

# Kansas City PM Characterization Study

## Final Report

### Appendix F

### Dynamometer Calculations

Assessment and Standards Division  
Office of Transportation and Air Quality  
U.S. Environmental Protection Agency

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## Calculations for the Dynamometer Determined Regulated Emissions

Individual phase and weighted regulated emissions rates and fuel economy were determined from both the modal and bag THC, CO, NO<sub>x</sub>, and CO<sub>2</sub> analyses. Emission rates were calculated according to procedures found in the Code of Federal Regulations (CFR) Title 40, Part 86, Paragraph 86.144-90. Methanol, formaldehyde, and methane were not measured, so emission rates for these compounds, as well as Non-Methane Hydrocarbon (NMHC) and Total hydrocarbon equivalent (THCE) were not determined.

Calculations were performed within a Lotus123 spreadsheet , *KC\_Regdata.wk4*, designed specifically for this study. The spreadsheet contained macros to import and process the modal data files and bag data files containing user input. The spreadsheet also served as a “log” file to distribute regulated emission results to study participants during the course of the study and is included as two separate files (one for Round 1 and one for Round 2) on the ERG study web site. The spreadsheet contains 203 data fields (including 22 blank fields included to improve readability) as listed in Table F-1. Specific calculations used for all calculated fields are described in the comments column of the Table. In reporting weighted emissions, the same phase weighting factors as used for the Federal Test Procedure were applied to this data set. Included within the spreadsheet are intermediary calculations for the NO<sub>x</sub> correction factor, V<sub>mix</sub>, and dilution factor, as follows:

$$\text{NOx correction factor} = 1 / (1 - 0.0047 \cdot (H - 75)),$$

where H = absolute humidity (grains H<sub>2</sub>O per lb dry air)

$$= \{(43.478)Ra \cdot Psat\} / \{Pb - (Psat \cdot Ra / 100)\}$$

where Ra = relative humidity (percent)

Pb = barometric pressure (in Hg)

Psat = saturated vapor pressure @ dry bulb temp (in Hg)

$$= 29.92 \cdot 218.167 / Pw,$$

where  $\text{Log}(Pw) = [A(x-t) + B(x-t)^2 + C(x-t)^4] / [t(1 + D(x-t))]$  and

$$A = 3.244$$

$$B = 0.005868$$

$$C = 0.0000000117$$

$$D = .002188$$

$$x = 647.27$$

$$t = T_{\text{dry}}, \text{ Farenheit.}$$

$$\mathbf{V_{mix}} = V_o \cdot N \cdot \{(Pb - P_{\text{pdp}}) \cdot 528 / (760 \cdot T_{\text{pdp}})\},$$

where V<sub>o</sub> = Volume of gas pumped by the PDP per revolution (cu ft / revolution)

N = number of PDP revolutions per test phase.

P<sub>pdp</sub> = PDP inlet pressure depression (mm Hg)

T<sub>pdp</sub> = average temperature at PDP inlet (degrees Rankine)

Pb = barometric pressure (mm Hg)

The constant, V<sub>o</sub> = 0.306 cu ft/rev, has been previously determined by propane injections. N is also considered a constant, determined from PDP rpm and phase duration.

$$\text{Dilution Factor} = 13.4 / \{CO_2 + (HC + CO) \cdot 10^{-4}\}$$

Where CO<sub>2</sub>, HC, and CO are the average dilute concentrations.

Emission rates (grams/mile) for each test phase for the regulated emissions were calculated from the following format:

$$\text{HC (gm/mile)} = \text{HC (ppmC)} \cdot 10^{-6} \cdot V_{\text{mix}} \cdot 16.33 \text{ (gm/cu ft) /Miles}$$

$$\text{CO (gm/mile)} = \text{CO (ppm)} \cdot 10^{-6} \cdot V_{\text{mix}} \cdot 32.97 \text{ (gm/cu ft) /Miles}$$

$$\text{CO}_2 \text{ (gm/mile)} = \text{CO}_2 (\%) \cdot 10^{-4} \cdot V_{\text{mix}} \cdot 51.81 \text{ (gm/cu ft) /Miles}$$

$$\text{NOx (gm/mile)} = \text{NOx (ppm)} \cdot 10^{-6} \cdot V_{\text{mix}} \cdot 54.16 \text{ (gm/cu ft) /Miles}$$

Since the fuel properties of the tested consumer vehicles were unknown, fuel properties for a “generic” fuel were used for fuel economy calculations. The control vehicle, however, was fueled with Indolene, so fuel properties for Indolene were used when performing fuel economy calculations for the control vehicle. Fuel economy was calculated as follows:

$$\text{Fuel Economy (mpg)} = \text{CGAL} / \{(.429 * \text{CO}) + (.273 * \text{CO}_2) + (0.8646 * \text{HC})\},$$

where CGAL = grams C / gallon fuel = 2350.00 and CO, CO<sub>2</sub>, and HC are grams/mile emitted per test phase.

