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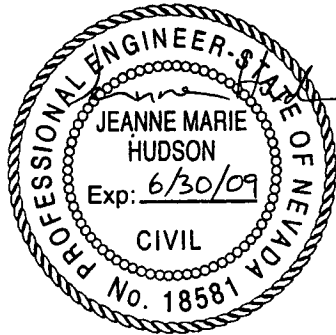
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Section 6.1.1 and Section 6.1.2	Shane Hsieh	Jeanne Hudson
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DISCLAIMER

The calculations contained in this document were developed by URS Corporation and are intended solely for the use of Bechtel SAIC Company, LLC in its work for the Yucca Mountain Project.

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ACRONYMS

COE	U.S. Army Corps of Engineers
CRWMS	Civilian Radioactive Waste Management System
CSCI	Computer Software Configuration Item
DOE	U.S. Department of Energy
DTN	Data Tracking Number
ESF	Exploratory Studies Facility
EIS	Environmental Impact Statement
FEMA	Federal Emergency Management Agency
FHWA	Federal Highway Administration
HEC	Hydrologic Engineering Center
HEC-RAS	Hydrologic Engineering Center, River Analysis System
HMR	Hydrometeorological Report
ITS	Important to Safety
ITWI	Important to Waste Isolation
M&O	Management and Operating Contractor
NOAA	National Oceanic and Atmospheric Administration
NRCS	Natural Resources Conservation Service
PMF	Probable Maximum Flood
PMP	Probable Maximum Precipitation
QARD	Quality Assurance Requirements and Description
SCS	Soil Conservation Service
STN	Software Tracking Number
TDMS	Technical Data Management System
TIN	Triangulated Irregular Network
URS	URS Corporation
USBR	U.S. Bureau of Reclamation
USDA	U.S. Department of Agriculture
YMP	Yucca Mountain Project

ABBREVIATIONS

cfs	cubic feet per second
ft	feet
ft ²	square feet
ft/s	feet per second
FY	Fiscal Year
mi	miles

1 PURPOSE

The purpose of this calculation is to demonstrate that the drainage features depicted in Attachment A of this calculation will adequately protect the Geologic Repository Operations Area (GROA) nuclear facilities from flooding associated with the Probable Maximum Precipitation (PMP) event. Flood control features (e.g., dikes and channels) are non-ITS and non-ITWI.

2 REFERENCES

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2.3 DESIGN CONSTRAINTS

None.

2.4 DESIGN OUTPUTS

None.

3 ASSUMPTIONS

3.1 ASSUMPTIONS REQUIRING VERIFICATION

None.

3.2 ASSUMPTIONS NOT REQUIRING VERIFICATION

3.2.1 Homogeneity of Watershed Properties

Watershed sub-area properties are assumed to be spatially uniform within each sub-area boundary during the entire duration of the storm.

Rationale: Since the relative size of the sub-areas is very small, significant variations in hydrologic properties within the sub-areas is unlikely. However, a sensitivity analysis for variations in soil types was performed in Section 6.2.4 of Reference 2.2.6. This calculation demonstrates that the effects of minor soil variations are small. Therefore, verification of this assumption is not required.

3.2.2 Initial Abstraction

Initial rainfall abstraction for any given watershed can vary over a relatively wide range depending on antecedent moisture conditions, season, and other factors. It was assumed that an initial rainfall abstraction (rainfall loss) of 1 inch would occur prior to rainfall runoff from the watershed to account for interception (wetting), depression storage, and rainfall required to saturate the uppermost layer of soil.

Rationale: Justification for this assumption is provided in Section 6.1.4.

3.2.3 Aging Pad Infiltration

For purposes of determining input parameters into the U.S. Army Corps of Engineers' HEC-1 computer model, it was conservatively assumed that the Aging Pads area shown on Attachment A is impervious to rainfall infiltration.

Rationale: The most conservative condition is assumed. Therefore, this is a bounding assumption that does not require verification.

3.2.4 Infiltration Rate

For all areas outside of the Aging Pads, a conservatively low rainfall infiltration rate of 1.5 inches per hour was assumed in the analysis.

Rationale:

Justification for this assumption is provided in Section 6.1.4.

3.2.5 Manning's Roughness Coefficient

A conservatively high Manning's n roughness coefficient of 0.09 was assumed for the HEC-1 and HEC-RAS computer calculations to provide conservatively high flow depths at project facilities.

Rationale: Justification for the assumed Manning's roughness coefficients is provided in Section 6.1.4.

3.2.6 Boundary Conditions

It was assumed that flows at upstream boundaries of the man-made channels around the Aging Pad and North Portal Facilities areas are at normal depth as determined by channel slopes and discharge. Flow was also assumed to be at normal depth at the downstream outlet of the channel system. The water surface elevation calculated by the HEC-RAS model in Segment 3 at its junction with Segment 2 was used as the downstream boundary of Segment 2. The water surface elevation calculated by the HEC-RAS model in Segment 2 at its junction with Segment 1 was used as the downstream boundary of Segment 1. See Figure 6-1 or 7-1 for definitions of Segments 1, 2, and 3.

Rationale: Upstream and downstream boundary conditions are dependent upon channel geometry and channel entrance and exit conditions at the boundaries, which are not in the scope of this analysis.

3.2.7 Fixed Bed Model

For the purpose of calculating PMF water surface elevations, it is assumed that channel sizes and locations, as defined by the current topography, will not change during the PMF event, i.e., a fixed bed model such as HEC-RAS can be used in the analyses.

Rationale: Flood channel design is not in the scope of this analysis. Sufficient watershed and sediment data are not available to predict possible changes in channel geometry and location during an extreme flood event such as the PMF. For purposes of the modeling, runoff has been directed toward the dike system. Should peak flows exceed the capacity of formed flow paths, water surface elevations adjacent to the dikes would be lower due to the overflow into adjacent channels farther away from the facilities.

3.2.8 Structural Integrity of the Dike System

It is assumed that structural failure of the dike system due to erosion or other factors will not occur.

Rationale: Structural design for the dike system is not in the scope of this analysis.

3.2.9 Flow Bulking Factor

In this study, it was conservatively assumed that flows will be bulked by 10% to account for sediment, debris, and air entrainment in the flowing water.

Rationale: Hydraulic equations and computer models do not account for entrainment of sediment, debris, and air bulking and must be separately accounted for by the investigator. Data are not available to estimate the amount of flow bulking at the project site during a PMF event. Justification for this assumption is provided in Section 6.1.4.

3.2.10 Detention Basin Design

As shown in Attachment A, runoff from the North Portal Facilities area will be detained on site and/or collected in detention ponds located at the southern and eastern boundaries of the North Portal Facilities area. It is assumed that detailed design will ensure that releases from the detention ponds through their outlet works will be controlled such that outflows will have no significant effect on peak flows in the downstream channel.

Rationale: The outlet works and detention storage volume for the detention ponds are not in the scope of this calculation.

4 METHODOLOGY

4.1 QUALITY ASSURANCE

This calculation was prepared in accordance with EG-PRO-3DP-G04B-00037, Calculations and Analyses (Ref. 2.1.1). The flood control structures have not been classified in the Basis of Design (Ref. 2.2.28). However, it is not anticipated that this system will perform any functions important to safety or important to waste isolation. Therefore, the approved version is designated as QA:N/A.

4.2 USE OF SOFTWARE

Software listed in Table 4-1 is qualified and was obtained from Software Configuration Management. The software was appropriate for the applications described in this report and the

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software was used within its range of validation as required by IT-PRO-0011 (Ref. 2.1.2). The computer used to run HEC-1 and HEC-RAS software is located in the URS office in Oakland, California. The computer was a Toshiba Satellite Pro with serial number 97244164. The computers used to run ArcGIS V.9.1 are also located in the URS office in Oakland, California. The computer types and identifiers are as follows: Hewlett-Packard hpxw4400 workstation, w021xp060928 and w021xp060917; and Hewlett Packard hp workstation xw6000, w021xp-8004. The computer used to run ArcINFO V.7.2.1 is located in the Yucca Mountain Las Vegas Office, Nevada. The BSC property tag number of this computer is 700810.

Table 4-1. Software Usage

Reference	Name	STN/CSCI Identifier	CPU Operating Platform	CPU Operating System
Ref. 2.2.4, Ref. 2.2.34	HEC-1 Version 4.0	30078-V4.0	PC	Windows 95-DOS Emulation
Ref. 2.2.5, Ref. 2.2.35	HEC-RAS Version 2.1	30079-V2.1	PC	Windows 95-DOS Emulation
Ref. 2.2.26, Ref. 2.2.30	ArcINFO V.7.2.1	STN 10033-7.2.1-00	SGI	IRIX 6.5
Ref. 2.2.20, 2.2.31	ArcGIS Desktop V.9.1	STN 11205-9.1-00	PC	Windows XP

4.2.1 Probable Maximum Flood Calculation

The HEC-1 computer software, Version 4.0 (Ref. 2.2.34, 2.2.4, 2.2.23) was used to perform the rainfall-runoff simulations using PMP amounts. This is the same software used in the previous studies (Ref. 2.2.6, 2.2.7).

4.2.2 Flood Inundation Calculation

The U.S. Army Corps of Engineers, Hydrologic Engineering Center, River Analysis System software (HEC-RAS), Version 2.1 (Ref. 2.2.35, 2.2.3, 2.2.5), was used for the flood inundation analysis. This program is designed for flood inundation studies and flood risk analysis. This software performs standard backwater computations to predict water surface elevations under steady gradually varied flow conditions. HEC-RAS is one of the FEMA nationally accepted computer programs that can be used to estimate flood elevations (Ref. 2.2.15). This is the same software used in the previous studies (Ref. 2.2.6 and 2.2.7).

4.2.3 Generation of Digital Terrain

A composite Triangulated Irregular Network (TIN) comprising two datasets (DTN #s MO0002SPATOP00.001 (Ref. 2.2.17) and MO9906COV98462.000 (Ref. 2.2.18)) was generated using ArcINFO V.7.2.1 (Ref. 2.2.26, 2.2.27) to produce a topographic representation of the project area. The dataset MO9906COV98462.000 (Ref. 2.2.18) contains 2-foot contour data encompassing the North Portal Facilities and vicinity, whereas the dataset MO0002SPATOP00.001 (Ref. 2.2.17) consists of an output gridded (100-foot spacing) surface that covers the entire watershed. The 2 datasets have overlapping information and the goal was to use the best available data for the region analyzed. The 2-foot contours from DTN MO9906COV98462.000 (Ref. 2.2.18) were the preferred data as they have the best vertical

resolution available. The 2-foot contours were clipped to the extent of the study area. The gridded elevation points from DTN MO0002SPATOP00.001 (Ref. 2.2.17) were then clipped to the same extent, and points overlapping the area where 2-foot contours existed were eliminated.

4.2.4 Geoprocessing and Displaying Results

ArcGIS V.9.1 (Ref. 2.2.20) was used to extract elevation data from the TIN described in Section 4.2.3 by querying information along user-defined section lines. ArcGIS V.9.1 was also used to calculate areas of watersheds defined as polygons, lengths of streams defined as lines, and present output from HEC-RAS graphically to show inundation boundaries. The solutions are documented in sufficient detail to allow an independent checker to reproduce or verify the results without recourse to the originator.

4.3 PMF CALCULATION METHOD

HEC-1 (Ref. 2.2.4), which was designed to simulate the surface runoff response of a watershed to precipitation, was used to calculate the Probable Maximum Flood (PMF). The program represents the watershed as an interconnected network of hydraulic and hydrologic components. A component may be a sub-area of the watershed, river channel, reservoir, or diversion. Each component is described by its physical characteristics and mathematical relations that describe the pertinent hydrologic and hydraulic processes. In the HEC-1 software, the study area is divided into drainage sub-areas with constant hydrologic properties. Separate hydrographs can be calculated for each sub-area. This method was necessary to provide information on flows at several key locations based on the proposed surface layout.

4.4 INUNDATION METHOD

The computational procedure used in HEC-RAS (Ref. 2.2.5) is based on solution of the one-dimensional energy equation. Energy losses consist of surface roughness and expansion/contraction losses. Energy loss by surface roughness is evaluated using Manning's equation and requires the user to define a roughness coefficient. The momentum equation is used in situations where flow is rapidly varied, such as hydraulic jumps and flow through bridges. A rigid channel boundary is used in the computations (i.e., channel cross section shapes do not change as a result of sediment deposition or scour). The HEC-RAS model uses input flows that are calculated by the HEC-1 model. Output from the model consists of water surface elevations at each user defined cross-section.

Three channel segments were analyzed using the HEC-RAS model. The channel segments are shown on Figure 7-1. Channel Segment 1 starts just north of the Aging Pads, follows the ditch and dike system towards the south and then continues south down the center of Midway Wash until it reaches Segment 2. Channel Segment 2 starts just north of the Aging Pads, and follows the ditch and dike system along the west side of the Aging Pad complex. At the southwest corner of the Aging Pad complex, Segment 2 turns east, passes through an opening in the dike, and flows east between the Aging Pads and the North Portal Facilities. At the northeast corner of the North Portal Facilities, Segment 2 turns south, follows the North Portal Loop eastern dike to its southern end, and then flows south away from the North Portal Facilities. Channel Segment 3 starts near the southwest corner of the North Portal Facilities, follows the North Portal Loop

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western dike to the southwest corner of the North Portal Facilities, turns toward the northeast, and flows under the H road through a series of culverts where it joins Segment 2 and flows out of Midway Valley. Assumption 3.2.6 was used to specify boundary conditions at the upstream and downstream ends of each Segment.

5 LIST OF ATTACHMENTS

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6 BODY OF CALCULATION

6.1 MODEL INPUTS

6.1.1 Topographic Data

A composite TIN was used to represent the topography of the project area. Generation of the TIN is described in Section 4.2.3. 10-foot contours were generated from the TIN using ArcGIS V.9.1 (Ref. 2.2.20) and were used in conjunction with the 2-foot contours from DTN M09906COV98462.000 (Ref. 2.2.18) to delineate the watershed and sub-areas and to determine channel flow paths. Elevations at the upstream and downstream ends of the flow paths defined for the HEC-1 model were also extracted from the TIN. Figure 6-1 shows sub-areas and drainage channels used in the HEC-1 model. A schematic of how the drainage system is represented in the HEC-1 model is provided in Attachment F. Elevation data from the TIN were also extracted at user-defined locations as input to the HEC-RAS models. The locations of extracted cross-sections are shown in Figure 7-1.

6.1.2 Layout Design

Preliminary layout sketches of the surface facilities, including the proposed North Portal Facilities, Aging Facilities, and dike and channel system, were used to define the extent of drainage sub-areas. A copy of the preliminary layout is provided in Attachment A. Project facilities are shown in the preliminary drawings as being protected by a ditch and dike system. The dimensions and elevations of the ditch and dike system were estimated from the drawings included in Attachment A. The dike system is included in the inundation study so that minimum elevations of the dikes could be estimated.

6.1.3 Precipitation

Section 4.2.10.2 of the Project Design Criteria (Ref 2.2.1) requires repository facilities to be protected from flooding utilizing the guidance from Regulatory Guide 1.102, "Flood Protection for Nuclear Power Plants" (Ref. 2.2.33), and Regulatory Guide 1.59, "Design Basis Floods for Nuclear Power Plants" (Ref. 2.2.32). These regulatory guides endorse National Oceanic and Atmospheric Administration (NOAA) methodology for determination of probable maximum precipitation (PMP). The PMP for the site was determined using procedures described in the National Oceanic and Atmospheric Administration's Hydrometeorological Report No. 49 (HMR 49) (Ref 2.2.16), which is considered to provide the best estimate of PMP potential (Ref. 2.2.13, p. 43). The HMR 49 method takes into account meteorological conditions and atmospheric processes in a region, moisture-maximized rains of record, and broad-scale terrain features among other factors to determine a theoretically maximum amount of precipitation for a region or a local watershed.

HMR 49 (Ref. 2.2.16) provides procedures and data for estimating local thunderstorm PMP and general storm PMP. In general the local thunderstorm PMP is the more critical event for small watersheds and the general storm PMP is more critical for large watersheds. Evaluations of the two types of storms (thunderstorm versus general storm) are provided in the previous report (Ref. 2.2.6). The all-seasons local thunderstorm PMP was used for the analyses because it is the critical PMP event for the small watershed considered in these studies.

Using the watershed size and geographical location, the estimated 6-hour duration local storm PMP over the North Portal Facilities area (herein referred to as PMP-North Portal) was determined in the previous study (Ref. 2.2.6) to be 13.2 inches, which has a higher precipitation intensity than the general storm PMP and is therefore the more critical storm to use in the PMF determination. The temporal distribution of the total precipitation was provided in the previous report (Ref. 2.2.6) and was developed based on recommendations in HMR 49. The time series precipitation amounts used in these calculations are presented in the HEC-1 input and output files contained in Attachments B and C. The PMP-North Portal was applied to sub-areas SB1, SB2, SB3, SB4, SB5, SB6, SB13, and Aging1 in the HEC-1 model. These sub-areas are shown on Figure 6-1.

Since a local thunderstorm system affecting the South Portal area can be independent of one that occurs at the North Portal Facilities, a separate PMP value was developed for the tributary area south of the North Portal Facilities. Separate and independent PMP storms for the North and South Portal areas provide a more conservative estimate of the maximum flows at the two portals because the rainfall intensity is inversely related to the drainage area. With an area of 6.5 square miles, the local 6-hour PMP for the South Portal area was computed to be 12.9 inches and is presented in Attachment E. The PMP for the South Portal area was applied to sub-areas SB7, SB8, SB9, SB10, SB11, and SB12. The sub-areas designated as NPP1, NPP2, and NPP3 on Figure 6-1 were excluded from the HEC-1 analysis because of assumption 3.2.10, which assumes that the design of the detention ponds will result in controlling runoff from the North Portal Facilities area such that peak PMF flows would not be affected.

6.1.4 Sub-Area Properties

The unit hydrograph method was used to develop a runoff hydrograph for each sub-area. Two parameters, sub-area size and lag time, are needed to determine the unit hydrograph for each sub-area using the NRCS Dimensionless Unit Hydrograph (Ref. 2.2.23, pp. 23-24). Sub-area sizes were obtained from the topographic data using ArcGIS V.9.1 (Ref. 2.2.20) and are summarized in Table 6-1.

The lag time parameter is used to define the shape of the unit hydrograph and is defined as the time difference between the occurrence of the center of mass of excess rainfall and the peak of the unit hydrograph. There are several formulae available to calculate lag time. Five commonly used formulae were evaluated in the previous report (Ref 2.2.6, pp. 18-19, 35-37). In general, lag time values computed using the U.S. Bureau of Reclamation (USBR) empirical formula (Ref. 2.2.14, pp. 29-38) were the smallest and, therefore, most conservative (i.e., produce the largest peak flow). Based on this consideration, lag times were calculated using the USBR formula, which is presented below (Ref. 2.2.14, pp. 29-38), with the results tabulated in Table 6-1.

$$lag = C \left(\frac{L \cdot L_{ca}}{\sqrt{S}} \right)^{0.33} \text{ (hours)}$$

where

C = 1.1 (Ref. 2.2.6, p. 19, 35-37)

L = total channel length (mi)

L_{ca} = length along the flow path from the basin outlet to the point opposite the centroid of the basin area (mi)

S = slope of the channel (ft/mi)

Table 6-1. Properties of Sub-Areas Used in HEC-1 Model

Basin Name	Area (mi ²)	Total channel length (mi)	Length from centroid to outlet (mi)	Slope (ft/mi)	Lag time (hr)
Aging1	0.46	N/A	N/A	N/A	N/A
SB1	0.83	2.72	1.39	370	0.64
SB2	0.42	1.62	0.71	570	0.40
SB3	1.6	3.82	1.71	500	0.73
SB4	1.2	3.34	1.33	460	0.65
SB5	0.39	2.36	1.10	180	0.64
SB6	0.76	3.01	1.44	180	0.76
SB7	2.9	4.83	2.50	430	0.92
SB8	1.2	2.68	1.26	440	0.60
SB9	1.7	2.46	1.10	480	0.55
SB10	0.44	0.89	0.41	150	0.35
SB11	0.46	1.35	0.64	360	0.40
SB12	0.15	0.39	0.24	88	0.24
SB13	0.19	0.81	0.39	250	0.30

An initial rainfall abstraction, or rainfall loss, is a sub-area property used in these calculations. It was assumed that an initial rainfall abstraction of 1 inch would occur prior to rainfall runoff from the watershed to account for interception (wetting), depression storage, and rainfall required to saturate the uppermost layer of soil. This assumed 1-inch initial rainfall loss is consistent with a rainfall loss measured during a July 1985 storm event (Ref. 2.2.8, p.7) and, as shown by sensitivity analyses presented in the previous report (Ref. 2.2.6, pp. 36-37), is a small enough value that the calculation results are relatively insensitive to it and, therefore, this assumption does not require confirmation.

A constant infiltration rate is also used in the calculations. Three double ring infiltrometer tests were conducted in the project vicinity that were used to estimate the constant infiltration rate used in these calculations. One test was conducted in Midway Wash at sampling location SA30 (MOL.19970513.0374, see ref 2.2.25, pp. 30-33), one was conducted in Pagany Wash at 32 cm below grade (MOL.19960112.0193, see ref 2.2.24), and one in 40 Mile Wash 200 feet south of H Road (MOL.19960112.0193, see ref. 2.2.24). A duplicate sample was collected at the 40 Mile Wash site. The infiltration rates after one hour varied from over 23 inches per hour (in/hr) at the 40 Mile Wash site, to 1.63 in/hr at the Pagany Wash site. The infiltration rate at the Midway Wash site was 5.58 in/hr.

A conservatively low rainfall infiltration rate of 1.5 inches per hour was assumed in the analysis. This is less than the lowest double infiltrometer test results and 0.3 inches per hour less than the 1.8 inches per hour infiltration rate estimated from percolation tests conducted at the ESF Muck Storage Area (Ref. 2.2.29, DTN#SNF29041993001.002). The assumed infiltration rate is consistent with hydrologic soil groups found in neighboring watersheds (Ref. 2.2.2, Table 8; Ref. 2.2.9, Tables 7 and 8) and soil particle size distributions found in Midway Valley (Ref. 2.2.19, DTN# GS921283114220.014). The influence of this assumed infiltration rate on the peak flood estimate was addressed through sensitivity analyses presented in the previous report (Ref. 2.2.6, pp. 36-37).

Bulking of flows by entrainment of sediment, debris, and air is another watershed sub-area characteristic that was considered in the studies. A review of literature regarding flow bulking suggests that bulking may not be a significant factor affecting PMF flows (Ref 2.2.6). This is because a PMF will have too much water for bulking to be significant. Bulking the PMF flow by 4 to 10 percent would be more than adequate. A bulking factor of 10 percent was assumed for the calculations, i.e., flows were increased by 10% to account for bulking and provide conservatism. Since the choice of this parameter is based primarily on literature, no confirmation is required.

6.1.5 Channel Properties

Manning's n roughness coefficient, which is used to calculate hydraulic losses of flows through a channel system, is needed for the HEC-1 and HEC-RAS models. Three different values for Manning's n, representing a lower limit, upper limit, and best estimate of PMF flow conditions, were considered for the analyses. The three different values for Manning's n that were considered are described below.

Clear Water Flow (Lower Limit)

Typically, a single value for Manning's n is used for the main channel, and a different coefficient is used for floodplains. Manning's n for clear flow conditions is based on typical values published in the literature (see Ref 2.2.10 pp. 101-123). A Manning's n value of 0.035 for the channel and a value of 0.05 for the floodplain would be appropriate based on ground cover and surface features shown in the project vicinity (Ref. 2.2.11, pp. 4-5; Ref. 2.2.22, pp. 6-10) and observed at the site in January 1999.

High Sediment Transport (Best Estimate)

During a PMF, the bed form is assumed to be continually changing and transporting large quantities of sediment, and may uproot plants and carry them and debris in the flow. This process will have the effect of increasing the effective roughness coefficient of the flow. Ref. 2.2.21 (pp. 197-371) lists Manning roughness coefficients for these forms and suggests increasing Manning's n by 0.02 to account for changing bed forms.

