## POWDER RIVER BASIN COALBED METHANE DEVELOPMENT AND PRODUCED WATER MANAGEMENT STUDY



## **U.S. Department of Energy**



Office of Fossil Energy and National Energy Technology Laboratory Strategic Center for Natural Gas



November 2002

#### DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference therein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed therein do not necessarily state or reflect those of the United States Government or any agency thereof.

## **Powder River Basin Coalbed Methane Development and Produced Water Management Study**

**Prepared for:** 

U.S. Department of Energy Office of Fossil Energy and National Energy Technology Laboratory

**Prepared by:** 

**Advanced Resources International, Inc.** 

November 2002



## **DEPARTMENT OF ENERGY**

## FOREWORD

The President's National Energy Policy Plan estimates that over the next 20 years annual natural gas consumption will increase by 50 percent, from approximately 20 to 31 trillion cubic feet (Tcf). To meet this growing demand for natural gas, the Plan concludes that we will have to fully develop, in an environmentally sensitive manner, our nation's economically recoverable natural gas resources.

Natural gas produced from coal, commonly referred to as coalbed methane (CBM), constitutes 7.5 percent of total annual domestic natural gas production. In 2000, about 1.4 Tcf of coalbed methane was produced in the United States. The Powder River Basin, located in northeastern Wyoming and southeastern Montana, is the nation's fastest growing source of coalbed methane.

In the next 10 years, natural gas development in the Powder River Basin is expected to increase dramatically. As many as 39,000 additional wells will be drilled with 23,900 of these being on Federal lands. Because of this increased drilling activity, the Department of the Interior, Bureau of Land Management (BLM), must prepare Environmental Impact Statements (EIS's) evaluating the environmental impacts associated with drilling activities in the region. BLM issued draft Wyoming and Montana EIS's for comment in January and February, 2002, and expects to have both EIS's completed in February, 2003. In a related matter, the U.S. Environmental Protection Agency (EPA Region 8) is conducting a study of Best Professional Judgment (BPJ) general permit requirements for produced water on Native American lands in the region. This study will be completed in December, 2002.

The BLM EIS's and the EPA Region 8 BPJ study (and possible follow-on actions) will have a significant impact on the development of natural gas resources in the Powder River Basin. Recognizing this, in April, 2002, the U.S. Department of Energy (DOE), Office of Fossil Energy, through its National Energy Technology Laboratory, contracted with Advanced Resources International, Inc. to analyze the basin's geology and underlying coalbed methane resources, estimate water production rates associated with coalbed methane development, and evaluate the costs, feasibility, and impacts of coalbed methane produced water disposal practices. BLM and EPA cooperated with DOE on this study, realizing that this information would be useful to them in their efforts to develop environmental policies and procedures that promote Powder River Basin coalbed methane development while protecting the basin's unique ecosystem.

The present study, Powder River Basin Coalbed Methane Development and Produced Water Management Study, projects that the Powder River Basin contains a considerably larger volume of coalbed methane resources than previously estimated. There is currently a range of resource

estimates for the Powder River Basin from Federal, State, and industry organizations, varying by almost a factor of five. For example, DOE, BLM, and the U.S. Geological Survey all have current estimates for the amount of recoverable coalbed methane in this basin ranging from 8 Tcf to 39 Tcf. The differences stem from employing alternative methodologies, different geologic models, and different assumptions. When calculating a quantity as uncertain as undiscovered recoverable natural gas resources, such differences are to be expected and even encouraged, as they lead to further scientific investigation and interagency cooperation that increases the state of knowledge about our Nation's energy resources. In addition, each source develops its estimates for different purposes, and this also leads to the use of different approaches. Federal agencies are working together to refine our understanding of the coal bed methane resources of this Basin, and we expect, therefore, that estimates of recoverable natural gas resources in the Powder River Basin will continue to change over time.

In addition, the study projects that recovering these resources will require fewer wells than those projected in the BLM EIS's. The study also reveals that the amount of water associated with coalbed methane production in the Powder River Basin is substantially less than previously estimated. Nevertheless, the study concludes that development of the basin's coalbed methane resources will be significantly impacted by the costs and economic feasibility of produced water management practices and requirements. The study outlines alternative water disposal options, clearly identifies their costs, and makes a compelling argument that requiring more costly methods of produced water management will substantially reduce the amount of economically recoverable Powder River Basin coalbed methane.

Review comments on the study by representatives of BLM, EPA, and State officials from Wyoming and Montana have been overwhelmingly positive. The reviewers expressed their appreciation for DOE support and indicated data contained in the study will be of great value in their efforts to promote responsible, environmentally sound development of the Powder River Basin's coalbed methane resources.

The present study is one of a number of studies sponsored by DOE that examine the issues surrounding coalbed methane development. These include development of best management practices, electronic mapping of environmental and well data, a CBM primer for the public, a handbook for the development and review of environmental documents required for CBM projects, analysis of the options for beneficial use of CBM produced water, and research on technologies for produced water treatment. DOE believes that CBM produced water represents a valuable resource in the Powder River Basin and elsewhere in the arid Western U.S., and that it can be, and is, managed with no significant adverse environmental impacts. Currently, this water is used for livestock and wildlife watering, irrigation, to maintain stream flows, and in municipal aquifer recharge. All discharges of this water are permitted and meet State and Federal standards. Additional beneficial uses are being studied.

For more information about DOE oil and natural gas environmental projects visit the Office of Fossil Energy website at *www.fe.doe.gov/oil\_gas/environment* or contact Peter Lagiovane at: 202-586-8116.

#### ACKNOWLEDGMENTS

This study was conducted by Advanced Resources International, Inc. (ARI), located in Arlington, Virginia, for the U.S. Department of Energy (DOE) Office of Fossil Energy, located in Washington, D.C., and the National Energy Technology Laboratory (NETL), with locations in Morgantown, West Virginia, Pittsburgh, Pennsylvania, and Tulsa, Oklahoma. The principal investigator at ARI was Vello Kuuskraa. Other ARI staff contributing to this effort included A. David Decker, Brian T. Kuck, Greg J. Bank and Joyce A. Frank. The contractor's effort was overseen by NETL's Strategic Center for Natural Gas. The Center's mission includes strategic planning and policy support, focused on creating a balanced portfolio of DOE natural gas research and development initiatives and policy analyses to support more informed government decision making. The Strategic Center for Natural Gas project manager for this analysis was John Duda. Other DOE staff contributing to the effort included H. William Hochheiser and Peter Lagiovane of the Office of Fossil Energy, Office of Natural Gas and Petroleum Technology, and William Lawson and John Ford of the National Petroleum Technology Office. The Department extends its appreciation to those companies operating in the Powder River Basin, and staff of the Department of the Interior, Environmental Protection Agency, and Wyoming and Montana State agencies who provided the technical input and assistance that enabled DOE to improve the scope and quality of the analysis.

## **TECHNICAL PREFACE**

Coalbed methane resources throughout the entire Powder River Basin were reviewed in this analysis. The study was conducted at the township level, and as with all assessments conducted at such a broad level, readers must recognize and understand the limitations and appropriate use of the results. Raw and derived data provided in this report will not generally apply to any specific location. The coal geology in the basin is complex, which makes correlation with individual seams difficult at times.

Although more than 12,000 wells have been drilled to date, large areas of the Powder River Basin remain relatively undeveloped. The lack of data obviously introduces uncertainty and increases variability. Proxies and analogs were used in the analysis out of necessity, though these were always based on sound reasoning. Future development in the basin will make new data and interpretations available, which will lead to a more complete description of the coals and their fluid flow properties, and refined estimates of natural gas and water production rates and cumulative recoveries.

Throughout the course of the study, critical data assumptions and relationships regarding gas content, methane adsorption isotherms, and reservoir pressure were the topics of much discussion with reviewers. A summary of these discussion topics is provided as an appendix. Water influx was not modeled although it is acknowledged that this phenomenon may occur in some settings.

As with any resource assessment, technical and economic results are the product of the assumptions and methodology used. In this study, key assumptions as well as cost and price data, and economic parameters are presented to fully inform readers. Note that many quantities shown in various tables have been subject to rounding; therefore, aggregation of basic and intermediate quantities may differ from the values shown.

## TABLE OF CONTENTS

Page

1.0	STUD	Y PURPOSE, APPROACH AND FINDINGS	1-1
	1.1 1.2	Purpose of Study	l-l 1 1
	1.2	Partitioning the Powder River Basin	1-1
	1.4	Study Approach	1-9
	1.5	Summary of Findings and Impacts	1-13
2.0	GEOL	OGIC SETTING AND RESERVOIR PROPERTIES	2-1
	2.1	Basin Area	2-1
	2.2	Basin Structure	2-2
	2.3	Basin Stratigraphy	2-3
	2.4	Major Coal Seams	2-6
	2.5	Key Reservoir Properties	2-6
	2.6	Summary of Reservoir Properties	2-15
3.0	COAL	BED METHANE RESOURCES	3-1
	3.1	Summary	3-1
	3.2	Coalbed Methane Resources	3-1
	3.3	In-Place and Technically Recoverable PRB CBM Resources, by Partition	3-3
	3.4	Estimating Gas and Water Production	3-8
4.0	COST	S OF PRB CBM DEVELOPMENT	4-1
	4.1	Basic Cost Model	4-1
	4.2	Discussion of CBM Development Capital Costs	4-5
	4.3	Discussion of CBM Well O&M Costs	4-9
5.0	ECON	OMICS OF PRB CBM UNDER ALTERNATIVE WATER DISPOSAL	
	OPTIC	DNS	5-1
	5.1	Summary	5-1
	5.2	Water Disposal Alternatives	5-3
	5.3	Costs of Water Disposal Alternatives	5-4
	5.4	Discussion of Water Disposal Capital and O&M Costs	5-6
	5.5	Detailed Economic Analyses of Water Management Options	5-10
6.0	PRESE	ENTATION OF RESULTS BY BASIN PARTITION	6-1
	6.1	Partition #1	6-1
	6.2	Partition #2	6-1
	6.3	Partitions #3 and #12	6-6
	6.4	Partition #4	6-9
	6.5	Partition #5	6-16

### Page

6.6	Partition #6	6-25
6.7	Partition #7	6-33
6.8	Partition #8	6-39
6.9	Partition #9	6-46
6.10	Partition #10	6-46
6.11	Partition #11	6-49

## Figures

Figure 1-1.	Powder River Basin, Growth of Coalbed Methane Production	1-2
Figure 1-2.	Powder River Basin, Growth in CBM Water Production	1-2
Figure 1-3.	CBM Water/Gas Production Ratio	1-3
Figure 1-4.	CBM Water Production Per Well	1-3
Figure 1-5.	Powder River Basin CBM Partitions	1-5
Figure 1-6.	Extent of CBM Drilling Map, Partition #4, Anderson Coal Seam Wells	1-6
Figure 1-7.	Extent of CBM Drilling Map, Partition #4, Canyon Coal Seam Wells	1-7
Figure 1-8.	Extent of CBM Drilling Map, Partition #4, Wyodak Coal Seam Wells	1-8
Figure 2-1.	Coal Basins of Wyoming	2-1
Figure 2-2.	Center of Powder River Basin Coalbed Methane Activity	2-2
Figure 2-3.	Regional Structure and Tectonic Map of the Powder River Basin	2-3
Figure 2-4.	Regional Cross Section of the Powder River Basin	2-4
Figure 2-5.	Upper Cretaceous and Tertiary Stratigraphic Chart for Powder River Basin	2-4
Figure 2-6.	Coal Bearing Units of the Tongue River Member of the Fort Union	
	Formation	2-5
Figure 2-7.	Simplified Representation of Fort Union Coalbeds Near Gillette, in	
	Campbell County, Wyoming	2-7
Figure 2-8.	Sample Log Upper Fort Union Coals in Partition #4	2-8
Figure 2-9.	Coal Correlation Diagram for Fort Union and Wasatch Formation,	
	Powder River Basin, Wyoming	2-9
Figure 2-10	. Cross-Section Showing Lateral Variation of Coalbeds in the Wyodak	
	Coal Zone	2-11
Figure 2-11	. Regional Pressure Gradient	2-11
Figure 2-12	. Reservoir Pressure Profile Used for PRB Study	2-12
Figure 2-13	. Gas Content Isotherm Used for Powder River Coalbed Methane	2-13
Figure 2-14	. Average Synthesized Adsorption Isotherm for 41 Coal Samples From the	
	PRB, Based on a Compilation of Data From Public and Private Sources	2-13
Figure 3-1.	Wyodak Coal Seam Time Zero Plot	3-9
Figure 3-2.	Wyodak Type Well History Match	3-10
Figure 3-3.	10-Year Simulation of Gas and Water Production for Wyodak Type Well	3-11

Figure 6-1. Partition #1 Base Map	. 6-2
Figure 6-2. Partition #2 Base Map	. 6-3
Figure 6-3. Canyon Time Zero Plot	. 6-6
Figure 6-4. Wyodak Time Zero Plot	. 6-7
Figure 6-5. Partition #3 Base Map	. 6-11
Figure 6-6. Partition #12 Base Map	. 6-12
Figure 6-7. Big George Time Zero Plot	. 6-15
Figure 6-8. Big George Partition #3	. 6-16
Figure 6-9. Partition #4 Base Map	. 6-18
Figure 6-10. Partition #4 Sample Log	. 6-20
Figure 6-11. Partition #4 Anderson Wells	. 6-22
Figure 6-12. Anderson Time Zero Plot	. 6-23
Figure 6-13. Anderson Type Well, Partition #4	. 6-24
Figure 6-14. Partition #4 Canyon Wells	. 6-26
Figure 6-15. Canyon Time Zero Plot	. 6-27
Figure 6-16. Canyon Type Well, Partition #4	. 6-28
Figure 6-17. Partition #4 Wyodak Wells	. 6-29
Figure 6-18. Wyodak Time Zero Plot	. 6-30
Figure 6-19. Wyodak Type Well, Partition #4	. 6-32
Figure 6-20. Partition #4 Cook Wells	. 6-33
Figure 6-21. Partition #4 Wall Wells	. 6-35
Figure 6-22. Wall Time Zero Plot	. 6-36
Figure 6-23. Wall Type Well, Partition #4	. 6-37
Figure 6-24. Partition #4 Pawnee Wells	. 6-39
Figure 6-25. Partition #4 Cache Wells	. 6-40
Figure 6-26. Partition #5 Base Map	. 6-42
Figure 6-27. Smith Time Zero Plot	. 6-45
Figure 6-28. Smith Type Well, Partition #5	. 6-46
Figure 6-29. Anderson Time Zero Plot	. 6-48
Figure 6-30. Canyon Time Zero Plot	. 6-50
Figure 6-31. Big George Coal Seam - Aggregate	. 6-52
Figure 6-32. Big George Coal Seam Well Location and Elevation Map, Partition #5	. 6-53
Figure 6-33. Big George Time Zero Plot	. 6-54
Figure 6-34. Big George Type Well Partition #5	. 6-55
Figure 6-35. Wyodak Time Zero Plot	. 6-57
Figure 6-36. Partition #6 Base Map	. 6-61
Figure 6-37. Partition #7 Base Map	. 6-70
Figure 6-38. Partition #8 Base Map	. 6-77
Figure 6-39. Anderson Time Zero Plot	. 6-80
Figure 6-40. Anderson Type Well, Partition #8	. 6-81

### <u>Page</u>

Figure 6-41.	Cook Time Zero Plot	6-83
Figure 6-42.	Cook Type Well, Partition #8	6-84
Figure 6-43.	Wall Time Zero Plot	6-86
Figure 6-44.	Wall Type Well, Partition #8	6-87
Figure 6-45.	Pawnee Time Zero Plot	6-89
Figure 6-46.	Pawnee Type Well, Partition #8	6-90
Figure 6-47.	Partition #9 Base Map	6-93
Figure 6-48.	Partition #10 Base Map	6-94
Figure 6-49.	Dietz Time Zero Plot	6-96
Figure 6-50.	Monarch Time Zero Plot	6-98
Figure 6-51.	Cook-Carney Time Zero Plot	6-100
Figure 6-52.	Partition #11 Base Map	6-102
Figure 6-53.	Dietz (Anderson) Time Zero Plot	6-103
Figure 6-54.	Dietz (Anderson), Partition #11	6-106
Figure 6-55.	Monarch (Canyon) Time Zero Plot	6-107
Figure 6-56.	Monarch (Canyon), Partition #11	6-109
Figure 6-57.	Carney (Cook) Time Zero Plot	6-110
Figure 6-58.	Carney (Cook), Partition #11	6-111
Figure A-1.	Gas Content Isotherm Used for Powder River Coalbed Methane	A-3
Figure A-2.	Average Synthesized Adsorption Isotherm for 41 Coal Samples From the	
	PRB, Based on a Compilation of Data From Public and Private Sources	A-3
Figure A-3.	Variation in Sorption Capacity with Temperature, Dietz #3 Coal	A-5
Figure A-4.	Comparison of Bustin and Downey Adsorption Iostherm for	
	Dietz #3 Coal with Advanced Resources Adsorption Isotherm for PRB Coals	A-5
Figure A-5.	Wyodak Time Zero Well Data	A-7
Figure A-6.	History Match Wyodak Type Well w/Free Gas	A-7
Figure A-7.	Reservoir Simulation of Wyodak Type Well w/No Free Gas	A-8
Figure A-8.	Reservoir Simulation of Wyodak Type Well w/23% Gas Undersaturation	A-8
Figure A-9.	Reservoir Simulation of Wyodak Type Well w/66% Gas Undersaturation	A-9
Figure A-10	. Big George Time Zero Well Data	A-10
Figure A-11	. History Match Big George Type Well	A-11
Figure A-12	. Reservoir Simulation of Big George Type Well w/23% Gas	
	Undersaturation	A-12

### Tables

Table S-1.	Volumes of Economically Recoverable CBM w/Alternative Water	
	Disposal Options (Tcf)	Х
Table S-2.	Summary of Impacts from Using Alternative Water Disposal Methods	
	for CBM Produced Water in the PRB	xi
Table 1-1.	Reports and Data for Powder River CBM and Water Study	1-10

### Page

Table 1-2. Electronic Data Sources for Powder River CBM and Water Study	1-12
Table 1-3. Economically Recoverable CBM (Tcf)	1-14
Table 1-4.    Volumes of Economically Recoverable CBM (Tcf)	1-14
Table 1-5.    Volumes of CBM Produced Water (Billion Bbls)	1-15
Table 1-6. Loss of Economically Recoverable CBM (Tcf)	1-15
Table 1-7. Loss of Mineral Royalties from CBM (\$MM)	1-16
Table 1-8. Loss of Well Drilling for CBM (# Wells)	1-16
Table 1-9. Loss of Capital Investment for CBM (\$MM)	1-17
Table 1-10.    Summary of Impacts	1-17
Table 2-1. Partition #4 Coal Depth	2-6
Table 2-2. Coal Thickness for Partition #4	2-10
Table 2-3. Average Data for Partition #4	2-15
Table 2-4. Key Reservoir Properties for Powder River Basin Coals	2-16
Table 3-1. Gas In-Place for Major PRB Coal Seams (Bcf)	3-2
Table 3-2. Technically Recoverable Resources for Major PRB Coal Seams (Bcf)	3-3
Table 3-3. In-Place and Technically Recoverable CBM, Partitions #1 and #2	3-4
Table 3-4. In-Place and Technically Recoverable CBM, Partitions #3 and #12	3-4
Table 3-5. In-Place and Technically Recoverable CBM, Partition #4	3-5
Table 3-6. In-Place and Technically Recoverable CBM, Partition #5	3-5
Table 3-7. In-Place and Technically Recoverable CBM, Partition #6	3-6
Table 3-8. In-Place and Technically Recoverable CBM, Partition #7	3-6
Table 3-9. In-Place and Technically Recoverable CBM, Partition #8	3-7
Table 3-10. In-Place and Technically Recoverable CBM, Partition #9	3-7
Table 3-11. In-Place and Technically Recoverable CBM, Partition #10	3-8
Table 3-12. Number and Nature of CBM Wells for History Matching	3-9
Table 3-13. Summary Results for PRB Coalbed Methane History Matching	3-10
Table 3-14.    Number of CBM Type Wells for Basin Assessment	3-12
Table 4-1. Capital Costs for PRB CBM Well	4-2
Table 4-2.    O&M Costs for PRB CBM Well	4-3
Table 4-3. Capital Costs for Alternate Method of Water Disposal	4-4
Table 4-4. Sample Tangible and Intangible Costs for Two PRB CBM Wells	4-6
Table 4-5. Additional Drilling and Completion Costs for Two PRB CBM Wells	4-7
Table 4-6. Pump Replacement Costs	4-9
Table 5-1. Volumes of Economically Recoverable CBM w/Alternative Water	
Disposal Options	5-2
Table 5-2. Volumes of Economically Recoverable CBM w/Alternative Water	
Disposal Options	5-3
Table 5-3. CBM Water Disposal Alternative Costs	5-4
Table 5-4. Capital Costs for Disposal Options	5-5
Table 5-5. Total Estimated Costs for Deep Disposal	5-5
Table 5-6. Total Capital Costs for Active Water Treatment	5-9

Table 5-7. Annual Operating Costs for Trucking	5-10
Table 5-8. Assumptions for Discounted Cash Flow Analyses	5-10
Table 5-9. Cashflow Model Surface Discharge    5-	-122
Table 6-1. Anderson Coal Seam	6-2
Table 6-2. Canyon Coal Seam	6-3
Table 6-3. Wyodak Coal Seam	6-4
Table 6-4. Big George Coal Seam	6-4
Table 6-5. Cook Coal Seam	6-5
Table 6-6. Pawnee Coal Seam	6-5
Table 6-7. In-Place and Technically Recoverable CBM, Partitions #1 and #2	6-6
Table 6-8. Anderson Coal Seam	6-7
Table 6-9. Canyon Coal Seam	6-8
Table 6-10. Big George Coal Seam	6-8
Table 6-11. Cook Coal Seam	6-9
Table 6-12. In-Place and Technically Recoverable CBM, Partitions #3 and #12	6-9
Table 6-13. Anderson Coal Seam	6-11
Table 6-14. Canyon Coal Seam	6-12
Table 6-15.    Wyodak Coal Seam	6-13
Table 6-16. Cook Coal Seam	6-13
Table 6-17. Wall Coal Seam	6-14
Table 6-18. Pawnee Coal Seam	6-15
Table 6-19. Cache Coal Seam	6-16
Table 6-20. In-Place and Technically Recoverable CBM, Partition #4	6-16
Table 6-21. Felix Coal Seam	6-17
Table 6-22. Roland Coal Seam	6-18
Table 6-23. Smith Coal Seam	6-18
Table 6-24. Swartz Coal Seam	6-19
Table 6-25. Anderson Coal Seam	6-20
Table 6-26. Canyon Coal Seam	6-20
Table 6-27. Big George Coal Seam	6-21
Table 6-28. Wyodak Coal Seam	6-22
Table 6-29. Cook Coal Seam	6-23
Table 6-30. Wall Coal Seam	6-23
Table 6-31. Pawnee Coal Seam	6-24
Table 6-32. Cache Coal Seam	6-25
Table 6-33. In-Place and Technically Recoverable CBM, Partition #5	6-25
Table 6-34. Cameron Coal Seam	6-26
Table 6-35. Murry Coal Seam	6-27
Table 6-36. Felix Coal Seam	6-27
Table 6-37. Ucross Coal Seam	6-28

### Page

Table 6-38.	Roland Coal Seam	. 6-28
Table 6-39.	Anderson Coal Seam	. 6-29
Table 6-40.	Canyon Coal Seam	. 6-30
Table 6-41.	Big George Coal Seam	. 6-30
Table 6-42.	Cook Coal Seam	. 6-31
Table 6-43.	Wall Coal Seam	. 6-31
Table 6-44.	Pawnee Coal Seam	. 6-32
Table 6-45.	In-Place and Technically Recoverable CBM, Partition #6	. 6-32
Table 6-46.	Wasatch Coal Seam	. 6-34
Table 6-47.	Roland Coal Seam	. 6-34
Table 6-48.	Smith Coal Seam	. 6-35
Table 6-49.	Anderson Coal Seam	. 6-35
Table 6-50.	Canyon Coal Seam	. 6-36
Table 6-51.	Cook Coal Seam	. 6-37
Table 6-52.	Wall Coal Seam	. 6-37
Table 6-53.	Pawnee Coal Seam	. 6-38
Table 6-54.	Cache Coal Seam	. 6-38
Table 6-55.	In-Place and Technically Recoverable CBM, Partition #7	. 6-39
Table 6-56.	Smith Coal Seam	. 6-40
Table 6-57.	Swartz Coal Seam	. 6-40
Table 6-58.	Anderson Coal Seam	. 6-41
Table 6-59.	Canyon Coal Seam	6-42
Table 6-60.	Cook Coal Seam	6-42
Table 6-61.	Wall Coal Seam	6-43
Table 6-62.	Pawnee Coal Seam	. 6-44
Table 6-63.	Cache Coal Seam	. 6-44
Table 6-64.	Oedekoven	. 6-45
Table 6-65.	In-Place and Technically Recoverable CBM, Partition #8	6-45
Table 6-66.	Dietz Coal Seam	6-47
Table 6-67.	Monarch Coal Seam	6-47
Table 6-68.	Carney Coal Seam	6-48
Table 6-69.	Pawnee Coal Seam	6-49
Table 6-70.	In-Place and Technically Recoverable CBM. Partitions #9 and #10	6-49
Table 6-71.	Dietz #1 Coal Seam	6-50
Table 6-72.	Dietz #2 Coal Seam	6-51
Table 6-73	Dietz #3 Coal Seam	6-51
Table 6-74	Monarch Coal Seam	6-52
Table 6-75	Carney Coal Seam	6-53
Table 6-76	In-Place and Technically Recoverable CRM Partition #11	6-53
14010 0 70.		

### Page

Table A-1.	Comparison PRB Wyodak Coal and Overseas Low Rank Coal	A-2
Table A-2.	Comparison of Gas Production Rates for Wyodak Type Well	A-9
Table A-3.	Wyodak Coal Seam Properties	A-10
Table A-4.	Comparison of Gas Production Rates for Big George Type Well	A-11
Table A-5.	Big George Coal Seam Properties	A-12
Table A-6.	Reservoir Parameters for Powder River Basin (Fort Union Coals)	A-13
Table A-7.	Comparison of 1995 USGS and 2002 ARI Values for Gas Content	
	of PRB Coals	A-14

## **EXECUTIVE SUMMARY**

**The Powder River Basin coals contain a considerably larger volume of gas in place than established by previous studies.** The Powder River Coalbed Methane Basin Study identifies 61 Tcf of natural gas in-place. This in-place resource value is significantly larger than previously reported and confirms that the Powder River Basin (PRB) coalbed methane (CBM) play has the potential for providing significant additions to future domestic natural gas supplies<sup>1</sup>. Major reasons for the increased PRB coalbed methane resource in-place of 61 Tcf in this Basin Study are the following:

- The study included extensive information on the deeper Fort Union coals prevalent in the basin, it compiled new data on the Wastach coals on the western edge of the basin, and it included the coals in the Montana portion of the PRB.
- The study identified the presence of free gas in certain coal formations and established higher gas content values for PRB coals, both increasing the gas in- place over previous estimates.

A significant portion of the coalbed methane resource in the Powder River Basin is technically recoverable. The estimate of 39 Tcf of technically recoverable resources is based on reservoir modeling and the construction of 142 "type wells" representative of the distribution in well performance (gas and water production) for 12 distinct coal seams in 12 basin partitions. All results include CBM development to date in the basin. The Basin Study's estimate of technically recoverable coalbed methane resources for the Powder River updates earlier estimates by the Potential Gas Committee (2000) of 24 Tcf and by the U.S. Geological Survey (2002) of 14 Tcf.

The costs and economic feasibility of further developing coalbed methane in the Powder River Basin will be significantly impacted by produced water management practices and requirements. The study finds that alternative produced water management options will have a profound influence on the economic viability of producing coalbed methane from the PRB. The costs of the alternative water management options in the PRB—assessed using a 15%, before corporate income tax, internal rate of return (IRR) and a long-term natural gas price (at the Henry Hub) of \$3 per Mcf as the economic threshold criteria—are significant and can make an otherwise profitable CBM project uneconomic.

The results of the economic analyses are presented on Table S-1 and are further discussed below.

<sup>&</sup>lt;sup>1</sup>Increased potential, however, should not be confused with additional impact. Higher per well gas recoveries will allow development of the resource using far fewer wells and as a consequence, with much less disturbance. In fact, this analysis forecasts that several thousand fewer wells will be needed to develop the CBM resources in the Powder River Basin, compared to widely-accepted well count estimates. Moreover, prudent resource development is expected to lead to less water production–billions of barrels less–as compared to the draft EIS estimate.

Economic Conditions	Surface Discharge	Impoundment	Shallow Reinjection	Active Treatment
Case 1 (Today)*	1.5			
Case 2 (Transition)**	22.4	20.0	18.8	7.1-10.2
Case 3 (Long Term)***	29.1	27.8	27.1	17.8-21.6

## Table S-1. Volumes of Economically Recoverable CBMw/Alternative Water Disposal Options (Tcf)

\* Basin differential remains at \$1.80 per Mcf.

\*\* Basin differential narrows from \$1.80 per Mcf in year 1 to \$0.80 per Mcf in year 3 and beyond.

\*\*\* Basin differential is \$0.80 per Mcf.

- Under **today's** volatile natural gas prices and unfavorable Wyoming basin differentials, only using surface disposal of produced water is economic. And, this low cost water management option is economic only in selected, highly productive portions of the PRB. More costly water disposal options would preclude further economic development of coalbed methane in the Powder River Basin. A significant portion of the 1.5 Tcf of economic CBM potential, shown in Table S-1, is already under development, leaving little opportunity for further economically justified expansion (at today's conditions and standard economic criteria) in the Powder River Basin.
- Assuming a **transition** toward more normal Wyoming basin price differentials, a significant portion of the basin becomes economic to further develop, with water management practices of surface discharge, impoundment or shallow re-injection<sup>2</sup>. Requiring active treatment of the water (with current reverse osmosis technology) greatly reduces the economically viable potential for CBM in the PRB. Specifically, instead of 19 to 22 Tcf of economically recoverable coalbed methane (using one of the first three water management options, shown in Table S-1), only 7 to 10 Tcf of coalbed methane remains economic to develop with a requirement for active water treatment. This represents a loss of 12 Tcf of otherwise economically recoverable natural gas resource from the Powder River Basin.
- Taking a **long-term** outlook on prices and assuming that the Wyoming basin differential returns to historically more normal values, the economically developable CBM resources of the PRB range from 27 to 29 Tcf (for the three lower cost water management options). Requiring active treatment of water (with current reverse osmosis technology) reduces the economically viable PRB CBM potential to a range of 18 to 22 Tcf for a loss of 7 to 9 Tcf of otherwise economically recoverable natural gas resource.

<sup>&</sup>lt;sup>2</sup>Shallow re-injection is considered in a generic sense and evaluated from a theoretical standpoint. Much uncertainty exists surrounding the real availability of shallow zones with the required geology and fluid flow properties necessary for long-term successful projects.

The loss of CBM resources, royalties and tax receipts from more stringent CBM produced water management practices would be substantial. Table S-2 provides a summary of the potential losses that would occur from requirements to use progressively more stringent water disposal alternatives. The PRB Study recognizes that, in practice, a combination of water disposal alternatives would be used. Once the final mix of options is established, the information in this study can be used to estimate these impacts.

	Loss of CBM Resource	Loss of CBM Royalty	Loss of Production/ Ad Valorem Taxes
Water Disposal Method	(Tcf)	(\$ million)	(\$ million)
Surface Discharge			
Infiltration Impoundment	(2.4)	(\$506)	(\$362)
Shallow Re-injection	(3.6)	(\$756)	(\$540)
Reverse Osmosis/w:			·
Trucking of Residual	(15.3)	(\$3,184)	(\$2,272)
Deep Disposal of Residual	(12.2)	(\$2,547)	(\$1,810)

## Table S-2.Summary of Impacts from Using Alternative Water Disposal Methods<br/>for CBM Produced Water in the PRB

**Improvements in coalbed methane production technology and water management practices can help maintain the economic viability of Powder River coalbed methane**. The current volatile natural gas prices and historically high basin differentials place major hurdles on the economics of Powder River CBM. Further raising the barrier is the recognition that a considerable portion of the shallower, thick coals in the basin have already been drilled, leaving deeper and thinner coals as the target. Finally, the costs of more stringent water management practices will further lower the economic viability of this large natural gas resource.

