## E907 Momentum Resolution Study Rajendran Raja 3-Sep-01

Method:-We have generated 1000 120GeV/c pp events using Pythia. For each track, two other tracks were generated the first with 1.1 times the track momentum and the other with 0.9 times the track momentum. These two tracks were used to find two values of the derivative  $dx_i/dp$  at each chamber, where  $x_i$  is the x co-ordinate in the i<sup>th</sup> chamber, and p the momentum of the parent track. The two values of  $dx_i/dp$  were averaged together to get the central  $dx_i/dp$  at the track. If we assume that all other track quantities are known and we are only determining the momentum resolution of the track, then the error matrix formula simplifies to

$$1/\sigma_p^2 = \Sigma_i (dx_i/dp)^2/\sigma_i^2$$

This enables one to determine the fractional momentum resolution  $\sigma_p / p$  as a function of momentum track by track. Multiple scattering is included, since Geant generates tracks in the presence of all interactions. (The special cases where the the two "differential tracks" tracks behave differently from the parent track due to Geant interactions and decay need careful treatment and has taken a significant amount of time.). The chamber resolutions  $\sigma_i$  are all taken to be 200 microns for this study. The momentum resolution thus obtained is clearly too optimistic, since it does not include the effects of the errors in the direction of the tracks. But this gives us an excellent way of studying the effect of chamber placement without smearing and fitting.

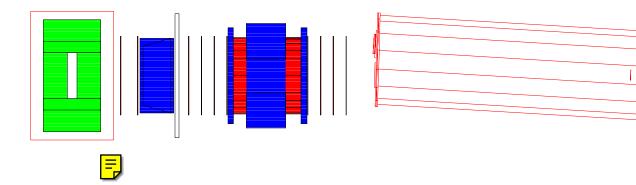
The chamber positions are given in the following table and illustrated in the following figure, which we include for completeness.

Geometry used:

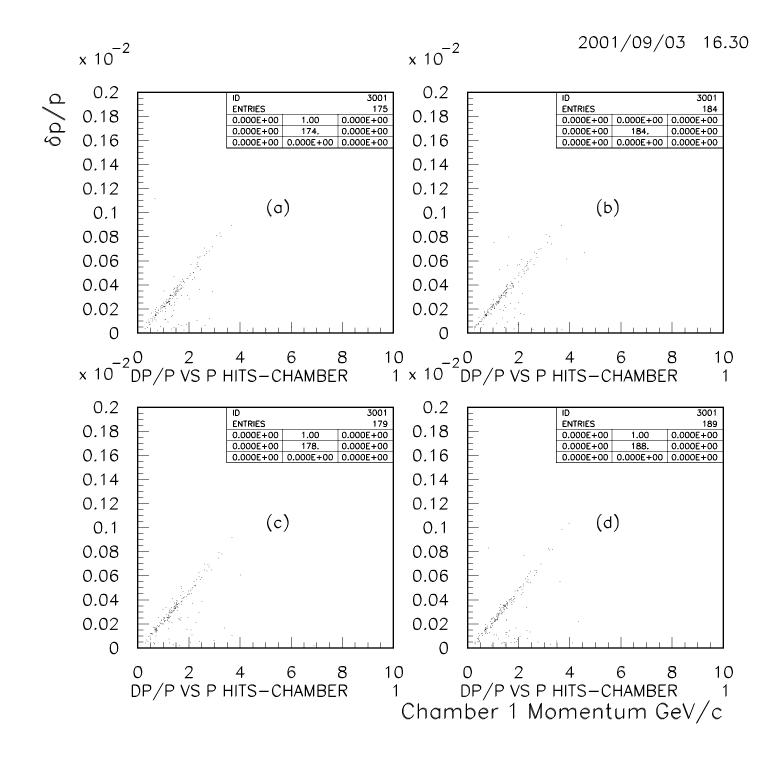
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The following table gives the positions of the detectors in E907 this simulation. The mother volume is called CAVE and is a tube. repect to the center of this tube in ContinuatersystEthe employed is axis along tube axis along the beam direction , y axis is vertic forming a right haondeinate system.
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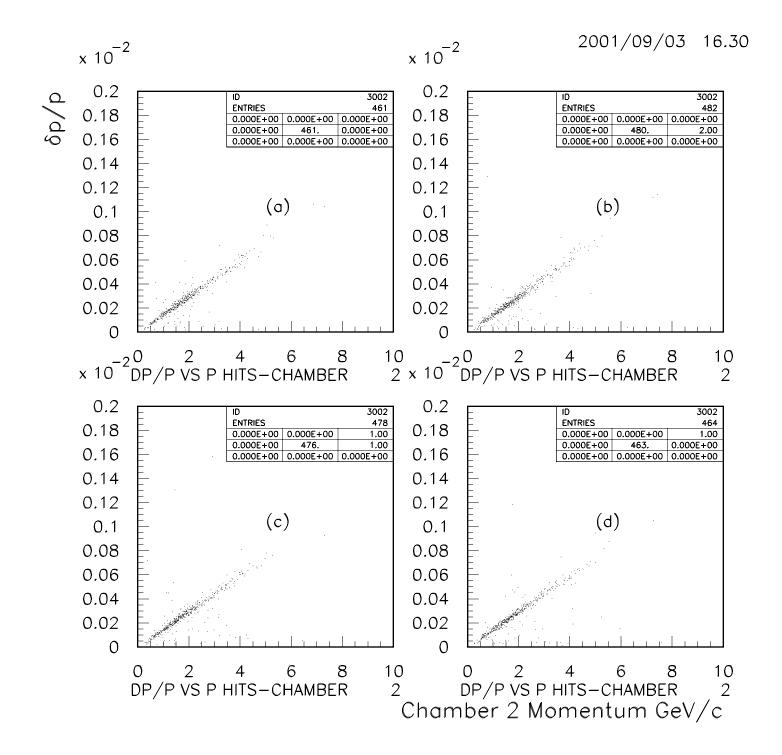
| Object            | Z position (cm)                |
|-------------------|--------------------------------|
| Target            | -843.5                         |
| Jolly Green Giant | -739.98                        |
| Rosy              | 12.998 vertical aperture=36" d |
| RICH              | 947.7                          |
| Chamber 1         | -552.9                         |
| Chamber 2         | -487.3                         |
| Chamber 3         | -290.5                         |
| Chamber 4         | -241.3                         |
| Chamber 5         | -192.1                         |
| Chamber 6         | -142.9                         |
| Chamber 7         | 168.7                          |
| Chamber 8         | 217.9                          |
| Chamber 9         | 267.1                          |
| Chamber 10        | 316.3                          |
| Chamber 11        | 1529.9                         |
| Chamber 12        | 1579.1                         |

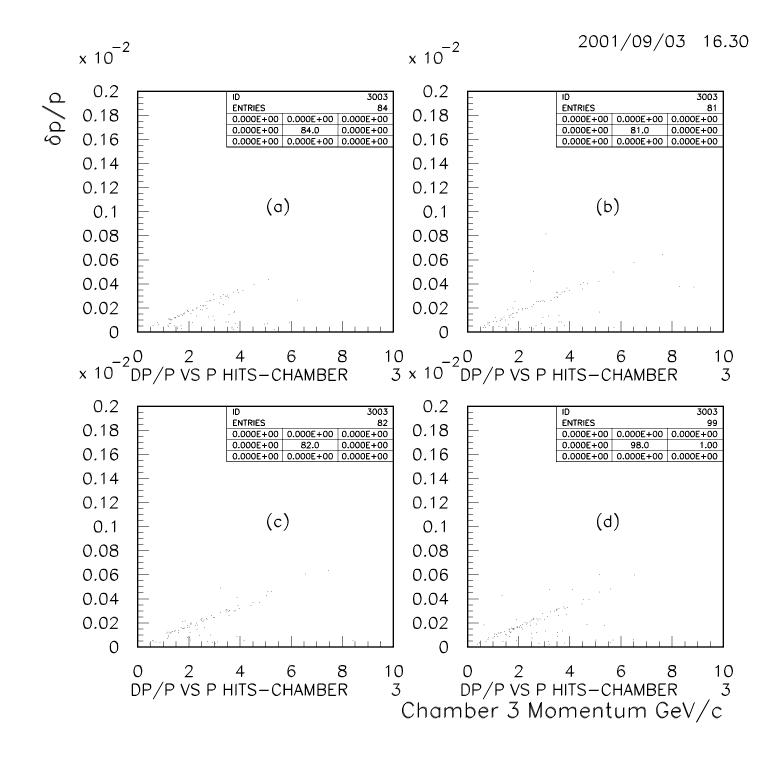
The following picture shows the experiment cut along a vertical  $x\!=\!0$ 

