash free.

$$\begin{aligned}q_v(\text{gross}) &= 9167 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5093 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21309 \text{ J g}^{-1}\end{aligned}$$

1883GOT

SPRUCE PINE; *Pinus glabra*; solid; samples were dried for 8 hours in a vacuum oven at 103°C (217°F).

specific heat: 333-413 K (140°-284°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.2472 + 5.577 \times 10^{-4} T \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= -0.0091 + 1.004 \times 10^{-3} T \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= -0.0389 + 4.201 \times 10^{-3} T\end{aligned}$$

68KAI/FRI

SPRUCE PINE, BARK; *Pinus glabra*; solid; bark specimens oven-dried at 152°C (306°F).

specific heat: 333-413 K (140°-284°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.3383 - 2.4489 \times 10^{-4} T + 1.5855 \times 10^{-6} T^2 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.7859 - 3.0645 \times 10^{-3} T + 5.137 \times 10^{-6} T^2 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 3.2882 - 1.2822 \times 10^{-2} T + 2.1493 \times 10^{-5} T^2\end{aligned}$$

68KAI/FRI

SPRUCE, RED; *Picea rubens*; solid; air-dried at 105°-110°C (221°-230°F); density, 0.39 g cm⁻³.

specific heat: 273-379 K (32°-223°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.332 \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.332 \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.389 \end{aligned}$$

12DUN

SWEETGUM; *Liquidambar styraciflua*; solid; mean age = 10 years, mean basal stem diameter = 7.0 cm, mean stem bark (proportion of dry weight) = 16.0%, ash content (proportion of oven dry weight) of components of sample: wood = 0.57%, branches = 2.0%, twigs = 3.3%, bark = 5.7%, and leaves = 3.9%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned} q_v(\text{gross}) &= 8498 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4721 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19753 \text{ J g}^{-1} \end{aligned}$$

bark:

$$\begin{aligned} q_v(\text{gross}) &= 8224 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4569 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19117 \text{ J g}^{-1} \end{aligned}$$

branches:

$$\begin{aligned} q_v(\text{gross}) &= 8431 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4684 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19598 \text{ J g}^{-1} \end{aligned}$$

twigs:

$$\begin{aligned} q_v(\text{gross}) &= 8464 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4702 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19673 \text{ J g}^{-1} \end{aligned}$$

leaves:

$$\begin{aligned} q_v(\text{gross}) &= 8384 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4658 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19489 \text{ J g}^{-1} \end{aligned}$$

79NEE/STE

SWEETGUM; *Liquidambar styraciflua*; solid; Material was collected from the southern Atlantic and Gulf coastal plains in bottom-, swamp- and wet flat-land natural stand sites. Samples were dried at 70°C (158°F) to a constant weight; reported values were averaged over all positions of similar plant tissue for each tree and six trees per species were used.

gross heat of combustion: assume values refer to room temperature; values are on a dry weight basis.

bole wood

$$\begin{aligned}q_v(\text{gross}) &= 8194 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4552 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19046 \text{ J g}^{-1}\end{aligned}$$

branch wood

$$\begin{aligned}q_v(\text{gross}) &= 8239 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4577 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19150 \text{ J g}^{-1}\end{aligned}$$

bole bark

$$\begin{aligned}q_v(\text{gross}) &= 7555 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4197 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17560 \text{ J g}^{-1}\end{aligned}$$

branch bark

$$\begin{aligned}q_v(\text{gross}) &= 7902 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4390 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18368 \text{ J g}^{-1}\end{aligned}$$

foliage

$$\begin{aligned}q_v(\text{gross}) &= 8500 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4722 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19757 \text{ J g}^{-1}\end{aligned}$$

82GOW/FRE

SWEETGUM, BARK; *Liquidambar styraciflua*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 5.7%; moisture content = 6.2%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 7450 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4139 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 17318 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

SYCAMORE; *Platanus occidentalis*; solid; Each tree was separated into small parts (being less than 0.64 cm (1/4 in.) in diameter and roughly equivalent to tops and branches) and large parts with the weighted proportion of small (25%) and large (75%) material in the whole tree. Overall mean specific gravity for whole tree = 0.42 (oven dry weight and green volume). Bark proportion of whole tree = 18%.

gross heat of combustion: oven-dried, assume values refer to room temperature.

small parts

$$\begin{aligned}q_v(\text{gross}) &= 8104 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4502 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18836 \text{ J g}^{-1}\end{aligned}$$

large parts

$$\begin{aligned}q_v(\text{gross}) &= 8323 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4624 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19347 \text{ J g}^{-1}\end{aligned}$$

whole tree

$$\begin{aligned}q_v(\text{gross}) &= 8269 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4595 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19221 \text{ J g}^{-1}\end{aligned}$$

81GEY

SYCAMORE, AMERICAN; *Platanus occidentalis*; solid; mean age = 11.3 years, mean basal stem diameter = 9.4 cm, mean stem bark (proportion of dry weight) = 8.7%, ash content (proportion of oven dry weight) of components of sample: wood = 0.54%, branches = 1.3%, twigs = 1.6%, bark = 4.5%, and leaves = 4.8%.

gross heat of combustion: oven dry weight basis; assume values refer to room temperature.

wood:

$$\begin{aligned}q_v(\text{gross}) &= 8561 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4756 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19899 \text{ J g}^{-1}\end{aligned}$$

bark:

$$\begin{aligned}q_v(\text{gross}) &= 8602 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4779 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 19995 \text{ J g}^{-1}\end{aligned}$$

branches:

$$\begin{aligned}q_v(\text{gross}) &= 8741 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4856 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20318 \text{ J g}^{-1}\end{aligned}$$

twigs:

$$\begin{aligned}q_v(\text{gross}) &= 8770 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4872 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 20384 \text{ J g}^{-1}\end{aligned}$$

leaves:

$$\begin{aligned}q_v(\text{gross}) &= 9308 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 5171 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 21635 \text{ J g}^{-1}\end{aligned}$$

79NEE/STE

SYCAMORE, AMERICAN; BARK; *Platanus heterophylla*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 5.8%; moisture content = 6.4%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned} q_v(\text{gross}) &= 7403 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4113 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 17209 \text{ J g}^{-1} \end{aligned}$$

55CHA/MIT

TUNDRA, INTERIOR; *Hylocomium splendens* and *Pleurozium schreberi*; solid; Sample material was top layer of black-spruce understory. Composition is ash = 34.10% and char yield = 35.5%. Char was obtained from heating the sample to 500°C (932°F) in nitrogen.

gross heat of combustion: ash-free, dry basis; assume values refer to room temperature.

fuel

$$\begin{aligned} q_v(\text{gross}) &= 8730 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4850 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 20290 \text{ J g}^{-1} \end{aligned}$$

char (from 500°C heating)

$$\begin{aligned} q_v(\text{gross}) &= 13780 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7650 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32020 \text{ J g}^{-1} \end{aligned}$$

82SUS

TUPELO, WATER; *Nyssa aquatica*; solid; Material was collected from the southern Atlantic and Gulf coastal plains in bottom-, swamp- and wet flat-land natural stand sites. Samples were dried at 70°C (158°F) to a constant weight; reported values were averaged over all positions of similar plant tissue for each tree and six trees per species were used.

gross heat of combustion: assume values refer to room temperature; values are on a dry weight basis.

bole wood

$$\begin{aligned} q_v(\text{gross}) &= 8361 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4645 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19435 \text{ J g}^{-1} \end{aligned}$$

branch wood

$$\begin{aligned} q_v(\text{gross}) &= 8442 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4690 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19623 \text{ J g}^{-1} \end{aligned}$$

bole bark

$$\begin{aligned} q_v(\text{gross}) &= 8575 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4764 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19933 \text{ J g}^{-1} \end{aligned}$$

branch bark

$$\begin{aligned} q_v(\text{gross}) &= 8532 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 4740 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 19832 \text{ J g}^{-1} \end{aligned}$$

(more)

TUPELO, WATER - Continued

foliage

$$q_v(\text{gross}) = 8820 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4900 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 20502 \text{ J g}^{-1}$$

82GOW/FRE

WARTY-BARKED SPINDLE TREE; *Eonymus verrucosus*; solid; Material is a tree, one of the dominant species of a 65-year-old climazonal oak forest (*Quercetum petraeae-cerris*) on brown forest soil, at 300 m above sea level located in the southern part of the Bukk Mountains of north Hungary. Samples were dried at 85°C (185°F), then ground and pelleted. The ash content was determined at 500°C (932°F) while the temperature was increased stepwise. Ash content of stem and branch wood = 0.7%; stem and branch bark = 6.3%; leaf = 9.5%; root = 8.1%.

gross heat of combustion: at 20 atm oxygen pressure, assume values refer to room temperature.

	dry weight basis	ash-free dry weight basis	std dev. of mean	
stem and branch wood (3 measurements)				
$q_v(\text{gross}) =$	8491	8548	16	Btu lb ⁻¹
$q_v(\text{gross}) =$	4717	4749	9.0	cal g ⁻¹
$q_v(\text{gross}) =$	19736	19870	38	J g ⁻¹
stem and branch bark (5 measurements)				
$q_v(\text{gross}) =$	8548	9146	42.8	Btu lb ⁻¹
$q_v(\text{gross}) =$	4749	5081	23.8	cal g ⁻¹
$q_v(\text{gross}) =$	19870	21259	99.6	J g ⁻¹
leaf (5 measurements)				
$q_v(\text{gross}) =$	8215	9074	82.6	Btu lb ⁻¹
$q_v(\text{gross}) =$	4564	5041	45.9	cal g ⁻¹
$q_v(\text{gross}) =$	19096	21092	192	J g ⁻¹
root (3 measurements)				
$q_v(\text{gross}) =$	8305	9041	35.6	Btu lb ⁻¹
$q_v(\text{gross}) =$	4614	5023	19.8	cal g ⁻¹
$q_v(\text{gross}) =$	19305	21016	82.8	J g ⁻¹

75PAP

WILLOW, BLACK; BARK; *Salix nigra*; solid; gross heat of combustion determined on 1 g samples of air-dried bark; ash content = 6.0%; moisture content = 6.7%.

gross heat of combustion: assume values refer to room temperature; values not corrected for moisture or ash contents; hence, are on an as-determined basis.

$$\begin{aligned}q_v(\text{gross}) &= 7168 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3982 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 16661 \text{ J g}^{-1}\end{aligned}$$

55CHA/MIT

WILLOW, SANDBAR; *Salix exigua*; solid; Each tree was separated into small parts (being less than 0.64 cm (1/4 in.) in diameter and roughly equivalent to tops and branches) and large parts with the weighted proportion of small (25%) and large (75%) material in the whole tree. Overall mean specific gravity for whole tree = 0.38 (oven dry weight and green volume). Bark of whole tree = 25%.

gross heat of combustion: oven-dried, assume values refer to room temperature.

small parts

$$\begin{aligned}q_v(\text{gross}) &= 8017 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4454 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18636 \text{ J g}^{-1}\end{aligned}$$

large parts

$$\begin{aligned}q_v(\text{gross}) &= 7922 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4401 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18414 \text{ J g}^{-1}\end{aligned}$$

whole tree

$$\begin{aligned}q_v(\text{gross}) &= 7943 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 4413 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 18464 \text{ J g}^{-1}\end{aligned}$$

81GEY

Miscellaneous

AMATOL; solid; an explosive mixture of ammonium nitrate (AN) and trinitrotoluene (TNT). Density of cast material: 80/20 AN/TNT, 1.46 g cm^{-3} ; 60/40 AN/TNT, 1.60 g cm^{-3} ; 50/50 AN/TNT, 1.59 g cm^{-3} .

gross heat of combustion: 25°C (77°F); calculated from the composition of the mixture.