The degree of obstructions to the flow can also increase the Manning's n value. Obstructions include such things as debris deposits, exposed roots, floating vegetation that snag on downstream vegetation, and boulders. The Manning's n is increased by a value of 0.02 to account for obstructions during high sediment transport conditions, as recommended in Ref. 2.2.10 (pp. 101-123). Assuming a base roughness of 0.05 and adding values of 0.02 and 0.02 for bed forms and obstructions, respectively, results in a Manning's n value of 0.09 for high sediment transport conditions.

Mudflow (Upper Limit)

Under extreme sediment and debris transport conditions, a mudflow phenomenon may result in which the concentration of sediments in the water is greater than 20 percent by volume. Mudflows behave differently than clear water flow in that they have higher viscosity and internal shear stress. Calibration studies presented in the literature (Ref. 2.2.12, pp. 21-30) that simulated observed mudflows at several sites having field measurements indicated that the effective Manning's n roughness coefficient for mudflows ranged from 0.07 to 0.35. A conclusion of the calibration studies was that a Manning's n value of 0.16 provides the best fit when all data are considered.

Although it is expected that a significant amount of sediment and debris will be transported by the PMF, the amount of clear water runoff will be very large and it is unlikely that a mudflow condition will develop. On the other hand, it is likely that relatively large amounts of sediment will be transported by the runoff and a roughness that is higher than a clear water flow value of 0.035 is expected. Thus, a Manning's n roughness coefficient of 0.09 was assumed in the analyses. This assumed roughness will provide conservatively high estimates of water surface elevations without significantly underestimating peak discharges from the sub-areas since HEC-1 calculated peak flows from the sub-areas are not sensitive to assumed channel roughness. Higher Manning's n values would tend to decrease peak flows but would have no effect on the calculated lag time or time of concentration, which have a greater effect on the peak flows calculated by HEC-1. In HEC-RAS, the higher Manning's n values tend to increase water

surface elevations. The results of a sensitivity analysis were provided in a previous study (Ref. 2.2.6, Section 6.3) for the three flow scenarios discussed above.

The Muskingum-Cunge method (Ref. 2.2.23, pp. 40-41) was used to perform HEC-1 hydrograph routing along the channels through the watershed network. Inputs for the HEC-1 model are presented in Table 6-2 and include the length, slope, and channel dimensions. Dimensions of the man-made channels were taken from the preliminary drawings included in Attachment A. Dimensions of the natural channels were based on the topographic data described in Section 4.2.3. In general the attenuation of peak flows is not sensitive to the assumed channel size.

To initiate the channel routing in HEC-RAS, a normal depth flow condition, based upon channel bed slopes, roughness and discharge were assumed at the boundaries of the man-made channel system around the Aging Pads and North Portal Facilities areas. Bed slopes at the upstream boundaries of channel Segments 1, 2, and 3 (see Section 4.4 and Figures 6-1 and 7-1 for Segment definition) were estimated from the topographic data described in Section 4.2.3 and are 0.044, 0.037, and 0.033, respectively. Flows at these upstream boundaries were obtained from the HEC-1 output. At the downstream outlet of the channel system, the combined flow in the channels and the 0.025 bed slope at the outlet were used to calculate normal depth flow for Segment 3. At the downstream boundaries of Segments 1 and 2, water surface elevations at the junctions of the channel segments were calculated by the HEC-RAS model using the flow downstream from the junction and the channel slope and geometry at the junction.

Table 6-2. Properties of Channels Used in HEC-1 Model

Channel Name ¹	Length (ft)	Slope (ft/ft)	Bottom Width (ft)	Side Slope (h:1)
SB1toCP1	2400	0.02	78	3
CP1toCP2	2600	0.02	68	3
CP2toCP3	3500	0.02	88	3
CP3toCP4	4100	0.03	30	4
CP4toCP9	3000	0.02	30	20
CP5toCP6	2000	0.03	30	20
CP6toCP7	2100	0.02	30	10
CP7toCP8	2000	0.02	30	4
CP8toCP9	1700	0.02	30	4
SB7toCP5	3200	0.04	30	20
SB9toCP6	4700	0.03	30	20

1. Channel name used in HEC-1 files, Attachment B.

6.1.6 Culvert Sizes

As shown in Attachment A, project facilities include a set of culverts that pass under the "H" road (H road culverts) located southeast of the North Portal Facilities area. As input to the HEC-RAS model and shown on the preliminary drawings in Attachment A, the H road culverts consist of eight 48-foot by 20-foot arch culverts. For later stages of design, other options, such as a bridge, could be used instead of the culverts to convey the PMF.

6.2 PROBABLE MAXIMUM FLOOD ANALYSIS

A rainfall-runoff simulation was performed using the HEC-1 computer software (Ref. 2.2.4) to determine PMF flows at pertinent locations in the vicinity of the North Portal and Aging Pad facilities. The study area encompasses Midway Valley Wash, Drillhole Wash, and Split Wash, and is bounded by Yucca Mountain to the west, and Fran Ridge and Alice Hill to the south and east. The area was divided into 17 sub-areas as presented in Figure 6-1 to provide information on flows near the surface facilities. The sub-area boundaries were modified from the previous report (Ref. 2.2.7) to reflect changes in design layout.

6.3 FLOOD INUNDATION ANALYSIS

Flood inundation calculations were performed for each channel Segment shown on Figure 6-1 and described in Section 4.4. Cross-sections for the HEC-RAS model (Ref. 2.2.5) for each Segment were cut from the TIN described in Section 6.1.1 using the ArcGIS software (Ref. 2.2.31, 2.2.20). Figure 7-1 shows the locations of the cross-sections.

7 RESULTS AND CONCLUSIONS

7.1 PROBABLE MAXIMUM FLOOD RESULTS

This calculation demonstrates that the designed drainage features, as depicted in Attachment A, are adequate to protect the GROA nuclear facilities from flooding associated with the Probable Maximum Precipitation (PMP) event. This conclusion is based on the peak discharges and flood inundation levels summarized below.

Table 7-1 summarizes peak discharges calculated by the HEC-1 computer software (Ref. 2.2.4) using the inputs and assumptions discussed in the preceding report sections. The complete HEC-1 inputs and results are included in Attachments B and C. In addition to the discharge for individual sub-areas, HEC-1 also calculated PMF discharges at flow concentration points where hydrographs from two or more sub-areas are combined before being routed downstream. The peak flow at a concentration point is not simply the sum of the peak flows from each contributing sub-area because the HEC-1 software routes the entire flood hydrograph downstream, and the time to reach peak flow varies between sub-areas. The locations of sub-areas and flow concentration points are shown on Figure 6-1. The HEC-1 schematic is included in Attachment F.

Table 7-1. Results of PMF Analysis

Sub-Area	Peak Flow from HEC-1 (cfs)	Peak Flow with 10% Bulking Factor (cfs)		Flow Concentration Point	Peak Flow from HEC-1 (cfs)	Peak Flow with 10% Bulking Factor (cfs)
SB1	4,097	4,510		CP1	6,164	6,780
SB2	2,881	3,170		CP2	18,927	20,820
SB3	7,148	7,860		CP3	20,138	22,150
SB4	5,782	6,360		CP4	25,090	27,600
Aging1	3,436	3,780		CP5	14,235	15,660
SB5	1,925	2,120		CP6	23,427	25,770
SB6	3,290	3,620		CP7	24,733	27,210
SB7	10,053	11,060		CP8	24,935	27,430
SB8	5,757	6,330		CP9	50,219	55,240
SB9	8,684	9,550				
SB10	3,043	3,350				
SB11	2,924	3,220				
SB12	1,300	1,430				
SB13	1,555	1,710				

7.2 FLOOD INUNDATION RESULTS

7.2.1 Flood Inundation Along Channel Segment 1

HEC-RAS software (Ref. 2.2.5) was employed using the cross-section data described in Section 6.1.1.

Table 7-2 summarizes results of the flood routing analysis of PMF peak flow through channel Segment 1. Cross-section locations along channel Segment 1 are shown in Figure 7-1. Between cross-sections 8069 and 9716, channel Segment 1 is located adjacent to the man-made dike system. Downstream from cross-section 8069, between cross-sections 2 and 7695, the ground slopes away from the dike and flow is no longer against the dike. Channel bed, PMF water surface, and minimum top-of-bank profiles along channel Segment 1 are presented in Attachment D.

Theoretically, the peak flow along a channel reach increases gradually toward the downstream direction because the peak flow at a particular channel cross-section is only the peak flow from the drainage area upstream of this cross-section. It is not practical to calculate the peak flow for each individual cross-section. Instead, the PMF peak flows calculated for sub-areas or concentration points in Table 7-1 were applied to the appropriate cross-sections in the HEC-RAS model. For Segment 1, the PMF peak flow of 2,120 cfs for Sub-Area SB5 was used for the reach between cross-sections 2219 to 9716. Downstream of cross-section 1938, where Segment 1 merges with Segment 2, the total flow of 27,600 cfs at Flow Concentration Point CP4 was used

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to account for the possibility that PMF peak flows in Segment 2 and from Sub-Area SB6 may merge into Segment 1.

Between cross-sections 7695 and 9716 and between 945 and 2219, ineffective flow areas were defined for the left (when facing downstream) portions of the cross-sections. This compensates for the possibility of an obstruction to the left of the main channel because the HEC-RAS software treats ineffective flow areas as stagnant, so they are not actively conveying. This approach keeps the majority of the PMF peak flow staying in the main flow path for more conservative flood inundation estimations. Otherwise, the HEC-RAS model would actively convey flow through the portions of the cross-section with the lowest elevations, whether these occur along the main channel or the overbanks.

Table 7-2. Flood Inundation Results for Segment 1

Stream Cross-Section	Peak PMF Flow (cfs)	Channel Invert Elevation (ft)	Water Surface Elevation (ft)	Channel Velocity (ft/s)	Channel Top width (ft)	Levee Elevation⁽¹⁾ (ft)	Levee Free Board⁽¹⁾ (ft)
9716	2120	3858.2	3862.1	4.9	430.6	3862.4	0.3
9310	2120	3840.5	3844.4	6.6	295.8	3852.5	8.1
8892	2120	3822.5	3826.4	5.8	146.4	3837.5	11.2
8494	2120	3806.8	3811.9	5.9	256.9	3818.1	6.2
8069	2120	3790	3794.6	6.3	297.9	3800.6	6
7695	2120	3771.9	3775.8	6.1	279.4	3784.1	8.3
7306	2120	3749.2	3755.1	9.1	56.5	3771.9	16.8
7030	2120	3737.1	3745.1	7.6	61.3	3771.3	26.2
6730	2120	3730.1	3736.1	7.2	72.7	3762.2	26.1
6433	2120	3723.9	3728.8	5.8	98.5	3750.6	21.8
6041	2120	3711	3717.4	8.1	63.1	3739	21.6
5558	2120	3698	3703.3	6.1	94.3	3722.8	19.5
5180	2120	3686	3690.7	7.6	84.4	3718.8	28
4815	2120	3676.4	3681.9	5.2	104	3699	17.2
4487	2120	3668	3673.3	7.1	95.1	3688.2	14.9
4064	2120	3658	3662.9	4.8	133.3	N/A	N/A
3468	2120	3642	3645.1	7.7	100	N/A	N/A
3008	2120	3628	3634.9	4.5	124.2	N/A	N/A
2601	2120	3619.8	3623.1	8.8	99.6	N/A	N/A
2219	2120	3608	3617.2	1.3	509.4	N/A	N/A
1938	27600	3602	3612.5	8.1	1113.6	N/A	N/A
1656	27600	3594	3603.7	9.4	748.6	N/A	N/A
1426	27600	3588	3597.4	7.8	1044.3	N/A	N/A
1183	27600	3582	3589.3	9.3	998.2	N/A	N/A
945	27600	3576	3582.6	7.4	1097.1	N/A	N/A
661	27600	3568.8	3576.2	6.4	1395.8	N/A	N/A
439	27600	3563.9	3571.3	7	1361.6	N/A	N/A
240	27600	3560	3567.5	7.2	1303.2	N/A	N/A
2	27600	3556	3563.4	5.8	1349.6	N/A	N/A

(1) N/A = Not applicable. Between sections 4064 and 2, channel Segment 2 is between the dike and channel Segment 1, so levee elevations and free board have been provided for channel Segment 2 in Table 7-3.

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7.2.2 Flood Inundation Along Channel Segment 2

Table 7-3 summarizes results of the flood routing analysis of PMF peak flows through channel Segment 2. Cross-section locations along channel Segment 2 are shown in Figure 7-1. Between cross-sections 14681 and 2799, channel Segment 2 is located adjacent to the man-made dike system. Downstream from cross-section 2589, between cross-sections 1 and 2589, the ground slopes away from the dike and flow is no longer against the dike.

Downstream from the southwest corner of the Aging Pad complex, where channel Segment 2 crosses the dike system (cross-section 10287 to 9676), the right (south) channel bank is adjacent to the North Portal Loop East dike system. Channel bed, PMF water surface, and minimum top-of-bank profiles along channel Segment 2 are presented in Attachment D.

The PMF peak flow at each cross-section was determined with a similar approach as discussed in 7.2.1.

Table 7-3. Flood Inundation Results for Segment 2

Stream Cross-Section	Peak PMF Flow (cfs)	Channel Invert Elevation (ft)	Water Surface Elevation (ft)	Channel Velocity (ft/s)	Channel Top width (ft)	Left Levee Elevation ⁽¹⁾ (ft)	Left Levee Free Board ⁽¹⁾ (ft)	Right Levee Elevation ⁽¹⁾ (ft)	Right Levee Free Board ⁽¹⁾ (ft)
14681	4510	3858.4	3865.8	3.8	433.4	3868.4	2.6	N/A	N/A
14432	4510	3854.6	3861.4	6.6	407.6	3869.5	8.1	N/A	N/A
14197	4510	3850	3855.3	5.8	432.1	3860	4.7	N/A	N/A
13836	4510	3842.5	3844	5.2	421.2	3852.7	8.7	N/A	N/A
13567	4510	3824	3832.8	4.9	213.9	3844	11.2	N/A	N/A
13161	4510	3818.6	3821.3	7.4	370.5	3836.5	15.2	N/A	N/A
12844	4510	3801	3809.8	4.5	140.9	3824.5	14.7	N/A	N/A
12382	6780	3796.5	3804.4	7.7	135.5	3821	16.6	N/A	N/A
12063	6780	3790	3797	8.8	130.2	3816.5	19.5	N/A	N/A
11833	6780	3780	3786.2	12.6	105.2	3810	23.8	N/A	N/A
11529	6780	3769.7	3779.3	7.3	125.6	3800	20.7	N/A	N/A
11193	6780	3765	3775.2	6.8	129	3789.7	14.6	N/A	N/A
10949	6780	3761	3773.9	4.6	173.4	3785	11.1	N/A	N/A
10642	6780	3760	3772.2	5.3	141.2	3781	8.8	N/A	N/A
10287	6780	3760	3765.4	12.1	120.2	N/A	N/A	N/A	N/A
9909	6780	3749.1	3758.8	3.8	380.5	N/A	N/A	N/A	N/A
9676	20820	3744.7	3751.2	13.4	490.6	N/A	N/A	3757.7	6.5
9350	20820	3727	3735.4	12.9	514.2	N/A	N/A	3747	11.6
9065	20820	3712	3723.9	11.9	499.9	N/A	N/A	3732	8.1
8785	20820	3706	3721.1	8.3	412.2	N/A	N/A	3726	4.9
8483	20820	3701.8	3719	7.8	277.5	N/A	N/A	3721.8	2.8
8188	20820	3698.5	3717.6	7.1	280.3	N/A	N/A	3718.5	0.9
7927	20820	3698	3715.8	8.2	221.5	N/A	N/A	3718	2.2
7698	20820	3697	3713.8	8.8	237.5	N/A	N/A	3717	3.2

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Stream Cross-Section	Peak PMF Flow (cfs)	Channel Invert Elevation (ft)	Water Surface Elevation (ft)	Channel Velocity (ft/s)	Channel Top width (ft)	Left Levee Elevation⁽¹⁾ (ft)	Left Levee Free Board⁽¹⁾ (ft)	Right Levee Elevation⁽¹⁾ (ft)	Right Levee Free Board⁽¹⁾ (ft)
7489	20820	3696.3	3710.8	10.6	195.6	N/A	N/A	3716.3	5.5
7280	20820	3695.3	3710.1	6.2	283.6	N/A	N/A	3715.3	5.2
7083	20820	3694	3705.7	14.1	179.2	N/A	N/A	3714	8.3
6922	20820	3688	3702.7	10.7	188	N/A	N/A	3708	5.3
6778	20820	3681.3	3696.4	15.3	187.1	3703.4	7	3702.3	6
6662	20820	3675.1	3692.5	9.5	267.2	3696.3	3.8	3702	9.5
6471	20820	3667.8	3683.3	16.2	156.8	3684.7	1.4	3696	12.7
6338	20820	3661.7	3678.9	10.6	220	N/A	N/A	3685	6.1
6147	20820	3656.9	3676.2	7.8	333.5	N/A	N/A	3677.8	1.6
5883	22150	3652	3671.7	9.6	257	N/A	N/A	3678.4	6.7
5618	22150	3646	3668.8	8.2	342.9	N/A	N/A	3675.6	6.8
5404	22150	3652.2	3665.1	10.7	533.4	N/A	N/A	3668.7	3.6
5234	22150	3648.7	3659.1	10.8	681.3	N/A	N/A	3661	1.9
5070	22150	3643.9	3651	9.1	696.7	N/A	N/A	3659.3	8.3
4882	22150	3633.2	3644.3	7.5	859.2	N/A	N/A	3653.8	9.5
4636	22150	3623.4	3632.1	12.6	482.9	N/A	N/A	3646.4	14.3
4339	22150	3609.8	3622.5	8	552	N/A	N/A	3639.9	17.4
4085	22150	3604	3616.4	11.4	264	N/A	N/A	3634.6	18.3
3869	22150	3598	3610.9	9.8	293.6	N/A	N/A	3631.3	20.4
3657	22150	3592.7	3605.6	10.1	300.2	N/A	N/A	3626.7	21.1
3460	22150	3588	3600.9	9.5	330.6	N/A	N/A	3622.3	21.3
3257	22150	3584.7	3595.6	9.2	416.3	N/A	N/A	3617.3	21.7
3012	22150	3579	3590.5	7.2	522.4	N/A	N/A	3612.4	21.9
2799	22150	3574	3582.4	11.2	518.6	N/A	N/A	3608.6	26.2
2589	27600	3569	3576.2	5.1	1395.8	N/A	N/A	3604.4	28.2
2357	27600	3563.9	3571.3	5.8	1361.6	N/A	N/A	3599.8	28.6
2180	27600	3560	3567.5	4.8	1303.2	N/A	N/A	3595	27.5
1943	27600	3556	3563.4	5.2	1349.3	N/A	N/A	3590.4	27
1722	27600	3552	3559.5	6	1241.9	N/A	N/A	3587.3	27.8
1499	27600	3548	3555	5.9	1471.8	N/A	N/A	3584.3	29.3
1371	27600	3546	3552.9	4.7	1532.9	N/A	N/A	3582.7	29.7
1190	27600	3541.2	3550.6	4.8	1630.7	N/A	N/A	3581.8	31.2
984	27600	3537.7	3546.8	5.9	1122	N/A	N/A	3581.2	34.4
882	27600	3534	3544.6	6.3	1096.5	N/A	N/A	3580.7	36
722	27600	3531.2	3540.5	6.8	1177.3	N/A	N/A	3580	39.5
577	27600	3528	3536.7	6.4	1259.1	N/A	N/A	3579.9	43.2
404	27600	3524	3531.5	7.2	1169.8	N/A	N/A	3580.8	49.3
183	27600	3520	3529.8	3.8	1233.8	N/A	N/A	3579.9	50.1
1	55240	3516.1	3528.7	5.1	1493.5	N/A	N/A	3570.8	42.1

(1) N/A = Not Applicable. The left and right levee and free board elevations are shown as N/A when the proposed dike is not adjacent to the channel on either the left or right sides.

7.2.3 Flood Inundation Along Channel Segment 3

Table 7-4 summarizes results of the flood routing analysis of PMF peak flows through channel Segment 3. Cross-section locations are shown in Figure 7-1. Between cross-sections 11551 and 6374, channel Segment 3 is located adjacent to the man-made dike system. Downstream from cross-section 6374, between cross-sections 647 and 6068, the ground slopes away from the dike and flow is no longer against the dike.

Eight 48-foot by 20-foot arch culverts were assumed to convey flow under the "H" road. These culverts can convey the PMF flow under the road with approximately 13 feet of freeboard to the road crest. In the final design, use of a bridge instead of the culverts should be considered. Downstream from the culverts, flow exits Midway Wash.

In Table 7-4, the levee elevations between cross-sections 11551 and 1599 were based on the height of the dike on the left bank of Segment 3 (facing downstream) along the North Portal Loop West, as shown in Attachment A. Between cross-sections 1184 and 647, the levee elevations shown in Table 7-4 were based on the height of the "H" Road (south of channel Segment 3) as shown in Attachment A. However, the elevation of the "H" Road is preliminary, so the downstream inundation area was not mapped in detail on Figure 7-1, and the elevations for sections downstream of cross-section 647 were not shown in Table 7-4.

Channel bed, PMF water surface, and minimum top-of-bank profiles along channel Segment 3 are presented in Attachment D.

The PMF peak flow at each cross-section was determined with a similar approach as discussed in 7.2.1. Ineffective flow areas were defined between cross-sections 10716 and 11551.