### 1.0 STUDY PURPOSE, APPROACH AND FINDINGS

#### 1.1 Purpose of Study

The overall purpose of the Powder River Basin Study is to assist DOE/FE, NETL and NPTO better understand the energy impacts of the alternative water disposal options being considered for Powder River Basin coalbed methane. The specific objectives of the study are:

- 1. Develop a stronger data and analytical base for the geology, resources and CBM potential of the Powder River Basin.
- 2. Divide the basin into a series of geologically similar partitions to facilitate the analysis of well performance and costs.
- 3. Project CBM and water production rates for a series of typical wells and the distribution of well performance in each partition.
- 4. Assemble information on the costs of CBM development and produced water management, including cash flows and economics.

#### 1.2 Background

The Powder River Basin of Wyoming and Montana is the site of the fastest growing domestic natural gas play—the development of coalbed methane (CBM) from the Wyodak and Big George fairways. As of the end of 2001:

- Nearly 12,000 CBM wells have been drilled with 8,177 wells producing.
- Coalbed methane production is at 823 million cubic feet a day (MMcfd) up from 111 MMcfd just three years earlier, as shown in Figure 1-1.

Along with the growth in CBM production has been the growth in produced water, as part of dewatering and depressuring the coal formations thus enabling the coals to release their adsorbed methane. As of the end of 2001, water production was at 1,444,000 barrels per day, up from 229,000 barrels per day at the end of 1998, as shown in Figure 1-2.

Progressive CBM development and dewatering, while increasing total water production, is leading to lower water to gas ratios and lower average production of water per well:

- The water to gas production ratio (at the end of 2001) is 1.75 barrels per Mcf, down from 2.88 barrels per Mcf two years ago, as shown in Figure 1-3.
- Water production per CBM well (at the end of 2001) is 177 barrels per day, down from 396 barrels per day two years ago, as shown in Figure 1-4.



Figure 1-1. Powder River Basin, Growth of Coalbed Methane Production



Figure 1-2. Powder River Basin, Growth in CBM Water Production



Figure 1-3. CBM Water/Gas Production Ratio



Figure 1-4. CBM Water Production Per Well

For the most part, produced CBM waters are either surface discharged or placed into impoundments providing beneficial use for agriculture, stock watering and grasslands. Should beneficial use of produced CBM water be constrained, other (more costly) options would need to be considered, impacting the economics and natural gas resource development in the basin. These options include: (a) shallow re-injection to conserve the water for future use; (b) pre-treatment of water with chemicals and reverse osmosis, with deep disposal of the residual concentrate; and/or,  $\mathbb{O}$ ) deep re-injection into non-potable water disposal aquifers.

#### **1.3** Partitioning the Powder River Basin

To provide a series of geologically consistent analytic units, the Powder River Basin is divided into 12 partitions, based on coal depth, development status, and geographic considerations. The 12 basin partitions are shown in Figure 1-5, and consist of the following:

- 1. Southern Extension
- 2. South Eastern Area
- 3. South Central Area
- 4. East Central Area
- 5. Main Central Area
- 6. West Central Area
- 7. North Western Area
- 8. North Eastern Area
- 9. Eastern Montana Area
- 10. Western Montana Area
- 11. NW Basin Edge, Wyoming
- 12. SW Basin Edge, Wyoming

Partition #4, in the east-central portion of the Power River, has seen the most extensive coalbed methane development, as well as surface mining of coal. Figures 1-6 through 1-8 show the extent of coalbed methane development (as of the end of 2001) for the Anderson, Canyon and Wyodak coal seams in Partition #4, and in surrounding townships along the eastern portion of the PRB.

This study provides the gas in-place, recoverable resources and economics of each of the major coal seams in each of these 12 basin partitions.



Figure 1-5. Powder River Basin CBM Partitions.



Figure 1-6. Extent of CBM Drilling Map, Partition #4, Anderson Coal Seam Wells



Figure 1-7. Extent of CBM Drilling Map, Partition #4, Canyon Coal Seam Wells

	53N 74W	53N 73W	53N 72W	53N 71W	53N 70W	53N 69W/	53468W
-	52N 74W	52N73W	Ban 2w	62N 71W	52N 70 W	52N 69W	521/681/
-	51N 74W	61N73W		51N71W	51N 70W	51N 69W	51N68V
	50N 74W	50N 73W	ON 72W		50N 70W	50N 69W/	50 <b>0</b> 68 V
	49N 74W	49N 73W	antizw Ante	Bleepy Hollo	49N 70W 49N 70W	49N 69W/	491 <b>4</b> 88 V
_	48N 74W	48N 73 W			48N 70 W	48 N 69 W	48N 681
_	47N 74W/	47 N 73 W			47N 70W	47N 69W	47N 68 \
	48N 74W	46N 73W		48117110		46N 69W	46N 68 \
	45N 7410/	45N 7310/			45N 70 W	46N 69W	45N 68V
	44N 74W	44N 73 W	44N 72 W	4 <b>4117</b> 71 W	44N 70W	44N 69W	44N 681

Figure 1-8. Extent of CBM Drilling Map, Partition #4, Wyodak Coal Seam Wells

#### 1.4 Study Approach

#### **1.4.1** Coal Resource Data Base

The Basin Study compiled available geologic data on the areal extent and thickness of the major Fort Union Formation coals in the PRB that met the following criteria:

- Below 300 feet of depth
- Thicker than 20 feet
- Sufficient data exist

For Montana, the depth and coal thickness criteria were relaxed (250 feet of depth and 15 feet of coal thickness) to more fully capture the coal and CBM resources in this portion of the basin. Even so, the CBM resources of Montana are only partly defined, as insufficient data existed for the deeper Knoblock coal zone in this portion of the basin.

A variety of data sources were used by the Basin Study, including data from the USGS, Wyoming and Montana State offices, private data and supplemental log analysis, as set forth in Tables 1-1 and 1-2.

The available data were assembled on a township by township basis for each of the major coal seams in the basin. Special attention was given to assembling new data on the deep coals in the central portion of the PRB and on the Wasatch coals along the western edge of the PRB.

#### 1.4.2 Projecting Gas and Water Production

The coalbed methane and water production estimates in the Basin Study were developed as follows:

<u>The geologic model</u> of the PRB (discussed in Chapter 2) provided the key reservoir properties of coal seam depth, thickness, gas content, and reservoir pressure.

<u>A gas and water production data base</u> (discussed in Chapter 3) of over 8,000 CBM wells in the PRB was organized by coal seam and by partition and then normalized by time (using "time zero" plots) to provide a foundation of actual CBM well performance.

<u>History matching</u> of gas and water production (discussed in Chapter 3) from 1,428 PRB CBM wells, organized into 14 distinct coal-seam and basin-partition sets, was used to establish:

- Permeability (matrix, fracture)
- Coal porosity (matrix, fracture)
- Gas and water saturation
- Confirmation of reservoir pressure and gas content

Group	File	Full Description
USGS	BULL 1078	Mapel, W.J., 1959, Geology and coal resources of the Buffalo-Lake de Smet area, Johnson and Sheridan Counties, Wyoming: U.S. Geological Survey Bulletin 1078, 148 p.
USGS	BULL 1917-F	Nichols, D.J., and Brown, J.L., 1992, Palynostratigraphy of the Tullock Member (lower Paleocene) of the Fort Union Formation in the Powder River Basin, Montana and Wyoming: U.S. Geological Survey Bulletin 1917-F, 35 p., 10 pls.
USGS	CI C-119-A.	McLellan, M.W., and Biewick, L.H., 1988, Stratigraphic framework of the Paleocene coal beds in the Broadus 30' x 60' quadrangle, Powder River Basin, Montana—Wyoming: U.S. Geological Survey Coal Investigations Map C-119-A.
USGS	CI MAP C-113	Culbertson, W.C., 1987, Diagrams showing proposed correlation and nomenclature of Eocene and Paleocene coal beds underlying the Birney 30' x 60'quadrangle, Big Horn, Rosebud, and Powder River Counties: U.S. Geological Survey Coal Investigations Map C-113.
USGS	CI MAP C-2	Combo, J.X., Holmes, C.N., and Christner, H.R., 1978, Map showing the coal resources of Montana: U.S. Geological Survey Coal Investigations Map C-2.
WGS	CIR 14	Glass, G.B., 1998, Coal resources of the Powder River Basin, in, Guidebook to Coal Geology of the Powder River Basin: Wyoming Geological Survey Information Circular no. 14, p. 97-131.
USGS	CIR 53	Combo, J.X., Brown, D.M., Pulver, H.F., and Taylor, D.A., 1949, Coal resources of Montana: U.S. Geological Survey Circular 53, 28 p.
USGS	CIR 81	Berryhill, H.L., Jr., Brown, D.M., Brown, A., and Taylor D.A., 1950, Coal resources of Wyoming: U.S. Geological Survey Circular 81, 78 p.
WGS	FIELD GUIDE	Culbertson, W.C., and Mapel, W.J., 1976, Coal in the Wasatch Formation, northwest part of the Powder River Basin near Sheridan, Sheridan County, Wyoming: Wyoming Geological Association Guidebook 28th Annual Field Conference, p. 193-201.
WGS	GUIDEBOOK	Mapel, W.J., 1958, Coal in the Powder River Basin: Wyoming Geological Association Guidebook, 13th Annual Field Conference, p. 218-224.
USGS	I-1128	Law, B.E., Barnum, B.E., and Wollenzien, T.P., 1979, Coal bed correlations in the Tongue River Member of the Fort Union Formation, Monarch, Wyoming, and Decker, Montana, areas: U.S. Geological Survey Miscellaneous Investigations Series Map I-1128.
USGS	I-1959A	McLellan, M.W., Biewick, L.H., Molnia, C.L., and Pierce, F.W., 1990, Coal stratigraphy of northern and central Powder River Basin, Montana and Wyoming: U.S. Geological Survey Miscellaneous Investigations Series Map I-1959-A.
USGS	I-1959-B	Pierce, F.W., Johnson, E.A., Molnia, C.L., and Sigleo, W.R., 1990, Coal stratigraphy of the southeastern Powder River Basin, Wyoming: U.S. Geological Survey Miscellaneous Investigations Map I-1959-B.
USGS	I-1959-C (MAP)	Hardie, J.K., 1991, Coal stratigraphy of the southwestern Powder River Basin,Wyoming: U.S. Geological Survey Miscellaneous Investigations Series Map I-1959-C.
USGS	I-1959-D	Molnia, Carol L., and Pierce, Frances Wahl, 1992, Cross sections showing coal stratigraphy of the central Powder River Basin, Wyoming and Montana: U.S. Geological Survey Miscel- laneous Investigations Series Map I-1959-D, scale 1:500,000.
USGS	I-2011	Pierce, F.W., and Johnson, E.A., 1991, Stratigraphic cross section showing upper Paleocene coal-bearing rocks of the Tongue River Member of the Fort Union Formation in the Piney Canyon NE and Piney Canyon NW quadrangles, Campbell and Weston Counties, south-eastern Powder River Basin, Wyoming: U.S. Geological Survey Miscellaneous Investigations Series Map I-2011.
USGS	1-2013	Johnson, E.A., and Pierce, F.W., 1991, Stratigraphic cross section showing upper Paleocene coal-bearing rocks of the Tongue River Member of the Fort Union Formation in the Coal Bank Draw and Dugout Creek North quadrangles, Campbell and Weston Counties, southeastern Powder River Basin, Wyoming: U.S. Geological Survey Miscellaneous Investigations Series Map I-2013.

## Table 1-1. Reports and Data for Powder River CBM and Produced Water Management Study

# Table 1-1. Reports and Data for Powder River CBM and Produced Water Management Study (Continued)

Group	File	Full Description
USGS	ISBN 1-890977-15-2	Roberts, L.N.R., Mercier, T.J., Biewick, L.R.H., and Blake, Dorsey, 1998, A procedure for producing maps and resource tables of coals assessed during the U.S. Geological Survey's National Coal Assessment: Fifteenth Annual International Pittsburgh Coal Conference Proceedings, CD-ROM (ISBN 1-890977-15-2), 4 p.
USGS	MF-1779 & MF-1929	Weaver, J.N., and Flores, R.M., 1985, Stratigraphic framework of the upper Fort Union Formation at the TA Hills, Western Powder River Basin, Wyoming: U.S. Geological Survey Miscellaneous Field Studies Map, MF1779 & MF-1929.
USGS	MF-1127 & MF-1126	Flores, R.M., 1979, Restored stratigraphic cross sections and coal correlations in the Tongue River member of the Fort Union Formation, Powder River area, Montana: U.S. Geological Survey, Miscellaneous Field Studies Map MF-1127 & MF-1126.
USGS	MF-1796	MF-1796
USGS	OF 76-450	OF 76-450
USGS	OF 77-283	OF 77-283
USGS	OF 77-721	OF 77-721
USGS	OF 79-1201	Culbertson, W.C., Kent, B.H., and Mapel, W.J., 1979, Preliminary diagrams showing correla- tion of coal beds in the Fort Union and Wasatch Formations across the northern Powder River Basin, northeastern Wyoming and southeastern Montana: U.S. Geological Survey Open-File Report 79-1201.
USGS	OF 82-026	OF 82-026
USGS	OF 85-621	Trent, V.A., 1985, Summary of results of the Coal Resource Occurance and Coal Develop- ment Potential Mapping Program in Part of the Powder River basin, MT & WY: U.S. Geo- logical Survey Open-file Report 85-621,49 p.,1 pl., 2 fig., 14 tables, Scale 1:1,000,000.
USGS	PP 1625-A	1999 Resource Assessment of Selected Tertiary Coal Beds and Zones in the Northern Rocky Mountains and Great Plains Region.
WGS	OF 92-4	Jones, Richard, and Glass G., 1991, Demonstrated reserve base of coal in Wyoming as of January 1, 1991: Wyoming Geological Survey Open-File Report 92-4.
USGS	OF 97-469	Molnia, C.L., Biewick, L.R.H., Blake, Dorsey, Tewalt, S.J., Carter, M.D., and Gaskill, Charlie, 1997, Coal availability in the Hilight quadrangle, Powder River Basin, Wyoming: a prototype study in a western coal field: U.S. Geological Survey Open-File Report 97-469, 21 p.
WGS	RI 35	Ayers, W.B., Jr., 1986, Coal resources of the Tongue River Member of the Fort Union Formation (Paleocene), Powder River Basin, Wyoming and Montana: Geological Survey of Wyoming Report of Investigations No. 35, 22 p.
WRD	WRIR 85-4305	Daddow, P.B., 1986, Potentiametric-Surface map of the Wyodak-Anderson coal bed, Powder River Structural Basin, Wyoming, 1973-84: U.S. Department of the Interior, Water Resources Division, Water Resources Investigation Report 85-4305 (prepared in cooperation with the Bureau of Land Management).
BLM		Bureau of Land Management, 1996, Powder River Basin Coal Production—1995; N. Braz, C. Gaskill and R. Nelson compilers, U.S. Department of the Interior, Bureau of Land Management, Casper, Wyoming, file D\drawings\wo-map.dwg.
USGS		U.S. Geological Survey Global Land Information System-GLIS, 1997, digital spatial data obtained from http://edcwww.cr.usgs.gov/glis/glis.html.
BLM		www.wy.blm.gov/minerals/og/re's.mgt/resevmgt.html

Table 1-2. Electronic Data Sources for Powder River CBM and Produced Water
Management Study

1.	Field Conference - Coalbed Methane - Powder River OF01-126
2.	http://greenwood.cr.usgs.gov/energy/coal/OF-97-469.html
3.	http://greenwood.cr.usgs.gov/pub/open-file-reports/ofr-98-0789-a/
4.	http://greenwood.cr.usgs.gov/pub/open-file-reports/ofr-98-0789-b/
5.	http://www.cbmcc.vcn.com/
6.	http://www.prb-eis.org/
7.	US Coal Quality Database
8.	http://www.deq.state.mt.us/coalbedmethane/
9.	http://www.cbmwyo.org
10.	http://www.powderriverbasin.org
11.	http://energy.cr.usgs.gov/oilgas/cbmethane/
12.	http://deq.state.wy.us/
13.	http://wogcc.state.wy.us/
14.	http://www.wsgsweb.uwyo.edu/
15.	http://www.wy.blm.gov/Directory/fo_map/fo_map.html
16.	Rick Marvel @WYOGC rmarve@state.wy.us 307-234-7147
17.	http://bogc.dnrc.state.mt.us/

Advanced Resources' <u>COMET3</u> reservoir simulator, a triple porosity and triple permeability finite difference model, specifically developed for coalbed methane production and reserve assessments, was used for history matching and establishing 14 "type wells" reflecting the geologic and reservoir diversity encountered by PRB coals (discussed in Chapter 3).

The history-matched "type wells" were extended in time (using COMET3) to provide ten year coalbed methane and water production rates and estimates of ultimate gas and water recovery (discussed in Chapter 3).

The 14 PRB "type wells" were scaled using actual depth, thickness and gas content to develop <u>142 individual "type wells"</u> to reflect average, high and low performance for each major coal seam in each basin partition.

#### **1.4.3 Basic Cost and Economic Model**

The study constructed a Powder River Basin coalbed methane cost and economic model, CECON (<u>C</u>oalbed <u>Econ</u>omics), to assess the economic feasibility of developing coalbed methane in the basin (discussed in Chapter 4). The model includes four components: (1) basic capital costs; (2) basic operating and maintenance costs; (3) gas transportation and compressions costs; and (4) other costs.

The economic model incorporates forecasts for future natural gas prices (at the Henry Hub), current and anticipated Wyoming "basin differentials," royalties, production taxes, and other factors that impact CBM costs and economics. The economic model is an industry standard discounted cash flow (DCF) model that provides both an internal rate of return and the net present value (NPV) of an investment at various discount rates and at various net gas prices.

#### 1.4.4 <u>Water Management Alternatives</u>

Finally, the Basin Study examined the costs and economic feasibility of four alternatives for CBM produced water management in the Powder River Basin. These include:

- 1. Untreated or passively treated produced water, with surface discharge;
- 2. Infiltration impoundment of the produced water, with enhanced evaporation and/or land application;
- 3. Shallow re-injection of the produced water; and
- 4. Actively treated produced water (with reverse osmosis), with surface discharge of the treated water and with disposal of the residual concentrate by trucking and/or deep re-injection.

Deep re-injection of the untreated, relatively high quality CBM produced water would constitute a loss of a valuable resource and thus was not included among the water disposal alternatives addressed in this study.

#### 1.5 Summary of Findings and Impacts

- **1.5.1** The Powder River Basin coals contain a considerably larger volume of gas in place than established by previous studies. Major reasons for the increased PRB coalbed methane resource in-place of 61 Tcf are: (1) the study included the deeper Fort Union coals prevalent in the basin, it compiled new data on the Wastach coals, and it included Montana coals; and (2) the study identified the presence of free gas in certain coal formations and established higher gas content values for PRB coals.
- **1.5.2** A significant portion of the coalbed methane resource in the Powder River Basin is technically recoverable. The estimate of 39 Tcf of technically recoverable resources is based on reservoir modeling and the construction of 142 "type wells" representative of the distribution in well performance (gas and water production) in the basin. This updates earlier estimates by the Potential Gas Committee (2000) of 24 Tcf and by the U.S. Geological Survey (2002) of 14 Tcf.

**1.5.3** The costs and economic feasibility of further developing coalbed methane in the Powder River Basin will be significantly impacted by produced water management practices and requirements. As shown in Table 1-3, requiring active treatment of water (such as reverse osmosis) imposes a high cost penalty, and with it, loss of economically recoverable resources.

	Alternative Water Disposal Options			
Economic Cases*	Surface Discharge	Impoundment	Shallow Reinjection	Active Treatment
Case 1 (Today)**	1.5 Tcf			
Case 2 (Transition)***	22.4 Tcf	20.0 Tcf	18.8 Tcf	7.1-10.2 Tcf
Case 3 (Long Term)****	29.1 Tcf	27.8 Tcf	27.1 Tcf	17.8-21.6 Tcf

Table 1-5. Economically Recoverable CBNI (1cf	Table 1-3.	Economically	Recoverable	CBM	(Tcf)
---	------------	--------------	-------------	-----	-------

\* Natural gas price (Henry Hub)of \$3 (real) per Mcf for life of project.

\*\* Basin differential remains at \$1.80 per Mcf.

\*\*\* Basin differential narrows from \$1.80 per Mcf in year 1 to \$0.80 per Mcf in year 3 and beyond.

\*\*\*\* Basin differential is \$0.80 per Mcf.

The distribution of economically recoverable CBM and estimated water production by mineral ownership (using Case 2 economic conditions) is provided in Tables 1-4 and 1-5.

Table 1-4.	Volumes	of Econo	mically	Recoverable	CBM (	(Tcf)
			•			

	Alternative Water Disposal Options					
Mineral Ownership	Surface Discharge	Impoundment	Shallow Reinjection	Active Treatment		
Federal	13.7 Tcf	12.2 Tcf	11.5 Tcf	4.3-6.2 Tcf		
State	1.5 Tcf	1.4 Tcf	1.3 Tcf	0.5-0.7 Tcf		
Private	7.2 Tcf	6.4 Tcf	6.0 Tcf	2.3-3.3 Tcf		
TOTAL	22.4 Tcf	20.0 Tcf	18.8 Tcf	7.1-10.2 Tcf		

All mineral ownership results based on a simplified methodology using draft EIS data.

	Alternative Water Disposal Options						
Mineral Ownership	Surface Discharge	Impoundment	Shallow Reinjection	Active Treatment			
Federal	16.6	14.6	13.8	3.7-6.5			
State	1.9	1.7	1.6	0.4-0.8			
Private	8.7	7.7	7.3	2.0-3.4			
TOTAL	27.2*	24.0	22.7	6.1-10.7			

#### Table 1-5. Volumes of CBM Produced Water (Billion Bbls)

\*Approximately 5 billion barrels <u>less</u> water than estimated in the WY draft EIS.

**1.5.4** More stringent CBM produced water management practices will lead to loss of recoverable CBM resources for federal, state and local mineral ownership. The loss of recoverable CBM resources by mineral ownership due to progressively more stringent CBM produced water management practices (using Case 2 economic conditions) is provided in Table 1-6.

	Alternative Water Disposal Options					
Mineral Ownership	Surface Discharge*	Impoundment	Shallow Reinjection	Active Treatment		
Federal		(1.5 Tcf)	(2.2 Tcf)	(7.5-9.4 Tcf)		
State		(0.1 Tcf)	(0.2 Tcf)	(0.8-1.0 Tcf)		
Private		(0.8 Tcf)	(1.2 Tcf)	(3.9-4.9 Tcf)		
TOTAL		(2.4 Tcf)	(3.6 Tcf)	(12.2-15.3 Tcf)		

\* An estimated 22.4 Tcf of economically recoverable CBM resource is available under Case 2 economic conditions and surface discharge.

**<sup>1.5.5</sup>** More stringent CBM produced water management practices will reduce royalty collections and state severance and ad valorem tax receipts. Federal, state and private royalty payments average about \$0.26/Mcf (assuming Case 2 economic conditions). The aggregate royalty payment losses would range from \$506 to \$3,184 million depending on the water management practice required, shown on Table 1-7.
		Alternative Wate	r Disposal Options				
Mineral Ownership	Surface Discharge*	Impoundment	Shallow Reinjection	Active Treatment			
Federal		(\$268)	(\$401)	(\$1,349-1,687)			
State		(\$41)	(\$61)	(\$207-\$258)			
Private		(\$197) (\$294) (\$991-\$1,23					
TOTAL		(\$506)	(\$756)	(\$2,547-\$3,184)			

#### Table 1-7. Loss of Mineral Royalties from CBM (\$MM)

\* A total of \$4,659 million of mineral royalties would be collected under Case 2 economic conditions and surface discharge.

State severance and county ad valorem tax receipts average about \$0.15/Mcf (assuming Case 2 economic conditions and 12% (WY) and 9.3% (MT) tax rates). The aggregate tax receipt losses range from \$360 to \$2,270 million depending on the water management practices required.

**1.5.6** More stringent CBM produced water management practices will lead to less capital investment and service work in the Powder River Basin. The loss of CBM well drilling and capital investment by mineral ownership due to more stringent CBM produced water management practices (using Case 2 economic conditions) is provided in Tables 1-8 and 1-9.

Table 1-8. Loss of Well Drilling for CBM (# Wells)

		Alternative Wate	r Disposal Options				
Mineral Ownership	Surface Discharge*	Impoundment	Shallow Reinjection	Active Treatment			
Federal		(4,041)	(6,324)	(17,919-21,257)			
State		(464)	(726)	(2,056-2,439)			
Private		(2,120) (3,318) (9,940-11,1					
TOTAL		(6,625)	(10,368)	(29,915-34,847)			

\* An estimated 46,944 wells would be drilled under Case 2 economic conditions and surface discharge. This represents more than 4,000 <u>fewer</u> wells compared to the WY draft EIS well-count estimate.

		Alternative Wate	r Disposal Options			
Mineral Ownership	Surface Discharge*	Impoundment	Shallow Reinjection	Active Treatment		
Federal		(\$455)	(\$712)	(\$2,016-\$2,391)		
State		(\$52)	(\$82)	(\$231-\$274)		
Private		(\$238) (\$373) (\$1,058-\$1,2				
TOTAL		(\$745)	(\$1,167)	(\$3,305-\$3,920)		

#### Table 1-9. Loss of Capital Investment for CBM (\$MM)

\* The capital expenditure for PRB CBM is estimated at \$5,281 million assuming Case 2 economic conditions and surface discharge.

**1.5.7** Summary of Impacts. The loss of CBM resources, royalties and tax receipts from more stringent CBM produced water management practices would be substantial. Table 1-10 provides a summary of the potential losses that would occur from use of progressively more stringent water disposal alternatives.

	Loss of CBM Resource	Loss of CBM Royalty	Loss of Production/ Ad Valorem Taxes
Water Disposal Method	(Tcf)	(\$ million)	(\$ million)
Surface Discharge			
Infiltration Impoundment	(2.4)	(\$506)	(\$362)
Shallow Re-injection	(3.6)	(\$756)	(\$540)
Reverse Osmosis/w:	-		
Trucking of Residual	(15.3)	(\$3,184)	(\$2,272)
Deep Disposal of Residual	(12.2)	(\$2,547)	(\$1,810)

Table 1-10. Summary of Impacts

**1.5.8** Improvements in coalbed methane production technology and water management practices would help maintain the economic viability of Powder River Basin coalbed methane. Advanced technology options offer promise for reducing costs and increasing reserves per well. Conducting assessments of these technology options and supporting their adaptation to PRB operating conditions would be of high value to basin operators.

#### 2.0 GEOLOGIC SETTING AND RESERVOIR PROPERTIES

#### 2.1 Basin Area

The Powder River Basin is one of a series of coal-bearing basins along the Rocky Mountains, stretching from northern New Mexico to central Montana, Figure 2-1. The basin covers approximately 28,500 square miles, with approximately one-half of this area underlain by producible coals. The basin is bounded on the east by the Black Hills uplift, on the north by the Miles City arch, on the south by the Laramide Mountains, and on the west by the Big Horn uplift and Casper arch.



Figure 2-1. Coal Basins of Wyoming

The bulk of coalbed methane activity to date has been in the east and central portion of the basin, around the town of Gillette, in Campbell County, Wyoming, Figure 2-2. To date, nearly 12,000 coalbed methane wells have been drilled in the Powder River Basin, providing a wealth of data for establishing the geologic setting and characteristics of the Wasatch and Fort Union Formation low rank coals in this basin.



Figure 2-2. Center of Powder River Basin Coalbed Methane Activity

#### 2.2 Basin Structure

The eastern flank of the Powder River Basin dips gradually at an average of 1.5° and is characterized by occasional normal faulting and folding, Figure 2-3. The basinal axis exists along the steeper western and southern margins, where the basin terminates against a complex of



Figure 2-3. Regional Structure and Tectonic Map of the Powder River Basin

basement thrusts and reverse faults, as shown on the generalized cross-section of the Powder River Basin, Figure 2-4.

# 2.3 Basin Stratigraphy

The Powder River Basin is filled mainly with thick Tertiary-age marine and fluvial deposits. The Tertiary units contain the coal bearing Fort Union and Wasatch formations that are the topic of this Basin Study, Figure 2-5.



Source: Montgomery, 1999.

Figure 2-4. Regional Cross Section of the Powder River Basin



Source: Law, Rice and Flores, 1991

# Figure 2-5. Upper Cretaceous and Tertiary Stratigraphic Chart for Powder River Basin

The Tongue River Member, consisting of sandstone, conglomerate, siltstone, limestone and coal, is the principal coal-bearing unit of the Fort Union Formation. The Tongue River Member contains a large number of distinct coal seams, ranging from a few feet to over 200 feet in thickness, as shown on Figure 2-6.



Figure 2-6. Coal Bearing Units of the Tongue River Member of the Fort Union Formation

The Tongue River Member can be further divided into upper and lower units. The Upper Tongue River unit contains the Smith/Swartz, Anderson (Deitz), Canyon (Monarch), Wyodak (where the Anderson and Canyon have merged), the Big George and the Cook (Carney) seams. The Lower Tongue River unit contains the Wall, Pawnee and Cache seams. A series of Wasatch Formation coals exist on the western edge of the basin and include the Cameron, Felix and Ucross seams. These coals coalesce into a thick coal package at Lake Desmet.

# 2.4 Major Coal Seams

The coals are exposed along the eastern edge of the basin where they are surface mined. The thickest exposed unit of coal along the east-central portion of the basin is the Wyodak seam, containing several individual coal units. As shown on Figure 2-7, the Wyodak seam splits into several thinner coal seams, such as the Anderson and Canyon, toward the basin center as well as to the north and south. Figure 2-8 provides a log of the major coals of the Upper Tongue River unit in the east-central portion of the basin.

A series of informal names have been assigned to the coals in the Powder River Basin, creating stratigraphic uncertainty. The Basin Study strives to use a consistent set of coal seam terminology, following the extensive stratigraphic work by Goolsby, Finley and Associates. The distribution and correlation of the coals in the Powder River Basin is shown in Figure 2-9, an east-west cross section of the basin.

# 2.5 Key Reservoir Properties

A series of reservoir properties, including depth, coal thickness, gas content, pressure gradient and gas saturation, were collected and assessed to calculate the gas in-place for each of the major coals in each of the 12 basin partitions. In addition, data on coal fracture and matrix porosity was established to calculate the volume of water in-place for each of the coals. Finally, coal reservoir permeability (for both the cleat system and the coal matrix) was established to calculate the amounts of recoverable methane and water.

# 2.5.1 Coal Seam Depth

Coal depth data from completed wells and from previous studies were used to build the coal depth data base for the Powder River Basin. Information on the depth of individual coal seams is provided in Chapter 6. Shown below is data on coal depth for basin Partition #4.

Coal Seam	Avg. Depth (ft)*	Depth Range (ft)*
Anderson	450	300-650
Canyon	540	300-800
Wyodak	600	330-750
Cook	790	600-930
Wall	1,020	800-1,250
Pawnee	1,300	1,150-1,500
Cache	1,500	1,150-1,750

# Table 2-1. Partition #4 Coal Depth

\* Top of coal



Figure 2-7. Simplified Representation of Fort Union Coalbeds Near Gillette, in Campbell County, Wyoming



Figure 2-8. Sample Log - Upper Fort Union Coals in Partition #4



Source: Law, Rice and Flores, 1991

# Figure 2-9. Coal Correlation Diagram for Fort Union and Wasatch Formation, Powder River Basin, Wyoming

#### 2.5.2 Coal Seam Thickness

Coal seam thickness (net pay) was established for each major coal throughout the basin. Coal interval data from completed wells, well logs from WOGCC, and coal thickness data from previous studies (particularly the work by Goolsby, Findley and Associates and the USGS in PP 1625A) were used to build the coal thickness data base for the Powder River Basin (PRB).

Information on thickness of individual coal seams is provided in Chapter 6. Shown below is data on coal thickness for basin Partition #4. Figure 2-10 provides a cross section showing the complexity of coal deposition for the Wyodak group of coals along the eastern portion of the PRB.