80/20 AN/TNT

$$q_v(\text{gross}) = 2194 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 1219 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 5100 \text{ J g}^{-1}$$

50/50 AN/TNT

$$q_v(\text{gross}) = 3793 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 2107 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 8816 \text{ J g}^{-1}$$

60/40 AN/TNT

$$q_v(\text{gross}) = 3260 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 1811 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 7577 \text{ J g}^{-1}$$

specific heat: for the temperature range $293\text{--}353 \text{ K}$ ($64^\circ\text{--}176^\circ\text{F}$) for 50/50 AN/TNT mixture.

$$C_p = 0.383 \text{ Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}$$

$$C_p = 0.383 \text{ cal g}^{-1} \text{ K}^{-1}$$

$$C_p = 1.602 \text{ J g}^{-1} \text{ K}^{-1}$$

71USA; 70COX/PIL; 68WAG/EVA

CELLULOSE NITRATE; solid; Cellulose does not form nitrate in a stoichiometric manner; the degree of nitration is measured by the percent of nitrogen in the ester.

mononitrocellulose: $[\text{C}_6\text{H}_9\text{NO}_7]_x$; 6.76% nitrogen

dinitrocellulose: $[\text{C}_6\text{H}_8\text{N}_2\text{O}_9]_x$; 11.11% nitrogen

trinitrocellulose: $[\text{C}_6\text{H}_7\text{N}_3\text{O}_{11}]_x$; 14.14% nitrogen

cellulose nitrate, grade B (guncotton) $\text{C}_6\text{H}_{7.26}\text{N}_{2.74}\text{O}_{10.48}$

cellulose nitrate, grade C (type I) $\text{C}_6\text{H}_{7.36}\text{N}_{2.67}\text{O}_{10.27}$

cellulose nitrate, grade C (type II) $\text{C}_6\text{H}_{7.33}\text{N}_{2.67}\text{O}_{10.34}$

cellulose nitrate, grade D (pyroxylin) $\text{C}_6\text{H}_{7.68}\text{N}_{2.32}\text{O}_{10.64}$

gross heat of combustion: at 30°C (86°F) for $[0.115 \leq N \leq 0.135]$; N = wt. fraction nitrogen.

$$q_v(\text{gross}) = 7516.8 - 25427N \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4176.0 - 14126N \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 17472.4 - 59103N \text{ J g}^{-1}$$

50JES/PRO; 74DEC/WAR

CORAL BRANCH TIPS; *Eunicella papillosa*; solid; Material was the mesoskeleton of the gorgonian tropical reef-building coral (Octocorallia) from the Atlantic side of Cape Peninsula, Africa. The 2 cm apex of the branches were oven-dried at 55°C (131°F) to constant weight. Because of high CaCO₃ content of the tissue, correction for endothermy was used to ensure accuracy. The relationship of organic protein nitrogen to tissue weight is 3.68 ± 0.62 mg g⁻¹. There was a 50% water loss per gram dry weight. Samples were taken from 14 colonies.

gross heat of combustion: mean values were for dry weight basis; 14 samples were used; assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 1777 \pm 379 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 987 \pm 210 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 4130 \pm 880 \text{ J g}^{-1}\end{aligned}$$

79VEL/KIN

CORAL BRANCHES; *Eunicella papillosa*; solid; Material was the mesoskeleton of the gorgonian tropical reef-building coral (Octocorallia) from the Atlantic side of Cape Peninsula, Africa. The branches (excluding tips), middle sections of branches, and ramification points were oven-dried at 55°C (131°F) to constant weight. Because of high CaCO₃ content, the tissue correction for endothermy was used to ensure accuracy. The relationship of organic protein nitrogen to tissue weight is 3.63 ± 0.80 mg g⁻¹. There was a 41% water loss per gram dry weight. Samples were taken from 14 colonies.

gross heat of combustion: mean values were for dry weight basis; 14 samples were used; assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 1549 \pm 327 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 860 \pm 182 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 3600 \pm 760 \text{ J g}^{-1}\end{aligned}$$

79VEL/KIN

DBX; solid; ammonium nitrate (AN), 21%; cyclotrimethylenetrinitramine (RDX), 21%; trinitrotoluene (TNT), 40%; aluminum, 18%; density, 1.68 g cm⁻³.

gross heat of combustion: assume values refer to room temperature; calculated from the composition of the mixture.

$$\begin{aligned}q_v(\text{gross}) &= 6082 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3379 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 14138 \text{ J g}^{-1}\end{aligned}$$

specific heat: 268 K (23°F)

$$\begin{aligned}C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.25 \\C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.25 \\C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 1.05\end{aligned}$$

71USA; 70COX/PIL; 68WAG/EVA; 76WAG/EVA; 73KRI/LIC

DOWTHERM A; liquid; (trademark, Dow Chemical Co.); a mixture of diphenyl and diphenyl oxide.

specific heat: 323–513 K (122°–464°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1}) &= 0.356 + 4.111 \times 10^{-4} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.167 + 7.40 \times 10^{-4} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.699 + 3.096 \times 10^{-3} T \end{aligned}$$

60BOW/GAR

FAT, WOOL; solid; (lanolin); Main constituents are cholesterol esters of higher molecular weight fatty acids.

gross heat of combustion: assume values refer to room temperature and are corrected for moisture and ash content.

$$\begin{aligned} q_v(\text{gross}) &= 17530 \pm 6.3 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 9741 \pm 3.5 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 40756 \pm 14.6 \text{ J g}^{-1} \end{aligned}$$

64PAL/REI

GRAPHITE, ARTIFICIAL; solid; National Carbon Co. spectroscopic grade.

gross heat of combustion: at 25°C (77°F), average of 2 samples

$$\begin{aligned} q_v(\text{gross}) &= 12664 \pm 4.3 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7035.8 \pm 2.4 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32785 \pm 10 \text{ J g}^{-1} \end{aligned}$$

38DEW/HAR

GRAPHITE, BUCKINGHAM; solid; 0.25% ash.

gross heat of combustion: at 25°C (77°F), average of 2 samples; corrected for ash content.

$$\begin{aligned} q_v(\text{gross}) &= 14106 \pm 3.6 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7836.8 \pm 2.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32789 \pm 8 \text{ J g}^{-1} \end{aligned}$$

38DEW/HAR

GRAPHITE, CEYLON; solid; 2.2% ash.

gross heat of combustion: at 25°C (77°F), average of 2 samples; corrected for ash content.

$$\begin{aligned} q_v(\text{gross}) &= 14085 \pm 0.9 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7825.0 \pm 0.5 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32740 \pm 2 \text{ J g}^{-1} \end{aligned}$$

38DEW/HAR

GRAPHITE, PYROLYTIC; Total gas content is less than 1 ppm; (sample 1) annealed at 2200°C (3992°F), having a density of 2.204 g ml⁻¹; (sample 2) annealed at 3000°C (5432°F), having a density of 2.265 g ml⁻¹.

gross heat of combustion: at 25°C (77°F)

sample 1

$$\begin{aligned} q_v(\text{gross}) &= 14121 \pm 3.1 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7844.9 \pm 1.7 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32823.1 \pm 7.1 \text{ J g}^{-1} \end{aligned}$$

sample 2

$$\begin{aligned} q_v(\text{gross}) &= 14083 \pm 5.4 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7823.9 \pm 3.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32735.2 \pm 12.6 \text{ J g}^{-1} \end{aligned}$$

65LEW/FRI

GRAPHITE, TICONDEROGA; solid; 0.33% ash.

gross heat of combustion: at 25°C (77°F), average of 2 samples; corrected for ash content.

$$\begin{aligned} q_v(\text{gross}) &= 14105 \pm 1.8 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 7836.0 \pm 1.0 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 32786 \pm 4 \text{ J g}^{-1} \end{aligned}$$

38DEW/HAR

LEATHER; solid; an animal skin or hide that has been permanently combined with a tanning agent; the tanning agent produces a transformation in the protein composition of the skin rendering it resistant to putrefactive bacteria, increasing its strength and abrasion resistance.

specific heat: 298 K (77°F)

moisture content, %	$C_p(\text{Btu lb}^{-1} \text{ } ^\circ\text{F}^{-1})$	$C_p(\text{cal g}^{-1} \text{ K}^{-1})$	$C_p(\text{J g}^{-1} \text{ K}^{-1})$
vegetable-tanned			

0	0.3334	0.3334	1.3949
1.15	0.3202	0.3202	1.3397
1.32	0.3274	0.3274	1.3698
2.59	0.3280	0.3280	1.3724
3.85	0.3844	0.3844	1.6083
6.20	0.3730	0.3730	1.5606
7.83	0.3835	0.3835	1.6046
9.31	0.3844	0.3844	1.6083
10.81	0.4129	0.4129	1.7276

(more)

LEATHER - Continued

moisture content, %	C_p (Btu lb ⁻¹ °F ⁻¹)	C_p (cal g ⁻¹ K ⁻¹)	C_p (J g ⁻¹ K ⁻¹)
chrome-tanned			
0	0.3045	0.3045	1.2740
1.98	0.2918	0.2918	1.2209
3.69	0.3631	0.3631	1.5192
7.59	0.3576	0.3576	1.4962
9.39	0.3737	0.3737	1.5636
11.07	0.3893	0.3893	1.6288
13.46	0.3841	0.3841	1.6071
14.96	0.4098	0.4098	1.7146
chrome-retanned			
0	0.3404	0.3404	1.4242
1.52	0.3287	0.3287	1.3753
2.12	0.3266	0.3266	1.3665
4.23	0.3448	0.3448	1.4426
7.23	0.3458	0.3458	1.4468
9.23	0.3474	0.3474	1.4535
11.29	0.3606	0.3606	1.5088

55KAN

LEATHER, SHOE; solid; ultimate analysis in percent by weight: carbon, 42.01%; hydrogen, 5.32%; oxygen, 22.83%; nitrogen, 5.98%; sulfur, 1.00%; ash, 22.86%; proximate analysis as received in percent by weight: moisture, 7.46%; volatile matter, 57.12%; fixed carbon, 14.26%; ash, 21.16%.

gross heat of combustion: assume values refer to room temperature.

as received

$$q_v(\text{gross}) = 7249 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4027 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 16847 \text{ J g}^{-1}$$

dry basis

$$q_v(\text{gross}) = 7832 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 4351 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 18203 \text{ J g}^{-1}$$

66KAI

NEAT'S FOOT OIL, REFINED; liquid; The saponification number, which is the mean molecular weight of the fatty acids present in the molecule = 194. The amount of iodine absorbed and expressed as a percentage of the molecular weight (a measure of the proportion of unsaturated fatty acid present) called the iodine number = 69.

enthalpy difference: temperature range measured -50° to 55°C (-58° to 131°F).