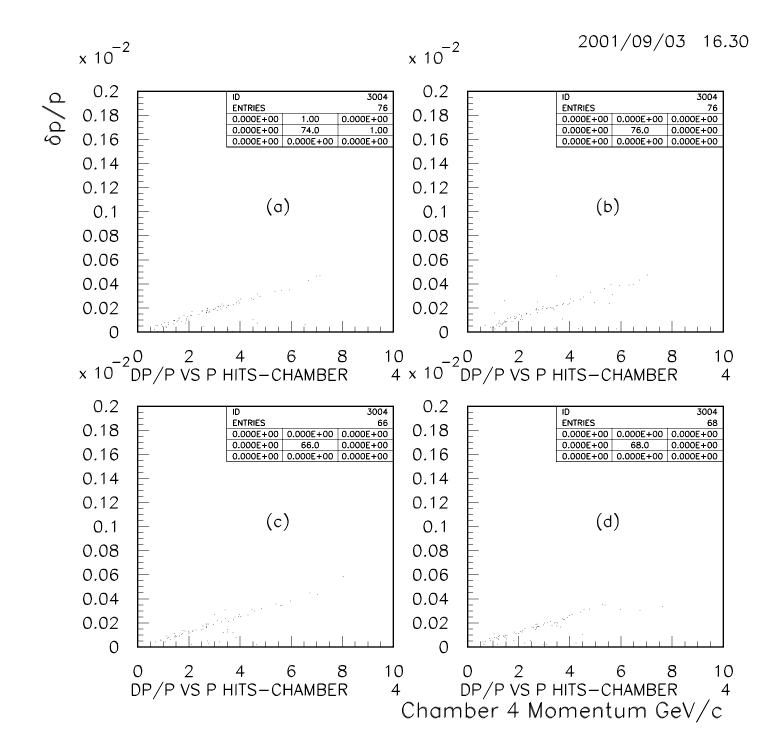


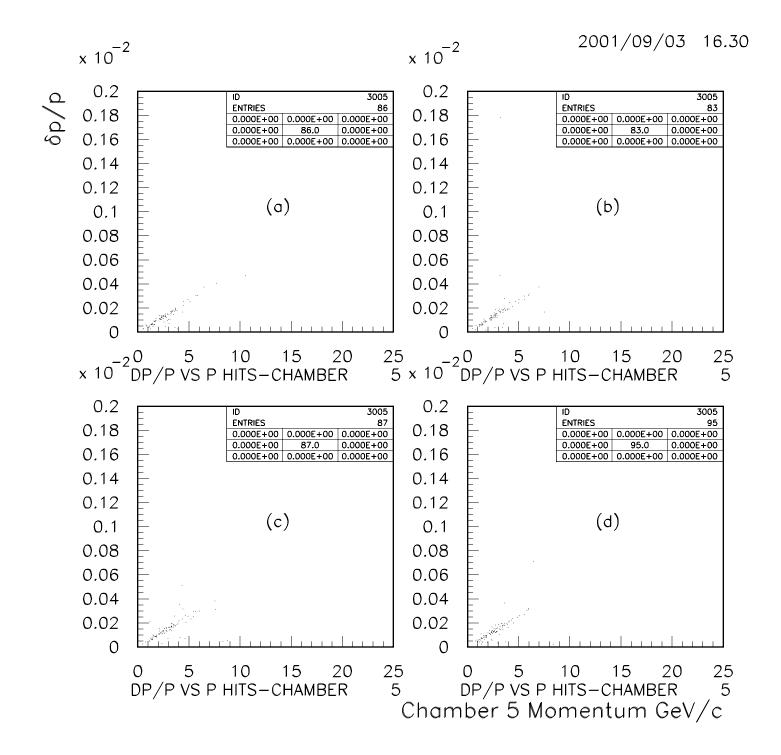
The following figures contain the fractional momentum resolution as a function of momentum for the 12 chambers. A track is plotted as being associated with a particular chamber if that is the last chamber hit by the track. The figures marked (a) are for ROSY field +1.2 Tesla, (b) for +0.6Tesla (c) for -0.6Tesla and (d) for -1.2Tesla. Clearly no difference is expected between the cases (a), (b),(c) and (d) for chambers upstream of ROSY, that is Chambers 1-6. It can be seen that the fractional resolution improves as more chambers come into play. TPC hits are included in all these plots. TPC is treated as 128 chambers in exactly the same way as the other chambers. The vertex z position of all tracks is constrained to smaller than -840cm to avoid particles that start in the middle of the TPC from strange particle decays.