Coal Seam	Avg. Thickness (ft)	Thickness Range (ft)
Anderson	30	20-50
Canyon	35	20-50
Wyodak	73	70-80
Cook	31	20-50
Wall	27	20-40
Pawnee	27	25-30
Cache	23	20-30

 Table 2-2. Coal Thickness for Partition #4

# 2.5.3 Regional Pressure Gradient

A regional pressure gradient versus depth function for PRB coal seams, Figure 2-11, was constructed to establish reservoir pressure for each of the coal formations. This was assembled using:

- Detailed hydrology data and pressure mapping by the Wyoming BLM,
- Actual pressure data from basin producers, and
- History matching (using COMET3) of the pressure gradient data using long-term (4+ year) gas and water production data in the PRB.

The regional pressure gradient function shows that the shallower coals are significantly underpressured and approach normal hydrostatic pressures as the coals become deeper, Figure 2-12.

## 2.5.4 Gas Content

The Basin Study assembled available gas content data and adsorption isotherms, appropriate for the low rank coals of the PRB, from the following sources:

- Past gas content data collected by the BLM and published gas content and isotherm data by industry and the USGS,
- Advanced Resources' own gas content and isotherm data collected for analogous low rank coals in other basins, and
- History matching (using COMET3) of alternative isotherms using long-term (4+year) gas and water production data in the PRB.



Figure 2-10. Cross-Section Showing Lateral Variation of Coalbeds in the Wyodak Coal Zone



Figure 2-11. Regional Pressure Gradient



## Figure 2-12. Reservoir Pressure Profile Used for PRB Study

The best fit coalbed methane isotherm was from actual gas content and isotherm data collected on an analogous overseas low rank coal basin, Figure 2-13. As a point of comparison, Figure 2-14 provides the average synthesized adsorption isotherm for coal in the PRB assembled from older data.

#### 2.5.5 Gas Saturation

The nature of early time water and gas production was used to establish whether the PRB coals were undersaturated, fully saturated or contained free gas in the pore space:

- A series of fourteen individual coal seams and partition data sets, shown on Table 2-1, were assembled involving gas and water production data from over 1,400 PRB CBM wells.
- History matching (using COMET3) of production data was used to establish the level of gas saturation and presence of free gas in the coal cleat and matrix system.



Figure 2-13. Gas Content Isotherm Used for Powder River Coalbed Methane



Figure 2-14. Average Synthesized Adsorption Isotherm for 41 Coal Samples From the PRB, Based on a Compilation of Data From Public and Private Sources

Overall, the study established that the coals are fully saturated with methane (at the reduced reservoir pressure conditions that generally exist in the basin) and that modest amounts of free gas exist in the matrix porosity and coal cleat (fracture) porosity systems in certain seam/partition data sets. However, operators report that low gas contents and severe undersaturation conditions may exist for certain deeper coals in the portions of the basin, south of Gillette. Collection and analysis of additional gas content data would help define their potential problem areas and seams in the basin.

Further discussion of the topics of gas content and gas saturation in the Powder River Basin is provided as Appendix A.

# 2.5.6 Coal Fracture and Matrix Porosity

History matching of water production was used to estimate the fracture and matrix porosity for the PRB coals:

- 1. In general, the coal cleat (fracture) porosity in the coals ranges from 0.1% to 1%, consistent with other data (The Big George coal in Partition #5 has an apparently higher than usual fracture porosity).
- 2. The matrix porosity for these low rank coals varies widely, ranging from 1% to 10%. Matrix porosity tends to increase for the deeper coals, such as the Wall, Pawnee, and Cache.

High coal matrix porosities would support the relatively high water production from otherwise thinner (25 to 30 feet) coal seams, such as the Wall. As an alternative explanation, some investigators have put forward the concept of aquifers in the Fort Union Formation as providing and supporting the high water production observed from PRB coals.

Some amount of water influx or aquifer leakage from associated sands no doubt exists in some portions of the basin. However, our assessment is that porosity in these low rank coals is the primary source of the produced water and that aquifer recharge, if and where it does exist, is relatively modest for the following reasons:

- First, high matrix porosity values have been documented for other low rank coals (such as the overseas low rank coal used for the gas sorption isotherm, discussed above). Seidle (2002), in his review of selected coalbed methane pilots, cites a value of 10% for the porosity of the Wyodak coal at the Rawhide Butte Field of the Powder River Basin. Cox (2000), in his assessment of aquifer controls on CBM in the PRB, used 5% for the Anderson-Wyodak coal.
- Second, the water production rates in the coalbed methane wells along the maturely developed eastern portion of the Powder River Basin (such as the Canyon coal wells Partition #4) have declined to about 20 to 30 barrels per day at the end of 3 years from about 300 barrels per day during year 1. And, some coal wells in the area have stopped producing any appreciable water. If aquifer leakage is occurring in this area, it would have to be low.

• Third, the pressure response and gas desorption rates would be considerably different for water held in coal porosity versus water influx from aquifer leakage. The assessment of gas production by reservoir simulation tended to support the coal matrix as the primary source of the produced water, although separating porosity source water from low levels of aquifer leakage would be difficult to establish.

## 2.5.7 Coal Permeability

In general, the coal cleat (fracture) permeability of PRB coals is favorable, ranging from 35 to 500 md. Coal matrix permeabilities are considerably lower and variable, ranging from 0.001 to 1.0 md. However, even the lower end of the range for cleat and matrix permeabilities for the coals in the PRB is sufficient to support reasonable gas recoveries (in 10 years) of 50 to 80+% of the gas in-place.

#### 2.6 Summary of Reservoir Properties

Table 2-4 provides a summary of the key reservoir properties established from the geologic study and history matching of 14 sets of coalbed methane data representing the combined well performance of 1,428 coalbed methane wells in the Powder River Basin. Additional information on individual coal seam reservoir properties is provided in Chapter 6.

Shown below is the average derived data on coal seam gas content, pressure, gas saturation and porosity for basin Partition #4.

Coal	Gas	Pressure	Free Gas	Saturation	Por	osity
Seam	Content	(Top of Coal)	Fracture	Matrix	Fracture	Matrix
	(cf/t)	(psi)	(%)	(%)	(%)	(%)
Anderson	40	141	8	10	0.2	1.5
Canyon	47	171	7	7	0.4	3.0
Wyodak	54	199	5	10	1.0	6.0
Cook*	67	257	0	1	0.1	2.4
Wall	84	340	0	0	1.0	10.0
Pawnee**	106	460	0	0	0.5	5.0
Cache**	121	558	0	0	0.5	5.0
* Based on extrap ** Based on extrap	olation from histor	ry-matched Cook c ry-matched Pawne	oal seam in Partiti e coal seam in Par	on #8. rtition #8.	-	

 Table 2-3.
 Average Data for Partition #4

in Coals	
River Bas	
or Powder	
operties fo	
servoir Pr	
. Key Re	
Table 2-4	

										Porosit	×	Water Satura	ation	Permeability (	(pm
Seam	Part	Area	# of Wells	Depth (Top) (ft)	Thickness (ft)	Spacing (A/w)	Pressure (top) (psi)	Gas Content (cf/cf)	Gas Content (cf/ton)	۴	E	۴	E	<b>4</b> -	E
Big G	е	T43-44N 74W	38	1,000	67.5	80	335	3.58	86	0.002	0.040	1.00	1.00	35.0	0.002
Anderson	4	T51N 73W	89	500	20.0	80	150	1.79	43	0.002	0.015	0.92	0.90	225.0	1.000
W yodak	4	T47-48 R72	159	541	78.0	40	163	2.73	65	0.010	0.060	0.95	0.90	500.0	1.000
Canyon	4 -	T52-51 R73	172	625	37.5	80	186 265	2.19	52	0.004	0.030	0.93	0.93	200.0	1.000
	4	MC / NIZCI	2	000	0.62	00	667	70.7	10	010.0	001.0	00.1	00.1	0.001	001.0
Big G*	S	1 WELL	-	1,260	150.0	80	451	4.33	104	0.010	0.100	1.00	1.00	250.0	0.001
Smith	ß	AVG	9	640	30.0	80	197	2.29	55	0.001	0.011	1.00	1.00	45.0	0.010
Anderson	80	T54 R76-77	261	650	52.5	80	200	1.80	43	0.002	0.015	1.00	0.78	175.0	0.001
Wall	80	AVG	107	963	30.0	80	300	3.22	11	0.010	0.095	1.00	1.00	42.0	1.000
Pawnee	ω (	AVG	19	1,055	33.0	88	358	3.70	68	0.005	0.050	1.00	1.00	125.0	1.000
Cook	×	T55N 75-76W	134	752	55.0	80	237	2.71	65	0.001	0.024	1.00	0.99	50.0	0.100
Anderson-Dietz	5	T57N R83-84W	191	650.0	22.5	80	200	2.30	55	0.005	0.025	0.98	0.98	450.0	1.000
Canyon-Monarch	1	T57N R83-84W	147	930.0	20.0	80	306	3.25	78	0.005	0.095	0.98	0.98	275.0	1.000
Cook-Carney	7	T57N R83-84W	65	1,050.0	30.0	80	356	3.68	88	0.010	0:080	0.99	0.99	150.0	1.000
Smith	ŝ	AVG	10	640	30.0	80	197	2.29	55	0.001	0.011	1.00	1.00	45.0	0.010
Anderson	4 0	T51N 73W	88	500	20.0	80	150	1.79	43	0.002	0.015	0.92	0.90	225.0	1.000
Anderson-Dietz	;, a	T57N R83-84W	9 16	650	27.5 27.5	8 8	200	2.30	43 55	0.005	0.025	0.98	0.78 0.98	450.0	1.000
Canyo <b>n</b> Canyon-Monarch	4 [	T52-51 R73 T57N R83-84W	172 147	625 930	37.5 20.0	80 80	186 306	2.19 3.25	52 78	0.004 0.005	0.030 0.095	0.93 0.98	0.93 0.98	200.0 275.0	1.000
W yodak	4	T47-48 R72	159	541	78.0	40	163	2.73	65	0.010	0.060	0.95	0.90	500.0	1.000
Big G Bin G*	<b>с</b> 10	T43-44N 74W 1 WFLI	- 38	1,000	67.5 150.0	80 08	335 451	3.58	86 104	0.002	0.040	1.00	00.1	35.0 250.0	0.002
) 1	<b>,</b>					3				200	2	2	20-	2.004	
Cook Cook-Carney	8 5	T55N 75-76W T57N R83-84W	134 65	752 1,050	55.0 30.0	80 80 80	237 356	2.71 3.68	65 88	0.001 0.010	0.024 0.080	1.00 0.99	0.99 0.99	50.0 150.0	0.100 1.000
Wall Wall	4 00	T52N 73W AVG	19 107	800 963	25.0 30.0	80 80 80	255 300	2.82	67 77	0.010 0.010	0.100 0.095	1.00	1.00 1.00	100.0 42.0	0.100
Pawnee	ø	AVG	19	1,055	33.0	80	358	3.70	89	0.005	0.050	1.00	1.00	125.0	1.000
* (17 wells modeled)	1														

# 3.0 COALBED METHANE RESOURCES

#### 3.1 Summary

The Powder River Coalbed Methane Basin Study estimates 61 Tcf of natural gas in-place, with 39 Tcf of this gas in-place being technically recoverable. The two reasons for the increased PRB coalbed methane resource in-place of 61 Tcf in this Basin Study are:

- *Larger Coal Volume Data Base.* The study includes extensive information on the deeper Fort Union coals prevalent in the basin; it compiles new data on the Wasatch coals on the western edge of the basin; and, it includes the shallower coals in the Montana portion of the PRB (although insufficient data was available for including the deeper Knoblock coal zone in the Montana portion of the PRB).
- *Free Gas and Higher Gas Contents*. The study identifies the presence of free gas in certain coal formations and establishes higher inherent gas content values for PRB coals than used by previous studies, both increasing the gas in-place over previous estimates.

The estimate of technically recoverable resources of 39 Tcf is based on reservoir simulation of 1,428 individual wells assembled into 14 history-matched "time zero" well clusters. These simulations are used to construct 142 "type wells" representative of the distribution in well performance (gas and water production) for 12 distinct coal seams in 12 basin partitions.

## 3.2 Coalbed Methane Resources

## 3.2.1 Gas In-Place

The distribution of the 61 Tcf of gas in-place ranges widely by basin partition and by coal seam:

- Basin Partition #5, in the center of the PRB, and where all of the major coal seams are present at favorable depths, holds over 25 Tcf of gas in-place.
- The Big George coal seam, that has extensive thickness in the southern and central portions of the PRB, holds over 14 Tcf of gas in-place, followed by the Canyon coal seam with nearly 9 Tcf of gas in-place.

Table 3-1 provides the partition and seam level tabulation for the coalbed methane gas in-place for the major coals in the Powder River Basin. (The Knoblock and other deeper coal seams are not included in these estimates.)

						Partiti	ons				
N	lajor Seams	1&2	3&12	4	5	6	7	8	9&10	11	TOTAL
1	Wasatch				181	460	292				933
2	Roland				96	375	2 4 9				720
3	Sm ith /Swartz				2,536		160	471			3,167
4	Anderson*	41	159	399	1,180	373	3 2 3	7 4 8	102	1,233	4,558
5	Canyon*	209	1,266	924	2,320	1,095	2 4 7	1,806	273	639	8,779
6	Wyodak*	756		891	250						1,897
7	Big George	544	6,618		6,763	928					14,853
8	Cook	154	210	447	3,056	693	401	2,281	381	214	7,837
9	Wall			441	2,252	196	210	1,894			4,993
10	Pawnee	473		567	4,004	1,273	254	1,201	210		7,982
11	Cache			545	2,696		679	493			4,413
12	Oedekoven**				180	7 5 7		298			1,235
	TOTAL	2,177	8,253	4,214	25,514	6,150	2,815	9,192	966	2,086	61,367

Table 3-1. Gas In-Place for Major PRB Coal Seams (Bcf)

"In certain basin partitions, such as Partitions #4, 5, and 6, certain of the townships in the partition contain the individual Anderson, Canyon and Cook coal seams; other townships in the partition contain the combined Anderson, Canyon and Cook seams called the Wyodak seam. \*\*Includes deep "wildcats."

Even with the extensive and detailed coal seam and township level mapping of the PRB coals, considerable uncertainty still remains in these resource estimates.

- First, only partial data exist on the volumes and location of the deep coals, because few wells have been drilled in the deeper portions of the basin. (New information would tend to increase the size of the in-place resource.)
- Second, localized areas of the basin may have encountered degassing of the coals. While this regional analysis indicates fully gas-charged coals, localized degassing of coals has been reported in other CBM basins. (Here, new information would tend to decrease the size of the in-place resource.)
- Third, coal seams with thickness of less than 20 feet are excluded from the resource estimate.
- Finally, considerable judgement is used in assigning a "name" to a particular coal seam, particularly where the Wyodak coal splits into sub-seams such as the Anderson and Canyon, which are major seams on their own. (Here, new information would shift the volume of resource among the seam, but would not appreciably affect the overall estimate.)

## 3.2.2 Technically Recoverable Resources

The distribution of the 39 Tcf of technically recoverable resources is shown on Table 3-2. Several insights emerge from the tabulation of data and reservoir simulation-based history matching of the well performance:

- *Recovery Efficiency With Depth.* Recovery efficiency of the gas in-place does not decline as severely as conventionally assumed for the deeper coals. Higher coal reservoir pressure and more favorable gas content tends to partially counter-balance the reduction in coal permeability. Even so, the technical recovery efficiencies for certain of the deeper coals still only range from 50 to 60% of the gas in-place.
- *Presence of Free Gas.* The upper group of Fort Union coals, including the Anderson, Canyon and Wyodak, tend to have early gas production due to the presence of free gas within the coal cleat (fracture) system and in the coal matrix porosity. In addition to increasing the resource in place, the presence of free gas promotes improved relative permeability to gas and an earlier peak in gas production.
- *Well Spacing*. Where the coals have higher permeability and free gas, wells drilled on 40 to 80 acre spacings produce the bulk of their economically recoverable gas relatively quickly, in 6 to 7 years.

						Partiti	ons				
ħ	lajor Seams	1&2	3&12	4	5	6	7	8	9&10	11	TOTAL
1	Wasatch				1 4 3	367	2 3 1				7 41
2	Roland				76	237	197				510
3	Sm ith /Swartz				1,733		95	372			2,200
4	Anderson	35	115	287	829	223	2 2 7	526	90	1,086	3,418
5	Canyon	181	874	798	1,501	661	1 4 9	1,558	2 4 6	575	6,543
6	Wyodak	553	÷	768	215						1,536
7	Big George	319	2,907		3,514	489					7 ,22 9
8	Cook	1 2 2	166	352	1,808	383	206	1,799	337	189	5,362
9	Wall			353	1,353	108	102	1,230			3,146
10	Pawnee	422		506	2,322	625	136	1,071	187		5,269
11	Cache			486	1,323		3 3 3	285			2,427
12	Oedekoven*				8 9	372		173			634
	TOTAL	1,632	4,062	3,550	14,906	3,465	1,676	7,014	860	1,850	39,015

#### Table 3-2. Technically Recoverable Resources for Major PRB Coal Seams (Bcf)

\*Includes deep "wildcats."

#### 3.3 In-Place and Technically Recoverable PRB CBM Resources, by Basin Partition

Tables 3-3 through 3-11 provide additional detail on in-place and technically recoverable PRB coalbed methane by basin partition. These tables display the areal extent (number of townships), depth, coal thicknesses, and gas content used to establish the gas in-place for each major coal seam. The tables also provide estimates of technically recoverable CBM resources by coal seam.

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable (Bcf)
Anderson	1	450	25	39	40	30
Canyon	2	575	48	51	210	180
Wyodak	5	440	86	42	760	560
Big George	2	863	90	86	550	320
Cook	2	740	30	65	150	120
Pawnee	5	1,336	22	108	470	420
Totals					2,170	1,630

 Table 3-3. In-Place and Technically Recoverable CBM, Partitions #1 and #2

\* Top of coal

 Table 3-4. In-Place and Technically Recoverable CBM, Partitions #3 and #12

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable (Bcf)
Anderson	1	800	55	70	160	110
Canyon	9	970	43	81	1,260	870
Big George	11	1,280	100	107	6,620	2,910
Cook	2	1,030	30	86	210	170
Totals					8,250	4,060

\* Top of coal

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Anderson	6	450	30	40	400	290
Canyon	12	540	35	47	920	800
Wyodak	6	601	73	54	890	770
Cook	5	790	31	67	450	350
Wall	5	1,020	27	84	440	350
Pawnee	5	1,295	27	106	570	510
Cache	5	1,550	23	121	540	480
Totals	44				4,210	3,550

 Table 3-5. In-Place and Technically Recoverable CBM, Partition #4

\* To top of coal

Table 3-6.	<b>In-Place</b> and	<b>Technically Reco</b>	verable CBM, Partitio	n #5
------------	---------------------	-------------------------	-----------------------	------

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Felix	4	530	24	46	180	140
Roland	2	540	25	47	100	80
Smith	18	820	39	70	2,310	1,560
Swartz	2	740	43	63	220	180
Anderson	9	1030	38	86	1,180	830
Canyon	16	1060	39	88	2,320	1,500
Big George	16	1280	97	107	6,760	3,510
Wyodak	2	1000	73	85	250	210
Cook	17	1320	40	109	3,060	1,810
Wall	16	1500	32	120	2,250	1,350
Pawnee	18	1710	41	137	4,000	2,320
Cache	14	2020	32	159	2,700	1,320
Wildcat	1	2190	45	101	180	90
Totals					25,510	14,910

\* To top of coal

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Cameron	1	700	20	60	50	40
Felix	1	750	30	63	140	110
Murry	1	800	50	69	80	60
Ucross	3	790	23	66	190	150
Roland	5	1,060	21	86	370	240
Anderson	3	1,220	30	99	370	220
Canyon	8	1,520	30	123	1,090	660
Big George	2	1,670	85	136	930	490
Cook	2	1,860	58	147	690	380
Wall	1	1,630	40	130	200	110
Pawnee	4	2,000	44	158	1,270	620
Wildcat	4	2,640	25	191	760	370
Totals					6,150	3,460

 Table 3-7. In-Place and Technically Recoverable CBM, Partition #6

\* To top of coal

Table 3-8.	<b>In-Place and</b>	Technically	Recoverable	CBM.	Partition #7
				<i>– – – , – , – , – , – , – , – , – , – ,</i>	

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Wasatch	6	540	25	47	290	230
Roland	3	820	27	70	250	200
Smith	2	1,180	20	96	160	90
Anderson	5	910	21	75	320	230
Canyon	2	1,500	25	120	250	150
Cook	2	2,300	28	178	400	210
Wall	1	2,500	30	186	210	100
Pawnee	1	2,050	40	160	250	140
Cache	3	2,623	30	190	680	330
Totals					2,820	1,680

\* To top of coal

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Smith	8	430	33	38	380	300
Swartz	2	580	21	49	90	70
Anderson	9	600	35	51	750	530
Canyon	19	620	37	54	1,810	1,560
Cook	22	730	39	62	2,280	1,800
Wall	21	960	30	80	1,890	1,230
Pawnee	11	1,060	33	87	1,200	1,070
Cache	4	1,550	27	123	490	290
Oedekoven	2	2,560	20	188	300	170
Totals					9,190	7,020

 Table 3-9. In-Place and Technically Recoverable CBM, Partition #8

\* To top of coal

Table 3-10.	<b>In-Place</b> and	Technically	<b>Recoverable CBM</b>	. Partitions #9 and #10
1 4010 0 100	III I luce und	1 commonly		y i ai thui his hy and hit

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable (Bcf)
Deitz (Anderson)	2	250	49	25	100	90
Monarch (Canyon)	7	470	24	41	280	250
Carney (Cook)	7	650	23	55	380	330
Pawnee	3	1,080	20	88	210	190
Totals					970	860

\* Top of coal

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable (Bcf)
Deitz #1 (Anderson)	5	910	24	75	510	450
Dietz #2	5	680	24	58	330	290
Dietz #3	6	1,030	22	84	390	340
Monarch (Canyon)	8	1,070	24	88	640	570
Carney (Cook)	3	1,030	23	84	220	190
Totals					2,090	1,850

 Table 3-11. In-Place and Technically Recoverable CBM, Partitions #11

\* Top of coal

#### 3.4 Estimating Gas and Water Production

The gas and water production estimates for the study were developed using the following six steps:

- 1. *Geologic Model*. The geologic model (discussed above) provided the key reservoir properties of coal seam depth, thickness, gas content and reservoir pressure.
- 2. *Well Performance*. The gas and water production data base (starting with over 8,000 CBM wells in the PRB) was organized by coal seam and by partition and then normalized by time (using "time zero" plots) to provide a foundation of actual CBM well performance. For example, Figure 3-1 provides the "time-zero" plot for "on average" wells completed in the Wyodak coal seam in a 2-township area of Partition #4. (See Section 6.4 for further discussion.)
- 3. *History Matching*. History matching of gas and water production (from 1,428 PRB CBM wells, organized into 14 distinct coal seam and basin partition sets (shown on Table 3-12) was used to establish:
  - Permeability (matrix, fracture)
  - Coal porosity (matrix, fracture)
  - Gas and water saturation
  - Confirmation of reservoir pressure and gas content

For example, Figure 3-2 provides the gas and water production history match for the "average" well completed in the Wyodak coal seam in the 2-township area of Partition #4, shown in Figure 3-1. (See Section 6.4 for further discussion.). Table 3-13 summarizes the reservoir properties and expected gas and water recoveries for the 14 sets of history-matched PRB coalbed methane wells.



Figure 3-1. Wyodak Coal Seam Time Zero Plot

Table 3	<b>B-12</b> .	Number and	Nature o	f CBM	Wells	for Hist	ory Matchi	ng
							•/	_

	Partitions <sup>4</sup>						
Coal Seam	3	4	5	8	11		
Smith			10 <sup>2</sup>				
Anderson		89 <sup>1</sup>		<b>261</b> <sup>1</sup>	191 <sup>1</sup>		
Canyon		172 <sup>1</sup>			147 <sup>1</sup>		
Wyodak		159 <sup>1</sup>					
Big George	38 <sup>1</sup>		17 <sup>3</sup>				
Cook				134 <sup>1</sup>	65 <sup>1</sup>		
Wall		<b>1</b> 9 <sup>1</sup>		107 <sup>2</sup>			
Pawnee				19 <sup>2</sup>			

Intensely drilled township area.
 Time zero well in partition.
 All Big George wells in Sec. 16, 48N 77W.
 Includes partitions with significant numbers of CBM wells, with sufficient production data for history matching.



Figure 3-2. Wyodak Type Well History Match

	В	С	D	E	F	G	Н		J	К	L	М	Ν	0	Р	Q	R
				# of	Donth	Thicknose	Spacing	Droceuro	Pressure	Comparison	Gas	Gas	Porosity	Porosity			Borm (md)
	Seam	Part	Area	Wolls	(Top) ft	(ft)	(A/W)	(ton) nei	Gradient,	to Regional	Content	Content	f	m	<u>Sw - f</u>	<u>Sw - m</u>	f
2				110113	<u>(10)/10</u>	<u></u>	<u></u>	<u>(top/psi</u>	psi/ft	Prs Grad	(cf/cf)	(cf/ton)	<u>.</u>				-
3	Big G	3	T43-44N 74W	38	1,000	67.5	80	335	0.320	Same	3.58	86	0.002	0.040	1.00	1.00	35.0
4											1 =0						
5	Anderson	4	T51N 73W	89	500	20.0	80	150	0.270	Same	1.79	43	0.002	0.015	0.92	0.90	225.0
6	Wyodak	4	T47-48 R72	159	541	78.0	40	163	0.274	Same	2.73	65	0.010	0.060	0.95	0.90	500.0
(	Canyon	4	152-51 R/3	1/2	625	37.5	80	186	0.273	Same	2.19	52	0.004	0.030	0.93	0.93	200.0
8	wall	4	152N 73W	19	800	25.0	80	255	0.300	Same	2.82	67	0.010	0.100	1.00	1.00	100.0
9	Dia C	-		1	1 000	150.0		454	0.240	Cama	4.00	104	0.010	0.100	1.00	1.00	250.0
10	Big G	5	I WELL	10	1,200	150.0	80	401	0.346	Same	4.33	104	0.010	0.100	1.00	1.00	250.0
10	Smun	5	AVG	10	640	30.0	00	197	0.264	Same	2.29	55	0.001	0.011	1.00	1.00	45.0
12	Andorson		TE4 D76 77	261	650	E 2 E	00	200	0.295	Sama	1 00	42	0.002	0.015	1.00	0.79	175.0
14	Mall	0	104 K/0-//	201	000	32.5	80	200	0.200	Jower	2.00	43	0.002	0.015	1.00	1.00	173.0
14	Dawnee	0	AVG	107	1 055	33.0	80	358	0.290	Same	3.22	80	0.010	0.095	1.00	1.00	42.0
10	Cook	8	T55N 75 76W	13/	752	55.0	80	237	0.325	Same	2 71	65	0.003	0.030	1.00	0.00	50.0
17	COOK	0	1331473-7044	134	132	33.0	00	201	0.235	Jame	2.71	05	0.001	0.024	1.00	0.33	50.0
18	Anderson Dietz	11	T57N D83 84W	101	650.0	22.5	80	200	0.285	Same	2 30	55	0.005	0.025	0.08	0.08	450.0
10	Canvon-Monarch	11	T57N R83-84W	147	930.0	20.0	80	306	0.203	Same	3.25	78	0.005	0.025	0.98	0.98	275.0
20	Cook-Carney	11	T57N R83-84W	65	1.050.0	30.0	80	356	0.325	Same	3.68	88	0.010	0.080	0.99	0.99	150.0
21																	
22																	
23																	
24	Anderson	4	T51N 73W	89	500	20.0	80	150	0.270	Same	1.79	43	0.002	0.015	0.92	0.90	225.0
25	Anderson	8	T54 R76-77	261	650	52.5	80	200	0.285	Same	1.80	43	0.002	0.015	1.00	0.78	175.0
26	Anderson-Dietz	11	T57N R83-84W	191	650	22.5	80	200	0.285	Same	2.30	55	0.005	0.025	0.98	0.98	450.0
27																	
28	Big G	3	T43-44N 74W	38	1,000	67.5	80	335	0.320	Same	3.58	86	0.002	0.040	1.00	1.00	35.0
29	Big G	5	1 WELL	1	1,260	150.0	80	451	0.346	Same	4.33	104	0.010	0.100	1.00	1.00	250.0
30																	
31	Canyon	4	T52-51 R73	172	625	37.5	80	186	0.273	Same	2.19	52	0.004	0.030	0.93	0.93	200.0
32	Canyon-Monarch	11	T57N R83-84W	147	930	20.0	80	306	0.313	Same	3.25	78	0.005	0.095	0.98	0.98	275.0
33																	
34	Cook	8	T55N 75-76W	134	752	55.0	80	237	0.295	Same	2.71	65	0.001	0.024	1.00	0.99	50.0
35	Cook-Carney	11	T57N R83-84W	65	1,050	30.0	80	356	0.325	Same	3.68	88	0.010	0.080	0.99	0.99	150.0
36																	
37	Pawnee	8	AVG	19	1,055	33.0	80	358	0.325	Same	3.70	89	0.005	0.050	1.00	1.00	125.0
38																	
39	Smith	5	AVG	10	640	30.0	80	197	0.284	Same	2.29	55	U.001	0.011	1.00	1.00	45.0
40	Mall		TEON 7014/	10	000	25.0		055	0.000	Como	2.02	07	0.040	0.400	1.00	1.00	100.0
41	Wall	4	152N / 3W	19	800	25.0	80	255	0.300	Same	2.82	6/	0.010	0.100	1.00	1.00	100.0
42	vvail	8	AVG	107	963	30.0	80	300	0.296	Lower	3.22	11	0.010	0.095	1.00	1.00	42.0
43	Wyodak	4	T47 48 D72	150	541	78.0	40	162	0.274	Same	2 7 2	6E	0.010	0.060	0.05	0.00	500.0
44	vvyouak	4	14/-40 11/2	159	541	/0.0	40	103	0.274	odifie	2.73	60	0.010	0.000	0.95	0.90	0.000

Lable & Let Summing Lesuns for Lite Counce incomments instory francement
--

- 4. *Reservoir Simulation*. Advanced Resources' COMET3 reservoir simulator, a triple porosity and triple permeability finite difference model specifically developed for coalbed methane production and reserve assessments, was used for history matching and establishing 14 "type wells" reflecting the geologic and reservoir diversity encountered in PRB coals.
- 5. *Production Forecast.* The history-matched "type wells" were extended in time (using COMET3) to provide 10-year gas and water rates and estimates of ultimate recovery. For example, Figure 3-3 provides the 10-year reservoir simulation-based forecast for gas and water production for the Wyodak type well in Partition #4, as presented previously in Figures 3-1 and 3-2.



Figure 3-3. 10-Year Simulation of Gas and Water Production for Wyodak Type Well

6. *Type Wells.* The 14 PRB "type wells" were scaled using actual depth, thickness and gas content to develop 142 individual "type wells" to reflect average, high and low performance for each major coal seam in each basin partition, shown on Table 3-14. For example, the history-matched set of 89 Anderson wells in T51N T3W of Partition #4 (shown previously on Table 3-13), with a coal thickness of 20 feet, were scaled to represent the average 30 foot coal thickness "type well" for the Anderson coal seam in Partition #4 (as shown in Table 3-5). The expected average, high and low well performance was based primarily on the variability in coal thickness in the partition. The average well represents the average coal thickness (and other reservoir properties) value and the low and high wells represent the lowest and highest 25% of the coal thickness in the townships of the partition.

		Partitions									
Ν	lajor Seams	1&2	3&12	4	5	6	7	8	9&10	11	TOTAL
1	Wasatch				1	4	3				8
2	Roland				1	1	3				5
3	Smith/Swartz				4		1	4			9
4	Anderson	1	1	3	3	1	3	3	1	9	25
5	Canyon	2	3	3	3	3	1	3	3	3	24
6	Wyodak	3		3	1						7
7	Big George	1	3		3	1					8
8	Cook	1	1	3	3	1	1	3	3	3	19
9	Wall			3	3	1	1	3			11
10	Pawnee	1		3	3	3	1	3	1		15
11	Cache			3	3		1	3			10
12	Oedekoven*					1					1
	TOTAL	9	8	21	28	16	14	23	8	15	142

Table 3-14. Number of CBM Type Wells for Basin Assessment

\* Includes deep "wildcats."