Table 7-4. Flood Inundation Results for Segment 3

Stream Cross-Section	Peak PMF Flow (cfs)	Channel Invert Elevation (ft)	Water Surface Elevation (ft)	Channel Velocity (ft/s)	Channel Top width (ft)	Levee Elevation (ft)	Levee Free Board (ft)
11551	15660	3795.8	3801.8	6.9	767.6	3807.8	6
11423	15660	3790.2	3796.9	7.8	549.6	3802.2	5.3
11278	15660	3784.4	3791.2	7.8	558.2	3796.1	4.8
11135	15660	3777.4	3785.5	7.6	598	3790.1	4.6
11003	15660	3772.7	3779.4	8.4	522.8	3784.7	5.3
10837	15660	3766	3772.3	8	567.2	3777.8	5.6
10716	15660	3761.5	3767.1	8	639	3772.8	5.7
10536	15660	3754	3758.9	7.4	695	3765.4	6.5
10312	15660	3743.7	3749.6	7	699.2	3756.2	6.6
10074	15660	3734	3739.3	7.4	719.5	3746	6.7
9863	15660	3724.9	3730.2	6.3	916.3	3737.1	6.8
9681	15660	3717.1	3721.1	7.3	892.3	3729.4	8.3
9526	15660	3708.4	3714.2	6.4	819.6	3723.2	9
9328	15660	3700	3706.3	7.3	722.5	3714.7	8.4
9095	15660	3691.8	3697.6	7	657.5	3704.8	7.2
8895	15660	3684	3689.7	8	587.2	3696.6	7

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Stream Cross-Section	Peak PMF Flow (cfs)	Channel Invert Elevation (ft)	Water Surface Elevation (ft)	Channel Velocity (ft/s)	Channel Top width (ft)	Levee Elevation (ft)	Levee Free Board (ft)
8736	15660	3678	3684	7.4	520.1	3690.2	6.2
8595	15660	3673.9	3679.4	8	479.6	3684.1	4.7
8468	15660	3668	3677	6.6	526.6	3679.6	2.6
8319	15660	3665.4	3673.2	8.5	1001	3674.4	1.2
8177	15660	3660.9	3667.9	5.3	1337.3	3670.5	2.6
8007	15660	3658.2	3661.8	4.9	1499.5	3667.0	5.2
7811	15660	3650.8	3655.3	4.9	1558.4	3662.8	7.5
7616	15660	3644.9	3650.7	3.9	1561.6	3658.8	8.1
7380	15660	3639.5	3645.8	5.3	921.7	3655.1	9.3
7117	15660	3634	3639.4	5.8	812.6	3652.0	12.6
7014	15660	3631	3636.2	6	993.6	3650.6	14.4
6935	15660	3628.6	3632.5	5.9	1444.1	3648.5	16.0
6735	15660	3618.3	3626.4	5.2	884.3	3646.7	20.3
6374	15660	3608.6	3617	7.3	568.6	3644.2	27.2
6068	15660	3601.6	3611.2	5.2	676.2	3643.3	32.1
5842	25770	3598	3606.9	6.7	818.2	3638.8	31.9
5612	25770	3592	3601.7	6.1	1146.7	3634.5	32.8
5250	25770	3586	3594.6	6.1	828.6	3630.3	35.7
5033	25770	3582	3590.8	6.5	800.9	3624.4	33.6
4778	25770	3576	3586.5	6.3	776.3	3621.7	35.2
4479	25770	3570.6	3583	5.7	670.2	3615.0	32.0
4191	25770	3566	3580.6	5.1	762.4	3606.8	26.2
3806	27210	3560	3574.4	9.2	489.2	3603.0	28.6
3472	27210	3554	3567.4	7.4	600	3600.7	33.3
3272	27210	3551.8	3564.7	6.1	704.9	3587.9	23.2
2855	27210	3543	3557.8	8.4	468.4	3584.5	26.7
2552	27210	3538	3552.3	8	479	3581.6	29.3
2270	27210	3532	3546.9	8.5	459.2	3578.3	31.4
2191	27210	3532	3545.5	8.1	497.9	3574.3	28.8
2044	27210	3530	3543.7	6.6	557	3572	28.3
1860	27430	3527.6	3541.2	7.4	487.1	3570	28.8
1599	27430	3522	3532.2	13.8	342.7	3567	34.8
1406	Culvert						
1184	27430	3513.1	3528.9	3.9	768	3533.7	4.7
1160	27430	3512	3528.9	3.8	827.2	3532.7	3.9
1139	27430	3512	3528.8	3.8	889.5	3532	3.2
1108	27430	3512	3528.7	3.8	819.9	3531.4	2.7
1060	27430	3512	3528.6	4.1	751.2	3530.8	2.2
1019	27430	3512	3528.5	4	823.9	3530.4	1.9
966	55240	3512	3527.1	9.1	712.4	3529.9	2.8
890	55240	3511.2	3525.7	10	655.9	3528.4	2.7
813	55240	3510	3524.3	10.2	729.8	3525.3	1.1
647	55240	3506	3519.3	12.5	580.9	3519.5	0.2

Legend

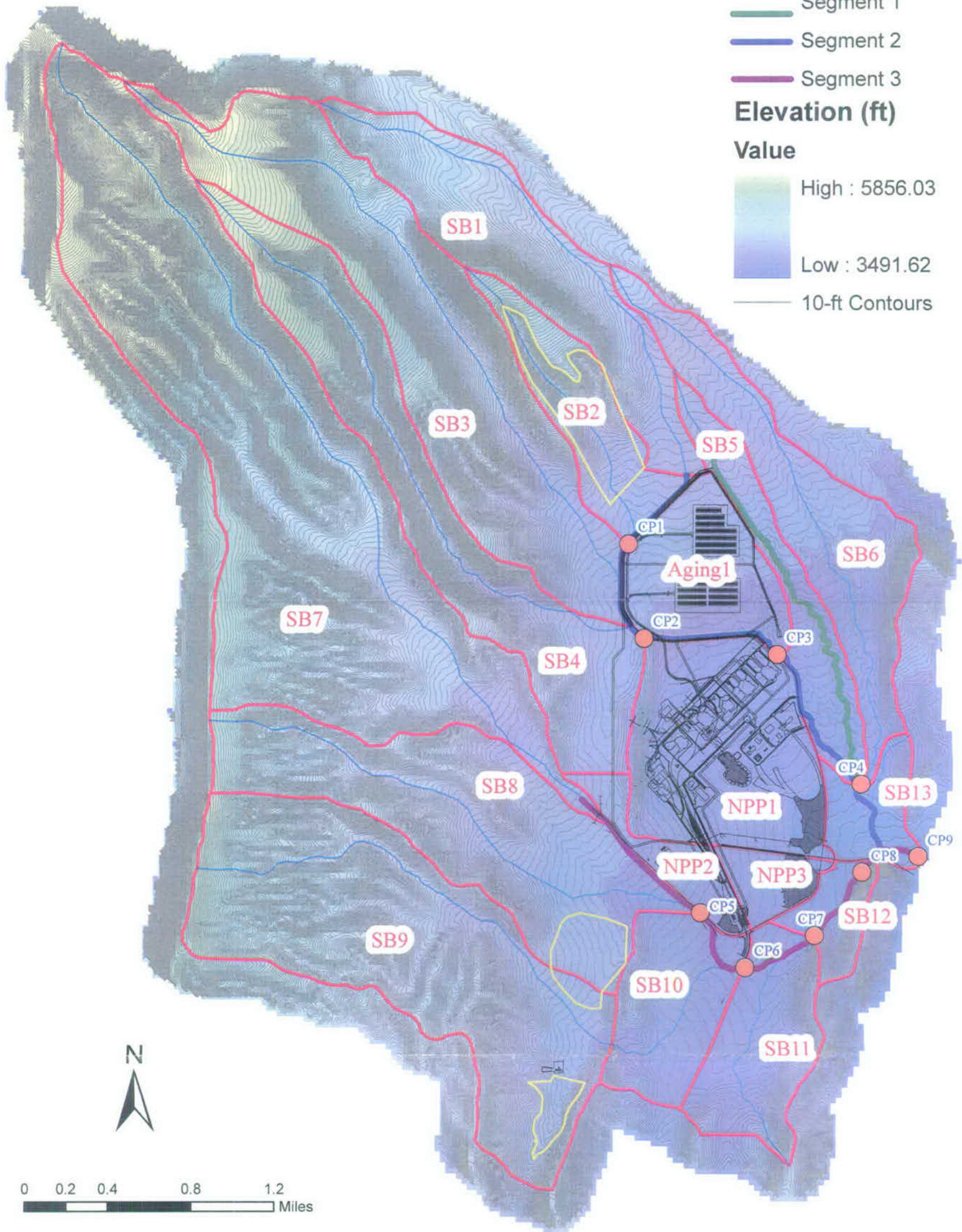
- Collection Points
- Drainage Channels
- Watershed Boundaries
- Proposed Layout
- Muck Piles

Conveyance Channels

- Segment 1
- Segment 2
- Segment 3

Elevation (ft)

- Value
- █ High : 5856.03
 - █ Low : 3491.62
 - 10-ft Contours



Source for preliminary layout of facilities: Electronic version of layout shown in Attachment A.

Source for topographic data: Generated from two datasets. MO9906COV98462.000, containing 2-foot contour data encompassing the North Portal Pad and vicinity and MO0002SPATOP00.001, consisting of an output gridded (100-foot spacing) surface that covers the entire watershed.

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gpd

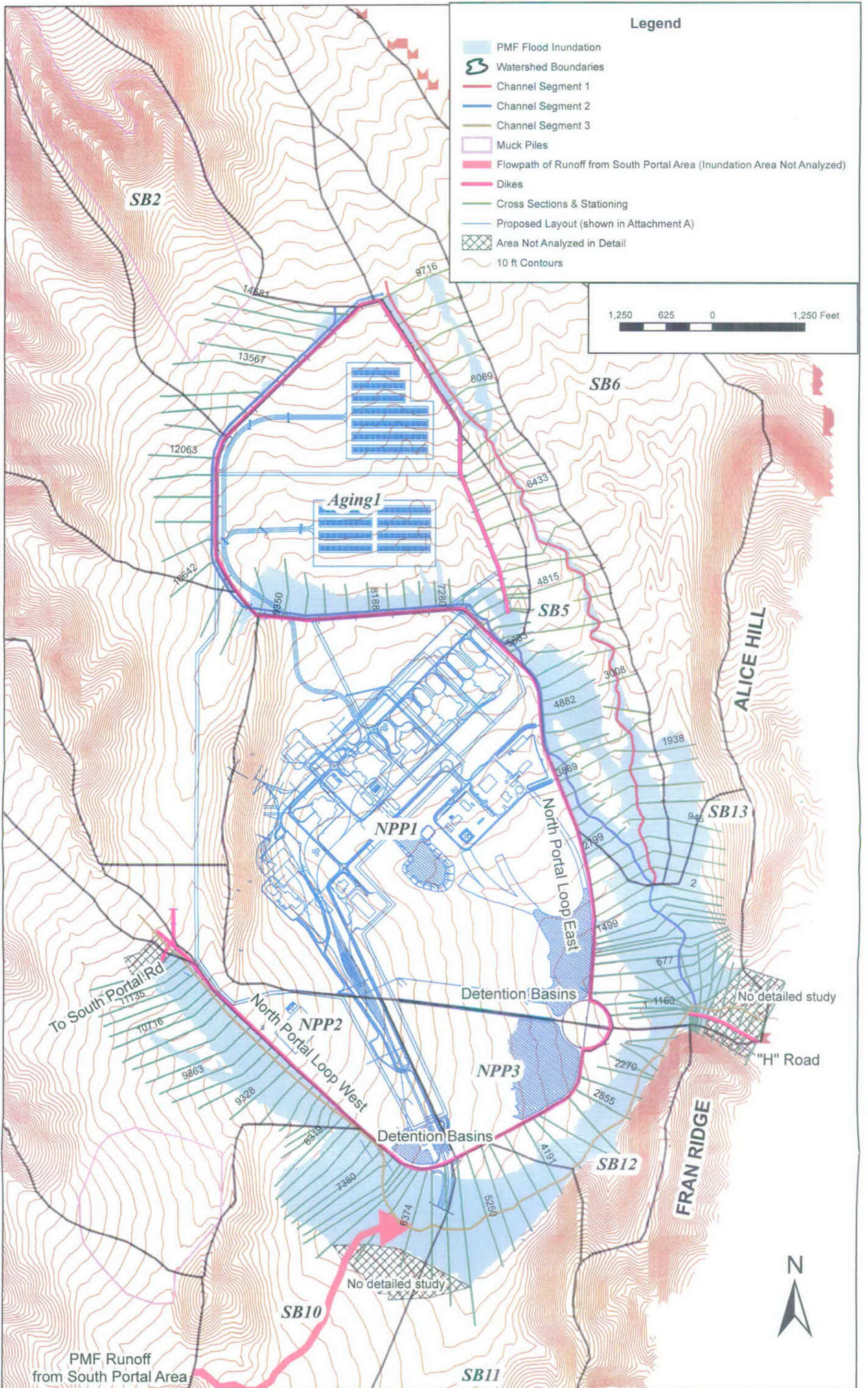


Yucca Mountain

26815949

Sub-Areas Used in the
 HEC-1 Calculation of the PMF

FIGURE
 6-1



Yucca Mountain

26815949

Probable Maximum Flood Inundation

FIGURE 7-1

APD



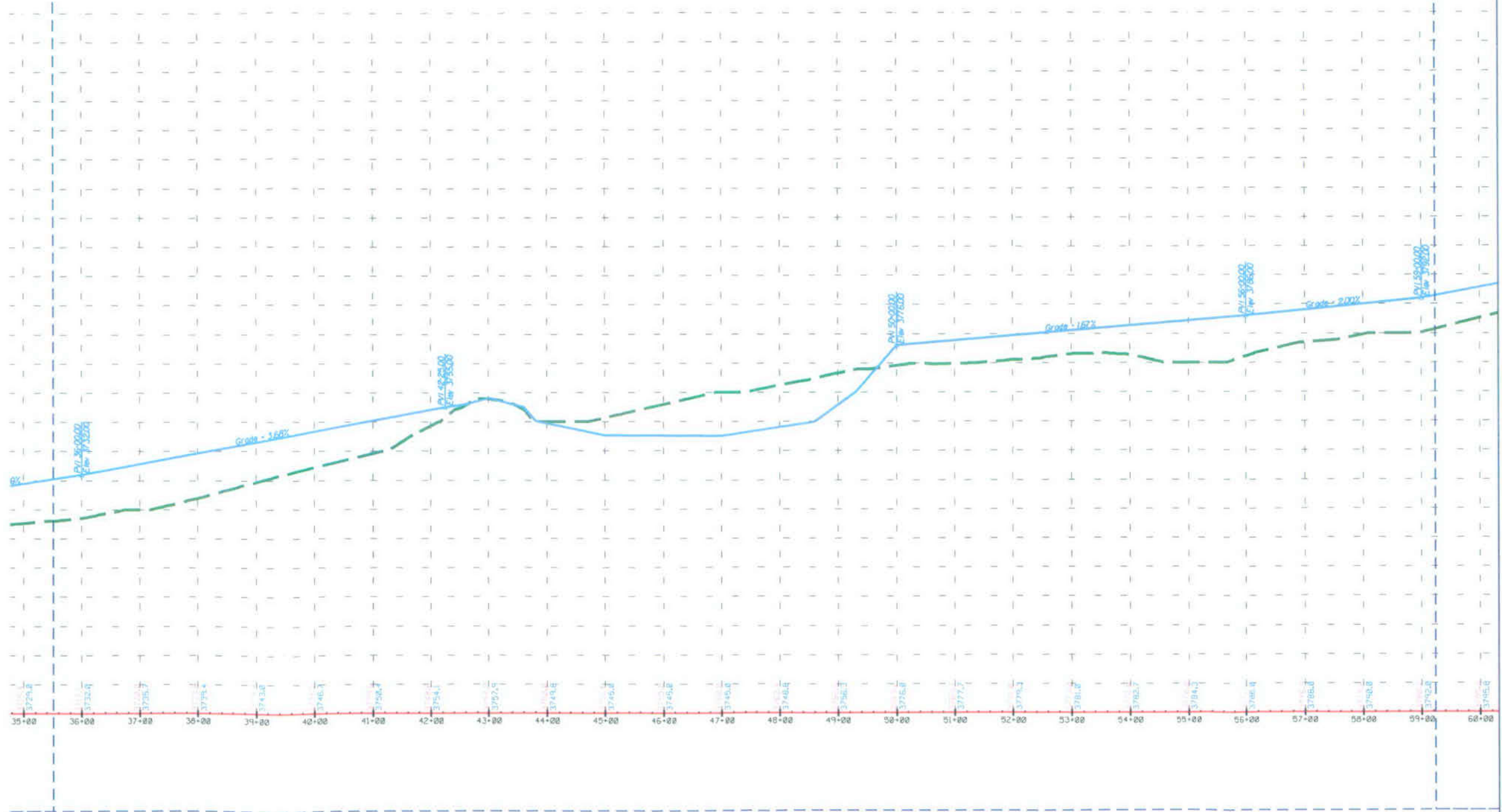
Project No.26815949

Attachment A
 Preliminary Layout, Plans and Profiles of Facilities at and Near North Portal Pad
 000-CDC-MGR0-00100-000-00A
 1 of 13