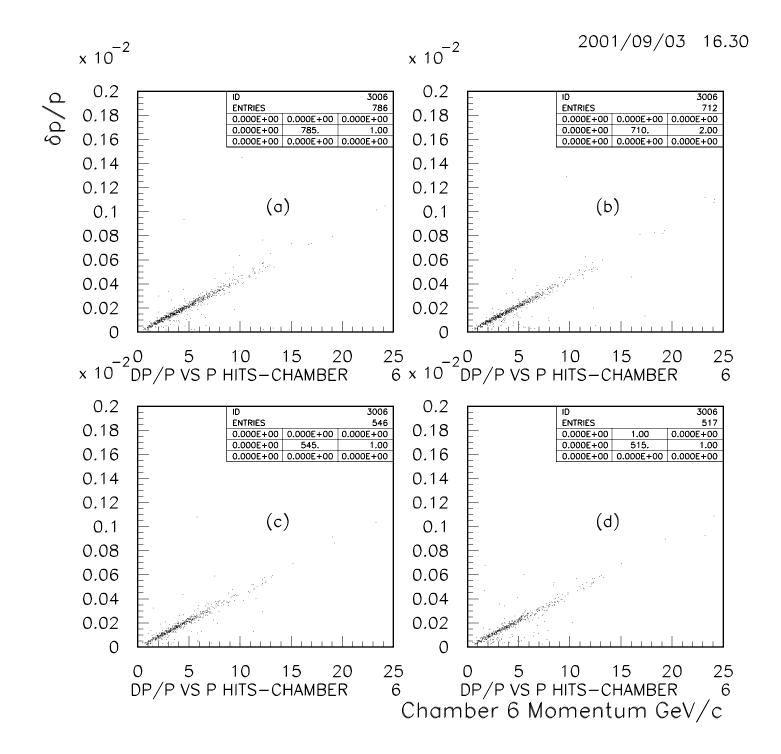


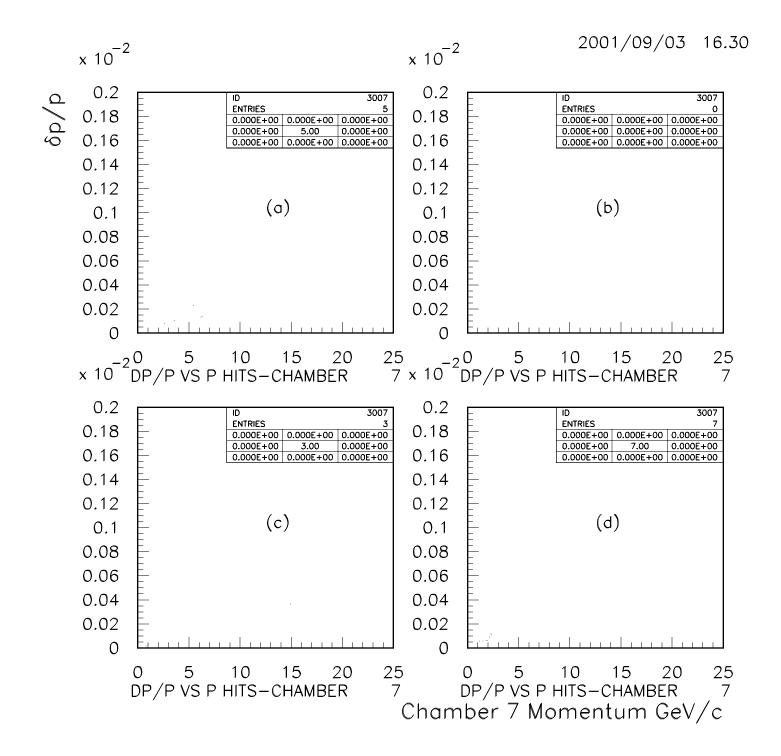


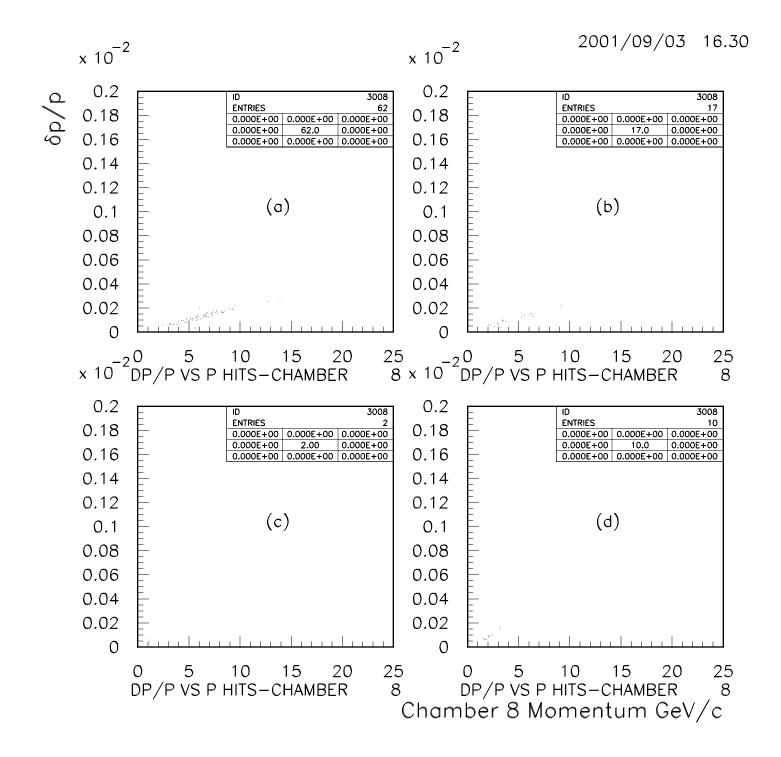


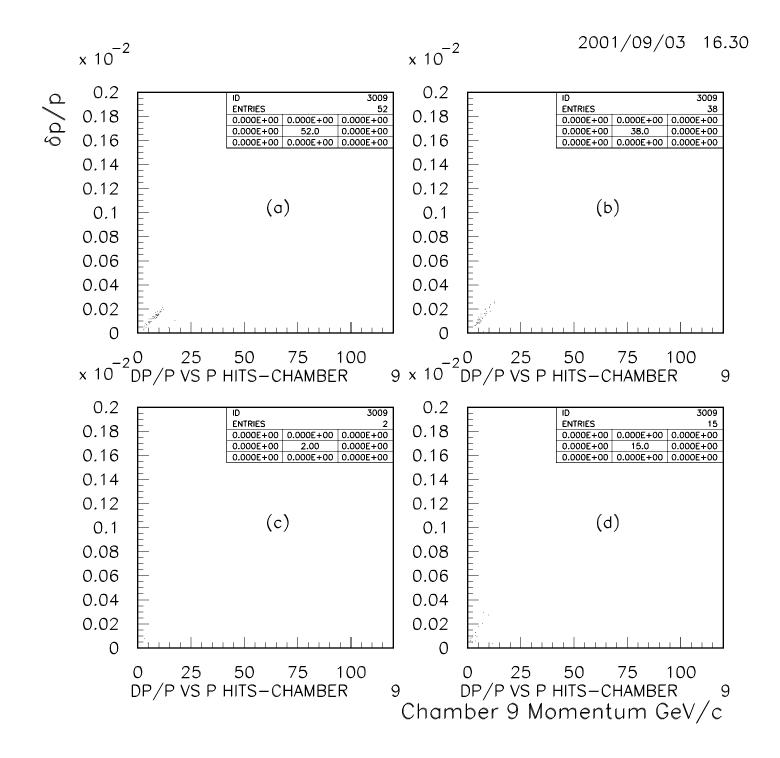


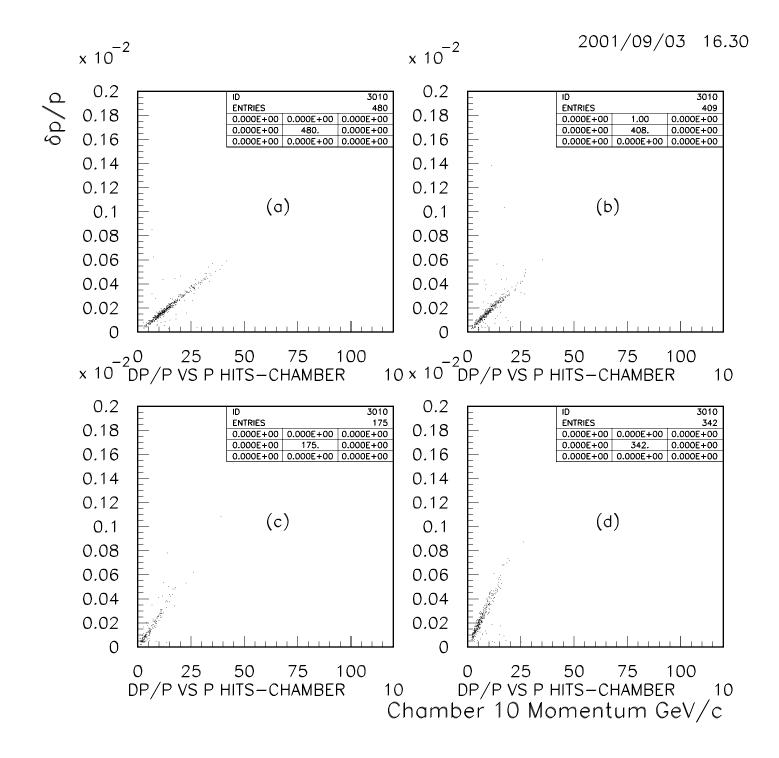


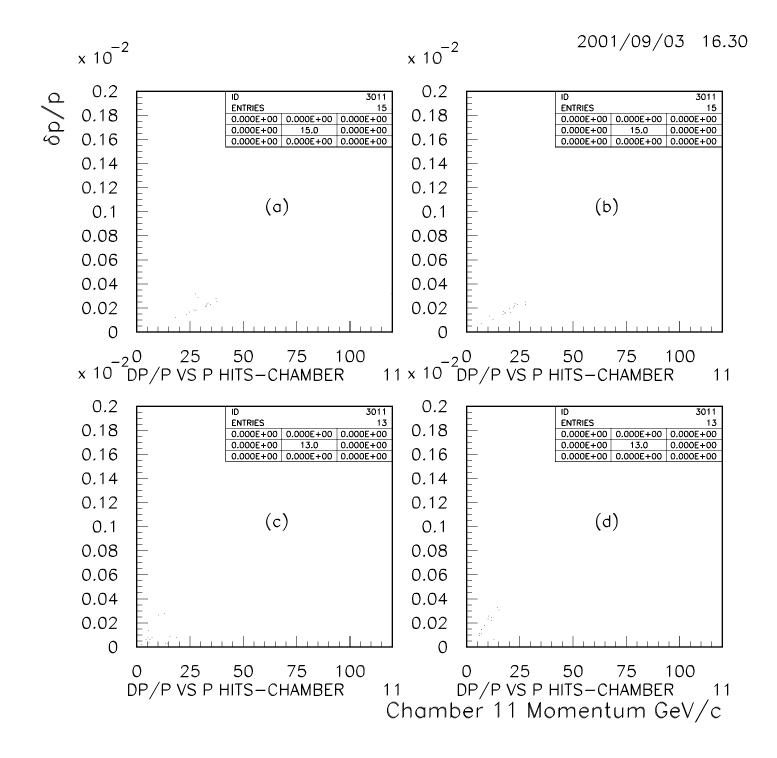


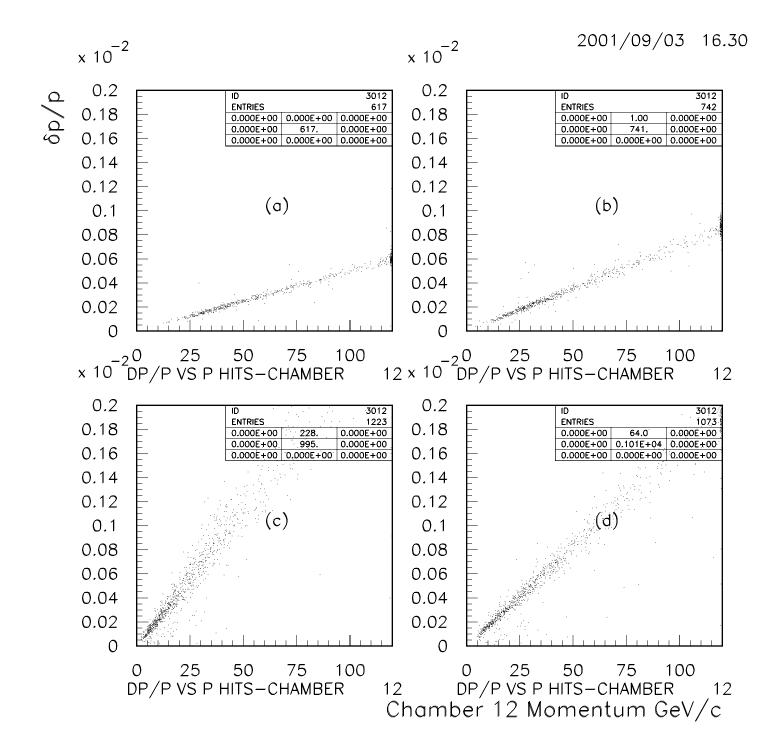


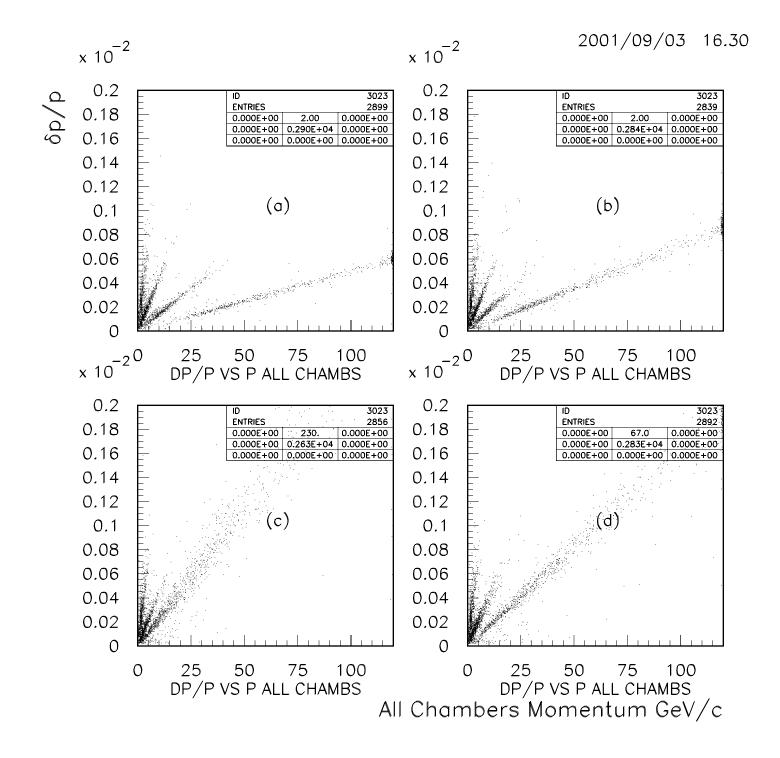


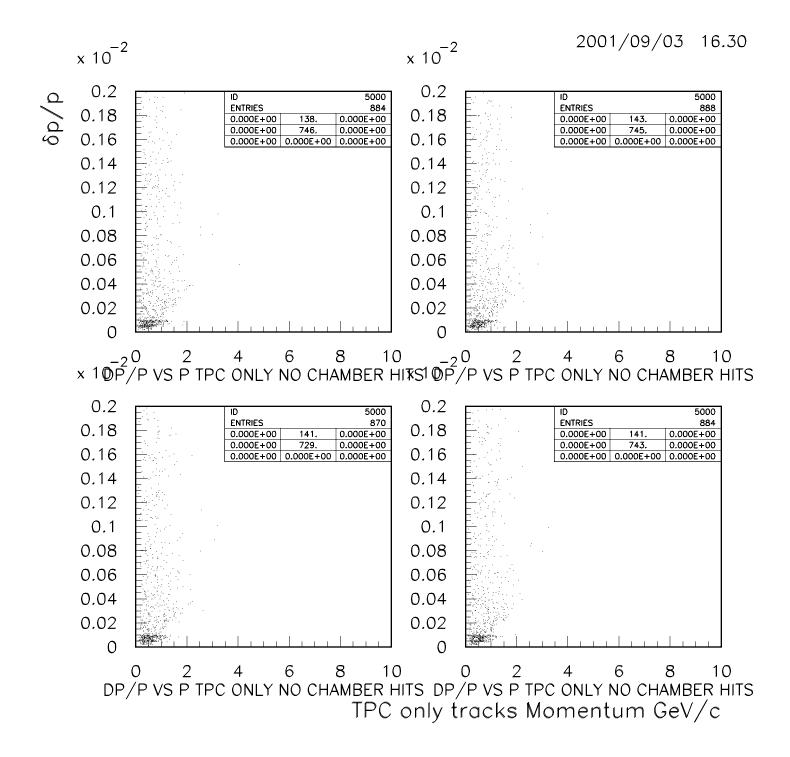












| Chamber | Rosy+1.2T | Rosy+0.6T | Rosy-0.6T | Rosy-1.2T |
|---------|-----------|-----------|-----------|-----------|
| 1       | 1.027E-04 | 1.065E-04 | 1.033E-04 | 1.033E-04 |
| 2       | 9.631E-05 | 9.537E-05 | 9.538E-05 | 9.448E-05 |
| 3       | 5.560E-05 | 6.071E-05 | 6.153E-05 | 6.060E-05 |
| 4       | 5.206E-05 | 5.346E-05 | 5.292E-05 | 5.100E-05 |
| 5       | 4.474E-05 | 4.610E-05 | 4.578E-05 | 4.539E-05 |
| 6       | 4.048E-05 | 3.994E-05 | 4.045E-05 | 3.969E-05 |
| 7       | 2.710E-05 | 0.000E+01 | 2.650E-05 | 3.764E-05 |
| 8       | 2.008E-05 | 2.337E-05 | 3.100E-05 | 3.460E-05 |
| 9       | 1.608E-05 | 1.907E-05 | 1.550E-05 | 2.863E-05 |
| 10      | 1.410E-05 | 1.721E-05 | 2.524E-05 | 3.384E-05 |
| 11      | 6.940E-06 | 9.260E-06 | 1.156E-05 | 1.899E-05 |
| 12      | 5.010E-06 | 7.241E-06 | 2.185E-05 | 1.593E-05 |