#### 4.0 COSTS OF PRB CBM DEVELOPMENT

This section presents the cost model used for assessing the economics of Powder River Basin (PRB) coalbed methane (CBM) development. The section contains:

- A summary presentation of the basic capital, operating and maintenance, gas transportation and compression, and water disposal costs,
- A discussion of other financial considerations such as royalties, production taxes, and basin differentials,
- More detailed discussions of CBM capital costs,
- More detailed discussion of CBM O&M costs, and
- A discussion of water disposal capital and O&M costs for four water management alternatives—surface disposal, infiltration impoundment, shallow re-injection and active treatment using reverse osmosis.

#### 4.1 Basic Cost Model

#### 4.1.1 Introduction

This section provides the basic capital and operating cost model for Powder River Basin coalbed methane development. The model attempts to reflect a series of "typical" CBM wells in the basin, with cost variability determined by well depth, geographic location and volume of gas and water production. In reality, the variability in costs is much greater than can be defined by these "typical" CBM wells and the three factors (depth, location, and gas and water production) that are used to capture a portion of this variability. As such, the cost and well performance information are intended for use on a regional rather than a site or prospect-specific basis.

The authors are deeply indebted to the many sources of cost information made available for this study. These include contributions of cost data from the producers and service companies in the basin, detailed cost data from Advanced Resources' past studies of coalbed methane in the Powder River Basin and other coal basins, and the cost surveys and comments by the Producers Association of Wyoming. We welcome suggestions and data that would improve the quality of the information and the cost model.

## 4.1.2 Capital Costs for PRB CBM Well

The basic capital costs for a PRB CBM well include outlays for land, permits, drilling and completion, and infrastructure (capital costs for water disposal are presented later). These costs vary considerably by well depth and location. For example purposes, we will use a Powder River Basin coalbed methane well at 600 feet of depth, spaced on 80 acres, with 2 wells per pad. Capital costs are per well, assuming a 16-well, 8-pad development unit. Gas treating and compression is assumed, provided by a third party contract. Additional detail on each of the cost items and how costs vary with depth are provided in subsequent sections of this report.

The basic capital costs for the above described example PRB CBM well are estimated at \$88,000, as shown below.

Cost Item	Capital Costs
Land Costs and Permits	\$13,000
Well Drilling and Completion (@600 feet)	48,180
Water Gathering*	10,210
Electric Power, inc. cable**	8,450
Gas Gathering***	7,820
Miscellaneous	340
Total	\$88,000

Table 4-1. Capital Costs for PRB CBM Well

\* Allocated based on small diameter water gathering piping of 2,000 feet per well (including common trenching and survey for water, gas, and electrical cable), central water transportation (2 lines) of 10,000 feet, right of way for 42,000 feet, two surface pumps and contingency insurance and other costs of 10%.

- \*\* Allocated based on central 3-phase power installation costs of \$75,000 per unit, electrical cable of 2,000 feet per well, and contingency, insurance and other costs of 10%.
- \*\*\* Allocated based on small diameter gas gathering piping of 2,000 feet per well, central gas transportation (2 lines) of 10,000 feet, and contingency, insurance and other costs of 10%.

## 4.1.3 O&M Costs for PRB CBM Well

The basic lease and well operating and maintenance (O&M) costs for a Powder River coalbed methane well varies by year of production, with higher costs during the initial years because of more frequent well enhancements and pump replacements. Additional detail on these costs is provided in subsequent sections of this report.

For illustrative example purposes, assuming CBM recovery of 0.3 Bcf (gross) per well, the O&M costs are \$0.215 per Mcf and G&A costs are \$0.043 per Mcf, for total O&M/G&A costs of \$0.258 per Mcf. Additional O&M costs are incurred for water management and disposal, as discussed later.

	O&M Costs/Well								
	Basic O	&M*	O&M Inc.G&A						
	Annual	Monthly	Annual	Monthly					
Year 1	\$16,700	\$1,390	\$20,040	\$1,670					
Years 2 - 4	\$7,500	\$625	\$9,000	\$750					
Years 5 - 10	\$4,200	\$350	\$5,040	\$420					
TOTAL (Years 1 - 10)	\$64,400	\$644	\$77,280	\$773					

## Table 4-2. O&M Costs for PRB CBM Well

\*A G&A charge of 20% for engineering, accounting, legal and other indirect costs is added to basic well costs.

## 4.1.4 Gas Transportation, Compression, and Fuel Use

The costs of gas treatment, compression and transportation are subtracted from the PRB netback price to establish a PRB CBM wellhead price. The costs will vary, depending on the gathering system charges for transporting natural gas from the compressor to the Colorado Interstate Gas (CIG), or another hub, and on the nature and extent of contracted third-party compression. These costs depend on the location of the CBM development in the PRB, as follows:

- A charge of \$0.43 per Mcf is used for third-party compression and dehydration (assuming no lease compression), and for transportation for the central and southern portions of the PRB (Partitions #1, 2, 3, 4, and 5).
- A charge of \$0.57 per Mcf is used for third-party compression and dehydration (assuming no lease compression), and for transportation for the northeast and southwest portions of the PRB (Partitions #6, 8, and 9).
- A charge of \$0.77 per Mcf is used for third-party compression and dehydration (assuming no lease compression), and for transportation for the northwest and western portions of the PRB (Partitions #7, 10, 11 and 12).

A fuel adjustment ("shrinkage") for operating gas powered compressor stations, estimated at 4 to 6% of gross production, is subtracted from the sales volume. A second fuel adjustment ("shrinkage"), involving the BTU adjustment for CBM, generally 2 to 8% (to account for 920 to 980 Btu content gas), is also subtracted from the sales volume.

## 4.1.5 Water Disposal Alternatives

*Alternatives*. A series of alternatives are being used or considered for CBM water disposal in the Powder River Basin, including:

• Untreated or passively treated water with surface discharge.

- Infiltration impoundment with enhanced evaporation and/or land application.
- Shallow re-injection of the produced water.
- Actively treated water with infiltration, evaporation, land application, and/or surface discharge, and disposition of the residual concentrate by trucking or deep re-injection.

Deep re-injection of the untreated, relatively high-quality CBM produced water would constitute a loss of a valuable resource and thus has not been included among the water disposal alternatives in this study.

*Capital Costs*. The capital costs for the alternative CBM water disposal options add from \$1,400 to \$35,200 per well, depending on the water management alternative selected, as shown for the example well below.

Water Disposal Costs Capital Costs/Well O&M Costs/Bbl.\* Water Disposal Surface Discharge \$1,400 \$0.02 Infiltration Impoundment \$10,300 \$0.06 Shallow Re-Injection \$15,150 \$0.06 Active Treatment w/Disposal of **Residual Concentrate**  Trucking \$19,600 \$0.24 Deep Re-Injection \$35,200 \$0.14

 Table 4-3. Capital Costs for Alternate Methods of Water Disposal

\* Per barrel of water produced for a "typical" CBM well producing 320 barrels per day (average) during the first 2 years.

O&M Costs. The operating costs of alternative CBM water disposal options will add from \$0.02 to \$0.25 per barrel of produced water to basic well and lease O&M costs, depending on the water management alternative selected.

## 4.1.6 Other Considerations

*Royalties*. Royalty payments for PRB CBM production depend on mineral ownership, as set forth below:

- Royalties on federal lands are 12.5%.
- Royalties on state lands are 16.7%.
- Royalties on private lands range from 15% to 20%.

*State Severance and Ad Valorem Taxes*. State and county tax payments for PRB CBM production are state specific, as set forth below:

• Wyoming severance and ad valorem taxes are 12%.

• Montana severance taxes are 9.3%.

## 4.1.7 Basin Differentials

Because of higher transportation costs and other market conditions, the gas price at the CIG (or another Wyoming/Rocky Mountain) hub is discounted from a marker price, as set by the Henry Hub or NYMEX (commonly called the "basin differential"). As of mid-June 2002, with the Henry Hub gas price at \$3.11 per MMBtu, the Wyoming Pool and the Opal hub are both at \$1.33 per MMBtu, for a basin differential of \$1.78 per MMBtu.

The economic model assumes that the long-term basin differential between Henry Hub and Rocky Mountain hubs reverts back to a historically-based value of \$0.80 per MMBtu, as published by Petrie Parkman & Co. (October 2000). Sensitivity cases have been run to examine the effects of higher basin differentials.

# 4.2 Discussion of CBM Development Capital Costs

# 4.2.1 Land Costs and Permits

Regular land and permit costs for CBM development in the Powder River Basin include the following:

- Mineral lease purchase and maintenance.
- WOGCC hearing, division orders, and permits.
- DEQ, State Engineer Office and BLM permits.

The costs for water disposal permits are included later.

The costs for mineral leases is \$200 per acre; the costs for regular permitting and studies is \$5,000 for an 80-acre well pad. For a federal lease, additional costs are required for NEPA and other permitting studies, estimated to cost an additional \$10,000 for an 80-acre well pad. Assuming approximately one-half of the leases are federal, this would add \$5,000 of costs for an average permit.

The total land and permit costs for an 80-acre well pad are estimated at \$26,000. With two wells per pad, the cost per CBM well is \$13,000.

## 4.2.2 Well Drilling and Completion

Well drilling and completion costs are governed primarily by well depth, assuming single zone coal seam completions. The intangible (expensed) and tangible (capitalized) drilling and completion costs for two representative PRB CBM wells, one at 500 feet and one at 850 feet, are provided below:

	Coal Seam Depth			
	500 feet	850 feet		
Well Drilling Costs	\$28,200	\$36,500		
Intangible	24,400	30,500		
Tangible	3,800	6,000		
Well Completion Costs	\$12,800	\$14,300		
Intangible	4,700	4,700		
Tangible	8,100	9,600		
TOTAL*	\$41,000	\$50,800		

 Table 4-4.
 Sample Tangible and Intangible Costs for Two PRB CBM Wells

\* Contingency, insurance costs and other costs, estimated at 10% ,are added to the above well D&C costs.

A significant number of the cost items, such as site preparation, rentals, wellhead, and gas/ water metering, are relatively insensitive to differences in well depth. Other cost items, such as production casing, tubing, and the pumping system, are directly related to well depth.

Based on the itemization of fixed and variable costs, the drilling and completion cost equation for a shallow (less than 1,000 foot) PRB CBM well is as follows:

(\$27,000 + \$28(WD)) \* 1.10where: WD is well depth  $\leq 1,000$  feet

As well depth increases, well drilling and completion costs rise to account for the extra costs involved with increasing depth. Based on experiences in the PRB and other CBM basins, we would estimate the cost equation for deeper, 1,000- to 3,000-foot CBM wells as follows:

(\$27,000 + \$28(1,000) + \$56 (WD-(1,000)) \* 1.10 where: WD is well depth <3,000 feet

Using the above equation, the well drilling and completion costs for the example 600-foot PRB CBM well and two deeper PRB CBM wells, one at 1,500 feet and one at 2,000 feet, are calculated as follows:

(\$27,000 + \$28(600)) \* 1.10 = \$48,180(\$27,000 + \$28,000 + \$56(500)) \* 1.10 = \$91,300(\$27,000 + \$28,000 + \$56(1,000)) \* 1.10 = \$122,100

Additional details on specific well drilling and completion costs are provided below.
	Well Depth	500'	850'
Drilling Costs			
Intangible Drilling Costs		\$24,400	\$30,500
Site Prep, Permit, Survey and ROW		3,700	3,700
Drilling Rig, Bits, Fluids		12,600	16,200
Cementing		4,200	4,400
Logging		700	800
Supervision (Drilling, Geologic)		2,400	3,600
Other		800	1,800
Tangible Drilling Costs		\$3,800	\$6,000
Surface Casing (9-5/8" @ \$10/ft)		600	850
Production String (7" @ \$5.50/ft)		2,750	4,300
Wellhead		<u>450</u>	<u>450</u>
Completion Costs			
Intangible Completion Costs		\$4,700	\$4,700
Supervision/Labor		2,400	2,400
Enhancement		1,200	1,200
Completion Rig		500	500
Water Handling		600	600
Tangible Completion Costs		\$8,100	\$9,600
Tubing (2" @ \$1.50/ft)		800	1,300
Pump, Motor, Cable		2,500	3,500
Electrical Controller/Transducer		2,000	2,000
Wellhead, Flowline Fittings		1,000	1,000
Gas and Water Metering		1,800	1,800
	Total	\$41,000	\$50,800

## Table 4-5. Additional Drilling and Completion Costs for Two PRB CBM Wells

## 4.2.3 Infrastructure Costs

*Basic Water Handling Facilities.* The facilities for gathering and transporting produced CBM water includes a pump and a water metering system (already included in well completion costs) plus small diameter (3 inch) polyethylene pipe connected to the tubing of the well. The polyethylene pipe is placed underground in a common trench from the wellhead to a point of common collection. A second, larger diameter (6 inch) polyethylene pipe transports the gathered water to a point of discharge involving a natural drainage outlet or a containment facility. For purposes of the cost estimate, the following assumptions are used:

- Well pads are placed on 80-acre spacing; on average, two wells exist per well pad; 16 wells (8 well pads on one 640-acre section) are linked together with an underground gathering and piping system.
- For cost estimation purposes, each well initially produces 400 BWD (in year 1) declining to 240 BWD in year 2 and declining by 25% each subsequent year. Total water production is 470,000 barrels per well for the 10 years of a well's life. (For this example well, average water production is about 4 gpm (137 barrels per day) for 10 years.)
- Approximately 2,000 feet of 3-inch polyethylene pipe is required for each well; 2 lines, each using approximately 5,000 feet of 6-inch polyethylene pipe, link the 16-well unit to 2 water disposal sites.
- Approximately 32,000 feet of common trenching is required for water gathering (as well as the electrical cable and small-diameter gas-gathering lines) and 10,000 feet of common trenching is required for water transportation (as well as for gas transmission).
- The cost for trenching and the survey is estimated at \$2.15 per foot; the cost of the polyethylene pipe is estimated at \$0.50 to \$0.70 per foot; and, the cost for right of way (ROW) is estimated at \$0.60 per foot.

The cost of the water gathering and subsurface piping system for a 16-well unit is estimated at \$163,350 or \$10,210 per well, based on the following:

•	Trenching and Survey: (42,000 ft @ \$2.15 ft)	=	\$ 90,300
•	Water Gathering: 3 inch poly pipe (32,000 ft @ \$0.50/ft.)	=	\$ 16,000
•	Water Transport: 6 inch poly pipe (10,000 ft @ \$0.70/ft.)	=	\$ 7,000
•	Surface Pump: (2 units @ \$5,000/unit)	=	\$ 10,000
•	Right of Way: (42,000 ft. @ \$0.60/ft.)	=	\$ 25,200
•	Contingency, insurance, etc. (@10%)	=	<u>\$ 14,850</u>
			\$163.350

Operating and maintenance costs for the water gathering and transportation system, including electric power, surface pump maintenance and other costs, are included in the O&M costs for surface discharge, are discussed later.

*Electric Power*. The costs of providing three-phase electric power and electrical cable to a 16-well unit (without trenching and survey) are as follows:

	Total	\$135,300
•	Contingency, insurance, etc. (@ 10%)	12,300
		\$123,000
•	Electric Cable (32,000 ft. @ \$1.50/ft.)	48,000
•	Central 3-Phase Power*	\$ 75,000

\* Costs can range from \$50,000 to \$100,000, depending on location.

Based on 16 wells, the cost per well is estimated at \$8,450.

*Gas Gatherings*. The costs of providing gas gathering and central gas transmission for the 16-well unit to a central compressor (without trenching and survey) are as follows:

	Total	\$125,180
•	Contingency, insurance, etc. (@10%)	11,380
		\$113,800
•	Gas Transmission: (10,000 ft, 12" @ \$8.50/ft.)	85,000
•	Gas Gathering: (32,000 ft., 4" @ \$0.90/ft.)	\$ 28,800

Based on 16 wells, the cost per well is estimated at \$7,820.

## 4.3 Discussion of CBM Well O&M Costs

## 4.3.1 O&M Costs for PRB CBM Well

Well and lease operating and maintenance (O&M) costs in the PRB are for electricity, wages for the pumper and miscellaneous site maintenance. In addition, particularly during the initial years of operation, CBM wells require periodic replacement of the downhole water pumping system and remediation.

The cost model assumes two pump replacements and a well workover during the first year of operation, an annual pump replacements during the next three years of operation (but no additional well workover), and annual pump replacement with a smaller capacity pump during the final 6 years of operation.

The costs for water lifting capacity depends on well depth and the water rate, as provided below:

Pump Size (bwpd)*	Pump Cost (\$)	Rig (\$)**
171	1,100	500
342	1,365	500
684	2,115	500
1,028	2,865	500
1,371	3,696	500

 Table 4-6.
 Pump Replacement Costs

\* Pump size of 171 to 684 bwpd are sufficient for well depths from 300 to 1,000 feet; pump size 1,028 to 1,371 bwpd are required for well depths below 1,000 feet.

\*\* The cost for the workover rig assumes replacements of two pumps per day.

The annual O&M costs for electricity are scaled by water production rates of the CBM well, with 305 barrels per day (average for the year) incurring \$3,050 annual costs for electricity.

The cost of replacement plumps is scaled by well depth and varies in time by changing waterletting capacity requirements. The annual cost for pump replacement for well depths from 300 to 1,000 feet is provided above. The cost for pump replacement for well depths below 1,000 feet is established by multiplying the pump replacement costs for 1,000-foot wells by the following cost scaling factor:

- Pump Replacement Cost (for 1,000' well) \*  $(WD/1,000')^2$
- For WD of 1,000' to 3,000'

The annual and monthly direct well and lease O&M costs for a PRB CBM well at 600 feet of depth and producing 305 barrels of water per day in year 1 (declining with time), are provided below, by year of operation:

Year 1	Annual	Monthly
Electricity	\$3,050	
Pumper	1,140	
Workover*	6,270	
1 <sup>st</sup> Pump Replacement	2,620	
2 <sup>nd</sup> Pump Replacement	2,620	
Annual ROW	700	
Misc.	<u>300</u>	
Total	\$16,700	\$1,390
***Total w/G&A	\$20,040	\$1,670
<u>Year 2-4</u>		
Electricity****	\$1,500	
Pumper	1,140	
Pump Replacement	1,860	
Workover**	2,000	
Annual ROW	700	
Misc.	<u>300</u>	
Total	\$7,500	\$625
Total w/G&A	\$9,000	\$750
Years 5-10		
Electricity****	\$480	
Pumper	1,140	
Pump Replac.	1,600	
Annual ROW	700	
Misc.	<u>280</u>	
Total	\$4,200	\$350
Total w/G&A	\$5,040	\$420

\* Each well is assumed to require one re-enhancement to restore productivity during the first year.

\*\* One out of three wells is assumed to require a clean-out during their second year.

\*\*\* A G&A cost of 20% is added to the well and lease O&M costs, annual and monthly costs are rounded.

\*\*\*\* Electricity costs are scaled based on annual water production.

## 5.0 ECONOMICS OF POWDER RIVER COALBED METHANE WITH ALTERNATIVE WATER MANAGEMENT OPTIONS

## 5.1 Summary

## 5.1.1 Key Economic Factors

The economics of coalbed methane produced water management in the Powder River Basin are influenced by four key factors:

- Future natural gas prices and, most critical today, the "basin differential." While natural gas prices at the Henry Hub have recently ranged from \$3 to \$3.50 per Mcf, the prices paid at the Wyoming hubs have ranged from \$1 to \$1.50 per Mcf, for an unprecedented and persistent "basin differential" of \$1.50 to \$2.00 per Mcf.
- The volume and timing of gas and water production from individual coal seams in distinct portions of the basin. Expected gas recovery from a CBM well ranges by order of magnitude, from 0.1 Bcf to 1 Bcf per well; and, water recovery varies twenty-fold, from 100,000 to 2,000,000 barrels per well.
- The capital and O&M costs for drilling and operating wells of different gas and water productivity and at depths of 300 to 3,000 feet.
- The coalbed methane produced water management option selected by the operator, as discussed further below.

## 5.1.2 Economic Cases

To examine the economic impact of alternative water production practices, the study used three gas price and "basin differential" cases:

*Case 1 (Today).* Case 1 assumes long-term natural gas prices of \$3.00 per Mcf (in constant year 2002 prices) at the Henry Hub, with a basin differential of \$1.80 per Mcf. This provides a natural gas price at the Wyoming Hub of \$1.20 per Mcf. (As a point of reference, on July 1, 2002 the natural gas price at the Wyoming Hub was \$1.07 per MMBtu, with a Henry Hub price of \$3.20 per MMBtu.)

*Case 2 (Transition).* Case 2 uses the same gas price (at Henry Hub) as Case 1, but assumes that the "basin differential" narrows with time, from \$1.80 per Mcf today, to \$1.30 per Mcf in 2003, and to \$0.80 per Mcf in 2003 and beyond.

*Case 3 (Long Term).* Case 3 uses the same gas price (at Henry Hub) as Cases 1 and 2, but assumes that the "basin differential" is and remains at \$0.80 per Mcf, consistent with historical trends.

For the volumes of gas and water expected to be produced, the study uses the 142 type wells representative of the different geological areas and coal seams in the PRB, presented in

Chapter 3. For capital and O&M costs, the study uses the cost and economic models presented in Chapter 4.

## 5.1.3 Overview of Economic Analyses

The economics of alternative water management options in the PRB are as follows, using a 15% (before corporate income tax) internal rate of return (IRR) as the threshold criteria.

Economic Cases	Surface Discharge	Impoundment	Shallow Reinjection	Active Treatment
Case 1 (Today)	1.5 Tcf			
Case 2 (Transition)	22.4 Tcf	20.0 Tcf	18.8 Tcf	7.1-10.2 Tcf
Case 3 (Long Term)	29.1 Tcf	27.8 Tcf	27.1 Tcf	17.8-21.6 Tcf

# Table 5-1. Volumes of Economically Recoverable CBM w/Alternative Water Disposal Options\*

\* Includes the 655 Bcf of CBM produced to date from the basin.

Analyses of the economics of alternative water management options for PRB CBM show the following:

*Case 1 (Today).* Under today's unfavorable economics (Case 1), surface disposal of produced water is the only economic water management option, and even this option is economic only in selected, high quality portions of the PRB. More costly water disposal options would preclude further economic development of coalbed methane in the Powder River Basin. A significant portion of the 1.5 Tcf of economic CBM potential shown in the above table is already under development with about 650 Bcf of this volume produced to date, leaving little opportunity for further economically justified expansion in this basin under today's gas price and PRB "basin differential."

*Case 2 (Transition).* Assuming a transition toward more normal Wyoming basin price differentials, a significant portion of the basin becomes economic to develop with water management practices of surface discharge, impoundment or shallow re-injection. Requiring active treatment of the produced water (with current reverse osmosis technology) greatly reduces the basin's economic potential. Specifically, instead of 19 to 22 Tcf of economically recoverable coalbed methane (using one of the first three water management options), only 7 to 10 Tcf of coalbed methane remains economic to develop with a requirement for active water treatment. This represents a loss of 12 Tcf of otherwise economically recoverable natural gas resource.

*Case 3 (Long Term).* Using a long-term outlook for gas prices in Wyoming (requiring that development be delayed until the basin differential reaches historically more normal values), the economic CBM resources of the PRB range from 27 to 29 Tcf (for the three lower cost water management options). Imposing active treatment of water (with current reverse osmosis tech-

nology) reduces the economically viable PRB CBM potential to a range of 18 to 22 Tcf, for a loss of 7 to 9 Tcf natural gas resources.

## 5.1.4 Impact of Risk Premium

Using a higher minimum rate of return—one potentially more reflective of the current higher economic and regulatory risks in the PRB—would reduce the natural gas resource and production contribution from the PRB. Imposing higher cost water management options, such as active produced water treatment with reverse osmosis, and a higher risk premium would also preclude further economic development of coalbed methane in the PRB. The result of this risk premium analyses, using Case 2 natural gas wellhead price and basin differential assumption, is shown below:

 Table 5-2. Volumes of Economically Recoverable CBM w/Alternative

 Water Disposal Options

Water Management Options	Case 2 w/15% IRR Treshold	Case 2 w/25% IRR Threshold
Surface Discharge	22.4 Tcf	16.6 Tcf
Impoundment	20.0 Tcf	12.7 Tcf
Shallow Reinjection	18.8 Tcf	12.4 Tcf
Active Treatment		
w/Trucking	7.1 Tcf	0.8 Tcf
w/Deep Disposal	10.2 Tcf	2.1 Tcf

## 5.2 Water Disposal Alternatives

A series of alternatives are being used or considered for CBM water disposal in the Powder River Basin, including:

- Untreated or passively treated water with surface discharge.
- Infiltration impoundment with enhanced evaporation and/or land application.
- Shallow re-injection of the produced water.
- Actively treated water with infiltration, evaporation, land application, and/or surface discharge, and disposition of the residual concentrate by trucking or deep re-injection.

Deep re-injection of the untreated, relatively high quality CBM produced water would be wasting a valuable resource and thus has not been included among the water disposal alternatives in this study.

## 5.3 Costs of Water Disposal Alternatives

## 5.3.1 Capital Costs

The capital costs for the alternative CBM water disposal options add from \$1,400 to \$35,200 per well, depending on the water management alternative selected, as shown for the example well below.

	Water Disposal Costs	
	Capital Costs/Well	O&M Costs/Bbl.*
Water Disposal		
Surface Discharge	\$1,400	\$0.02
Infiltration Impoundment	\$10,300	\$0.06
Shallow Re-Injection	\$15,150	\$0.06
Active Treatment w/Disposal of Residual Concentrate		
Trucking	\$19,600	\$0.24
Deep Re-Injection	\$35,200	\$0.14

Table 5-3. CBM Water Disposal Alternative Costs

\* Per barrel of water produced for a "typical" CBM producing 320 barrels per day (average) during the first 2 years.

## 5.3.2 **O&M** Costs

The operating costs of alternative CBM water disposal options will add from \$0.02 to \$0.24 per barrel of produced water to basic well and lease O&M costs, depending on the water management alternative selected.

## 5.3.3 Capital Costs for Water Treating and Associated Disposal

The total capital costs for using active water treatment (with RO) are as follows for a 900-gpm (30,860 barrel per day) facility:

		Trucking	Deep Disposal
Three RO Unit (installed)		\$1,600,000	\$1,600,000
Deep Disposal well and facilities		-	\$1,500,000
Three Impoundments		\$150,000	\$150,000
Three surface discharge points		\$130,000	\$130,000
	TOTAL	\$1,880,000	\$3,380,000

## Table 5-4. Capital Costs for Disposal Options

The cost for the RO unit and associated facilities, assuming trucking of the residual concentrate to disposal, is \$1,880,000 or \$19,600 per well for a 96-well unit.

Using a deep disposal well and injection facilities would eliminate the costs of trucking the residual concentrate, but would raise the capital costs to \$3,380,000 or \$35,200 per well for a 96-well unit.

## 5.3.4 Operating Costs for Water Treatment and Associated Disposal

Operating costs for the three RO units are estimated at \$233,100 per year for a 96-well unit, or \$0.02 per barrel of water treated (assuming a capacity of 30,000 barrels per day), and an operating factor of 95%. Adding the costs of maintaining the discharge points and impoundments, and providing electricity and maintenance for the pumps, bring operating costs to \$0.04 per barrel of water produced.

For trucking, the total costs are estimated at \$0.24 per barrel of water produced, assuming water trucking costs of \$2.00 per barrel and 10% residual concentrate.

For deep disposal, the total costs are estimated at \$0.14 per barrel of water produced, assuming deep re-injection well and facility O&M costs of \$0.10 per barrel of water injected.

	Operating Costs*
Electric Power	\$57,000
Chemicals	
Anti-scalant	\$73,000
Cleaning	\$5,000
Iron removal	\$3,500
Membrane Replacement (After 5 years, annualized)	\$33,600
Reject Disposal (10% residual concentrate)	see below
Annual Labor	\$22,000
	\$194,200
G&A of 20%	\$38,800
TOTAL	\$233,000

Table 5-5. Total Estimated Costs for Deep Disposal

Γ

Δnnual

\* Assuming a 96-well unit.

## 5.4 Discussion of Water Disposal Capital and O&M Costs

## 5.4.1 Surface Discharge

This alternative involves building two water discharge points with limestone rock (rip-rap) for passive treatment of the produced water. (The cost for the water transportation system and pumps has been included above.)

- The cost for 20 cubic yards of limestone rock is estimated at \$600.
- The cost for building a discharge point is estimated at \$5,000.
- Contingency, insurance, and other costs of 10% are added to the above.
- The cost for the NPDES permit is approximately \$1,000 per well.
- The total cost is estimated at \$6,200 for a 16-well facility or \$400 per typical CBM well, plus \$1,000 per well for the NPDES permit.

The operating costs for monitoring surface discharge, including electricity and maintenance for the surface pumps, are estimated at \$0.02 per barrel.

## 5.4.2 Infiltration Impoundment

This alternative involves constructing an impoundment (pond) and installing enhanced evaporation equipment (atomizers) or a surface irrigation system.

- The size of the impoundment is 3 acres with a dam of 13 feet, providing 20 acre-feet (150,000 barrels) of water capacity sufficient to hold 30 days of production from a 16-well unit.
- Annual water infiltration is estimated at 8 feet of water loss per year, with enhanced evaporation and surface irritation providing 12 feet of water loss per year. Together, this provides 60 acre-feet (approximately 465,000 barrels) of water loss per year or about 1,275 barrels per day (with more during summer months and less during winter months).
- An irrigation or atomizing system is added to the impoundment. One such unit is able to dispose of 45 gpm or 1,500 barrels per day.
- At an average water rate of 320 barrels per day (during the first two years of well operation), the 16-well unit will produce about 5,000 barrels per day of water. One impoundment with an irrigation system will accommodate about 8 wells (and more wells during subsequent years). A 16-well unit requires two such infiltration and evaporation impoundments.

- The cost for constructing each impoundment is estimated at \$25,000 to \$50,000, based on handling approximately 50,000 cubic yards of material at \$0.50 to \$1.00 per cubic yard. (Reclamation costs of \$10,000 (on a present value basis) are added to this total).
- The cost for one atomizer or irrigation system is estimated at \$16,500 for a 1,500-barrels per day (45 gpm) unit, with installation costs of about 20% or \$3,500. Two such units are required.
- Contingency, insurance, right of way and other costs of 10% are added.
- The total cost for two infiltration and evaporation impoundments is \$148,500, or \$9,300 per typical CBM well plus \$1,000 per well for the NPDES permit.

Construction	\$ 75,000
Reclamation (PV)	20,000
Atomizers/Irrigation (2 units)	40,000
Contingency, etc.	13,500
	\$148,500

The operating cost for the infiltration and evaporation impoundment is estimated at \$0.06 per barrel of water produced, including \$0.02 per barrel for electricity and maintenance for the surface pumps and \$0.04 per barrel for operating the irrigation system and maintaining the impoundment.

## 5.4.3 Shallow Re-injection

This alternative involves identifying shallow, ideally relatively fresh water zones into which the CBM produced water could be re-injected. A handful of such shallow well injection projects exist, but with a mixed record of success. Basically, shallow re-injection is a high risk option and may be considered a speculative alternative at this time. Therefore, shallow re-injection was evaluated from a theoretical standpoint in this analysis.

Ideally, the shallow re-injection zone would be under pressured and highly permeable. This would help reduce (or eliminate) pumped costs and reduce the number of required injection wells.

The costs for a large, central shallow re-injection facility (or two smaller facilities) capable of dispersing 30,000 barrels per day from 96 producing CBM wells is as follows:

- The cost of two 3-acre (20 acre-foot) infiltration impoundments (with a combined capacity fo 300,000 barrels) is estimated at \$104,500. This would provide storage for about 10 days of water production from a 96-well unit. The annual water loss from two impoundments would be modest, the order of 1,500 barrels per day.
- The remainder of the produced water would be injected into a series of shallow wells. Assuming water injection capacity of 2,000 barrels per day (based on water production

and a select number of injection projects in the basin), approximately 15 shallow wells would be required.