temperature (°C)	(°F)	Btu lb ⁻¹	H°(t)-H°(-50°C) cal g ⁻¹	J g ⁻¹
-50	-58	0.00	0.00	0.00
-25	-13	17.89	9.89	41.38
0	32	53.37	29.65	124.06
25	77	90.58	50.32	210.54
50	122	112.18	62.32	260.75
55	131	116.57	64.76	270.96

heat of fusion: result is a mean value for temperature range -50° to 55°C (-58° to 131°F).

$$L_f = 34.2 \text{ Btu lb}^{-1}$$

$$L_f = 19.0 \text{ cal g}^{-1}$$

$$L_f = 79.5 \text{ J g}^{-1}$$

55RIE

PB-RDX; solid; cyclotrimethylenetrinitramine (RDX), 90%; unmodified polystyrene, 8.5%; dioctyl phthalate, 1.5%.

gross heat of combustion: assume values refer to room temperature.

$$q_v(\text{gross}) = 5449 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 3027 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 12665 \text{ J g}^{-1}$$

71USA

PENTOLITE; solid; an explosive mixture of trinitrotoluene (TNT) and pentaerythritol tetranitrate (PETN); 50/50 PETN/TNT; density, 1.65 g cm⁻³.

gross heat of combustion: 25°C (77°F); calculated from the composition of the mixture.

$$q_v(\text{gross}) = 4993 \text{ Btu lb}^{-1}$$

$$q_v(\text{gross}) = 2774 \text{ cal g}^{-1}$$

$$q_v(\text{gross}) = 11606 \text{ J g}^{-1}$$

71USA; 70COX/PIL

POLYVINYL NITRATE; solid; repeating unit: $C_2H_3NO_3$; used in explosive applications.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 5328 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 2960 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 12385 \text{ J g}^{-1} \end{aligned}$$

71USA

PROPELLANT, BAKELITE RESIN BINDER FUEL; solid; Material is a phenol-formaldehyde casting resin used as a binder fuel.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned} q_v(\text{gross}) &= 12506 \text{ Btu lb}^{-1} \\ q_v(\text{gross}) &= 6948 \text{ cal g}^{-1} \\ q_v(\text{gross}) &= 29070 \text{ J g}^{-1} \end{aligned}$$

76GIR/ARO

PROPELLANT, OS/AP; solid; Oxygen-styrene copolymer was prepared by passing oxygen at 1 atm through styrene for 24 hours in the presence of azobisisobutyronitrile; the reaction was completed by adding benzoyl peroxide and maintaining the solution at 50°C (122°F) for another 24 hours until it became sufficiently viscous; (OS/AP) = (oxygen-styrene copolymer) - ammonium perchlorate composite propellant.

gross heat of combustion: assume values refer to room temperature.

copolymer (wt. %)	Btu lb ⁻¹	$q_v(\text{gross})$ cal g ⁻¹	J g ⁻¹
30	1996 ± 18	1109 ± 10	4640 ± 42
25	2102 ± 41	1168 ± 23	4887 ± 96
20	2342 ± 14	1301 ± 8	5443 ± 33

74RAS/KIS

SANTOWAX R; liquid; (trade mark, Monsanto Co.); mixture of terphenyl hydrocarbons.

specific heat: 453-593 K (356° - 608°F)

$$\begin{aligned} C_p(\text{Btu lb}^{-1} \text{ }^\circ\text{F}^{-1}) &= 0.372 + 3.256 \times 10^{-4} T \\ C_p(\text{cal g}^{-1} \text{ K}^{-1}) &= 0.222 + 5.86 \times 10^{-4} T \\ C_p(\text{J g}^{-1} \text{ K}^{-1}) &= 0.929 + 2.452 \times 10^{-3} T \end{aligned}$$

60BOW/GAR

Miscellaneous

VACUUM CLEANER CATCH; solid; ultimate analysis on dry basis in percent by weight: carbon, 35.69%; hydrogen, 4.73%; oxygen, 20.08%; nitrogen, 6.26%; sulfur, 1.15%; ash, 32.09%; proximate analysis as received in percent by weight: moisture, 5.47%; volatile matter, 55.68%; fixed carbon, 8.51%; ash, 30.34%.

gross heat of combustion: assume values refer to room temperature.

as received

dry basis

$$\begin{aligned}q_v(\text{gross}) &= 6390 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3550 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 14854 \text{ J g}^{-1}\end{aligned}$$

$$\begin{aligned}q_v(\text{gross}) &= 6761 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 3756 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 15714 \text{ J g}^{-1}\end{aligned}$$

66KAI

VASELINE; solid; semi-solid mixture of hydrocarbons having a melting point range from 38°-60°C (100°-140°F); colorless or pale yellow petroleum jelly.

gross heat of combustion: assume values refer to room temperature.

$$\begin{aligned}q_v(\text{gross}) &= 19890 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 11050 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 46233 \text{ J g}^{-1}\end{aligned}$$

56ROT/BEC

WAX, PARAFFIN; solid; hard wax, freezing point 53°-55°C (127°-131°F); density, 0.902 g cm⁻³; repeating unit: CH₂.

gross heat of combustion: 25°C (77°F)

$$\begin{aligned}q_v(\text{gross}) &= 19888 \text{ Btu lb}^{-1} \\q_v(\text{gross}) &= 11049 \text{ cal g}^{-1} \\q_v(\text{gross}) &= 46229 \text{ J g}^{-1}\end{aligned}$$

56MAG

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Appendix A

A FORMULA FOR THE EMPIRICAL ESTIMATION OF THE HEATS OF COMBUSTION OF CARBONACEOUS MATERIALS (Thomas B. Reed, Solar Energy Research Institute)

In modeling biomass reactions and reactors it is necessary to have values for the heats of formation and combustion of the various materials considered. A collection of representative data for biomass and wastes appears in the main body of this publication. In some cases, the composition of carbonaceous materials is known or can be estimated, while the heats have not been measured.

In 1978, the Institute of Gas Technology developed a formula for predicting the higher heating values (heat of combustion) (HHV, dry basis) of coal (IGT, 1978)

$$\text{HHV} = \Delta H_C = 146.58 C + 568.78 H - 51.53 (O + N) - 6.58 A + 29.45 S \text{ Btu/lb}$$

(where C, H, O, N, S, and A are the weight percents of carbon, hydrogen, oxygen, nitrogen, sulfur, and ash respectively). This equation was derived by correlating the thermal data with the composition on more than 700 samples of coal. In the *Survey of Biomass Gasification* (Reed, 1979) Graboski and Bain used this formula, as well as two others, on 15 samples of biomass and 5 samples of char and found average errors from the measured values of 1.7% and 2.1% respectively. The error of actual measurements of composition and heats of combustion probably exceeds this, so that this suggests that the method can be used for all biomass solids.

Reed (1985) has extended the IGT equation to a wide variety of carbonaceous materials. The equation in the modified SI form is:

$$\text{HHV} = 0.341 C + 1.322 H - 0.12 (O + N) - 0.0153 A + 0.0686 S \text{ kJ/g}$$

Note that in general the last two terms will be very small compared to the first three. The equation is also useful in the molecular form:

$$\Delta H_C = 4.092 n_C + 1.322 n_H - 1.916 n_{(N + O)} \text{ kJ/mole on a dry, ash-free, sulfur-free basis.}$$

(where n_i is the number of moles of each element in the formula) to estimate the heat of combustion for biomass in which the formulas are given. The heat of formation can be calculated from the heat of combustion from using the equation:

$$\Delta H_f = \Delta H_C - n_C [\Delta H_C(C)] - n_H [\Delta H_C(H_2)/2]$$

where $\Delta H_C(C)$ and $\Delta H_C(H_2)$ are the heats of combustion of carbon and hydrogen.

The above equations were used to calculate thermal data for the biomass-related materials shown in Table A-1. This table includes representative samples of biomass, charcoals, pyrolysis oils, and tars taken from the literature but not included in this handbook. The average absolute error for each of these materials was 1.6%, 1.6%, 2.5%, and 2.5% respectively. Thus, it seems that the above equations form a reliable basis for predicting biomass thermochemical data where measured heats are not available, and can form a supplement to the representative heats of combustion shown in this publication.

Table A-1. Calculated and Measured Heats of Combustion for Various Biomass Materials Using an Empirical Formula

Name	Reference	Composition Dry, ash-free basis, Wt%			Heat of Combustion		Error (Meas-Calc) Measured	
		C	H	O	Measured HHV-kJ/g	Calculated HHV-kJ/g		
Biomass Components								
Cellulose (Avicel)	Mok	43.3	6.3	50.4	NA	17.14	NA	
Lignin (Indulin)	Mok	66.8	5.5	27.7	NA	26.77	NA	
Biomass								
Pine Sawdust	Diebold	51.3	6.0	42.7	20.21	20.40	-0.009	
Maple	Tillman	51.5	6.1	42.4	20.28	20.59	-0.015	
Douglas Fir	Tillman	52.8	6.4	40.9	21.22	21.56	-0.016	
Paper	Reed (1981)	46.4	6.2	47.4	18.82	18.41	0.022	
Maritime Pine	Bourgeois	52.6	6.2	41.2	20.59	21.23	-0.031	
Chestnut & Oak	Bourgeois	50.1	5.6	44.3	19.20	19.27	-0.004	
"Typical biomass"	Reed (1985)	52.2	6.1	41.7	NA	20.89	NA	
					Avg Abs error		0.016	
Primary Oils								
Primary Oils R 35CS	Diebold	54.5	5.7	39.8	20.31	21.44	-0.055	
Primary Oils R 40CS	Diebold	57.6	5.9	36.5	22.88	23.11	-0.010	
Primary Oils R 40PS	Diebold	57.1	5.6	37.2	22.27	22.53	-0.011	
					Avg Abs error		0.025	
Chars								
	*							
Torrefied Pine	280	Bourgeois	60.8	5.7	33.5	23.90	24.30	-0.017
Torr. Chestnut & Oak	275	Bourgeois	57.8	5.3	36.9	22.70	22.36	0.015
Charcoal		Tillman	84.8	3.3	11.9	32.81	31.85	0.029
Fir Bark Char		Reed (1981)	63.6	5.1	31.3	24.49	24.75	-0.011
Grass Straw Char		Reed (1981)	68.5	5.0	26.5	25.93	26.82	-0.035
Rice Hull Char		Reed (1981)	71.6	5.2	23.3	28.18	28.50	-0.011
Redwood Charcoal	549	Reed (1981)	77.7	3.4	18.9	29.62	28.75	0.029
Oak Charcoal	571	Reed (1981)	78.6	2.6	18.9	28.02	27.96	0.002
Oak Charcoal	641	Reed (1981)	80.1	2.8	17.0	29.32	29.07	0.008
Redwood Charcoal	941	Reed (1981)	82.5	3.7	13.8	31.88	31.37	0.016
FP Char, Run 53	625	Diebold	87.7	3.8	8.4	34.40	33.98	0.012
FP Char, Run 54	625	Diebold	83.2	3.7	13.1	34.09	31.72	0.070
FP Char, Run 59	625	Diebold	84.1	3.8	12.1	33.63	32.25	0.041
FP Char, Run X	800	Diebold	92.6	1.9	5.5	33.42	33.47	-0.002
					Avg Abs error		0.016	
Secondary Tars								
Sec Tars - Run 55	650	Diebold	82.2	5.3	12.5	32.44	33.59	-0.035
Sec Tars - Run 56	730	Diebold	85.4	5.0	9.6	34.08	34.60	-0.015
Sec Tars - Run 59	825	Diebold	79.3	5.9	14.8	33.92	33.09	0.024
					Avg Abs error		0.025	

* Temperature of formation, degrees Celsius.