## Cutting on Momentum resolution

In order to determine the aperture needed by chambers at particular positions, we employ the following technique. Let us say that a track passes through k chambers before exiting. Then for each chamber i, i=1,k, we associate a quantity called the fractional resolution  $f_i$  where  $f_i$  is defined as the resolution that would be obtained by all chambers preceding chamber i (including the TPC, but not including i) expressed as a fraction of the resolution obtained by all chambers including the last chamber k.

i.e.

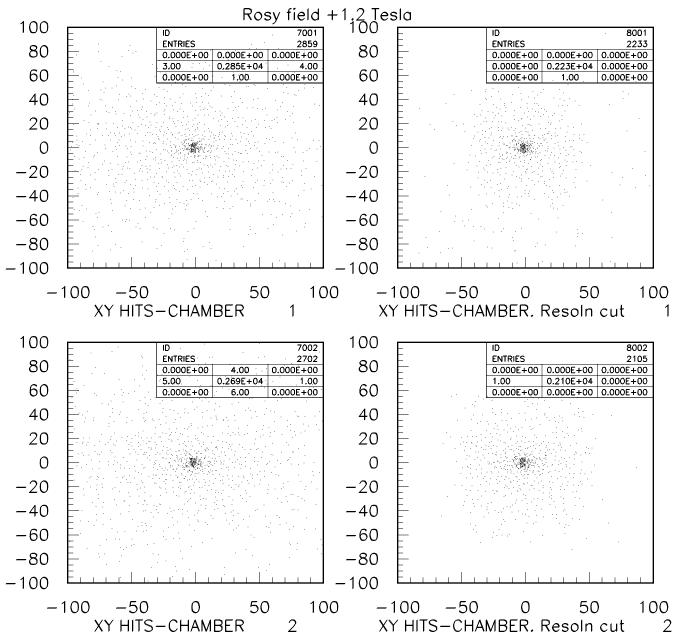
 $f_{i=(resolution of track using all chambers 1-k)/(resolution of track using chambers TPC to chamber i-1)$ 

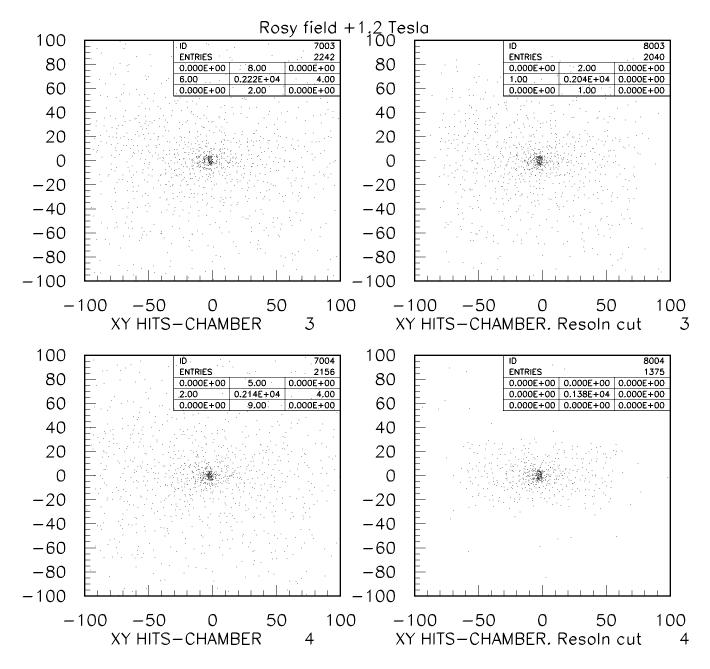
We then plot the x and y position of hits in each chamber for all tracks and compare it with xy plots where the track is not plotted in chamber m if  $f_m$  is greater than a cut off (0.5). This means that the m<sup>th</sup> chamber and the following chambers will add less than 50% more resolution for this track. 50% is a harsh cut and we will want to optimize this further and increase it to say 70% or so. So for each chamber we get two plots. The overall xy distribution and the truncated xy distribution. The truncated xy distribution gives the chamber size at that point.

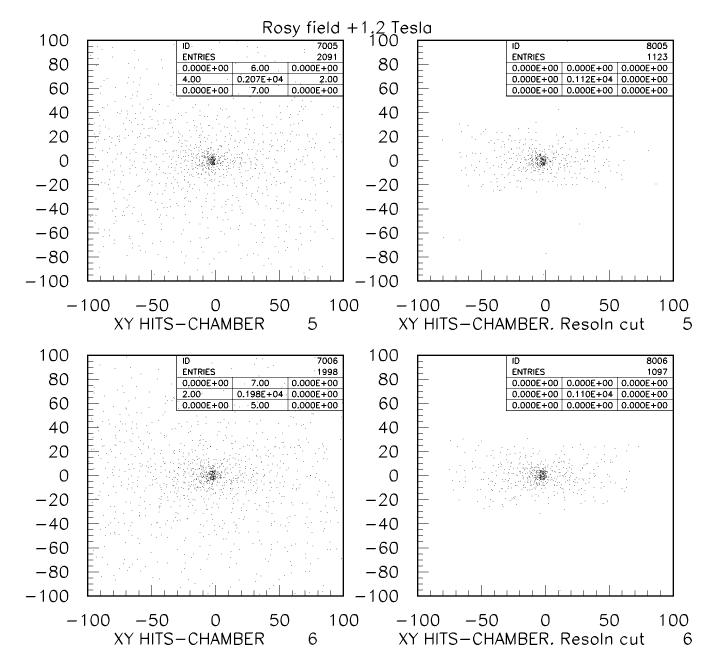
The following figures give such distributions for all chambers for Rosy fields +1.2T and for chambers 7-12 (downstream of ROSY) for ROSY fields +0.6T, -0.6T and -1.2T.

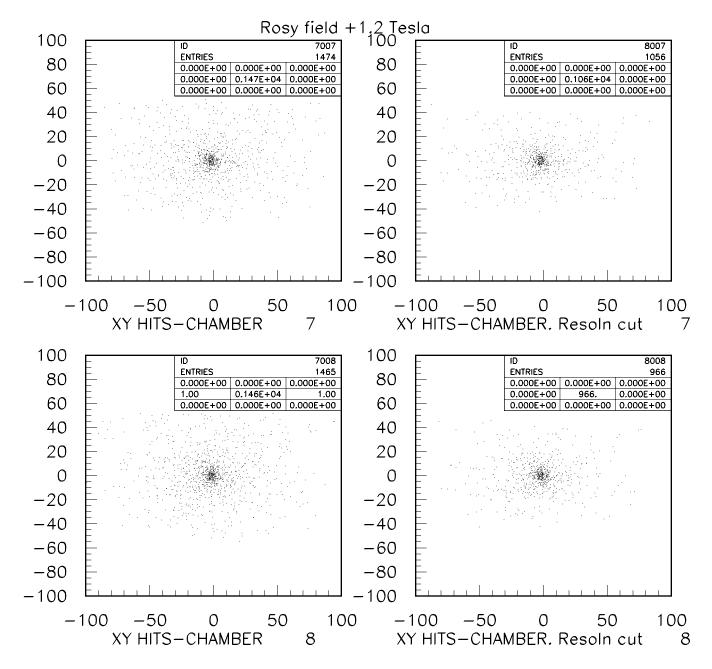
This is followed by a spreadsheet of available chambers.