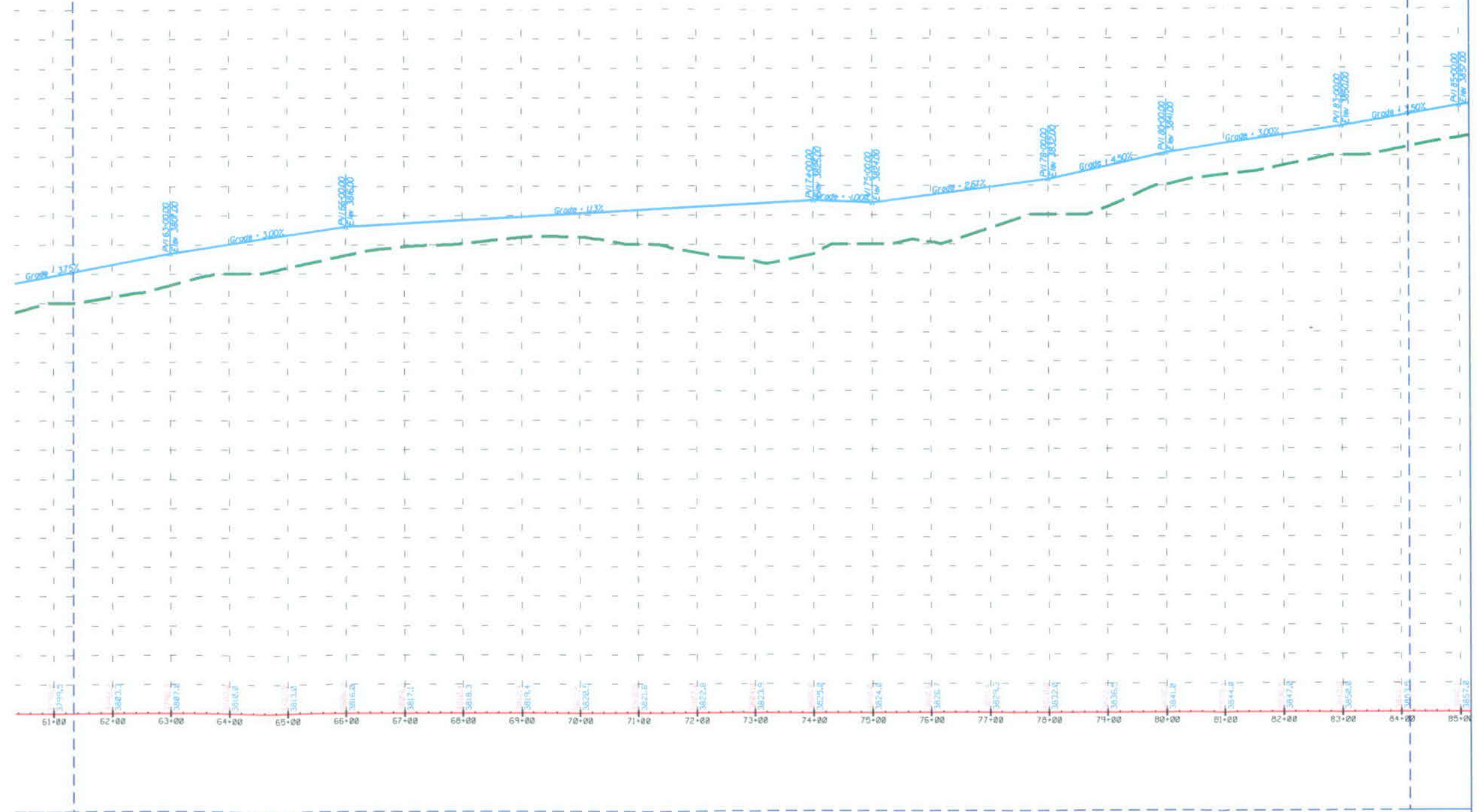


Yucca Mountain Project
 Drainage Report and Analysis

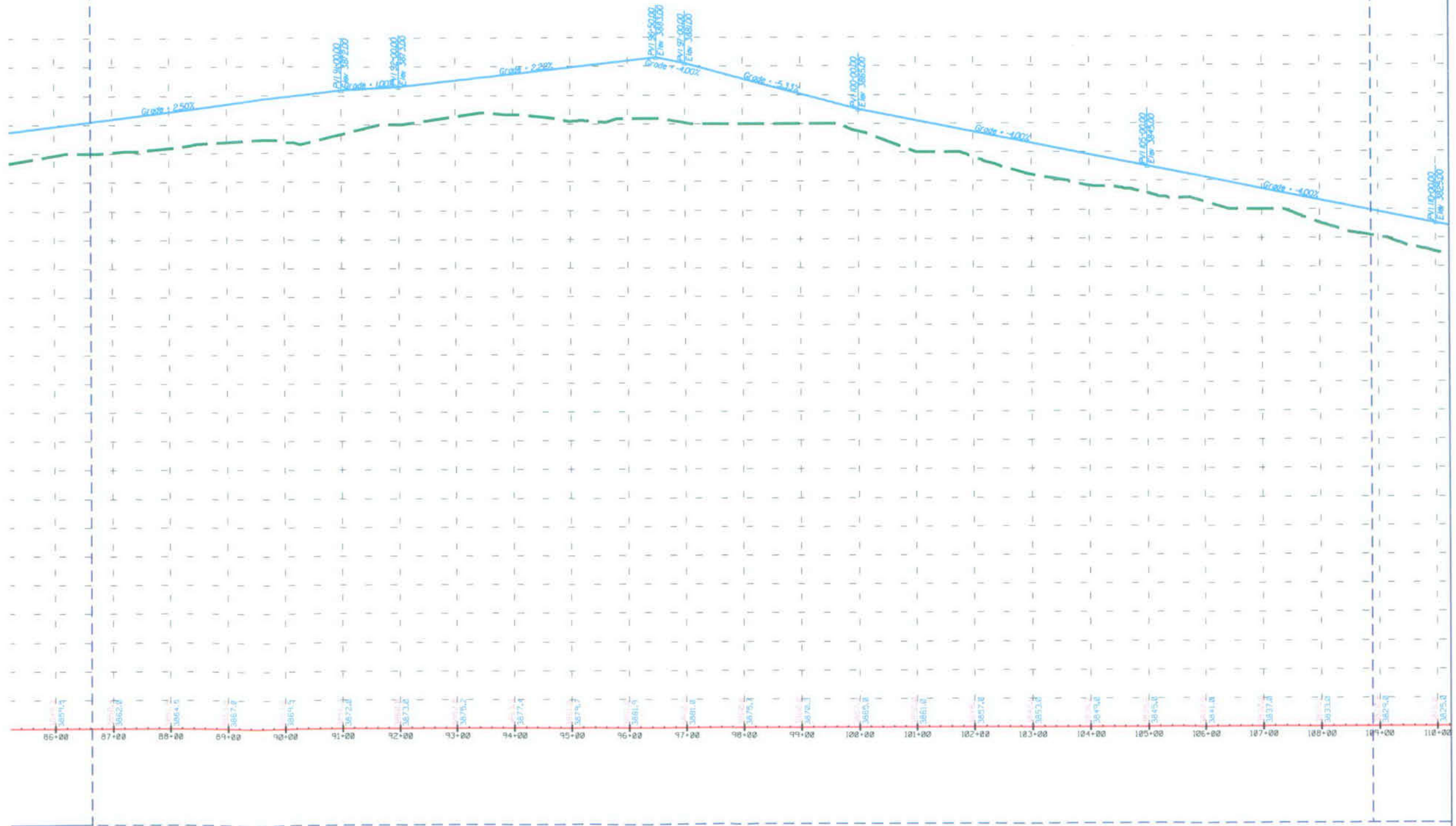
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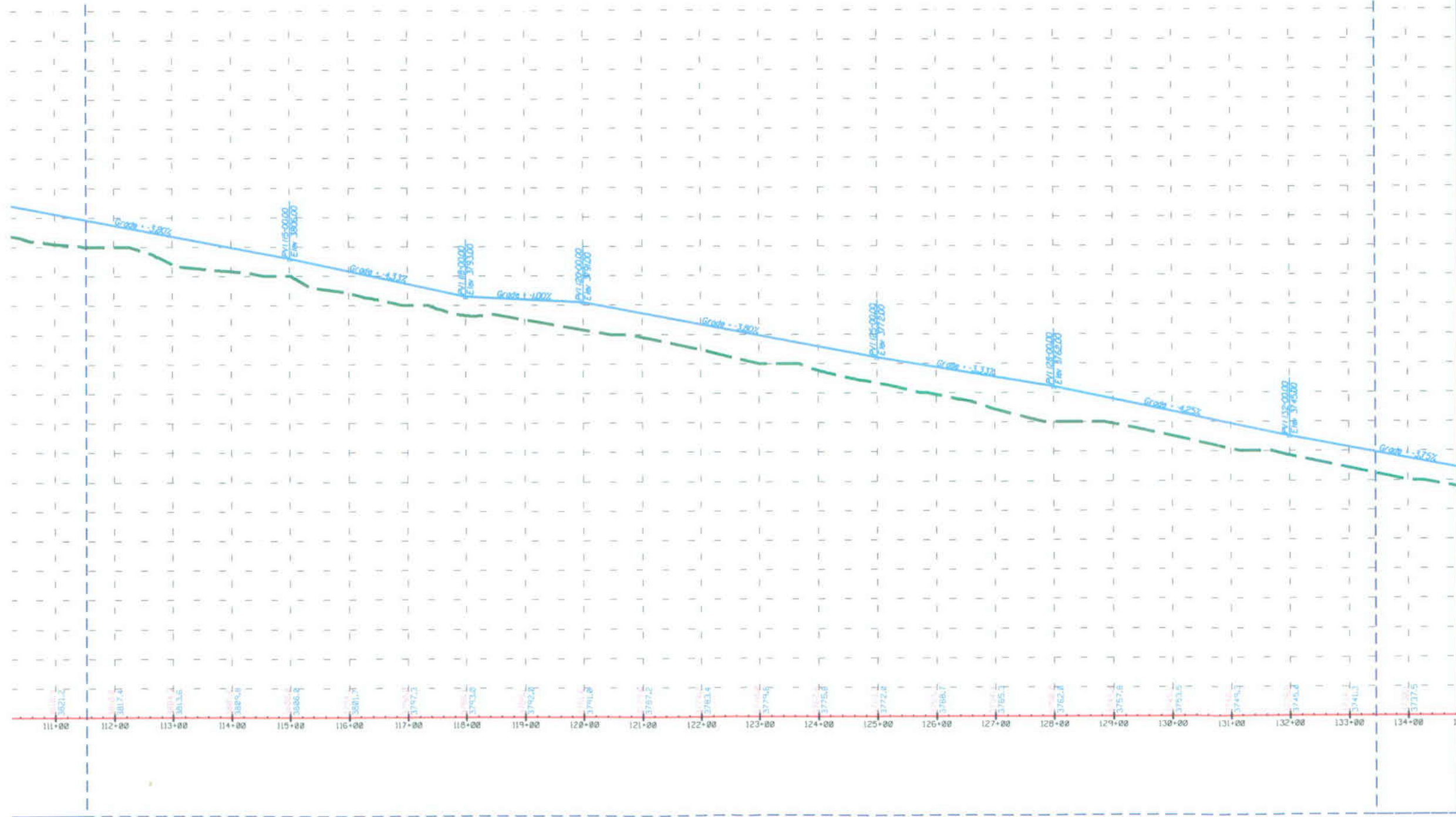
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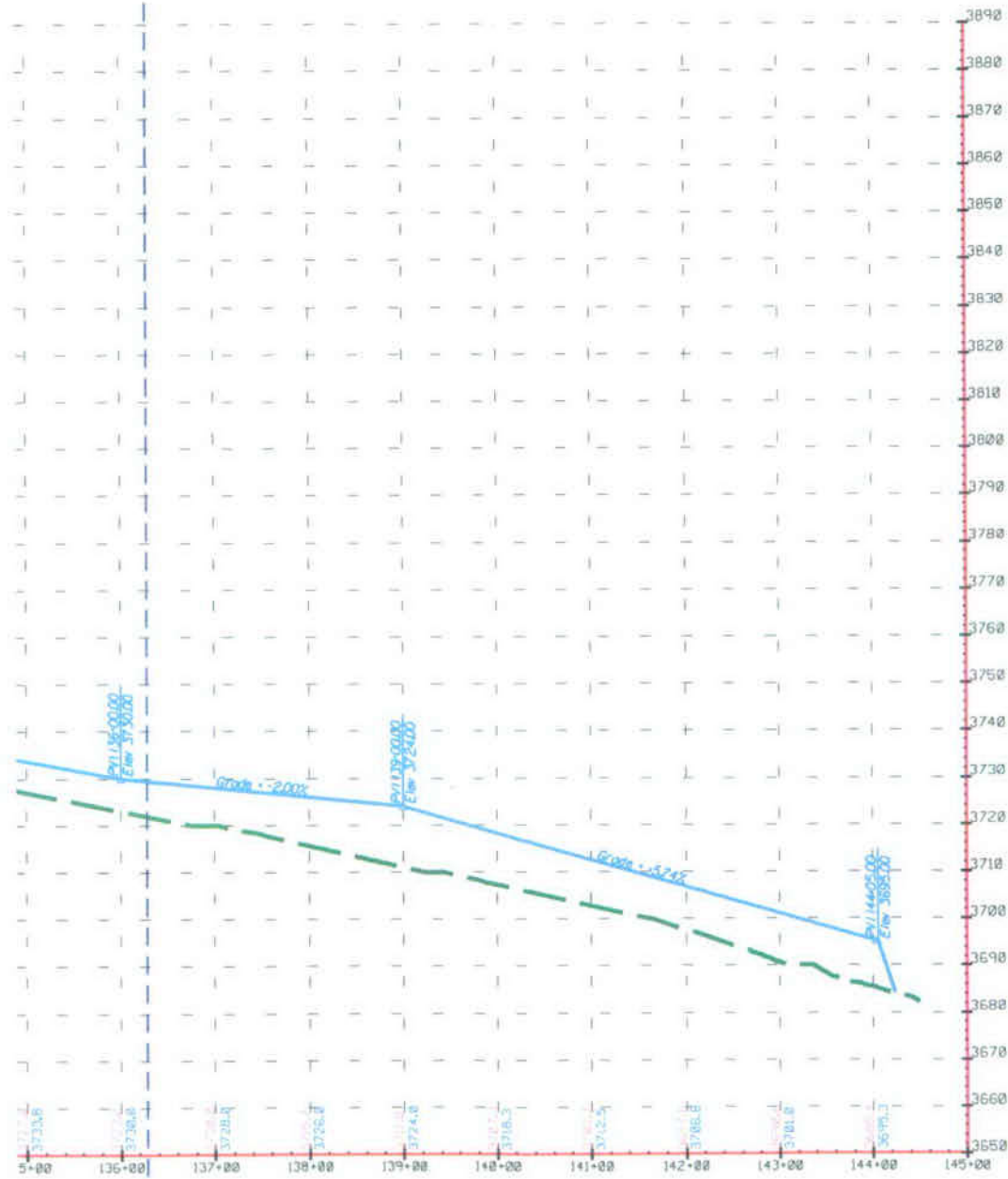
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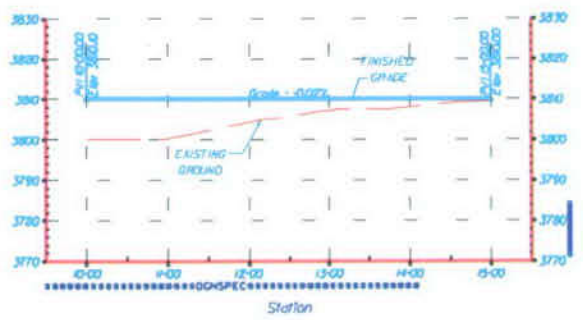
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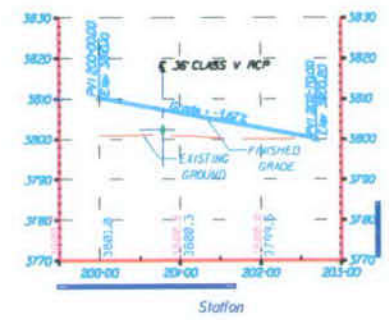
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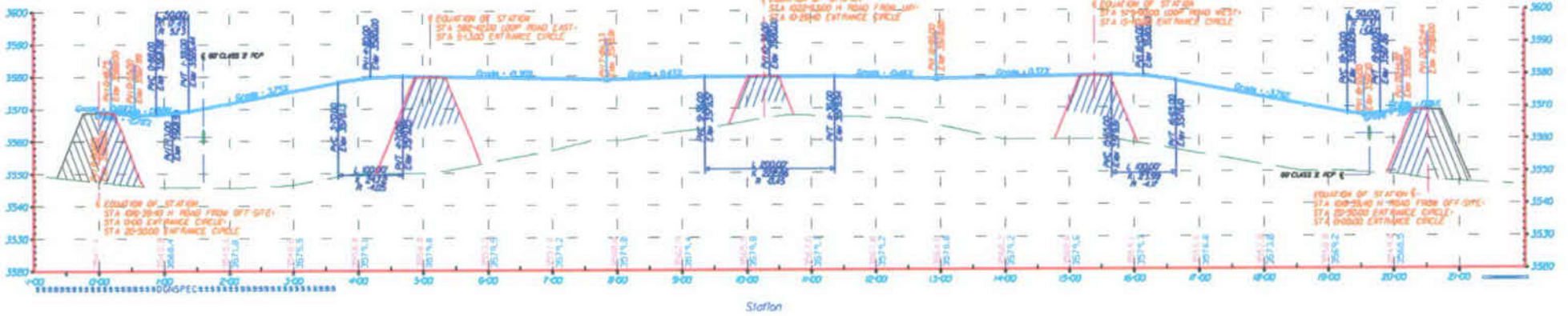
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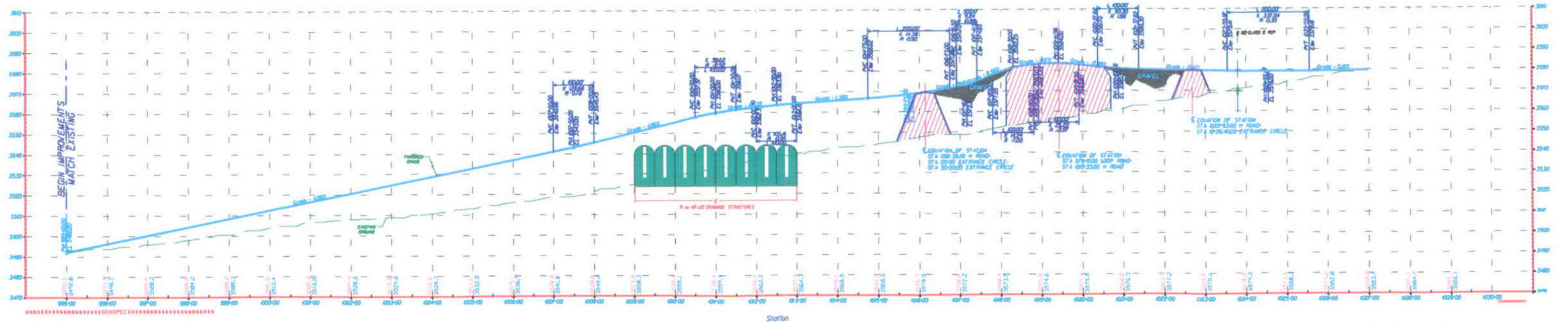
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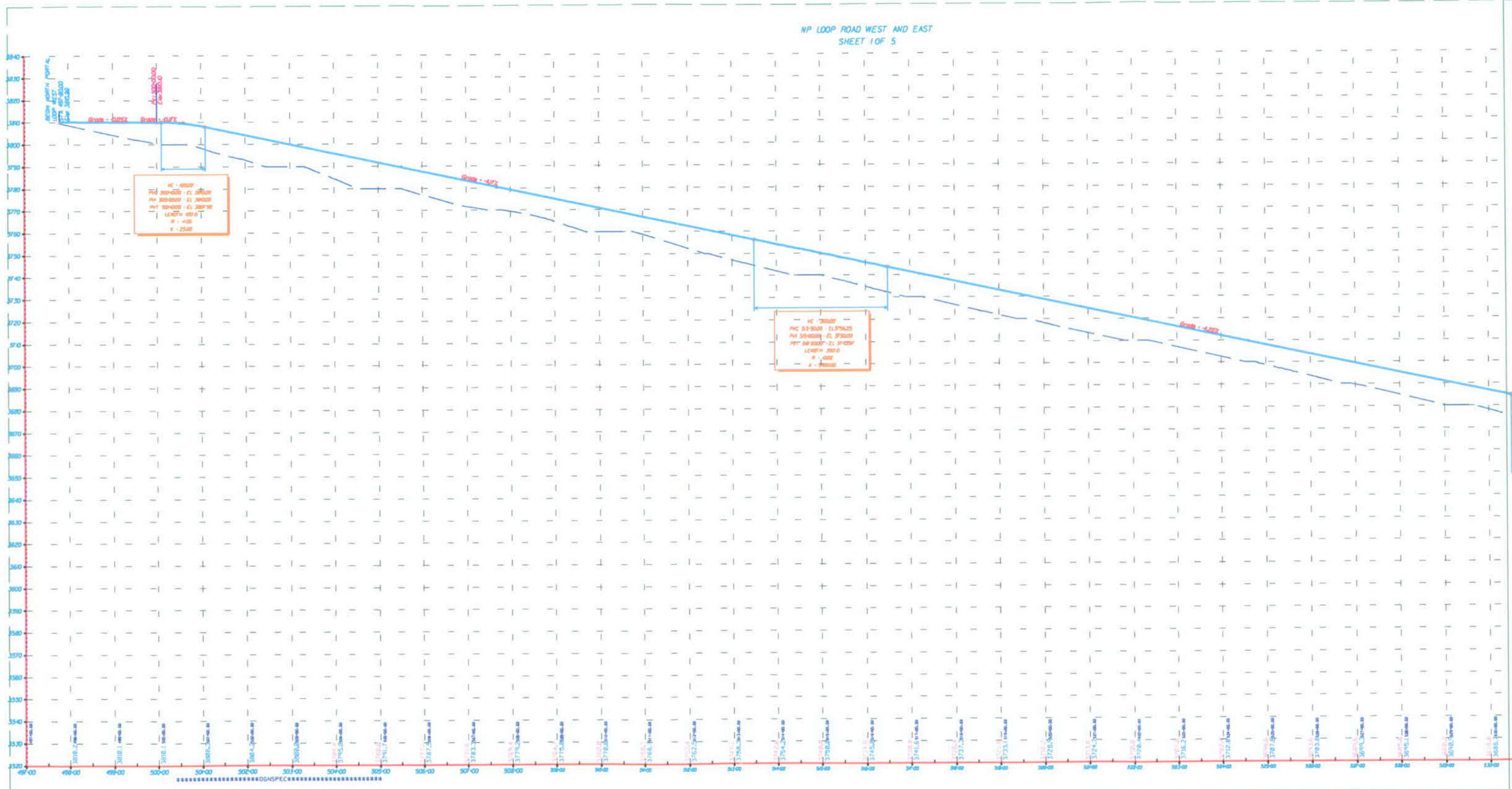


Entrance Circle

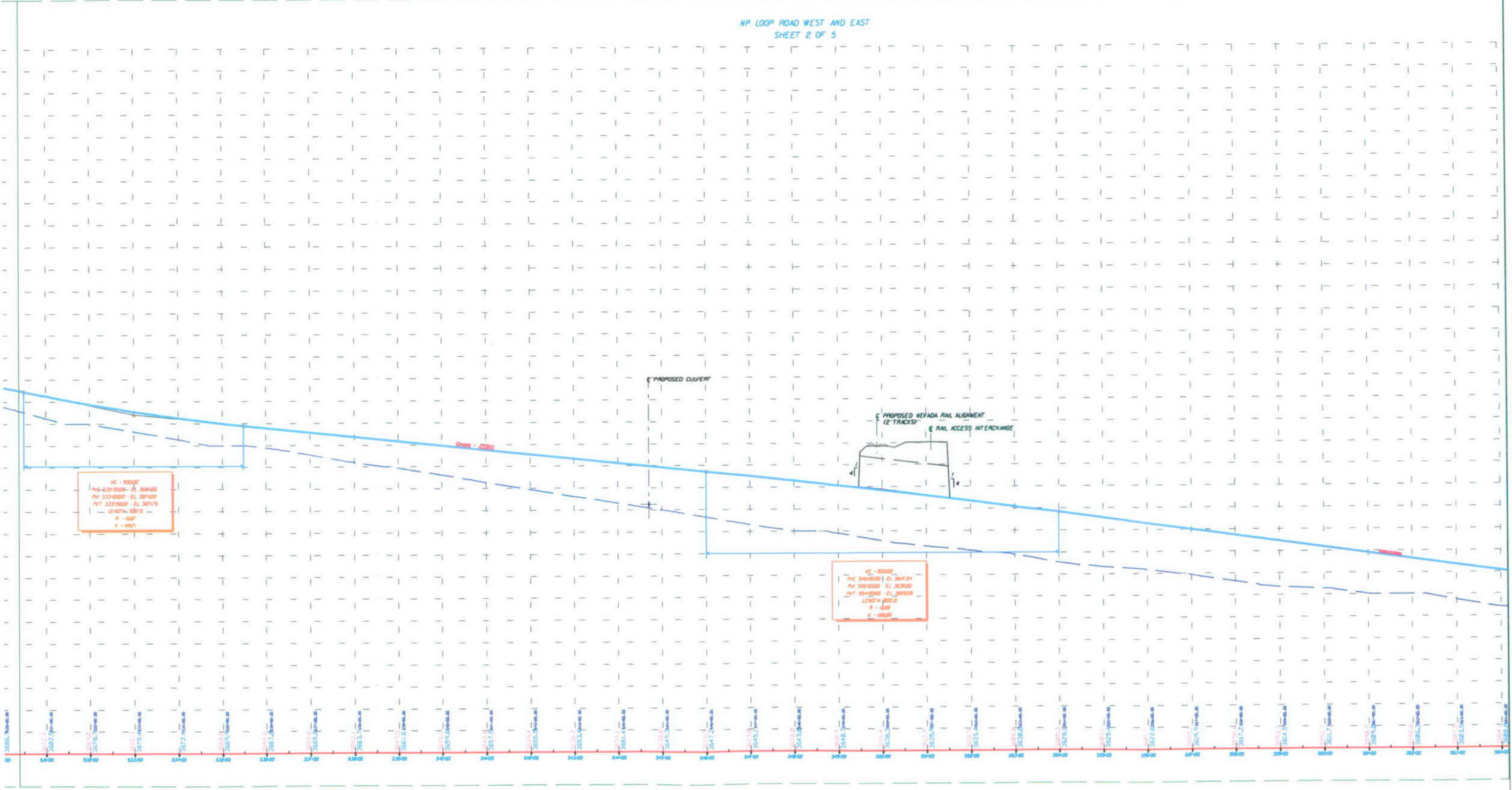


Plant North H Road





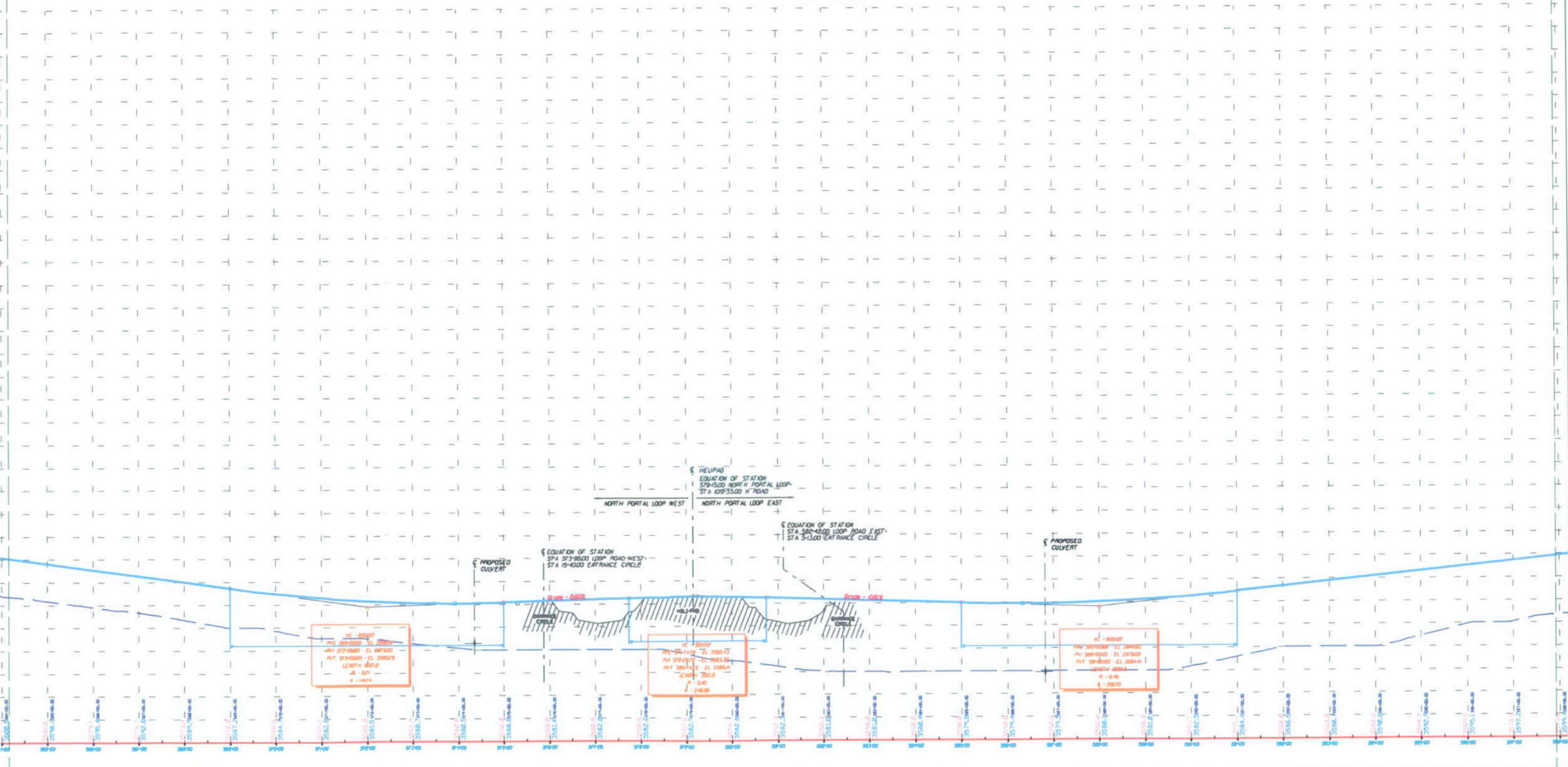
NP LOOP ROAD WEST AND EAST
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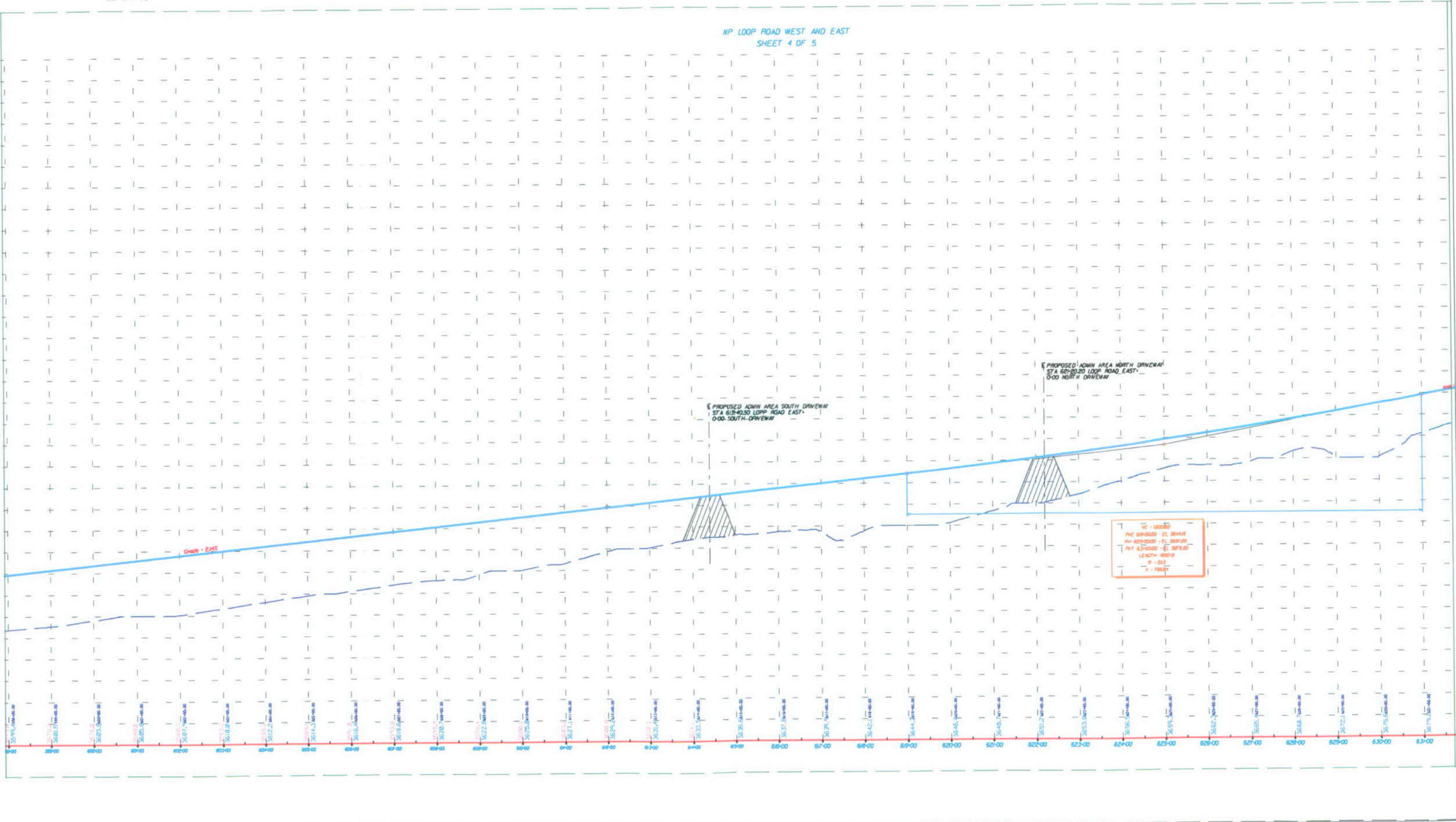
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3680.0 (elevation)