References for Appendix A

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- Bourgeois, J.P. and J. Dort. (1985). "Torrefied Wood from Temperate and Tropical Species." *BioEnergy* 84. H. Egneus and A. Ellegard, eds. Vol. III, p. 153. Elsevier Applied Science Publishers: London.

Appendix B

ADDITIONAL INFORMATION ON HEATS OF COMBUSTION OF BIOMASS MATERIALS

The main body of this publication contains several hundred listings of measured heats of combustion of biomass materials. Still, this is only a small sampling of the extant data. Listed below are several references to additional, often special, materials for which heats have been determined. Again, this is only a sampling and shows the diversity of sources of such published information. Also listed are names and addresses of several likely continuing sources of new information on heats of combustion of biomass materials.

A. References to Correlations and General Remarks about Biomass Fuel Values

1. Jenkins, B.M. and J.M. Ebeling (1985). "Correlation of Physical and Chemical Properties of Terrestrial Biomass with Conversion" in *Energy from Biomass and Wastes IX*. Jan. 1985. Lake Buena Vista, Florida. Institute of Gas Technology.

Develops correlations, based on experimental data for 62 samples of field crop residues, orchard prunings, vineyard prunings, food and fiber processing wastes, forest residues, and land-based crops. Correlation equations are derived to predict heating values (dry basis) from (a) ash content only; (b) ash and volatile matter from proximate analysis; (c) carbon only, from ultimate analysis; and (d) a combination of carbon, hydrogen, and oxygen content from ultimate analysis. (Several entries in this handbook come from this source.)

2. Graboski, M. and R. Bain (1981). In Reed, T.B., ed. *Biomass Gasification: Principles and Technology*, pp. 41-71. Noyes Data Corporation: Park Ridge, N.J.

Three correlations are compared for whole biomass and for chars: (a) The historical Dulong-Berthelot equation:

$$\text{HHV (Btu/lb)} = 146.76 C + 621 H - \frac{N+O-1}{8} + 39.96 S;$$

(b) the Tillman correlation (see below); and (c) the IGT correlations (see below).

3. Tillman, D.A. (1978). *Wood as an Energy Resource*. New York: Academic Press.

Uses the simple correlation: $\text{HHV (Btu/lb)} = 188 C - 718$

4. Institute of Gas Technology. (1978). *Coal Conversion Systems Technical Data Book*. DOE Contract EX-76-C-01-2286. Available NTIS, Springfield, VA.

$$\text{HHV(Btu/lb)} = 146.58 C + 568.78 H - 51.53 (O + N) - 6.58 A + 29.45 S$$

This correlation, which works well for both whole biomass and chars, is discussed and applied in Appendix A of this publication.

5. Ince, Peter J. (1979). *How to Estimate Recoverable Heat Energy in Wood or Bark Fuels*. USDA, Forest Service, Forest Products Laboratory, GTR FPL 29.

A reference source is provided for estimating the amount of heat energy that may be recovered using wood or bark fuel in a typical furnace, boiler, or hot air combustion heat recovery system. A survey of reported data on higher heating values for various species of wood and bark fuels is provided. A set of formulas of a type commonly used by combustion technologists is also provided for estimating combustion system heat losses and net recoverable heat energy per pound of fuel as-fired, based on fuel higher heating value, moisture content, and excess air, stack gas temperature, and ambient temperature assumptions.

6. Baker, A. (February 1983). "New Findings on Wood Fuel Values." *American Forest*, pp. 45-47, 51-52.

A general discussion of the heating value and burning characteristics of cord wood for home heating.

B. References to Extensive Collections of Heats of Combustion of Biomass Materials

1. Kryla, J.M. (February 1984). *Determination of Available Heat of Combustion Data for Canadian Woody Species*. ENFOR Project P-256. Forintek Canada Corp., Ottawa, Ontario, Canada.

A literature review was conducted to obtain reliable, experimentally determined calorific data for the various components of Canadian tree species. Information was obtained for 48 tree species native to Canada and is presented in tabular form. For indigenous species, the overall mean calorific value was found to be 21.18 MJ/kg for softwood materials (i.e. stem wood, stem bark, foliage, etc.) compared to 19.35 MJ/kg for hardwoods. Variation between reported values for a component of a particular species was found to be generally less than 5% but, in some instances, exceeded 10%. Calorific data are also presented for hybrid poplar and for several foreign species commonly planted in Canada.

2. Kuester, J.L. (1985). Arizona State University, Tempe, Arizona.

In a multi-year program for DOE, Kuester's laboratory has measured the heats of combustion and composition of more than 100 highly diverse forms of biomass (from almond shells to skunkbrush). Heating values (dry basis) vary from 7400 to 12,700 Btu lb⁻¹ for materials with ash ranging from 0.1% to 35.9%; protein from 0.1% to 25.3%; lignin from 7.8% to 28.8%; cellulose from 17.7% to 46.7%, and lipids from 5.1% to 14.9%. Results have been reported in *Conversion of Cellulosic Wastes to Liquid Fuels*. DOE Interim Report No. COD-2982-83. Contract No. DE-AC02-76CS40202, August 1982, and in a forthcoming Summary Report.

3. Fisher, J.A. (October 1984). Fiber Fuels Institute. *Standards Specifications Development. Phase I Activities, Final Report*. (Fiber Fuels Institute, 310 Cedar St., St. Paul, MN 55101)

This report contains as received and dry-basis heating values for about 50 samples of pelletized fuels from forest and agricultural residues, peat, and wastes. For many samples, ultimate and proximate analysis, ash analysis, and physical properties are also reported.

C. Selected Publications of Biomass Heats of Combustion

1. Kryla, J.M. (1985). "Calorific Value of Wood as Affected by Sample Particle Size and Radial Position in Stem." In *Fundamentals of Thermochemical Biomass Conversion*. Edited by R.P. Overend, T.A. Milne, and L.K. Mudge. Elsevier Applied Science Publishers, New York.
2. Chang, Y.P.E. and R.L. Mitchell. (1955). "Chemical Composition of Common North American Pulpwood Barks." *TAPPI* 38 (5) 315.
3. Leong, S.K. (1983). "Determination of Calorific Values and Energy Content in Hevea Trees." *J. Rubb. Res. Inst. Malaysia* 31 (1) 1.
4. Barnes, D.P. and S.A. Sinclair. (1983). "Gross Heat of Combustion of Living and Spruce Budworm-Killed Balsam Fir." *Wood and Fiber Science* 16 (4) 518.
5. Goering, C.E., A.W. Schwab, M.J. Daugherty, E.H. Pryde, and A.J. Heakin. "Fuel Properties of Eleven Vegetable Oils." *Transactions of the ASAE* 25 (6) 1472.
6. Hall, C.W. (1981). *Biomass as an Alternative Fuel*. Government Institutes, Inc.: Rockville, MD.
7. Howard, E.T. (1973). "Heat of Combustion of Various Southern Pine Materials." *Wood Science* 5 (3) 194.
8. Corder, S.E. (August 1973). *Wood and Bark as Fuel*. Research Bulletin 14. Forest Research Laboratory, Oregon State University, Corvallis.
9. Hough, W.A. (December 1969). *Caloric Value of Some Forest Fuels of the Southern United States*. USDA Forest Service Research Note SE-120. Southern Forest Experiment Station, Asheville, NC.
10. Kossuth, S.V., D.R. Roberts, J.B. Huffman, and S-C. Wang. (1982). "Resin Acid, Turpentine, and Caloric Content of Paraquat-Treated Slash Pine." *Can. J. For. Res.* 12 489.
11. Kossuth, S.V., D.R. Roberts, J.B. Huffman, and S-C. Wang. (1984). "Energy Value of Paraquat-Treated and Resin-Soaked Loblolly Pine." *Wood and Fiber* 16 (3) 398.
12. Rockwood, D.L. et al. (1983). *Energy and Chemicals from Woody Species in Florida*. ORNL/Sub/81-9050/1. University of Florida, Gainesville.
13. Bowersox, T.W., P.R. Blankenhorn, and W.K. Murphey. (1979). "Heat of Combustion, Ash Content, Nutrient Content and Chemical Content of Populus Hybrids." *Wood Science* 11 (4) 257.
14. Blankenhorn, P.R., R.C. Baldwin, W. Merrill, Jr., and S.P. Ottone. (1980). "Calorimetric Analysis of Fungal Degraded Wood." *Wood Science* 13 (1) 26.

15. Baileys, R.T. and P.R. Blankenhorn. (1982). "Calorific and Porosity Development in Carbonized Wood." *Wood Science* 15 (1) 19.

D. Sources of Information-Government Programs.

1. Ranney, J.W., Oak Ridge National Laboratory, P.O. Box X, Oak Ridge, TN 37830.

DOE Biofuels and Municipal Waste Technology Division Woody Species Program. Major activities in short-rotation forestry for energy.
2. Forest Products Laboratory, USDA, Forest Service, P.O. Box 5130, Madison, WI 53705.
3. Forintek Canada Corporation, 800 Chemin Montreal Road, Ottawa, Ontario, Canada K16 3Z5.
4. Northeastern Forest and Range Experiment Station, USDA, Forest Service, 705 Spear Street, P.O. Box 968, Burlington, VT 05402.
5. Intermountain Forest and Range Experiment Station, USDA, Forest Service, 507 25th St., Ogden, UT 84401.
6. North Central Forest and Range Experiment Station, USDA, Forest Service, 1992 Folwell Ave., St. Paul, MN 55108.
7. Northeastern Forest and Range Experiment Station, USDA, Forest Service, 370 Reed Rd., Broomall, PA 19008.
8. Pacific Northwest Forest and Range Experiment Station, USDA, Forest Service, 809 NE 6th Ave., Portland, OR 97232.
9. Pacific Southwest Forest and Range Experiment Station, USDA, Forest Service, 1960 Addison St. (P.O. Box 245), Berkeley, CA 94701.
10. Rocky Mountain Forest and Range Experiment Station, USDA, Forest Service, 240 W. Prospect Ave., Fort Collins, CO 80526.
11. Southeastern Forest and Range Experiment Station, USDA, Forest Service, 200 Weaver Blvd., Asheville, NC 28804.
12. Southern Forest and Range Experiment Station, USDA, Forest Service, 701 Loyola Ave., U.S. Postal Service Bldg., New Orleans, LA 70113.
13. Northern Regional Research Center (NRRC), Agricultural Research Service, USDA. 1815 N. University Street, Peoria, IL 61604.
14. Eastern Regional Research Center (ERRC), Agricultural Research Service, USDA. 600 E. Mermaid Ln., Philadelphia, PA 19118.
15. Western Regional Research Center (WRRRC), Agricultural Research Service, USDA. 800 Buchanan St., Berkeley, CA 94710.
16. Southern Regional Research Center (SRRRC), Agricultural Research Service, USDA. 1100 Robert E. Lee Blvd., P.O. Box 19687, New Orleans, LA 70179.

17. Beltsville Agricultural Research Center, Agricultural Research Service, USDA. Beltsville, MD 20705.
18. Russell (Richard B.) Agricultural Research Center, Agricultural Research Service, USDA. P.O. Box 5677, College Station Rd., Athens, GA 30613.