- The drilling and completion costs for shallow wells estimated to be on the order of \$30,000 to \$70,000 per well. Adding other costs, such as water transportation, pumps, injection facilities, permits, etc., is estimated to be about \$30,000 to \$50,000 per well, and provides total well costs of \$90,000 (Source: CBM Producers Information Survey Results, January 2002).
- Assuming average shallow well drilling and completion costs per well of \$90,000, the costs for 15 wells would be \$1,350,000 plus \$104,500 for the impoundment facilities for a total of \$1,454,500 or \$15,150 per typical CBM well, as shown below:

Impoundments (2)	\$ 104,500
Shallow Wells (10)	<u>\$1,350,000</u>
Total	\$1,454,500

The operating costs for the shallow wells and impoundment (including electricity and maintenance for the surface pumps) are estimated at \$0.06 per barrel of water produced.

## 5.4.4 Active Treatment Using Reverse Osmosis

This alternative involves constructing water holding and residual concentration storage impoundments, installing a water treatment system involving reverse osmosis (RO), surface discharging the treated water, and either trucking or deep re-injecting the residual concentrate.

*Capital Costs*. The capital costs are for a large, central unit able to service 96-producing CBM wells.

- The cost of three surface discharge points is estimated at \$18,600 (from above), plus \$15,000 for water piping and \$96,000 for studies and permits, for a total of \$130,000 for a 96-well unit.
- The cost of one 3-acre (20 acre-foot) infiltration impoundment (with a capacity of 150,000 barrels) is estimated at \$52,250 (from above). This would provide storage for about 5 days of water production from a 96-well unit. Two such impoundments are required to provide 10 days of produced water storage capacity. The cost of a third smaller (10 acre-foot) lined impoundment for storing the reject water (concentrate) from the RO unit is estimated at \$32,000, plus piping. This would provide storage for up to one month of reject water. The total cost for impoundments is estimated at \$150,000.
- Assuming a 96-well unit and 320 barrels of water per day per well (average water rate for first 2 years), 3 300-gpm (10,286 barrel per day) units are required with capacity to treat 30,000 barrels per day.

- The cost for 3 RO units (from Filter Tech) is \$1,212,000. Assuming 20% for site preparation, the electrical system, building, etc., plus 10% for contingency, insurance and other, the cost for three units is \$1,600,000.
- Two options, trucking and deep disposal, exist for disposing of the residual concentrate, estimated at 10% of the treated water, or 3,000 barrels per day.
- If trucking is the option, these costs are included in O&M costs, presented in the next section.
- If disposal is the option, additional capital costs are required for a deep disposal well and an injection facility for the residual concentrate. The costs of the re-injection well and associated facilities are estimated at \$1,000,000 for the deep re-injection well and \$500,000 for the facility (including large capacity pumps, electricity, water transportation and other costs).

The total capital costs for using active water treatment (with RO) are as follows for a 900-gpm (30,860 barrel per day) facility:

	Trucking	Deep Disposal
Three RO Unit (installed)	\$1,600,000	\$1,600,000
Deep Disposal well and facilities (est.)	-	\$1,500,000
Three Impoundments	\$150,000	\$150,000
Three surface discharge points	\$130,000	\$130,000
TOTAL	\$1,880,000	\$3,380,000

## Table 5-6. Total Capital Costs for Active Water Treatment

The cost for the RO unit and associated facilities, assuming trucking of the residual concentrate to disposal, is \$1,880,000 or \$19,600 per well for a 96-well unit. Adding a deep disposal well and injection facilities would eliminate the costs of trucking the residual concentrate, but would raise the capital costs to \$3,380,000 or \$35,200 per well for a 96-well unit.

*Operating and Maintenance Costs.* Operating costs for the 3 RO units are estimated at \$233,100 per year for a 96-well unit, or \$0.03 per barrel of water treated (assuming a capacity of 30,000 barrels per day) and an operating factor of 95%, as shown below. Adding the costs of maintaining the discharge points and impoundments, and providing electricity and maintenance for the pumps, brings operating costs to \$0.04 per barrel of water produced.

If trucking is the option, the costs for operating the RO unit, pumping the water, operating the discharge points, and disposing of the residual concentrate are estimated at \$0.24 per barrel of water produced assuming water trucking costs of \$2.00 per barrel of residual concentrate and 10% residual concentrate.

		Annual Operating Costs*
Electric Power		\$57,000
Chemicals		
Anti-scalant		\$73,000
Cleaning		\$5,000
Iron removal		\$3,500
Membrane Replacement (After 5 years, annualized)		\$33,600
Reject Disposal (10% residual concentrate)		see below
Annual Labor		\$22,000
		\$194,200
G&A of 20%		\$38,800
	TOTAL	\$233,000

## Table 5-7. Annual Operating Costs for Trucking

\* Assuming a 96-well unit.

If deep disposal of the residual concentrate is the option, the costs for operating the RO unit, pumping the water, operating the discharge points, and operating and maintaining the deep injection facility are estimated at \$0.14 per barrel of water produced, assuming deep re-injection well and facility O&M costs of \$1.00 per barrel of residual concentrate injected and 10% residual concentrate.

### 5.5 **Detailed Economic Analyses of Water Management Options**

An example of the discounted cash flow analysis, prepared for one of the 142 PRB CBM type wells is provided in Table 5-9. The economic analysis is for the Big George coal seam with 97 feet of coal at 1,372 feet of depth, in Partition #5 of the PRB. The economic assumptions are:

Table 5-8.	Assumptions for Discounted Cash Flow Analyses
------------	---

Price Calculation								
Gas Price (Henry Hub)	\$3.00/Mcf							
Basin Differential (PRB)	\$1.80 to \$0.80/Mcf							
Gathering and Compression	\$0.57/Mcf							
Net Wellhead Price	\$0.63 to \$1.63/Mcf							
Sales Volume Adjustment								
Btu Adjustment	(5%)							
Lease Fuel	(5%)							

The Big George coal seam in Partition #5 is estimated to recover 0.7 Bcf of natural gas plus 1,500,000 barrels of water. Economic analyses of this high water producing seam show that current practices of produced water management enable this coal seam to be economically developed. However, more costly water management options, such as reverse osmosis, will make this major coal seam in Partition #5 uneconomic.

	Total	100 C 10		69	1,523	1'1E-	-34.1	624.5	0.0	-13.1	-104.8	-1.8		5 977.26	F (163.20	5 814.06	F (48.84	F (48.84	F (142.36	5 (30.43	5 543.58	5 424.01	044200045330300		F 102.93						
	11 0	133	169	24	62	-2.4	-2.4	9.64		829		0.13	1.63	71.13	(11.88)	59.25	(3.56) ÷	(3.56)	(2.97)	(1.24)	41.93	11.93	424.01	0.21	9.01	102.93		233			
	63	2	3							82	0	<u>93</u>	₩	\$	\$ (	\$	\$ (	\$	\$ (	\$	₩	19	₩	10	H	¥9		53	_	25	
	10	15:	191	56	72	-2.8	-2.8	50.7	0.000				1.63	81.63	(13.63	68.00	(4.08	(4.08	( <b>9.25</b>	0.44	49.16	49.16	382.07	0.25	12.15	93.92			1	S.	
-	50	16	32	19	85	9.2	3.2	<b>D</b> Q		0.000 11.00		2010	₽ E	6 \$	\$ (£.	4 3	1) \$	€	± (0)	\$ (63	*	*	92 \$	28	1	₩	+	2000 A 222	-		
	σ	1	2	35	8	36) (14)	3	57					F 1.6	5 94.1	F (15.7	5 78.4	F (4.7	F (4.7	F (9.6	F (1.6	F 57.7	5 57.7	5 332 S		F 16.4	5 81.7					
-	98	Đ	77	11	1	1.E	5. E	10		8.9	0	89	÷ E9	89	19)	11	(++)	11	05) :	12)	52	15	10	EE.	15	35	1	200			
	80	2	2		5	i (	C.O	9					1.1	108.	(18.	90.	3	3	CID.	3.1	67.1	67.	275.	-	22.	65.					
	6.8		338					22		82		23	H		\$		\$	14		14	₩	¥9	14		¥9	\$		5,63			
	-	235	338	38	123	E'1-	6.1-	1.17					1.63	125.65	(20.98)	104.66	(6.28)	(6.28)	(10.66)	(2.47)	18.91	78.97	207.42	0.38	29.69	43.20					
	200					0						353	₩		\$	19	\$	\$	\$	\$	\$	₩	5		₩	19		_	_		
	9	267	131	36	157	5.4-	-1.5	87.8					1.63	113.04	(23.89	119.15	Q.15,	G.15	(11.58	0.14	90.12	90.12	128.45	0.43	38.96	13.52		•		•	
	52	10		5	-	P	P	· /		983	_	39	\$	*	\$	10	3 \$	\$	\$	\$	₩	₩	₩	-	₩	₩ (0	+	908 939			
	S	28	59	10:	21	-5.	-5.	94.					1.63	154.32	(25.7)	128.55	0.71	0.71	(17.45	(4.34	91.36	91.36	28°33	0.5	45.42	(25.45					
	25	9		P	5	50	50	-		232		244	₩	\$	\$ (	*	\$ (	*	*	\$	₩	*	\$ (	-	₩	\$	-	3.5	-	-	
	3	240	64	91	235	-4.5	-4.4	80.5					1.63	131.57	(21.97	109.60	(6.58	(6.58	(17.92	(4.70	13.83	53.83	(53.03	0.5	42.21	70.87					
	-	-	-	6	10	50	80	6	_	533			₩	*	\$ (1		\$ (3	₩ (2	\$ 0	\$	₩	10	\$ (2	6	₩ 10	8	+		_		
		15	64	5	236	-2.	-2.	50.0				de	1.13	7.13	9.54	7.59	2.86	2.86	7.92	1.70	9.26	9.26	16.86	0.6(	2.66	BO'E					
	12	ľ									. 1	UEIS	J.A.	5	LA.	*	- A	- LA	5 3	- IA	-	T IS	5 (12		F IA	111					
	2.5	11	11	17	SE	6.1	6.0			453		DBC	ES	2	52) 4		\$ (61	(61	\$ (86	9	\$ (95	551 3	12) \$	16	\$ (SE	11	+	5.25		2	
	2		9		2	7	-	15				I rtace	9.0	1.6	3. IJ .6	8.1	1. D. 1	9.6	28.5	(4.7	26.6	26.8	0116.1		(2D.L	(125.)					
	E da	-		Η		-	2		-		(9)	1) S	₩	\$	\$	\$	₩	**	₩		₩	\$ .12	\$ 22	12	1) \$	\$ 113	-				
	-										1.10	(1.8		-								3.90	19.5	1.1	92.6	05.6					
	25-6										\$ 0	64				Í						\$ 0	\$ (1		14	€ 0					
-	555		200	H	269		-			Koo						-			0.000			(00	(00	-	Koo	1		-	53	1	
LE										(13.												(13.	CD.	25	(13.	613.			102.	Sec. Sec.	
Yes	0.00		0.0		500		1		-	\$						£	53.2		0.10	~		₩	\$		₩	\$		2.9	₩	č C C	
Factor	200		205			950	5%					1.051			16.7%	SCONFEED OF	6%	6%	205	\$ (0.02)				15%	10.00				15%	20.00	
	8.9	£	(pd)	40	(m)	- 23		() of	10000	8.9		E	6		3	2	50		8.3		899	- 3	-	853	-		1		-		
	BAb	<b>W cfc</b>	0 W	JU IN C	(MI		4	B				Svst	O M/S	100000																	
	ge.	101	ctlo i	101	ctlo I	40/1	D to	C G a	10000		otte re	ett	ce @	No. 1 No.					6 S	59	1000								X	23.62	
4	eor	dict	rodi	dict	1 pol	tat	1510	Net	1000	겯	s tra c	dem	I P L	\$			5 5		34 B	0615	e E			2	F bu	E F			18T	1000	
ode	Vig G	P ro	e r P I	P TO	e r P	1	10.01		1	Te m	In Tra	EIE	Head			e	Tax	1 199	Exp	EXL	1001	MOI:	FD	ac to	135	Cat			NPV		
W W	5 8	G at	UN a t	6 as	W a t	1151	Fre		1 1	d / D	11 211	er M	e II F	Reu	~	U e h	1 Ce	E E O	N 2 1	02.0	E B H	51 5	1 382	ITF	etc	E					
hflo	8	\$\$0	\$\$0	\$\$0	\$\$0	DA 1	ase		le s th	Lah	W e	UU 31	IN B	\$\$0	ya by	t Re	ue a	NEV.	5 10 0	ater	terat	tCa	0.E	1005	SC. N	\$0. C					
Cas		1 0 1	2 C L	C D	101	5 8 14	5 Le		110	ח	à	0	S P R	00	D R O	1 Ne	2 5e	D'A E	T B B	5 M 1	6 O D	7 Ne	0 20	9 D 6	900	10 8	-		_		
B.)	8	22		1	1	*			88				<u> </u>	1	11	1	1	1.	1	1.	÷	1	-	1	2	N					

# Table 5-9. Cashflow Model Surface Discharge.

Note: All dollars are in thousands of real year 2002 dollars

A before tax return on investment is used for simplicity of calculations and the great variety in actual company tax rates. In general, a 15% before tax return on investment is Comparable to a 10% tax return on investment is

5-12

## 6.0 PRESENTATION OF RESULTS BY BASIN PARTITION

The materials presented in the previous chapters of the Powder River Coalbed Methane Basin Study provide an overview of the study methodology and findings. Chapter 6 provides a review of this information at a more detailed, "basin partition" level. As such, Chapter 6 contains a series of sections that provide the input data and the discussion of study findings for each of the twelve basin partitions, identified previously<sup>1</sup>. Within each section, additional information is provided on the major Wasatch and Fort Union Formation coal seams present in the partition.

The individual sections in Chapter 6 provide the geologic setting of the partition and its in-place and technically recoverable coalbed methane resources. This is followed by a coal seam by coal seam discussion of key reservoir properties that govern the producibility of each coal seam. Finally, each section presents the distribution of expected gas and water production for major coal seams, as represented by an average, high and low productivity CBM well completed in the seam. A series of maps, tables and figures summarize the data base and analytic work performed on the major coal seams in the Powder River Basin.

Section 6.4 of Chapter 6, discussing the study findings for Partition #4, contains the full set of maps, type logs, well performance profiles, and reservoir simulation-based history matches that serve as the foundation for the PRB Basin Study. For purposes of brevity, more summary information is provided for the other basin partitions.

## 6.1 Partition #1

## 6.1.1 Summary

Partition #1 covers a 20-township area in the southern portion of the Powder River Basin, from 36N to 39N and from 72W to 76W, Figure 6-1. Only one township in Partition #1 contains coal that meets the depth and thickness criteria of the study, the Anderson seam with 25 feet of coal at 450 feet. As such, the discussion of the Anderson coal in this partition is combined into Partition #2, northeast of Partition #1.

## 6.2 Partition #2

## 6.2.1 Summary

The main features of Partition #2, in the southeastern portion of the Powder River Basin, are as follows:

• The partition covers a 17-township area on the eastern edge of the PRB, from 40N to 44N and from 70W to 73W, Figure 6-2.

<sup>&</sup>lt;sup>1</sup>Some quantities have been subject to rounding.

N 80 W	41N 79W	41N 78W	41N 77W	41N 76W	41N 75W	61N 76W	41N 73W	41N 72W	
40 N 80W	un 1900 dwest	∎∎"Edge	nton	40N 76W	40N 75W	40 N 7 4W	40N 73W		LON 7 IW
89 N 80 W	39N 79W	39N 78W	39 N 77 W	39N 76W	39N 75W	39 N 7 4W	39N 73W	39N 72W	39N 71W
18N 80W	38 N 7 9 W	38N 78W	38N 77W	38 N 76W	38N 75W	36 N 7 6W	38N 73W	38N 72W	38 N 7 1 W
7 N 80 V	Real C	×	37N 77W	37 N 76W	37N 75W	37N 74W	37 N 73W	37 N 72 W	37 N 71W
36N 80		80	36 N 77 W	36N 76W	36N 75 W	36 N 74 W	36N 73W	36 N 7 2 W	36N 71W
35 N 80	-	sw	35 N 77 W	35N 76W	35N 75W	35 N 7 4 W	35N 73W	35 N 7 2 W	35N 71W
34N 80W	34N 79W	34N 78W	34N 77W	34N 76W	3411 7540	34N 74W	34N 73W	34N 72W	3 KN 71 W

Figure 6-1. Partition #1 Base Map



Figure 6-2. Partition #2 Base Map

- A series of coal mines exist in the townships along the shallower eastern edge; as a result, the townships on the eastern edge of the partition (in 70W) are no longer available for CBM development.
- The stratigraphic section contains the Canyon, Wyodak, Big George, Cook and Pawnee coal seams (plus the Anderson from Partition #1). The depth of these coals ranges from 450 to 1,340 feet, with coal seam thickness ranging from 22 to 90 feet (township level averages).
- The gas in-place in the two partitions is 2.2 Tcf, with technically recoverable gas of 1,630 Bcf. The results by coal seam are provided in Table 6-7.

## 6.2.2 Discussion of Major Seams

- *Anderson*. The Anderson is the only significant seam in Partition #1. It does not meet the depth and thickness criteria in Partition #2.
  - *Area.* The Anderson coal seam meets study inclusion criteria in 1 township, located in the southern portion of Partition #1.
  - *Coal Thickness.* The Anderson seam coal thickness averages 25 feet.
  - *Coal Depth.* The depth to the top of the Anderson seam averages 450 feet.
  - **Development.** Only a few Anderson wells currently exist in this partition.
  - *Time Zero Plot.* Not available.
  - *Type Well.* The history-matched Anderson well in Partition #4, adjusted for depth, gas content and coal thickness, serves as the Anderson type well for Partition #1.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	475	25	0.12	120

## Table 6-1. Anderson Coal Seam

- *Canyon*. The first major coal seam in Partition #2 is the Canyon, at times included within or called the Wyodak.
  - *Area*. The Canyon coal seam meets study inclusion criteria in 2 townships located in the western portion of the partition.
  - *Coal Thickness*. The Canyon coal seam thickness averages 48 feet, with a range of 35 to 60 feet.

- *Coal Depth*. The depth to the top of the Canyon seam averages 575 feet, with a range of 450 to 700 feet.
- **Development**. Considerable Canyon coal well development exists in this partition with nearly 100 shut-in and permitted wells.
- *Time Zero Plot*. The time zero plot for 7 recently drilled Canyon coal wells is provided in Figure 6-3.
- *Type Well*. Because the Canyon well production data in Partition #2 is recent, limited and still erratic, the history-matched Canyon well in Partition #4, adjusted for depth, gas content, and coal thickness, serves as the Canyon type well for Partition #2. Because only two townships contain the Canyon coal seam, with significantly different coal properties, only a high and low Canyon well are used.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
High	760	60	0.46	460
Low	485	35	0.17	270

## Table 6-2. Canyon Coal Seam

- *Wyodak*. A thick package of Wyodak coals exists in the central portion of Partition #2.
  - *Area.* The Wyodak coal seam meets study inclusion criteria in 5 townships.
  - *Coal Thickness*. The Wyodak coal seam thickness averages 86 feet, with a range of 70 to 100 feet.
  - *Coal Depth*. The depth to the top of the Wyodak seam averages 440 feet, with a range of 300 to 600 feet.
  - **Development**. Wyodak coal well development is active in this partition with over 500 wells having been drilled or permitted.
  - *Time Zero Plot*. The time zero plot for 181 Wyodak coal wells is provided in Figure 6-4.
  - *Type Well*. Because the Wyodak well production performance in Partition #2 is similar to the Wyodak well performance in Partition #4, the history-matched Wyodak well in Partition #4, adjusted for depth, gas content, and coal thickness, serves as the Wyodak type well for Partition #2.



Figure 6-3. Canyon Time Zero Plot



Figure 6-4. Wyodak Time Zero Plot

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	525	86	0.37	1,140
High	700	100	0.58	1,330
Low	370	70	0.22	930

## Table 6-3. Wyodak Coal Seam

*Big George*. The Big George coal seam, stratigraphically and depositionally similar to the Wyodak, exists in the western portion of Partition #2.

٠

- *Area*. The Big George coal seam meets study inclusion criteria in 2 townships.
- *Coal Thickness*. The Big George coal seam thickness averages 90 feet, with a range of 80 to 100 feet.
- *Coal Depth*. The depth to the top of the Big George seam averages 860 feet, with a range of 850 to 875 feet.
- **Development**. Approximately 300 Big George coal wells have been drilled or permitted in this partition.
- *Time Zero Plot*. The Big George coal wells in Partition #2 have been combined into a composite Fort Union interval in the production data base. Thus, a distinct time zero plot for this coal seam is not available.
- **Type Well**. The history-matched Big George well in Partition #3, adjusted for depth, gas content, and coal thickness, serves as the Big George type well for Partition #2. Because the Big George coal exists in only two townships and has relatively uniform depth and thickness, only an average Big George well is used.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	950	90	0.55	700

## Table 6-4. Big George Coal Seam

- *Cook.* The Cook coal seam exists at sufficient thickness in the central portion of Partition #2.
  - Area. The Cook coal seam meets study inclusion criteria in two townships.
  - *Coal Thickness*. The Cook coal seam thickness averages 30 feet.

- *Coal Depth*. The depth to the top of the Cook seam averages 740 feet, with a range of 650 to 830 feet.
- *Development*. The Cook coal seam is undeveloped.
- *Time Zero Plot*. Not available.
- *Type Well*. The history-matched Cook well in Partition #8, adjusted for depth, gas content, and coal thickness, serves as the Cook type well for Partition #2. Because the Cook coal exists in only two townships with the same thickness, only an average Cook well is used.

## Table 6-5. Cook Coal Seam

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	770	30	0.21	200

- *Pawnee*. The Pawnee seam exists at sufficient thickness in the southwestern portion of Partition #2.
  - Area. The Pawnee coal seam meets study inclusion criteria in 5 townships.
  - *Coal Thickness*. The Pawnee coal seam thickness averages 22 feet with a range of 20 to 30 feet.
  - *Coal Depth*. The depth to the top of the Pawnee seam averages 1,340 feet, with a range of 1,200 to 1,620 feet.
  - *Development*. The Pawnee coal seam is undeveloped.
  - *Time Zero Plot*. Not available.
  - *Type Well*. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability, and coal thickness, serves as the Pawnee type well for Partition #2. Because the Pawnee coal seam has relatively uniform depth and thickness, only an average well is used.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,360	22	0.29	290

## Table 6-6. Pawnee Coal Seam

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable Resources (Bcf)
Anderson	1	450	25	39	40	30
Canyon	2	575	48	51	210	180
Wyodak	5	440	86	42	760	560
Big George	2	860	90	86	550	320
Cook	2	740	30	65	150	120
Pawnee	5	1,336	22	108	470	420
Totals					2,170	1,630

 Table 6-7. In-Place and Technically Recoverable CBM, Partitions #1 and #2

\* Top of coal

## 6.3 Partitions #3 and #12

## 6.3.1 Summary

The main features of Partitions #3 and #12, in the Powder River Basin, are as follows:

- Partition #3 covers a 21-township area in the south-central portion of the PRB, from 40N to 44N and from 73W to 79W, Figure 6-5. Partition #12 covers a 12-township area along the western edge of the PRB, Figure 6-6. Only one township (42N 77W) and only one coal seam, the Big George, meet the study inclusion criteria in Partition #12. Because this township forms the western extent of the Big George coal seam in Partition #3, this single township and coal seam in Partition #12 is included in the data and discussion of the Big George coal seam in Partition #3.
- The stratigraphic section contains the Anderson, Canyon, Wyodak, Big George, and Cook coal seams. (The Wyodak "fairway" boundary crosses the northeast corner of the partition.) The remainder of the area is included in the Big George "fairway" for coal seam designation purposes.
- The depth to the top of these coals ranges from 730 to 1,500 feet, with individual coal seam thickness ranging from 30 to 130 feet (township level averages).
- The gas in place in the partition is 8.3 Tcf, with technically recoverable gas of 4,060 Bcf. The results by coal seam are provided in Table 6-12.

## 6.3.2 Discussion of Major Seams

- *Anderson.* The Anderson exists as a distinct seam on the eastern portion of the partition.
  - *Area*. The Anderson coal seam meets study inclusion criteria in one township.



Figure 6-5. Partition #3 Base Map



Figure 6-6. Partition #12 Base Map

- *Coal Thickness*. The Anderson seam coal thickness averages 55 feet.
- *Coal Depth*. The depth of the Anderson seam averages 855 feet to top of coal.
- **Development.** Anderson coal seam development is just starting.
- *Time Zero Plot*. Not available.

•

- *Type Well*. The history-matched Anderson well in Partition #4, adjusted for depth, gas content and coal thickness, serves as the Anderson type well for Partition #3. Since only one township contains Anderson coal of sufficient depth and thickness, only an average well is used.

Table 6-8. Anderson Coal Seam

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	855	55	0.40	270

- *Canyon*. The Canyon exists as a distinct seam primarily in the eastern and central portions of Partition #3. The Canyon is sometimes included within or called the Wyodak.
  - *Area*. The Canyon coal seam meets study inclusion criteria in 9 townships located in the western portion of the partition.
  - *Coal Thickness*. The Canyon coal seam thickness averages 43 feet, with a range of 25 to 65 feet.
  - *Coal Depth*. The depth to the top of the Canyon seam averages 970 feet, with a range of 730 to 1,425 feet.
  - *Development*. Canyon coal seam development is just starting and is concentrated in township 44N 74W.
  - *Time Zero Plot*. Not available.
  - *Type Well*. The history-matched Canyon well in Partition #4, adjusted for depth, gas content and coal thickness, serves as the Canyon type well for Partition #3.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)	
Average	1,013	43	0.33	330	
High	960	60	0.43	460	
Low	830	30	0.25	230	

## Table 6-9. Canyon Coal Seam

*Big George*. The Big George coal seam, stratigraphically and depositionally similar to the Wyodak, exists in the central portion of Partition #3 and in Partition #12.

٠

- *Area*. The Big George coal seam meets study inclusion criteria in 11 townships, including one township in Partition #12.
- *Coal Thickness*. The Big George seam coal thickness averages 100 feet, with a range of 70 to 125 feet.
- *Coal Depth*. The depth to the top of the Big George seam averages 1,280 feet, with a range of 970 to 1,500 feet.
- **Development**. Over 300 Big George coal wells have been drilled or permitted in this partition.
- *Time Zero Plot*. The time zero plot for 38 producing Big George wells in T43-44N, R74W is provided in Figure 6-7.
- *Type Well*. The history-matched Big George well shown in Figure 6-8, adjusted for depth, gas content and coal thickness, serves as the Big George type well for Partition #3.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,380	100	0.66	770
High	1,525	125	0.89	970
Low	1,420	70	0.48	540

Table 6-10.	<b>Big George</b>	Coal Seam
1 4010 0 100	Dig George	Cour Scam

- *Cook.* The Cook coal seam exists at sufficient thickness in the eastern portion of Partition #3.
  - *Area*. The Cook coal seam meets study inclusion criteria in two townships.
  - *Coal Thickness*. The Cook coal seam thickness averages 30 feet.



Figure 6-7. Big George Time Zero Plot



Figure 6-8. Big George Partition #3

- *Coal Depth*. The depth to the top of the Cook seam averages 1,030 feet, with a range of 930 to 1,125 feet.
- **Development**. The Cook coal seam is essentially undeveloped.
- *Time Zero Plot*. Not available.
- *Type Well*. The history-matched Cook well in Partition #8, adjusted for depth, gas content, and coal thickness, serves as the Cook type well for Partition #3. Because the Cook coal exists in only two townships with the same coal thickness, only an average Cook well is used in Partition #3.

## Table 6-11. Cook Coal Seam

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,060	30	0.29	200

 Table 6-12. In-Place and Technically Recoverable CBM, Partitions #3 and #12

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable Resources (Bcf)
Anderson	1	800	55	70	160	110
Canyon	9	970	43	81	1,260	870
Big George	11	1,280	100	107	6,620	2,910
Cook	2	1,030	30	86	210	170
Totals					8,250	4,060

\* Top of coal

## 6.4 Partition #4

## 6.4.1 Summary

The main features of Partition #4, in the east-central portion of the Powder River Basin, are as follows:

- The partition covers a 22-township area on the eastern edge of the PRB, from 45N to 52N and from 70W to 73W, Figure 6-9.
- A series of coal mines exists in the townships along the shallower eastern edge; as a result, the bulk of CBM development is in the eight townships along the western edge of



Figure 6-9. Partition #4 Base Map

this partition. The partition contains some of the earliest CBM wells and "fields" in the PBR, such as Caballo and Bonepile.

- Partition #4 contains 7 major coal seams in the Fort Union Formation. The depth to these coals ranges from 450 to 1,500 feet, with coal seam thickness ranging from 23 to 73 feet (township level averages). The gas in place in the partition is 4.2 Tcf, with technically recoverable gas of 3,540 Bcf. The results, by coal seam, are provided in Table 6-20.
- The stratigraphic sequence for some of the major coal seams in this partition, such as the Anderson, Canyon and Cook, is shown in Figure 6-10, a sample log from Sec. 3, 53N, 74W. The log identifies coals that meet the study criteria for selection in that township (depth greater than 300 feet and thickness greater than 20 feet. In addition, a series of thinner coals, with thickness of 10 to 20 feet, exist in this partition, such as the Smith and Swartz.

## 6.4.2 Geologic Background

Partition #4 is located along the eastern rim of the Powder River Coal Basin in an area of Fort Union Formation outcrops. Structural strike is NW/SE with a southwestern dip of 1.5 degrees. Subtle structural nosing and low relief normal faulting locally interrupt the gentile southwest dip.

Stratigraphically, the coal seams in Partition #4 exist in two groups – an upper group consisting of the Smith, Swartz, Anderson, Canyon, Wyodak, and Cook seams, and a lower group consisting of the Wall, Pawnee and the Cache seams. These groups are recognizable by their depth, stratigraphic proximity and thickness.

The upper group, a thick succession of coals separated by thin "parts" and "splits," is characterized by shallow depth (450 to 790 feet) and considerable coal thickness (30 to 70 feet). Correlation challenges exist due to stratigraphic proximity and apparent stratigraphic overlap due to averaging data over an entire township. (Some Powder River CBM geologist include all upper groups of coals within the Wyodak.)

The lower group is characterized by deeper depth (1,020 to 1,500), lower coal thickness (20 to 30 feet), and considerable stratigraphic separation (200 to 300) feet between coal seams.

CBM operators have extensively developed this partition, with the great majority of the wells in the Wyodak seam and/or its stratigraphic equivalents, the Anderson and Canyon seams, that are often called the Fort Union.

## 6.4.3 Discussion of Major Seams

• *Anderson.* The first major coal seam in Partition #4 is the Anderson, often included in the Wyodak seam interval. The stratigraphic proximity of the Anderson to the adjacent Canyon, Smith and Swartz seams provides correlation challenges. (This can lead to correlation problems especially in the eastern portion of the partition where the Fort Union Formation thins dramatically.)



Figure 6-10. Partition #4 Sample Log
- *Area*. The Anderson coal seam meets study inclusion criteria in 6 townships located in the western and central portions of the partition.
- *Coal Thickness*. The Anderson seam coal thickness averages 30 feet, with a range of 20 to 50 feet.
- *Coal Depth*. The depth to the top of the Anderson seam averages 450 feet, with a range of 300 to 650 feet.
- **Development**. Figure 6-11 provides the location of the currently drilled Anderson CBM wells.
- **Time Zero Plot.** The time zero plot for 89 producing Anderson coal seam wells in T51N, R73W is provided in Figure 6-12. After initial rates of 150 barrels of water per day, the water rates decline to about 60 barrels per day at the end of year 1. Gas production starts and peaks early at about 100 Mcfd indicating the presence of free gas.
- *Type Well*. The history-matched type well for the Anderson coal seam is provided in Figure 6-13. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows:

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	480	30	0.12	150
High	700	50	0.29	240
Low	470	20	0.08	100

 Table 6-13.
 Anderson Coal Seam

- *Canyon*. The Canyon seam is stratigraphically below the Anderson and is also often included within the Wyodak seam. Like the Anderson, the Canyon presents correlation problems in the western portion of the study area due the proximity of adjacent coal seams.
  - *Area*. The Canyon coal seam meets study inclusion criteria in 12 townships located in the western and central portion of the partition.
  - *Coal Thickness*. The Canyon coal seam thickness averages 35 feet, with a range of 25 to 50 feet.
  - *Coal Depth*. The depth to the top of the Canyon seam averages 540 feet, with a range of 300 to 800 feet.