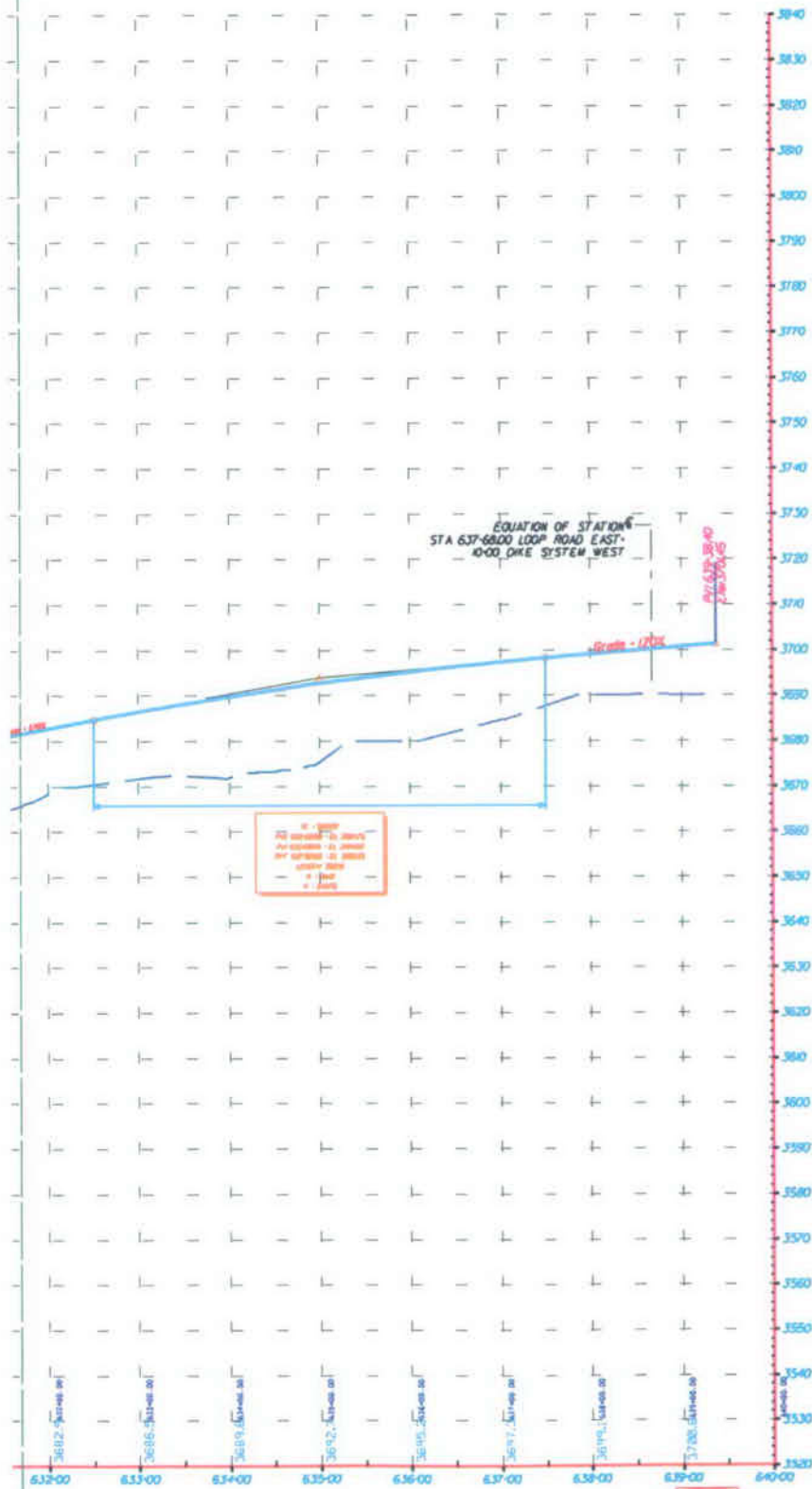
NP LOOP ROAD WEST AND EAST
 SHEET 3 OF 5



NP LOOP ROAD WEST AND EAST
 SHEET 4 OF 5



NP LOOP ROAD WEST AND EAST
SHEET 5 OF 5



KM COMBINE HYDROGRAPHS FROM SB7, SB8					KM	046
HC 2					HC	030
*						
KKCP5CP6					KK	045
KM ROUTE HYDROGRAPH FROM CP5 TO CP6					KM	046
RD 2000 .03 .09 TRAP	30	20			RD	087
*						
KK SB9					KK	045
KM SCS RUNOFF COMPUTATION FOR SB9					KM	046
BA 1.7					BA	008
UD .55					UD	112
*					*	001
KKSB9CP6					KK	045
KM ROUTE HYDROGRAPH FROM SB9 TO CP6					KM	046
RD 4700 .03 .09 TRAP	30	20			RD	087
*						
KK SB10					KK	045
KM SCS RUNOFF COMPUTATION FOR SB10					KM	046
BA 0.44					BA	008
UD .35					UD	112
*						
KK CP6					KK	045
KM COMBINE HYDROGRAPHS FROM CP5, SB10, SB9					KM	046
HC 3					HC	030
*						
KKCP6CP7					KK	045
KM ROUTE HYDROGRAPH FROM CP6 TO CP7					KM	046
RD 2100 .02 .09 TRAP	30	10			RD	087
*						
KK SB11					KK	045
KM SCS RUNOFF COMPUTATION FOR SB11					KM	046
BA 0.46					BA	008
UD .40					UD	112
*						
KK CP7					KK	045
KM COMBINE HYDROGRAPHS FROM CP6, SB11					KM	046
HC 2					HC	030
*						
KKCP7CP8					KK	045
KM ROUTE HYDROGRAPH FROM CP7 TO CP8					KM	046
RD 2000 .02 .09 TRAP	30	4			RD	087
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KK SB12					KK	045
KM SCS RUNOFF COMPUTATION FOR SB12					KM	046
BA 0.15					BA	008
UD .24					UD	112
*						
KK CP8					KK	045
KM COMBINE HYDROGRAPHS FROM CP7, SB12					KM	046
HC 2					HC	030
*						
KKCP8CP9					KK	045
KM ROUTE HYDROGRAPH FROM CP8 TO CP9					KM	046
RD 1700 .02 .09 TRAP	30	3			RD	087
*						
* combine south and north portal areas						
*						
KK CP9					KK	045
KM COMBINE HYDROGRAPHS FROM CP4, SB13, CP8					KM	046
HC 3					HC	030
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*						
ZZ						

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* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

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2         ID          YUCCA MOUNTAIN FLOOD STUDY PROJECT
3         ID          ANALYSIS BY URS CORPORATION
4         ID  FILE IDENTIFICATION INFORMATION
5         ID  FILENAME--\\S021emc2\yucca_pmf_study\HEC1\HEC-1\FINAL4.HC1
*         *          this run is based on response to comments
*         *          FIND Q AT CRITICAL LOCATIONS AFTER CONSTRUCTION OF FACILITIES
*         *          NUMBER OF BASINS DEFINED USING THE 2007 DRAWINGS SHOWN IN
*         *          ATTACHMENT A.
*         *
*         *          SET BASE OF WATERSHED AT THE GAP AT ALICE HILL
6         ID          USE PMP CALCULATED FOR STORM AT PORTAL & FACILITY
7         ID          PMP obtained from previous PMF study - ANL-EBS-MD-000060 Rev 00D
8         ID          PMP - 10/1/98 (COE ENGINEERING MANUAL TIME SEQUENCE)
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*         *
9         ID
*DIAGRAM
10        IT          3 01OCT98      0000      200
  
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      *
      *      watersheds are input in order from NE to SW as much as possible
      *
      *
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22      PI      .085      .085      .085      .085      .085      .085      .085      .085      .085      .085
23      PI      1.18      1.18      1.18      1.18      1.18      .38      .38      .38      .38      .38
24      PI      .18      .18      .18      .18      .18      .14      .14      .14      .14      .14
25      PI      .04      .04      .04      .04      .04      .04      .04      .04      .04      .04
26      PI      .04      .04      .04      .04      .04      .04      .04      .04      .04      .04
27      PI      .025      .025      .025      .025      .025      .025      .025      .025      .025      .025
28      PI      .025      .025      .025      .025      .025      .025      .025      .025      .025      .025
29      LU      1      1.5
30      UD      .64
      *

```

```

31      KK      SB1CP1
32      KM      ROUTE HYDROGRAPH FROM SB1 TO CP1
33      RD      2400      .02      .09      TRAP      78      3
      *

```

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

34      KK      SB2
35      KM      SCS RUNOFF COMPUTATION FOR SB2
36      BA      0.42
37      UD      .40
      *

```

```

38      KK      CP1
39      KM      COMBINE FLOWS FROM SB1 AND SB2
40      HC      2
      *

```

```

41      KK      CP1CP2
42      KM      ROUTE HYDROGRAPH FROM CP1 TO CP2
43      RD      2600      .02      .09      TRAP      68      3
      *

```

```

44      KK      SB3
45      KM      SCS RUNOFF COMPUTATION FOR SB3
46      BA      1.6
47      UD      .73
      *

```

```

48      KK      SB4
49      KM      SCS RUNOFF COMPUTATION FOR SB4
50      BA      1.2
51      UD      .66
      *

52      KK      CP2
53      KM      COMBINE FLOWS FROM SB3, SB4 and CP1
54      HC      3
      *

55      KK      CP2CP3
56      KM      ROUTE HYDROGRAPH FROM CP2 TO CP3
57      RD      3500 .02 .09 TRAP 88 3
      *

58      KK      AGING
59      KM      COMPUTE RUNOFF FROM Aging pad area USING OVERLAND FLOW ELEMENT
60      BA      0.460
61      LU      1 1.5 25.5 1 1.5 100
62      UK      .4000 .03 .1 83 50
63      UK      900 .02 .1 17 50
64      RK      3500 .02 .09 TRAP 88 3 NO 50
      *
      *

65      KK      CP3
66      KM      COMBINE FLOWS FROM CP2 and Aging1
67      HC      2
      *
  
```

1

HEC-1 INPUT

PAGE 3

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

68      KK      CP3CP4
69      KM      ROUTE HYDROGRAPH FROM CP3 TO CP4
70      RD      4100 .03 .09 TRAP 30 4
      *

71      KK      SB5
72      KM      SCS RUNOFF COMPUTATION FOR SB5
73      BA      0.39
74      LU      1 1.5 0
75      UD      .64
      *

76      KK      SB6
77      KM      SCS RUNOFF COMPUTATION FOR SB6
78      BA      0.76
79      UD      .76
      *

80      KK      CP4
81      KM      COMBINE FLOWS FROM SB5,SB6 and CP3
82      HC      3
      *
  
```



```

83      KK      CP4CP9
84      KM      ROUTE HYDROGRAPH FROM CP4 TO CP9
85      RD      3000 .02 .09 TRAP 30 20
      *

86      KK      SB13
87      KM      SCS RUNOFF COMPUTATION FOR SB13
88      BA      0.19
89      UD      .30
      *
      * Bottom of Northern watershed
      *
      *
      *
      *
      * south Portal Area

90      KK      SB7
91      KM      SCS RUNOFF COMPUTATION FOR SB7
92      BA      2.9
93      PB
94      PI      .020 0.020 .020 .020 .020 .020 .020 .020 .020 .020
95      PI      .020 0.020 .020 .020 .020 .020 .020 .020 .020 .020
96      PI      .030 .030 .030 .030 .030 .030 .030 .030 .030 .030
97      PI      .030 .030 .030 .030 .030 .030 .030 .030 .030 .030
98      PI      .080 .080 .080 .080 .080 .080 .080 .080 .080 .080
99      PI      .080 .080 .080 .080 .080 .080 .080 .080 .080 .080
100     PI      1.10 1.10 1.10 1.10 1.10 .36 .36 .36 .36 .36
101     PI      .18 .18 .18 .18 .18 .16 .16 .16 .16 .16
102     PI      .04 .04 .04 .04 .04 .04 .04 .04 .04 .04
103     PI      .04 .04 .04 .04 .04 .04 .04 .04 .04 .04
      *
      * HEC-1 INPUT

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
104      PI      .025 .025 .025 .025 .025 .025 .025 .025 .025 .025
105      PI      .025 .025 .025 .025 .025 .025 .025 .025 .025 .025
106      UD      .92
      *

107      KK      SB7CP5
108      KM      ROUTE HYDROGRAPH FROM SB7 TO CP5
109      RD      3200 .04 .09 TRAP 30 20
      *

110      KK      SB8
111      KM      SCS RUNOFF COMPUTATION FOR SB8
112      BA      1.2
113      UD      .60
      *

114      KK      CP5
115      KM      COMBINE HYDROGRAPHS FROM SB7, SB8
116      HC      2
      *

117      KK      CP5CP6
  
```

```

118      KM      ROUTE HYDROGRAPH FROM CP5 TO CP6
119      RD      2000 .03 .09 TRAP      30      20
          *

120      KK      SB9
121      KM      SCS RUNOFF COMPUTATION FOR SB9
122      BA      1.7
123      UD      .55
          *

124      KK      SB9CP6
125      KM      ROUTE HYDROGRAPH FROM SB9 TO CP6
126      RD      4700 .03 .09 TRAP      30      20
          *

127      KK      SB10
128      KM      SCS RUNOFF COMPUTATION FOR SB10
129      BA      0.44
130      UD      .35
          *

131      KK      CP6
132      KM      COMBINE HYDROGRAPHS FROM CP5, SB10, SB9
133      HC      3
          *

134      KK      CP6CP7
135      KM      ROUTE HYDROGRAPH FROM CP6 TO CP7
136      RD      2100 .02 .09 TRAP      30      10
          *
  
```

1

HEC-1 INPUT

PAGE 5

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

137      KK      SB11
138      KM      SCS RUNOFF COMPUTATION FOR SB11
139      BA      0.46
140      UD      .40
          *

141      KK      CP7
142      KM      COMBINE HYDROGRAPHS FROM CP6, SB11
143      HC      2
          *

144      KK      CP7CP8
145      KM      ROUTE HYDROGRAPH FROM CP7 TO CP8
146      RD      2000 .02 .09 TRAP      30      4
          *

147      KK      SB12
148      KM      SCS RUNOFF COMPUTATION FOR SB12
149      BA      0.15
150      UD      .24
          *

151      KK      CP8
  
```

```

152      KM   COMBINE HYDROGRAPHS FROM CP7, SB12
153      HC       2
        *
154      KK   CP8CP9
155      KM   ROUTE HYDROGRAPH FROM CP8 TO CP9
156      RD   1700 .02 .09          TRAP   30   3
        *
        *   combine south and north portal areas
        *
157      KK   CP9
158      KM   COMBINE HYDROGRAPHS FROM CP4, SB13, CP8
159      HC       3
        *
        *
160      ZZ
  
```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.             (.) CONNECTOR    (<---) RETURN OF DIVERTED OR PUMPED FLOW

12      SB1
        V
31      SB1CP1
        .
34      .          SB2
        .
38      CP1.....
        V
41      CP1CP2
        .
44      .          SB3
        .
48      .          .          SB4
        .
52      CP2.....
        V
55      CP2CP3
        .
58      .          AGING
        .
65      CP3.....
        V
68      CP3CP4
  
```

71	.	SB5	.
76	.	.	SB6
80	CP4
	V		
83	CP4CP9		
86	.	SB13	.
90	.	.	SB7
	.	.	V
	.	.	V
107	.	SB7CP5	.
110	.	.	SB8
114	.	CP5
	.	V	
	.	V	
117	.	CP5CP6	.
120	.	.	SB9
	.	.	V
	.	.	V
124	.	SB9CP6	.
127	.	.	SB10
131	.	CP6
	.	V	
	.	V	
134	.	CP6CP7	.
137	.	.	SB11
141	.	CP7
	.	V	
	.	V	
144	.	CP7CP8	.
147	.	.	SB12

151 CP8
 V
 V
 154 CP8CP9

 157 CP9

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 10AUG07 TIME 10:41:35 *
*
*****
  
```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****
  
```

HEC-1 FLOOD HYDROGRAPH SIMULATION
 YUCCA MOUNTAIN FLOOD STUDY PROJECT
 ANALYSIS BY URS CORPORATION
 FILE IDENTIFICATION INFORMATION
 FILENAME--\\S021emc2\yucca_pmf_study\HEC1\HEC-1\FINAL4.HC1
 USE PMP CALCULATED FOR STORM AT PORTAL & FACILITY
 PMP obtained from previous PMF study - ANL-EBS-MD-000060 Rev 00D
 PMP - 10/1/98 (COE ENGINEERING MANUAL TIME SEQUENCE)

11 IO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1OCT98 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 200 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1OCT98 ENDING DATE
 NDTIME 0957 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 9.95 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES

TEMPERATURE DEGREES FAHRENHEIT

```

*****
*           *
12 KK      *   SB1   *   watershed
*           *
*****
  
```

SCS RUNOFF COMPUTATION FOR SB1

```

15 IN      TIME DATA FOR INPUT TIME SERIES
           JXMIN      3   TIME INTERVAL IN MINUTES
           JXDATE    1OCT98  STARTING DATE
           JXTIME    0   STARTING TIME
  
```

SUBBASIN RUNOFF DATA

```

14 BA      SUBBASIN CHARACTERISTICS
           TAREA      .83  SUBBASIN AREA
  
```

PRECIPITATION DATA

```

16 PB      STORM      13.20  BASIN TOTAL PRECIPITATION
  
```

17 PI INCREMENTAL PRECIPITATION PATTERN

.01	.01	.01	.02	.01	.02	.02	.02	.01	.02
.02	.02	.02	.02	.02	.02	.02	.02	.01	.01
.03	.03	.03	.03	.03	.03	.03	.03	.03	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.08	.08	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.09	.09	.09	.09	.09
1.18	1.18	1.18	1.18	1.18	1.18	.38	.38	.38	.38
.18	.18	.18	.18	.18	.18	.14	.14	.14	.14
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

```

29 LU      UNIFORM LOSS RATE
           STRTL      1.00  INITIAL LOSS
           CNSTL      1.50  UNIFORM LOSS RATE
           RTIMP      .00  PERCENT IMPERVIOUS AREA
  
```

```

30 UD      SCS DIMENSIONLESS UNITGRAPH
           TLAG      .64  LAG
  
```

UNIT HYDROGRAPH
 66 END-OF-PERIOD ORDINATES

14.	39.	74.	115.	169.	236.	313.	399.	472.	529.
570.	597.	602.	600.	587.	559.	528.	493.	453.	407.
353.	305.	265.	233.	206.	182.	162.	146.	129.	115.
101.	88.	79.	70.	62.	55.	48.	43.	38.	33.

29. 26. 23. 21. 18. 16. 14. 12. 11. 10.
 9. 8. 7. 6. 6. 5. 5. 4. 3. 3.
 2. 2. 2. 1. 1. 0.

*** **

HYDROGRAPH AT STATION SB1

TOTAL RAINFALL = 13.20, TOTAL LOSS = 5.12, TOTAL EXCESS = 8.08

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	9.95-HR
+	4097.	721.	435.	435.	435.
	3.85	8.076	8.076	8.076	8.076
		358.	358.	358.	358.

CUMULATIVE AREA = .83 SQ MI

31 KK

 * SB1CP1 *

ROUTE HYDROGRAPH FROM SB1 TO CP1

HYDROGRAPH ROUTING DATA

33 RD

MUSKINGUM-CUNGE CHANNEL ROUTING
 L 2400. CHANNEL LENGTH
 S .0200 SLOPE
 N .090 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 78.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
MAIN	.17	1.59	3.00	800.00	4093.01	234.00	8.08	8.61

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.17	1.59	3.00		4093.01	234.00	8.08	
------	-----	------	------	--	---------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3575E+03 EXCESS= .0000E+00 OUTFLOW= .3576E+03 BASIN STORAGE= .1048E-01 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION SB1CP1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
4093.	3.90	721.	435.	435.	435.
		(INCHES)	8.079	8.079	8.079
		(AC-FT)	358.	358.	358.

CUMULATIVE AREA = .83 SQ MI

34 KK *
 * SB2 *
 *

SCS RUNOFF COMPUTATION FOR SB2

SUBBASIN RUNOFF DATA

36 BA SUBBASIN CHARACTERISTICS
 TAREA .42 SUBBASIN AREA

PRECIPITATION DATA

16 PB STORM 13.20 BASIN TOTAL PRECIPITATION

17 PI INCREMENTAL PRECIPITATION PATTERN

.01	.01	.01	.02	.01	.02	.02	.02	.01	.02
.02	.02	.02	.02	.02	.02	.02	.02	.01	.01
.03	.03	.03	.03	.03	.03	.03	.03	.03	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.08	.08	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.09	.09	.09	.09	.09
1.18	1.18	1.18	1.18	1.18	.38	.38	.38	.38	.38
.18	.18	.18	.18	.18	.14	.14	.14	.14	.14
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

29 LU UNIFORM LOSS RATE
 STRTL 1.00 INITIAL LOSS

870

37 UD CNSTL 1.50 UNIFORM LOSS RATE
 RTIMP .00 PERCENT IMPERVIOUS AREA
 SCS DIMENSIONLESS UNITGRAPH
 TLAG .40 LAG

UNIT HYDROGRAPH
 42 END-OF-PERIOD ORDINATES

20.	63.	121.	202.	304.	394.	451.	474.	474.	451.
412.	367.	308.	245.	198.	163.	134.	113.	94.	77.
63.	52.	43.	36.	29.	24.	20.	17.	14.	11.
9.	8.	6.	5.	5.	4.	3.	3.	2.	1.
1.	0.								

HYDROGRAPH AT STATION SB2

TOTAL RAINFALL = 13.20, TOTAL LOSS = 5.12, TOTAL EXCESS = 8.08

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
2881.	3.60	365.	220.	220.	220.
		(INCHES) (AC-FT)	8.076 181.	8.076 181.	8.076 181.
CUMULATIVE AREA =		.42 SQ MI			

38 KK

 *
 * CP1 *
 *

COMBINE FLOWS FROM SB1 AND SB2

40 HC

HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
		(CFS)			

JPD

+ 6164. 3.75 1086. 655. 655. 655.
 (INCHES) 8.078 8.078 8.078 8.078
 (AC-FT) 539. 539. 539. 539.
 CUMULATIVE AREA = 1.25 SQ MI

 * CP1CP2 *
 * *

ROUTE HYDROGRAPH FROM CP1 TO CP2

HYDROGRAPH ROUTING DATA

43 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 2600. CHANNEL LENGTH
 S .0200 SLOPE
 N .090 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 68.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.19	1.58	3.00	866.67	6159.40	228.00	8.08	10.29

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.19	1.58	3.00		6159.40	228.00	8.08	
------	-----	------	------	--	---------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5385E+03 EXCESS= .0000E+00 OUTFLOW= .5387E+03 BASIN STORAGE= .9970E-02 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION CP1CP2

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ (CFS)	(HR)	(CFS)			

JPD

+ 6159. 3.80 (INCHES) 1086. 655. 655. 655.
 (AC-FT) 8.080 8.080 8.080 8.080
 539. 539. 539. 539.
 CUMULATIVE AREA = 1.25 SQ MI

44 KK *****
 * SB3 *
 * *

 SCS RUNOFF COMPUTATION FOR SB3

SUBBASIN RUNOFF DATA

46 BA SUBBASIN CHARACTERISTICS
 TAREA 1.60 SUBBASIN AREA

PRECIPITATION DATA

16 PB STORM 13.20 BASIN TOTAL PRECIPITATION

17 PI INCREMENTAL PRECIPITATION PATTERN

.01	.01	.01	.02	.01	.02	.02	.02	.01	.02
.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.03	.03	.03	.03	.03	.03	.03	.03	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.08	.08	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.09	.09	.09	.09	.09
1.18	1.18	1.18	1.18	1.18	.38	.38	.38	.38	.38
.18	.18	.18	.18	.18	.14	.14	.14	.14	.14
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

29 LU UNIFORM LOSS RATE
 STRTL 1.00 INITIAL LOSS
 CNSTL 1.50 UNIFORM LOSS RATE
 RTIMP .00 PERCENT IMPERVIOUS AREA

47 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .73 LAG

UNIT HYDROGRAPH
 75 END-OF-PERIOD ORDINATES

20.	54.	101.	162.	233.	314.	422.	539.	668.	778.
872.	946.	990.	1016.	1023.	1018.	998.	957.	910.	860.
806.	740.	668.	586.	516.	455.	408.	366.	327.	293.
267.	242.	217.	196.	176.	155.	140.	127.	113.	102.

JPD

92.	82.	73.	66.	59.	53.	48.	43.	38.	35.
31.	28.	25.	22.	20.	18.	16.	15.	13.	12.
11.	10.	9.	8.	8.	7.	6.	5.	4.	4.
3.	2.	2.	1.	0.					

*** *** *** *** ***

HYDROGRAPH AT STATION SB3

TOTAL RAINFALL = 13.20, TOTAL LOSS = 5.12, TOTAL EXCESS = 8.08

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 7148.	3.95	1390.	838.	838.	838.
		(INCHES)	8.076	8.076	8.076
		(AC-FT)	689.	689.	689.

CUMULATIVE AREA = 1.60 SQ MI

48 KK