Appendix C

SYMBOLS, UNITS, CONVERSION FACTORS, ATOMIC WEIGHTS

Symbols for Thermodynamic Quantities

The symbols indicated in this Appendix are those adopted by the International Union of Pure and Applied Chemistry (IUPAC), 1969.

Symbols in parentheses are alternates, accepted but not recommended by IUPAC. Also indicated are other commonly used symbols and names of quantities not accepted by IUPAC.

NOTE: The Gibbs energy is frequently called free energy, Gibbs free energy, or Gibbs function. The commonly encountered term free energy in American work on thermodynamics almost invariably refers to Gibbs energy. This usage of the term free energy and the symbol F are being discouraged by the IUPAC because of confusion with the Helmholtz energy and the common European usage of F for the latter.

Primary Symbols

T	thermodynamic temperature (absolute temperature)
K	Kelvin temperature
t, θ	Celsius temperature
R	molar gas constant
k	Boltzmann constant
q, Q	heat
w, W	work
U, (E)	internal energy
H	enthalpy: $H = U + pV$
S	entropy
A	Helmholtz energy: $A = U - TS$
J	Massieu function: $J = -A/T$
G	Gibbs energy: $G = H - TS$

Y	Planck function: $Y = -G/T$
Z	compressibility factor: $Z = pV/nRT$
C_p	heat capacity
c_p	specific heat capacity (heat capacity divided by mass)
$\gamma, (\kappa)$	heat capacity ratio: C_p/C_v
μ	Joule-Thomson coefficient
λ, k	thermal conductivity
a	thermal diffusivity: $a = \lambda/\rho C_p$
h	coefficient of heat transfer
α	cubic expansion coefficient: $\alpha = (\partial V/\partial T)_p/V$
k	isothermal compressibility: $k = -(\partial V/\partial p)_T/V$
β	pressure coefficient: $\beta = (\partial p/\partial T)_V$

μ_B	chemical potential of substance B	M_r	relative molecular mass (also called "molecular weight")
λ_B	absolute activity of substance B: $\lambda_B = \exp(\mu_B/RT)$	L, N_A	Avogadro constant
$f, (p^*)$	fugacity	N	number of molecules
Π	osmotic pressure	$n, (v)$	amount of substance
I	ionic strength: $I = \frac{1}{2} \sum_i m_i z_i^2$ or $I = \frac{1}{2} \sum_i c_i z_i^2$	x_B, y_B	mole fraction of substance B: $x_B = n_B / \sum_i n_i$
a_B	activity, relative activity of substance B	w_B	mass fraction of substance B
f_B	activity coefficient, mole fraction basis	ϕ_B	volume fraction of substance B
γ_B	activity coefficient, molality basis	m_B	molality of solute substance B (amount of B divided by the mass of solvent)
y_B	activity coefficient, concentration basis	$c_B, [B]$	concentration of substance B (amount of B divided by the volume of the solution)
ϕ	osmotic coefficient	ρ_B	mass concentration of substance B (mass of B divided by the volume of the solution)
Selected Symbols for Other Quantities in Thermodynamics		ν_B	stoichiometric coefficient of substance B (negative for reactants, positive for products). (The general equation for a chemical reaction is $\sum_B \nu_B B = 0$, [Example: for the reaction $H_2O \rightarrow H_2 + \frac{1}{2} O_2$, $H_2 + \frac{1}{2} O_2 - H_2O = 0$])
A, S	area	τ	extent of reaction: ($d\tau = dn_B / \nu_B$)
V	volume	K	equilibrium constant
t	time	α	degree of dissociation
m	mass	z_B	charge number of an ion B (positive for cations, negative for anions)
ρ	density (mass divided by volume)		
p	pressure		
A_r	relative atomic mass (also called "atomic weight")		

**Units of Measurement - International System (SI)
SI - Base Units and Supplementary Units**

Quantity	Name of Unit	Symbol
length	meter	m
mass	kilogram	kg
time	second	s
temperature	kelvin	K
electric current	ampere	A
luminous intensity	candela	cd
amount of substance	mole	mol
plane angle	radian	rad
solid angle	steradian	sr

placed 1 meter apart in vacuum, would produce between these conductors a force equal to 2×10^{-7} newton per meter of length.

candela: The candela is the luminous intensity, in the perpendicular direction, of a surface of $1/600\,000$ square meter of a black body at the temperature of freezing platinum under a pressure of 101 325 newtons per square meter.

Definitions of the SI Base Units

meter: The meter is the length equal to 1 650 763.73 wavelengths in vacuum of the radiation corresponding to the transition between the levels $2p_{10}$ and $5d_5$ of the krypton-86 atom.

kilogram: The kilogram is equal to the mass of the international prototype of the kilogram.

second: The second is the duration of 9 192 631 770 periods of the radiation corresponding to the transition between the two hyperfine levels of the ground state of the cesium-133 atom.

kelvin: The kelvin is the fraction $1/273.16$ of the thermodynamic temperature of the triple point of water. The kelvin is used both for thermodynamic temperature and for thermodynamic temperature interval.

ampere: The ampere is that constant current which, if maintained in two straight parallel conductors of infinite length, of negligible cross section, and

mole: The mole is the amount of substance of a system which contains as many elementary entities as there are carbon atoms in 0.012 kilogram of carbon-12.

NOTE: The elementary entities must be specified and may be atoms, molecules, ions, electrons, other particles, or specified groups of such particles.

Prefixes

SI Symbol	Prefix Name	Multiplication Factor
T	tera	10^{12}
G	giga	10^9
M	mega	10^6
k	kilo	10^3
h	hecto	10^{+2}
da	deka	10^{+1}
d	deci	10^{-1}
c	centi	10^{-2}
m	milli	10^{-3}
μ	micro	10^{-6}
n	nano	10^{-9}
p	pico	10^{-12}
f	femto	10^{-15}
a	atto	10^{-18}

SI Derived Units (Partial Listing)

		<u>Symbol for SI unit</u>	<u>Definition of SI unit</u>	<u>Other Definitions</u>
force	newton	N	$\text{m} \cdot \text{kg} \cdot \text{s}^{-2}$	
pressure	pascal	Pa	$\text{m}^{-1} \cdot \text{kg} \cdot \text{s}^{-2}$	$\text{N} \cdot \text{m}^{-2}$
energy	joule	J	$\text{m}^2 \cdot \text{kg} \cdot \text{s}^{-2}$	$\text{N} \cdot \text{m}$
power	watt	W	$\text{m}^2 \cdot \text{kg} \cdot \text{s}^{-3}$	$\text{J} \cdot \text{s}^{-1}$
electric charge	coulomb	C	$\text{A} \cdot \text{s}$	
electric potential difference	volt	V	$\text{m}^2 \cdot \text{kg} \cdot \text{s}^{-3} \cdot \text{A}^{-1}$	$\text{W} \cdot \text{A}^{-1}$
electric resistance	ohm	Ω	$\text{m}^2 \cdot \text{kg} \cdot \text{s}^{-3} \cdot \text{A}^{-2}$	$\text{V} \cdot \text{A}^{-1}$
electric conductance	siemens	S	$\text{m}^{-2} \cdot \text{kg}^{-1} \cdot \text{s}^3 \cdot \text{A}^2$	$\text{A} \cdot \text{V}^{-1}$
electric capacitance	farad	F	$\text{m}^{-2} \cdot \text{kg}^{-1} \cdot \text{s}^4 \cdot \text{A}^2$	$\text{C} \cdot \text{V}^{-1}$
magnetic flux	weber	Wb	$\text{m}^2 \cdot \text{kg} \cdot \text{s}^{-2} \cdot \text{A}^{-1}$	$\text{V} \cdot \text{s}$
inductance	henry	H	$\text{m}^2 \cdot \text{kg} \cdot \text{s}^{-2} \cdot \text{A}^{-2}$	$\text{Wb} \cdot \text{A}^{-1}$
magnetic flux density	tesla	T	$\text{kg} \cdot \text{s}^{-2} \cdot \text{A}^{-1}$	$\text{Wb} \cdot \text{m}^{-2}$
luminous flux	lumen	lm	$\text{cd} \cdot \text{sr}$	
illumination	lux	lx	$\text{m}^{-2} \cdot \text{cd} \cdot \text{sr}$	
frequency	hertz	Hz	s^{-1}	

Other Units Exactly Defined in Terms of SI Units (Partial Listing)

<u>Quantity</u>	<u>Name</u>	<u>Symbol</u>	<u>Definition</u>
length	inch	in.	$2.54 \times 10^{-2} \text{ m}$
mass	pound (av.)	lb	0.453 592 37 kg
force	kilogram force	kgf	9.806 65 N
pressure	atmosphere	atm	$101\,325 \text{ N}\cdot\text{m}^{-2}$
pressure	torr	Torr	$(101\,325/760) \text{ N}\cdot\text{m}^{-2}$
pressure	millimeter of mercury	mmHg	$13.5951 \times 980.665 \times 10^{-2} \text{ N}\cdot\text{m}^{-2}$
energy	kilowatt-hour	kWh	$3.6 \times 10^6 \text{ J}$
energy	thermochemical calorie*	cal _{th}	4.184 J
energy	thermochemical Btu*	Btu _{th}	1054.35 J**
energy	IT calorie***	cal _{IT}	4.1868 J
energy	IT British thermal unit****	Btu _{IT}	1055.056 J*****
temperature (thermodynamic)	degree Rankine	°R	5/9 K*****
temperature	degree Celsius	°C	K*****
temperature	degree Fahrenheit	°F	5/9 K*****
volume	liter	l	10^{-3} m^3

* The thermochemical calorie and thermochemical Btu are used in this publication.

** The exact relationship is: $1 \text{ Btu}_{\text{th}} = (4.1840/1.8) \times 453.59237$.

*** IT refers to International Tables (International Steam Tables).

**** The exact relationship is: $1 \text{ Btu}_{\text{IT}} = (4.1868/1.8) \times 453.59237$

***** $[T(^{\circ}\text{R}) = 1.8T(\text{K})]$; $[T(^{\circ}\text{R}) = t(^{\circ}\text{F}) + 459.67]$; $[T(^{\circ}\text{R}) = 1.8t(^{\circ}\text{C}) + 491.67]$.

***** $[t(^{\circ}\text{C}) = T(\text{K}) - 273.15]$.

***** $[t(^{\circ}\text{F}) = 1.8t(^{\circ}\text{C}) + 32]$.

Conversion Factors

Subscript:	th - thermochemical units
Subscript:	IT - International Steam Table units
Abbreviations:	calorie - cal
	joule - J
	British thermal unit - Btu
	gram - g
	pound - lb
	Fahrenheit degree - °F
	Celsius degree - °C
	Kelvin - K

In the chemical literature, authors occasionally identify the calorie or British thermal unit as either th or IT, but rarely is the joule subscripted in any way. An absence of any subscripting to indicate the kind of energy unit is the more common occurrence.