53N 74W	53N 73W	53N 72W	53N71W	53N 701W	53N 69W	53468W
52N 74W			62N 71W	52N 70 W	52N 69W	52N680
€ 51N 74W			51N71W	51N 70W	51N 89W	51N68V
50N 74W	50N 73 W	Son 72W		50N 70W	50N 89W	50 <b>0</b> 68 V
48N 74W	49 N 73 W		Sleepy Holld	W 49N 70W view	49N 69W	4914681
48N 74W	48N 73W	48N 72W		48N 70 W	43 N 69 W	48N 681
47N 74 <i>W</i>	47N 73W	47 N 72 W		47N 70 W	47 N 69W	47N 681
46N 741W	46N 731W	46N 721W	48N71W		46 N 691W	46N 681
45N 74W	45N 731W	5N-72W	4 <mark>6N</mark> 71W	45N 70W	45N 69W	45N 68V
4 <b>4N 7</b> 4W	44N 73 W	44N 72W	44N 71 W	44N 70 W	44N 69W	44N 681

Figure 6-11. Partition #4 Anderson Wells



Figure 6-12. Canyon Time Zero Plot



Figure 6-13. Anderson Type Well, Partition #4

- **Development**. Figure 6-14 provides the location of the currently drilled Canyon CBM wells.
- *Time Zero Plot*. The time zero plot for 173 producing Canyon coal seam wells in T51-52N, R73W is provided in Figure 6-15. Initial water rates are 300 or more barrels producing for the first year, declining to about 50 barrels per day at the end of year 3. Gas production starts early and peaks at nearly 300 Mcfd during year 1, indicating the presence of free gas.
- **Type Well**. The history-matched type well for Canyon coal seam is provided in Figure 6-16. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows below.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	575	35	0.20	270
High	700	50	0.35	380
Low	550	25	0.14	190

 Table 6-14.
 Canyon Coal Seam

*Wyodak*. The Wyodak seam is the stratigraphic equivalent of the combined Anderson and Canyon seams. As such, separating the Anderson and Canyon from the Wyodak is often arbitrary.

•

- *Area*. The Wyodak coal seam meets study inclusion criteria in 6 townships located in the western portion of the partition.
- *Coal Thickness*. The Wyodak seam coal thickness averages 73 feet, with a range of 70 to 80 feet.
- *Coal Depth*. The depth to the top of the Wyodak seam averages 600 feet, with a depth range of 330 to 750 feet.
- **Development**. Figure 6-17 provides the locations of the currently drilled Wyodak CBM wells.
- *Time Zero Plot*. The time zero plot for 164 producing Wyodak coal seam wells in T47-48N, R72W is provided in Figure 6-18. Initial water rates are at 600 barrels per day, declining to about 400 barrels per day at the end of year 1 and to about 130 barrels per day at the end of year 4. Gas production increases steadily, reaching 300 Mcfd during year 1. After a 12-month plateau, gas production declines to about 150 Mcfd at the end of year 2 and to about 80 Mcf at the end of year 4.

53N 74W	53N 73W	53N 72W	53N 71W	53N 70W	53N 69W	53H 68W
52N 74W			52N 71W	52N 70 W	52N 89W	521/681
51N 74W			61N71W	51N 70 W	51N 89W	5110681/
50N 741W	50N 73W	50N 72W		50N 70W	50N 69W	50 <b>0</b> 68 V
49 N 74 W	49N 73 W	49H 72W Ante	Sleepy Hollo 49N71W Iope Valley-Cresty	49N 70 W 49N 70 W view	49N 69W	491 <b>4</b> 881/
48N 74W	48N 73 W	48N 72 VV		48N 70 W	48 N 69 W	48N 681
47N 74W	47 N 73 W	• 47 N 72 W		47N 70W	47 N 69W	47N 681
48N 74 <i>\</i> ₩	46N 73W	46N 72W	CON 7 1 M		46N 69W	46 N 68 \
45N 74W	45N 73 W	611-72W	- 2000 - 400 71 W	45N 701W	46N 69W	45N 68 V
44N 74W	44N 73 W	44N 72 W	44N 71 W	44N 70 W	44N 69W	44N 681

Figure 6-14. Partition #4 Canyon Wells



Figure 6-15. Canyon Time Zero Plot



Figure 6-16. Canyon Type Well, Partition #4

	53N 74W	53N 73W	63N 72W	53N 71W	53N 70W	53N 69W	5346830
-	52N 74W	52H73W		52N 71W	52N 70 W	52N 69W	52N68V
4	51N 74W	<del>5111</del> 73W		61N71W	51N 70W	51N 69W	51N68V
	50N 74W	50N 73W	SON 72W		50N 70W	50N 69W	50 <b>0</b> 68 V
	49N 74W	49N 73W	4nr72w Ante	Sleepy Holld	49N 70W 19W	49N 69W	49 <b>11</b> 68 V
	48N 741M	48N 73W			48N 70 W	48 N 69 W	48N 681
	47N 74W	47 N 73 W			47N 70 W	47N 69W	47N 681
	46N 74VV	46N 7310/		46N 71 W		46N 69W	46N 681
	45N 74 <i>\</i> \/	45N 73W		Con 1 W	46N 70W	46N 69W	45N 68V
	44N 74W	44N 73 W	44N 72 W	441071W	44N 70 W	44N 69W	44N 681

Figure 6-17. Partition #4 Wyodak Wells



Figure 6-18. Wyodak Time Zero Plot

- *Type Well*. The history-matched type well for the Wyodak coal seam is provided in Figure 6-19. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows:

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	670	73	0.48	960
High	760	80	0.58	1,060
Low	400	70	0.28	930

 Table 6-15.
 Wyodak Coal Seam

- *Cook.* The Cook seam defines the base of the upper group of Fort Union coals in Partition #4. The Cook seam is stratigraphically below the Canyon and Wyodak equivalents. The proximity of the Cook seam to the basal boundary of the Wyodak and equivalents poses correlation problems throughout the partition.
  - *Area*. The Cook coal seam meets study inclusion criteria in 5 townships in the western portion of the partition.
  - *Coal Thickness*. The Cook seam coal thickness averages 31 feet, with a range of 20 to 50 feet.
  - *Coal Depth*. The depth to the top of the Cook seam averages 790 feet, with a depth range of 600 to 930 feet.
  - **Development**. The drilled Cook CBM wells are shown in Figure 6-20.
  - *Time Zero Well*. Not available.

•

- *Type Well*. The history-matched Cook well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cook type well for Partition #4.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	820	31	0.23	210
High	900	50	0.41	340
Low	620	20	0.12	140

Table	6-16.	Cook	Coal	Seam
ant	0-10.	CUUK	Cuar	Scam



Figure 6-19. Wyodak Type Well, Partition #4

53N 74W	53N 73 W	53N 72W	53N 71W	53N 701W	53N 69VV	53468W
52N 74W	<mark>52N</mark> 73W		52N 71W	\$2N 70 W	52N 69W	52N/68 V
61N 74W	611173W	WE HE	61N71W	51N 70W/	51N 89W	51N68V
50N 74W/	50N 73 W	SON 72W		50N 70W	50N 89W	50 <b>0</b> 68 V
49N 74W	49N 73 W	49N 72W Ante	Sleepy Holld	₩ 49N 70₩ ∕iew	49N 69W	49M68V
48N 74W/	48N 73 W	48N 72 W		48N 70 W	48 N 69 W	48N 681
47N 74W	47N 73W	.● 47N 72W		47N 70W	47 N 69W	47N 681
46N 74W	46N 73W	46N 72W	48N71W		46N 69W	46N 681
45N 74W	45N 73 ₩	4 <mark>511 7</mark> 2W	4 <mark>511</mark> 71W	45N 70W	46N 69W	45N 68 V
44N 74W	44N 73 W	44N 72 W	4411771W	44N 70 W	44N 69W	44N 681

Figure 6-20. Partition #4 Cook Wells

- *Wall*. The Wall seam defines the top of the lower group of Fort Union Formation coals in Partition #4. The Wall coal seam is stratigraphically below the Cook, separated by an average of 230 feet.
  - *Area*. The Wall coal seam meets study inclusion criteria in 5 townships in the central and western portions of the partition.
  - *Coal Thickness*. The Wall seam coal thickness averages 27 feet, with a range of 20 to 40 feet.
  - *Coal Depth*. The depth to the top of the Wall seam averages 1,020 feet, with a depth range of 800 to 1250 feet.
  - *Development*. The drilled Wall CBM wells are shown in Figure 6-21.
  - *Time Zero Plot*. The time zero plot for 19 producing Wall coal seam wells in Partition #4 is provided in Figure 6-22. Initial water rates are 300 or more barrels producing for the first year, declining to about 50 barrels per day at the end of year 3. Gas production starts early and peaks at nearly 90 Mcfd during year 1.
  - **Type Well**. The history-matched type well for Wall coal seam is provided in Figure 6-23. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows in Table 6-17.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,050	27	0.24	460
High	1,060	40	0.35	680
Low	970	20	0.16	340

 Table 6-17.
 Wall Coal Seam

- *Pawnee*. The Pawnee seam is stratigraphically below the Wall, separated by 275 feet of section.
  - *Area*. The Pawnee coal seam meets study inclusion criteria in 5 townships in the western portion of the partition.
  - *Coal Thickness*. The Pawnee seam coal thickness averages 27 feet with a range of 25 to 30 feet.
  - *Coal Depth*. The depth to the top of the Pawnee seam averages 1,290 feet, with a depth range of 1,150 to 1,500 feet.

53N 74W	53N 73 W	53N 72W	53N 71 W	53N 70W/	53N 69W	53/468W
52N 74W	52N73V		62N 71W	52N 70 W	52N 89W	52N/68V
51N 74W	<b></b>		51N71W	51N 7010/	51N 69W	51N68V
50N 74W	50N 73 W	50N 72W Gillette		50N 70W	50N 89W	500 68 V
49 N 74 W	49N 73 W	4911-7200 Ante	Sleepy Hollo 49N71W lope Valley-Crestv	₩ 49N 70₩ View	49N 69W	49N68V
48N 74W	48N 73 W	€ 48N 72W [		48N 70 W	48 N 69 W	48N 681
47N 74W	47N 73W	47 N 72 W		47 N 70 W	47 N 69W	47N 681
46N 74W	46N 73W/	46N 72W	48N 71 W		46 N 69 W	46N 681
45N 7410/	46N 73 W	4 <mark>511 7</mark> 2100	4 <mark>511</mark> 71W	45N 70 W	46N 69W	45N 68V
44N 74W	44N 73 W	44N 72 W	44N 71 W	44N 70 W	44N 69W	44N 681

Figure 6-21. Partition #4 Wall Wells



Figure 6-22. Wall Time Zero Plot



Figure 6-23. Wall Type Well, Partition #4

- **Development**. Figure 6-24 provides the location of the currently drilled Pawnee CBM wells.
- *Time Zero Plot*. Not available.

•

- *Type Well*. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Pawnee type well for Partition #4.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,320	27	0.35	360
High	1,330	30	0.40	400
Low	1,230	25	0.30	330

Table 6-18. Pawnee Coal Seam

- *Cache*. The Cache coal seam is the basal unit of the lower group of Fort Union coals in Partition #4. The Cache seam is stratigraphically below the Pawnee, separated by 205 feet of section.
  - *Area*. The Cache coal seam meets study inclusion criteria in 5 townships in the western portion of the partition.
  - *Coal Thickness*. The Cache seam coal thickness averages 23 feet, with a range of 20 to 30 feet.
  - *Coal Depth*. The depth to the top of the Pawnee seam averages 1,500 feet, with a depth range of 1,150 to1,750 feet.
  - **Development**. The Cache seam is lightly developed, as shown in Figure 6-25.
  - *Time Zero Well*. Not available.
  - *Type Well*. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cache type well for Partition #4.

	53N 74W	53N 73W	53N 72W	53N 71W	53N 7010/	53N 89W	53/H 68 W
-	52N 74W	52N73W		62N 71W	52N 70W	52N 69W	52N/681
-	51N 74W	<b>211</b> 273 W	STR 12W	51N71W	51N 7010/	51N 69VV	51N68V
	50N 74W	50N 73 W	SON 72W Gillette		50N 70W	50N 69W	50 <b>0</b> 68 V
	49N 74W	49N 73W	49N 72W Ante	Sleepy Holld 49171W lope Valley-Cresty	₩ 49N 70₩ ∕iew	49N 69W	49N68V
-	48N 74W	48N 73 W	4 <mark>8N 72</mark> W		48N 70 W	48 N 69 W	48N 681
_	47N 74W/	47 N 73 W	47 N 72 W		47N 70W	47 N 69W	47N 681
_	46N 7410/	46 N 73 W	46 N 72 W	48N71W		46 N 69 W	46 N 68 \
	45N 7410/	46N 73W	4 <mark>511 7</mark> 2W	4 <mark>511</mark> 71W	45N 70W	46N 69W	45N 68V
	44N 74W	44N 73 W	44N 72 W	4 <b>4</b> N71W	44N 7D W	-44N 69W/	44N 681

Figure 6-24. Partition #4 Pawnee Wells

	53N 74W	53N 73W	63N 72W	53N 71W	53N 70W	53N 69W	534 68 W
-	52N 74W	521173W	Conversion Conversion	52N 71W	52N 70 W	52N 69W	52N68V
	51N 74W	5TN73W		51N71W	51N 70W	51N 89W/	51N68V
	50N 74W	50N 73 W	SON 72W		50N 70W	50N 69W/	50 <b>0</b> 68 V
	49N 74W	49N 73 W	4 <del>9N 7</del> 2W Ante	Sleepy Holld	₩ 49N 70₩ /iew	49N 69W/	49N68V
-	48N 74W	48N 73 W	48N 72W [		48N 70 W	48 N 69 W	48N 681
	47N 74W/	47N 73W	47N 72W 🏶		47N 70 W	47 N 69W	47N 68\
	46N 741W	46N 73W/	● 48N 72W/	46N 71 W		-46N 69W/	46N 681
	45N 74₩	46N 73 W	4 <mark>511 7</mark> 2W	4 <mark>511</mark> 71 W	46N 70 W	46N 69W	45N 68V
	44N 74W	44N 73 W	44N 72 W	44N 71 W	44N 70 W	44N 69W	44N 681

Figure 6-25. Partition #4 Cache Wells

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,520	23	0.34	300
High	1,780	25	0.43	330
Low	1,170	20	0.23	260

## Table 6-19. Cache Coal Seam

### Table 6-20. In-Place and Technically Recoverable CBM, Partition #4

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Anderson	6	450	30	40	400	290
Canyon	12	540	35	47	920	800
Wyodak	6	601	73	54	890	770
Cook	5	790	31	67	450	350
Wall	5	1,020	27	84	440	350
Pawnee	5	1,295	27	106	570	510
Cache	5	1,550	23	121	540	480
Totals	44				4,210	3,550

\* To top of coal

#### 6.5 Partition #5

#### 6.5.1 Summary

The main features of Partition #5, in the central portion of the Powder River Basin, are as follows:

- The partition covers a 38-township area in the PRB, from 45N to 52N and from 73W to 77W, Figure 6-26.
- Partition #5 contains 12 major coal seams in the Wasatch and Fort Union Formation. The depth to these coals ranges from 320 to 2,260 feet, with coal seam thickness ranging from 20 to 150 feet (township level averages). The gas in place in the partition is 25.5 Tcf, with technically recoverable gas of 14,910 Bcf. The results by coal seam are provided in Table 6-33.

BN TSW	sein 78w	59N 77W	99N 78W	99N 75W	59N 74W	SEN TOW	95N 72W	59N 71W	59N 70W	55N 69W	$\sim$
<b>5</b> 24	san mar Clearmo	nt see 700	SHIN THW	54N 75W	54N 74W	54N 73W	54N 72W	54N 77W	54N 70W	54N 62W	J
ian taw	San Taw	(Jan TW) San TW	SIN 78W	san 75 w	san 74w	san 7aw	san 72w	6an 71w	san 70w	53N 69W	
52N 75W	szn Taw	52N 77W	52% 76 W	52N 79W	1284 T-444	raw [		52N TIW	52N 70W	52N 69W	
in 19w	SIN 78W	5 IN 77W	STIN 74W	51N 75W	51N 74W				51N 70W	STN 69W	
0N 75W	50 N 78W	50N 77W	50N 78W	Sign 75 Ver	50N 74W	50% 73W	Gi	let <b>te</b>	901 704	SON 69W	
an 7900	-ran Taw	48N 77N	-6294 700V	-1514 75147	484 TAN	-80 T3W		Antelop	py Hollo e Valley	w -Crest	view
EN 75W	481N 78W	489 TW	48N 70W	48N 75W	48N 74W	4894 7.397	and the second		48N 70 W	48N 89W	T
17N 75W	47 N TBW	ATN TW	489 789	40% 75W	नाम रनम	ATTN TOWN	47N 72W		47N 70W	47N 89W	
6N 75WY	48N TAW	48N 77W	4894 7899	-451N 175 Ver	-1294 T-1404	-REN TOWN	-HEIN TZW	- The			
3N 75W	461N TAW	49N 77W	-ean item	45IN 75W	-894 T-84	NET ND-				-	
an Taw	44N TBW	44N 77W	44N 78W	484 7 <i>50</i> 7	-491 74W	-981 73W	44N 72W	-1	-	-	
3N 75W	-ran Taw	-GN TTV	-tan 78W	-61N 75W	-EIN 74W	-SIN 73W	-GIN 72W				
94 TEW	-004 MBN	42N 77W	42N 78W	42N 75W	-294 7 <i>44</i> 1	-KEN TOW	42N 72W				

Figure 6-26. Partition #5 Base Map

## 6.5.2 Discussion of Major Seams

- *Felix*. The first major coal seam in Partition #5 is the Felix. The stratigraphic proximity of the Felix to the adjacent Roland seam provides correlation challenges.
  - *Area*. The Felix coal seam meets study inclusion criteria in 4 townships in the eastern portion of the partition.
  - *Coal Thickness*. The Felix seam coal thickness averages 24 feet, with a range of 20 to 30 feet.
  - *Coal Depth*. The depth to the top of the Felix seam averages 530 feet, with a range of 320 to 780 feet.
  - *Development*. The Felix coal is essentially undeveloped.
  - *Time Zero Plot*. Not available.

•

- *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5, discussed later, serves as the type well for the Felix coal seam in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	555	24	0.12	90

#### Table 6-21. Felix Coal Seam

- *Roland*. The Roland seam is stratigraphically below the Felix. Like the Felix, the Roland presents correlation problems in the eastern portion of the partition due the proximity of adjacent coal seams.
  - *Area*. The Roland coal seam meets study inclusion criteria in only 2 townships located in the northern portion of the partition.
  - *Coal Thickness*. The Roland coal seam thickness averages 25 feet, with a range of 20 to 30 feet.
  - *Coal Depth*. The depth to the top of the Roland seam averages 540 feet.
  - *Development*. The Roland coal is essentially undeveloped.
  - *Time Zero Plot*. Not available.

- *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5, discussed later, serves as the type well for the Roland coal seam in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	565	25	0.13	100

# Table 6-22. Roland Coal Seam

- *Smith*. The Smith seam lies stratigraphically below the Roland seam and is a significant coal seam in Partition #5.
  - *Area*. The Smith coal seam meets study inclusion criteria in 18 townships located throughout the partition.
  - *Coal Thickness*. The Smith seam coal thickness averages 40 feet, with a range of 25 to 60 feet.
  - *Coal Depth*. The depth to the top of the Smith seam averages 820 feet, with a depth range of 320 to 1,200 feet.
  - *Development*. The are a total of 339 drilled or permitted Smith CBM wells in Partition #5.
  - *Time Zero Plot*. The time zero plot for 10 producing Smith coal seam wells is provided in Figure 6-27. Initial water rates are at 130 barrels per day declining to about 70 barrels per day after 6 months. Gas production increases steadily, reaching 40 Mcfd during year 1.
  - *Type Well*. The history-matched type well for the Smith coal seam is provided in Figure 6-28. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	860	40	0.31	150
High	1160	60	0.47	230
Low	500	25	0.12	100

# Table 6-23. Smith Coal Seam

*Swartz*. Stratigraphically, the Swartz seam is between the overlying Smith seam and the underlying Anderson coal seam.



Figure 6-27. Smith Time Zero Plot



Figure 6-28. Smith Type Well, Partition #5

- *Area*. The Swartz coal seam meets study inclusion criteria in 2 townships in the northern portion of the partition.
- *Coal Thickness*. The Swartz seam coal thickness averages 43 feet, with a range of 40 to 45 feet.
- *Coal Depth*. The depth to the top of the Swartz seam averages 740 feet, with a depth range of 700 to 770 feet.
- *Development*. The Swartz coal is essentially undeveloped.
- *Time Zero Well*. Not available.

٠

- *Type Well*. The history-matched Smith well in Partition #5, adjusted for depth, gas content, permeability and coal thickness, serves as the Swartz type well in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	785	43	0.30	160

Table 6-24. Swartz Coal Seam

- *Anderson.* The Anderson coal seam is stratigraphically below the Swartz, separated by an average of 300 feet of section. The Anderson seam is often included with the Canyon seam or the Wyodak elsewhere in the Powder River Basin.
  - *Area*. The Anderson coal seam meets study inclusion criteria in 9 townships.
  - *Coal Thickness*. The Anderson seam coal thickness averages 38 feet, with a range of 25 to 60 feet.
  - *Coal Depth*. The depth to the top of the Anderson seam averages 1,030 feet, with a depth range of 800 to 1,400 feet.
  - **Development**. The are a total of 362 drilled or permitted Anderson CBM wells in Partition #5.
  - *Time Zero Plot*. The time zero plot for 216 producing Anderson coal seam wells in Partition #5 is provided in Figure 6-29. Initial water rates remain high, at 250 to 300 barrels per day through the first 2 years. Gas production starts early and reaches 60 Mcfd during year 1, indicating the presence of free gas.



Figure 6-29. Anderson Time Zero Plot

- *Type Well*. The history-matched Anderson well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Anderson type well in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1070	38	0.33	100
High	860	60	0.43	160
Low	920	25	0.20	70

# Table 6-25. Anderson Coal Seam

- *Canyon*. The Canyon seam is the most intensely developed coal seam in Partition #5.
  - *Area*. The Canyon coal seam meets study inclusion criteria in 16 townships throughout the partition.
  - *Coal Thickness*. The Canyon seam coal thickness averages 39 feet with a range of 30 to 55 feet.
  - *Coal Depth*. The depth to the top of the Canyon seam averages 1,060 feet, with a depth range of 700 to 1,400 feet.
  - **Development**. A total of 1,610 drilled or permitted Canyon CBM wells exist in Partition #5.
  - *Time Zero Plot*. The time zero plot for 73 producing Canyon coal seam wells in Partition #5 is provided in Figure 6-30. Initial water rates are high, at 300 to 450 barrels per day, dropping to about 130 barrels per day after 18 months. Gas production reaches 80 Mcfd after 6 months.
  - *Type Well*. The history-matched Canyon well in Partition #4, adjusted for depth, gas content, permeability and coal thickness, serves as the Canyon type well for Partition #5.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,100	39	0.32	300
High	1,060	55	0.43	420
Low	1,030	30	0.23	230

|--|



Figure 6-30. Canyon Time Zero Plot

- *Big George*. The Big George is the second most intensely developed seam in Partition #5. It lies approximately 200 feet deeper than the Canyon seam and is equivalent to the Wyodak coal in the eastern portion of this partition.
  - *Area*. The Big George coal seam meets study inclusion criteria in 16 townships in the central and southern portions of the partition.
  - *Coal Thickness*. The Big George seam coal thickness averages 97 feet, with a range of 80 to 140 feet.
  - *Coal Depth*. The depth to the top of the Big George seam averages 1,280 feet, with a depth range of 1,150 to1,460 feet.
  - **Development**. The are a total of 1,027 drilled or permitted Big George CBM wells in Partition #5.
  - *Time Zero Well*. The time zero plot for 121 producing Big George coal seam wells in Partition #5 is provided in Figure 6-31. Initial water rates start at 480 barrels per day, climbing to a peak late in year 2 at 1,800 barrels per day. Water rates drop off only slightly at the end of year 2 to 1,330 barrels per day. Gas production begins slowly and gradually peaks at 270 Mcfd after 20 months. The time zero plot for the Big George wells in Partition #5 shows constraints in water production during initial production. Therefore, a relatively intensely drilled area of the partition, Sec. 16 T44N, R77W, was examined in more detail. The location of these wells and the elevation map for the section is provided in Figure 6-32. These 17 wells were combined to establish the time zero plot for the Big George coal well in Partition #5, Figure 6-33.
  - *Type Well*. The history-matched Big George coal seam well in Partition #5 was used to develop the 80 acre type well in Figure 6-34. After normalizing for coal thickness, depth, and gas content, the estimated gas and water recoveries are as follows in Table 6-27.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,380	97	0.69	1,520
High	1,440	140	1.05	2,210
Low	1,320	80	0.56	1,260

<b>Table 6-27.</b>	<b>Big George</b>	<b>Coal Seam</b>
		Cour Scum

• *Wyodak*. Essentially an equivalent of the thick Big George seam, the Wyodak coal seam exists only on the eastern side of the partition, adjacent to Partition #4.



Figure 6-31. Big George Coal Seam - Aggregate



Figure 6-32. Big George Coal Seam Well Location and Elevation Map, Partition #5.



Figure 6-33. Big George Time Zero Plot



Figure 6-34. Big George Type Well Partition #5

- *Area*. The Wyodak coal seam meets study inclusion criteria in 2 townships in the southeastern portion of the partition.
- *Coal Thickness*. The Wyodak seam coal thickness averages 73 feet, with a range of 70 to 75 feet.
- *Coal Depth*. The depth to the top of the Wyodak seam averages 1,000 feet, with a depth range of 950 to 1,050.
- **Development**. The Wyodak coal seam is extensively developed with nearly 700 drilled or permitted wells in Partition #5.
- *Time Zero Well*. The time zero plot for 442 producing Wyodak coal seam wells in Partition #5 is provided in Figure 6-35. Initial water rates start at 270 barrels per day. Gas production begins early at about 60 Mcfd and increases steadily to nearly 220 Mcfd at the end of 2 years.
- *Type Well*. The history-matched Wyodak well in Partition #4, adjusted for depth, gas content, permeability and coal thickness, serves as the type well for Partition #5. Because the Wyodak coal exists in only two townships with relatively uniform production, only an average well is used.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,075	73	0.37	480

 Table 6-28.
 Wyodak Coal Seam

- *Cook.* The Cook seam defines the base of the upper group of Fort Union coals in Partition #5. The proximity of the Cook seam to the basal boundary of the Wyodak and equivalents poses correlation problems throughout the partition.
  - *Area*. The Cook coal seam meets study inclusion criteria in 17 townships throughout the partition.
  - *Coal Thickness*. The Cook seam coal thickness averages 40 feet, with a range of 25 to 60 feet.
  - *Coal Depth*. The depth to the top of the Cook seam averages 1,320 feet, with a depth range of 900 to 1,700.
  - **Development**. A total of 1,321 drilled or permitted Cook CBM wells exist in Partition #5.
  - *Time Zero Well*. Not available.


Figure 6-35. Wyodak Time Zero Plot

- *Type Well*. The history-matched Cook well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cook type well for Partition #5.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,360	40	0.37	270
High	1,460	60	0.58	410
Low	960	25	0.16	170

# Table 6-29. Cook Coal Seam

- *Wall*. The Wall coal seam defines the top of the lower group of Fort Union Formation coals in Partition #5. The Wall coal seam is stratigraphically below the Cook, separated by an average of 175 feet.
  - *Area*. The Wall coal seam meets study inclusion criteria in 16 townships throughout the partition.
  - *Coal Thickness*. The Cook seam coal thickness averages 33 feet, with a range of 20 to 45 feet.
  - *Coal Depth*. The depth to the top of the Cook seam averages 1,500 feet, with a depth range of 1,220 to 1,900.
  - **Development**. The Wall coal seam is extensively developed in only one township in the southern portion of Partition #5.
  - *Time Zero Well*. Not available.
  - *Type Well*. The history-matched Wall well in Partition #4, adjusted for depth, gas content, permeability and coal thickness, serves as the type well for the Wall seam in Partition #5.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,530	33	0.31	560
High	1,520	45	0.39	760
Low	1,470	20	0.18	340

*Pawnee*. The Pawnee coal seam is stratigraphically below the Wall, separated by an average of 215 feet.

- *Area*. The Pawnee coal seam meets study inclusion criteria in 18 townships throughout the central and northern portions of the partition.
- *Coal Thickness*. The Pawnee seam coal thickness averages 41 feet, with a range of 25 to 70 feet.
- *Coal Depth*. The depth to the top of the Pawnee seam averages 1,710 feet, with a depth range of 1,350 to 2,260.
- **Development**. A total of 368 drilled or permitted Pawnee CBM wells, concentrated in a handful of townships, exist in Partition #5.
- *Time Zero Well*. Not available.
- *Type Well*. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Pawnee type well for Partition #5.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,750	41	0.45	540
High	1,470	70	0.64	920
Low	1,580	25	0.25	330

Table 6-31. Pawnee Coal Seam

- *Cache*. The Cache coal seam is the basal unit of the lower group of Fort Union coals in Partition #5. The Cache seam is stratigraphically below the Pawnee, separated by approximately 300 feet of section.
  - *Area*. The Cache coal seam meets study inclusion criteria in 14 townships throughout the central and northern portions of the partition.
  - *Coal Thickness*. The Cache seam coal thickness averages 32 feet, with a range of 20 to 50 feet.
  - *Coal Depth*. The depth to the top of the Cache seam averages 2,020 feet, with a depth range of 1,510 to 2,350.
  - **Development**. The Cache coal seam is essentially undeveloped.
  - *Time Zero Well*. Not available.

- *Type Well*. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cache type well for Partition #5.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	2,050	32	0.34	420
High	1,910	50	0.50	660
Low	2,220	20	0.14	260

### Table 6-32. Cache Coal Seam

<b>Table 6-33.</b>	<b>In-Place and</b>	Technically	Recoverable	CBM.	Partition #5

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Felix	4	530	24	46	180	140
Roland	2	540	25	47	100	80
Smith	18	820	39	70	2,310	1,560
Swartz	2	740	43	63	220	180
Anderson	9	1030	38	86	1,180	830
Canyon	16	1060	39	88	2,320	1,500
Big George	16	1280	97	107	6,760	3,510
Wyodak	2	1000	73	85	250	210
Cook	17	1320	40	109	3,060	1,810
Wall	16	1500	32	120	2,250	1,350
Pawnee	18	1710	41	137	4,000	2,320
Cache	14	2020	32	159	2,700	1,320
Wildcat	1	2190	45	101	180	90
Totals					25,510	14,910

\* To top of coal

## 6.6 Partition #6

### 6.6.1 Summary

The main features of Partition #6, in the western portion of the Powder River Basin, are as follows:

• The partition covers a 31-township area in the west-central portion of the PRB, from 45N to 52N and from 78W to 80W in the south and 78W to 82W in the north, Figure 6-36.