**Table F-1. Data Fields for the Regulated Emission Calculation Spreadsheet.**

| Data Field # | Label               | Units           | Source         | Example Value     | Comment   |
|--------------|---------------------|-----------------|----------------|-------------------|---|
| 1            | Run#                |                 | Keyboard Input | 84101             | Test number   |
| 2            | Veh.Tag #           |                 | Keyboard Input | 763TTY            | Vehicle License Plate number  |
| 3            | Veh Yr, Make, Model |                 | Keyboard Input | 2004 Toyota Camry | Vehicle Make,model, and model year  |
| 4            | Odometer            | <i>Miles</i>    | Keyboard Input | 169043            | Vehicle odometer reading, may not be actual miles   |
| 5            | Inertia             | <i>Lbs</i>      | Keyboard Input | 3500              | Dynamometer test inertia used   |
| 6            | Hp@50mph            | <i>Hp</i>       | Keyboard Input | 7.2               | Dynamometer load used   |
| 7            | Time                |                 | Keyboard Input | 1:22 p.m.         | Test start time   |
| 8            | Date                |                 | Keyboard Input | 07/30/2004        | Test date   |
| 9            | Comments            |                 | Keyboard Input |                   |   |
| 10           | (Blank Field)       |                 |                |                   |   |
| 11           | Vo                  | <i>ACF/Rev</i>  | Keyboard Input | 0.306             | Positive displacement pump (PDP) volume per revolution  |
| 12           | PDP_Speed           | <i>Rpm</i>      | Keyboard Input | 1770              | PDP speed   |
| 13           | Ph_Length_1         | <i>Seconds</i>  | Constant       | 300               | Phase 1 duration  |
| 14           | Ph_Length_2         | <i>Seconds</i>  | Constant       | 1136              | Phase 2 duration  |
| 15           | Ph_Length_3         | <i>Seconds</i>  | Constant       | 300               | Phase 3 duration  |
| 16           | Pi_pdp              | <i>mmHg</i>     | Keyboard Input | 20.46             | PDP inlet pressure depression   |
| 17           | Pbaro.              | <i>mmHg</i>     | Realtime       | 742.87            | Barometric pressure   |
| 18           | Tpdp_1              | <i>degreesC</i> | Realtime       | 46.36             | PDP inlet air average temperature for Phase 1   |
| 19           | Tpdp_2              | <i>degreesC</i> | Realtime       | 46.91             | PDP inlet air average temperature for Phase 2   |
| 20           | Tpdp_3              | <i>degreesC</i> | Realtime       | 46.23             | PDP inlet air average temperature for Phase 3   |
| 21           | Vmix_1              | <i>Cu. Ft</i>   | Calculated     | 2361.87           | $Vo * (PDP\_Speed / Ph\_Length\_1 / 60) * \{(Pbaro - Pi\_pdp)/760\} * \{528 / ((Tpdp\_1 * 9 / 5) + 32 + 460)\}$ |
| 22           | Vmix_2              | <i>Cu. Ft</i>   | Calculated     | 8928.29           | $Vo * (PDP\_Speed / Ph\_Length\_2 / 60) * \{(Pbaro - Pi\_pdp)/760\} * \{528 / ((Tpdp\_2 * 9 / 5) + 32 + 460)\}$ |
| 23           | Vmix_3              | <i>Cu. Ft</i>   | Calculated     | 2362.83           | $Vo * (PDP\_Speed / Ph\_Length\_3 / 60) * \{(Pbaro - Pi\_pdp)/760\} * \{528 / ((Tpdp\_3 * 9 / 5) + 32 + 460)\}$ |
| 24           | (Blank Field)       |                 |                |                   |   |

| Data Field # | Label         | Units            | Source     | Example Value | Comment  |
|--------------|---------------|------------------|------------|---------------|--|
| 25           | Tamb          | <i>F</i>         | Realtime   | 77.4          | Average ambient temperature during all test Phases and hot soak.   |
| 26           | Rel_Hum       | %                | Realtime   | 49.9          | Average relative humidity during all test Phases and hot soak.   |
| 27           | DryBulbT      | <i>degrees K</i> | Calculated | 298.4         | $(T_{amb} - 32) * (5/9) + 273.15$  |
| 28           | PsatDry       | <i>inHg</i>      | Calculated | 0.94648       | $29.92 * 218.167 / (@EXP(@LN(10) * (647.27 - DryBulbT) / DryBulbT * (3.2437814 + 0.00586826 * (647.27 - DryBulbT) + 1.1702379E-008 * (647.27 - DryBulbT)^3) / (1 + (0.0021878462 * (647.27 - DryBulbT))))))$ |
| 29           | Spec_Humidity | <i>Grains/lb</i> | Calculated | 71.31191      | $4347.8 * (Rel\_Hum / 100) * PsatDry / \{(P_{baro} / 25.4) - PsatDry * (Rel\_Hum / 100)\}$   |
| 30           | NOx_Corr_Fac  |                  | Calculated | 0.98296       | $1 / \{1 - 0.0047 * (Spec\_Humidity - 75)\}$   |
| 31           | (Blank Field) |                  |            |               |  |
| 32           | RR_Spd_1      | <i>MPH</i>       | Realtime   | 14.3732       | Average speed for Phase 1 (t=1 to 301seconds)  |
| 33           | RR_Spd_2      | <i>MPH</i>       | Realtime   | 27.5901       | Average speed for Phase 2 (t=302 to 1437 seconds)  |
| 34           | RR_Spd_3      | <i>MPH</i>       | Realtime   | 14.2443       | Average speed for Phase 3 (t=2037 to 2337 seconds)   |
| 35           | RR_Dist_1     | <i>Miles</i>     | Calculated | 1.198         | Test distance for phase 1= $RR\_Spd\_1 * Ph\_Length\_1 / 3600$   |
| 36           | RR_Dist_2     | <i>Miles</i>     | Calculated | 8.706         | Test distance for phase 2= $RR\_Spd\_2 * Ph\_Length\_2 / 3600$   |
| 37           | RR_Dist_3     | <i>Miles</i>     | Calculated | 1.187         | Test distance for phase 3= $RR\_Spd\_3 * Ph\_Length\_3 / 3600$   |
| 38           | (Blank Field) |                  |            |               |  |
| 39           | HC_1_Exh_m    | <i>ppmC</i>      | Realtime   | 102.562       | Avg HC concentration Phase 1 (t = 1 to 301 seconds)  |
| 40           | HC_1_Bkg_m    | <i>ppmC</i>      | Realtime   | 2.733         | Avg HC concentration Hot Soak Background (t = 1494 to 1994 seconds)  |
| 41           | HC_2_Exh_m    | <i>ppmC</i>      | Realtime   | 27.095        | Avg HC concentration Phase 2 (t = 317 to 1437 seconds)   |
| 42           | HC_2_Bkg_m    | <i>ppmC</i>      | Realtime   | 2.733         | Avg HC concentration Hot Soak Background (t = 1494 to 1994 seconds)  |
| 43           | HC_3_Exh_m    | <i>ppmC</i>      | Realtime   | 15.615        | Avg HC concentration Phase 3 (t = 2037 to 2337 seconds)  |
| 44           | HC_3_Bkg_m    | <i>ppmC</i>      | Realtime   | 2.733         | Avg HC concentration Hot Soak Background (t = 1494 to 1994 seconds)  |