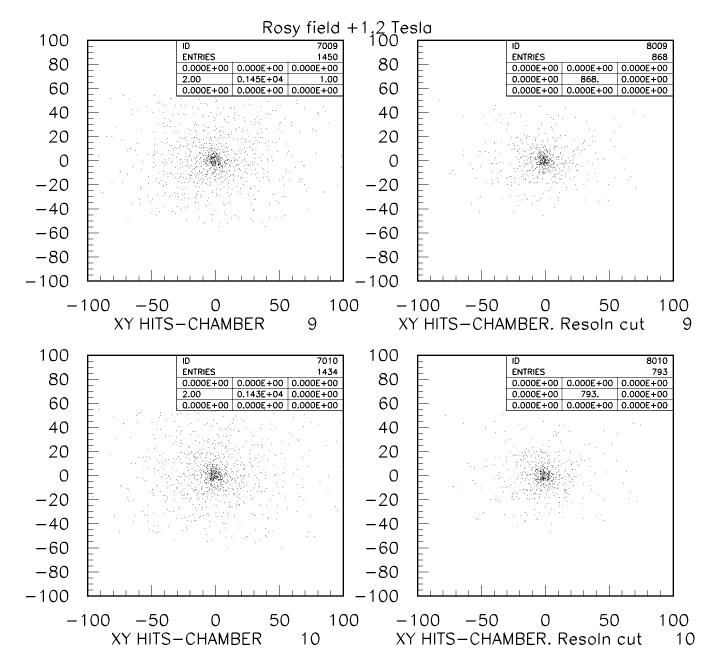
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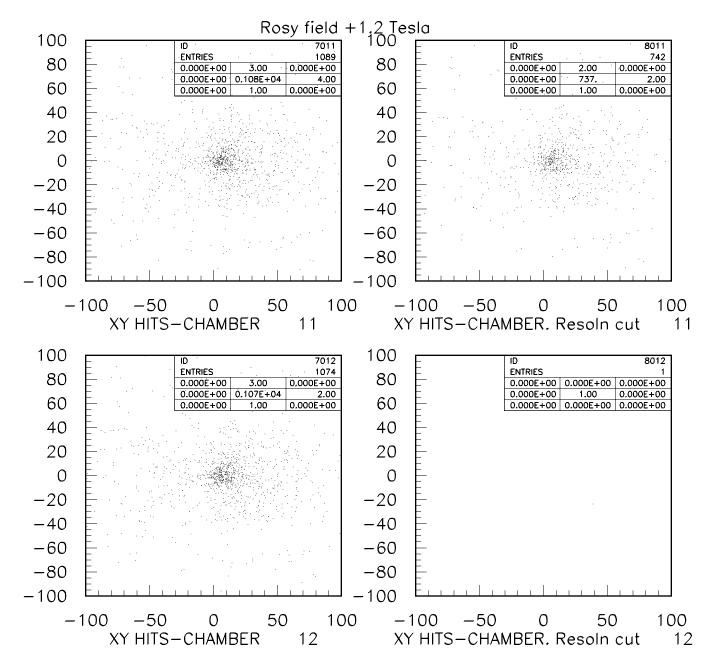