8577	54 N 8 4/V	54N 83/V	541 82/V	54 N B 11VI	54 N 80/W	∎ <sup>™</sup> Cle	armont	5+ <b>N</b> 77VV	54 N 76/VI
85W	53N 8+VV	53 K 83W	53N 82/V	53 <b>H</b> 81W	53 N 80/W	53 <b>11</b> 7940	53 H 7 SW	57 I 77W	531 7600
:# 85/V	52M 844V	52W 83W	52 H 82/V	52N 81W	52H 80W	528 7944	5211 7 BW	52N 77W	52 N 76/V
N 85W	51 N 8 4/V	51# 83W	51# 82W	51 N 8 1VV	51N BOW	51# 79W	51 M 7 BIAN	51N 77W	51N 76W
85/V	944V	50H 83W	90 K 82W	lffalo ∞n ≋ IW	SON BOW	901 79Wi	93N 78W	50 N 77W	50M 76/A
85W	43 N 8+1VI	@ N 83W	ON BZW	iðn 81W	49 N 200V	4911 79VV	49N 78VV	<b>Ø K</b> 77W	69N 76/VI
:# 85/V	43N 84W	481 83W	6H SQU	49N SIVV	43N BOW	4311 794V	45W 7 8VV	48N 771VI	431 76/N
# 85M	47 N 8 400	<i>4</i> N 83W	4 ¥ 82W	47 M 81/W	47 M BOW	47 H 79VU	<b>€7 11</b> 7 8/W	47 N 771VJ	47 N 76/N
	Mat		+5H 822V	45 N 8 1V)	45N 80W	45N 79VU	<b>611</b> 7 8/W	46N 77W	45N 761/V
8		-	45M 820V	45N 8 1VV	4511 80W	45H 75MU	45# 78W	45 M 77VV	45N 761/V
**	-		44W 820V	<b>N</b> 8100	44 N 80 W	44N 79W	44N 7 BIA	44 <b>H</b> 77W	44 N 76/V
3 N 85/V	43M 844VV	43M 83W	43 N 82/W	Kayce	B anow	43N 79VV	43N 78VV	<b>G N</b> 77VV	43 <b>8</b> 76/N

Figure 6-36. Partition #6 Base Map

• Partition #5 contains 12 major coal seams in the Wasatch and Fort Union Formations. The depth to these coals ranges from 560 to 2,900 feet, with coal seam thickness ranging from 20 to 100 feet (township level averages). The gas in place in the partition is 6.2 Tcf, with technically recoverable gas of 3,460 Bcf. The results, by coal seam, are provided in Table 6-45.

## 6.6.2 Discussion of Major Seams

- *Cameron*. The first major coal seam in Partition #6 is the Cameron. The Cameron is separated from the underlying Murry seam by an average of 100 feet of section.
  - *Area*. The Cameron coal seam meets study inclusion criteria in one township in the northwestern portion of the partition.
  - *Coal Thickness*. The Cameron seam coal thickness averages 20 feet.
  - *Coal Depth*. The depth to the top of the Cameron seam averages 700 feet.
  - **Development**. The Cameron coal seam is essentially undeveloped in Partition #6.
  - *Time Zero Plot*. Not available.
  - *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Cameron coal seam.

Table 6-34.	Cameron	<b>Coal Seam</b>
-------------	---------	------------------

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	720	20	0.14	80

- *Murry*. The Murry seam is stratigraphically below the Cameron coal seam. Due to stratigraphic proximity, separation of these seams is difficult outside of the northwestern portion of the partition.
  - *Area*. The Murry coal seam meets study inclusion criteria in one township located in the northwestern portion of the partition.
  - *Coal Thickness*. The Murry coal seam thickness averages 50 feet.
  - *Coal Depth*. The depth to the top of the Murry seam averages 800 feet.
  - **Development**. The Murry seam is essentially undeveloped in Partition #6.
  - *Time Zero Plot*. Not available

- *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Murry coal seam.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	850	50	0.40	190

Table 6-35. Murry Coal Seam

- *Felix.* The Felix coal seam lies stratigraphically below the Cameron and Murry seams.
  - *Area*. The Felix coal seam meets study inclusion criteria in one township located in the northwestern portion of the partition.
  - *Coal Thickness*. The Felix seam coal thickness averages 30 feet.
  - *Coal Depth*. The depth to the top of the Felix seam averages 750 feet.
  - **Development**. The Felix seam is essentially undeveloped in Partition #6.
  - *Time Zero Plot*. Not available.
  - *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Felix coal seam.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	780	30	0.22	120

## Table 6-36. Felix Coal Seam

- *Ucross*. The Ucross coal seam is often difficult to distinguish from the overlying Cameron, Murry, and Felix seams.
  - *Area*. The Ucross coal seam meets study inclusion criteria in 3 townships in the northwestern portion of the partition.
  - *Coal Thickness*. The Ucross seam coal thickness averages 23 feet, with a range of 20 to 25 feet.
  - *Coal Depth*. The depth to the top of the Ucross seam averages 790 feet, with a depth range of 560 to 950 feet.

- **Development**. A small number of Ucross coal seams exist in one of the town-ships in Partition #6.
- *Time Zero Well*. Not available.
- *Type Well*. The history-matched Smith well in Partition #5, adjusted for depth, gas content, permeability and coal thickness, serves as the Ucross type well in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	810	23	0.18	90

Table 6-37. Ucross Coal Seam

- *Roland*. The Roland is the uppermost Fort Union coal seam in Partition #6.
  - *Area*. The Roland coal seam meets study inclusion criteria in 5 townships in the northern portion of the partition.
  - *Coal Thickness*. The Roland seam coal thickness averages 21 feet, with a range of 20 to 25 feet.
  - *Coal Depth*. The depth to the top of the Roland seam averages 1,060 feet, with a depth range of 830 to 1,480 feet.
  - **Development**. The are a total of 107 drilled or permitted Roland CBM wells in two of the townships in Partition #6.
  - *Time Zero Plot*. Not available.
  - *Type Well*. The history-matched Smith well in Partition #5, adjusted for depth, gas content, permeability and coal thickness, serves as the Roland type well in this partition.

Table 6-38.	Roland	Coal	Seam

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	Average 1,080		0.16 8	80

- *Anderson*. The Anderson coal seam is thin and relatively undeveloped in Partition #6.
  - *Area*. The Anderson coal seam meets study inclusion criteria in 3 townships in the central portion of the partition.

- *Coal Thickness*. The Anderson seam coal thickness averages 30 feet, with a range of 20 to 40 feet.
- *Coal Depth*. The depth to the top of the Anderson seam averages 1,220 feet, with a depth range of 1,030 to 1,480 feet.
- **Development**. The Anderson coal seam is undeveloped in Partition #6.
- *Time Zero Plot*. Not available.
- *Type Well*. The history-matched Anderson well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Anderson type well for Partition #6.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,250	30	0.26	80

### Table 6-39. Anderson Coal Seam

- *Canyon*. The Canyon seam in Partition #6 is approximately 300 feet deeper than the overlying Anderson seam.
  - *Area*. The Canyon coal seam meets study inclusion criteria in 8 townships throughout the partition.
  - *Coal Thickness*. The Canyon seam coal thickness averages 30 feet, with a range of 20 to 50 feet.
  - *Coal Depth*. The depth to the top of the Canyon seam averages 1,520 feet, with a depth range of 1,300 to1,720 feet.
  - **Development.** The Canyon coal seam is undeveloped in Partition #6.
  - *Time Zero Well*. Not available.
  - *Type Well*. The history-matched Canyon well in Partition #4, adjusted for depth, gas content, permeability and coal thickness, serves as the Canyon type well for Partition #6.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,550	30	0.32	230

## Table 6-40. Canyon Coal Seam

High	1,600	50	0.27	190
Low	1,740	20	0.24	150

- *Big George*. Stratigraphically equivalent to the Anderson and Canyon coals, the Big George seam exists in areas where these two coals merge.
  - *Area*. The Big George coal seam meets study inclusion criteria in 2 townships in the southeastern portion of the partition.
  - *Coal Thickness*. The Big George seam coal thickness averages 85 feet, with a range of 70 to 100 feet.
  - *Coal Depth*. The depth to the top of the Big George seam averages 1,665 feet, with a depth range of 1,630 to 1,700 feet.
  - *Development*. The Big George coal seam is essentially undeveloped in Partition #6.
  - *Time Zero Well*. Not available.
  - *Type Well.* The history-matched Big George well in Partition #3, adjusted for depth, gas content, permeability and coal thickness, serves as the Big George type well for Partition #6.

Table 6-41.	Big	George	Coal	Seam
1 4010 0 110	~ 5	George	0044	

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,750	85	0.85	660

- *Cook.* The Cook seam defines the base of the upper group of Fort Union coals in Partition #6. The proximity of the Cook seam to the basal boundary of the Canyon and equivalents poses correlation problems.
  - *Area*. The Cook coal seam meets study inclusion criteria in 2 townships along the eastern edge of the partition.
  - *Coal Thickness*. The Cook seam coal thickness averages 58 feet, with a range of 25 to 90 feet.
  - *Coal Depth*. The depth to the top of the Cook seam averages 1,863 feet, with a depth range of 1,850 to 1,875 feet.
  - **Development**. The Cook seam is essentially undeveloped in Partition #6.

- *Time Zero Well*. Not available.
- *Type Well*. The history-matched Cook well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cook type well for Partition #6.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,920	58	0.66	390

### Table 6-42. Cook Coal Seam

- *Wall.* The Wall coal seam defines the top of the lower group of Fort Union Formation coals in Partition #6.
  - *Area*. The Wall coal seam meets study inclusion criteria in one township in the northeastern portion of the partition.
  - *Coal Thickness*. The Cook seam coal thickness averages 40 feet.
  - *Coal Depth*. The depth to the top of the Cook seam averages 1,630 feet.
  - **Development**. The are no Wall CBM wells drilled in Partition #6.
  - *Time Zero Well*. Not available.

٠

- *Type Well*. The history-matched Wall well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the type well for the Wall seam in Partition #6.

### Table 6-43. Wall Coal Seam

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)	
Average	1,670	40	0.38	520	

- *Pawnee*. The Pawnee coal seam is stratigraphically below the Wall, separated by an average interval of 365 feet.
  - *Area*. The Pawnee coal seam meets study inclusion criteria in 4 townships in the north-central portion of the partition.
  - *Coal Thickness*. The Pawnee seam coal thickness averages 44 feet, with a range of 20 to 100 feet.

- *Coal Depth*. The depth to the top of the Pawnee seam averages 2,000 feet, with a depth range of 1,730 to 2,270 feet.
- **Development**. The Pawnee coal seam is essentially undeveloped in Partition #6.
- *Time Zero Well*. Not available.
- *Type Well*. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Pawnee type well for Partition #6.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)	
Average	2,040	44	0.47	580	
High	2,000	100	1.05	1,320	
Low	1,750	20	0.19	260	

 Table 6-44.
 Pawnee Coal Seam

 Table 6-45. In-Place and Technically Recoverable CBM, Partition #6

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Cameron	1	700	20	60	50	40
Felix	1	750	30	63	140	110
Murry	1	800	50	69	80	60
Ucross	3	790	23	66	190	150
Roland	5	1,060	21	86	370	240
Anderson	3	1,220	30	99	370	220
Canyon	8	1,520	30	123	1,090	660
Big George	2	1,670	85	136	930	490
Cook	2	1,860	58	147	690	380
Wall	1	1,630	40	130	200	110
Pawnee	4	2,000	44	158	1,270	620
Wildcat	4	2,640	25	191	760	370
Totals					6,150	3,460

\* To top of coal

## 6.7 Partition #7

## 6.7.1 Summary

The main features of Partition #7, in the northern Wyoming portion of the Powder River Basin, are as follows:

- The partition covers a 23-township area in the northwestern portion of the PRB, from 53N to 58N and from 78W to 82W, Figure 6-37.
- Partition #7 contains 9 major coal seams in the Wasatch and Fort Union Formations. The depth to these coals ranges from about 390 to 2,980 feet, with coal seam thickness ranging from 20 to 40 feet (township level averages). The gas in place in the partition is 2.8 Tcf, with technically recoverable gas of 1,680 Bcf. The results, by coal seam, are provided in Table 6-55.

# 6.7.2 Discussion of Major Seams

- *Wasatch*. The shallowest major coal seam in Partition #7 is the Wasatch that combines the Felix and Ucross seams. The Wasatch is separated from the underlying Roland seam by an average of 280 feet of section.
  - *Area*. The Wasatch coal seam meets study inclusion criteria in 6 townships located in the southern portion of the partition.
  - *Coal Thickness*. The Wasatch seam coal thickness averages 25 feet, with a range of 20 to 34 feet.
  - *Coal Depth*. The depth to the top of the Wasatch seam averages 540 feet, with a range of 390 to 730 feet.
  - **Development**. The are a total of 124 drilled or permitted Wasatch CBM wells in Partition #7.
  - *Time Zero Plot*. Not available.
  - *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Wasatch coal seam in this partition.



Figure 6-37. Partition #7 Base Map

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	570	25	0.13	100
High	620	34	0.19	130
Low	420	20	0.08	80

- *Roland*. The Roland seam lies stratigraphically below the Wasatch and is the first Fort Union coal seam in this partition.
  - *Area*. The Roland coal seam meets study inclusion criteria in 3 township located in the southern portion of the partition.
  - *Coal Thickness*. The Roland seam coal thickness averages 27 feet, with a range of 20 to 40 feet.
  - *Coal Depth*. The depth to the top of the Roland seam averages 820 feet, with a range of 800 to 850 feet.
  - **Development**. The are a total of 169 drilled or permitted Roland CBM wells in Partition #7.
  - *Time Zero Plot*. Not available.

٠

- *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Roland coal seam in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	850	27	0.21	100
High	840	40	0.31	150
Low	840	20	0.16	80

<b>Table 6-47.</b>	<b>Roland Coal Seam</b>
--------------------	-------------------------

- *Smith*. The Smith seam is stratigraphically below the Roland coal seam, separated by approximately 350 feet of section.
  - *Area*. The Smith coal seam meets study inclusion criteria in two townships, located in the central portion of the partition.
  - *Coal Thickness*. The Smith coal seam thickness averages 20 feet.

- *Coal Depth*. The depth to the top of the Smith seam averages 1,180 feet, with a range of 1,065 to 1,300 feet.
- **Development**. The are a handful of Smith wells and permits in Partition #7.
- *Time Zero Plot*. Not available
- *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Smith coal seam in this partition.

Table 6-48. S	Smith (	Coal	Seam
---------------	---------	------	------

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,200	20	0.16	80

- *Anderson.* The Anderson seam is stratigraphically below the Smith coal seam.
  - *Area*. The Anderson coal seam meets study inclusion criteria in 5 townships, 4 of which lie in the northernmost portion of the partition.
  - *Coal Thickness*. The Anderson seam coal thickness averages 21 feet, with a range of 20 to 25 feet.
  - *Coal Depth*. The depth to the top of the Anderson seam averages 910 feet, with a depth range of 370 to 1,480 feet.
  - *Development*. The Anderson coal seam is essentially undeveloped in Partition #7.
  - *Time Zero Well*. Not available.
  - *Type Well*. The history-matched Anderson well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Anderson type well in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	930	21	0.16	60
High	1,500	25	0.24	50
Low	390	20	0.07	50

## Table 6-49. Anderson Coal Seam

- *Canyon*. The Canyon is about 600 feet below the Anderson.
  - *Area*. The Canyon coal seam meets study inclusion criteria in two townships in the southern portion of the partition.
  - *Coal Thickness*. The Canyon seam coal thickness averages 25 feet.
  - *Coal Depth*. The depth to the top of the Canyon seam averages 1,500 feet, with a depth range of 1,450 to 1,540 feet.
  - *Development*. The Canyon coal seam is undeveloped in Partition #7.
  - *Time Zero Plot*. Not available.
  - *Type Well*. The history-matched Canyon well in Partition #4, adjusted for depth, gas content, permeability and coal thickness, serves as the Canyon type well in this partition.

Table 6-50. Canyon Coal Seam

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,520	25	0.26	190

- *Cook.* The Cook seam is the next deepest coal in Partition #7.
  - *Area*. The Cook coal seam meets study inclusion criteria in two townships in the northern portion of the partition.
  - *Coal Thickness*. The Cook seam coal thickness averages 28 feet, with a range of 25 to 30 feet.
  - *Coal Depth*. The depth to the top of the Cook seam averages 2,300 feet, with a depth range of 2,250 to 2,350 feet.
  - **Development**. The Cook coal seam is undeveloped in Partition #7.
  - *Time Zero Plot*. Not available.
  - *Type Well*. The history-matched Cook well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cook type well for Partition #7.

Table 6-51.	<b>Cook Coal Seam</b>
-------------	-----------------------

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	2,330	28	0.36	190

- *Wall.* The Wall coal underlies the Cook coal seam by 250 feet of section.
  - *Area*. The Wall coal seam meets study inclusion criteria in one township in the northern portion of the partition.
  - *Coal Thickness*. The Wall seam coal thickness averages 30 feet.
  - *Coal Depth*. The depth to the top of the Wall seam averages 2,500 feet.
  - **Development**. Wall coal seam is undeveloped in Partition #7.
  - *Time Zero Well*. Not available.

2,530

Average

- *Type Well*. The history-matched Wall well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Wall type well for Partition #7:

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)

30

#### Table 6-52. Wall Coal Seam

- *Pawnee*. The Pawnee coal seam underlies the Wall coal in this partition.
  - *Area*. The Pawnee coal seam meets study inclusion criteria in one township in the southeastern portion of the partition.

0.36

390

- *Coal Thickness*. The Pawnee seam coal thickness averages 40 feet.
- *Coal Depth*. The depth to the top of the Pawnee seam averages 2,050 feet.
- **Development**. The Pawnee coal seam is undeveloped in Partition #7.
- *Time Zero Well*. Not available.
- **Type Well**. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Pawnee type well for this partition.

Table 6-53.	Pawnee	<b>Coal Seam</b>
-------------	--------	------------------

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	2,090	40	0.47	530

- *Cache*. The Cache seam is the deepest major coal seam, both stratigraphically and structurally, in Partition #7. It is nearly 600 feet below the Pawnee seam.
  - *Area*. The Cache coal seam meets study inclusion criteria in 3 townships in the northern and central portions of the partition.
  - *Coal Thickness*. The Cache seam coal thickness averages 30 feet in each of the 3 townships.
  - *Coal Depth*. The depth to the top of the Cache seam averages 2,623 feet, with a depth range of 2,200 to 2,980 feet.
  - **Development**. The Cache coal seam is undeveloped in Partition #7.
  - *Time Zero Well*. Not available.
  - *Type Well*. The history-matched Cache well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cache type well for Partition #7:

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	2,650	30	0.38	400

 Table 6-54.
 Cache Coal Seam

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Wasatch	6	540	25	47	290	230
Roland	3	820	27	70	250	200
Smith	2	1,180	20	96	160	90
Anderson	5	910	21	75	320	230
Canyon	2	1,500	25	120	250	150
Cook	2	2,300	28	178	400	210
Wall	1	2,500	30	186	210	100
Pawnee	1	2,050	40	160	250	140
Cache	3	2,623	30	190	680	330
Totals					2,820	1,680

 Table 6-55. In-Place and Technically Recoverable CBM, Partition #7

\* To top of coal

# 6.8 Partition #8

## 6.8.1 Summary

The main features of Partition #8, in the Wyoming portion of the Powder River Basin, are as follows:

- The partition covers a 41-township area in the northeastern portion of the Powder River Basin, from 53N to 58N and from 72W to78W, Figure 6-38.
- Partition #8 contains 9 major coal seams in the Fort Union Formation. The depth of these coals ranges from about 300 to 2,770 feet, with coal seam thickness ranging from 20 to 85 feet (township level averages). The gas in place in the partition is 9.2 Tcf, with technically recoverable gas of 7,020 Bcf. The results, by coal seam, are provided in Table 6-64.

## 6.8.2 Discussion of Major Seams

- *Smith*. The Smith coal seam is the shallowest major coal seam in Partition #8.
  - *Area*. The Smith coal seam meets study inclusion criteria in 8 townships, most of which are located in the southern portion of Partition #8.
  - *Coal Thickness*. The Smith seam coal thickness averages 33 feet, with a range of 20 to 38 feet.
  - *Coal Depth*. The depth to the top of the Smith seam averages 430 feet, with a range of 300 to 500 feet.

			L,												r	-	
68 + + 6	: e⊡ +5	E	68 46E	63 47 E		63 48E		63 49 E	I	68 506	E	68 51	E	68 52	E	@ 53E	
78 + + E	73 456		78 <b>4</b> 5E	78 +7 E		78 48E		78 49E		78 50E	•	78 51	E	78 52		78 5 3 E	1
83 + 41	E 884	ьSE	88 +6 E	83 47 E	•	83 <b>4</b> 8E	:	80 49E		æ 50E	E	88 51	E	88 52	•	æ 53E	
96 + 46	≣ 984	5E	98 46 E	98 47 E	•	98 48E		98 49E		98 508	E	98 51	E	96 52	E	98 5 3 E	:
	<b>TH 1000</b>	-		26101	-81	750	-81	7 4101	_	10107	531	7 200	98 <b>I</b>	7 1WI	SHTO		53 <b>H</b> 69V
98W 79W	95 <b>8</b> 7 8/V	58 <b>8</b> 77W								58 7 599							
57 H 75WI	57 NI 7 8/V	57 # 77W	5	7 # 76W	51	7500	51	17 400	5	7# 73W	5 H	7 2/V	ទេង	7 11/1	57 N 70V	, \ \	57 N 69/
95 H 7 9VV	95 <b>H</b> 78W	95 H 771		5# 76W	95 H 1	75N	51	7 40/0	55	N 73VV	551	17 290	58 H	7 11/1	96N 70V	v	95 1/21
55 N 79W	95 N 781AI	55 H 77V	N S	5N 76W	95 N 7	' SW	£∎	7 400	55	N 73VV	551	17 29/1	55 N	7 1I/V	55N 70V	v	55N 694
r™ Cle	swa 7800 armont	54 N 77V	N E	4N 76W	548 1	75N	54 11	7 400	54	N 73W	541	17 290	5411	7 11/1	5+W 70V	v	54N 690
53# 79W	53# 79W	(F) # 77V	v) I	3N 76W	51	75W	ទា	7 4/11	5	N 73VV	ទា	7 200	51	7 IVV	53N 70V	v	53N 694
5	Mar -	-	<u> </u>	≌N 76W	21	75W	21	7 4/11	Ę	ж <sup>7</sup> зw		1 2W	21	1 7 11/1	52 <b>1</b> 70	w	2 <b>8</b> 69
5		-	4	SIN 76VV	51 N	75M	51 1	7 4/11	÷1	<b>*</b> 73W	L'AL			7 100	51N 70V	v	51N 69
s	t		-	DN 76VU	50 H T	75M	50 H	7400	Ð	H 73W	sur	Gi	lette		50 X 70V	v	90 N 694
	-	-												Slee	руН	ollo	w
49N 79W	4911 7 SI/V	49H 77W	ı   4	9N 76W	617	5/1	68	7 44/1	0	N 73W	.ew	7 200	en e	11/1	491 700	v	<b>491</b> 691

Figure 6-38. Partition #8 Base Map

- *Development*. The are a total of 66 drilled and permitted Smith CBM wells in Partition #8.
- *Time Zero Plot*. Not available.
- *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Smith coal seam in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	460	33	0.15	130
High	500	38	0.18	150
Low	320	20	0.06	80

Table 6-56. Smith Coal Seam

- *Swartz*. The Swartz seam lies stratigraphically below the Smith seam, separated by an average of 150 feet of section.
  - *Area*. The Swartz coal seam meets study inclusion criteria in 2 township located in the southern portion of the partition.
  - *Coal Thickness*. The Swartz seam coal thickness averages 21 feet.
  - *Coal Depth*. The depth to the top of the Swartz seam averages 580 feet.
  - **Development**. The Swartz coal seam is undeveloped in Partition #8.
  - *Time Zero Plot*. Not available.

٠

- *Type Well*. After adjustment for depth, gas content, permeability and coal thickness, the type well for the Smith coal seam in Partition #5 serves as the type well for the Swartz coal seam in Partition #8.

Table 6-57.	Swartz	Coal	Seam
-------------	--------	------	------

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	600	21	0.12	80

• *Anderson*. The Anderson seam is often grouped with the underlying Canyon coal seam as the Wyodak coal. Close stratigraphic proximity with the Canyon makes recognition of the Anderson difficult in much of the partition.

- *Area*. The Anderson coal seam meets study inclusion criteria in 9 townships located in the southern and central portions of the partition.
- *Coal Thickness*. The Anderson coal seam thickness averages 35 feet, with a range of 25 to 50 feet.
- *Coal Depth*. The depth to the top of the Anderson seam averages 600 feet, with a range of 400 to 900 feet.
- *Development*. The are a total of 532 drilled and permitted Anderson CBM wells in Partition #8.
- *Time Zero Plot*. The time zero plot for 261 producing Anderson coal seam wells is provided in Figure 6-39. Initial water rates are 130 barrels per day declining to about 90 barrels per day after 1 year. Gas production begins immediately with an initial rate of 30 Mcfd. The gas rate peaks at 135 Mcfd at the beginning of year 2.
- *Type Well*. The history-matched type well for the Anderson coal seam is provided in Figure 6-40. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows in the table below.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	630	35	0.18	90
High	710	50	0.29	130
Low	630	25	0.13	70

### Table 6-58. Anderson Coal Seam

- *Canyon*. The Canyon seam is stratigraphically below the Anderson seam but is often difficult to distinctly identify.
  - *Area*. The Canyon coal seam meets study inclusion criteria in 19 townships throughout the partition.
  - *Coal Thickness*. The Canyon seam coal thickness averages 37 feet, with a range of 30 to 47 feet.
  - *Coal Depth*. The depth to the top of the Canyon seam averages 620 feet, with a depth range of 300 to 950 feet.
  - *Development*. The are a total of 1184 drilled and permitted Canyon CBM wells in this partition.
  - *Time Zero Well*. Not available.



Figure 6-39. Anderson Time Zero Plot



Figure 6-40. Anderson Type Well, Partition #8

- *Type Well*. The history-matched Canyon well in Partition #4, adjusted for depth, gas content, permeability and coal thickness serves as the Canyon type well in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	660	37	0.24	280
High	950	47	0.45	360
Low	560	30	0.17	230

## Table 6-59. Canyon Coal Seam

- *Cook.* The Cook coal seam is about 100 feet below the Canyon coal seam.
  - *Area*. The Cook coal seam meets study inclusion criteria in 22 townships throughout the partition.
  - *Coal Thickness*. The Cook seam coal thickness averages 39 feet, ranging from 25 to 52 feet.
  - *Coal Depth*. The depth to the top of the Cook seam averages 730 feet, with a depth range of 400 to 1,200 feet.
  - *Development*. The are a total of 1,211 drilled and permitted Cook CBM wells in Partition #8.
  - *Time Zero Plot*. The time zero plot for 134 producing Cook coal seam wells is provided in Figure 6-41. Initial water rates are 400 barrels per day declining to about 200 barrels per day after 1 year. Gas production begins immediately with an initial rate of 70 Mcfd. The gas rate continues to climb through 18 months to 200 Mcfd.
  - **Type Well**. The history-matched type well for the Cook coal seam is provided in Figure 6-42. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows in Table 6-60.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	770	39	0.27	270
High	970	52	0.46	350
Low	530	25	0.12	170

## Table 6-60. Cook Coal Seam



Figure 6-41. Cook Time Zero Plot



Figure 6-42. Cook Type Well, Partition #8

- *Wall*. The Wall seam is stratigraphically below the Cook seam, separated by an average of 230 feet of section.
  - *Area*. The Wall coal seam meets study inclusion criteria in 21 townships throughout the partition.
  - *Coal Thickness*. The Wall seam coal thickness averages 30 feet, with a range of 20 to 40 feet.
  - *Coal Depth*. The depth to the top of the Wall seam averages 960 feet, with a depth range of 530 to 1,300 feet.
  - **Development**. The are 486 drilled and permitted Wall CBM wells in Partition #8.
  - **Time Zero Plot**. The time zero plot for 107 producing Cook coal seam wells is provided in Figure 6-43. Initial water rates are about 200 barrels per day and remain high for 15 months. Gas production begins slowly with an initial rate of 10 Mcfd. The gas rate gradually climbs to a maximum of 100 Mcfd at the end of 2 years.
  - *Type Well*. The history-matched type well for the Wall coal seam is provided in Figure 6-44. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows in Table 6-61.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	990	30	0.20	390
High	1,120	40	0.30	530
Low	800	20	0.11	260

 Table 6-61.
 Wall Coal Seam

- *Pawnee*. The Pawnee coal seam is the deepest, currently producing major coal in this partition.
  - Area. The Pawnee coal seam meets study inclusion criteria in 11 townships.
  - *Coal Thickness*. The Pawnee seam coal thickness averages 33 feet, ranging from 25 to 40 feet.
  - *Coal Depth*. The depth to the top of the Pawnee seam averages 1,060 feet, ranging from 600 to 1,400 feet.
  - *Development*. There are 150 Pawnee CBM wells drilled and permitted in Partition #8.



Figure 6-43. Wall Time Zero Plot



Figure 6-44. Wall Type Well Partition #8

- *Time Zero Well*. The time zero plot for 19 producing Pawnee coal seam wells is provided in Figure 6-45. Initial water rates are 300 barrels per day. Gas production begins slowly with an initial rate of 10 Mcfd, but steadily climbs to over 200 Mcfd in 8 months.
- *Type Well*. The history-matched type well for the Pawnee coal seam is provided in Figure 6-46. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows:

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,090	33	0.35	430
High	840	40	0.33	530
Low	1,330	25	0.33	330

Table 6-62. Pawnee Coal Seam

- *Cache*. The Cache seam is separated from the Pawnee seam by an average of 490 feet.
  - *Area*. The Cache coal seam meets study inclusion criteria in 4 townships.
  - *Coal Thickness*. The Cache seam coal thickness averages 27 feet, ranging from 20 to 40 feet.
  - *Coal Depth*. The depth to the top of the Cache seam averages 1,540 feet, ranging from 1,100 to 2,430 feet.
  - **Development**. The Cache coal seam is undeveloped in Partition #8.
  - *Time Zero Well*. Not available.
  - *Type Well*. The history-matched Cache well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Cache type well for this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,570	27	0.26	350
High	1,140	40	0.29	530
Low	1,370	20	0.18	260

Table 6-63. Cache Coal Seam



Figure 6-45. Pawnee Time Zero Plot



Figure 6-46. Pawnee Type Well Partition #8

- *Oedekoven*. The Oedekoven seam is the deepest major coal seam in Partition #8, an average of 1,000 feet below the Cache seam.
  - *Area*. The Oedekoven coal seam meets study inclusion criteria in 2 townships in the western portion of the partition.
  - *Coal Thickness*. The Oedekoven seam coal thickness averages 20 feet.
  - *Coal Depth*. The depth to the top of the Oedekoven seam averages 2,560 feet, with a depth range of 2,340 to 2,770 feet.
  - **Development**. The Oedekoven coal seam is undeveloped in Partition #8.
  - *Time Zero Well*. Not available.
  - *Type Well*. The history-matched Oedekoven well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Oedekoven type well for Partition #8.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	2,580	20	0.30	260

Table 0-04. Ueuekoven Coal Sean	<b>Table 6-64.</b>	Oedekoven	<b>Coal Seam</b>
---------------------------------	--------------------	-----------	------------------

Table 6-65. In-Place and Techni	cally Recoverable CBM. Partition #8
---------------------------------	-------------------------------------

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas In Place (Bcf)	Technically Recoverable (Bcf)
Smith	8	430	33	38	380	300
Swartz	2	580	21	49	90	70
Anderson	9	600	35	51	750	530
Canyon	19	620	37	54	1,810	1,560
Cook	22	730	39	62	2,280	1,800
Wall	21	960	30	80	1,890	1,230
Pawnee	11	1,060	33	87	1,200	1,070
Cache	4	1,550	27	123	490	290
Oedekoven	2	2,560	20	188	300	170
Totals					9,190	7,020

\* To top of coal

# 6.9 Partition #9

# 6.9.1 Summary

Partition #9 covers 22 townships in the eastern Montana portion of the Powder River Basin, Figure 6-47. Only one township in Partition #9 contains coal that meets the depth and thickness criteria of the study, the Pawnee seam, with 20 feet of coal at 1,075 feet. As such, the discussion of the Pawnee coal in this partition is combined into Partition #10, on the west of Partition #9.

## 6.10 Partition #10

# 6.10.1 Summary

The main features of Partition #10, in the western Montana portion of the Powder River Basin, are as follows:

- The partition covers a 10-township area on the western edge of the PRB, from 6S to 9S and from 39E to 41E, Figure 6-48.
- A series of coal mines exist in the townships along the northern edge and the coals shallow to the north; as a result, the townships on the northern edge of the partition are excluded.
- The stratigraphic section contains the Deitz (Anderson equivalent), the Monarch (Canyon equivalent), and the Carney (Cook equivalent) seams, plus the Pawnee coal seam from Partition #9. The depth of these coals range from 250 to 1,200 feet, with coal seam thickness ranging from 20 to 50 feet (township level averages).
- The gas in place in the two partitions is 1.0 Tcf, with technically recoverable gas of 860 Bcf. The results by coal seam are provided in Table 6-70.