Energy Conversion Factors

$$\begin{aligned}1 \text{ cal}_{\text{th}} &= 4.1840 \text{ J} \\1 \text{ cal}_{\text{IT}} &= 4.1868 \text{ J} \\1 \text{ Btu}_{\text{th}} &= 1054.35 \text{ J} \\1 \text{ Btu}_{\text{IT}} &= 1055.056 \text{ J}\end{aligned}$$

$$\begin{aligned}1 \text{ cal}_{\text{th}}/\text{g} &= 1.8 \text{ Btu}_{\text{th}}/\text{lb} \\1 \text{ cal}_{\text{IT}}/\text{g} &= 1.8 \text{ Btu}_{\text{IT}}/\text{lb} \\1 \text{ cal}_{\text{th}}/\text{g} &= 4.1840 \text{ J/g} \\1 \text{ cal}_{\text{IT}}/\text{g} &= 4.1868 \text{ J/g} \\1 \text{ cal}_{\text{th}}/\text{g} &= 1.798796 \text{ Btu}_{\text{IT}}/\text{lb} \\1 \text{ Btu}_{\text{th}}/\text{lb} &= 2.326000 \text{ J/g} \\1 \text{ Btu}_{\text{IT}}/\text{lb} &= 2.324444 \text{ J/g}\end{aligned}$$

$$\begin{aligned}1 \text{ Btu}_{\text{th}}/(\text{lb})(^{\circ}\text{F}) &= 1 \text{ cal}_{\text{th}}/(\text{g})(\text{K}) \\1 \text{ Btu}_{\text{IT}}/(\text{lb})(^{\circ}\text{F}) &= 1 \text{ cal}_{\text{IT}}/(\text{g})(\text{K})\end{aligned}$$

$$\begin{aligned}\text{Btu}_{\text{th}}/(\text{lb})(^{\circ}\text{F}) &= 4.1840 \text{ J}/(\text{g})(\text{K}) \\ \text{Btu}_{\text{IT}}/(\text{lb})(^{\circ}\text{F}) &= 4.1868 \text{ J}/(\text{g})(\text{K})\end{aligned}$$

Temperature Conversion Factors:

$1.8(^{\circ}\text{C}) + 32$	$= ^{\circ}\text{F}$
$273.15 + ^{\circ}\text{C}$	$= \text{K}$
$[(459.67) + ^{\circ}\text{F}]/1.8$	$= \text{K}$
$(1.8)\text{K}$	$= ^{\circ}\text{R}$
$(1.8)\text{K}$	$= 459.67 + ^{\circ}\text{F}$
$^{\circ}\text{R}$	$= 459.67 + ^{\circ}\text{F}$

Physical Constants*

Gas Constant, R	$82.0568 (26) \text{ cm}^3 \text{ atm mol}^{-1} \text{ K}^{-1}$
	$8.31441 (26) \text{ J mol}^{-1} \text{ K}^{-1}$
	$1.98719 (6) \text{ cal}_{\text{th}} \text{ mol}^{-1} \text{ K}^{-1}$
Molar Gas Volume, V_m	$0.02241383 (70) \text{ m}^3 \text{ mol}^{-1}$
(at $T_0 = 273.15 \text{ K}$ and $p_0 = 1 \text{ atm}$)	
$V_m = R T_0/p_0$	

*Physical Constants were taken from the International Council of Scientific Unions, CODATA Bulletin No. 11, Dec. 1973. The digits in parentheses following a numerical value represent the standard deviation of that value in terms of the final listed digits.

Atomic Weights of the Elements 1983

(Scaled to $A_r(^{12}\text{C})=12$)

N.E. Holden and R.L. Martin, *Pure & Appl. Chem.* 56, 653-674 (1984).

IUPAC Commission on Atomic Weights and Isotopic Abundances

The atomic weights of many elements are not invariant but depend on the origin and treatment of the material. The footnotes to this Table elaborate the types of variation to be expected for individual elements. The values of $A_r(E)$ given here apply to elements as they exist naturally on earth. When used with due regard to the footnotes they are considered reliable to ± 1 in the last digit, unless otherwise noted.

Alphabetical order in English

<u>Names</u>	<u>Symbol</u>	<u>Atomic Number</u>	<u>Atomic Weight</u>	<u>Footnotes</u>
Actinium*	Ac	89		A
Aluminium	Al	13	26.98154	
Americium*	Am	95		A
Antimony (Stibium)	Sb	51	121.75 \pm 3	
Argon	Ar	18	39.948	g r
Arsenic	As	33	74.9216	
Astatine*	At	85		A
Barium	Ba	56	137.33	g
Berkelium*	Bk	97		A
Beryllium	Be	4	9.01218	
Bismuth	Bi	83	208.9804	
Boron	B	5	10.811 \pm 5	m r
Bromine	Br	35	79.904	
Cadmium	Cd	48	112.41	g
Caesium	Cs	55	132.9054	
Calcium	Ca	20	40.078 \pm 4	g
Californium*	Cf	98		A
Carbon	C	6	12.011	r
Cerium	Ce	58	140.12	g
Chlorine	Cl	17	35.453	
Chromium	Cr	24	51.9961 \pm 6	
Cobalt	Co	27	58.9332	
Copper	Cu	29	63.546 \pm 3	r
Curium*	Cm	96		A
Dysprosium	Dy	66	162.50 \pm 3	g
Einsteinium*	Es	99		A
Element 104* (a)	Unq	104		A
Element 105* (b)	Unp	105		A
Element 106* (c)	Unh	106		A
Element 107* (d)	Uns	107		A
Erbium	Er	68	167.26 \pm 3	g
Europium	Eu	63	151.96	g
Fermium*	Fm	100		A
Fluorine	F	9	18.998403	

(a)-(d) Systematic names: (a) Unnilquadium; (b) Unnilpentium; (c) Unnilhexium; (d) Unnilseptium

Atomic Weights 1983 (cont'd)

<u>Names</u>	<u>Symbol</u>	<u>Atomic Number</u>	<u>Atomic Weight</u>	<u>Footnotes</u>	
Francium*	Fr	87			A
Gadolinium	Gd	64	157.25 ± 3	g	
Gallium	Ga	31	69.723 ± 4		
Germanium	Ge	32	72.59 ± 3		
Gold	An	79	196.9665		
Hafnium	Hf	72	178.49 ± 3		
Helium	He	2	4.002602 ± 2	g	r
Holmium	Ho	67	164.9304		
Hydrogen	H	1	1.00794 ± 7	g	m r
Indium	In	49	114.82	g	
Iodine	I	53	126.9045		
Iridium	Ir	77	192.22 ± 3		
Iron	Fe	26	55.847 ± 3		
Krypton	Kr	36	83.80	g	m
Lanthanum	La	57	138.9055 ± 3	g	
Lawrencium*	Lr	103			A
Lead	Pb	82	207.2	g	r
Lithium	Li	3	6.941 ± 2	g	m r
Lutetium	Lu	71	174.967	g	
Magnesium	Mg	12	24.305		
Manganese	Mn	25	54.9380		
Mendelevium*	Md	101			A
Mercury	Hg	80	200.59 ± 3		
Molybdenum	Mo	42	95.94		
Neodymium	Nd	60	144.24 ± 3	g	
Neon	Ne	10	20.179	g	m
Neptunium*	Np	93			A
Nickel	Ni	28	58.69		
Niobium	Nb	41	92.9064		
Nitrogen	N	7	14.0067	g	
Nobelium*	No	102			A
Osmium	Os	76	190.2	g	
Oxygen	O	8	15.9994 ± 3	g	r
Palladium	Pd	46	106.42	g	
Phosphorus	P	15	30.97376		
Platinum	Pt	78	195.08 ± 3		
Plutonium*	Pu	94			A
Polonium*	Po	84			A
Potassium (Kalium)	K	19	39.0983		
Praseodymium	Pr	59	140.9077		
Promethium*	Pm	61			A
Protactinium*	Pa	91			A
Radium*	Ra	88			A
Radon*	Rn	86			A
Rhenium	Re	75	186.207		
Rhodium	Rh	45	102.9055		
Rubidium	Rb	37	85.4678 ± 3	g	
Ruthenium	Ru	44	101.07 ± 2	g	
Samarium	Sm	62	150.36 ± 3	g	

Atomic Weights 1983 (cont'd)

<u>Names</u>	<u>Symbol</u>	<u>Atomic Number</u>	<u>Atomic Weight</u>	<u>Footnotes</u>
Scandium	Sc	21	44.95591 ± 1	
Selenium	Se	34	78.96 ± 3	
Silicon	Si	14	28.0855 ± 3	r
Silver	Ag	47	107.8682 ± 3	g
Sodium (Natrium)	Na	11	22.98977	
Strontium	Sr	38	87.62	g
Sulfur	S	16	32.066 ± 6	r
Tantalum	Ta	73	180.9479	
Technetium*	Tc	43		A
Tellurium	Te	52	127.60 ± 3	g
Terbium	Tb	65	158.9254	
Thallium	Tl	81	204.383	
Thorium*	Th	90	232.0381	g X
Thulium	Tm	69	168.9342	
Tin	Sn	50	118.710 ± 7	
Titanium	Ti	22	47.88 ± 3	
Tungsten (Wolfram)	W	74	183.85 ± 3	
Uranium*	U	92	238.0289	g m Y
Vanadium	V	23	50.9415	
Xenon	Xe	54	131.29 ± 3	g m
Ytterbium	Yb	70	173.04 ± 3	
Yttrium	Y	39	88.9059	g
Zinc	Zn	30	65.39 ± 2	
Zirconium	Zr	40	91.224 ± 2	g

- g geologically exceptional specimens are known in which the element has an isotopic composition outside the limits for normal material. The difference between the atomic weight of the element in such specimens and that given in the Table may exceed considerably the implied uncertainty.
- m modified isotopic compositions may be found in commercially available material because it has been subjected to an undisclosed or inadvertent isotopic separation. Substantial deviations in atomic weight of the element from that given in the Table can occur.
- r range in isotopic composition of normal terrestrial material prevents a more precise $\bar{A}_r(E)$ being given; tabulated $\underline{A}_r(E)$ value should be applicable to any normal material.
- A Radioactive element that lacks a characteristic terrestrial isotopic composition.
- X Thorium has a well defined (mononuclidic) composition in minerals with only rare exceptions. In certain places, however (most notably in ocean water), measurable quantities of Thorium 230 (Ionium) can be found.
- Y Uranium is the only element with no stable isotopes but which has a characteristic terrestrial composition of long-lived isotopes such that a meaningful atomic weight can be given for natural samples.
- * Element has no stable isotopes.