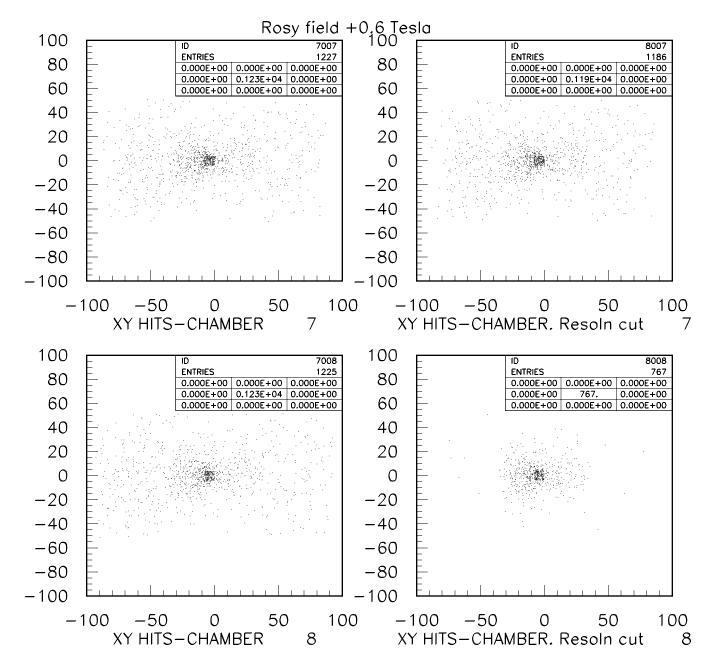


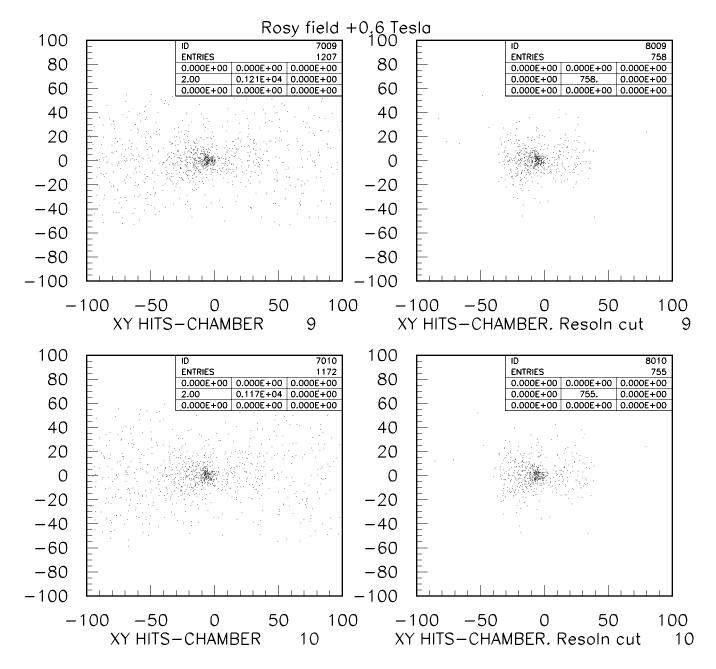


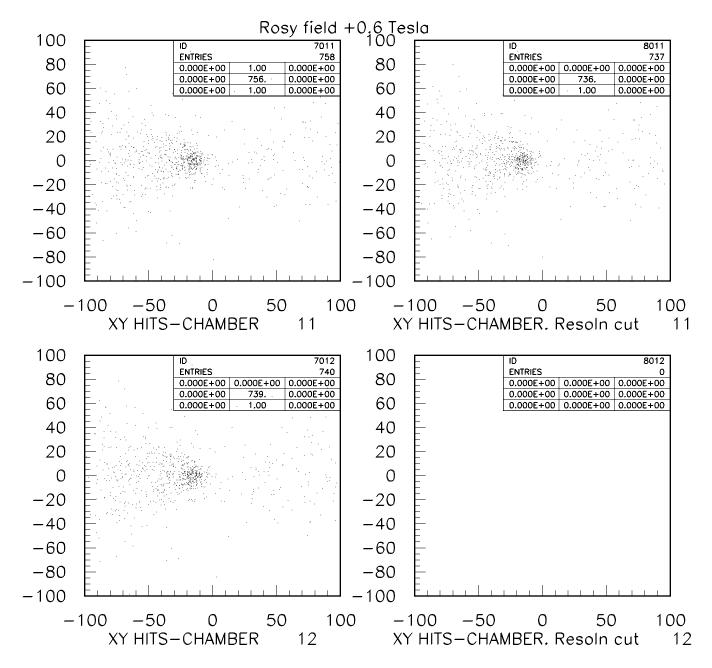


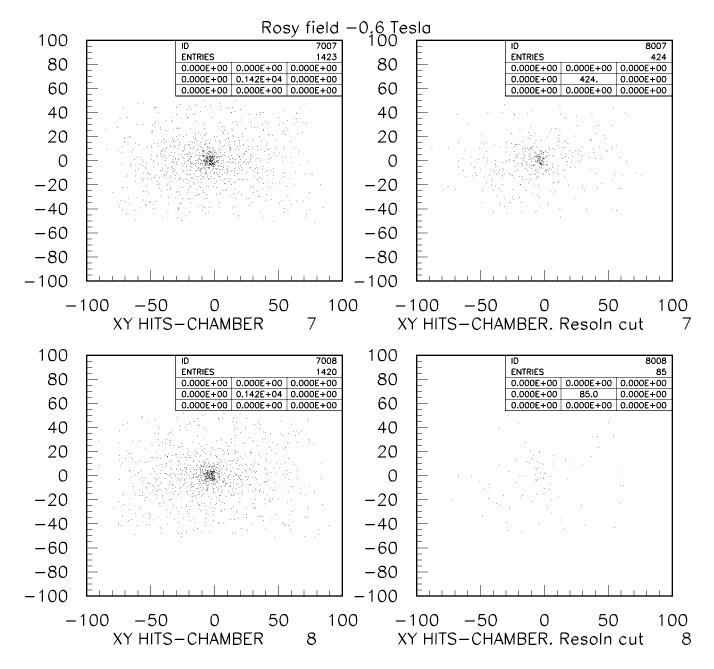




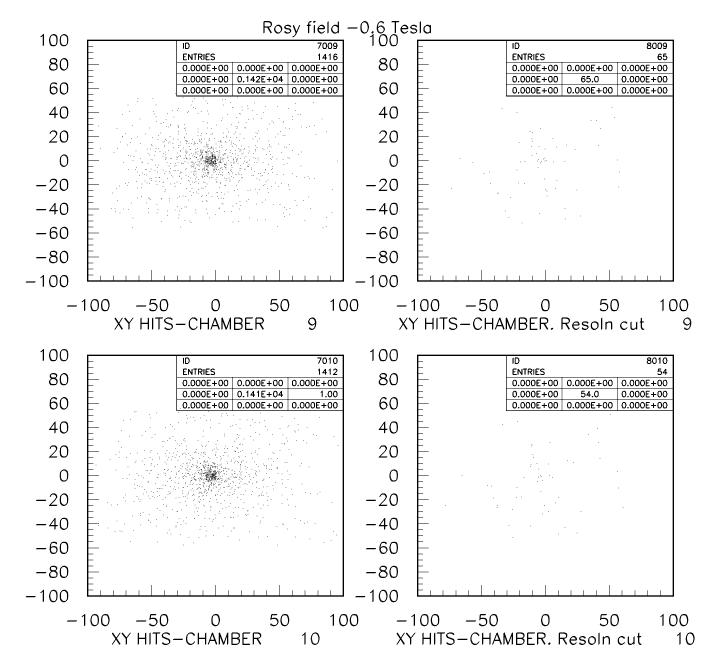




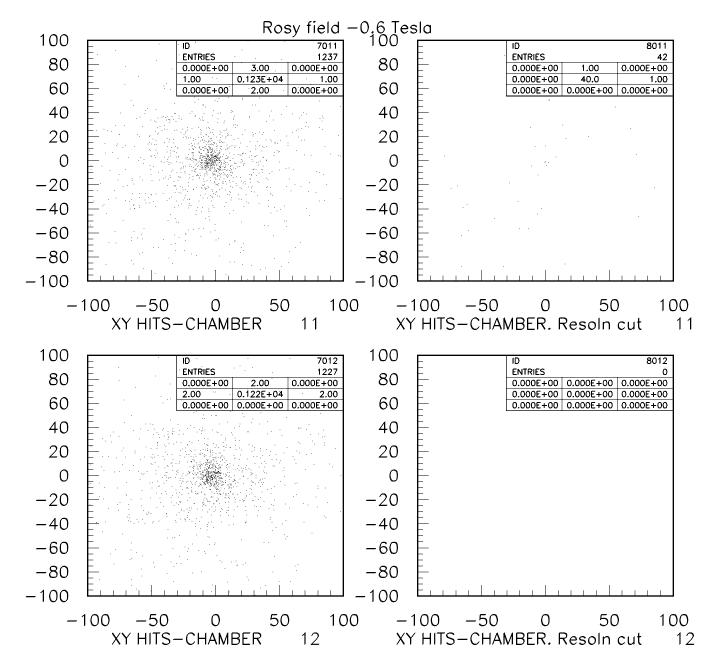


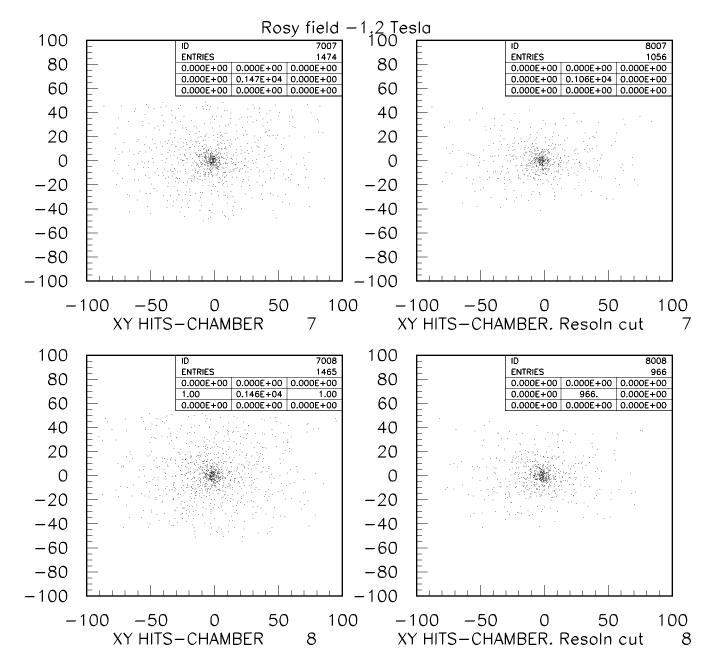


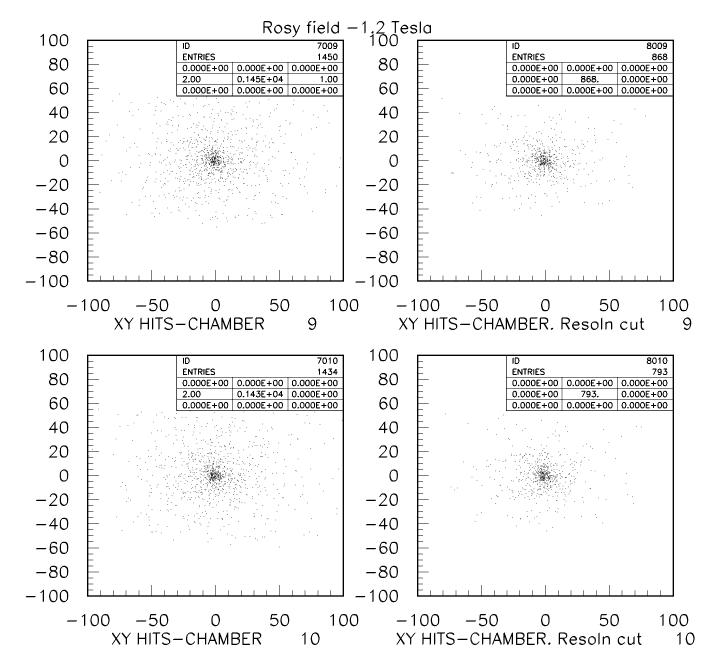
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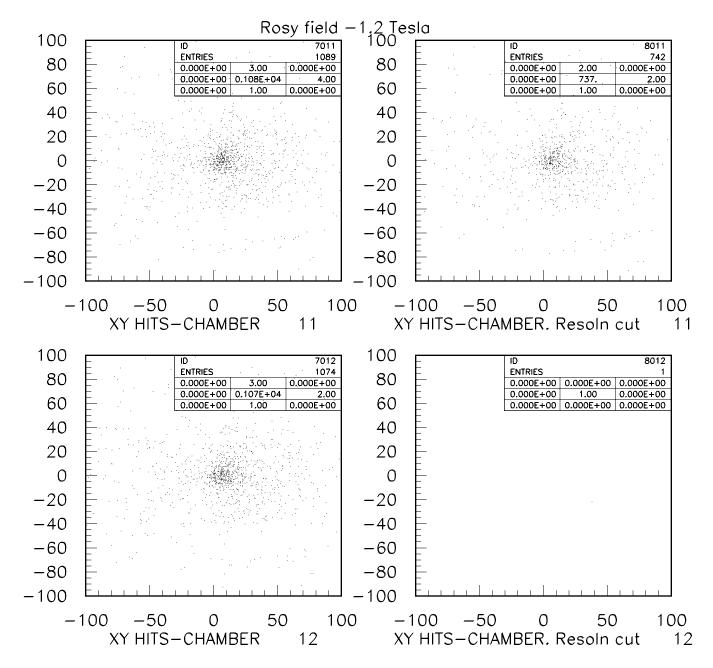


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| experiment chamber type chamber name |                           | x-aperture (cm) y-aper | y-aperture (cm) anode | anode spacing (mm) anode-to-cathode spacing (mm) #planes | ode spacing (mm) #planes | #wires     |                            |                                   |  |
|--------------------------------------|---------------------------|------------------------|-----------------------|--|--------------------------|------------|----------------------------|-----------------------------------|--|
| E687 (Focus) PWC                     | Type I (P0, P3)           | 76.2                   | 127                   | 2.032  | 5.969                    | 4          | 2296 x-y-u-v               | 0,90,101.3,-88.7                  |  |
|                                      | P4'<br>Type II (D1 D2 D4) | 101.6                  | 152.4<br>228.6        | 2 048  | 8 006                    | <b>σ</b> ₹ | 1372 x-u-v<br>2044 x-v-u-v | 0,101.3,-88.7<br>0 00 101 3 -88 7 |  |
|                                      | (1, 1, 1, 2, 1, 1)        | 76.0                   | AE 70                 | 1 08/375   | 2.050                    | + =        | 1626 c-t-u-v               | -21 7 -7 02 +7 02 +21 6           |  |
|                                      | Chamber 2                 | 01 44                  | 50.06<br>60.06        | 1 084375   | 3.0512                   | 1 4        | 1 920 S-t-u-v              | -21 7 -7 03 47 03 40 6            |  |
|                                      | Chamber 2                 | 152 4                  | 101 6                 | 2 175  | 3.0512                   | t <b>z</b> | 1020 s-t-u-v               | -21 7 7 27 03 47 03 401 6         |  |
|                                      | Chamber J                 | 152.4                  | 101.6                 | 2.175  | 3 2512                   | • •        | 1020 s-t-u-v               | -21 7 7 03 47 03 47 03 401 6      |  |
|                                      | Chamber 5                 | 152.4                  | 101.6                 | 3.175  | 3.2512                   | 14         | 1920 s-t-u-v               | -21.77.93.+7.93.+21.6             |  |
|                                      | Chamber 6                 | 182.88                 | 121.92                | 3.4925   | 3.2512                   | 4          | 2048 s-t-u-v               | -21.77.93.+7.93.+21.6             |  |
|                                      | Beam Chamber 1-1          | 15.24                  | 10.16                 | 1.016  | 1.397                    | - 4        | 640 s-t-u-v                | -21.77.93.+7.93.+21.6             |  |
|                                      | Beam Chamber 7-i          | 38.1                   | 20.32                 | 1.524  | 1.397                    | - 4        | 1024 s-t-u-v               | -21.7,-7.93,+7.93,+21.6           |  |
| E871(Selex) MWC                      | m1_pwc_1                  | 220                    | 220                   | ę  |                          |            | n-v-v-x                    | 0,90,+28,-28                      |  |
|                                      | m1_dc1                    | 200                    | 150                   |  |                          |            | ×-×                        | 0'0                               |  |
| MWC                                  | m1_pwc_2                  | 220                    | 220                   | ę  |                          |            | n-v-y                      | 0,90,+28,-28                      |  |
| DC                                   | m1 dc2                    | 200                    | 150                   |  |                          |            | x-x                        | 0,0                               |  |
| MWC                                  | m1 pwc 3                  | 220                    | 220                   | б  |                          |            | n-v-v                      | 0.90.+2828                        |  |