# 6.10.2 Discussion of Major Seams

- *Dietz* (Anderson). The Dietz is the uppermost significant seam in Partition #10 and contains three subunits, called Dietz #1, #2, and #3.
  - *Area*. The Dietz coal seam meets study inclusion criteria in 2 townships, located in the southern portion of Partition #10.
  - **Coal Thickness**. The Dietz seam coal thickness averages 49 feet. The thickness of the Dietz in any locale depends on how many of the Dietz subunits are present and have been combined.
  - *Coal Depth*. The depth to the top of the Dietz seam averages 250 feet.
  - **Development.** A limited number of Dietz wells currently exist in this partition.
|     |                    | 1      |         | ٦            |        | _         | 5+1E           | 43 42 E |         | 43 H3E           | 6       | 44E              | 4G 45          | ie              | <b>4</b> 3 46 8 | I           | 43 47 E           |               | 43 48E          | 43 49 E        |
|-----|--------------------|--------|---------|--------------|--------|-----------|----------------|---------|---------|------------------|---------|------------------|----------------|-----------------|-----------------|-------------|-------------------|---------------|-----------------|----------------|
|     | - Me               |        | 2       | E            | 50 40E | 53        | 3 41E          | 50 42 E |         | 50 +3E           | 55      | ++E              | 53 45          | E               | 50 46E          |             | 55 47 E           |               | 53 48E          | 53 49 E        |
|     | -                  |        | -       | 6            | 40E    | 60 +1E    | e              | 3 42E   | 60 +3E  |                  | 65 ++E  |                  | 80 45E         | 68 (            | 6E              | 60 47 E     | •                 | 60 486        |                 | 63 49E         |
| 1   | -                  |        | 7       | 70           | 40E    | 78 +1E    | T              | I 42E   | 78 +3 E |                  | 73 + +E | 7                | S 45E          | 78 (            | 6E              | -<br>1947 ( |                   | 73 488        | :               | 78 <b>49</b> E |
| 8   | 37E                | 80 38E | 83 39E  |              | 40E    | 88 +1E    | 8              | 42E     | 80 43 E |                  | 80 ++E  |                  | 80 45E         | 8               | 3 46 E          | 88 +7       | 7 E               | 80 48E        |                 | 80 49E         |
| 98: | 37 E               | 96 38E | 90 39E  | 96           | IOE    | 98 +1E    | 50             | 42E     | 98 43E  |                  | 90 ++E  |                  | 90 <b>4</b> 5E | g               | ) 46 E          | 98 47       | E                 | 96 48E        |                 | 90 49E         |
| Ц   | 93 N 85VV          |        | 841/1   | 58 N 8 34VI  |        | N 821/1   | 58 N 811VI     | 581     | 80W     | 98 <b>H</b> 79 V | ,       | 98 N 78W         | 9              | B# 77VV         | 9               | BN 76VV     |                   | 75W           | 58 <b>H</b> 744 | v 581          |
|     | s™ ®SW<br>Ra       | anche  | ster    | 57 N 83W     | នា     | N 82W     | <b>ज ॥</b> 81W | 51      | 1 80W   | 57 N 79V         |         | <b>ମ 1</b> 7 ଖନା | s              | 1 7700          | 5               | 1 1 76/1    | 51                | 7 <i>5</i> /N | S N 74          | u 571          |
|     | 56 N 89/V          | 95     | N 8 470 | saaw<br>Sher | dan .  | 95 N 82/V | 95 N 81V       |         | EN SOW  | 95 N 79          | w       | 95 N 78V         | v              | 96 <b>8</b> 77W |                 | 5N 76W      | 55 N <sup>-</sup> | 7 5/1         | 95 # 7 4VI      | 95 N           |
|     | <b>1</b> 55 8 8970 | 51     | L BAW   | oner         | Gait   |           |                |         |         |                  |         |                  | _              |                 |                 |             |                   |               |                 |                |

Figure 6-47. Partition #9 Base Map

58 3 5E	5.	S 36E		5S 37E		5S 38E		58 39E	55 4 08		5S 41E		5S 42 E		5S 43E		58 44E	
			65	S 37E	65	38E	6S 39E		6S 40E	65	S & 1E	6	S 42E	65	43E	65 4 4	<u>.</u>	65
	7S 36E		15	37 E	75	38E	7 S 3 9 E		7S 40E	75	: 41E	75	3 4 2 E	75 (	3 E	75 i i e		754
	8S 36E		85	: 37 E	85	S 38 E	85 39	E	7 <u>.55</u> 40E 8540E	7.5j 85	S 4 1E	85	\$ 4 2 E	ľ.	- Ane		-	8:
	95 36E		95	37E	95	38E	95 391	=	95 4 DE	95	41E	95	42E	17	1	-	-	95
58 N 87 V	,   \R	an	che	son os ester	510	581	I 84W	58N 83V		8 N 82 W	58	N 81W	58	N 80 V	-	J.	7 -	N
57 N 87 W		57 N 86 W		57 N 85	w	57 N	84W	57 N 83 W	5	7 N 82W	57	N 81W					67.8	1 0 IAI

Figure 6-48. Partition #10 Base Map

- *Time Zero Plot*. The time zero plot for 22 recently drilled Dietz coal wells is provided in Figure 6-49.
- *Type Well*. The history-matched Dietz well in Partition #11, adjusted for depth, gas content and coal thickness, serves as the Dietz type well for Partition #10. Because the Dietz coal seam exists in only two townships, only one average well is used in Partition #10.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	300	49	0.16	410

Table 6-66. Dietz Coal Seam

- *Monarch* (Canyon). The major coal seam in Partition #10 is the Monarch, located in the southern portion of the partition.
  - Area. The Monarch coal seam meets study inclusion criteria in 7 townships.
  - *Coal Thickness*. The Monarch coal seam thickness averages 24 feet, with a range of 20 to 30 feet.
  - *Coal Depth*. The depth to the top of the Monarch seam averages 470 feet, with a range of 325 to 680 feet.
  - **Development**. Considerable Monarch coal well development exists in this partition.
  - *Time Zero Plot*. The time zero plot for 25 recently drilled Monarch coal wells is provided in Figure 6-50.
  - **Type Well**. The Monarch well production profile in Partition #10 is similar to the Monarch wells in Partition #11. Thus, the history-matched Monarch well in Partition #11, adjusted for depth, gas content and coal thickness, serves as the Monarch type well in this partition.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	490	24	0.12	420
High	580	30	0.17	530
Low	420	20	0.08	350

### Table 6-67. Monarch Coal Seam



Figure 6-49. Dietz Time Zero Plot

- *Carney* (Cook). The Carney coal seam exists at sufficient thickness in the central and southern portions of Partition #10.
  - Area. The Carney coal seam meets study inclusion criteria in seven townships.
  - *Coal Thickness*. The Carney coal seam thickness averages 23 feet, with a range of 15 to 35 feet.
  - *Coal Depth*. The depth to the top of the Carney seam averages 650 feet, with a range of 530 to 860 feet.
  - **Development**. The Carney coal seam is lightly developed.
  - *Time Zero Plot*. The time zero plot for 25 recently drilled Carney coal wells is provided in Figure 6-51.
  - *Type Well*. The history-matched Carney well in Partition #11, adjusted for depth, gas content, and coal thickness, serves as the Carney type well for Partition #10.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	670	23	0.15	390
High	685	35	0.23	590
Low	870	15	0.13	250

Table 6-68. Carney Coal Seam

- *Pawnee*. The Pawnee seam exists in Partition #9 (eastern Montana portion of the PRB) and includes one undesignated (wildcat) seam in Partition #10, as discussed above.
  - *Area*. The Pawnee coal seam (including the wildcat coal seam) meets study inclusion criteria in 3 townships.
  - *Coal Thickness*. The Pawnee seam coal thickness averages 20 feet, with a range of 20 to 22 feet.
  - *Coal Depth*. The depth to the top of the Pawnee seam averages 1,100 feet, with a range of 1,000 to 1,200 feet.
  - **Development**. The Pawnee coal seam is undeveloped.
  - *Time Zero Plot*. Not available.
  - *Type Well*. The history-matched Pawnee well in Partition #8, adjusted for depth, gas content, permeability and coal thickness, serves as the Pawnee type well for



Figure 6-50. Monarch Time Zero Plot

Partition #10. Because the Pawnee coal seam has relatively uniform depth and thickness, only an average well is used.

Table 6-69.	Pawnee	<b>Coal Sean</b>	n
-------------	--------	------------------	---

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,120	20	0.22	260

### Table 6-70. In-Place and Technically Recoverable CBM, Partitions #9 and #10

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable Resources (Bcf)
Deitz (Anderson)	2	250	49	25	100	90
Monarch (Canyon)	7	470	24	41	280	250
Carney (Cook)	7	650	23	55	380	330
Pawnee	3	1,080	20	88	210	190
Totals					970	860

\* Top of coal

## 6.11 Partition #11

### 6.11.1 Summary

The main features of Partition #11, in the Wyoming portion of the Powder River Basin, are as follows:

- The partition covers a 12-township area on the northwestern portion of the PRB, from 53N to 58N and from 82W to 84W, Figure 6-52.
- The stratigraphic section contains the locally named Dietz (Anderson equivalent), Monarch (Canyon equivalent), and Carney (Cook equivalent) coal seams. The depth of these coals range from 990 to 1,070 feet, with coal seam thickness ranging from 20 to 40 feet (township level averages).
- The gas in place in the two partition is 2.1 Tcf, with technically recoverable gas of 1,850 Bcf. The results by coal seam are provided in Table 6-76.



Figure 6-51. Cook-Carney Time Zero Plot

### 6.11.2 Discussion of Major Coal Seams

- *Dietz #1* (Anderson). The Dietz #1 coal, the first major seam, extends over much of the northern portion of Partition #11 and shallows along the western and northern edge of the partition.
  - *Area*. The Dietz #1 coal seam meets study inclusion criteria in 5 townships.
  - *Coal Thickness*. The Dietz #1 coal seam coal thickness averages 24 feet, with a range of 20 to 25 feet.
  - *Coal Depth*. The depth to the top of the Dietz #1 seam averages 910 feet, with a range of 300 to 1,840 feet.
  - *Development*. The Dietz #1 seam is being aggressively developed.
  - *Time Zero Plot*. The time zero plot for 191 producing Dietz (Anderson) coal seam wells in T57N, R83-84W is provided in Figure 6-53. After initial rates of nearly 300 barrels per day, water production declines sharply to about 180 barrels per day after 1 year. Gas production starts early at 100 to 200 Mcfd.
  - **Type Well**. The type well for the Dietz (Anderson) series of coal seams (Dietz #1, #2, and #3) is provided in Figure 6-54. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries for the Dietz #1 coal seam are as follows in Table 6-71.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	930	24	0.22	200
High	1,140	25	0.29	210
Low	800	20	0.16	170

 Table 6-71. Dietz #1 Coal Seam

- *Dietz* #2. The Dietz #2 coal, the second split of the larger Dietz (Anderson) seam, exists along the northern portion of Partition #11.
  - Area. The Dietz #2 coal seam meets study inclusion criteria in 5 townships.
  - *Coal Thickness*. The Dietz #2 coal seam coal thickness averages 24 feet, with a range of 20 to 30 feet.
  - *Coal Depth*. The depth to the top of the Dietz #2 seam averages 680 feet, with a range of 300 to 1,160 feet.



Figure 6-52. Partition #11 Base Map



Figure 6-53. Dietz (Anderson) Time Zero Plot

- **Development**. The Dietz #2 seam is lightly developed in this area.
- *Time Zero Plot*. The time zero plot and data for Dietz #2 coal seam wells are included in the overall Dietz time zero plot, discussed previously.
- *Type Well*. The type well for the Dietz #2 coal seam is the aggregate Dietz well, provided previously in Figure 6-54, adjusted for coal thickness, depth and gas content. The estimated gas and water recoveries are as follows in Table 6-72.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	700	24	0.17	200
High	1,190	30	0.36	250
Low	620	20	0.13	170

Table 6-72. Dietz #2 Coal Seam

*Dietz* #3. The Dietz #3 coal, the third split of the larger Dietz (Anderson) seam, exists along the northern portion of Partition #11.

٠

- *Area.* The Dietz #3 coal seam meets study inclusion criteria in 6 townships.
- *Coal Thickness*. The Dietz #3 coal seam coal thickness averages 22 feet, with a range of 20 to 25 feet.
- *Coal Depth*. The depth to the top of the Dietz #3 seam averages 1,030 feet, with a range of 350 to 1,970 feet.
- **Development**. The Dietz #3 seam is lightly developed in this area.
- *Time Zero Plot*. The time zero plot and data for Dietz #3 coal seam wells are included in the overall Dietz time zero plot, discussed previously.
- *Type Well*. The type well for the Dietz #3 coal seam is the aggregate Dietz well, provided previously in Figure 6-54, adjusted for coal thickness, depth and gas content. The estimated gas and water recoveries are as follows below.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,050	22	0.23	180
High	980	25	0.25	210
Low	600	20	0.12	170

 Table 6-73. Dietz #3 Coal Seam

- *Monarch* (Canyon). The Monarch coal is stratigraphically below the Dietz and extends over much of the partition. It shallows on the western edge of the PRB basin.
  - Area. The Monarch coal seam meets study inclusion criteria in 8 townships.
  - *Coal Thickness*. The Monarch coal seam thickness averages 22 feet, with a range of 20 to 25 feet.
  - *Coal Depth*. The depth to the top of the Monarch seam averages 1,070 feet, with a range of 500 to 2,200 feet.
  - **Development**. The Monarch coal seam is under development.
  - *Time Zero Plot*. The time zero plot for 147 producing Monarch (Canyon) coal seam wells in T57N, R83-84W is provided in Figure 6-55. Water production starts at 300 barrels per day and remains high for the first 2 years. Gas production starts early, reaching 200 Mcfd in year 2.
  - **Type Well**. The type well for the Monarch (Canyon) coal seam is provided in Figure 6-56. After normalizing for coal thickness, depth and gas content, the estimated gas and water recoveries are as follows:

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,090	24	0.26	430
High	1,340	25	0.32	440
Low	820	20	0.16	350

 Table 6-74.
 Monarch Coal Seam

- *Carney* (Cook). The Carney coal, stratigraphically below the Monarch, exists over a limited portion of the partition.
  - Area. The Carney coal seam meets study inclusion criteria in three townships.
  - *Coal Thickness*. The Carney seam coal thickness averages 23 feet, with a range of 20 to 30 feet.
  - *Coal Depth*. The depth to the top of the Carney seam averages 1,030 feet, with a range of 600 to 1,440 feet.
  - *Development*. The Carney coal seam is undeveloped.



Figure 6-54. Dietz (Anderson), Partition #11



Figure 6-55. Monarch (Canyon) Time Zero Plot

- *Time Zero Plot*. The time zero plot for 65 producing Carney (Cook) wells in Partition #11 is provided in Figure 6-57. After initial rates of about 300 barrels of water per day, the water rates decline to about 200 barrels per day at the end of year 1. Gas production starts early and peaks at about 200 Mcf at the end of year 1.
- **Type Well**. The history-matched Carney (Cook equivalent) well, Figure 6-58, adjusted for depth, gas content and coal thickness, serves as the Carney type well for Partition #11. Since only three townships include the Carney and the coal thickness is relatively uniform, only an average well is used.

Type Well	Well Depth (ft)	Coal Thickness (ft)	Cumulative Gas Recovery (Bcf)	Cumulative Water Recovery (M bls)
Average	1,050	23	0.23	390

Table 6-75.	Carney	Coal	Seam
1 abic 0-75.	Carney	Cuar	Stam

Table 6-76.	In-Place and	Technically	Recoverable	<b>CBM</b> , Partition	ns #11
-------------	--------------	-------------	-------------	------------------------	--------

Coal Seam	No. Full Townships	Average Depth (ft)*	Average Thickness (ft)	Average Gas Content (cf/ton)	Gas in Place (Bcf)	Technically Recoverable Resources (Bcf)
Deitz #1 (Anderson)	5	910	24	75	510	450
Dietz #2	5	680	24	58	330	290
Dietz #3	6	1,030	22	84	390	340
Monarch (Canyon)	8	1,070	24	88	640	570
Carney (Cook)	3	1,030	23	84	220	190
Totals					2,090	1,850

\* Top of coal



Figure 6-56. Monarch (Canyon), Partition #11



Figure 6-57. Carney (Cook) Time Zero Plot



Figure 6-58. Carney (Cook), Partition #11

# **APPENDIX A**

# GAS SORPTION CAPACITY AND GAS CONTENT FOR POWDER RIVER BASIN COALS

## INTRODUCTION

Considerable differences of opinion surround two closely related issues of importance to the outlook for coalbed methane in the Powder River Basin:

- First, what is the correct sorption (storage) capacity of the low rank PRB coals, and how does this sorption capacity change by coal depth and coal seam?
- Second, what is the actual (in situ) gas content in these coals, and are the PRB coals essentially fully saturated or undersaturated with gas?

Attempts to conclusively answer these two questions in the past have been impeded by the high permeability in the coals, difficulties with conventional gas content measurement approaches, and the presence of much lower than normal pressure conditions in the shallow coals.

This memorandum provides the data and assumptions used by Advanced Resources to address these two issues for the Powder River Basin in the DOE/NETL report "Powder River CBM Development and Produced Water Management Study" (PRB Study) of November, 2002.

### SUMMARY OF ADVANCED RESOURCES DATA AND METHODOLOGY

### Background

Operators in the basin have struggled greatly with the issue of the gas content and the level of gas saturation in the coal. Early gas content data, gathered in the 1980s, showed the shallow coals along the eastern portion of the PRB to hold little methane. This gas content data led to extremely low values for gas in place, considerably below the actual gas recovery volumes established by the producing CBM wells.

Further uncertainty was introduced by the significantly underpressured conditions of these shallow coals. For example, the Wyodak coal (in T47-48 R72) has a pressure gradient of 0.274 psi/ft, giving it a pressure of 163 psi (at a depth of 541 ft to top of coal with a coal thickness of 78 ft), approximately 35% less than a normal pressure of about 250 psi. This condition, plus the high water production and delay in the arrival of gas production in the initial sets of wells, led many to conclude that the coals were also undersaturated with gas. [As is further discussed below, high initial water production and delay in gas production was due to the high permeability of the coals and the immaturity of development (lack of sufficient numbers of bounded wells) in the basin.]

These data and observations led many operators to conclude that the PRB coals were uneconomic, delaying industry's entry into the basin.

## **Gas Content**

The Advanced Resources PRB Study assembled available gas content data and adsorption isotherms, appropriate for the low rank coals of the Powder River Basin, from the following sources:

- Past gas content data collected by the BLM and published gas content and isotherm data by industry and the USGS were used as a point of reference,
- Advanced Resources' own gas content and isotherm data collected for analogous low rank coals in other basins, and
- Verification of the gas content and isotherm data using history matching (with COMET3) of alternative isotherms against long-term (4+year) gas and water production data in the PRB.

The best fit coalbed methane isotherm was from actual gas content and isotherm data collected on an analogous overseas low rank coal basin. Advanced Resources was the on-site field service contractor for the gas content measurement for these coals and used Terra Tek (in our view one of the most consistent, high quality CBM labs) for the adsorption isotherm (sorption capacity). The moisture content, volatile matter and fixed carbon content of the overseas low rank coal and the PRB Wyodak coal were similar as shown on Table A-1.

	PRB Wyodak Coal * (59 Analyses)		Overseas Low Rank Coal **
	Average	Range	
Rank	Lignite/Su	Lignite/Sub-bituminous	
Fixed Carbon	33.5%	30-41%	32.4%
Volatile Matter	30.7%	26-33%	44.6%
Moisture Content	29.8%	23-37%	23.0%***
Ash	6%	3-12%	11%
Heating Value (Btu/lb)	8,224	7,420-9,310	7,440

Table A-1. Comparison PRB Wyodak Coal and Overseas Low Rank Coal

\* Source: Breckenridge, et al, (1974)

\*\* Source: Advanced Resources Int'l, Inc. (1995)

\*\*\* Moisture at 96% RH and 40°C

Figure A-1 provides the gas content isotherm used in the study of Powder River Basin coalbed methane. As a point of comparison, Figure A-2 provides the average synthesized adsorption isotherm for coal in the PRB assembled by the Wyoming BLM from earlier data.



Figure A-1. Gas Content Isotherm Used for Powder River Coalbed Methane



Figure A-2. Average Synthesized Adsorption Isotherm for 41 Coal Samples From the PRB, Based on a Compilation of Data From Public and Private Sources

## **Free Gas Saturation**

The nature of actual early time water and gas production from producing CBM wells in the basin was used to establish whether the PRB coals were undersaturated, fully saturated or contained free gas in the pore space:

- Gas and water production data were assembled and compiled for over selected 1,400 PRB CBM wells.
- Observation of production data from these 1,400 wells and history matching (with COMET3) of this production data was used to establish that the coals were (in general) fully gas saturated and, for certain seams, had free gas in the coal cleat and matrix system.

Based on this work, the PRB Study established that modest amounts of free gas exist in the coal cleat (fracture) and matrix porosity system for the shallower coal seams.

## FINDINGS BY OTHER INVESTIGATORS

### **Bustin and Downey**

The most recent, publicly available data on gas sorption and content for the Powder River Basin was presented by Bustin and Downey on the Dietz #3 (Anderson equivalent) coal in the northwestern portion of the PRB. Their work on the sorption capacity of the Dietz #3 coal (as a function of temperature and pressure) is provided in Figure A-3. The 20°C sorption capacity line would be reasonably representative of the upper Tongue River coals in the PRB.

- A. *Sorption Capacity*. The Sorption Capacity Isotherm used in the Advanced Resources Study is compared with the sorption isotherm of Bustin and Downey in Figure A-4, with the vertical scale enlarged for easier comparison. The overlay of the data shows that the Advanced Resources Sorption Capacity Isotherm for PRB coals is somewhat lower than the 20°C Sorption Capacity Isotherm of Bustin and Downey for the Dietz #3 coal.
- B. *Gas Content and Saturation*. In the same paper, Bustin and Downey provide a series of observations with respect to the gas content and gas saturation conditions for the coals in the PRB. (Note that when coals are saturated and/or have free gas, the gas content value is the same as the value on the Sorption Capacity Isotherm. And, it is not physically possible to have free gas and undersaturated coals at the same time). Bustin and Downey wrote:

"There have been some 12,000 coalbed methane gas wells in the Powder River Basin to date, to produce methane gas from Eocene Fort Union Formation coal seams. Most have targeted the thick Wyodak coal seam(s) along the eastern flank of the basin where the coals are saturated and/or have free gas...."



Figure A-3. Variation in Sorption Capacity with Temperature, Dietz #3 Coal



Figure A-4. Comparison of Bustin and Downey Adsorption Isotherm for Dietz #3 Coal with Advanced Resources Adsorption Isotherm for PRB Coals

"Free gas in coals is predicted wherever structural closure and uplift can be demonstrated. If the coals have been substantially uplifted, desorbed gas may partially flush the fractures resulting in lower water saturations. Near one of the coal mines on the east side of the Powder River Basin, coal seam gas contents and isotherm data, correlate very well and suggest the Wyodak coal is saturated at current pressure conditions although the gas content is markedly depleted as a result of depressurization."<sup>1</sup>

However, Bustin and Downey do state that they have observed that "some of the deeper coal seams, such as the Cache and Pawnee, may be void of methane in some areas", particularly in areas south of Gillette, while "these coals appear to contain (and produce) methane in areas north of Gillette."

#### **Empirical Observations of Production Data**

A. *Basic Mechanisms.* The production profile for a typical coalbed methane well is high initial water production with little to no gas production. As the water rate declines and the reservoir pressure decreases, gas is desorbed from the coal, moves through the coal matrix by diffusion and through the coal cleat system by Darcy flow to the production well. The need to establish a critical gas saturation and overcome the low initial relative permeability to gas further delay the arrival of the released methane in the production well.

Depending on reservoir and development conditions (and assuming no free gas), it may take 3 months to a year (or longer) to observe significant rates of gas production.

B. *Evidence of Free Gas and Fully Saturated Coals.* The early production of gas, as demonstrated by the 164 Wyodak coal wells drilled in the mid-1990s in T47-48N, R72W, Figure A-5, can only be explained by the presence of free gas. Advanced Resources reservoir simulation-based history matching of this set of wells, indicates the presence of 10% free gas in the matrix porosity and 5% free gas in the cleat system, Figure A-6.

To examine the difference that the presence or absence of free gas has on gas production rates and recovery, we set the free gas values to zero in our next simulation run, while helping other reservoir properties the same. The resulting production curve clearly shows that gas production is much lower and later than has actually occurred, Figure A-7.

Finally, we examine how the Wyodak coal wells would produce in this area if they were 23% to 66% undersaturated. The use of such extreme gas undersaturation values for the Wyodak coal provides a gas production curve that is many-fold lower than actually observed, making this coal essentially non-productive, as shown on Figures A-8 and A-9.

<sup>&</sup>lt;sup>1</sup>"Gas-in-place in the Powder River Basin: Coal Core – Why Do Them? Some Field Results, Comparisons, and Suggestion", R. Marc Bustin, the University of British Columbia, Vancouver, and Rover A. Downey, Energy Ingenuity Company, RMAG PTTC GTI 2002 Coalbed Methane Symposium, June 19, 2002.



Figure A-5. Wyodak Time Zero Well Data



Figure A-6. History Match Wyodak Type Well w/ Free Gas



Figure A-7. Reservoir Simulation of Wyodak Type Well w/ No Free Gas



Figure A-8. Reservoir Simulation of Wyodak Type Well w/ 23% Gas Undersaturation



Figure A-9. Reservoir Simulation of Wyodak Type Well w/ 66% Gas Undersaturation

Table A-2 provides a comparison of the results from reservoir modeling of the four gas saturation cases against actual production data.

		<b>Reservoir Simulation Output</b>				
	Actual	Fully Saturated		Undersaturated		
	Data	w/Free Gas	w/No Free Gas	23%	66%	
Gas Rate (Mcfd)						
@ 46 days	263	276	69	41	0	
@ 289 days	301	291	200	142	51	
Cumulative Gas Recovery (MMcf)						
@1,475 days	255	255	196	144	58	

Table A-2. Comparison of Gas Production Rates for Wyodak Type Well

Table A-3 provides data on key reservoir properties, such as coal seam depth, gas content, pressure, and porosity used in the history match and sensitivity cases for the Wyodak coals discussed in this memo.

		_	_	Pressure	Por	osity
Cool	Depth	Gas Content	Pressure Gradient	(Top of Coal)	Fracture	Matrix
Seam	(feet)	(cf/t)	(psi/ft)	(psi)	(%)	(%)
Wyodak (Partition #4)	541	65	0.274	163	1.0	6.0

Table A-3. Wyodak Coal Seam Properties

### **Evidence for Undersaturated Coals**

No doubt undersaturated coals exist for some of the coal seams in some portions of the basin, as discussed earlier by Bustin and Downey. Even in the Warrior Basin, some pockets of low gas saturation have been observed in seams where the coals have been breached by faults.

However, high early water production and a delay in gas production (accepted as normal in most other coal basins of the world) are not necessarily evidence that the coals are undersaturated. To examine this, we assembled data on a group of 38 Big George coal wells in a deep, immaturely developed portion of the basin. The time-zero gas and water production curve for these wells is provided in Figure A-10. The reservoir simulation history match for these wells showed that the coals were fully gas saturated (but with no free gas) and that the delayed onset of gas production was caused by the difficulties in drawing down reservoir pressure due to high permeability and the unconfined nature of the wells, Figure A-11.



Figure A-10. Big George Time Zero Well Data



Figure A-11. History Match Big George Type Well

As for the Wyodak, we examined how the Big George coal wells in this area would produce if they were 23% to 66% undersaturated. Again, the use of such extreme gas undersaturation values for the Big George coal provides gas production and recovery values that are much lower than actually observed, as shown in Figure A-12 for the 23% gas undersaturated case. (No gas production occurs from the Big George coal for the 66% undersaturated case during the first year).

Table A-4 provides a comparison of the results from reservoir modeling of the three gas saturation cases against actual production data.

		Reservoir Simulation Output				
	A stud	Fully Saturated	Undersat	turated		
	Data	w/No Free Gas	23%	66%		
Gas Production (N	/lcfd)					
@ 76 days	24	21	0	0		
@ 289 days	78	61	20	0		
Gas Recovery (M	Mcf)					

 Table A-4. Comparison of Gas Production Rates for Big George Type Well



Figure A-12. Reservoir Simulation of Big George Type Well w/23% Gas Undersaturation

Table A-5 provides the data on key reservoir properties, such as coal seam depth, gas content, pressure, and porosity used in the history match and sensitivity cases for the Big George coal discussed in the memo.

		0.00	Dressure	Pressure	Por	osity
Coal	Depth	Gas Content	Gradient	(Top of Coal)	Fracture	Matrix
Seam	(feet)	(cf/t)	(psi/ft)	(psi)	(%)	(%)
Big George (Partition #3)	1,000	86	0.320	335	0.2	4.0

Table A-5. Big George Coal Seam Propert
---

### **OTHER STUDIES**

The 1995 USGS National Assessment included estimates for coalbed methane in the Powder River Basin. Dudley Rice, of the USGS, collected the geologic and reservoir data and Advanced Resources conducted the reservoir simulations to establish recoverable gas. This past assessment included the following data for the coals in the PRB, Table A-6:

- The shallow coals were assumed to be fully gas saturated (desorption pressure equals reservoir pressure); the deep coals were assumed to be 86% gas saturated.
- The gas content for the shallow coals (at 500 feet and 165 psi) was calculated at 60 scf/ton; the gas content for the deep coals (at 1,250 feet and 490 psi) was calculated at 126 scf/ton.
- The shallow coals were assumed to have 30% free gas in the fracture system; the deep coals were assumed to have no free gas.

	Shallow	Deep
Coal Depth, feet	500	1,250
Coal Thickness, feet	90	90
Pressure Gradient, psi/ft	0.30	0.38
Initial Reservoir Pressure, psia	165	490
Initial Water (Gas) Saturation, %	70 (30)	100 (0)
In Situ Langmuir Volume, scf/ton <sup>a</sup>	562	562
Langmuir Pressure, psia	1,380	1,380
In Situ Gas Content, scf/ton <sup>a</sup>	60	126
Desorption Pressure, psia	165	390 <sup>b</sup>
Sorption Time, days	3	3
Reservoir Temperature, °F	72	100
Cleat Porosity, %	4	2
Pore Volume Compressibility, 10 <sup>-6</sup> psi <sup>-1</sup>	200	200
Cleat Spacing, inches	0.2	0.2
Gas Gravity	0.75	0.75
Water Viscosity at Reservoir Conditions, cp	0.96	0.69
Water Formation Volume Factor, RB/STB	1.01	1.01
Completion and Stimulation	Open-hole/Cased & Frac'd °	Cased & Frac'd $xf = 40$ ft <sup>d</sup>
Well Operation	Pump Down Schedule	150 bwpd Pump Rate
Well Spacing, acres/well	40	40
Aquifer Recharge Rate, bwpd	Weak (50), Strong (400)	None
Absolute Cleat Permeability, md	10, 50, 75	1, 5, 10

#### Table A-6. Reservoir Parameters for Powder River Basin (Fort Union Coals)

<sup>a</sup> In situ conditons include 3% ash and 20% moisture

<sup>b</sup> Deeper coals are 86% saturated relative to the adsorptive capacity

<sup>c</sup> Both completion types yield similar performance;  $r_w = 0.26$  ft used in simulations with no skin factor applied

<sup>d</sup> Assumes infinite conductivity fracture half-length (xf)

The comparison of gas content in the two studies, Table A-7 below, shows the PRB Study used somewhat lower gas content values for the PRB coals than those used in the 1995 USGS National Assessment.

	Shallow Coal		Deep Coal		
	1995 USGS	2002 ARI	1995 USGS	2002 ARI	
Pressure (psi)	165	165	490	490	
Gas Content (cf/t)	60	45	126	105	

Table A-7.	Comparison	of 1995 U	SGS and	2002 ARI	Values for	Gas	Content o	f PRB	Coals
------------	------------	-----------	---------	----------	------------	-----	-----------	-------	-------