| <b>Data Field #</b> | <b>Label</b>  | <b>Units</b> | <b>Source</b> | <b>Example Value</b> | <b>Comment</b>   |
|---------------------|---------------|--------------|---------------|----------------------|--|
| 45                  | (Blank Field) |              |               |                      |  |
| 46                  | NOx_1_Exh_m   | <i>Ppm</i>   | Realtime      | 42.574               | Avg NOx concentration Phase 1 (t = 1 to 301 seconds)                 |
| 47                  | NOx_1_Bkg_m   | <i>Ppm</i>   | Realtime      | 0.008                | Avg NOx concentration Hot Soak Background (t = 1494 to 1994 seconds) |
| 48                  | NOx_2_Exh_m   | <i>Ppm</i>   | Realtime      | 36.455               | Avg NOx concentration Phase 2 (t = 317 to 1437 seconds)              |
| 49                  | NOx_2_Bkg_m   | <i>Ppm</i>   | Realtime      | 0.008                | Avg NOx concentration Hot Soak Background (t = 1494 to 1994 seconds) |
| 50                  | NOx_3_Exh_m   | <i>Ppm</i>   | Realtime      | 24.800               | Avg NOx concentration Phase 3 (t = 2037 to 2337 seconds)             |
| 51                  | NOx_3_Bkg_m   | <i>Ppm</i>   | Realtime      | 0.008                | Avg NOx concentration Hot Soak Background (t = 1494 to 1994 seconds) |
| 52                  | (Blank Field) |              |               |                      |  |
| 53                  | CO_1_Exh_m    | <i>Ppm</i>   | Realtime      | 613.094              | Avg CO concentration Phase 1 (t = 1 to 301 seconds)                  |
| 54                  | CO_1_Bkg_m    | <i>Ppm</i>   | Realtime      | 0.379                | Avg CO concentration Hot Soak Background (t = 1494 to 1994 seconds)  |
| 55                  | CO_2_Exh_m    | <i>Ppm</i>   | Realtime      | 675.482              | Avg CO concentration Phase 2 (t = 317 to 1437 seconds)               |
| 56                  | CO_2_Bkg_m    | <i>Ppm</i>   | Realtime      | 0.379                | Avg CO concentration Hot Soak Background (t = 1494 to 1994 seconds)  |
| 57                  | CO_3_Exh_m    | <i>Ppm</i>   | Realtime      | 181.040              | Avg CO concentration Phase 3 (t = 2037 to 2337 seconds)              |
| 58                  | CO_3_Bkg_m    | <i>Ppm</i>   | Realtime      | 0.379                | Avg CO concentration Hot Soak Background (t = 1494 to 1994 seconds)  |
| 59                  | (Blank Field) |              |               |                      |  |
| 60                  | CO2_1_Exh_m   | %            | Realtime      | 0.631                | Avg CO2 concentration Phase 1 (t = 1 to 301 seconds)                 |
| 61                  | CO2_1_Bkg_m   | %            | Realtime      | 0.044                | Avg CO2 concentration Hot Soak Background (t = 1494 to 1994 seconds) |
| 62                  | CO2_2_Exh_m   | %            | Realtime      | 0.723                | Avg CO2 concentration Phase 2 (t = 317 to 1437 seconds)              |
| 63                  | CO2_2_Bkg_m   | %            | Realtime      | 0.044                | Avg CO2 concentration Hot Soak Background (t = 1494 to 1994 seconds) |
| 64                  | CO2_3_Exh_m   | %            | Realtime      | 0.515                | Avg CO2 concentration Phase 3 (t = 2037 to 2337 seconds)             |
| 65                  | CO2_3_Bkg_m   | %            | Realtime      | 0.044                | Avg CO2 concentration Hot Soak Background (t = 1494 to 1994 seconds) |
| 66                  | (Blank Field) |              |               |                      |  |

| Data Field # | Label         | Units   | Source     | Example Value | Comment   |
|--------------|---------------|---------|------------|---------------|---|
| 67           | SPCO2         | %       | Constant   | 13.40         | Engine out CO2 (%) emitted at Stoichiometry = 13.4 for both INDOLINE and UNKNOWN fuels.   |
| 68           | DilFac_1_m    |         | Calculated | 19.07         | Dilution Factor Phase 1 = $SPCO2 / \{CO2\_1\_Exh\_m + (CO\_1\_Exh\_m * 0.0001) + (HC\_1\_Exh\_m * 0.0001)\}$  |
| 69           | DilFac_2_m    |         | Calculated | 16.90         | Dilution Factor Phase 2 = $SPCO2 / \{CO2\_2\_Exh\_m + (CO\_2\_Exh\_m * 0.0001) + (HC\_2\_Exh\_m * 0.0001)\}$  |
| 70           | DilFac_3_m    |         | Calculated | 25.08         | Dilution Factor Phase 3 = $SPCO2 / \{CO2\_3\_Exh\_m + (CO\_3\_Exh\_m * 0.0001) + (HC\_3\_Exh\_m * 0.0001)\}$  |
| 71           | (Blank Field) |         |            |               |   |
| 72           | HC_Density    | gm/cuft | Constant   | 16.33         | Density of HC   |
| 73           | NOx_Density   | gm/cuft | Constant   | 54.16         | Density of NOx  |
| 74           | CO_Density    | gm/cuft | Constant   | 32.97         | Density of CO   |
| 75           | CO2_Density   | gm/cuft | Constant   | 51.81         | Density of CO2  |
| 76           | HC_1_mass_m   | Gm      | Calculated | 3.856         | HC mass for Phase 1 = $Vmix\_1 * HC\_Density * \{HC\_Exh\_1\_m - HC\_Bkg\_1\_m * (1 - 1/DilFac\_1\_m)\} / 1,000,000$                                  |
| 77           | HC_2_mass_m   | Gm      | Calculated | 3.576         | HC mass for Phase 2 = $Vmix\_2 * HC\_Density * \{HC\_Exh\_2\_m - HC\_Bkg\_2\_m * (1 - 1/DilFac\_2\_m)\} / 1,000,000$                                  |
| 78           | HC_3_mass_m   | Gm      | Calculated | 0.501         | HC mass for Phase 3 = $Vmix\_3 * HC\_Density * \{HC\_Exh\_3\_m - HC\_Bkg\_3\_m * (1 - 1/DilFac\_3\_m)\} / 1,000,000$                                  |
| 79           | NOx_1_mass_m  | Gm      | Calculated | 5.445         | NOx mass for Phase 1 = $Vmix\_1 * NOx\_Density * \{NOx\_Exh\_1\_m - NOx\_Bkg\_1\_m * (1 - 1/DilFac\_1\_m)\} / 1,000,000$                              |
| 80           | NOx_2_mass_m  | Gm      | Calculated | 17.625        | NOx mass for Phase 2 = $Vmix\_2 * NOx\_Density * \{NOx\_Exh\_2\_m - NOx\_Bkg\_2\_m * (1 - 1/DilFac\_2\_m)\} / 1,000,000$                              |
| 81           | NOx_3_mass_m  | Gm      | Calculated | 3.173         | NOx mass for Phase 3 = $Vmix\_3 * NOx\_Density * \{NOx\_Exh\_3\_m - NOx\_Bkg\_3\_m * (1 - 1/DilFac\_3\_m)\} / 1,000,000$                              |
| 82           | NOx_1_mass_mc | Gm      | Calculated | 5.352         | NOx (corrected) mass for Phase 1 = $Vmix\_1 * NOx\_Density * NOx\_Corr\_Fac * \{NOx\_Exh\_1\_m - NOx\_Bkg\_1\_m * (1 - 1/DilFac\_1\_m)\} / 1,000,000$ |
| 83           | NOx_2_mass_mc | Gm      | Calculated | 17.324        | NOx (corrected) mass for Phase 2 = $Vmix\_2 *$  |