| MWC                                  | m2 pwc 1                  | 93                     | 63                    | 2  |                          |            | х-х                        | 0.90                              |  |
| MWC                                  | m2 pwc 2                  | 93                     | 93                    | 2  |                          |            | х-х                        | 0.90                              |  |
| MWC                                  | m2 pwc 3                  | 93                     | 93                    | 2  |                          |            | n-v                        | +28,-28                           |  |
| MWC                                  | m2_pwc_4                  | 93                     | 93                    | 2  |                          |            | y-x                        | 0'06                              |  |
| MWC                                  | m2_pwc_5                  | 132                    | 93                    | 2  |                          |            | n-v                        | -28,+28                           |  |
| MWC                                  | m2_pwc_6                  | 132                    | 93                    | 2  |                          |            | y-x                        | 90'0                              |  |
| MWC                                  | m2_pwc_7                  | 132                    | 93                    | 2  |                          |            | y-x                        | 90'0                              |  |
| MWC                                  | m3_pwc_1                  | 84.2                   | 84.2                  |  |                          |            | n-x-v-v                    | +28,90,0,-28                      |  |
| MWC                                  | m3_pwc_2                  | 84.2                   | 84.2                  |  |                          |            | y-x                        | 0'06                              |  |
|                                      | m3_pwc_3                  | 135                    | 109.4                 |  |                          |            | y-x-v                      | 90,0,+28                          |  |
| HYPERCP MWC                          | C1                        | 45.72                  | 25.4                  | 1.0  |                          | 4          | 1408 x-x'-u-v              |                                   |  |
| MWC                                  | C2                        | 45.72                  | 25.4                  | 1.0  |                          | 4          | 1408 x-x'-u-v              |                                   |  |
| MWC                                  | C                         | 55.88                  | 30.48                 | 1.25   |                          | 4          | 1408 x-x'-u-v              |                                   |  |
| MWC                                  | C4                        | 55.88                  | 30.48                 | 1.25   |                          | 4          | 1408 x-x'-u-v              |                                   |  |
| MWC                                  | C5                        | 152.4                  | 40.64                 | 1.5  |                          | 4          | 3232 x-x'-u-v              |                                   |  |
| MWC                                  | C6                        | 152.4                  | 40.64                 | 1.5  |                          | 4          | 3232 x-x'-u-v              |                                   |  |
| MWC                                  | C7                        | 203.2                  | 55.88                 | 2.0  |                          | 4          | 4000 x-x'-u-v              |                                   |  |
| MWC                                  | C8                        | 203.2                  | 55.88                 | 2.0  |                          | 4          | 4000 x-x'-u-v              |                                   |  |
| MWC                                  | C9                        | 203.2                  | 55.88                 | 2.0  |                          | 4          | 4000 x-x'-u-v              |                                   |  |