Name Index

	<u>Page</u>
2,5-METHYLOLMELAMINE, HARDENED	173
2,5-METHYLOLMELAMINE, UNHARDENED	173
80 NICKEL-20 CHROMIUM	34
α -BRASS	33
α -CELLULOSE, FROM LOBLOLLY PINE WOOD	67
ALDER, EUROPEAN BLACK	233
ALDER, RED; BARK	233
ALFALFA, SEED, STRAW	9
ALGAE	143
ALMOND HULLS	9
ALMOND, ORCHARD PRUNINGS	10
ALMOND SHELLS	10
ALMONDS	77
ALUMINUM	34
ALUMINUM 2024-T4	35
ALUMINUM 7075-T6	35
AMATOL	305
ARALDITE	167
ARCHANGEL (WOOD BETONY OR BLIND NETTLE)	143
ASH	233
ASH, GREEN	234
ASH, WHITE	235
ASPEN, QUAKING	236
ASPEN, QUAKING; BARK	236
ASPEN, QUAKING; FOLIAGE	236
ASPEN, TREMBLING	237
ASPHALT	103
BABASSU HUSKS	11
BAKELITE VARNISH, FORMITE VIII05	167
BARLEY OIL	213
BARLEY STRAW	11
BARNACLE	55
BEAN STRAW	12
BEANS, GREEN	77
BEANS, NAVY, WHITE, DRY	77
BEECH	237, 238
BEEF SUET, COMMERCIAL	78
BEEFWOOD (SHE-OAK)	238
BEEBLE	55
BEETS	78
BENTONITE, PEMBINA	127
BENTONITE, WYOMING	127
BIG SAGEBRUSH	143
BIG SAGEBRUSH, FOLIAGE	144
BIG SAGEBRUSH, STEMS	144
BIRCH	239
BIRCH, PAPER	239
BIRCH, PAPER; BARK	240
BIRCH, YELLOW	240
BIRCH, YELLOW; BARK	241

Name Index

	<u>Page</u>
BIVALVE55
BLACK WALNUT, ORCHARD PRUNINGS12
BLACKGUM241
BLACKGUM, BARK242
BOVINE CHYMOTRYPSINOGEN A191
BOXELDER	242, 243
BRACHIOPOD55
BRACKEN FERN, FRONDS144
BROAD-LEAVED STITCHWORT (WOOD STARWORT)145
BROWN PAPER137
BULBIFEROUS TOOTHWORT (TOOTH-CRESS)145
BUTADIENE-STYRENE COPOLYMER, GL-622168
BUTADIENE-STYRENE COPOLYMER, X-454168
BUTADIENE-STYRENE COPOLYMER, X-478169
BUTENE-1-POLYSULFONE169
BUTTERFAT, SUMMER79
BUTTERFAT, WINTER79
CABBAGE80
CABBAGE WOOD243
CABERNET SAUVIGNON GRAPES, VINEYARD PRUNINGS13
CADMIUM36
CARDINAL GRAPES, VINEYARD PRUNINGS13
CARROTS80
CASEIN, MILK191
CASTOR OIL213
CATTAILS145
CATTLE56
CAULIFLOWER80
CEDAR, RED244
CELLULOID170
CELLULOSE	67, 68
CELLULOSE DIACETATE68
CELLULOSE, HOLOCELLULOSE; FROM LOBLOLLY PINE WOOD68
CELLULOSE NITRATE305
CELLULOSE TRIACETATE68
CEMENT HYDRATES128
CHAMISE, FOLIAGE244
CHAPARRAL245
CHARCOAL, WOOD69
CHEATGRASS, CURED146
CHENIN BLANC GRAPES, VINEYARD PRUNINGS14
CHERRY245
CHERRY, BLACK246
CHERRY, CORNELIAN246
CHESTNUT247
CHITON56
CHROMIUM37
CHYMOTRYPSIN191
CILIATE56
cis-BUTENE-2-POLYSULFONE169

Name Index

	<u>Page</u>
CITRUS FRUIT, RINDS AND SEEDS	81
CLADOCERA	56
CLAY, CHINA	128
CLAY, HALLOYSITE (DJEBEL DEBAR)	129
CLAY, K. PLASTIC KAOLIN	129
CLAY, MOROCCAN NO. 4	129
CLAY, NEWTON ABBOT BALL	130
CLOVERROOT (HERB BENNET)	146
COAL, ANTHRACITE	103
COAL, BITUMINOUS	104
COAL, BITUMINOUS (HIGH GRADE)	104
COAL, BITUMINOUS (LOW GRADE)	104
COAL, BITUMINOUS (MEDIUM GRADE)	105
COAL, CANNEL	105
COAL, SEMI-ANTHRACITE	105
COAL, SEMI-BITUMINOUS	106
COAL, SUB-BITUMINOUS	106
COCKS-FOOT GRASS	146
COCOA BUTTER	81
COCOA HULLS	14
COCOBOLA NEGRA	247
COCONUT	81
COCONUT FIBER, DUST	15
COCONUT OIL	214
COKE	106, 107
COKE BREEZE	107
COLLAGEN	192
COLTSFOOT	147
CONSTANTAN	38
COPEPOD	57
COPPER	38
CORAL BRANCH TIPS	306
CORAL BRANCHES	306
CORN (MAIZE), GREEN	82
CORN COBS	15
CORN OIL	215
CORN OIL (MAIZE)	215
CORN STOVER	16
CORRUGATED BOX	137
COTTON GIN TRASH	16
COTTON STALKS	17
COTTON (THREAD)	69
COTTONSEED OIL	215
COTTONSEED OIL, HYDROGENATED	216
COTTONSEED OIL, REFINED	216
COTTONWOOD, MISSOURI	248
COTTONWOOD, NEBRASKA	248
COWPEAS	82
COWSLIP LUNGWORT	147
CRAMBE OIL	217

Name Index

	<u>Page</u>
CUCUMBERS	.82
DBX	.306
DELRIN	.170
DEXTRIN	.69
DICYANDIAMIDE (TECHNICAL)	.170
DISCARDED AUTOMOBILES TIRES	.207
DOG VIOLET	.148
DOGWOOD, BLOOD-TWIG	.249
DOWTHERM A	.307
DURETHAN U20	.171
EGG ALBUMIN	.83
EGG YOLK	.83
ELM, AMERICAN; BARK	.249
ELM, WHITE	.250
ENCHANTER'S NIGHTSHADE	.148
ENGLISH WALNUT, ORCHARD PRUNINGS	.17
EPILOX EG1, HARDENED	.171
EPILOX EG1, UNHARDENED	.171
EUCALYPTUS CAMALDULENSIS	.250
EUCALYPTUS GLOBULUS	.251
EUCALYPTUS GRANDIS	.251
EXCELSIOR, DEAD WOOD	.252
FAT, ANIMAL	.83
FAT, BARLEY	.83
FAT, BEEF	.84
FAT, BUTTER	.84
FAT, FRIED	.84
FAT, LARD	84, 85
FAT, MUTTON	.85
FAT, OAT	.85
FAT, PORK	.85
FAT, RYE	.86
FAT, WHEAT	.86
FAT, WOOL	.307
FILTER PAPER WHATMAN	.69
FIR	.252
FIR, BALSAM; BARK	.252
FIR, BALSAM; NEEDLES	.252
FIR, DOUGLAS	.253
FIR, DOUGLAS; BARK	.253
FIR, DOUGLAS; FOLIAGE	.254
FIR, DOUGLAS; LUMBER	.254
FIR, DOUGLAS; ROTTEN WOOD	.254
FIR, DOUGLAS; STEMS	.255
FIR, GRAND	.255
FIR, WHITE	255, 256
FIR, WHITE; ROTTEN WOOD	.256
FLATWORM	.57
FLATWORM, TERRESTRIAL	.57
FLOUR, SOY BEAN	.86

Name Index

	<u>Page</u>
FLOUR, WHEAT87
FLY, CADDIS58
FOOD CARTONS137
FOOD WASTES, VEGETABLE87
FOURWING SALTBUSH148
FUEL, AVIATION	108, 109
FUEL, COED-1 FMC WESTERN KENTUCKY COAL DERIVED109
FUEL, COED-2 UTAH COAL DERIVED109
FUEL, COED-3 WESTERN KENTUCKY COAL DERIVED110
FUEL, COED-4 UTAH COAL DERIVED110
FUEL, COED-5 WESTERN KENTUCKY COAL DERIVED110
FUEL, GASOLINE115
FUEL, JP-9 RAMJET111
FUEL, PARAHO OIL SHALE DERIVED111
FUEL, PETROLEUM-A DERIVED111
FUEL, RJ-4 RAMJET112
FUEL, RJ-4-I RAMJET112
FUEL, RJ-6 RAMJET113
FUEL, TAR SANDS (ALTERNATIVE JET FUEL)114
GALLBERRY, FOLIAGE149
GAS, NATURAL114
GASOLINE115
GELATIN88
GELATINE192
GERMANDER SPEEDWELL (ANGEL'S-EYE)149
GEWURZTRAMINER GRAPES, VINEYARD PRUNINGS18
GLABER CRESS149
GLASS, PYREX	130, 131
GLASS, SODA-LIME131
GLASS, VYCOR132
GLIADIN193
GLUTEN193
GLUTENIN194
GLYCOGEN70
GLYPTAL172
GR-S RUBBER207
GRAPE POMACE18
GRAPES, THOMPSON SEEDLESS88
GRAPHITE, ARTIFICIAL307
GRAPHITE, BUCKINGHAM307
GRAPHITE, CEYLON307
GRAPHITE, PYROLYTIC308
GRAPHITE, TICONDEROGA308
GRASS, LAWN CLIPPINGS150
GREASE, APIEZON N115
GREASE, APIEZON P116
GREASE, APIEZON R117
GREASE, APIEZON S117
GREASE, APIEZON T117
GREASEWOOD150

Name Index

	<u>Page</u>
GROATS, SUN IX89
GROUND NUT SEED OIL217
GUPPIE58
HASTELLOY X39
HEMICELLULOSE70
HEMLOCK, EASTERN; BARK257
HEMLOCK, WESTERN257
HERB ROBERT (RED ROBIN)150
HERBS, ALPINE TUNDRA151
HERRING OIL89
HEVEA (RUBBER TREE)258
HEVEA (RUBBER TREE), CLONE RRIM 527258
HEVEA (RUBBER TREE), CLONE RRIM 707259
HICKORY	259, 260
HIGH OLEIC SAFFLOWER OIL217
HOMINY90
HONEYDEW MELON90
HORNBEAM260
HYDRA, GREEN58
IDAHO FESCUE, CURED151
INCONEL, ANNEALED40
INCONEL "X"40
INSULIN, BOVINE ZINC194
INULIN70
INULIN TRIACETATE70
IRISH SHAMROCK (EUROPEAN WOOD SORREL)151
IRON40
IRON, CAST41
iso-BUTENE POLYSULFONE (2-methylpropene polysulfone)170
JUNIPER, UTAH; BARK260
JUNIPER, UTAH; FOLIAGE261
JUNIPER, UTAH; STEMS261
JUNK MAIL138
JUPITER'S-DISTAFF152
KEROSINE118
LADY FERN152
LARCH261
LARCH, BARK262
LARCH, LUMBER262
LARCH, WESTERN; BARK262
LARD, AMERICAN COMMERCIAL90
LARD, GERMAN COMMERCIAL91
LEAD42
LEATHER308
LEATHER, SHOE309
LEAVES, TREE; RIPE HARDWOOD MIXTURE263
LETTUCE MURALIS152
LIGNIN71
LIGNIN, HARDWOOD71
LIGNIN, LOBLOLLY PINE WOOD71