| Data Field # | Label         | Units   | Source     | Example Value | Comment   |
|--------------|---------------|---------|------------|---------------|---|
|              |               |         |            |               | $\text{NOx\_Density} * \text{NOx\_Corr\_Fac} * \{\text{NOx\_Exh\_2\_m} - \text{NOx\_Bkg\_2\_m} * (1 - 1/\text{DilFac\_2\_m})\} / 1,000,000$   |
| 84           | NOx_3_mass_mc | Gm      | Calculated | 3.119         | $\text{NOx (corrected) mass for Phase 3} = \text{'Vmix\_3} * \text{NOx\_Density} * \text{NOx\_Corr\_Fac} * \{\text{NOx\_Exh\_3\_m} - \text{NOx\_Bkg\_3\_m} * (1 - 1/\text{DilFac\_3\_m})\} / 1,000,000$ |
| 85           | CO_1_mass_m   | Gm      | Calculated | 47.714        | $\text{CO mass for Phase 1} = \text{'Vmix\_1} * \text{CO\_Density} * \{\text{CO\_Exh\_1\_m} - \text{CO\_Bkg\_1\_m} * (1 - 1/\text{DilFac\_1\_m})\} / 1,000,000$   |
| 86           | CO_2_mass_m   | Gm      | Calculated | 198.734       | $\text{CO mass for Phase 2} = \text{'Vmix\_2} * \text{CO\_Density} * \{\text{CO\_Exh\_2\_m} - \text{CO\_Bkg\_2\_m} * (1 - 1/\text{DilFac\_2\_m})\} / 1,000,000$   |
| 87           | CO_3_mass_m   | Gm      | Calculated | 14.075        | $\text{CO mass for Phase 3} = \text{'Vmix\_3} * \text{CO\_Density} * \{\text{CO\_Exh\_3\_m} - \text{CO\_Bkg\_3\_m} * (1 - 1/\text{DilFac\_3\_m})\} / 1,000,000$   |
| 88           | CO2_1_mass_m  | Gm      | Calculated | 721.378       | $\text{CO2 mass for Phase 1} = \text{'Vmix\_1} * \text{CO2\_Density} * \{\text{CO2\_Exh\_1\_m} - \text{CO2\_Bkg\_1\_m} * (1 - 1/\text{DilFac\_1\_m})\} / 100$   |
| 89           | CO2_2_mass_m  | Gm      | Calculated | 3152.989      | $\text{CO2 mass for Phase 2} = \text{'Vmix\_2} * \text{CO2\_Density} * \{\text{CO2\_Exh\_2\_m} - \text{CO2\_Bkg\_2\_m} * (1 - 1/\text{DilFac\_2\_m})\} / 100$   |
| 90           | C2O_3_mass_m  | Gm      | Calculated | 578.488       | $\text{CO2 mass for Phase 3} = \text{'Vmix\_3} * \text{CO2\_Density} * \{\text{CO2\_Exh\_3\_m} - \text{CO2\_Bkg\_3\_m} * (1 - 1/\text{DilFac\_3\_m})\} / 100$   |
| 91           | (Blank Field) |         |            |               |   |
| 92           | HC_1_ER_m     | gm/mile | Calculated | 3.219         | $\text{HC Emission Rate for Phase 1} = \text{HC\_1\_mass\_m} / \text{RR\_Dist\_1}$  |
| 93           | HC_2_ER_m     | gm/mile | Calculated | 0.411         | $\text{HC Emission Rate for Phase 2} = \text{HC\_2\_mass\_m} / \text{RR\_Dist\_2}$  |
| 94           | HC_3_ER_m     | gm/mile | Calculated | 0.422         | $\text{HC Emission Rate for Phase 3} = \text{HC\_3\_mass\_m} / \text{RR\_Dist\_3}$  |
| 95           | NOx_1_ER_m    | gm/mile | Calculated | 4.546         | $\text{NOx Emission Rate for Phase 1} = \text{NOx\_1\_mass\_m} / \text{RR\_Dist\_1}$  |
| 96           | NOx_2_ER_m    | gm/mile | Calculated | 2.024         | $\text{NOx Emission Rate for Phase 2} = \text{NOx\_2\_mass\_m} / \text{RR\_Dist\_2}$  |
| 97           | NOx_3_ER_m    | gm/mile | Calculated | 2.673         | $\text{NOx Emission Rate for Phase 2} = \text{NOx\_2\_mass\_m} / \text{RR\_Dist\_2}$  |