```

*****
*           *
*   SB4   *
*           *
*****
  
```

SCS RUNOFF COMPUTATION FOR SB4

SUBBASIN RUNOFF DATA

50 BA

SUBBASIN CHARACTERISTICS
 TAREA 1.20 SUBBASIN AREA

PRECIPITATION DATA

16 PB

STORM 13.20 BASIN TOTAL PRECIPITATION

17 PI

INCREMENTAL PRECIPITATION PATTERN

.01	.01	.01	.02	.01	.02	.02	.02	.01	.02
.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.03	.03	.03	.03	.03	.03	.03	.03	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.08	.08	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.09	.09	.09	.09	.09
1.18	1.18	1.18	1.18	1.18	.38	.38	.38	.38	.38
.18	.18	.18	.18	.18	.14	.14	.14	.14	.14
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

29 LU

UNIFORM LOSS RATE

8 PD

STRTL 1.00 INITIAL LOSS
 CNSTL 1.50 UNIFORM LOSS RATE
 RTIMP .00 PERCENT IMPERVIOUS AREA

51 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .66 LAG

UNIT HYDROGRAPH
 68 END-OF-PERIOD ORDINATES

19.	53.	99.	155.	227.	314.	415.	533.	636.	722.
788.	826.	842.	844.	838.	803.	763.	718.	669.	609.
542.	469.	407.	359.	317.	280.	249.	223.	201.	178.
159.	141.	123.	111.	98.	87.	78.	68.	61.	54.
47.	42.	38.	33.	30.	27.	24.	21.	19.	17.
15.	13.	12.	10.	9.	8.	8.	7.	6.	5.
5.	4.	3.	3.	2.	2.	1.	0.		

HYDROGRAPH AT STATION SB4

TOTAL RAINFALL = 13.20, TOTAL LOSS = 5.12, TOTAL EXCESS = 8.08

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
5782.	3.90	1042.	629.	629.	629.
		(INCHES) 8.076	8.076	8.076	8.076
		(AC-FT) 517.	517.	517.	517.

CUMULATIVE AREA = 1.20 SQ MI

 * *
 52 KK CP2 *
 * *

COMBINE FLOWS FROM SB3, SB4 and CP1

54 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP2

PEAK FLOW TIME MAXIMUM AVERAGE FLOW

820

			6-HR	24-HR	72-HR	9.95-HR
+	(CFS)	(HR)				
		(CFS)				
+	18927.	3.90	3519.	2122.	2122.	2122.
		(INCHES)	8.078	8.078	8.078	8.078
		(AC-FT)	1745.	1745.	1745.	1745.

CUMULATIVE AREA = 4.05 SQ MI

55 KK *****
 * CP2CP3 *

ROUTE HYDROGRAPH FROM CP2 TO CP3

HYDROGRAPH ROUTING DATA

57 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	3500.	CHANNEL LENGTH
S	.0200	SLOPE
N	.090	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	88.00	BOTTOM WIDTH OR DIAMETER
Z	30.00	SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.26	1.41	3.00	875.00	18905.50	240.00	8.08	8.03

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.26	1.41	3.00		18905.50	240.00	8.08	
------	-----	------	------	--	----------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1745E+04 EXCESS= .0000E+00 OUTFLOW= .1745E+04 BASIN STORAGE= .1214E-01 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION CP2CP3

PEAK FLOW TIME MAXIMUM AVERAGE FLOW

APD

			6-HR	24-HR	72-HR	9.95-HR
+	(CFS)	(HR)				
		(CFS)				
+	18906.	4.00	3520.	2122.	2122.	2122.
		(INCHES)	8.080	8.080	8.080	8.080
		(AC-FT)	1745.	1745.	1745.	1745.

CUMULATIVE AREA = 4.05 SQ MI

 * AGING *
 *

58 KK

COMPUTE RUNOFF FROM Aging pad area USING OVERLAND FLOW ELEMENT

SUBBASIN RUNOFF DATA

60 BA SUBBASIN CHARACTERISTICS
 TAREA .46 SUBBASIN AREA

PRECIPITATION DATA

16 PB STORM 13.20 BASIN TOTAL PRECIPITATION

17 PI INCREMENTAL PRECIPITATION PATTERN

.01	.01	.01	.02	.01	.02	.02	.02	.01	.02
.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.03	.03	.03	.03	.03	.03	.03	.03	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.08	.08	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.09	.09	.09	.09	.09
1.18	1.18	1.18	1.18	1.18	.38	.38	.38	.38	.38
.18	.18	.18	.18	.18	.14	.14	.14	.14	.14
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

61 LU UNIFORM LOSS RATE

STRTL	1.00	INITIAL LOSS
CNSTL	1.50	UNIFORM LOSS RATE
RTIMP	25.50	PERCENT IMPERVIOUS AREA

LOSS RATE VARIABLES FOR SECOND OVERLAND FLOW ELEMENT

STRTL	1.00	INITIAL LOSS
CNSTL	1.50	UNIFORM LOSS RATE
RTIMP	100.00	PERCENT IMPERVIOUS AREA

62 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 4000. OVERLAND FLOW LENGTH

890

63 UK
 S .0300 SLOPE
 N .100 ROUGHNESS COEFFICIENT
 PA 83.0 PERCENT OF SUBBASIN
 DXMIN 50 MINIMUM NUMBER OF DX INTERVALS
 OVERLAND-FLOW ELEMENT NO. 2
 L 900. OVERLAND FLOW LENGTH
 S .0200 SLOPE
 N .100 ROUGHNESS COEFFICIENT
 PA 17.0 PERCENT OF SUBBASIN
 DXMIN 50 MINIMUM NUMBER OF DX INTERVALS

64 RK
 KINEMATIC WAVE
 MAIN CHANNEL
 L 3500. CHANNEL LENGTH
 S .0200 SLOPE
 N .090 CHANNEL ROUGHNESS COEFFICIENT
 CA .46 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 88.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 NDXMIN 50 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	2.58	1.67	.54	80.00	2970.04	208.64	9.31	3.09
PLANE2	2.11	1.67	.31	18.00	1189.81	194.88	13.18	1.99
MAIN	.15	1.59	.27	70.00	3441.74	202.75	9.94	10.32

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2461E+03 OUTFLOW= .2439E+03 BASIN STORAGE= .1963E+01 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .15 1.59 3.00 3436.19 204.00 9.94

*** *** *** *** ***

HYDROGRAPH AT STATION AGING

TOTAL RAINFALL = 13.20, TOTAL LOSS = 3.17, TOTAL EXCESS = 10.03

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	9.95-HR (CFS)
+	3436.	3.40	486.	297.	297.
+			9.825	9.943	9.943
			241.	244.	244.

880

CUMULATIVE AREA = .46 SQ MI

65 KK

 * CP3 *
 * *

COMBINE FLOWS FROM CP2 and Aging1

67 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CP3

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
		(CFS)			
+ 20138.	3.95	4006.	2419.	2419.	2419.
		(INCHES)	8.258	8.270	8.270
		(AC-FT)	1986.	1989.	1989.

CUMULATIVE AREA = 4.51 SQ MI

68 KK

 * CP3CP4 *
 * *

ROUTE HYDROGRAPH FROM CP3 TO CP4

HYDROGRAPH ROUTING DATA

70 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	4100.	CHANNEL LENGTH
S	.0300	SLOPE
N	.090	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
W	30.00	BOTTOM WIDTH OR DIAMETER
Z	40.00	SIDE SLOPE

gpd

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.47	1.35	3.00	820.00	20106.10	243.00	8.27	8.41

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.47	1.35	3.00		20106.10	243.00	8.27	
------	-----	------	------	--	----------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1989E+04 EXCESS= .0000E+00 OUTFLOW= .1989E+04 BASIN STORAGE= .7397E+00 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION CP3CP4

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 20106.	4.05	4006.	2419.	2419.	2419.
		(INCHES) 8.259	8.271	8.271	8.271
		(AC-FT) 1987.	1989.	1989.	1989.

CUMULATIVE AREA = 4.51 SQ MI

71 KK *****
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 * *
 * *
 * *

SCS RUNOFF COMPUTATION FOR SB5

SUBBASIN RUNOFF DATA

73 BA SUBBASIN CHARACTERISTICS
 TAREA .39 SUBBASIN AREA

PRECIPITATION DATA

16 PB STORM 13.20 BASIN TOTAL PRECIPITATION

17 PI INCREMENTAL PRECIPITATION PATTERN

JPD

*

SCS RUNOFF COMPUTATION FOR SB6

SUBBASIN RUNOFF DATA

78 BA SUBBASIN CHARACTERISTICS
TAREA .76 SUBBASIN AREA

PRECIPITATION DATA

16 PB STORM 13.20 BASIN TOTAL PRECIPITATION

17 PI INCREMENTAL PRECIPITATION PATTERN

.01	.01	.01	.02	.01	.02	.02	.02	.01	.02
.02	.02	.02	.02	.02	.02	.02	.02	.01	.01
.03	.03	.03	.03	.03	.03	.03	.03	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.08	.08	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.09	.09	.09	.09	.09
1.18	1.18	1.18	1.18	1.18	.38	.38	.38	.38	.38
.18	.18	.18	.18	.18	.14	.14	.14	.14	.14
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

74 LU UNIFORM LOSS RATE
STRTL 1.00 INITIAL LOSS
CNSTL 1.50 UNIFORM LOSS RATE
RTIMP .00 PERCENT IMPERVIOUS AREA

79 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .76 LAG

UNIT HYDROGRAPH
78 END-OF-PERIOD ORDINATES

9.	23.	44.	70.	99.	135.	179.	228.	285.	336.
384.	417.	443.	461.	466.	467.	464.	450.	432.	411.
388.	364.	334.	302.	266.	236.	209.	188.	169.	152.
137.	124.	114.	103.	93.	84.	75.	67.	61.	55.
49.	45.	40.	36.	33.	29.	26.	24.	21.	19.
17.	16.	14.	13.	12.	10.	9.	8.	8.	7.
6.	6.	5.	5.	4.	4.	4.	3.	3.	3.
2.	2.	2.	1.	1.	1.	0.	0.		

HYDROGRAPH AT STATION SB6

TOTAL RAINFALL = 13.20, TOTAL LOSS = 5.12, TOTAL EXCESS = 8.08

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW
(CFS)	(HR)	6-HR 24-HR 72-HR 9.95-HR
+	(CFS)	

820

+ 3290. 4.00 660. 398. 398. 398.
 (INCHES) 8.076 8.076 8.076 8.076
 (AC-FT) 327. 327. 327. 327.
 CUMULATIVE AREA = .76 SQ MI

80 KK

 * CP4 *

COMBINE FLOWS FROM SB5, SB6 and CP3

82 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CP4

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 25090.	4.05	5005.	3022.	3022.	3022.
		(INCHES) 8.222	8.231	8.231	8.231
		(AC-FT) 2482.	2485.	2485.	2485.

CUMULATIVE AREA = 5.66 SQ MI

83 KK

 * CP4CP9 *

ROUTE HYDROGRAPH FROM CP4 TO CP9

HYDROGRAPH ROUTING DATA

85 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 3000. CHANNEL LENGTH
 S .0200 SLOPE
 N .090 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA

JP

SHAPE TRAP CHANNEL SHAPE
 WD 30.00 BOTTOM WIDTH OR DIAMETER
 Z 20.00 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.41	1.37	3.00	1000.00	25046.78	246.00	8.23	9.46

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.41	1.37	3.00		25046.78	246.00	8.23	
------	-----	------	------	--	----------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2485E+04 EXCESS= .0000E+00 OUTFLOW= .2485E+04 BASIN STORAGE= .6271E+00 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION CP4CP9

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW 6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	9.95-HR (CFS)
+ 25047.	4.10	5006.	8.223	2482.	3022.
		3022.	8.231	2485.	3022.
		3022.	8.231	2485.	3022.
		3022.	8.231	2485.	3022.

CUMULATIVE AREA = 5.66 SQ MI

86 KK

 * SB13 *
 * *

SCS RUNOFF COMPUTATION FOR SB13

SUBBASIN RUNOFF DATA

88 BA

SUBBASIN CHARACTERISTICS
 TAREA .19 SUBBASIN AREA

PRECIPITATION DATA

8 PD

16 PB STORM 13.20 BASIN TOTAL PRECIPITATION

17 PI INCREMENTAL PRECIPITATION PATTERN

.01	.01	.01	.02	.01	.02	.02	.02	.01	.02
.02	.02	.02	.02	.02	.02	.02	.01	.01	.01
.03	.03	.03	.03	.03	.03	.03	.03	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.08	.08	.09	.09	.09	.09	.09	.09	.09	.09
.09	.09	.09	.09	.08	.09	.09	.09	.09	.09
1.18	1.18	1.18	1.18	1.18	.38	.38	.38	.38	.38
.18	.18	.18	.18	.18	.14	.14	.14	.14	.14
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

74 LU UNIFORM LOSS RATE

STRTL 1.00 INITIAL LOSS
 CNSTL 1.50 UNIFORM LOSS RATE
 RTIMP .00 PERCENT IMPERVIOUS AREA

89 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .30 LAG

UNIT HYDROGRAPH
 32 END-OF-PERIOD ORDINATES

19.	56.	115.	193.	253.	280.	280.	257.	224.	179.
132.	102.	79.	63.	49.	38.	30.	23.	18.	14.
11.	8.	7.	5.	4.	3.	3.	2.	2.	1.
1.	0.								

HYDROGRAPH AT STATION SB13

TOTAL RAINFALL = 13.20, TOTAL LOSS = 5.12, TOTAL EXCESS = 8.08

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
1555.	3.45	165.	100.	100.	100.
		8.076	8.076	8.076	8.076
		82.	82.	82.	82.

CUMULATIVE AREA = .19 SQ MI

 * *
 90 KK * SB7 *

JPO

*

SCS RUNOFF COMPUTATION FOR SB7

15 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 3 TIME INTERVAL IN MINUTES
JXDATE 1OCT98 STARTING DATE
JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

92 BA SUBBASIN CHARACTERISTICS
TAREA 2.90 SUBBASIN AREA

PRECIPITATION DATA

93 PB STORM 12.90 BASIN TOTAL PRECIPITATION

94 PI INCREMENTAL PRECIPITATION PATTERN

.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
1.10	1.10	1.10	1.10	1.10	.36	.36	.36	.36	.36	.36
.18	.18	.18	.18	.18	.16	.16	.16	.16	.16	.16
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

74 LU UNIFORM LOSS RATE
STRIL 1.00 INITIAL LOSS
CNSTL 1.50 UNIFORM LOSS RATE
RTIMP .00 PERCENT IMPERVIOUS AREA

106 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .92 LAG

UNIT HYDROGRAPH

94 END-OF-PERIOD ORDINATES