Name Index

	<u>Page</u>
LIGNIN, SOFTWOOD	72
LIGNITE	118
LINSEED OIL	218
LINSEED OIL, UNREFINED	219
LITTER FALL	263
LOCUST, BLACK	264
LUCITE	172
MACADAMIA SHELLS	19
MADRONE	264
MAGAZINE	138
MAI CHAMPAH	265
MALE FERN	153
MALTING BARLEY	91
MANURE, PIG	72
MANZANITA	265
MANZANITA, GREENLEAF; FOLIAGE	265
MAPLE	266
MAPLE, HEDGE	266
MAPLE, RED	267, 268
MAPLE, SILVER	269
MAPLE, SUGAR	269, 270
MAPLE, SUGAR; BARK	270
MAPLE, TATARIAN	271
MARGARINE, TABLE	92
MARGARINE, COMMERCIAL	92
MEADOW-RUE ISOPYRUM	153
MEAL, CORN (MAIZE)	93
MEAT, COOKED SCRAPS	93
MELIC GRASS	153
MELINEX FILM	173
MERCURIALIS PERENNIS	154
MERCURY	43
MERLOT GRAPES, VINEYARD PRUNINGS	19
MITE	58
MONEL	44
MONEL "K"	44
MOSESSES, ALPINE TUNDRA	154
MOUNTAIN RUSH	155
MYLAR FILM	173
NAPHTHA, ALASKA	118
NAPHTHA, AROMATIC	119
NAPHTHA, HIGH BOILING	119
NAPHTHA, JET	119
NAPHTHA, LOW BOILING	119
NEAT'S FOOT OIL, REFINED	310
NEWSPRINT	138
NICKEL	44
NORYL RESIN III	174
NYLON-6	175
NYLON-6,6	176

Name Index

	<u>Page</u>
GROATS, SUN IX	89
GROUND NUT SEED OIL	217
GUPPIE	58
HASTELLOY X	39
HEMICELLULOSE	70
HEMLOCK, EASTERN; BARK	257
HEMLOCK, WESTERN	257
HERB ROBERT (RED ROBIN)	150
HERBS, ALPINE TUNDRA	151
HERRING OIL	89
HEVEA (RUBBER TREE)	258
HEVEA (RUBBER TREE), CLONE RRIM 527	258
HEVEA (RUBBER TREE), CLONE RRIM 707	259
HICKORY	259, 260
HIGH OLEIC SAFFLOWER OIL	217
HOMINY	90
HONEYDEW MELON	90
HORNBEAM	260
HYDRA, GREEN	58
IDAHO FESCUE, CURED	151
INCONEL, ANNEALED	40
INCONEL "X"	40
INSULIN, BOVINE ZINC	194
INULIN	70
INULIN TRIACETATE	70
IRISH SHAMROCK (EUROPEAN WOOD SORREL)	151
IRON	40
IRON, CAST	41
iso-BUTENE POLYSULFONE (2-methylpropene polysulfone)	170
JUNIPER, UTAH; BARK	260
JUNIPER, UTAH; FOLIAGE	261
JUNIPER, UTAH; STEMS	261
JUNK MAIL	138
JUPITER'S-DISTAFF	152
KEROSINE	118
LADY FERN	152
LARCH	261
LARCH, BARK	262
LARCH, LUMBER	262
LARCH, WESTERN; BARK	262
LARD, AMERICAN COMMERCIAL	90
LARD, GERMAN COMMERCIAL	91
LEAD	42
LEATHER	308
LEATHER, SHOE	309
LEAVES, TREE; RIPE HARDWOOD MIXTURE	263
LETTUCE MURALIS	152
LIGNIN	71
LIGNIN, HARDWOOD	71
LIGNIN, LOBLOLLY PINE WOOD	71

Name Index

	<u>Page</u>
PINE, LODGEPOLE; FOLIAGE	283
PINE, LODGEPOLE; NEEDLES	283
PINE, LONGLEAF	283
PINE, PINYON; FOLIAGE	283
PINE, PINYON; STEMS	284
PINE, PONDEROSA	284, 285
PINE, PONDEROSA; AZ 78 FOLIAGE	285
PINE, PONDEROSA; BARK	286
PINE, PONDEROSA; CA 77 FOLIAGE	286
PINE, PONDEROSA; DEAD FOLIAGE	286
PINE, PONDEROSA; HEARTWOOD LUMBER	287
PINE, PONDEROSA; MT 77 FOLIAGE	287
PINE, PONDEROSA; MT 78 FOLIAGE	287
PINE, SLASH; BARK	288
PINE, SLASH; FOLIAGE	288
PINE, SUGAR	288
PINE, WESTERN WHITE; DEAD FOLIAGE	289
PINE, WHITE	289
PINE, WHITE; SAWDUST	289
PINOT NOIR GRAPES, VINEYARD PRUNINGS	21
PISTACHIO SHELLS	22
PLANTS, FLOWER GARDEN	155
PLANTS, VASCULAR AQUATIC	156
PLASTIC COATED PAPER	139
POLY(OXY-2-METHYL-1,4-CYCLOHEXYLENE)	183
POLY-1,1-DICHLOROETHYLENE	181
POLY-1,1-DIFLUOROETHYLENE	181
POLY-1-BUTENE	180
POLY-2,6-DIMETHYLPHENYLENE ETHER	181
POLY-4,4'-DIOXYDIPHENYL-2,2-PROPANE CARBONATE	181
POLY-ε-ENANTHOLACTAM	182
POLY-α-METHYL STYRENE	183
POLY-iso-BUTENE	180
POLY-N-ETHYL-N-METHYL PROPIONAMIDE	195
POLYACENAPHTHYLENE	179
POLYALLYLPHTHALATE	179
POLYBUTADIENE 41°F	179
POLYBUTADIENE 122°F	180
POLYETHYLENE	182, 183
POLYPROPYLENE	184
POLYSTYRENE	184
POLYUREA (POLYHARNSTOFF)	184
POLYVINYL CHLORIDE	185
POLYVINYL NITRATE	311
POND MURREL, TAIL	59
POND MURREL, TRUNK	59
POPLAR	289, 290
POPLAR, YELLOW	290
POPPY SEED OIL, BLEACHED	223
POPULUS HYBRIDS	291

Name Index

	<u>Page</u>
NYLON-6,10	178
OAK	272
OAK, BLACK; DEAD FOLIAGE	272
OAK, DURMAST	273
OAK, NORTHERN RED	274
OAK, NORTHERN RED; BARK	274
OAK, RED	275
OAK, TAN	276
OAK, TAN; BARK	276
OAK, TAN; SAPWOOD	276
OAK, TURKEY	277
OAK, WATER	278, 279
OAK, WHITE	279, 280
OAK, WHITE; BARK	280
OAT OIL	219
OATS	93
OATS, SUN II	94
OIL, CRUDE	120
OIL, FUEL	120
OIL, GAS	121
OIL, PARAFFIN	121
OIL, RAW SHALE	122
OIL, SPENT SHALE	122
OLIVE OIL	219
OLIVE OIL, ITALIAN	220
OLIVE PITS	20
PALM OIL, HARDENED	220
PALM OIL, UNREFINED	221
PALM-KERNEL OIL	221
PB-RDX	310
PEACH PITS	20
PEANUT BUTTER, HARDENED	94
PEANUT HULLS	21
PEANUT OIL	222
PEANUT OIL, UNREFINED	222
PEANUTS	95
PEARS, BARTLETT	95
PEAT	123
PECANS	95
PENTOLITE	310
PERILLA OIL	223
PHENOL-FORMALDEHYDE RESIN, HARDENED (EDELKUNSTHARZ B)	178
PHENOL-FORMALDEHYDE RESIN, UNHARDENED	179
PHENYLALANINE POLYMER	194
PINE, EASTERN WHITE	281
PINE, JACK; BARK	281
PINE LITTER, DUFF	282
PINE, LOBLOLLY	282
PINE, LOBLOLLY; EXTRACTIVES	282
PINE, LODGEPOLE; BARK	282

Name Index

	<u>Page</u>
SNAIL	62
SNAIL, AQUATIC	63
SOUTHERN HARDWOOD, SAWMILL RESIDUE, FRESH	294
SOUTHERN HARDWOOD, SAWMILL RESIDUE, PILED	294
SOW-TEAT STRAWBERRY (WOODLAND STRAWBERRY)	158
SOYBEAN OIL	227
SOYBEAN OIL, REFINED	227
SPITBUG	63
SPREADING RABBITBRUSH	159
SPRUCE PINE	295
SPRUCE PINE, BARK	295
SPRUCE, BALSAM	294
SPRUCE, BLACK; BARK	294
SPRUCE, ENGELMANN; BARK	295
SPRUCE, NORWAY	295
SPRUCE, RED	296
SPURGE ALMOND	159
STARCH	72
STARCH TRIACETATE	72
STARFISH	63
STEEL, NPL NO. 19	46
STEEL, SAE-1010	45
STEEL, STAINLESS	46
STEEL, STAINLESS 347	47
STEEL, STAINLESS 446	47
STINGING NETTLE	159
SUDAN GRASS	160
SUGARCANE BAGASSE	25, 26
SULFITE LIQUOR, SPENT	73
SUNFLOWER OIL	228
SUNFLOWER OIL, UNREFINED	229
SUNFLOWER, SEED OIL	228
SWEET WOODRUFF	160
SWEETGUM	296, 297
SWEETGUM, BARK	297
SYCAMORE	298
SYCAMORE, AMERICAN	298
SYCAMORE, AMERICAN; BARK	299
TALL OXEYE	160
TANNIN EXTRACT, CHESTNUT	73
TANNIN EXTRACT, QUEBRACHO	73
TEFLON	186
THOMPSON SEEDLESS GRAPES, VINEYARD PRUNINGS	27
TIN	48
TIRE	209
TITANIUM, Ti-75A	49
TITANIUM, Ti-150A	49
TOKAY GRAPES, VINEYARD PRUNINGS	27
TOUCH-ME-NOT	161
trans-BUTENE-2-POLYSULFONE	169

Name Index

	<u>Page</u>
PORCELAIN	132
POTATO, WHITE	96
PROPARGYL AZIDE POLYMER	185
PROPELLANT, BAKELITE RESIN BINDER FUEL	311
PROPELLANT, OS/AP	311
PRUNE PITS	22
PURIFIED NATURAL RUBBER HYDROCARBON	208
RAPE OIL, REFINED	224
RAPESEED OIL	224, 225
REDBUD	291
REDWOOD	292
REDWOOD, BARK	292
REDWOOD, HEARTWOOD	292
REDWOOD, MILL WASTES	293
REDWOOD, SAPWOOD	293
REFUSE	201
REFUSE, MUNICIPAL	203, 204
REFUSE-DERIVED FUEL	201, 202, 203
RESIN, ABS I	185
RIBIER GRAPES, VINEYARD PRUNINGS	23
RICE	96
RICE, FULLY FINISHED (ITALIAN ORIGIN)	96
RICE HULLS	23
RICE, ROUGH (ITALIAN ORIGIN)	97
RICE, SHELLD (ITALIAN ORIGIN)	97
RICE STRAW (COLLECTED AFTER HARVEST)	24
RICE STRAW, WEATHERED (COLLECTED 1/2 YEAR AFTER HARVEST)	24
RICE, SWAMP PADDY	98
RILSAN	186
RUBBER	208
RUBBER RABBITBRUSH	156
RUBBER-SULFUR COMPOUNDS	209
RYE OIL	225
SAFFLOWER OIL	225
SAFFLOWER STRAW	25
SANTOWAX R	311
SARCOSINE POLYMER	195
SAW-PALMETTO, FRONDS	156
SEDGE GRASS	157
SEQUOIA, GIANT	293
SESAME OIL	226
SHEEP, BLOOD	60
SHEEP, CARCASS	60
SHEEP, HIDE	61
SHEEP, INGESTA-FREE BODY	61
SHEEP, VISCERA	62
SHRIMP, BRINE	62
SHRUBS, DECIDUOUS; ALPINE TUNDRA	157
SHRUBS, EVERGREEN; ALPINE TUNDRA	158
SHRUBS, EVERGREEN; CUTTINGS	158