| Data Field # | Label         | Units   | Source     | Example Value | Comment  |
|--------------|---------------|---------|------------|---------------|--|
| 98           | NOx_1_ER_mc   | gm/mile | Calculated | 4.469         | Corrected NOx Emission Rate for Phase 1 =<br>NOx_1_mass_mc / RR_Dist_1   |
| 99           | NOx_2_ER_mc   | gm/mile | Calculated | 1.990         | Corrected NOx Emission Rate for Phase 2 =<br>NOx_2_mass_mc / RR_Dist_2   |
| 100          | NOx_3_ER_mc   | gm/mile | Calculated | 2.627         | Corrected NOx Emission Rate for Phase 3 =<br>NOx_3_mass_mc / RR_Dist_3   |
| 101          | CO_1_ER_m     | gm/mile | Calculated | 39.836        | CO Emission Rate for Phase 1 = CO_1_mass_m /<br>RR_Dist_1  |
| 102          | CO_2_ER_m     | gm/mile | Calculated | 22.827        | CO Emission Rate for Phase 2 = CO_2_mass_m /<br>RR_Dist_2  |
| 103          | CO_3_ER_m     | gm/mile | Calculated | 11.857        | CO Emission Rate for Phase 3 = CO_3_mass_m /<br>RR_Dist_3  |
| 104          | CO2_1_ER_m    | gm/mile | Calculated | 602.271       | CO2 Emission Rate for Phase 1 = CO2_1_mass_m /<br>RR_Dist_1  |
| 105          | CO2_2_ER_m    | gm/mile | Calculated | 362.153       | CO2 Emission Rate for Phase 2 = CO2_2_mass_m /<br>RR_Dist_2  |
| 106          | CO2_3_ER_m    | gm/mile | Calculated | 487.342       | CO2 Emission Rate for Phase 3 = CO2_3_mass_m /<br>RR_Dist_3  |
| 107          | (Blank Field) |         |            |               |  |
| 108          | HC_wt_ER_m    | gm/mile | Calculated | 0.558         | Weighted HC emission rate = $0.43 * \{(HC\_1\_mass\_m + HC\_2\_mass\_m) / (RR\_Dist\_1 + RR\_Dist\_2)\} + 0.57 * \{(HC\_3\_mass\_m + HC\_2\_mass\_m) / (RR\_Dist\_3 + RR\_Dist\_2)\}$                      |
| 109          | NOx_wt_ER_m   | gm/mile | Calculated | 2.200         | Weighted NOx emission rate = $0.43 * \{(NOx\_1\_mass\_m + NOx\_2\_mass\_m) / (RR\_Dist\_1 + RR\_Dist\_2)\} + 0.57 * \{(NOx\_3\_mass\_m + NOx\_2\_mass\_m) / (RR\_Dist\_3 + RR\_Dist\_2)\}$                 |
| 110          | NOx_wt_ER_mc  | gm/mile | Calculated | 2.162         | Weighted NOx (corrected) emission rate = $0.43 * \{(NOx\_1\_mass\_mc + NOx\_2\_mass\_mc) / (RR\_Dist\_1 + RR\_Dist\_2)\} + 0.57 * \{(NOx\_3\_mass\_mc + NOx\_2\_mass\_mc) / (RR\_Dist\_3 + RR\_Dist\_2)\}$ |
| 111          | CO_wt_ER_m    | gm/mile | Calculated | 22.961        | Weighted CO emission rate = $0.43 * \{(CO\_1\_mass\_m + CO\_2\_mass\_m) / (RR\_Dist\_1 + RR\_Dist\_2)\} + 0.57 * \{(CO\_3\_mass\_m + CO\_2\_mass\_m) / (RR\_Dist\_3 + RR\_Dist\_2)\}$                      |
| 112          | CO2_wt_ER_m   | gm/mile | Calculated | 383.202       | Weighted CO2 emission rate = $0.43 * \{(CO2\_1\_mass\_m + CO2\_2\_mass\_m) / (RR\_Dist\_1 + RR\_Dist\_2)\} + 0.57 * \{(CO2\_3\_mass\_m + CO2\_2\_mass\_m) / (RR\_Dist\_3 + RR\_Dist\_2)\}$                 |

| Data Field # | Label         | Units              | Source         | Example Value | Comment  |
|--------------|---------------|--------------------|----------------|---------------|--|
|              |               |                    |                |               | {(CO2_3_mass_m + CO2_2_mass_m) / (RR_Dist_3 + RR_Dist_2)}                                      |
| 113          | (Blank Field) |                    |                |               |  |
| 114          | CRHC          | <i>Fuel Wt% C</i>  | Constant       | 0.840         | Weight percent carbon in fuel / 100 = 0.867 for INDOLINE and 0.840 for UNKNOWN fuels.          |
| 115          | CGAL          | <i>gmC/galFuel</i> | Constant       | 2350.000      | Carbon density in fuel = 2434 for INDOLINE and 2350 for UNKNOWN fuels.                         |
| 116          | FE_1_m        | <i>mpg</i>         | Calculated     | 12.76         | Fuel Economy for Phase 1 = GGAL / ( CRHC * HC_1_ER_m + 0.429 * CO_1_ER_m + 0.273 * CO2_1_ER_m) |
| 117          | FE_2_m        | <i>mpg</i>         | Calculated     | 21.56         | Fuel Economy for Phase 2 = GGAL / ( CRHC * HC_2_ER_m + 0.429 * CO_2_ER_m + 0.273 * CO2_2_ER_m) |
| 118          | FE_3_m        | <i>mpg</i>         | Calculated     | 16.97         | Fuel Economy for Phase 3 = GGAL / ( CRHC * HC_3_ER_m + 0.429 * CO_3_ER_m + 0.273 * CO2_3_ER_m) |
| 119          | FE_wt_m       | <i>mpg</i>         | Calculated     | 20.45         | Weighted Fuel Economy = GGAL / ( CRHC * HC_wt_ER_m + 0.429 * CO_wt_ER_m + 0.273 * CO2_wt_ER_m) |
| 120          | (Blank Field) |                    |                |               |  |
| 121          | HC_1_Exh_b    | <i>ppmC</i>        | Keyboard Input | 93.0          | Bag HC diluted exhaust concentration for Phase 1   |
| 122          | HC_1_Bkg_b    | <i>ppmC</i>        | Keyboard Input | 4.0           | Bag HC background concentration for Phase 1  |
| 123          | HC_2_Exh_b    | <i>ppmC</i>        | Keyboard Input | 30.0          | Bag HC diluted exhaust concentration for Phase 2   |
| 124          | HC_2_Bkg_b    | <i>ppmC</i>        | Keyboard Input | 4.0           | Bag HC background concentration for Phase 2  |
| 125          | HC_3_Exh_b    | <i>ppmC</i>        | Keyboard Input | 18.0          | Bag HC diluted exhaust concentration for Phase 3   |
| 126          | HC_3_Bkg_b    | <i>ppmC</i>        | Keyboard Input | 5.0           | Bag HC background concentration for Phase 3  |
| 127          | (Blank Field) |                    |                |               |  |
| 128          | NOx_1_Exh_b   | <i>Ppm</i>         | Keyboard Input | 27.7          | Bag NOx diluted exhaust concentration for Phase 1  |
| 129          | NOx_1_Bkg_b   | <i>Ppm</i>         | Keyboard Input | 0.0           | Bag NOx background concentration for Phase 1   |
| 130          | NOx_2_Exh_b   | <i>Ppm</i>         | Keyboard Input | 25.1          | Bag NOx diluted exhaust concentration for Phase 2  |
| 131          | NOx_2_Bkg_b   | <i>Ppm</i>         | Keyboard Input | 0.1           | Bag NOx background concentration for Phase 2   |
| 132          | NOx_3_Exh_b   | <i>Ppm</i>         | Keyboard Input | 23.4          | Bag NOx diluted exhaust concentration for Phase 3  |