24.	51.	105.	164.	234.	313.	407.	515.	640.	779.
928.	1061.	1187.	1282.	1368.	1420.	1467.	1475.	1482.	1474.
1458.	1411.	1361.	1306.	1248.	1185.	1114.	1035.	947.	853.
771.	692.	634.	579.	532.	486.	446.	409.	381.	352.
323.	297.	273.	250.	226.	208.	192.	176.	161.	148.
137.	125.	113.	105.	96.	88.	80.	74.	68.	62.
57.	53.	48.	44.	41.	38.	34.	31.	29.	27.
24.	22.	20.	19.	17.	16.	15.	14.	13.	12.
11.	10.	9.	8.	7.	7.	6.	5.	4.	4.
3.	2.	1.	0.						

HYDROGRAPH AT STATION

SB7

JPD

TOTAL RAINFALL = 12.90, TOTAL LOSS = 5.30, TOTAL EXCESS = 7.60

PEAK FLOW (CFS)	TIME (HR)	(CFS)	6-HR	24-HR	72-HR	9.95-HR
+ 10053.	4.15	2370.	1429.	1429.	1429.	1429.
		(INCHES)	7.600	7.600	7.600	7.600
		(AC-FT)	1175.	1175.	1175.	1175.

CUMULATIVE AREA = 2.90 SQ MI

107 KK

 * SB7CP5 *
 * *

ROUTE HYDROGRAPH FROM SB7 TO CPS

HYDROGRAPH ROUTING DATA

109 RD

MUSKINGUM-CUNGE CHANNEL ROUTING

L	3200.	CHANNEL LENGTH
S	.0400	SLOPE
N	.090	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	30.00	BOTTOM WIDTH OR DIAMETER
Z	20.00	SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.59	1.37	3.00	800.00	10052.46	255.00	7.60	9.48

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.59	1.37	3.00		10052.46	255.00	7.60	
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .1175E+04 EXCESS= .0000E+00 OUTFLOW= .1176E+04 BASIN STORAGE= .5540E-02 PERCENT ERROR= .0

*** *** *** *** ***

SPD

HYDROGRAPH AT STATION SB7CP5

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
10052.	4.25	2371.	1430.	1430.	1430.
		(INCHES) 7.600	7.601	7.601	7.601
		(AC-FT) 1176.	1176.	1176.	1176.

CUMULATIVE AREA = 2.90 SQ MI

110 KK

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*           *
*   SB8   *
*           *
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SCS RUNOFF COMPUTATION FOR SB8

SUBBASIN RUNOFF DATA

112 BA

SUBBASIN CHARACTERISTICS
 TAREA 1.20 SUBBASIN AREA

PRECIPITATION DATA

93 PB

STORM 12.90 BASIN TOTAL PRECIPITATION

94 PI

INCREMENTAL PRECIPITATION PATTERN

.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
1.10	1.10	1.10	1.10	1.10	.36	.36	.36	.36	.36	.36
.18	.18	.18	.18	.18	.16	.16	.16	.16	.16	.16
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

74 LU

UNIFORM LOSS RATE

STRTL 1.00 INITIAL LOSS
 CNSTL 1.50 UNIFORM LOSS RATE
 RTIMP .00 PERCENT IMPERVIOUS AREA

113 UD

SCS DIMENSIONLESS UNITGRAPH
 TLAG .60 LAG

JPO

 * CP5CP6 *
 *

ROUTE HYDROGRAPH FROM CP5 TO CP6

HYDROGRAPH ROUTING DATA

119 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 2000. CHANNEL LENGTH
 S .0300 SLOPE
 N .090 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 30.00 BOTTOM WIDTH OR DIAMETER
 Z 20.00 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.51	1.37	3.00	1000.00	14233.66	246.00	7.60	9.39

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.51	1.37	3.00		14233.66	246.00	7.60	
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .1662E+04 EXCESS= .0000E+00 OUTFLOW= .1662E+04 BASIN STORAGE= .2786E-02 PERCENT ERROR= .0

HYDROGRAPH AT STATION CP5CP6

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 14234.	4.10	3352.	2021.	2021.	2021.
		(INCHES) 7.600	7.601	7.601	7.601
		(AC-FT) 1662.	1662.	1662.	1662.
CUMULATIVE AREA =		4.10 SQ MI			

880

* SB9 *
* *

SCS RUNOFF COMPUTATION FOR SB9

SUBBASIN RUNOFF DATA

122 BA SUBBASIN CHARACTERISTICS
TAREA 1.70 SUBBASIN AREA

PRECIPITATION DATA

93 PB STORM 12.90 BASIN TOTAL PRECIPITATION

94 PI INCREMENTAL PRECIPITATION PATTERN

.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
1.10	1.10	1.10	1.10	1.10	.36	.36	.36	.36	.36	.36
.18	.18	.18	.18	.18	.16	.16	.16	.16	.16	.16
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

74 LU UNIFORM LOSS RATE
STRTL 1.00 INITIAL LOSS
CNSTL 1.50 UNIFORM LOSS RATE
RTIMP .00 PERCENT IMPERVIOUS AREA

123 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .55 LAG

UNIT HYDROGRAPH
57 END-OF-PERIOD ORDINATES

37.	117.	221.	353.	522.	730.	962.	1161.	1301.	1388.
1422.	1422.	1388.	1311.	1223.	1124.	1002.	859.	725.	618.
535.	462.	400.	354.	309.	270.	232.	200.	175.	151.
132.	114.	99.	85.	74.	65.	56.	49.	42.	37.
32.	28.	24.	21.	18.	16.	14.	13.	11.	10.
8.	7.	6.	4.	3.	2.	1.			

SPD

HYDROGRAPH AT STATION SB9

TOTAL RAINFALL = 12.90, TOTAL LOSS = 5.30, TOTAL EXCESS = 7.60

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
8684.	3.75	1390.	838.	838.	838.
		(INCHES) 7.600	7.600	7.600	7.600
		(AC-FT) 689.	689.	689.	689.

CUMULATIVE AREA = 1.70 SQ MI

124 KK

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*
* SB9CP6
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ROUTE HYDROGRAPH FROM SB9 TO CP6

HYDROGRAPH ROUTING DATA

126 RD

MUSKINGUM-CUNGE CHANNEL ROUTING

L	4700.	CHANNEL LENGTH
S	.0300	SLOPE
N	.090	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	30.00	BOTTOM WIDTH OR DIAMETER
Z	20.00	SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
MAIN	.51	1.37	3.00	8680.31	234.00	7.60	8.21

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.51	1.37	3.00	8680.31	234.00	7.60
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .6891E+03 EXCESS= .0000E+00 OUTFLOW= .6895E+03 BASIN STORAGE= .9283E-02 PERCENT ERROR= -.1

JP

UNIT HYDROGRAPH
 37 END-OF-PERIOD ORDINATES

30.	91.	176.	303.	435.	528.	563.	563.	528.	473.
405.	318.	248.	199.	159.	131.	106.	83.	68.	55.
44.	35.	28.	23.	19.	15.	12.	10.	8.	6.
5.	4.	4.	3.	2.	1.	0.			

HYDROGRAPH AT STATION SB10

TOTAL RAINFALL = 12.90, TOTAL LOSS = 5.30, TOTAL EXCESS = 7.60

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 3043.	3.55	(CFS) 360.	217.	217.	217.
		(INCHES) 7.600	7.600	7.600	7.600
		(AC-FT) 178.	178.	178.	178.

CUMULATIVE AREA = .44 SQ MI

131 KK *****
 * CP6 *
 * *

COMBINE HYDROGRAPHS FROM CP5, SB10, SB9

133 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP6

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 23427.	4.00	(CFS) 5101.	3077.	3077.	3077.
		(INCHES) 7.601	7.602	7.602	7.602
		(AC-FT) 2530.	2530.	2530.	2530.

CUMULATIVE AREA = 6.24 SQ MI

8/20

 *
 134 KK * CP6CP7 *
 *

ROUTE HYDROGRAPH FROM CP6 TO CP7

HYDROGRAPH ROUTING DATA

136 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 2100. CHANNEL LENGTH
 S .0200 SLOPE
 N .090 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 300.00 BOTTOM WIDTH OR DIAMETER
 Z 100.00 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.16	1.42	3.00	525.00	23431.39	243.00	7.60	6.01

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.16	1.42	3.00		23431.39	243.00	7.60	
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .2530E+04 EXCESS= .0000E+00 OUTFLOW= .2530E+04 BASIN STORAGE= .9920E-02 PERCENT ERROR= .0

HYDROGRAPH AT STATION CP6CP7

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR	72-HR	9.95-HR
+ 23431.	4.05	5102. (INCHES) (AC-FT)	3077. 7.602 2530.	3077. 7.603 2530.	3077. 7.603 2530.
CUMULATIVE AREA =		6.24 SQ MI			

JP

 * SB11 *

SCS RUNOFF COMPUTATION FOR SB11

SUBBASIN RUNOFF DATA

139 BA SUBBASIN CHARACTERISTICS
 TAREA .46 SUBBASIN AREA

PRECIPITATION DATA

93 PB STORM 12.90 BASIN TOTAL PRECIPITATION

94 PI INCREMENTAL PRECIPITATION PATTERN

.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
1.10	1.10	1.10	1.10	1.10	.36	.36	.36	.36	.36	.36
.18	.18	.18	.18	.18	.16	.16	.16	.16	.16	.16
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

74 LU UNIFORM LOSS RATE
 STRTL 1.00 INITIAL LOSS
 CNSTL 1.50 UNIFORM LOSS RATE
 RTIMP .00 PERCENT IMPERVIOUS AREA

140 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .40 LAG

UNIT HYDROGRAPH
 42 END-OF-PERIOD ORDINATES

22.	69.	133.	221.	333.	432.	493.	520.	520.	493.
452.	402.	337.	268.	217.	178.	146.	124.	103.	84.
69.	57.	48.	39.	32.	26.	22.	18.	15.	12.
10.	8.	7.	6.	5.	4.	4.	3.	2.	2.
1.	0.								

HYDROGRAPH AT STATION SB11

TOTAL RAINFALL = 12.90, TOTAL LOSS = 5.30, TOTAL EXCESS = 7.60

800

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	9.95-HR
2924.	3.60	(CFS)	376.	227.	227.	227.
		(INCHES)	7.600	7.600	7.600	7.600
		(AC-FT)	186.	186.	186.	186.

CUMULATIVE AREA = .46 SQ MI

141 KK

 * CP7 *

COMBINE HYDROGRAPHS FROM CP6, SB11

143 HC
 HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP7

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	9.95-HR
24733.	4.05	(CFS)	5477.	3304.	3304.	3304.
		(INCHES)	7.601	7.603	7.603	7.603
		(AC-FT)	2716.	2717.	2717.	2717.

CUMULATIVE AREA = 6.70 SQ MI

144 KK

 * CP7CP8 *

ROUTE HYDROGRAPH FROM CP7 TO CP8

HYDROGRAPH ROUTING DATA

880

146 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 2000. CHANNEL LENGTH
 S .0200 SLOPE
 N .090 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 30.00 BOTTOM WIDTH OR DIAMETER
 Z 40.00 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.38	1.35	3.00	666.67	24724.83	246.00	7.60	7.63

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.38	1.35	3.00		24724.83	246.00	7.60	
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .2717E+04 EXCESS= .0000E+00 OUTFLOW= .2717E+04 BASIN STORAGE= .1205E-01 PERCENT ERROR= .0

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HYDROGRAPH AT STATION CP7CP8

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 24725.	4.10	(CFS) 5477.	3304.	3304.	3304.
		(INCHES) 7.601	7.603	7.603	7.603
		(AC-FT) 2716.	2717.	2717.	2717.

CUMULATIVE AREA = 6.70 SQ MI

147 KK *****
 * SB12 *
 * *

SCS RUNOFF COMPUTATION FOR SB12

SUBBASIN RUNOFF DATA

820

149 BA SUBBASIN CHARACTERISTICS
 TAREA .15 SUBBASIN AREA
 PRECIPITATION DATA

93 PB STORM 12.90 BASIN TOTAL PRECIPITATION

94 PI INCREMENTAL PRECIPITATION PATTERN

.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.03	.03	.03	.03	.03	.03	.03	.03	.03	.03	.03
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
.08	.08	.08	.08	.08	.08	.08	.08	.08	.08	.08
1.10	1.10	1.10	1.10	1.10	.36	.36	.36	.36	.36	.36
.18	.18	.18	.18	.18	.16	.16	.16	.16	.16	.16
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.04	.04	.04	.04	.04	.04	.04	.04	.04	.04	.04
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02

74 LU UNIFORM LOSS RATE
 STRTL 1.00 INITIAL LOSS
 CNSTL 1.50 UNIFORM LOSS RATE
 RTIMP .00 PERCENT IMPERVIOUS AREA

150 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .24 LAG

UNIT HYDROGRAPH
 26 END-OF-PERIOD ORDINATES

25.	77.	163.	241.	272.	266.	231.	183.	126.	92.
69.	51.	37.	28.	20.	15.	11.	8.	6.	4.
3.	3.	2.	1.	1.	0.				

*** **

HYDROGRAPH AT STATION SB12

TOTAL RAINFALL = 12.90, TOTAL LOSS = 5.30, TOTAL EXCESS = 7.60

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
1300.	3.40	123.	74.	74.	74.
		(INCHES) 7.600	7.600	7.600	7.600
		(AC-FT) 61.	61.	61.	61.

CUMULATIVE AREA = .15 SQ MI

JP

 * CP8 *
 *

COMBINE HYDROGRAPHS FROM CP7, SB12

153 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

PEAK FLOW + (CFS)	TIME (HR)	HYDROGRAPH AT STATION CP8			
		6-HR	24-HR	72-HR	9.95-HR
+ 24935.	4.10	(CFS) 5599.	3378.	3378.	3378.
		(INCHES) 7.600	7.603	7.603	7.603
		(AC-FT) 2777.	2778.	2778.	2778.
CUMULATIVE AREA =		6.85 SQ MI			

 * CP8CP9 *
 *

ROUTE HYDROGRAPH FROM CP8 TO CP9

HYDROGRAPH ROUTING DATA

156 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	1700.	CHANNEL LENGTH
S	.0200	SLOPE
N	.090	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	30.00	BOTTOM WIDTH OR DIAMETER
Z	30.00	SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)

JPD

MAIN .40 1.36 3.00 850.00 24919.09 249.00 7.60 8.32

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .40 1.36 3.00 24919.09 249.00 7.60

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2778E+04 EXCESS= .0000E+00 OUTFLOW= .2778E+04 BASIN STORAGE= .2106E-01 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION CP8CP9