| Data Field # | Label         | Units | Source         | Example Value | Comment  |
|--------------|---------------|-------|----------------|---------------|--|
| 133          | NOx_3_Bkg_b   | Ppm   | Keyboard Input | 0.2           | Bag NOx background concentration for Phase 3   |
| 134          | (Blank Field) |       |                |               |  |
| 135          | CO_1_Exh_b    | Ppm   | Keyboard Input | 601.0         | Bag CO diluted exhaust concentration for Phase 1   |
| 136          | CO_1_Bkg_b    | Ppm   | Keyboard Input | 0.0           | Bag CO background concentration for Phase 1  |
| 137          | CO_2_Exh_b    | Ppm   | Keyboard Input | 661.0         | Bag CO diluted exhaust concentration for Phase 2   |
| 138          | CO_2_Bkg_b    | Ppm   | Keyboard Input | 0.0           | Bag CO background concentration for Phase 2  |
| 139          | CO_3_Exh_b    | Ppm   | Keyboard Input | 183.0         | Bag CO diluted exhaust concentration for Phase 3   |
| 140          | CO_3_Bkg_b    | Ppm   | Keyboard Input | 0.0           | Bag CO background concentration for Phase 3  |
| 141          | (Blank Field) |       |                |               |  |
| 142          | CO2_1_Exh_b   | %     | Keyboard Input | 0.6319        | Bag CO2 diluted exhaust concentration for Phase 1  |
| 143          | CO2_1_Bkg_b   | %     | Keyboard Input | 0.0419        | Bag CO2 background concentration for Phase 1   |
| 144          | CO2_2_Exh_b   | %     | Keyboard Input | 0.7136        | Bag CO2 diluted exhaust concentration for Phase 2  |
| 145          | CO2_2_Bkg_b   | %     | Keyboard Input | 0.0404        | Bag CO2 background concentration for Phase 2   |
| 146          | CO2_3_Exh_b   | %     | Keyboard Input | 0.5300        | Bag CO2 diluted exhaust concentration for Phase 3  |
| 147          | CO2_3_Bkg_b   | %     | Keyboard Input | 0.0449        | Bag CO2 background concentration for Phase 3   |
| 148          | (Blank Field) |       |                |               |  |
| 149          | DilFac_1_b    |       | Calculated     | 19.11         | Dilution Factor Phase 1 = $\text{SPCO}_2 / \{ \text{CO}_2\text{_1\_Exh\_b} + (\text{CO\_1\_Exh\_b} * 0.0001) + (\text{HC\_1\_Exh\_b} * 0.0001) \}$                   |
| 150          | DilFac_2_b    |       | Calculated     | 17.12         | Dilution Factor Phase 2 = $\text{SPCO}_2 / \{ \text{CO}_2\text{_2\_Exh\_b} + (\text{CO\_2\_Exh\_b} * 0.0001) + (\text{HC\_2\_Exh\_b} * 0.0001) \}$                   |
| 151          | DilFac_3_b    |       | Calculated     | 24.36         | Dilution Factor Phase 3 = $\text{SPCO}_2 / \{ \text{CO}_2\text{_3\_Exh\_m} + (\text{CO\_3\_Exh\_m} * 0.0001) + (\text{HC\_3\_Exh\_m} * 0.0001) \}$                   |
| 152          | (Blank Field) |       |                |               |  |
| 153          | HC_1_mass_b   | Gm    | Calculated     | 3.441         | HC mass for Phase 1 = $\text{Vm}_{\text{mix\_1}} * \text{HC\_Density} * \{ \text{HC\_Exh\_1\_b} - \text{HC\_Bkg\_1\_b} * (1 - 1/\text{DilFac\_1\_b}) \} / 1,000,000$ |
| 154          | HC_2_mass_b   | Gm    | Calculated     | 3.825         | HC mass for Phase 2 = $\text{Vm}_{\text{mix\_2}} * \text{HC\_Density} * \{ \text{HC\_Exh\_2\_b} - \text{HC\_Bkg\_2\_b} * (1 - 1/\text{DilFac\_2\_b}) \} / 1,000,000$ |
| 155          | HC_3_mass_b   | Gm    | Calculated     | 0.509         | HC mass for Phase 3 = $\text{Vm}_{\text{mix\_3}} * \text{HC\_Density} * \{ \text{HC\_Exh\_3\_b} - \text{HC\_Bkg\_3\_b} * (1 - 1/\text{DilFac\_3\_b}) \} /$           |

| Data Field # | Label         | Units | Source     | Example Value | Comment   |
|--------------|---------------|-------|------------|---------------|---|
|              |               |       |            |               | 1,000,000   |
| 156          | NOx_1_mass_b  | Gm    | Calculated | 3.548         | NOx mass for Phase 1 = 'Vmix_1 * NOx_Density * {NOx_Exh_1_b - NOx_Bkg_1_b * (1 - 1/ DilFac_1_b)} / 1,000,000                            |
| 157          | NOx_2_mass_b  | Gm    | Calculated | 12.091        | NOx mass for Phase 2 = 'Vmix_2 * NOx_Density * {NOx_Exh_2_b - NOx_Bkg_2_b * (1 - 1/ DilFac_2_b)} / 1,000,000                            |
| 158          | NOx_3_mass_b  | Gm    | Calculated | 2.966         | NOx mass for Phase 3 = 'Vmix_3 * NOx_Density * {NOx_Exh_3_b - NOx_Bkg_3_b * (1 - 1/ DilFac_3_b)} / 1,000,000                            |
| 159          | NOx_1_mass_bc | Gm    | Calculated | 3.488         | NOx (corrected) mass for Phase 1 = 'Vmix_1 * NOx_Density * NOx_Corr_Fac * {NOx_Exh_1_b - NOx_Bkg_1_b * (1 - 1/ DilFac_1_b)} / 1,000,000 |
| 160          | NOx_2_mass_bc | Gm    | Calculated | 11.885        | NOx (corrected) mass for Phase 2 = 'Vmix_2 * NOx_Density * NOx_Corr_Fac * {NOx_Exh_2_b - NOx_Bkg_2_b * (1 - 1/ DilFac_2_b)} / 1,000,000 |
| 161          | NOx_3_mass_bc | Gm    | Calculated | 2.915         | NOx (corrected) mass for Phase 3 = 'Vmix_3 * NOx_Density * NOx_Corr_Fac * {NOx_Exh_3_b - NOx_Bkg_3_b * (1 - 1/ DilFac_3_b)} / 1,000,000 |
| 162          | CO_1_mass_b   | Gm    | Calculated | 46.800        | CO mass for Phase 1 = 'Vmix_1 * CO_Density * {CO_Exh_1_b - CO_Bkg_1_b * (1 - 1/ DilFac_1_b)} / 1,000,000                                |
| 163          | CO_2_mass_b   | Gm    | Calculated | 194.576       | CO mass for Phase 2 = 'Vmix_2 * CO_Density * {CO_Exh_2_b - CO_Bkg_2_b * (1 - 1/ DilFac_2_b)} / 1,000,000                                |
| 164          | CO_3_mass_b   | Gm    | Calculated | 14.256        | CO mass for Phase 3 = 'Vmix_3 * CO_Density * {CO_Exh_3_b - CO_Bkg_3_b * (1 - 1/ DilFac_3_b)} / 1,000,000                                |
| 165          | CO2_1_mass_b  | Gm    | Calculated | 724.662       | CO2 mass for Phase 1 = 'Vmix_1 * CO2_Density * {CO2_Exh_1_b - CO2_Bkg_1_b * (1 - 1/ DilFac_1_b)} / 100                                  |
| 166          | CO2_2_mass_b  | Gm    | Calculated | 3125.115      | CO2 mass for Phase 2 = 'Vmix_2 * CO2_Density * {CO2_Exh_2_b - CO2_Bkg_2_b * (1 - 1/ DilFac_2_b)} / 100                                  |
| 167          | CO2_3_mass_b  | Gm    | Calculated | 596.042       | CO2 mass for Phase 3 = 'Vmix_3 * CO2_Density * {CO2_Exh_3_b - CO2_Bkg_3_b * (1 - 1/ DilFac_3_b)} / 100                                  |

| Data Field # | Label         | Units   | Source     | Example Value | Comment   |
|--------------|---------------|---------|------------|---------------|---|
| 168          | (Blank Field) |         |            |               |   |
| 169          | HC_1_ER_b     | gm/mile | Calculated | 2.873         | HC Emission Rate for Phase 1 = HC_1_mass_b / RR_Dist_1  |
| 170          | HC_2_ER_b     | gm/mile | Calculated | 0.439         | HC Emission Rate for Phase 2 = HC_2_mass_b / RR_Dist_2  |
| 171          | HC_3_ER_b     | gm/mile | Calculated | 0.429         | HC Emission Rate for Phase 3 = HC_3_mass_b / RR_Dist_3  |
| 172          | NOx_1_ER_b    | gm/mile | Calculated | 2.963         | NOx Emission Rate for Phase 1 = NOx_1_mass_b / RR_Dist_1  |
| 173          | NOx_2_ER_b    | gm/mile | Calculated | 1.389         | NOx Emission Rate for Phase 2 = NOx_2_mass_b / RR_Dist_2  |
| 174          | NOx_3_ER_b    | gm/mile | Calculated | 2.499         | NOx Emission Rate for Phase 2 = NOx_2_mass_b / RR_Dist_2  |
| 175          | NOx_1_ER_bc   | gm/mile | Calculated | 2.912         | Corrected NOx Emission Rate for Phase 1 = NOx_1_mass_bc / RR_Dist_1   |
| 176          | NOx_2_ER_bc   | gm/mile | Calculated | 1.365         | Corrected NOx Emission Rate for Phase 2 = NOx_2_mass_bc / RR_Dist_2   |
| 177          | NOx_3_ER_bc   | gm/mile | Calculated | 2.456         | Corrected NOx Emission Rate for Phase 3 = NOx_3_mass_bc / RR_Dist_3   |
| 178          | CO_1_ER_b     | gm/mile | Calculated | 39.073        | CO Emission Rate for Phase 1 = CO_1_mass_b / RR_Dist_1  |
| 179          | CO_2_ER_b     | gm/mile | Calculated | 22.349        | CO Emission Rate for Phase 2 = CO_2_mass_b / RR_Dist_2  |
| 180          | CO_3_ER_b     | gm/mile | Calculated | 12.010        | CO Emission Rate for Phase 3 = CO_3_mass_b / RR_Dist_3  |
| 181          | CO2_1_ER_b    | gm/mile | Calculated | 605.013       | CO2 Emission Rate for Phase 1 = CO2_1_mass_b / RR_Dist_1  |
| 182          | CO2_2_ER_b    | gm/mile | Calculated | 358.952       | CO2 Emission Rate for Phase 2 = CO2_2_mass_b / RR_Dist_2  |
| 183          | CO2_3_ER_b    | gm/mile | Calculated | 502.130       | CO2 Emission Rate for Phase 3 = CO2_3_mass_b / RR_Dist_3  |
| 184          | (Blank Field) |         |            |               |   |
| 185          | HC_wt_ER_b    | gm/mile | Calculated | 0.565         | Weighted HC emission rate = 0.43 * {(HC_1_mass_b + HC_2_mass_b) / (RR_Dist_1 + RR_Dist_2)} + 0.57 * {(HC_3_mass_b + HC_2_mass_b) / (RR_Dist_3 + RR_Dist_2)} |