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 24919.	4.15	(CFS) 5600.	3378.	3378.	3378.
		(INCHES) 7.600	7.603	7.603	7.603
		(AC-FT) 2777.	2778.	2778.	2778.
CUMULATIVE AREA =		6.85 SQ MI			

157 KK

 * CP9 *
 * *

COMBINE HYDROGRAPHS FROM CP4, SB13, CP8

159 HC

HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CP9

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	9.95-HR
+ 50219.	4.15	(CFS) 10769.	6499.	6499.	6499.
		(INCHES) 7.884	7.890	7.890	7.890
		(AC-FT) 5340.	5344.	5344.	5344.
CUMULATIVE AREA =		12.70 SQ MI			

JPD

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+									
	HYDROGRAPH AT								
+		SB1	4097.	3.85	721.	435.	435.	.83	
	ROUTED TO								
+		SB1CP1	4093.	3.90	721.	435.	435.	.83	
	HYDROGRAPH AT								
+		SB2	2881.	3.60	365.	220.	220.	.42	
	2 COMBINED AT								
+		CP1	6164.	3.75	1086.	655.	655.	1.25	
	ROUTED TO								
+		CP1CP2	6159.	3.80	1086.	655.	655.	1.25	
	HYDROGRAPH AT								
+		SB3	7148.	3.95	1390.	838.	838.	1.60	
	HYDROGRAPH AT								
+		SB4	5782.	3.90	1042.	629.	629.	1.20	
	3 COMBINED AT								
+		CP2	18927.	3.90	3519.	2122.	2122.	4.05	
	ROUTED TO								
+		CP2CP3	18906.	4.00	3520.	2122.	2122.	4.05	
	HYDROGRAPH AT								
+		AGING	3436.	3.40	486.	297.	297.	.46	
	2 COMBINED AT								
+		CP3	20138.	3.95	4006.	2419.	2419.	4.51	
	ROUTED TO								
+		CP3CP4	20106.	4.05	4006.	2419.	2419.	4.51	
	HYDROGRAPH AT								
+		SB5	1925.	3.85	339.	204.	204.	.39	
	HYDROGRAPH AT								
+		SB6	3290.	4.00	660.	398.	398.	.76	
	3 COMBINED AT								
+		CP4	25090.	4.05	5005.	3022.	3022.	5.66	
	ROUTED TO								
+		CP4CP9	25047.	4.10	5006.	3022.	3022.	5.66	

+	HYDROGRAPH AT	SB13	1555.	3.45	165.	100.	100.	.19
+	HYDROGRAPH AT	SB7	10053.	4.15	2370.	1429.	1429.	2.90
+	ROUTED TO	SB7CP5	10052.	4.25	2371.	1430.	1430.	2.90
+	HYDROGRAPH AT	SB8	5757.	3.80	981.	592.	592.	1.20
+	2 COMBINED AT	CP5	14235.	4.05	3351.	2021.	2021.	4.10
+	ROUTED TO	CP5CP6	14234.	4.10	3352.	2021.	2021.	4.10
+	HYDROGRAPH AT	SB9	8684.	3.75	1390.	838.	838.	1.70
+	ROUTED TO	SB9CP6	8680.	3.90	1390.	838.	838.	1.70
+	HYDROGRAPH AT	SB10	3043.	3.55	360.	217.	217.	.44
+	3 COMBINED AT	CP6	23427.	4.00	5101.	3077.	3077.	6.24
+	ROUTED TO	CP6CP7	23431.	4.05	5102.	3077.	3077.	6.24
+	HYDROGRAPH AT	SB11	2924.	3.60	376.	227.	227.	.46
+	2 COMBINED AT	CP7	24733.	4.05	5477.	3304.	3304.	6.70
+	ROUTED TO	CP7CP8	24725.	4.10	5477.	3304.	3304.	6.70
+	HYDROGRAPH AT	SB12	1300.	3.40	123.	74.	74.	.15
+	2 COMBINED AT	CP8	24935.	4.10	5599.	3378.	3378.	6.85
+	ROUTED TO	CP8CP9	24919.	4.15	5600.	3378.	3378.	6.85
+	3 COMBINED AT	CP9	50219.	4.15	10769.	6499.	6499.	12.70
1								

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)
 INTERPOLATED TO
 COMPUTATION INTERVAL

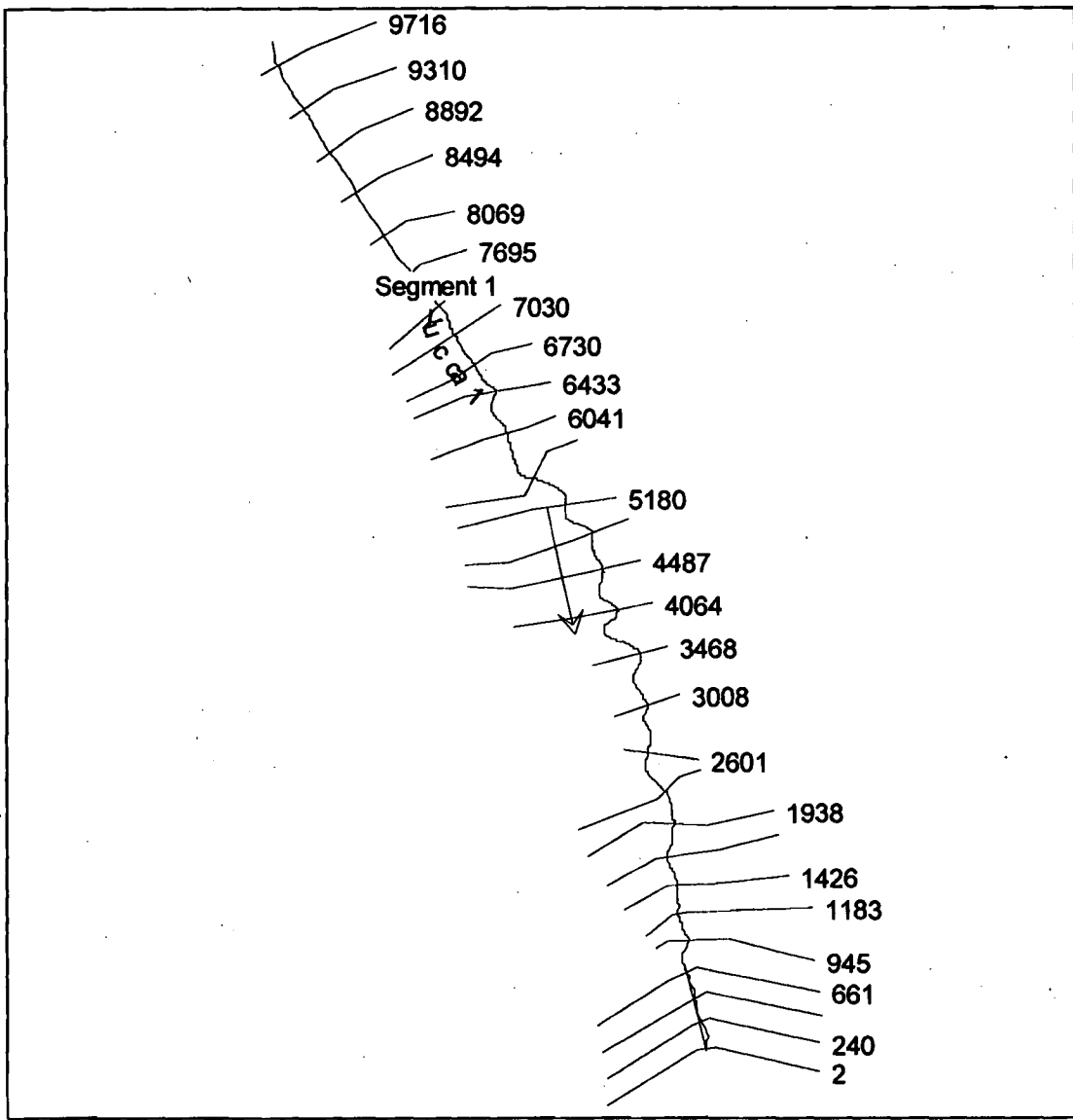
dat

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	
SB1CP1	MANE	3.00	4093.01	234.00	8.08	3.00	4093.01	234.00	8.08	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3575E+03 EXCESS= .0000E+00 OUTFLOW= .3576E+03 BASIN STORAGE= .1048E-01 PERCENT ERROR= .0										
CP1CP2	MANE	3.00	6159.40	228.00	8.08	3.00	6159.40	228.00	8.08	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5385E+03 EXCESS= .0000E+00 OUTFLOW= .5387E+03 BASIN STORAGE= .9970E-02 PERCENT ERROR= .0										
CP2CP3	MANE	3.00	18905.50	240.00	8.08	3.00	18905.50	240.00	8.08	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1745E+04 EXCESS= .0000E+00 OUTFLOW= .1745E+04 BASIN STORAGE= .1214E-01 PERCENT ERROR= .0										
AGING	MANE	.27	3441.74	202.75	9.94	3.00	3436.19	204.00	9.94	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2461E+03 OUTFLOW= .2439E+03 BASIN STORAGE= .1963E+01 PERCENT ERROR= .1										
CP3CP4	MANE	3.00	20106.10	243.00	8.27	3.00	20106.10	243.00	8.27	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1989E+04 EXCESS= .0000E+00 OUTFLOW= .1989E+04 BASIN STORAGE= .7397E+00 PERCENT ERROR= .0										
CP4CP9	MANE	3.00	25046.78	246.00	8.23	3.00	25046.78	246.00	8.23	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2485E+04 EXCESS= .0000E+00 OUTFLOW= .2485E+04 BASIN STORAGE= .6271E+00 PERCENT ERROR= .0										
SB7CP5	MANE	3.00	10052.46	255.00	7.60	3.00	10052.46	255.00	7.60	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1175E+04 EXCESS= .0000E+00 OUTFLOW= .1176E+04 BASIN STORAGE= .5540E-02 PERCENT ERROR= .0										
CP5CP6	MANE	3.00	14233.66	246.00	7.60	3.00	14233.66	246.00	7.60	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1662E+04 EXCESS= .0000E+00 OUTFLOW= .1662E+04 BASIN STORAGE= .2786E-02 PERCENT ERROR= .0										
SB9CP6	MANE	3.00	8680.31	234.00	7.60	3.00	8680.31	234.00	7.60	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6891E+03 EXCESS= .0000E+00 OUTFLOW= .6895E+03 BASIN STORAGE= .9283E-02 PERCENT ERROR= -.1										

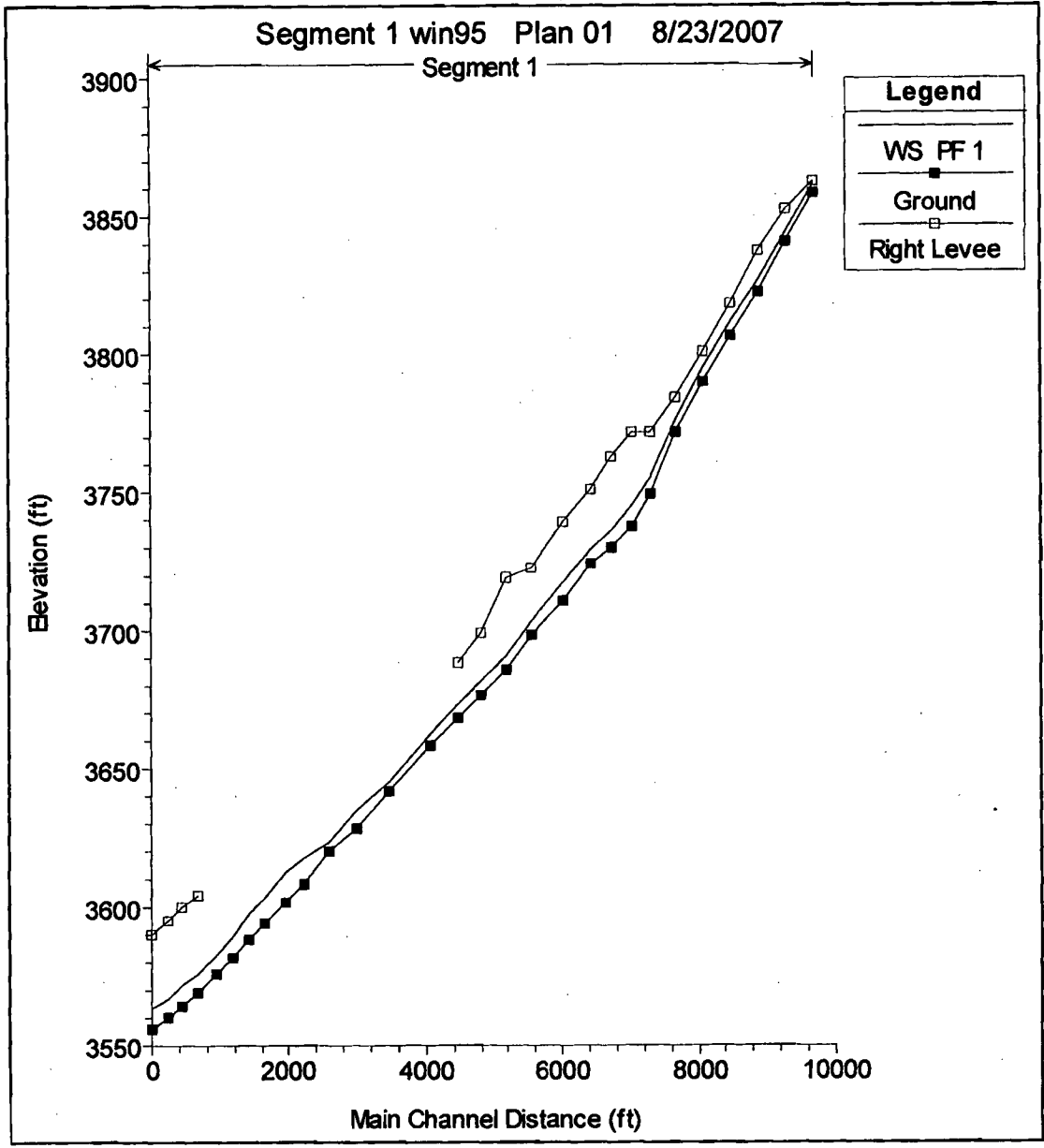
CP6CP7	MANE	3.00	23431.39	243.00	7.60	3.00	23431.39	243.00	7.60
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2530E+04 EXCESS= .0000E+00 OUTFLOW= .2530E+04 BASIN STORAGE= .9920E-02 PERCENT ERROR= .0									
CP7CP8	MANE	3.00	24724.83	246.00	7.60	3.00	24724.83	246.00	7.60
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2717E+04 EXCESS= .0000E+00 OUTFLOW= .2717E+04 BASIN STORAGE= .1205E-01 PERCENT ERROR= .0									
CP8CP9	MANE	3.00	24919.09	249.00	7.60	3.00	24919.09	249.00	7.60
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2778E+04 EXCESS= .0000E+00 OUTFLOW= .2778E+04 BASIN STORAGE= .2106E-01 PERCENT ERROR= .0									

*** NORMAL END OF HEC-1 ***

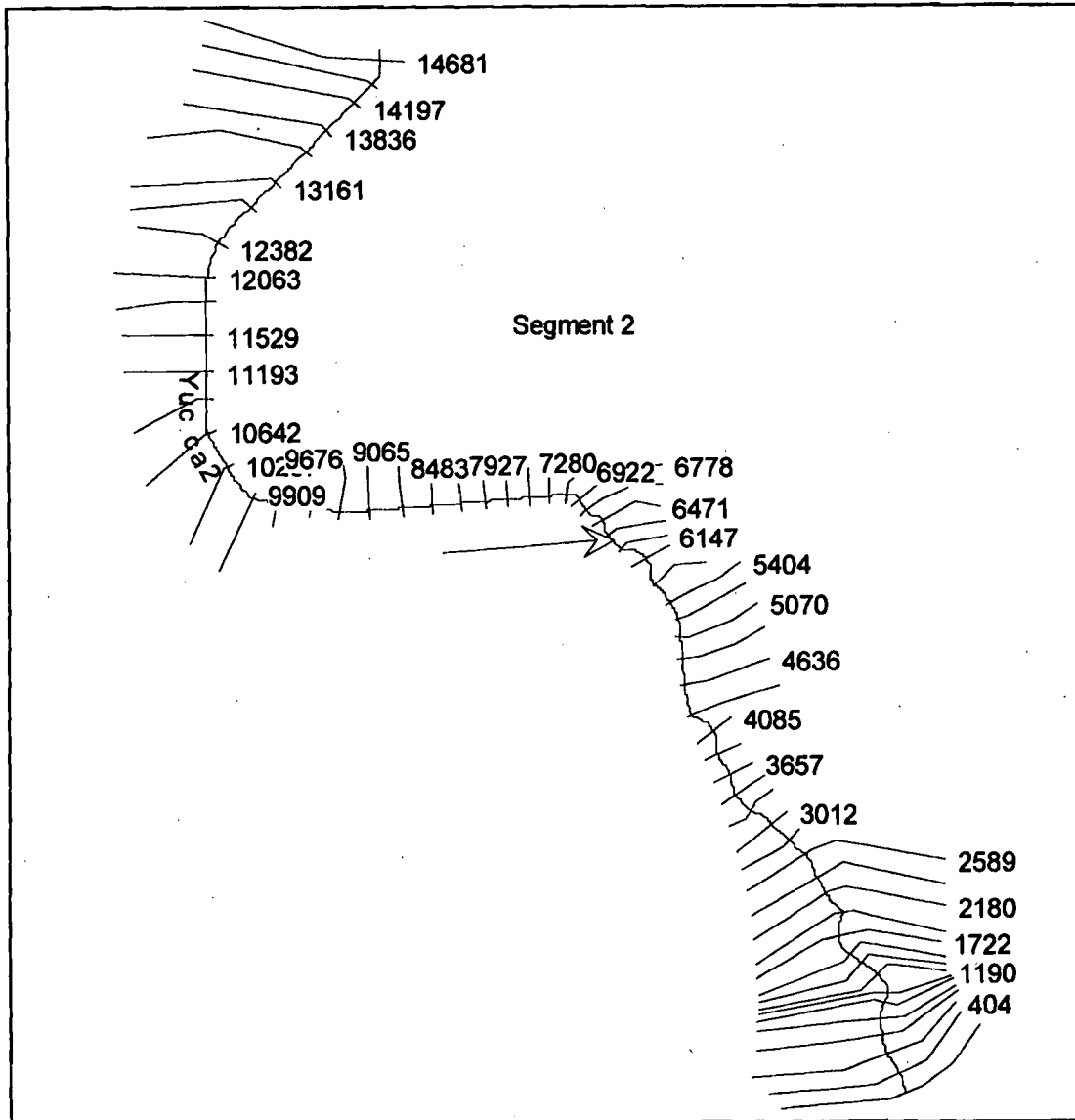
HEC-RAS Schematic for Segment 1



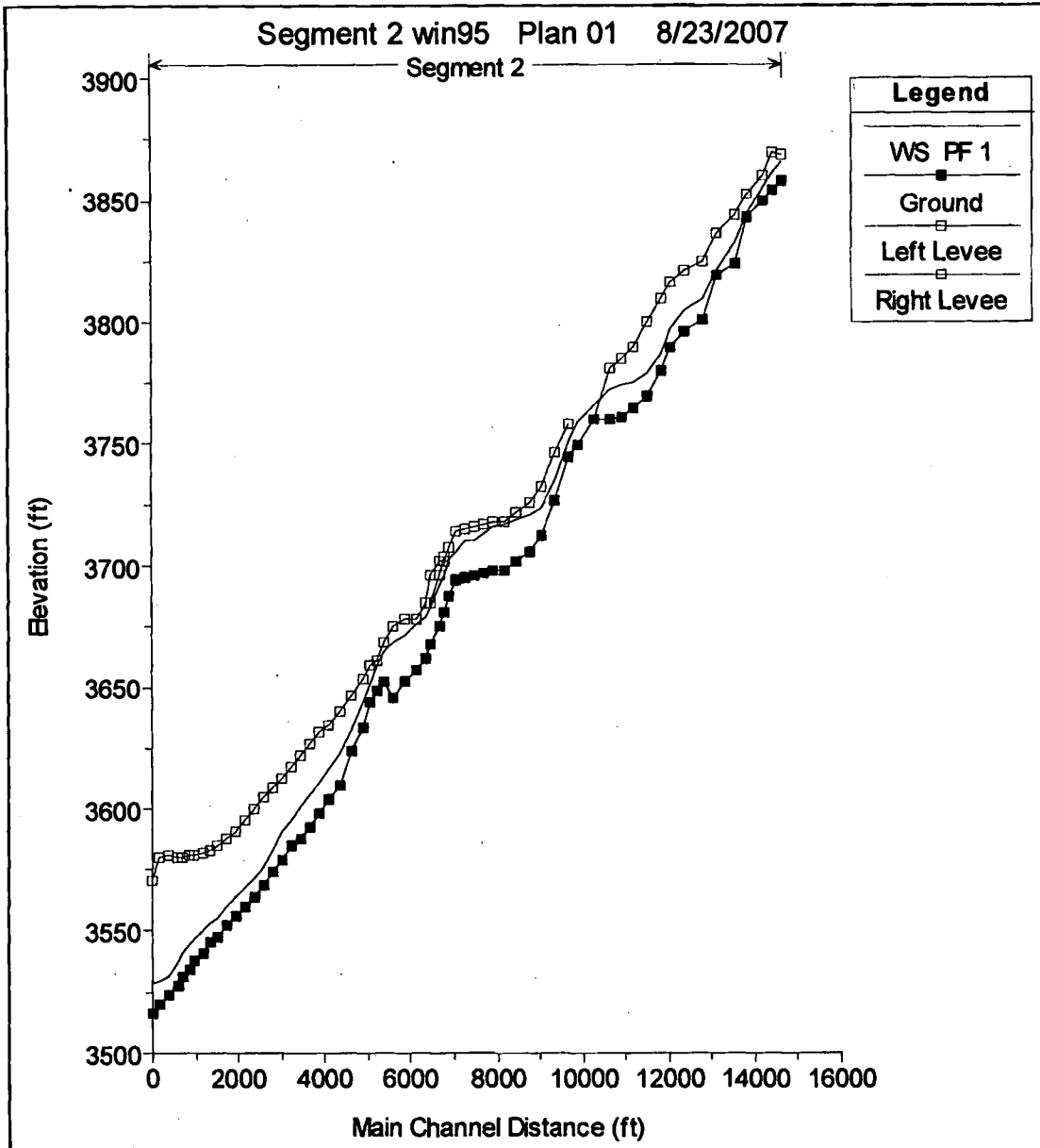
Water Surface Profile of Probable Maximum Flood for Segment 1



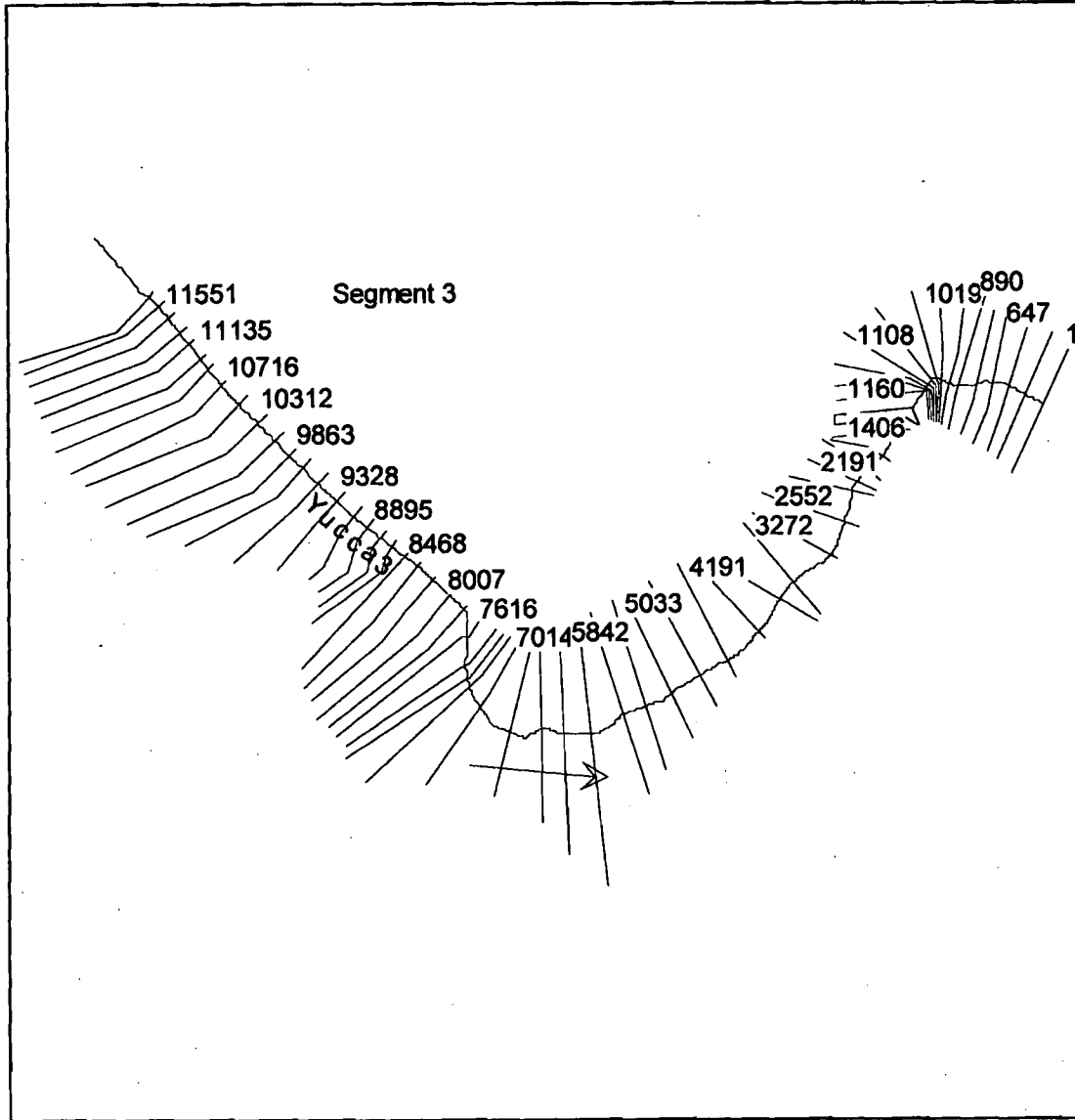
HEC-RAS Schematic for Segment 2



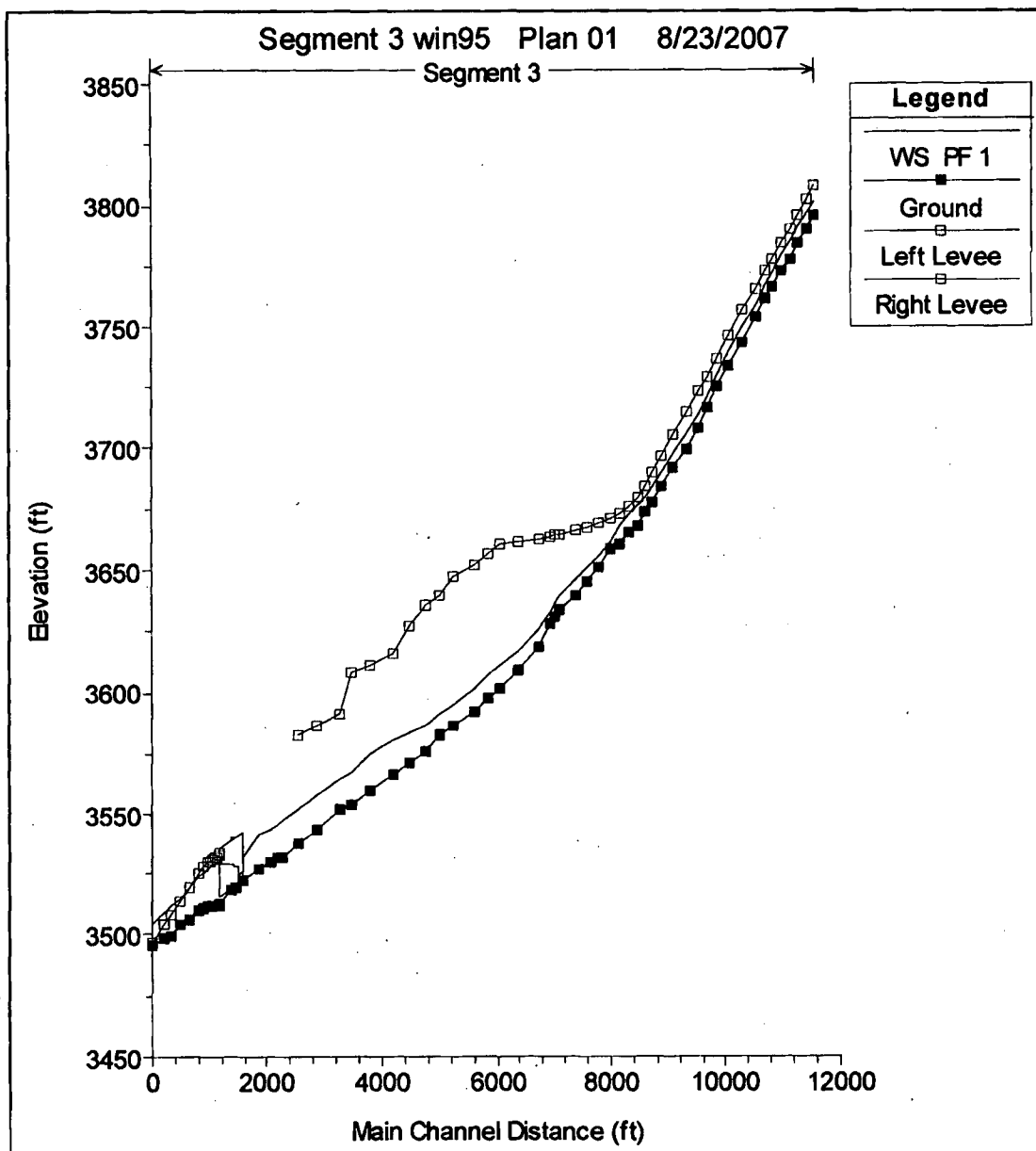
Water Surface Profile of Probable Maximum Flood for Segment 2



HEC-RAS Schematic for Segment 3



Water Surface Profile of Probable Maximum Flood for Segment 3



Note: Left levee elevations have changed from those shown between HEC-RAS stations 8468 and 2552 (North Portal Loop Road West stations 531+00 and 572+00). The revised road profile is shown in Attachment A. The revised values for levee freeboard are included in Table 7-4: Flood Inundation Results for Segment 3.

Attachment E

PMP Calculations for South Portal

000-CDC-MGR0-00100-000-00A *LT*

1 of 4

The procedures presented in HMR 49 (Ref. 2.2.16) were used to calculate the PMP in the vicinity of the South Portal. The calculations on the following pages (performed using United States customary units) show that the 6-hour duration local storm PMP of 12.9 inches is more severe than the largest 6-hour general storm of 5.8 inches, which was calculated to occur during the month of September. The local storm PMP hyetograph has been included in this attachment.

Table 6.1.--General-storm PMP computations for the Colorado River and Great basin

Step	Month <u>September</u>						
	6	12	18	24	48	72	
Drainage <u>Midway Valley - South Portal Area</u>	Area <u>6.5</u> mi ² (km ²)						
Latitude <u>36° 51'</u> , Longitude <u>116° 27'</u> of basin center							
A. Convergence PMP							
1. Drainage average value from one of figures 2.5 to 2.16	<u>10.8 in. (mm)</u>						
2. Reduction for barrier-elevation [fig. 2.18]	<u>65 %</u>						
3. Barrier-elevation reduced PMP [step 1 X step 2]	<u>7.0 in. (mm)</u>						
4. Durational variation [figs. 2.25 to 2.27 and table 2.7].	<u>68</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>%</u>
5. Convergence PMP for indicated durations [steps 3 X 4]	<u>4.8</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>in. (mm)</u>
6. Incremental 10 mi ² (26 km ²) PMP [successive subtraction in step 5]	<u>4.8</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>in. (mm)</u>
7. Areal reduction [select from figs. 2.28 and 2.29]	<u>100</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>%</u>
8. Areal reduction PMP [step 6 X step 7]	<u>4.8</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>in. (mm)</u>
9. Drainage average PMP [accumulated values of step 8]	<u>4.8</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>in. (mm)</u>
B. Orographic PMP							
1. Drainage average orographic index from figure 3.11a to d.	<u>3.0 in. (mm)</u>						
2. Areal reduction [figure 3.20]	<u>100 %</u>						
3. Adjustment for month [one of figs. 3.12 to 3.17]	<u>100 %</u>						
4. Areal and seasonally adjusted PMP [steps 1 X 2 X 3]	<u>3.0 in. (mm)</u>						
5. Durational variation [table 3.6]	<u>32</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>%</u>
6. Orographic PMP for given durations [steps 4 X 5]	<u>1.0</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>in. (mm)</u>
C. Total PMP							
1. Add steps A9 and B6	<u>5.8</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>NA</u>	<u>in. (mm)</u>
2. PMP for other durations from smooth curve fitted to plot of computed data.							
3. Comparison with local-storm PMP (see sec. 6.3).							

Table 6.3A.--Local-storm PMP computation, Colorado River, Great Basin and California drainages. For drainage average depth PMP. Go to table 6.3B if areal variation is required.

Drainage Midway Valley - South Portal Area Area 6.5 mi^2 (km^2)
 Latitude 36° 51' Longitude 116° 27' Minimum Elevation 3520 ft (m)

Steps correspond to those in sec. 6.3A.

1. Average 1-hr 1-mi^2 (2.6-km^2) PMP for drainage [fig. 4.5]. 10.3 in. (mm)
2. a. Reduction for elevation. [No adjustment for elevations up to 5,000 feet (1,524 m): 5% decrease per 1,000 feet (305 m) above 5,000 feet (1,524 m)]. 100 %
 b. Multiply step 1 by step 2a. 10.3 in. (mm)
3. Average 6/1-hr ratio for drainage [fig. 4.7]. 1.36
4. Durational variation for 6/1-hr ratio of step 3 [table 4.4].

	Duration (hr)										%
	1/4	1/2	3/4	1	2	3	4	5	6		
	<u>67</u>	<u>85</u>	<u>94</u>	<u>100</u>	<u>116</u>	<u>124</u>	<u>129</u>	<u>133</u>	<u>136</u>		%
5. 1-mi^2 (2.6-km^2) PMP for indicated durations [step 2b X step 4].

	<u>6.9</u>	<u>8.8</u>	<u>9.7</u>	<u>10.3</u>	<u>11.9</u>	<u>12.8</u>	<u>13.3</u>	<u>13.7</u>	<u>14.0</u>	in. (mm)
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6. Areal reduction [fig. 4.9].

	<u>80</u>	<u>83</u>	<u>85</u>	<u>87</u>	<u>88</u>	<u>89</u>	<u>90</u>	<u>91</u>	<u>92</u>	%
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7. Areal reduced PMP [steps 5 X 6].

	<u>5.5</u>	<u>7.3</u>	<u>8.2</u>	<u>9.0</u>	<u>10.5</u>	<u>11.4</u>	<u>12.0</u>	<u>12.5</u>	<u>12.9</u>	in. (mm)
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8. Incremental PMP [successive subtraction in step 7].

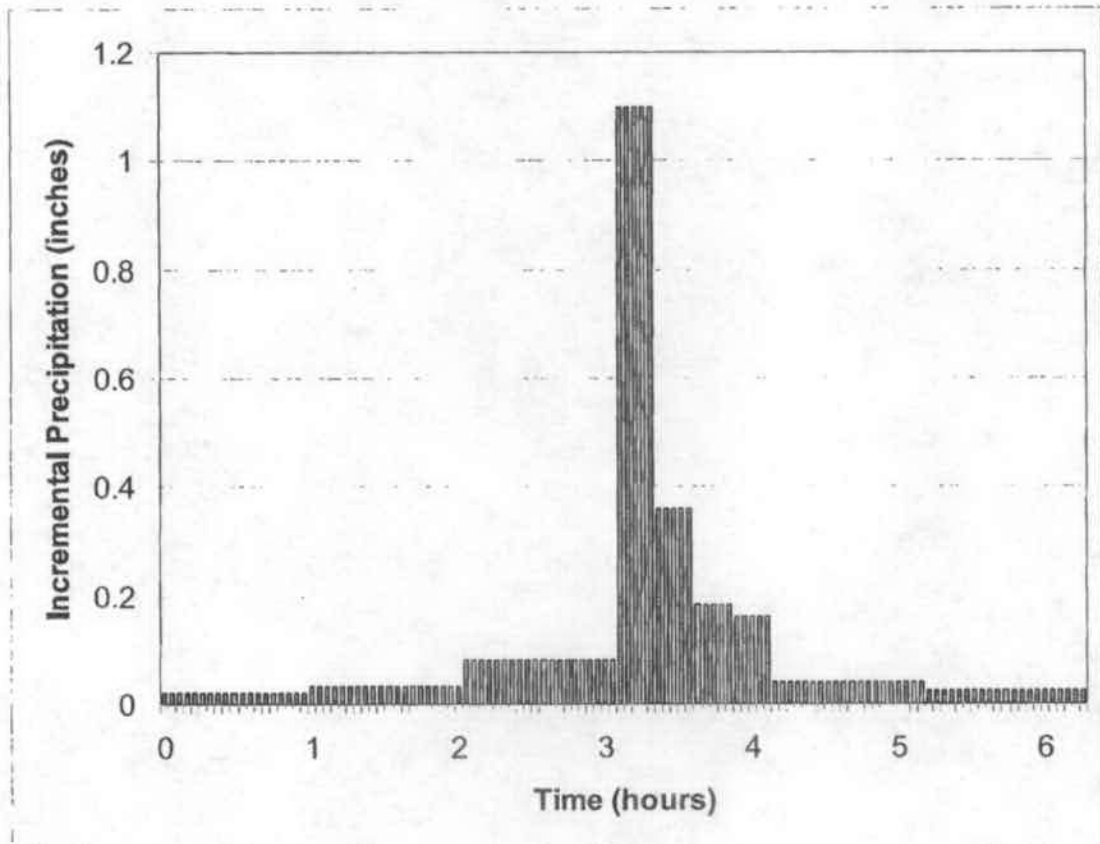
				<u>9.0</u>	<u>1.5</u>	<u>0.9</u>	<u>0.6</u>	<u>0.5</u>	<u>0.4</u>	in. (mm)
	<u>5.5</u>	<u>1.8</u>	<u>0.9</u>	<u>0.8</u>	} 15-min. increments					
9. Time sequence of incremental PMP according to:

Used EM 1110-2-1411 COE
 Method as in previous report
 (Ref. 2.2.6, p. 16)

Hourly increments [table 4.7]. 0.4 0.6 1.5 9.0 0.9 0.5 in. (mm)

Four largest 15-min. increments [table 4.8]. 5.5 1.8 0.9 0.8 in. (mm)

**PMP Hyetograph for the South Portal
(3-minute interval)**



SCHMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE NO.	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
12	SB1	
	V	
	V	
31	SB1CP1	
	.	
34	.	SB2
	.	.
38	CP1.....	
	V	
	V	
41	CP1CP2	
	.	
44	.	SB3
	.	.
48	.	SB4
	.	.
52	CP2.....	
	V	
	V	
55	CP2CP3	
	.	
58	.	AGING
	.	.
65	CP3.....	
	V	
	V	
68	CP3CP4	
	.	
71	.	SB5
	.	.
76	.	SB6
	.	.
80	CP4.....	