| Data Field # | Label         | Units   | Source     | Example Value | Comment  |
|--------------|---------------|---------|------------|---------------|--|
| 186          | NOx_wt_ER_b   | gm/mile | Calculated | 1.547         | Weighted NOx emission rate = $0.43 * \{(\text{NOx\_1\_mass\_b} + \text{NOx\_2\_mass\_b}) / (\text{RR\_Dist\_1} + \text{RR\_Dist\_2})\} + 0.57 * \{(\text{NOx\_3\_mass\_b} + \text{NOx\_2\_mass\_b}) / (\text{RR\_Dist\_3} + \text{RR\_Dist\_2})\}$                 |
| 187          | NOx_wt_ER_mb  | gm/mile | Calculated | 1.520         | Weighted NOx (corrected) emission rate = $0.43 * \{(\text{NOx\_1\_mass\_bc} + \text{NOx\_2\_mass\_bc}) / (\text{RR\_Dist\_1} + \text{RR\_Dist\_2})\} + 0.57 * \{(\text{NOx\_3\_mass\_bc} + \text{NOx\_2\_mass\_bc}) / (\text{RR\_Dist\_3} + \text{RR\_Dist\_2})\}$ |
| 188          | CO_wt_ER_b    | gm/mile | Calculated | 22.512        | Weighted CO emission rate = $0.43 * \{(\text{CO\_1\_mass\_b} + \text{CO\_2\_mass\_b}) / (\text{RR\_Dist\_1} + \text{RR\_Dist\_2})\} + 0.57 * \{(\text{CO\_3\_mass\_b} + \text{CO\_2\_mass\_b}) / (\text{RR\_Dist\_3} + \text{RR\_Dist\_2})\}$                      |
| 189          | CO2_wt_ER_b   | gm/mile | Calculated | 381.540       | Weighted CO2 emission rate = $0.43 * \{(\text{CO2\_1\_mass\_b} + \text{CO2\_2\_mass\_b}) / (\text{RR\_Dist\_1} + \text{RR\_Dist\_2})\} + 0.57 * \{(\text{CO2\_3\_mass\_b} + \text{CO2\_2\_mass\_b}) / (\text{RR\_Dist\_3} + \text{RR\_Dist\_2})\}$                 |
| 190          | (Blank Field) |         |            |               |  |
| 191          | FE_1_b        | mpg     | Calculated | 12.748        | Fuel Economy for Phase 1 = $\text{GGAL} / (\text{CRHC} * \text{HC\_1\_ER\_b} + 0.429 * \text{CO\_1\_ER\_b} + 0.273 * \text{CO2\_1\_ER\_b})$  |
| 192          | FE_2_b        | mpg     | Calculated | 21.769        | Fuel Economy for Phase 2 = $\text{GGAL} / (\text{CRHC} * \text{HC\_2\_ER\_b} + 0.429 * \text{CO\_2\_ER\_b} + 0.273 * \text{CO2\_2\_ER\_b})$  |
| 193          | FE_3_b        | mpg     | Calculated | 16.480        | Fuel Economy for Phase 3 = $\text{GGAL} / (\text{CRHC} * \text{HC\_3\_ER\_b} + 0.429 * \text{CO\_3\_ER\_b} + 0.273 * \text{CO2\_3\_ER\_b})$  |
| 194          | FE_wt_b       | mpg     | Calculated | 20.561        | Weighted Fuel Economy = $\text{GGAL} / (\text{CRHC} * \text{HC\_wt\_ER\_b} + 0.429 * \text{CO\_wt\_ER\_b} + 0.273 * \text{CO2\_wt\_ER\_b})$  |
| 195          | (Blank Field) |         |            |               |  |
| 196          | FR_Dist_1     | Miles   | Realtime   | 1.196         | Not used - Front roll Distance Phase 1   |
| 197          | FR_Dist_2     | Miles   | Realtime   | 8.615         | Not used - Front roll Distance Phase 2   |
| 198          | FR_Dist_3     | Miles   | Realtime   | 1.172         | Not used - Front roll Distance Phase 3   |
| 199          | Avg_Tork_1    | Ft-lbs  | Realtime   | 2.235         | Not used - Average torque Phase 1  |
| 200          | Avg_Tork_2    | Ft-lbs  | Realtime   | 6.363         | Not used - Average torque Phase 2  |

| <b>Data Field #</b> | <b>Label</b> | <b>Units</b>  | <b>Source</b> | <b>Example Value</b> | <b>Comment</b>   |
|---------------------|--------------|---------------|---------------|----------------------|--|
| 201                 | Avg_Tork_3   | <i>Ft-lbs</i> | Realtime      | 2.111                | Not used - Average torque Phase 3  |
| 202                 | PAU Temp.    | <i>C</i>      | Realtime      | 29.78                | Not used - Average dynamometer PAU temperature over entire test cycle            |
| 203                 | Amb. HC      | <i>ppmC</i>   | Realtime      | 2.07                 | Not used - Average HC concentration inside test facility over entire test cycle. |



